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Galileo Probe Parachute Test Program: Wake Properties of the Galileo Probe at Mach Numbers From 0.25 to 0.95

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Information Division

GALILEO PROBE PARACHUTE TEST PROGRAM:

WAKE PROPERTIES OF THE GALILEO PROBE AT MACH NUMBERS FROM 0.25 TO 0.95

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SUMMARY

The results of surveys of the near and far wake of the Galileo Probe are presented for Mach numbers from 0.25 to 0.95. The trends in the data resulting from changes in Mach number, radial and axial distance, angle of attack, and a small change in model shape are shown in crossplots based on the data. A rationale for selecting an operating volume suitable for parachute inflation based on low Mach number flight results is outlined.

INTRODUCTION

The deployment, inflation, performance, and stability of a parachute in the wake of a payload to which it is attached are frequently sensitive to the velocity gradients of the wake itself. This sensitivity is expected to be particularly great for cases in which the wake diameter is comparable to that of the parachute because the radial velocity gradient is largest at the periphery of the parachute before the parachute is fully open. That is to say, a very small parachute (such as a drogue) may deploy and inflate satisfactorily in a large wake (because only small differences of imposed velocity occur near it), whereas a somewhat larger parachute might inflate slowly or not at all. In contrast, the larger parachute may inflate satisfactorily in the wake of a small payload - the usual configuration employed in parachute development and structural tests. The descent parachute configuration of the Pioneer Venus Large Probe (ref. 1) is believed to have exhibited a "reluctance" to open at Mach numbers above 0.6 both for the system tests in the Earth's atmosphere and for the actual Probe during its flight in the atmosphere of Venus. The rather gradual inflation did not compromise the collection of scientific data in the Venutian atmosphere because no critical events, such as entering a recognized cloud layer, occurred before the altitude for parachute deployment and inflation. In the case of the Galileo Probe (ref. 2), on the other hand, it is most important to deploy and inflate the parachute somewhat earlier, i.e., at higher Mach number, in order to remove the instrumented descent configuration from the aeroshell and permit operation of the cloud-analysis instrument before entering the first clouds in the postulated atmosphere of Jupiter.

During Earth-based flight tests to verify adequate system behavior for the Galileo flight conditions, however, the inflation was achieved at an undesirably low Mach number; once inflation was complete, the performance and stability proved to be the same as the earlier tests and flights. Rather than accept the loss of the scientific data and the risk of even further delayed inflation for the flight in the atmosphere of Jupiter, it was decided to investigate the reasons for the marginal behavior and to seek means to ensure prompt inflation at the desired flight Mach number. In order to relate the anticipated wake-survey data to the earlier experience, tests at conditions spanning those for both Venus and Jupiter were desired. Two types of tests were believed necessary in order to guide decisions on design variations: wake-flow surveys and tests of scale model parachutes. This report describes the wake-flow study and suggests a simple rationale for employing the summary plots derived from the data. Tests of a scale model parachute are reported in reference 3.

TEST EQUIPMENT AND TEST FACILITY

Probe Models

The wakes of two one-eighth-scale models (6-in. diameter) of the Galileo Entry Probe aeroshell were surveyed in the NASA Ames 6- by 6-ft transonic wind tunnel to define the initial operating environment of the descent parachute. The principal configuration represented the expected form of the "ablated" Galileo Probe deceleration-module heat shield. The second configuration represented the "ballasted" configuration to be used in a planned system drop test to verify that parachute deployment, inflation, performance, and stability were satisfactory. The two model profiles are shown in figure 1. In addition to matching the forebody profile for the

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system drop test, the model in figure 1(b) also is essentially the same as that of the Pioneer Venus Large Probe; thus the results from both programs can be directly related. The principal difference between the latter model and the Pioneer Venus Large Probe is the short cylinder between the 45° half-angle cone and the base. In neither case was the form of the afterbody (from the rim of the cylinder aft) made to simulate a real configuration because of the expected insensitivity to the afterbody of the distant wake flow and most of the reverse-flow region. At high Reynolds numbers (above critical for transition), the flow separates at the cone-cylinder junction at subsonic and transonic speed.

The models were affixed to the support structures at a pivot located 0.084 model diameter ahead of the base plane. Thus, when positive angles of attack were set, the center of the model base moved slightly in the direction of negative Z.

The area surrounding the model noses was covered by a fairly densely spaced single layer of glass spheres out to a radius of 0.167 model diameter to assure early transition to turbulent boundary-layer flow. This feature in combination with the nominal test Reynolds number 1.5 million, was used to assure good simulation of full-scale flow. A brief sequence of tests was run at Re_D equal to 3 million and showed no alteration of flow patterns.

Model Supports

Two types of support were used during the tests. All of the data reported herein were obtained with the models supported on the sting-strut assembly shown in figure 2. A few preliminary tests were run with the ablated-form model mounted conventionally on a long slender sting equipped with a fixed rake of five pitot-pressure tubes located 2.6 model diameters from the model base. Tests were conducted with and without the strut in place about 0.3 model diameter from the base. The strut reduced the size of the wake significantly at M = 0.95; therefore, the two-diameter extension sting was installed to reduce the interference. Subsequent surveys with the traversing survey probe described later revealed a wake profile which matched that of the sting-mounted model much more closely. Directly comparable tests using only the five-tube probe were not possible, but it was concluded that support interference was reduced to a degree which would allow accurate determination of data trends with Mach number, distance downstream and angle of attack, and model profile. The strut was stabilized with guy wires to avert possible coupled torsionbending oscillations.

Wake Survey Apparatus

All of the data presented herein were obtained using the pitot-static probe illustrated in figure 3. Included on this

probe were forward- and aft-facing pitot tubes; the forwardfacing tube incorporated a coaxial static-pressure tube as well (four orifices at 0.29 model diameter from its tip). This spacing permitted good determination of flow properties in weak and moderately strong axial pressure gradients. The aft-facing pitot tube was about 1 model diameter downstream of the static-pressure taps, so that strong gradients made interpretation of the data in the reverse-flow region difficult. After completing the far-wake survey, the forward-facing pitotstatic probe was accordingly converted to aft-facing (fig. 3(b)) by bending it through 180°. The orifice nearest the inside of this bend was sealed with epoxy to avoid the strongest aerodynamic effects of the bend. Even with this alteration, the strong pressure gradients in the reverse-flow region required that the separation between pitot and static orifices be recognized in obtaining the data. This was accomplished by traversing the probe in increments of 1.75-in. (0.29 model diameter) and using the measurement in adjacent test sequence points to obtain spatially coincident measurements of pitot and static pressures.

The same procedure can, in effect, be achieved with the far-wake results by interpolation of the static-pressure data to obtain coincident determination of the pressures; this has not been done in reducing the data because the gradients there are an order of magnitude less severe than in the reverse-flow region.

Pitot and static-pressure measurements made using probes of this sort are degraded if the local flow is highly inclined (more than 10°) relative to the tube axis. Since this degradation is small for angles less than about 10°, the only regions in the wake where errors are expected to be large are well removed from the axis in the near wake. Approximate numerical analysis of the wake profiles downstream of the model by more than 5 model diameters indicated that radial inflow into the accelerating wake resulted in inclinations of less than 3°. Unsteadiness of the flow in the wake doubtless interfered with the static-pressure determination; since the goal of the present surveys was to determine the qualitative influence of Mach number, position, and angle of attack on dynamic-pressure distribution, the small and slowly changing bias on the static-pressure measurement was ignored in studying the data.

The pitot-static probe was located at the tip of the short radial arm so that as the survey assembly was rolled, the probe moved to the left or right to survey at positions other than the vertical plane of symmetry. The location of the roll mechanism is indicated in figure 4.

Vertical positioning of the survey probe was accomplished by translating the wind tunnel model-support body of revolution (BOR) by simultaneous operation of its two positioning screws. Streamwise positioning of the survey probe was effected by means of the linear-actuator mechanism connected between the probe arm and the roll mechanism. The maximum extension range of the linear actuator was slightly less than 4 model diameters; it was therefore necessary to position the model-support strut at several stations along the test-section ceiling to achieve the full streamwise array of surveys desired.

Deflections of Survey Apparatus

As noted above, the entire survey apparatus was cantilevered from a large floor-to-ceiling strut located in the entrance to the wind tunnel diffuser. The maximum cantilever length is approximately 12 ft. Late in the test program it was discovered that aerodynamic loads deflected the apparatus upward by an amount that is believed to be influenced by extension length, dynamic pressure, Mach number, roll position, and position relative to the model's wake. Additionally, backlash in the vertical-positioning drive may have yielded a small irregularity in vertical position, although calibration tests without airflow revealed no such effect greater than about 0.5% of the model diameter. The aerodynamic deflection, on the other hand, produced in one case a deflection of at least 8% of the model diameter. As far as could be determined, this deflection was nearly constant for a given test condition and streamwise position of the survey probe (axial and roll), so that the shapes of the vertical profiles of dynamic pressure, Mach number, etc., were preserved, but the absolute position of the survey probe relative to the model axis was not accurately known. From a study of the flow-profile plots, the effect of the elastic deflection can be seen to yield a "movement" of the wake progressively in the +Z direction as the dynamic pressure increased; i.e., increasing Mach number at constant Reynolds number. A similar lateral deflection may have occurred as well, but observation was not possible.

Interpretations of the profiles of flow properties were therefore based on the assumption that vertical deflection was constant throughout any one run, i.e., vertical traverse. Also, where effects of angle of attack were under study, it was assumed that deflection was independent of angle of attack.

TESTS

Most of the test period was spent obtaining the complete survey of the static and pitot pressure variations in the wake of the "ablated" model configuration supported on the strut. The matrix of test conditions and survey points is detailed in table 1. The abbreviated test matrix for the second, i.e., "ballasted," model consists of runs 333 through 335. In this listing an entry is made in a column only at the run at which that parameter is changed. The special tests, designed to reveal the extent of support interference on the nominal wake properties, are not included.

The test sequence was dictated by the most efficient use of tunnel time, except that the special support interference study was accomplished first to obtain early assurance that support interference would not be excessive.

While the test airflow conditions were being established, the survey apparatus was maneuvered into the desired position: for height, Z, by raising the BOR conventionally used for model support, for lateral position, Y, by rotating the roll positioner on the BOR and extending the survey apparatus linear actuator to the desired streamwise position, X. Each run thereafter consisted of a vertical traverse to all the points at which measurements were needed.

Succeeding runs were made at the remaining lateral positions desired for the same axial station before moving to the next axial station. Once the three linear dimensions had been adequately surveyed, the next Mach number was established and the desired spacial survey was completed. The time required to position the survey probe was sufficient to assure equilibration of the pressure sensors without additional delay.

The only occasions requiring breaks in the wind tunnel operation were those to adjust the streamwise location of the model-support strut and its guy wires, adjust the angle of attack of the model (by rotation about the pivot inside the model), or exchange the ablated model for the ballasted model. At each such break in the testing, the glass-bead boundary-layer trip area was inspected and refurbished as needed.

RESULTS

All of the wake-survey results for both the ablated and ballasted configurations supported on the short sting with strut are provided in table 2. Table 2 has been subdivided into four sections. Sections 2a and 2c present data for the ablated model shape with the pitot-static probe facing forward. Section 2b presents data for the ballasted model profile, and section 2d presents data for the ablated shape with the pitot-static probe facing aft. Data were taken at Mach numbers of 0.25, 0.60, 0.80, 0.85, 0.90, and 0.95 at a Reynolds number of 0.75 million based on model diameter. The pitot-static surveys yielded profiles of Mach number, dynamic pressure, velocity, and static pressure as functions of vertical position relative to the horizontal axis of the small sting at selected lateral positions and several axial stations between 1 and 11 model diameters downstream from the model base.

Definitions of column headings are presented in table 2. To preserve direct accountability of the table, the actual run numbers and order of table 1 may facilitate rapid location of a desired test listing. Gaps in the number sequence represent runs made at a Mach number of 1.1; these runs were deleted because of serious disturbance of the flow by the normal-shock wave upstream of the linear actuator of the survey system. A few unexplained anomalies have been observed in individual sequence (i.e., data-point) listings. These anomalies have not been deleted.

Selected groups of runs have been plotted and crossplotted in figures 5 through 8 to reveal the shape, Mach number, distance, and angle-of-attack effects on the properties of the wake. In these plots attention is concentrated on the variation of the ratio of local dynamic pressure to freestream dynamic pressure. Other parameters, such as velocity or pitot pressure, may be as meaningful in applying the results for various purposes. Sufficient information is tabulated so that such plots may be constructed.

All of the tabulated results, with the exception of runs 367 through 390, are presented with no post-test alteration. These exceptions are the tests made with the modified (reversed by a 180° bend) pitot-static tube. In these tests, very strong axial gradients resulted in a large static pressure difference between the positions of the pitot and static pressure orifices. Therefore, the X increment used in these tests was selected so that the static pressure determined at a particular sequence point could be used with the pitot pressure obtained at the previous sequence point. The tabulated data have been treated in this manner.

With considerable effort the same kind of correction can be applied to the data from surveys at 3.5 model diameters, and farther, behind the base. There is little to be gained, however, because the pressure gradients are an order of magnitude less severe than in the reverse flow near the model base.

DISCUSSION OF RESULTS

Far-Wake Region

The momentum defect in the wake of a simple nonlifting body is directly equivalent to the drag of the body. The wakes of the two aerodynamic models used in this study illustrate that the ballasted model has slightly less drag than the more bluff ablated model used in most of the tests. The profiles of dynamic pressure (fig. 5) show a smaller loss in the wake core of the ballasted model than in the wake core of the ablated model. The extent and precision of the surveys in this study are not sufficient to determine the absolute drag coefficients with great accuracy, but the difference is clear. While the two configurations showed only modest differences in dynamic pressure loss (and gradients of dynamic pressure), much greater changes were observed for the ablated model as Mach number and distance from the model to the survey station were changed. The lower portion of each part of figure 6 illustrates the rapid increase of dynamic pressure in the wake core as the survey station is moved downstream from the wake stagnation point -0 dynamic

pressure. Even as far downstream as 11 model diameters, the continued recovery toward free-stream conditions is clear.

This acceleration of the wake core is achieved at the cost of deceleration of the airflow immediately outside the wake; at all times the total loss in momentum flux must represent the model drag. This redistribution of momentum is summarized in the contour plots of constant dynamic pressure presented in the upper portions of figure 6. At some distance downstream of the body, probably about 6 model diameters from the base, the profiles become "similar." That is, when normalized to the maximum loss in velocity at the core and to the local wake diameter, the profile plots will remain unchanged. Once similarity is established, the radial gradients are seen to vary as the 1.5 power of the maximum loss at the core.

The Effects of Angle of Attack

The total drag of bodies like those tested in this study is quite insensitive to angle of attack, for angles of attack very much less than the body cone half angle; therefore the total change in loss of momentum in the wake was correspondingly slight as angle of attack increased to 20° . The generation of even a modest lift force, however, results in the discharge of a trailing vortex system which rolls up into a vortex pair at great distances downstream. This vortex system causes the wake to move in a direction opposite to that of the lift vector. This deflection of the wake is the most prominent feature in the vertical profiles of dynamic pressure ratio at angles of attack of both plus and minus 10° and 20° (fig. 7). The surveys revealed no further major changes in the dynamic pressure profiles.

Reverse-Flow Region

In deploying the Galileo Probe parachute, it is necessary first to propel a small drogue through the near wake of the probe (where the flow moves toward the base). Further, the drogue must then remove the afterbody heat shield and drag it through the volume of reverse flow before the main parachute can be drawn aft in turn. In order to permit estimation of the performance requirements placed on the drogue, the reverse-flow region was surveyed in detail using the modified pitot-static probe (runs 367 through 390). These data are summarized as contour plots of dynamic pressure in figure 8.

The length of the reverse flow increases significantly as Mach number increases from 0.25 to 0.95. The relative severity of the reverse flow, on the other hand, diminishes.

The dynamic pressure profiles deduced (from crossplotting the data) to act along the axis of the flow core are shown in figure 8.

APPLICATION OF RESULTS TO DESIGN OF GALILEO PROBE PARACHUTE CONFIGURATION

Experience with the Pioneer Venus Large Probe (ref. 1) and with the System Drop Test Configuration for the Galileo Probe (ref. 2) suggested a "reluctance" to inflate at Mach numbers above 0.60. In these cases the parachutes were deployed at approximately 5.5 Probe diameters behind the Probe base. The present data indicate that at this location and flight speed the loss of dynamic pressure near the wake core was severe and the wake diameter was comparable to that of the parachute itself. It is believed that these features combined to cause poor inflation. The result of increasing the Mach number was to aggravate the loss of dynamic pressure and increase the wake size. A slight aggravation was noted when the blunter shape of the Galileo (ablated form) was substituted for that of the Pioneer Venus Large Probe. In order to promote satisfactory parachute inflation for the more severe Galileo requirements, it is necessary, therefore, to find that region in the wake which appears to be more conducive to reliable inflation than that for the Pioneer Venus case at Mach 0.60.

The mixing of external-flow air with the wake is found to produce a rapidly improving wake profile with increasing distance downstream. A comparison of the appropriate profiles suggests that proper parachute inflation can be achieved for the Galileo at a Mach number of 0.80 by incorporating only a modest increase in deployment distance.

CONCLUSIONS

The wakes of the Galileo Probe and a system drop test configuration have been surveyed to determine the variation of flow properties between the model base and a station almost 11 model diameters downstream.

It was found that (compared to the Pioneer Venus Large Probe) the wake of the more bluff configuration (the shape representative of the expected ablated heat shield after entry into Jupiter) had slightly larger dynamic pressure losses and that the severity of these losses increased markedly with Mach numbers from 0.25 to 0.95. Further, it was found that entrainment of adjacent air monotonically increased the wake size and the dynamic pressure in the core.

It was also found that the length of the reverse-flow region immediately downstream of the model increased slightly with increasing Mach number whereas the relative severity of the reverse flow diminished substantially.

A simple rationale was described whereby a region in which a parachute might be expected to inflate at high speed may be identified based on successful parachute operation at lower speed.

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Mach Run Mach Run X/D_B X/D_B Y/D_B Y/D_B Alpha Alpha No. No. No. No. 0.95 0.02 194 0.95 8.5 -0.45 +20144 7.0 0 195 10.9 145 8:5 -0.44 0.90 0 146 0 196 0.90 8.5 147 0.44 197 0.85 10.9 ¥ ¥ 8.5 0.80 7.0 0 198 0.85 148 -0.44 199 0.80 10.9 0.41 149 8.5 150 0 200 0 ¥ 151 ¥ 0.44 201 -0.38 -0.48 0 202 152 0.60 7.0 8.5 0.43 8.5 -0.44 203 153 154 0 204 0 0.44 205 -0.36 155 156 0.95 -0.39 206 -0.45 157 0 207 0.60 10.9 0.41 0.43 208 0 158 -0.38 159 10.5 0.41 209 210 -0.48 160 0 211 8.5 0.43 161 -0.38 162 -0.48212 0 163 10.0 0 213 -0.36 0.45 0.80 10.9 0.41 214 164 10.9 165 0 215 0.25 0.41 -0.38 0 166 216 -0.48 217 -0.38 167 168 10.0 0 218 -0.48 219 0.43 169 0.60 10.9 0.41 8.5 0 220 0 170 -0.38 171 221 -0.36 172 -0.48 222 -0.45 0 223 0.95 10.9 0.41 -20 173 10.0 174 0.90 10.9 224 0 175 0.90 0.85 225 -0.38 0.85 0.85 226 -0.48 176 177 0.85 10.9 227 8.5 0.43 178 0.25 0.41 228 0 179 0 229 -0.36 -0.38 180 230 -0.45 0.90 10.9 181 -0.48 231 0 182 10.0 0 232 0.90 8.5 7.0 0 233 0.85 10.9 183 8.5 -0.45 234 0.85 8.5 184 235 0.80 10.9 0.41 185 0 0.43 236 186 ¥ 0 0 187 0.95 10.9 0.41 +20 237 -0.38 188 0 238 -0.48 239 189 -0.36 8.5 0.43 -0.48 240 190 0 0.43 -0.36 191 8.5 241 -0.45 192 0 242 ᡟ 193 ¥ -0.36 243 0.60 10.9 0.41

TABLE 1.- TEST CONDITION LISTING

Run Mach Run Mach X/D_B Y/D_B X/D_B Y/D_R Alpha Alpha No. No. No. No. 0 294 0.25 -0.45 +10244 0.60 10.9 -20 8.5 -10 -0.38 295 0.95 10.9 0.41 245 246 -0.48 296 0 -0.38 247 8.5 0.43 297 298 -0.48 248 0 249 -0.36 299 8.5 0.43 250 -0.45 300 0 251 0.25 10.9 0.41 301 -0.36 252 302 -0.45 0 -0.38 303 0.90 10.9 253 0 8.5 254 -0.48 304 0.90 255 8.5 0.43 305 0.85 8.5 0 306 0.85 256 10.9 257 -0.36 307 0.80 0.41 -0.45 258 308 0 259 0.95 10.9 0.41 +10309 -0.38 260 0 310 -0.48 -0.38 8.5 0.43 261 311 262 -0.48 312 0 263 8.5 0.43 -0.36 313 264 -0.45 0 314 -0.36 265 315 0.60 10.9 0.41 -0.45 266 316 0 267 0.90 10.9 0 317 -0.38 8.5 -0.48 268 0.90 318 10.9 269 0.85 319 8.5 0.43 8.5 ¥ 270 0.85 320 0 271 0.80 10.9 0.41 322 -0.45 272 0 323 0.25 10.9 0.41 273 -0.38 324 0 274 -0.48 325 -0.38 275 -0.48 8.5 0.43 326 8.5 0.43 276 0 327 -0.36 277 328 0 278 -0.45 329 -0.36 279 0.60 10.9 0.41 330 -0.45 280 0 333 0.95 5.5 0 0 -0.38 281 334 0.80 282 -0.48 335 0.25 283 8.5 0.43 340 0.95 3.5 284 0 341 5.5 0.44 285 -0.36 342 0 286 -0.45 343 -0.44 287 0.25 10.9 0.41 344 7.0 0 288 0 345 0.90 7.0 289 -0.38 346 5.5 290 -0.48 347 3.5 291 8.5 0.43 7.0 349 0.85 292 0 350 5.5 ł 293 -0.36 351 3.5

TABLE 1.- CONTINUED

Run No.	Mach No.	X/D _B	Y/D _B	Alpha	Run No.	Mach No.	X/D _B	Y/D _B	Alpha
352	0.80	3.5	0	0	372	0.90	0.25	0	0
353	1	5.5	0.44		373		0.40		1
354			0		374	₩	0.50		
355		♥	-0.44		375	0.85	0.17		
356	♥	7.0			376		0.25		
357	0.60	7.0	•		377		0.40		
358		5.5	0.44		378	♥	0.50		
359			0		379	0.80	0.17		
360		♥	-0.44		380		0.25		
361	🕈	3.5	0		381		0.40		
362	0.25	3.5	0		382	♥	0.50		
363		5.5	0.44		383	0.60	0.18		
364			0		384		0.25		
365		♥	-0.44		385		0.40		
366	♥	7.0	0		386	♥	0.50		
367	0.95	0.17			387	0.25	0.18		
368		0.25			388		0.25		
369		0.40			389		0.40		
370	♥	0.50			390	♥	0.50	♥	•
371	0.90	0.17	*	*					

TABLE 1.- CONCLUDED

TABLE 2.- MEASURED WAKE PROPERTIES

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	Heading Definitions
Run:	Serial number within the test program.
Test P TN:	Identifier for the entire test program.
CONF:	Configuration of model and support system.
5	Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section; forward-facing pitot-static probe. (Sections 2a and 2c.)
6	Ballast-profile model supported as in 5. (Section 2b.)
7	Ablated model supported as in 5, except that pitot-static probe is bent to face downstream. (Section 2d.)
Mach:	Mach number in free-stream wind tunnel flow.
RN/L:	Reynolds number per unit length (1 ft) in free-stream flow.
PT:	Pressure in stagnation chamber upstream of wind tunnel test section, pounds per square foot.
Q:	Dynamic pressure of wind tunnel free-stream airflow. Q = 0.7 $M^2 \times P$, pounds per square foot.
P :	Static pressure of wind tunnel free-stream airflow, pounds per square foot.
TT:	Temperature of air in stagnation chamber of wind tunnel, °F.
Alpha:	Inclination of model axis to an intersecting line parallel to the free-stream direction.
Seq:	Serial number of data record within run.
X/DB:	Distance from model base to streamwise station of pitot orifice on pitot-static tube, diameters of model base.
Y/DB:	Horizontal component of distance from axis of short sting to pitot orifice on pitot static tube, diameters of model base.
Z/DB:	Vertical component of distance from axis of small sting to pitot orifice of pitot-static probe, diameters of model base.
MF/M:	Ratio of Mach number determined from measured pitot and static pressures on the pitot-static probe to Mach.
MA/M:	As above, but using the pressure acting on the aft-facing pitot probe.
QF/Q:	Ratio of dynamic pressure acting on pitot-static probe to the free-stream dynamic pressure.
QA/Q:	As above, but using the pressure acting on the aft-facing pitot tube.
VF/V:	Ratio of air velocity deduced from pitot-static tube to free-stream velocity.
VA/V:	As above but using aft-facing pitot tube.
CP:	Static pressure acting on pitot-static probe minus free-stream static pressure, all divided by free-stream dynamic pressure. $CP = (PF - P)/Q$.
PF:	Static pressure acting on static pressure orifices of pitot-static probe, pounds per square foot.
PF/P:	Ratio of static pressure acting on pitot-static probe to free-stream static pressure.

Table 2(a)

Configuration 5 – Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section: forward-facing pitot-static probe.

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	0 E / D	1.013	1.009	1.004	0.993	165.0	0.988	C. 530	0.973	0.974	112.0	0.979	0.986	9999. C	1.019	1.029				pF/0	1.021	1.013	1.009	1.000	0.596	0.993	0.992	0.986	0.988	0.586	0.984	3.588	1.004	1.021	- 00 -
	C D	0.021	0.015	0.005	-0.012	-0.014	-0.020	-0-031	-0-043	-0-041	-0.036	-0.033	-0.023	-0.002	0.030	0.046				C P	0.033	0.021	0.015	100.0	-0.006	-0.012	-0.012	-0.022	-0.019	-0.023	-0.025	610.0-	0.006	0.033	
	V A /V	•																		V A /V															
ALPHA	DA/U VF/V	0.905	0.936	0.933	0.909	0.883	0.849	0.323	0.805	0.793	0.776	0.801	0.347	0.946	0.980	116.0			0.00	0A/Q VF/V	0.976	0.981	0.969	0.914	0.894	0.830	0.854	0.836	0.332	0.842	0.856	0.884	0.946	0.976	
11	0F/0	0.804	0.865	0.853	0.796	0.744	0.679	0.628	0.594	0.574	0.549	0.590	0.674	0.877	6.973	0.962	ŢŢ		1.01	0F/0	0.963	0.969	0.937	0.811	0.768	6:1.0	0.691	0.654	0.648	0.663	0.688	0.744	0.881	C.964	1 1 1
<u>ר</u> מ מ	N A N																0		585	NV VN															
5 K C	MF/W	158 * 0	c. 926	C- 922	C.895	0.866	0.829	C-800	0.781	0.767	c.75C	0.776	C.827	0.937	(.977	C.967	Ċ.		242.0		0.972	C.978	0.964	0.901	0.878	0.863	0.834	0.814	0.810	C.829	0.836	0.868	0.937	0.972	
L PT 687	Z/DB	-2.02	-1.52	-1.01	-0.68	-0.52	-0.35	-0.18	-0.01	0.15	0.32	0.48	0.65	0.99	1.45	1•95	La l		0 001	Z/CB	-2.03	-1.52	-1.03	-0-65	-0.52	-0.36	-0.19	-0.02	0.14	0.31	0.48	0.64	0.58	1.49	
H RN/	Y/08	0.02	0.02	C• C2	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	C- C2	0.02	0.02	H RN/		16.1 4	۲/ <u>۳</u> .	-0-44	-0-44	-0-44	- C • 44	-0-44	- 6 - 6 - 0 -	- 64 - 6-	-0-44	-0-44	-0-44	-0-44	-0-44	-0-44	-0-44	
F NAC	X / 0B	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	7.04	N N U	C C	9 1 • 9 4	X/CB	8.49	8.49	E.49	8.49	8.49	E. 49 .	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	
TST P IN CONF	MACH Q	0.948 242.6	0.948 242.6	0.947 242.2	0.948 242.7	0.948 242.7	0.948 242.7	0.948 242.7	0.948 242.7	0.948 242.7	0.947 242.2	0.947 242.2	0.947 242.2	0.947 242.2	0.947 242.2	0.948 242.7	TST P IN CONF			MACH C	0.949 242.5	0.947 241.6	0.948 242.6	0.947 242.1	0.947 242.1	0.947 242.1	0.947 242.1	0.947 242.2	0.947 242.2	0.946 241.7	0.946 241.7	0.946 241.7	0.947 242.2	0.948 242.7	
RUN	SEC	H	~	m	4	ŝ	9	•	ω	σ	0	11	12	E1	14	12	NNA	1 4 5		SEG	م سو	2	m	4	ŝ	v	-	ω	σ	10		12	13	14	

						٠		•																												
		pF/D	1.009	1.010	1.000	0.996	0.593	166.0	0.989	0.586	0.585	0.583	0.987	065.0	1.002	1.021	I.02€			DE /D		1.014	1.010	1.008	1.002	1.000	165.0	0.994	0.588	0.987	0.985	0.586	0.987	0.997	1.018	1.026
		СÞ	0.014	0.015	0.001	-0.007	-0.011	-0.014	-0.018	-0.023	-0.023	-0.027	-0.020	-0.017	0.003	0.034	0.042			60		0.022	0.016	0.013	0.003	-0.001	-0.005	-0.009	-0.018	-0.020	-0.023	-0.022	-0.021	-0.005	0.028	0.041
		V A /V																		V V V V	~ ~ ~ ~															
PHA	• 00	VLA DI	0.909	0.938	0.936	0.911	0.835	0.871	0.841	0.840	0.820	0.824	0.821	0.346	0.924	0.975	0.978	рнд	00			0.982	0.934	0.977	0.940	0.947	0.950	0.931	0.912	0.901	0.389	0.891	0.918	0.967	0.984	0.979
AL	4 0	0 0	7	0	8	¢.	6	0	4	0	ŝ	0	8	m	~	-	5	۷	0			2	5	\$	~	0	4	1	2	5	õ	4	60	17	30	5
TT	70.	QF/	0.80	0.87	0.85	0.80	0.74	0.72	0.66	0.66	0.62	0.63	0.62	0.67	0.83	0.96	16.0	L L				16.0	0.97	0.95	0.86	C-8E	0.88	0.84	0.79	0.77	0.75	0.7	0.80	0.92	0.98	6.0
٩	384	MVVW																C.	300																	
ى	243.5	NF/N	0.895	0.928	0.926	C.858	0.868	0.852	C.819	0.819	0.756	0.801	0.798	0.825	0.912	C.970	0.975	U	21.7		211	0.979	C.9 82	0.974	C.930	0.938	0.942	0.920	0.895	0.887	0.872	0.874	0.906	0.961	136.0	276-0
ЪТ	688	2/08	2.02	L • 53	L•02	0.69	0.53	0.36	0.19	0.02	0.15	0.31	0.48	0.64	0.98	1.48	1.98	Ld	00.	α α α α α α α	20/7	2.03	1.52	1.02	0.69	0.52	0.36	0.19	0.02	0.14	15.0	0.48	0.65	0.98	1.48	1-98
RN/L	1.478	VDB 1	0.00	- 00.0	0.00 -1	0.00 -(0.00 -(0.00 -()- 00.0	0.00 -(0.00	00.0	00-00	00.00	00.00	0.00	0.00			I - 4 - I	A / LE	0.44 -	0.44 -	0.44 -	0.44 -	0.44 -	0.44 -	0.44 -	0.44 -	0.44	0.44	C.44	C - 44	0.44	0.44	0-44
NACH	0.952	X/CB	8.49 (8.49 (8.49 (8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49			166.0	X/LB	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8-49
TN CONF	66 5	G	243.5	244.0	243.5	244.0	244.0	244.0	243.5	243.5	244.0	244.0	244.C	243.5	243.0	243.0	242.7	CINE CINE		1 0 0 1 0 0	3	243.5	243.5	244.C	243.5	243.5	243.5	244-0	243-5	243.5	244.0	244.0	243.5	243.5	243.5	0 846
TST P	571 1	MACH	0.952	0.954	0.952	0.953	0.953	0.953	0.951	0.951	0.952	0.952	0.952	0-950	0.949	0.949	0.948	1 171	1	115	MACH	0.951	0.951	0.953	0.952	0.952	0.952	0.953	0-951	0.951	0.952	0.952	0.951	0-951	0.951	070 0
RUN	146	SEG	, 	2	~	4	ŝ	40	-	æ	σ	10	11	1	1	14	15			147	SEG	1	2	ŝ	4	ŝ	-	~	.α	σ	01		1	13	14	- LC

PF/P 1.011 1.007 1.001	0.998 0.996 0.996 0.997 0.997 0.997 0.993 0.993 1.004 1.004 1.009	PF/P 1 • C09 0 • 994 0 • 9989 0 • 9989 1 • C09 1 • C09 1 • C003 1 • C003 1 • C109 1
CP 0.023 0.016 0.003	-0.009 -0.009 -0.0013 -0.0113 -0.0113 -0.0113 -0.013 0.019 0.019	0.020 0.021 0.021 0.0200000000
V A V		∧ ∨ ∧
ALPHA 0.00 0.400 0.893 0.911 0.915 0.915	0.883 0.831 0.831 0.831 0.834 0.834 0.834 0.834 0.830 0.982 0.983 0.983 0.983 0.983	ALPHA 0.00 0.00 0.986 0.986 0.986 0.861 0.861 0.861 0.9861 0.933 0.956 0.953 0.956 0.958 0.958 0.958 0.958 0.958 0.958 0.979
11 70.7 27/0 0.786 0.818 C.820 C.820	0 7 - 7 0 7 - 9 0 661 0 665 0 655 0 751 0 980 0 9800 0 9800 0 9800000000000000000000000000000000000	7 7
5 7 7 7 7 7 7 7 7 7 7		2 4 4 9 7 2 3 3 7 2 3
223 233 233 24 25 25 25 25 25 25 25 25 25 25 25 25 25	CC 8 8 2 7 8 8 7 7 8 7 7 7 8 7 7 7 8 7 7 7 7 8 7	00000000000000000000000000000000000000
L PT 5 757 2/08 -2.02 -1.52 -1.61		2 2 2 2 2 2 2 2 2 2 2 2 2 2
74 847 74 877 74 75 74 75 74 75 75 75 75 75 75 75 75 75 75 75 75 75 7		T B I I I I I I I I I I I I I I I I I I
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7 TN CCI 66 223-5 223-0 223-0 223-0		2223 2223 2223 2223 2223 2223 2223 222
571 571 6.803 0.801 0.801 0.801		754 771 777 777 777 777 777 777 777 777 77
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1.019 1.009 1.000 762.0 0.998 0.995 1.004 1.006 1.013 1.014 1.011 1.006 1.004 1.003 1.000 1.000 1.010 1.016 1.004 0.998 1.002 165.0 DF/D 1.0.1 013 1.006 0.996 1.009 DE/ --0.000 -0.007 -0.010 -0.003 -0.011 0.032 0.013 0•007 -0•002 -0•006 0.025 0.020 0.009 0.010 0.004 0.014 0.028 0.029 0.042 0.013 0.00.0-0.001 0.019 0.022 0.029 0.035 -0.005 0.024 <u>م</u> ð V A /V V A /V 0.988 0.978 0.978 0.929 0.937 0.919 0.910 0.910 0.928 0.983 0.983 0.909 0.882 0.871 0.856 0.863 0.850 0.852 0.852 0.840 0.860 0.887 0.948 0.980 VF/V 894 0.911 V F / V 776.0 0.984 • ALPHA 0.00 04/0 ALPHA 0.60 0.4/0 C-967 C.961 0.853 C.869 C.870 C.870 0.832 0.832 0.832 0.832 C.810 C.810 C.855 C.930 66.3 QF/Q 0.792 0.822 0.816 0.750 0.770 0.719 0.697 0.697 0.697 0.697 0.697 0.719 67.2 QF/0 0.974 0.767 892 972 968 975 972 3 . . 00 4 9 2 W / MN 491 MV/W ۵ 220.6 NF/N 220.7 MF/W 0.883 0.893 0.893 C.980 C.975 C.921 416.0 0.929 0.923 0.910 0.897 0.896 0.849 0.835 0.835 0.825 0.846 0.925 0.870 C.858 O.841 £53. 006-0 0.875 0.942 0.981 C.98C 0.960 0.978 C.982 749 2 Z/D8 16 751 3 Z/DB 1 -2.03 0. \mathbf{O} -1.52 -1.03 -1.53 -1.03 -0.70 -0.53 -0.52 -0.36 -0.19 0.15 0.30 0.48 0.66 0.98 -0.19 0.15 0.31 0.48 0.64 0.98 1.48 1.98 -0.68 -2.03 F d anω F d 4.5 PNJL CCNF MACH PN/L 5 C-800 1-516 Y/CB 0.00 0.00 0.00 0.00 0.00 0.00 00.00 NACH 571 1 66 MACH 0 3.801 220.6 -802 220.6 799 220.1 799 220.1 798 219.6 8 7 219.1 8. 220.7 219.6 219.6 220.1 220.1 220.6 220.1 220.1 220.1 20 220.6 220.1 221.2220. D. 571 1 C-8CC 0.799 0.797 0.798 0.797 0.798 0.797 0.797 0.797 0.797 661.0 661.0 661.0 661.0 861.0 861.0 861.0 861.0 861.0 861.0 861.0 C. 80C 0. 800 MACH C.8CC 0.800 551.0 0.800 801 σ 0.800 0.800 799 SI ð \circ m 550 150 S50 13 4500 ŝ σ 10 12 4 4 N N LCN . 5 m ω σ C \geq U.Y 4 Ľ

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		DF/D	1.006	1.006	1.001	1.001	0.599	192.0	162.0	166.0	C•598	79.597	965.0	0.598	1.001	1.000	1.004
		نە	0.023	0.026	0.003	0.032	-0.003	-0.014	-0.013	-0.013	-0.009	-0.013	-0.017	-0.010	0.004	0.002	0.017
		V A /V															
		VF/V	0.911	0.916	0.921	0.893	0.867	0.843	0.827	0.820	0.852	0.852	0.362	0.897	0.971	0.995	0.989
AHQLA	0.00	0A/0			-	-			-		-	•			-	_	-
77	67.0	01 40	0.824	0.834	C.840	0.786	C.738	0.693	0.667	0.655	0.711	c.710	0.726	6.793	0.939	066.0	0.981
٥	702	NV N															
o	176.6	NF /N	C.9C5	c. 910	6.916	C.885	C. 855	C.834	0.818	C-81C	C.844	0.844	C.854	C. 891	C•965	366-0	G. 988
Ld	895	Z/08	2.02	1.53	1.02	0.69	0.52	0.95	0.18	0.01	0.16	0.33	0.48	0.65	55.0	1.45	I•99
J/Na	1.513	Y/DB	0.02 -	0.02 -	C. C2 -	0.02 -	C. C2 -	0.02 -	0.02 -	0.02 -	0.02	C•C2	0.02	0.02	C.C2	0.02	0.02
NACH	0.599	(/ CB	1.05	1.05	1.05	1. C5	1.05	1.05	1.05	7.C5	1.05	1.05	1.05	1.05	1.05	7.05	1. C5
CONF	ŝ	î	. 6	•	4.	4.	4.	.4	4.	0	4.	4	4.	0	÷.	. 2	• 5
N I N	1 66	e	176	176	175	175	175	175	175	176	175	175	175	176	176	177	177
TST	571	MACH	0.599	0.559	0.597	0.557	0.557	0.597	7253.0	0.598	0.557	155.0	0.597	0.558	0.599	0.600	0.601
RUN	152	SEQ	اسو	2	n)	4	u v	\$	7	ß	σ	10	11	12	13	14	5

0E /0	1.009	1.005	1.002	1.001	100.1	0.598	0.999	1.001	665.0	0.998	0. 998	1.002	1.005	1.005	1.007
٤	0.035	0.019	0.007	0.003	0.003	-0.006	-0.002	0.006	-0.005	-0.006	-0.006	0.007	0.022	0.019	0.027
V A V															
VF/V	616.0	0.985	0.960	0.934	0.880	0.890	0.867	0.365	0.871	0.879	0.895	0.924	0.947	0.982	0.983
ALPHA 0.00 0.40															
TT 67.2 GF/0	0.964	0.972	0.918	0.807	0.763	0.779	0.739	0.735	0.744	0.758	C.789	0.846	C•895	0.967	179.0
101 1 × 1 × 1															
C 177.8 NF/N	C.978	0.984	0.957	0.898	0.873	0.883	0.860	C. E57	0.863	C.872	0.889	0.919	C.944	0.981	0.982
рт 896 2/Гв	2.03	1.52	1.03	0.69	0.52	0.35	0.19	0.02	0.14	0.31	0.48	0.65	0.58	I.48	1.58
RN/L 1.518 //DE	0.44 -	3.44 -	0.44 -	0.44 -	- 44 -	0.44 -	0.44 -	0.44 -	0.44	0.44	0.44	0.44	2.44	0.44	0.44
VACH 0.602 (/DB	- 49 -1	- 64 -	- 65.5	- 64.9	- 49 -	3.49 -(9-49-6	64.6	- 64.9	- 65-3	3.49 -(9-49-1	- 65-8	3.49 -(- 49 -(
CONF 5	8	~	ۍ ۳	0	~~~	~	÷.	م	~	÷.	ۍ ب	۳ ۳	۳	°~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
2 9 0 2 9 0	177.	176.	176.	176.	177.	177.	176.	176.	176.	176.	176.	176.	176.	177.	177.
TST P 571 1 MACH	0.602	0.559	0.599	0.598	0.601	0.601	0.559	0.599	0.599	0.599	0.559	0.599	0.559	0.600	0.600
RUN SEO SEO	-	2	m	4	U N	Q	~	œ	σ	10	1	12	13	14	

1.000 • 005 0.999 1.000 0.996 ..003 100.1 1.000 0.998 1.004 666.0 0.998 0.999 .003 pr/p 1.004 0.022 -0.002 0.011 0.003 -0.003 -0.008 -0.005 -0.014 -0.010 -0.001 ഹ 0.001 0.011 0. a V A /V 0.874 0.872 0.885 0.939 0.926 0.878 0.850 0.869 0.889 0.911 0.930 0.899 0.847 066 VF/V 0.939 ٠ 0.00 ALPHA QA70 67.3 CF/0 0.857 0.855 0.855 0.858 0.858 0.858 0.858 0.858 0.858 0.758 0.758 0.751 0.751 0.751 0.751 0.770 C.979 O.983 0.778 0.877 7 C3 N V V N ۵. 4T 5 4 2/68 μF/ν • 2/68 μF/ν • 06 -2.02 C.9^c • -1.53 0 • -2.02 MF/W C.9C6 0.921 C.926 C.893 C.871 C.842 0.861 0.838 0.867 0.864 0.878 0.882 C.935 9.8 9.8 9.8 \mathbf{c} -0.53 0.14 ω 0.64 0.98 ω .98 •98 ω -0-69 -0.19 -0.02 0.31 0.4 5 0.597 1.507 X/DB Y/DB Z 8.49 0.00 -1 8.49 0.00 -1 00.00 00.00 00.00 00.0 00-00 MACH 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.4 **LONF** 176.6 175.4 176.0 176.0 176.6 176.6 176.6 176.6 176.6 177.2 177.2 177.2 177.2 176.6 176.6 L N 99 0 571 1 ۵ 0.600 0.600 MACH 0.598 566 599 599 599 600 0.600 ST . 212 RUN 154 SFO 4500 ω σ 0 4 S N m

1.006 ..002 • 000 .002 or∕a .. 004 .005 • 003 .002 .001 .006 .001 .001 .006 0.015 0.007 0.004 0.007 0.0010 0.005 •001 •023 110.0 0.023 0.003 a U Ó O V A /V 0.935 0.929 0.925 0.918 0.905 0.984 0.989 0.977 0.909 0.889 0.908 0.924 0.959 VF/V 0.982 98 • 0.00 0.4/0 ALPHA C.859 0.856 0.856 0.836 0.836 0.836 0.836 0.836 0.816 0.816 0.846 0.972 0.981 0.957 0.968 67.3 QF / Q 0.916 76.0 702 N / VN 0 1.515 896 177.2 Y/DB Z/CB MF/W C.44 -2.03 C.983 C.983 O.988 C.976 C.931 O.925 C.925 C.925 C.9C3 0.882 0.919 0.957 0.986 0.899 C.9C3 0.48 -1.52 -0.52 -0.69 -0.36 0.14 • 64 0.98 Id -0.19 0.31 α -0.03 • 4 σ Ľ 0 RN/L 0.600 1.515 (/DB Y/DB 7 0.44 C.44 0.44 0.44 C.44 0.44 0.44 0.44 0.44 C.44 4 4. .4 0.4 4 0 TN CONF WACH 8.49 8.49 8.49 8.49 8.49 8.49 8.49 ۲. س 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 66 C 571 1 MACH TST P 0.600 0.600 0.600 0.600 11 RUN 155 SEQ H CI M 5 σ 0 ຕາ 4 \$ ω 4 5

		pF/p	41 1-026	38 1-074	24 1.015		03 1.002	000 1 000	160-0 71	19 0.988	15 0.990	17 0.989	15 0.997	100 0 401				45 I.C28					711 1 013		1010	08 1.005	3 0.998	1 0.993	3 0.992	9 0.588	0 0.987	7 0. 583	2 0.986	6 0.990	666 0 10	14 1.021	9 1.031
		VA/V CP	0-0	0.0	0.0		0 0	0.0	0-0-	0-0-	0-0-	0-0-						0.0								0-0	0.0-	-0-0	-0-01	-0-01	20-0-	-0-05	-0.02	-0.01	-0-00	0.03	0.04
AL PHA	0.00	DA/Q VF/V	0.971	0.975	0.972	0.935	0.911	0.899	0.888	0.869	0.843	0.846	0.852	0.881	0.939	0.984		016.0		AI PHA	0.00			0.933	0.931	0.909	0.896	0.877	0.838	0.831	0.818	0.820	0.820	0.833	0.919	0.977	0.974
T T	8 64.8	M QF/Q	0.957	0.963	0.948	0.857	0.807	0.781	0.753	0.714	0.669	0.673	C-69D	0.744	0.865	C.979	0 0	1		11	0 66.9		0.812	0-865	0.856	0.804	0.774	0.732	0.662	0.646	0.623	0.624	0.626	0.652	0.821	0.968	0.969
۵.	.2 37	N MA/	6	0	7	4	7	4	2	0	2	5	0	6 0	6	 1	<i>c</i>	J	-	۵	.7 380	V V W V			0	10		~	~	•		_				-	-
2	79 241	B MF/	3 C.96	3 0.97	2 0.96	5 0.92	2 0.89	6 0.88	9 0.87	3 C.85	4 0.82	1 0.82	8 0.83	4 0.86	9 0.92	8 C.98	R 0.07			U L	31 241.	NE /	0.89	3 0.92	2.0.92(C. 89	0.88]	. C. 859	C.81	C.805	751.0 1	151.0	161.0	C.811	906-0	16.0	0.965
N/L P	482 6	B Z/D	5 -2.0	5	5 -1.0	5 -0.6	5-0-2	5 -0-3	2 -0 -1	5-0-0	5 0.1	5 0.3	5 0.4	5 0.6	5 0° 3	5 1.4	5 1.9	•		V/L PI	478 68	27/04	l -2.02	1-1-5	I -1.02	-0-6	1-0-53	1-0.36	-0-13	-0.02	0.14	. 0.31	0.45	0.64	0.98	I.48	1.59
ACH R	954 1.	B Y/D	8 -0.4	8 -0.4	8 -0.4	8 -0.4	8 -0.4	8 -0.4	8 -0.4	8 -0-4	8 -0.4	8 -0-4	8 -0-4	8 -0-4	8 -0-4	8 -0.4	8 -0-4			ACP PA	954 1.4	3017 F	0.0	3 -0.01	3 -0.01	3 -0°C	3 -0.01	0-0- 0	-0-01	8 -0.01	8 -0.01	-0-01	-0-01	-0-01	-0-0-	-0-0-	-0-0- 8
CNF V	50.	X/C	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4			UNF NI	50.5	X/C	8.48	8.45	8*48	£•4{	8.48	8.48	8.45	8.48	8.45	8•46	8•46	8.48	ε . 46	8.48	8.48
PINC	1 66	с , с	241.2	240.1	240.7	240.7	240.1	240.1	239.6	Z40•I	241.7	241.8	241.8	241.2	240.8	241.3	240.8			D IN CI	1 66	a	241.7	242.3	241.2	241.2	240.7	241.2	241.2	241.2	241.2	241.2	241.2	241.2	241.2	241•2	240.8
151	571	MACH	0.954	0.951	0.952	0.952	0.951	166.0	066.0	166.0	0.954	0.953	0.953	0.951	0.949	0.950	0.949			TST	571	MACH	0.954	0.955	0.952	0.952	0.950	0.951	0.951	0.951	0.951	0.951	0.951	0.951	0.951	1.451	0•949
RUN	156	S T C	~ (4 1	r J	0	~ 0	00	л (,	2:	::	77		14		16			RUN	151	C L V	-	2	3	4	ŝ	9		ευ	6	10		17		4 I 1 ,	15

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1.017 0.595 0,993 065 *0 0.987 0.993 0.989 1.000 966 • 0 1.02 .005 1.018 1.013 1.001 1.019 bF/P 0.027 -0.016 -0.012 -0.007 -0.017 0.029 0.028 0.021 0.007 0.002 -0.010 -0.007 ĉ V A /V 0.978 0.950 710.0 0.892 0.874 0.874 0.888 0.939 0.911 0.877 0.935 0.929 0.978 0.971 0.979 VF/V 0.00 QA/Q ALPHA 0.802 0.754 0.729 0.724 0.724 0.724 0.833 0.963 974 0.945 0.858 0.865 0.842 0.969 QF /0 7.8 6 MA/M а 381 C.973 C.974 0.858 0.871 0.859 0.855 0.855 0.855 0.876 0.942 C.974 C.966 C.924 O.929 Ś C.917 C 242.5 MF/M C.975 0.48 0.64 0.58 1.48 1.98 E1 684 2/08 -2.03 0 -1.53 0 -1.53 0 -1.53 0 -0.36 2 -0.36 -0.19 -0.02 0.14 51 NACH RN/L 0.954 1.481 ŝ CCNF 242.9 242.9 242.3 242.3 242.3 242.3 242.3 242.3 242.9 241.8 241.8 241.8 241.8 241.8 241.8 241.9 241.9 241.0 66 0 2 0.954 0.953 0.953 0.954 0.952 0.952 0.950 0.950 0.950 0.950 0.950 0.947 1 112 1 112 MACH 0.954 14 112 - NEARONOO RUN 158 SEQ

.018 C2 8 1.002 0.588 0.991 0.991 966.0 1.008 1.007 1.022 1.018 1.013 1.019 --0.014 0.003 0.029 0.020 0.012 0.012 0.011 0.010 -0.010 0.040 0.030 0.035 đ V A /V 0.978 0.957 0.929 0.929 0.919 0.906 0.935 0.897 0.933 0.903 0.888 116 0.976 0.975 VF/V 0.00 0A/9 ALPHA 0.962 0.963 0.925 0.856 0.858 0.858 0.828 0.801 0.801 0.802 0.768 0.770 0.754 0.967 0.852 416. 68.8 QF/0 M / M 381 ٥ 319.0 242.9 vF/N 0.972 0.906 C.892 C.895 C.875 C.888 C.872 0.922 0.881 16. C.918 179.0 C.950 0.13 78 684 Z/DB 0.63 -0.19 0.46 9.29 19.0 -1-53 -0.54 1-9-I -2.05 -1.04 4. -0.71 5 0.954 1.478 RN/L C.41 C.41 C • 41 0.4] 0.41 Y/CB C. 41 0.41 NACE 1C-87 1C-87 1C-87 1C-87 1C.87 10.87 1C.87 1C.87 1C.87 1C.87 1C.87 1C.87 1C.87 5.87 0.87 X/CB LND UDNE 241.4 241.4 542.5 241.2 241.6 241.6 241.6 241.5 241.5 241.5 241.5 241.5 241.5 241.4 241.4 241.4 2 66 0,949 0,949 0,949 0,949 NW2R0280012845 RUN 159 SEC

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		pF/p	1.016	1.014	1.007	1.003	1.003	665.0	1.005	1.001	1.002	1.002	0.996	1.001	1.004	1.007	1.022	1.031			of/p	1.020	1.021	1.021	1.012	1.010	1.007	1.001	1.002	0.9999	0.599	1.003	1.003	1.006	1.019	1.C29
		d D	0.025	0.023	0.012	0.005	0.005	100.0-	0.008	0.002	0.004	0.003	-0.006	0.001	0.007	0.011	0.035	0.049			م	0.032	0.033	0.034	0.019	0.016	0.011	0.002	0.004	-0.002	-0.002	0.006	0.005	010-0	0.030	0.047
		V A / V																			V A /V															
ALPHA	0.00 0	0A/Q VF/V	0.912	0.939	0.939	0.913	0.895	0.885	0.881	0.865	0.347	0.845	0.852	0.843	0.854	0.903	0.965	0.976	ALPHA	0.00	QA/Q VF/V	0.968	0.973	0.962	0.927	0.902	0.892	0.889	0.875	0.867	0.863	0.866	0.870	0.921	0.968	776.0
11	69.6	0F/0	0.821	0.875	0.869	0.812	0.776	0.753	0.750	0.716	0.685	C.631	0.689	0.676	0.699	0.795	0.941	0.974	TT	70.5	QF /0	0.944	0.957	0.932	0.849	0.796	0.772	C.762	0.737	0.719	0.712	0.720	0.739	0.830	0.945	0.974
Q.	3 83	N/VN																	۵.	383	M / M															
0	5 241.9	NF / N	0.899	0.929	0-929	c.900	0.880	9.868	C.864	C.846	C.826	C.824	0.832	C.822	C-834	C.888	0.959	0.972	ى	3 244.0	ドード	0.962	0.968	C.955	C.916	0.888	0.875	0.872	0.857	0.848	0.844	0.847	C.858	0.908	C-963	0.973
L PT	3 685	Z/08	-2.04	-1.55	-1.04	-0.71	-0-54	-0.37	-0.37	-0.20	-0.03	0.12	0.29	0.46	0.63	16.0	1.46	1.97	L PT	9 688	2/08	-2.03	-1.54	-1.04	-0.71	-0-54	-0.37	-0.20	-0.04	0.14	0•30	0-47	0.63	0.96	1.47	1.97
F PN/	0 1.47	Y/DB	-0-03	-0.03	-0-03	-0.03	-0.03	-0-03	-0.03	-0-03	-0.03	-C+C3	-0-03	-0.03	-0.03	-0-03	-0.03	-0-03	H RN/	4 1.47	Y/CB	-0-38	-0-38	-0.38	-0.13	-0.38	-C•38	-0.38	-0-38	-0.38	-0-38	-C.38	-0.38	-0.38	a n • 0-	-0.38
NF VAC	5 0.95	X/08	10.87	10.87	10-87	10.87	10.87	10.87	1 C - 87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	NF NAC	5 0.95	X/CB	10.87	10.87	10.87	10.87	1C.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	1C.87
P TN CCI	1 66	Ċ	241.5	242.4	242.4	242.9	242.9	242.5	244.5	244.C	243.5	243.5	242.6	242.6	242.6	242.2	242.7	242.7	P TN CCI	1 66	ø	244.C	243.5	243.5	242.5	243.5	243.C	242.7	242.2	241.8	241.8	241.3	241.8	242.3	242.3	242.3
TST	571	MACH	0.950	C.951	0.951	0.953	0.953	0.953	0.955	0.953	0.951	0.951	0.948	0.948	0.948	0.947	0.948	0.948	TST I	571	MACH	0.954	0.953	0.953	0.949	0.951	0.949	0.948	0.947	0.945	0.945	0.944	0.945	0.946	0.946	0.946
RUN	160	SEQ		2	~ ``	4	ഹ	9	~	œ	6	10	11	12	13	14	15	16	RUN	161	SEC	-	~	m	4	ŝ	Ŷ	~	ω	σ	10	11	12	.	14	15

	d/∃d	1.022	1.019	1.013	1.008	1.005	1.004	1.001	1.001	6665.0	166.0	0.999	1.000	1.007	1.025	1.033			DF/D	965-0
	CD	0.035	0.031	0.021	0.013	0.008	0.006	0.001	0.001	-0.001	-0.005	-0.001	0.001	0.011	0.040	0.053			d D	-0-004
	V A /V									-									V A /V	
-	VF/V	0.975	0.978	0.909	0.929	0.919	0.905	0.891	0.890	0.873	0.866	0.470	0.887	0.926	0.967	0.973	4	0	VF/V	0.882
AL PHA	04/0																AL PH/	0.0(0A/0	
TT 20	0F/0	0.963	0.968	0.941	0.849	0.825	0.795	0.766	0.764	0.729	0.715	0.725	0.757	0.842	0.947	0.968	11	70.9	0F/0	0-746
a .	WAN WAN																٩	385	MA/M	
י ט ט ני	NF/N	179.0	C.974	0.964	c.918	0.906	c.850	0.875	0.874	0.854	0.847	0.851	c.870	0.915	0.961	0.968	ى	244.C	NL /N	0.865
PT .	583 2/08	2.04	1.53	1.04	0.10	0.54	0.37	0.20	0.04	0.12	0.30	0.46	0.62	16.0	1.47	1.96	La	683	Z/CB	76.0
RN/L	1.4//	- 48 -	- 48 -	- 48 -	- 34.0	- 48 -	.48 +	- 84.0	.48 -	.48	0.48	0.48	0.48	0.48	.48	0.48	RN/L	1.479	1/08	
VACH	0.952 X/CB	0.87 -(0.87 -(C.87 -(C-87 -(0.87 -(C.87 -(0.87 -(C.87 -(C.87 - (C.87 -(C. 87 -(0.87 -(C. 88 - (C.87 -(C.87 -(NACH	0.952	X/CB	0000
CONF	ົີ	5	5 1(0	0	0 1	τ̈́ υ	0 1	- - -	C	C I	0	5		0	1	CCNF	L C)	, ,	c
D T V	0 0 0 1	243.	243.	244.	244	244.	244.	244	244.	244.	244.	244	243.	244.	244	243.	D TN	1 66	0 -	246
TST	571 MACH	0.952	0.952	0.954	0.954	0.954	0.954	0.954	0.954	0.954	0.954	0.954	0.952	0.953	0.953	0.950	TST	571	MACH	050
RUN	162 SEC		~	e	4	ŝ	Ś	~	ω	6	10	11	12	13	14	5	RUN	163	S E C E C E C	-

0.994 0.993 0.993 0.993 0.993 1.004 1.019 1.019 -0.010 -0.011 -0.014 -0.019 -0.008 -0.008 0.008 0.031 0.972 0.972 0.972 0.972 0.972 0.972 0.440 0.714 0.686 0.688 0.688 0.688 0.688 0.688 0.588 0.573 0.795 0.795 0.976 9, 99 9, 99 9, 99 110, 00 110, 00 110, 00 110, 00 110, 00 246.0 949.0 949.0 949.0 949.0 949.0 949.0 949.0 949.8 949.8 948.8 948.8 948.8 948.8 948.8 948.8 948.8

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		pr/p	1.020	1.015	1.010	1.005	1.007	1.004	1.007	1.000	1.000	0.995	0.599	799.0	1.006	1.009	1.011
		СÞ	0.045	0.034	0.022	0.011	0.015	0.009	0.015	0000-0-	-0.000	-0.011	-0.003	-0.016	0.013	0.020	0.023
		V 4 / V															
		VF/V	0.976	0.982	0.969	0.939	0.925	0.918	0.905	0.911	0.910	0.903	0.907	0.921	0.949	0.984	0.989
ALPHA	0.00	0 / NO	-	•	-		-	-	-	-		-		-	-	-	-
11	70.6	0F/0	0.967	0.974	0.941	0.872	0.846	0.830	0.806	0.813	0.809	0.793	0.803	0.830	C.894	0.972	0.985
۵.	495	N/VN															
Ċ	223.0	NE / N	0.973	C.98C	0.965	0.932	C.917	C.909	C.895	0.902	006-0	C.893	C.857	C.913	0.943	C.9 82	C•987
L PT	3 757	Z/08	-2.05	-1.54	-1.03	-0.10	-0.53	-0.37	-0.21	-0.05	0.13	0.29	0.47	0.63	0.96	1.47	1.97
IN A	1.51	Y/0.P	0-41	0.41	C.41	0.41	C.41	0.41	0.41	C.41	0.41	C.41	0.41	0.41	0.41	0.41	C.41
F WACH	5 0.802	X / C9	10.88	1C.88	1C.88	1C.88	1C.88	1C.88	1C.88	10.88	1C.88	1C.88	10.88	1 C. 88	10.88	10.88	1C.88
N CCN	50	G	3.0	2.0	2.5	2.5	2.5	2.5	2.5	2.0	2•5	3.1	3.5	3.5	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3.5	3•0
L d	1 6	r	2 22	9 22	0 22	0 22	0 22	0 22	0 22	8 22	0 22	1 22	2 22	3 22	3 22	3 22	1 22
TST	571	MAC	0.80	0.79	0.80	0.80	0.80	0.80	C. 80	0.79	C. 80	0.80	0.80	0.80	0.80	0.80	0.80
RUN	164	SEQ		2	m	4	ſ	9	2	80	σ	10	11	12	13	14	15

0117 0015 0015 0015 0015 0005 0005 0003 0003	1.006
0,000 0,000000	0.013 0.022 0.027
∧ ∧ ∨	
VF/V VF/V 0.907 0.924 0.830 0.878 0.878 0.878 0.878 0.878 0.878 0.878 0.878	0.937 0.977 0.985
ALPHA 0.00 0.00 0.00	
7 1 1 7 1 1 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.870 0.959 0.977
22 22 22 22 23 24 24 25 25 25 25 25 25 25 25 25 25	-930 -974
00000000000000000000000000000000000000	0.96 1.46 1.97 0.70
<pre>~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~</pre>	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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ST P 751 P 779 757 222 300 222 302 222 302 222 301 222 301 222 301 222 301 222 301 222 301 222 301 222 301 222 301 222 302 222 300 222 300 2000 20000000000	301 22 301 22 301 22
200 200 200 200 200 200 200 200 200 200	15 0.6 15 0.6

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					00.1	1.00	1-00	00-1	0.999	0.99	1-00	1-00	1.00	1.00	1.01	1.01			05 70			1.006	1.004	1.002	1.002	1.000	1.001	1.004	1.001	1.004	1.004	1.005	1-010
		0-029	0.021	0-015	110-0	0.008	0.013	110-0	-0.003	-0.003	-0-001	0.004	0.006	0.013	0.027	0.030			٥L	120-0	02000	0.013	0.009	0.005	0.004	-0.001	0.002	0.010	0.001	0.008	0.010	0.010	0-022
																			V A /V							-							
	VEZV	984	984	.961	.918	.891	.879	.878	. 880	.868	.886	.889	.899	. 940	• 978	.983			VFIV	983	- 988	.969	.921	.902	.897	.896	.897	• 884	. 892	. 902	.912	• 944	- 980
ALPHA	00.00		, 0		0		0	0	5	0	0	0	0	0	0	0	AL PHA	0.00	DA/G		0	0	0	0	0	0	0	0	0	0	0	0	C
11	0.10	0.976	0.972	0.921	0.830	0.777	0.755	0.753	0.751	0.729	0.763	0.771	0.792	0.876	0.962	0.976	77	70.4	0F / 0	0.974	0.982	0.938	0.836	797.0	787.0	0.782	0.786	0.764	0.775	197.0	0.818	3.884	1.965
d 0	164 N / N	Ī															۵	497	N V N			-		U		Ŭ	U	Č	C	U	0	Ŭ	
с 237 ғ	N - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 -	C.982	0.982	0.956	0.909	0.880	3.866	3.865	0.867	0.854	0.874	0.877	.889	0.933	.975	0.981	G	222.5	NE / N	.980	1.98.	.9566	.912	.892	.386	.885	.886	.872	.880	.891	.902	• 9 3 8	978
PT 757	2/08	2.04	1.54	1.04	0.71 (0.54 1	0.35 (0.21 (0.04 (0.13 (0.29 (0.47 (0.63 (0.57 (1.47 (1.97 (ЪЪ	757	2/CB	2.04 (1.54 0	1.04 C	0.71 0	0.52 0	0.37 0	0.21 0	0.04 0	0.12 0	0.29 0	0.47 0	0.63 0	3.96 C	46 0
1 512	1.0.14	0.38 -	J • 38 -	3.38 -	3.38 -	1.38 -	3•38 -	J • 38 -	38 -	38	38	.38		ω • •	38	38	RN/L	1.514	108	- 48 -	- 48 -	• 48 -	•48 -(- 48 -	•48 -(•48 -0	•48 -(• 4 8	•48 (• 48	• 48	•48	4 8
MOCH NACH		.88 -(. 88 -(.88 -(. 88 -(. 88 - (.88 -(. 88 -	• 88 -(. 88 -(. 88 - (• 88	. 88 -(.88 -(.88 -(• 88 - (NACH	0.800	/08 /	.88 -0	.88 -0	.88 -0	.88	- 88 - 0	.88	.88 -0	- 68 - C	.88	• 88 - C	• 88 - 0	.88 -0	- 88 - 0	- 88 - C
CONF 5		5 10	5 10	5	5	5 I C	10	5	6 10	1 10	10	0 10	C 1C	0 10	5 10	1 1C	CONF	n	×	57 5	2 I C	0 1 0	-							10		5,	
D T N	20	222.	222.	222.	222.	222.	222.	222.	222.	223.	222.	223.	223.	223.	222.	223.	O TV	1 66	o	222.	222.	222.	223.(223.(223.(222	223.(223•(223	223	223	- CZZ	- 272
TST 571	MACH	0.300	0.800	0.800	C. 8 C O	0.800	0.800	0.800	0.799	0.801	0.800	0.801	0.801	0.801	C. 800	0.801	TST	571	MACH	0.800	0.800	0.800	0.801	0.901	0.801	C. 8CU	0.802	0.802	0.803	0.803	0.802	0.802	0.802
RUN	S E C	-	2	f	4	Ś	\$	-	œ	σ	10	11	12	13	14	1	NDa	167	SEO	1	2	س ا	4	n i	01	~ (ω	r (21	n ,	4

		0 L / D		6 1.003	100 1 0	1001 2	0 1.000	F00 0 V	144.0 0	965 0 6		2 1.001	F 1.003		4 T.006	200 1 6	0 T•000	200 1 3	
		c c	<u>د</u>	0.00		0.00	00.0-		-0.00	00-00-		0.00	00.00		0.01	r c	1.01		
			V 4 V																
	-	11 L L L	V - / V	0.870		0.864	0.852		0.818	0.870		0.870	000 0		0.932	100	0.480	000 0	1.404
AL PHA	0.00		D/A/U																
11	70.3		0110	736		0.723	0.701		0.748	022 0		0.734	565 0		0.859		C.974		1.482
۵	497																		
ى v	777.5		N / 1 N	0 053		C.850	758.0		0.866	054	0.0.0	0.857	020 0	0.010	0-924		0.984		0.988
1d	4 757	•	2/08	74		-0.20	20		0.15		00.00	0.47		0.03	0.97		1-47		1.97
RN/I	1.51				2	00-0			00-00		00	00-00		00-00			00-00		00.0
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	pF/D	1.CO8	1.005	1.003	1.001	1.002	1.002	1.000	1.003	1.001	1.003	1.003	1.002	1.006	1.008	1.004
	Cb	120.0	0.019	0.011	0.004	0.008	0.008	0.001	0.013	0.003	0.012	010.0	0.006	0.022	0.030	0.014
	V A /V															
	VF/V	0.985	0.987	0.973	0.935	0.924	0.924	0.919	0.906	0.916	0.902	0.919	0.931	0.946	0.973	0.992
ALPHA 0.00	0 A / 0				-		-									
11 69.1	0F /0	0.976	0.978	0.945	0.867	0.847	0.847	0.836	0.814	0.830	0.806	0.838	0.861	C. 892	0.950	0.985
ч СОС	M A / W															
3170.0	MF /N	480.0	7.987	126-0	126-0	026-0	0.920	0.914	0.900	0.911	C.896	0.914	0.927	0.942	C.971	156.0
PT 904	7/08	2.04	1.54	70-1-	02.0	-0-55	-0.37	-0-20	-0-02	0.13	0.29	0.46	0.64	0.98	1.46	1.97
RN/L	V 7 7 P				- 17-0	- 17-0	1410		6.41 -	0.41	0.41	0.41	0.41	C-41	0.41	0.41
F VACH	20000 2 7 7 8	10 00				10.98	10.88	10.88	10.88	10.88	10.88	10.88	10.58	10.88	10.88	10.88
TN CCN	υc			110.4	1 0 0 4		5-121	178.4	178.4	178.4	178.4	178-4	178.4	178.4	7871	178.4
TST P							200 0	0.603		0.403	0.603	0.603	0.603	0.603		0.603
RUN	2010	3 - 10		2	n x	t U	N N		- α	σ				1 F	4	

666.0 1.005 1.005 1.000 1.002 1.002 1.002 1.002 1.001 ..006 1.002 666.0 1.000 1.00.1 0.599 0.598 1.001 .005 .007 .000 1.c01 .003 I.C04 1.005 0.999 0110 1/10 0.020 0.004 -0.002 -0.005 0.003 0.008 0.008 0.022 0.002 0.007 0.000 0.004 0.016 0.024 0.019 0.044 0.007 -0-001 -0.010 0.028 -0.003 0.005 100.0 -0.00-0.014 0.021 0.004 0.021 <u>م</u> d C V A /V V A /V 0.879 0.885 0.888 0.875 0.901 0.970 0.836 0.387 0.894 **U** • 902 0.392 0.897 0.400 0.892 0.932 0.953 0.896 0.982 V F/ V 0.929 0.931 0.901 0.929 179.0 0.924 0.903 0.893 0.925 0.983 V F/V 0.913 **779.0** 0.00 0.00 AL PHA AHQJA QA/Q QA/Q 65.0 0.859 0.863 C.760 0.753 0.805 0.963 0.970 0.948 0.957 0.907 0.824 0.794 0.784 0.802 QF /0 0.786 0.771 0.776 0.773 0.788 0.944 0.967 QF /0 0.775 0.801 64.1 0.849 0.808 0.786 0.798 0.849 0.792 0.858 700 MA/M 697 N V V N с. ۵ 174.1 NF/V 177.1 C.925 C.927 616.0 C.872 0.868 0.896 0.920 0.968 C.975 C-95C C.890 O.886 O.886 C.886 0.881 C.88C 0.880 558.0 C.924 0**.**969 C**.**980 NE / N C.878 0.894 C.981 0.897 C.886 0.388 C.894 C-982 890 168 -1.54 -1.04 -0.21 0.62 -0-53 -0.36 -0.20 0.12 1.47 0.13 0.46 0.29 0.46 1.46 - 51 0.63 F d Z / DB -2.04 -0-55 -0.38 Y/PB Z/DB -0.38 -2.04 -C.38 -L.54 -1.04 -0.70 0.96 1.96 -0.71 -0.04 **b** J/Na 5 0.596 1.509 5 0.602 1.519 PN/L -0.03 -0.03 -0.03 -0.03 Y/DB E0.0--0.03 -0.03 -0.03 -0.03 -0-03 -0.38 -0.38 -0.38 -C.38 -C.38 -0.38 -0.38 -0.38 -0-38 -C.38 -0.03 -0.03 -0.03 -0-03 -0.38 œ -0.0 -0-38 ri, ပို P TN CONF MACH VACH X / D.B X / DB 1C.87 1C.87 C.87 C.87 O.87 0.87 C.87 C 87 C 87 C 87 C 87 C-87 C-87 C.87 C.87 C.87 C . 87 C.87 C.87 C.87 C.87 1 C . 87 C.87 C+87 C.87 C.87 C.87 10.87 .C.87 C.87 C.87 TST P TN CCNF 175.9 175.5 176.5 176.5 175.3 175.3 177.1 175.9 177.1 177.1 177.1 177.1 177.1 174.1 177.7 177.7 174.1 175.3 **(**1) 177.1 177.1 177.1 176.5 175. 175. 175. 177. 176. 66 C 66 \mathbf{C} 571 1 MACH 571 I 0.558 0.598 0.558 0.558 0.558 0.598 MACH 0.596 0.556 0.602 0.602 0.602 C.6C2 0.600 0-600 0.600 0.600 0.601 0.602 0.602 0.602 0.604 0.602 0.600 0.601 0.602 0.602 0.604 0.602 0.601 0.601 TST 10 RUN 170 SEQ \sim 21 3 S 4 SON ω **o** o 4 Ś KUN N 171 SEQ Ľ١. Q ŝ σ 2 m 4 ភ

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		СР	0.020	0.016	0.013	0.005	0.008	-0.003	-0.005	0.002	-0.006	0.008	0.008	0.014	0.001	0.016	0.027			СÞ	-0.007	-0-003	-0.010	-0.006	0.001	0.007	0.002	0.022	0.018
		V A /V																		V A /V									
		VF/V	0.985	0.984	0.966	0.921	.905	.907	.892	0.895	0.903	.897	.911	.908	0.951	0.975	.982			V F / V	0.864	0.879	0.879	0.884	.874	0.887	0.900	.926	0.970
ALPHA	0.00	0A/Q	•	U	~	•		Ŭ)		Ŭ))				AL PHA	0.00	0 A / 0		•	Ŭ		Ŭ)	9
TT	65.5	01-10	0.973	0.969	0.931	0.839	0.811	0.811	0.784	0.789	0.803	0.796	C.821	0.817	0.898	0.952	0.968	ŢŢ	66.2	0140	0.732	0.759	0.759	0.768	0.751	0.776	0.800	0.853	120.0
۵	698	MA/M					-					-		-			-	۵	159	W / M			-			_	-	-	
Ċ	176.5	NF/N	.584	.983	.963	-915	.900	106.	.886	.888	163.0	168.	.905	.902	.948	.974	186.	G	177.1	MF/N	.856	.871	.872	.877	.866		.894	.921	. 968
۲q	891	Z/08	2.04 0	1.54 0	1.04 C	0.71 C	0.54 0	0.38 0	0.21 0	0.04 0	0.12 0	0.29 0	0.47 C	0.63 0	0.56 0	1.47 0	1.96 0	F 1	168	Z/08	0.37 0	0.20 C	0.03 0	0.14 0	0.30 0	0.47 0	0.63 0	0 12.0	J 247 1
RN/L	1.514	Y/DB	0.48 -	0.48 -	0.48 -	0.48 -	0.48 -	0.48 -	0.48 -	0.48	0.48	0.48	0.48	0.48	C.48	0.48	0.48	RN/L	1.514	Y/DP	- 00.0	- 00.0	1 00 • 0	00.00	0.00	00.00	0.00	0°.C	00.00
F WACH	5 0.601	X/DB .	10.87 -(1 C . 87 -1	IC.87 -	1C-87 -(1C.87 -1	10.87 -(1C-87 -4	10.87 -1	10.87 -1	IC.87 -(10.87 -(1C.87 -(10.87 -1	10.87 -(10.87 -1	F NACH	5 0.602	X/CB	- 66 ° 5	66 * 5	66*5	66*5	66*5	1C.00	10.00	10.00 (66.6
TN CON	66	0	176.5	177.1	177.1	177.1	177.1	177.1	177.1	177.1	177.1	177.1	177.1	177.1	177.7	177.1	176.5	TN CON	66	G	177.1	177.1	177.1	17.7	177.7	177.1	176.5	176.5	76.5
TST P	571 1	MACH	0.601]	0.602	0.602	0.602]	0.602	0.602]	0.602]	0.602	0.602]	0.602	0.602]	0.602]	0.604]	0.602	0.601	TST P	571 1	MACH	0.602	0.603]	0.603	0.604]	0.604	0.602]	0.601	0.601	3.601 1
PUN	172	SEQ	-1	2	m	4	i n	Ŷ	~	œ	¢	10	11	12	. 1	14	<u>ا</u> سم	RUN	173	0 S E O	-	2	M 1	4	5	\$	~	œ	σ

1.030 0.595 1.003 966.0 1.022 1.013 1.007 1.008 1.011 0.599 1.010 666.0 1.021 oF/p .023 DF/ 1.01/ 1.02 0.018 0.014 0.019 0.036 0.045 0.025 0.039 -0.008 -0.003 0.053 0.024 0.012 -0.007 -0.001 0.041 ĉ d U V A /V V A /V 0.933 0.939 0.907 0.879 0.865 0.858 0.858 0.858 0.870 0.870 0.875 0.911 VF/V 0.934 0.929 970 964 VF/V 0.929 0.00 0A/0 0.00 04/0 ALPHA **ALPHA** 0.879 0.885 0.753 0.713 0.819 0.866 0.805 0.724 0.726 0.736 0.936 0.956 0.868 68.6 QF 10 0.711 0.864 0.709 0.738 69.2 0140 412 M / M 412 NVVW ۵. ۵ 233.8 234.7 NL /N C.924 C.924 C.924 C.863 C.863 0.845 C.854 0.858 0.915 C.840 C.84C NF / N C.860 C.855 0.847 C.958 C.965 569 697 2708 -1.98 -1.54 -0.54 Z/08 -2.03 -0.20 -0.04 0.13 0.30 0.46 0.62 16.0 1.46 **7**2. -1.03 -0.70 -1.52 RN/L MACH RN/L 5 0.902 1.479 Y/08 -0.03 -0.03 -0-03 X/CB Y/DB 8.49 -0.01 -0.03 -0.03 -0.03 -0.03 -0-03 -0.03 -0.03 -0.03 -0.03 10.0--0.03 -0.03 E0.0-TST P IN CONF MACH NACH X/CB 10.87 1C.87 1C.88 1C.88 1C.87 1C.87 1C.87 1C.87 1C.87 1C.87 1C.87 10.87 10.87 1 C. 87 C. 88 C.87 ŝ CONF 234.1 234.8 235.3 234**.**8 234.3 234.4 234.4 235.3 234.3 234.7 235**.1** 235.6 235.1 235.1 N 66 6 66 0 571 1 MACH 571 1 LL. 0.902 0.902 0.902 0.900 0.900 0.900 0.900 MACH 0.902 0.902 0.903 0.900 0.902 0.903 0.903 0.903 0.904 **TS1** RUN 174 SEQ \simeq 2 175 SFQ 450 $\boldsymbol{\omega}$ σ ---m \mathbf{C} 4 NN N

1.027 1.015 1.010 0.589 1.003 0.989 0.992 1.006 008 792.0 0.584 1.013 10 . • اسر 0.005 0.048 0.026 -0.019 0.015 0.017 -0.019 -0.014 0.023 0.011 0.880 0.852 0.855 0.835 0.835 0.831 0.831 0.827 0.933 0.895 0.921 0.849 0.831 0.976 0.658 0.668 0.866 0.750 0.645 0.962 0.784 0.650 0.661 C.699 C.919 C.924 C.881 C.865 0.834 0.815 C.8C6 0.910 C.824 0.810 C.811 C.831 0.97 -0.53 -0.19 -0.01 0.14 -1.03 0.47 0.64 10.97 -0.69 15.0 1.47 -0.01 -0.01 -0.01 -0-01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.01 -0.0-8.49 8.49 8•49 8•49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 233.8 233.6 233.6 233.9 233.9 233.9 233.9 234.3 235.2 232.6 235.1 235.1 \mathbf{c} 233.7 233.0 234.1 0.901 0.956 0.895 85 • 0 2 m 4500 æ Q 212 14

	VA/V CP PE/P	0.030 1.015	0.024 1.012	0.014 1.007										0.037 1.019					0.026 1.013	0.026 1.013	0.018 1.009			0 010 1 003					201°T 200°0		0.011 1.096	110-1 220-0	0.036 1.018
AL PHA 0.00	CA/Q VE/V	0.915	0.933		0.879	210.0	1 - H - H - H - H - H - H - H - H - H -	0.833	0.823	0-844	0.867	0.936	0.974	0.978	VHO IV				066.0		0.920	0.805	0.470	0 . 871	0.873	0.876	0.871	0.872	2 0 0 0	0.000	0.976		N-N-0
0 IT 452 69.8	MA/N CF/O	0.830	0.364	622 U	0-735	0.685	0.669	0-662	0.646	0.684	0.722	0.865	0.959	C.968	P 11	453 70.0	WA/W OF 10	979.0	0946		782 0	0.100	0-750	0.739	0.738	0.742	0.734	0.737	0-765	0-843	0.952	0.970	010.0
NF WACH PN/L PT C 5 0.852 1.458 726 229.7	X/CB Y/CB Z/CB MF/W	6.443 -C.01 -Z.03 0.964 8.40 -0 01 -1 53 5 035		E-49 -C.Cl -0.69 C.877	8.49 -0.01 -0.53 0.857	8.49 -0.01 -0.36 0.827	8-49 -C.01 -0.19 C.820	8.49 -C.CI -0.02 C.815	8-49-C.01 0.31 C.8C5	8-49 -0.01 0.48 C.827	8.49 -0.01 0.65 0.851	8-49 -0.01 0.97 C.528	8.49 -C.01 1.48 0.971	8.49 -0.01 1.98 C.975	JE MACH RAJL PT C	5 C.850 1.457 727 229.4	X/CB Y/CE Z/CB ME/N	10.87 -0.03 -2.05 0.920	1C+87 -0.03 -1.53 C.925	1C.87 -0.03 -1.03 C.916	1C.87 -C.C3 -0.71 C.884	10.87 -0.03 -0.55 0.872	1C.87 -C.03 -O.38 C.865	10.87 -C.C3 -0.20 C.857	10.87 -0.03 -0.03 C.859	10.87 -C.C3 0.13 C.861	1C-87 -C.03 0.29 C.857	1C-87 -C-03 0.46 0.857	10.87 -0.03 0.63 0.875	10.87 -0.03 0.96 0.915	1C.87 -C.03 1.46 C.970	1C.87 -C.03 1.97 C.97£	
RUN TST P TN CCI 176 571 1 66	SEC MACH 0 1 0.057 220 7	2 0.852 229.7	3 0.853 230.1	4 0.853 230.1	5 0.853 230.1	6 0.853 230.1	7 0.853 230.1	8 0.853 230.1	10 0.852 229.8	11 0.852 229.E	12 0.852 225.8	13 0-853 230-1	14 0.853 230.1	15 0.851 229.3	PUN TST P TN CON	177 571 1 66	SFQ MACH C	1 0.850 229.4	2 0.850 229.4	3 0.850 229.4	4 0.850 229.4	5 0.850 229.0	6 0.850 229.C	7 0.850 229.0	8 0.848 228.6	9 0.849 229.1	10 0.849 229.1	4 622 058 0 11	12 0.850 229.4	13 0.850 229.4	14 0.852 229.8	15 0.852 229.8	

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1.000 0.9999 665°0 665°0 665 0.599 1.000 666.0 0.599 0.599 1.000 0.599 0.599 0.999 -L 66 :0 -0.010 -0.012 -0.012 -0.012 -0.010 -0.010 -0.019 ¢, -0.012 -0.012 -0.014 -0.015 -0.012 -0.012 -0.021 -0-01 ŝ 0.000 0.000 0.000 0• 000 0.000 U. 000 0.000 0.000 0.000 0.000 000 000 0.000 0.000 3 . 0.929 909 0.920 0.929 0.984 918 950 986 F/V 6.995 366 0.919 0.939 0.924 0.916 0.911 • ් > • <u>.</u> 0 ALPHA 0.00 0.000 0000-0 000 0.000 c. 000 c. 000 0 A V O 000.0 000-0 000-0 000.0 c. 000 0.00.0 0.000 0.967 0.937 0.841 0.851 0.851 070.1 0.844 0.827 0.861 66.4 QF/Q 0.837 0.380 .901 0.989 0.843 O O Ó 0000.0 0.000 0.000 0.000 0.000 811 0000-000 0.000 0.00.0 000-0 0.000 0 79.5 MF / N C.984 C.968 556°D C.923 C.528 C.915 516.0 0.928 055°) 526°) C.986 C.955 C.917 C.918 C.91C 0.96 1.47 1.96 -0.71 -0.54 -0.37 -1.54 0.13 0.38 0.46 0.63 891 Z / DB -0.20 -0.03 -2.04 **P** C.250 1.517 1 J/Na ¥7.08 C • 41 C • 41 O • 41 0.41 C.41 C.41 C.41 C.41 C.41 C.41 C.41 C • 41 C • 41 C • 41 C • 41 MACH x / FB 0 87 10 87 10 87 10 87 10 87 10 87 10 87 10 87 10 87 10 87 10 87 10 87 ŝ CONF 11 C(66 0 779.5 779.5 779.5 779.5 779.5 5-51 5-51 5-51 79-51 5-52 5-52 5-52 5-52 D. 571 1 №
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0.9999 665°0 0.9999 0.599 DF/D 0.999 665 665 0.999 665.0 665*0 0.999 0.999 000 000 . . 0 --0.021 -0.028 -0.025 -0.925 -0.030 -0.019 -0.030 -0.019 -0.010 -0.010-0.021 -0.021 -0.021 -0.021 ð 0.000 0• 000 0• 000 0.000 0.000 0.000 2/2 0.000 0.000 000 0.000 0.000 > 0.912 0.914 0.896 VF/V 0.940 416 0.947 931 984 992 0.945 0.394 0.911 0.891 0.894 0.927 0 . 0 0 0.00 ALPHA c.000 0.000 0A/0 0.00.0 0.000 c•000 c•000 0.00.0 000.0 000.0 c.000 0.000 .000 c.000 000.0 0.827 0.792 66.2 QF/Q 0.881 0.891 0.894 C.829 C.796 0.801 C.796 0.857 0.833 C.864 0.833 968 986 °• • 0.000 0000-0 0.000 1812 MA/N 0.000 0.000 0.000 000.0 0.000 0.000 ۵ 78.8 MF/W C.935 C. 944 C.946 C.911 C.852 0.895 C.892 0.990 619.0 0.926 016.0 C.913 C-93C N **-**587 56 Ċ Ĵ 5 0.249 1.512 1892 X/CB Y/DP Z/DP 10.87 -0.03 -2.04 C 1C.87 -0.03 -1.54 C 10.87 -0.03 -1.04 C 1C.87 -0.03 -0.71 C C -0.37 0.13 0.46 0.63 6 -0.04 0.54 • 4 σ ٠ RN/L -0-03 -0-03 -0.03 -0.03 -0.03 -0.03 -0.03 NACH C.87 C.87 C-87 C-87 C-87 0.87 0.87 87 ω 000 ഹ CCNF 66 0 78.8 78.1 78.1 78.1 78.1 78.1 78.1 78.1 78.178.1 8.1 œ αu **.** . N L 78. 78. œ τ 571 571 0.246 0.246 0.246 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 Φ σ ST 4 $\sim \sim$ • PUN 179 SEQ 10 22 NW4W9200 3 4 ഹ

		pr/p	0.999	1.000	0.9999	665.0	0.9999	0.999	665*0	665*0	0.999	0.999	0.999	665*0	0.999	0.599	666°0
		C D	-0.019	-0.010	-0.021	-0.023	-0-021	-0.012	-0.012	-0.021	-0.021	-0.021	-0.021	-0.021	-0.012	-0.021	-0.019
		V A / V	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	000000	0.000	0.000	0.000	0.000	0.000
_	_	VF/V	0.994	0.980	0.946	0.938	0.924	0.907	0.891	0.902	0.911	0.901	6.904	0.955	0.942	0.966	166*0
ALPHA	0.00	0A/Q	C.00U	0.00.0	0.00.0	000.0	0.00.0	c.000	0.00.0	c. 000	0.00.0	0.000	c.000	000.0	C.00U	0.000	0.000
11	65.9	0F/0	C.987	0.960	C•892	0.822	C.852	C. 820	0.792	0.811	0.827	0.810	0.815	0.910	0.836	0.932	0.981
٩	1812	N / VN	0000-0	0000.0	0.000	0.00.00	000.0	0.000	000.0	0000.0	0000.0	0.000	0.000	0.000	0.000	0.00.0	0.000
e	78.1	NF / N	0.954	C.98C	C.945	C.907	C.923	0.506	068.0	C•5C1	0.910	005.0	0.903	0.954	C * 5 * 2	0.566	C• 591
L pT	é 1891	Z/08	-2.03	-1.54	-1.05	-0-71	-0-54	-0.37	-0.21	-0-05	0.13	0.30	0.46	0.63	0.56	1.47	1•96
H PN/	8 1.50	Y/08	-0-38.	-C.38	-0-38-0-	-0.38	- C.38 -	-0-38	-0.38	- C • 3 8	-0-38	-0.38	-0.38	-0.38	-0-38	-0.38	-0.38
F VAC	5 0.24	X / CB	10.87	10.87	10.87	1C-87 -	10.87 -	10.87	10.87 -	10.87	10.87	10.87	1C.88 ·	1C - 88	1C.88 ·	1C.88 ·	10.87 -
TN CCN	66	o	78.1	78.8	78.1	78.1	78.1	78.1	78.8	78.8	78.1	78.1	78.1	78.1	78.8	78.8	78.8
TST P	1 1 L S	MACH	1.248	1.249	.248	.248	1.248	.248	3.249	.249	3.248	0.248	.248	3.248	0.249	.249	.249
NUA	180	SEG	10	2	n O	4	50	9	2 2	8	0	10 0	11 0	12 0	13 0	14 C	150

I.

				666.0	1,000		566 · C	0.999	0,040		666°0	0.999	00000		0.999	0.999	000 0		777.0	0.999)))))	1.000
		c c	7	-0.019	-0-010		-0.014	-0.012	-0-012		120.00-	-0.028			-0.030	-0-012	-0-012		710.0-	-0.012			-0.010
			V A / V	0.000	0-000			0.000	0.000		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.000	0.000		0.000	0.000	00000		000.00	0.000	0.000		0.000
		V. 2 V V		166.0	0.976	0.955		0.913	0.906	000	000	0.924	0.915		0.400	0.915	0.909	1000	176.0	0.952	0.990		0.990
AI PHA				000-0	0.00.0	0.000		000-0	c. ouo	0.000		000-0	0.000		000-0	0.000	000.0	0000		c. 000	0.000		000.0
TT	65.7	OF/O		104.0	0.951	0.910		U•8.5I	0.818	C2822		0.852	0.834		0.000	0.835	0.823	0.858		0.905	0.979		6.919
٩	1812	N / VN		222.0	0.000	0.000		000.00	000.0	000-00		0.000	0.000		000.00	000.0	0.000	0.000		0.000	000000		000.00
ى	78.8	NE / N	100 0		C-975	C.954			C.905	102-0			C.914	0000		- 615 - 2	0° 908	100		192.	065-0		- - - - - - - - - - - - - -
Lo .	1892	Z/DB	5	- 	-I-54	1.04			0.53	0.38		.12.0	0.04	0 1 2		0.25	0.47 (0.63 (0.96 (1.46 (1 07 1	1 - 2 - 1
RN/I	1.514	Y/DB	37.0		- 84° -	C-48 -	- av 0		0•48 -	C.48 -	0 × 0	1 0 1 1 0	C.48 -	0.49		C• 4 8	0.48	C.48		C. 4 X	0.48	375	0
F NACH	5 0.249	X / 0.3	10.87 -		- J8.JI	10.87 -	10.87 -	~ 1	- / R *) T	10.87 -	1 0 07		10.87 -	10.87 -		10.87	10.87 -	1C.87 -		10.87 -	1C.87 -	1 C 87 -	- C - C -
TN CON	66	c	78.8		8.81	78.1	78.8		C + 5 /	78.8	2 a C		78.8	78.8) L) - P	n • n -	19.5	5-51	300	C • A -	19.5	79.5	•
TST P	571 1	MACH	0.249		557-1	3.248	7.249		062.0	0.249	0720		J. 249	.249				0.250	0000		3.250	1.250	
RUN	181	SEQ	1	Ċ	V	m	4	·u		9	7.6	- (× ×	6				12 (12		14 0	150	> 1 1

		F/V VA/V Co PF/P		894 0.000 -0.076 0.999	394 0.000 -0.076 0.999 336 0.000 -0.022 0.999	394 0.000 -0.076 0.999 886 0.000 -0.022 0.999 836 0.000 -0.021 0.999	394 0.000 -0.076 0.999 886 0.000 -0.022 0.999 836 0.000 -0.021 0.999 832 0.000 -0.024 0.999	894 0.000 -0.076 0.999 886 0.000 -0.022 0.999 886 0.000 -0.021 0.999 832 0.000 -0.024 0.999 392 0.000 -0.024 0.999 301 0.000 -0.024 0.999	894 0.000 -0.076 0.999 886 0.000 -0.022 0.999 836 0.000 -0.021 0.999 835 0.000 -0.024 0.999 892 0.000 -0.024 0.999 892 0.000 -0.024 0.999 901 0.000 -0.024 0.999 905 0.000 -0.012 0.999	894 0.000 -0.076 0.999 886 0.000 -0.022 0.999 886 0.000 -0.021 0.999 892 0.000 -0.024 0.999 892 0.000 -0.024 0.999 901 0.000 -0.024 0.999 916 0.000 -0.023 0.999	894 0.000 -0.076 0.999 886 0.000 -0.022 0.999 886 0.000 -0.021 0.999 832 0.000 -0.024 0.999 901 0.000 -0.024 0.999 906 0.000 -0.012 0.999 916 0.000 -0.023 0.999 959 0.000 -0.021 0.999	894 0.000 -0.076 0.999 886 0.000 -0.022 0.999 886 0.000 -0.021 0.999 886 0.000 -0.024 0.999 892 0.000 -0.024 0.999 901 0.000 -0.021 0.999 905 0.000 -0.012 0.999 916 0.000 -0.021 0.999 959 0.000 -0.021 0.999 969 0.000 -0.021 0.999
ALPHA	0.00	JA/Q VF/	000 0 AG		.000 0.88	R8 0 000 88 88 900 900 88 89 900 900 88 900 900	58 0 000 88 0 000	88 0 000 88 0 000	96 0 000 96 0 000 98 0 000 88 0 000 88 0 000	16 0 000 06 0 000 58 0 000 88 0 000 88 0 000	000 0 90 000 0 88 000 0 86 000 0 0 86 000 0 86 0000 0 86 000 0 000 0000000000	950 0 900 96 0 900 90 0 900 900
	65.5	QF/Q Q	.796 0.		.782 0.	.782 0.	-782 0- -782 0-	-782 0. -782 0. -792 C.	-782 0. -782 0. -792 C. -810 0.	-782 0 -782 0 -792 C -1-792 C -1-792 C -1-792 C -1-818 0 -836 0	782 0. 782 0. 1.792 0. 1.810 0. 1.818 0. 1.836 0.	782 0. 782 0. 782 0. 810 0. 818 0. 918 0. 918 0.
Q	1812	WA/W	0.000.0		0.000.0	0.000.0	0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000	0.000 0 0.000 0 0.000 0 0.000 0	000000000000000000000000000000000000000			
Ç	78.8	MF/N	3.852 0		3.885 0	3.885 0 3.885 0	3.885 0 3.885 0 0.891 0).885 0 3.885 0 3.885 0 0.891 0 0.900 0).885).885).885 0.891 0.891 0.900 0.915 0.915 0.915 0.915 0.915	0 885 0 885 0 8885 0 8885 0 8885 0 8885 0 8885 0 90 8885 0 90 8855 0 90 80 80 80 0 90 80 80 80 0 90 80 80 0 90 80 80 0 90 80 80 80 0 90 80 80 80 0 90 80 80 80 80 0 90 80 80 80 0 90 80 80 80 80 80 80 80 80 80 80 80 80 80	0 0 0 0 0 0 0 0 0 0 0 0 0 0
L p1	4 1892	Z/CP	-0.37 (-0.19 (-0.19 0	-0.19 C	-0.19 C	0.19 0.13 0.13 0.13 0.46 0.13	-0-19 -0-0-04 -0-0	-0-19 -0-0-0-04 -0-0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0-04 -0-0	-0-19 -0-19 -0-00-00-00 -0-00-00-00-00-00-00-00-00-
	1.514	γ/ŋ Β	- 00-0		00.0	00 - 00 - 0						
	5 0.245	X / DP	IC.00		1C.00	10.00 10.00	10.00 10.00 10.00	10.00 10.00 10.00 5.59	1C 00 1C 00 1C 00 5 59 9 59	1C.00 1C.00 1C.00 9.99 5.99	10.00 110.00 10.00 10.00 9.99 9.99 9.99	1C•00 1C•00 5•59 5•59 5•59 5•59 5•59
TN CONF	56	0	78.8		79.5	79.5	20.01 20.01	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0	200 200 200 200 200 200 200 200 200 200	677 677 677 677 677 677 677 677	
TST P	5711 (MACH	0.249		0.250	3. 250	0+250 0+250 0+250	0, 250 0, 250 0, 250 0, 250	0.250 0.250 0.250 0.250	2 2 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2000 2000 2000 2000 2000 2000 2000 200	2000 2000 2000 2000 2000 2000 2000 200
RUN	182	SEQ	-		2	20	0000 0 m 4	00000 0000	000000 0 m 4 m 0	000000 0 m 4 m 0 M	0000000 0 m 4 m 0 m 0	00000000000000000000000000000000000000

		pF/p	1.000	666*0	665*0	0.999	0.999	0.999	666.0	0.998	0.598	666*0	0.598	0.999	0.599	0.999	666•0
		СР	-0.010	-0.019	-0.012	-0.025	-0.025	-0.019	-0.025	-0-039	-0-037	-0-025	-0.037	-0-028	-0.021	-0.019	-0.019
		V A /V	· 000 • 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
		VF/V	0.937	0.950	0.937	0.902	0.850	0.855	0.814	0.833	0.886	0.868	0.894	0.909	0.947	0.992	166.0
ALPHA	00 • 0	QA/Q	0.000	0.000	000.000	C. U00	0.00.0	0.00.0	000 • 0	0.00.0	0.00.0	C. UQU	0.00.0	c. 000	c. 000	0.00.0	000- 0
11	65.4	QF /0	0.876	0.901	0.877	0.811	C.720	0.727	0.659	0690	0.782	0.750	0.796	0.824	0.895	0.982	0.981
٩	1812	W V V W	0000.0	0.000	0000.0	0.000	0.000	0.000	0000.0	0000.0	0.000	0.000	0.000	0.000	000.00	0000.0	0000.0
U	78.8	NF / N	0.936	0-95C	0.937	0.901	(•845	0.853	0.812	0.832	0.885	C.867	0.893	C.9C8	C.947	155.0	156°0
L pT	5 1892	Z/FR	-2.02	-1.51	-1.01	-0.68	-0.52	-0-35	-0.19	-0.01	0.15	0.32	0.48	0.66	56*0	1.45	1.95
ING -	1.51	Y/CP	0.01	0.01	0.01	C•01	0.01	C.01	0.01	C.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
VACH	0.245	X/CB	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05	7.05
N CONF	с С	с С	8•8	8.1	8.1	8°8	8.1	8 . 8	8.8	8°8	8 . 8	8.8	8 . 8	8.8	8 . 8	8 . 8	9 • 8
STPT	71 1 6	LCH VCH	249 7	7 842	248 7	249 7	248 7	1 642	1 642 J	7 945	249 7.	7 642	249 7	7 642	7 945	1 542	1 640
UN TS	83 51	NN UH	1 0.2	2 0.3	3 0.2	4 0.5	5 0.2	6 0.2	7 0.2	8 0.5	0.6	10 0.2	11 0.2	12 0.2	13 0.5	14 0.2	15 0.2
α.	-	S															

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PF/P 0.999 1.000 1.000	0, 999 0, 9990 0, 9990 0, 9990 0, 9990 0, 9990 0, 9990 0, 9990 0, 9990 0	665 °0 665 °0 665 °0 665 °0 665 °0 665 °0	рғ/Р 1.000
CP -0.017 -0.010 -0.010	-0.017 -0.021 -0.033 -0.030	-0.039 -0.039 -0.023 -0.021 -0.012 -0.019	0100 -0-010 -0-010
× ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓			V ∧ V 0.0000
VF/V 0.992 0.973	0.908 0.884 0.909 909	0.937 0.895 0.895 0.929 0.929 0.929	VF/V 0-932
AL PHA 0.00 0.00 0.000 0.000 0.000 0.000			ALPHA 0.00 0A/0 0.000
TT 65.3 0F/0 0.984 0.972 0.972	0.822 0.778 0.804 C.824	0.801 0.801 0.806 0.865 0.861 0.981 0.989	TT 65.3 0670 0.887
3 1812 MA/M 0.0000 0.000			3 1811 MA/W 0.000 0.000
С МГ/М 0.992 С.985 С.573	C • 9C 1 C • 898 C • 5C 8	C. 8996 C. 8996 C. 923 C. 923 C. 933 C. 933 C. 933 C. 933 C. 933 C. 935 C. 9355 C. 9355 C. 9355 C. 9355 C. 9355 C. 9355 C. 9355 C. 9355	C 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
L PT 5 1892 2/08 -2.03 -1.52	-0-10-10 -0-35 -0-19		L PT 5 1891 -2,02 -1,53
9 9 1 7 1 7 1 7 7 7 7 7 7 7 7 7 7 7 7 7	1 1 1 0 0 0 0 0 4 4 4 4 0 0 0 0 0 0	0 10 10 10 10 10 10 10 10 10 10 10 10 10	F RN/ 91.51 -0.01 -0.01
F VAC 5 0 24 X/CB 8 49 8 49	8 8 8 8 8 8 • • • • • • • • • • • •	0 0 0 0 0 0 0 0 0 0 0 0 0 0	F VAC X 7.24 8.49 8.49
TN CCN 66 C 78.8 78.8 78.8	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	779.88 28.88 28.88 28.87 28.87 28.88	11 CCN 56 738 88 88
TST P 571 1 MACH 0.249 0.249 0.249	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	00 250 00 249 00 250 00 200 00 200 00 200 00 20000000000	TST P 571 P MACH 0.249 3.249
285 285 285 285 285 285 285 285 285 285	450000	0000040	810 850 200

		pr/p	1.000	1.000	1.000	665.0	0.999	0.599	0.998	665.0	0.999	0.9999	0.999	0.999	0.599	1.000	1.000	
		ڻ <u>م</u>	-0.010	-0.010	-0.010	-0.012	-0.021	-0.025	-0.037	-0.033	-0.033	-0.033	-0.028	-0.033	-0.021	-0.001	010-0-	
		V A / V	0.000	0000.0	0.000	0.000	0.000	0.000	U. 000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	-	VF/V	0.932	0.942	166.0	0.909	0.873	0.878	0.887	0.8555	0.876	0.388	0.915	0.933	0.949	0.982	0.995	
ALPHA	0.00	0A/Q	0.00.0	0.000	0.00.0	0.00.0	c. 000	0.00.0	0.00.0	0.00.0	000.0	c. 000	0.00.0	000.0	0.00.0	C.000	000-0	
11	65.3	0F/0	0.867	0.886	0.902	0.823	C.759	0.768	0.783	0.728	0.764	0.785	0.834	0.868	006-0	0.964	0.989	
٩	1811	MAZM	0000.0	0.000	0000.0	0000.0	0.000	0.000	000.000	0.000	0.000	0.00.0	0000.0	0.000	000.000	000.0	0.000	
U	78.8	N/ JR	C.931	C.942	036.0	C. 508	C.872	0.877	C.886	C • 854	C.875	C.887	0.914	5-6-D	C.945	0.982	C.9955	
- PT	5 1891	1/08	-2.02	-1.53	-1.03	-0-65	-0.53	-0.36	-0.20	-0.02	0.15	0.31	0.48	0.65	0.98	1.48	1. 98	
	9 1.51!	Y/DB	- 10-0-	- 10.0-	- 10-0-	-0-01 -	- 10.0-	-10.0-	- 0.01 -	- 10-0-	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	
L VAC	5 0.24	X/FB	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	
TN CCN	66	C	78.8	78.8	78.8	2-62	78.8	78.8	78.8	2°61	78.8	78.8	3.97	2.61	79.5	80.2	2.91	
TST P	571 1	MACH	0.249	0.249	0.249	0.250	0.249	0.249	0.249	0.250	0.249	0.249	0.250	0.250	0.250	0.251	0.250	
2	85	2	-	2	~	4	ŝ	\$	~	e e	6	10		12	13	14	15	

555 °C 6655 °C 6655 °C 6655 °C 5555 °C 0•999 0-999 0.999 0.999 666 u/⊐ 666 000 000 0 ċ _____ **C**. . CP -0.019 -0.019 -0.021 -0.021 -0.021 -0.029 -0.029 -0.029 -0.023 -0.012 -0.012 \mathbf{O} C 10. -0.01 0 U. 000 0. 000 000 0.000 **.** 0.993 0.978 0.978 0.913 0.913 0.913 0.912 0.912 VF/V 0.993 906 0.910 944 0.982 988 0.906 ੱ ं ిం AL PHA 0.00 04/0 0.000 0.000 0.000 0.000 0000.0 c. 000 c. 000 c. 000 c. 000 0.00.0 0.000 0.000 0.000 c.000 000.000 918 818. 65.4 67.4 67.7 0.986 0.986 0.955 0.818 0.832 0.861 C.872 C.828 O.837 827 890 964 5 976 ్ర • 0 . 5 0 0.000 1811 M / M 000 000 0.000 0.000 00 ۵. 0 0 0 N 08 80•2 ₩F / Y 506.0 0.999 0.999 0.997 0.978 0.978 0.928 0.928 0.928 0.537 0.531 0.915 c.905 c.905 .944 .982 m a ŝ 2/08 2/08 -2.03 -1.52 -1.65 -1.63 -0.69 3-0.36 -0.17 -0.02 0.14 0.31 0.48 0.64 Fa. • 4 σ • F MACH PN/L 5 0.251 1.528 • • • • • • • • **C**11 4. \mathbf{c} 00 CONF Ο. ----

0E/D	1.031	1.029	1.021	1.015	1.013	1.011	1.010	1.007	1.005	1.005	1.006	1.003	1.004	I.004	1.006	1.025
a C	0.049	0.046	0.033	0.023	0-020	0.017	0.015	0.010	0.007	0.009	0.009	0.005	0.007	0.006	0.010	0-040
V A / V																
A 0 VF/V	0.971	0.971	0.960	0.929	0.933	0.944	0.930	0.932	0.920	0.901	0.902	0.895	0.906	0.925	0.961	0.974
ALPH/ 20.00 04/0																
TT 63.8 0F/0	0.962	096.0	0.942	0.854	0.861	0.884	0.852	0.855	0.827	0.789	0.792	0.775	0.798	0.838	0.917	0.963
979 879 878																
240.7 NF /N	C.966	0.966	0.960	0.918	0.922	0.935	C.919	C.922	C.907	0.386	0.888	C.879	C.891	0.914	0.954	C•965
PT 679 2/DR	2.04	1.54	1.04	0.71	0.53	0.37	0.20	0.04	0.12	0.29	0.46	0.63	0.96	1.16	1.47	1.96
RN/L 1.484 7/DB	0.41 -	0.41 -	- 15.0	0.41 -	0.41 -	0.41 -	0.41 -	0.41 -	0.41	C.41	0.41	C.41	0.41	0.41	C.41	0.41
F MACH 5 0.952 X/PB	10.88	1 C. 88	1C.88	10.87	10.87	10.88	1C.88	1C-88	1C.88	1C.88	10.88	1C.88	1C.88	1 C - 88	1C-88	10.87
TA CCN 66	240.7	240.7	240.7	240.1	240.1	239.6	240.1	239.6	239.6	239.6	238.8	238.8	239.3	239.3	239.7	239.3
TST P 571 1 MACH	0.952 2	0.952	0.952 2	C.950 2	0.950 ¿	0.950 2	2 0 2 6 * 0	0.950	0.950 2	0.950	0.947 2	. 749.0	0.948	0.948	2 576 0	0.948 2
20N 550	0	m	4	ഹ	Ŷ	~	ω	σ	10	11	12	13	14	5	16	17

		p pr/p	031 1.020	040 1.026	032 1.021	026 1.016	025 1.016	019 1.012	015 1.010	015 1.009	012 1.008	014 1.009	005 1.003	004 0.598	008 0.595	004 0.998	009 1.006	040 1.025			b pr/p	031 1.020	.028 1.018	.024 1.016	022 1.014	024 1.015	.027 1.017	.018 1.011	021 1.013	.013 1.008	.009 1.005	.005 1.003	001 0.599	.008 1.CO5	005 1.003	.015 1.009	.043 1.027
			•0	•0	•0	•0	•0	•	•	•0	•	•0	•0	• 0 -	•0-	•0-	•0	0				0	0	.0	•	•	0	0	0	ċ	c	0	0-	0	o l	0	0
ALPHA	20.00	0A/Q VF/V	0.912	0.926	0.928	0.916	0.902	0.899	0.895	0.891	0.891	0.887	0.895	0.894	0.902	0.903	0.943	0.972	ALPHA	20.00	QA/Q VF/V	0.973	0.975	0.968	0.936	0.915	016.0	0.909	0.912	0.893	0.881	0.894	0.886	0.895	0.922	0.941	0.966
11	65.3	QF /Q	0.824	0.856	0.857	0.828	0.799	061.0	0.781	0.773	0.771	0.765	0.776	0.769	0.783	797.0	0.877	0.959	TT	66.3	0F/0	0.956	C.958	C•940	C.869	0.825	0.316	0.811	0.818	0.777	0.751	0.773	0.756	0.778	0.830	0.877	0.948
٩	377	MV/W																	۵	378	MA/W																
C)	240.6	ME /N	0.895	C.914	C.916	C. 902	0.887	0.384	C.879	C.875	0.875	C.871	C.880	0.878	0.887	0.894	C.934	0.967	Cr	3 241.2	MF/N	0.968	C-97C	C.962	C-926	0.901	0.356	C.895	C.899	C.878	0.364	C.878	C.370	C.38C	0.910	0.932	0.961
L PT	7 678	Z/08	-2.04	-1.55	-1-04	-0.70	-0-54	-0.38	-0.21	-0-04	0.13	0+29	0.46	0.62	0.56	1.16	1.46	1.97	L pT	6 670	Z/DP	-2.04	-1.54	-1.05	11.0-	-0.54	-0.37	-0.21	-0.04	0.13	0.30	0.47	0.64	15.0	1.17	1.46	1.96
F RN	4 1.47	Y/08	-0-03	· 20 • 0 -	- 20-0-	-0-03	-0.03	-0-03	-0-03	-0-03	-0.03	-0-03	-0.03	-0-03	-0-03	-0.03	-0.03	-0.03	ли ч	4 1.47	Y/CB	-0.38	-0.38	-0.38	-0.38	-0.38	-C.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0-38
VF VACI	5 0.95	X/DB	10.88 -	10.88 -	10.88 -	1C.88	10.88 -	IC.88.	10.88	10.88	1C.88	10.88	1C.88	10.88	10.88	10.88	10.87	10.87	NF VAC	5 0.95	X/Cq	10.87	10.87	10.88	10.87	10.87	10.87	1C.87	10.88	10.87	10.87	10.87	10.87	10.87	IC.87	1C.87	10.87
TN CC	66	Ç	240.6	240.1	240.1	24C.1	240.1	235.6	239.6	239.3	239.3	239.3	238.9	238.9	239.3	240.2	240.2	239.3	C TN CC	66		241.2	241.7	241.7	241.1	240.1	240.1	239.1	239.1	239.2	239.6	239.3	239.7	239.7	239.3	239.3	238.0
TST P	571 1	MACH	0.954	0.953	0.952	0.951	0.951	0.950	0.950	0.948	0.948	0.948	0.946	0.946	0.947	0.950	0.950	0.948	1 121	571	MACH	0-954	0.956	0.957	0.956	0.953	0.953	0.949	0.949	0.949	C.950	0.948	0.945	0°045	0.947	0.947	0.944
RUN	188	SEQ	-	2	6 7)	4	5	9	2	æ	6	10	11	12	13	14	15	16	NIN	189	C L V	,	5	(m)	4	U)	v	1	8	5	10	11	12	13	14	51	16

1.005 1.009 1.008 1.005 1.007 1.002 1.009 1.004 1.021 1.020 1.013 0.970 1.002 1.021 965-0 0.588 0.983 1.023 1.022 1.013 1.011 0.592 f/p 1.019 1.000 1.026 1.008 1.000 166.0 1.001 1.000 0.981 027 ۵ _ 0•033 0•032 0.029 0.020 0.033 0.006 0.007 0.015 500.0 0.034 -0.000 0.013 0.012 0.047 0.002 -0.000 £00°0 0.003 0.014 0.021 0.017 0.012 -0.007 -0.015 -0.019 -0.026 -0.013 -0.000 0.038 -0.031 0.041 3 ð V A /V V V V 0.921 0.916 0.945 0.978 0.977 0.966 0.928 0.922 0.924 0.940 0.910 0.927 0.893 0.975 TT6.0 0.966 0.928 0.943 0.895 VF/V 0.931 0.952 0.974 0.895 VF/V 0.929 980 0.908 0.893 0.927 0.939 0.975 . AL PHA 20.00 20.00 0A/0 ALPHA 0 A / 0 0.938 0.836 C.845 O.850 0.963 0.822 CF/Q 0.851 0.831 819 0.849 0.769 C.800 0.852 0.872 0.800 0.777 0.765 0.756 11 67.1 899 966 0F 70 0.941 853 855 975 0.969 0.965 0.775 69.1 0.880 0.843 941 0.834 0.968 5 . 00 0 . N/VN 384 382 MA/W ۵ ۵ 242.0 C.917 MF /N C.974 C.96C C.910 0.915 0.920 0.908 C.936 0.877 NF / N 0.973 C.97C C.96C C.917 0.933 C•930 C.922 0.896 C.97C .903 0.929 0.972 C.854 C.877 C.880 0.918 0.886 C.880 0.912 0.944 **C.915** 0.976 C.97 242 \circ 9 1.483 685 Y/DR Z/DB 5 0.952 1.479 684 X/08 Y/08 Z/08 -2.03 -1.05 -0.65 0.14 0.48 0.63 -0-37 0.47 0.96 -0.36 0.65 -0.48 -2.05 -0.48 -1.54 0.29 .16 -1.52 -0-15 ω -0-04 0.12 •46 -1.03 -0.03 ω ω a Fa. -0.54 PT 6. 36.0 4. σ, NACH RN/L 0.949 1.483 RN/L 0.43 0.43 -C.48 -0.48 -0-48 -0.48 -C.48 -0.48 .48 0.43 C+43 0.43 C. 43 - 43 C.43 • 43 -C.48 C.43 C.43 0.43 • 43 -0.48 -0.48 -0.48 -0.48 -0.48 -C.48 4. 4 9 Ó C NACH X/CB 0.87 X/08 8.49 C. 87 10.87 8.49 8.49 8.49 C. 87 0.87 0.87 E.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 C. 87 C.87 C.87 C.87 C. 87 C. 87 C.87 0.87 8.49 8.49 8.49 8.49 TN CCNF ŝ CONF 242.0 242.0 242.4 242.4 242.4 242.4 242.4 242.4 242 4 242 4 242 4 242.4 242.4 242.4 241.5 241.5 S 241.9 5 4. SU) 15 σ $\mathbf{\circ}$ 241.9 241. 241. 241.9 241.(242. • 66 242 66 O Z O 24 u. TST F 571 1 MACH 151 P 571 1 MACH 0.949 0.952 0.952 0.952 0.951 0.951 0.951 0•952 0•953 0.954 0.957 0.957 0.950 0.950 0.950 0.956 0.956 0.956 0.948 0.950 0-950 0.950 0.950 0.948 0.951 948 0.950 . : PUN 190 SFQ 0 5 m 5 2 3 14 123 ~ œ o 0 ŝ RUN NUN 191 SFG 0 4 m S ~ ω o 15 16

		V CP PF/P	0.021 1.014	0.026 1.017	0.017 1.011	0.009 1.006	0.009 1.006	-0.002 0.999	-0.004 0.598	-0.010 0.994	-0.019 0.988	-0.018 0.588	-0.022 0.986	-0.025 0.984	-0.013 0.592	-0.004 9.997	0.011 1.007	0.042 1.026			۷ (۵ ۵۶/۵	0.031 1.020	0.028 1.C18	0.028 1.018	0.017 1.011	0.009 1.006	0.001 1.001	-0.003 0.598	-0.008 0.995	-0.012 0.992	-0.016 0.990	-0.014 0.991	-0.011 0.993	-0.007 0.996	-0.014 0.591	0.007 1.005	0.039 1.025	
ALPHA	20.00	CA/U VE/V VA/	0.913	0.927	0.935	0.919	0.914	0.900	0.886	0.872	0.835	0.879	0.368	0.868	0.391	0.926	0.962	179.0		20-00	DA/O VE/V VA/	0.976	0.977	0.971	0.935	0.915	0.904	0.901	0.899	0.893	0.887	0.865	0.878	0.903	0.939	0.979	0.980	
TT	3 68.6	M 0F/0	0.821	C.853	0.865	0.825	0.816	0.782	0.754	0.724	0.744	0.734	0.711	0.710	0.759	0.833	616.0	0.973	ŢŢ	1 64 6	M CF/O	C•963	0.964	0.950	0.865	0.819	0.791	0.783	0.776	0.763	0.751	0.709	0.734	0.785	0.856	0.956	0.976	
a .	4 38	VA/																_	۵	2 C	MA/									_							_	
U	5 242.	N / J N	0.900	C.916	0.925	0.906	0.901	C.885	C-865	C-853	0.868	C.862	(•84S	C-850	C.875	C.914	0.955	C.974	L.	242		C.972	6.973	C.966	0.925	0.902	C.885	0.886	0.883	0.877	0.871	C-846	C.860	0.888	0.929	0.976	C.976	
L pT	89 83	Z/C8	-2.03	-1.53	-1.02	-0-65	-0.53	-0.36	-0.19	-0.01	0.15	0.31	0.48	0.65	0.58	1.18	1.48	1.98	10	5 × 57	2/58	-2.02	-1.52	-1.03	-0-69	-0.52	-0.36	-0.19	-0.01	0.14	0.32	0.48	0.65	0.58	1.18	1.48	1.58	
L RV	1 1.47	Y/C8	-0-01	-0.01	-0-01	-C•C1	-0-01	-0-01	-0-01	-0.01	-0-01	-0-01	-0.01	10.0-	-0.01	-0-01	-0-01	-0.01		0 1 67		-0-36	-0.36	-0.36	-0.36	-0.36	-0.36	-0.36	-0.36	-0.36	-0.36	-0-36	-0.36	-0.36	-0-36	-0-36	-0.36	
F VAC	5 0.95	X/58	8.49	8.49	8.49	8.49 -	5.49 ·	8.49 -	8.49	E. 49 -	8.49 -	8.49	6 4 9	8.49	E. 49	E.49 -	E.49	E.49 .		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	X/CB	£ • 49	8.49	8.49 -	8.49	8.49	8.49	8.49	8.49	8.49	8.49	64.8	8.49	8.49 -	8.49	E.49	8.49	
TST P TN CCN	571 1 66	MACH C	0.951 242.4	0.952 242.3	0.951 241.6	0.953 242.9	0.953 242.5	0.953 242.9	0.951 242.4	0.951 242.4	0.951 242.4	0.951 242.4	0.952 242.9	0.952 242.9	0.952 242.9	0.951 242.4	0.950 241.5	0.950 241.9	IST D TV CCN	571 1 66 C	MACH 0	0.952 242.3	0.952 242.3	0.953 242.5	0.952 242.9	0.954 243.4	0.952 242.9	0.950 241.9	0.949 241.4	0.949 241.4	0.949 241.4	0.949 241.4	C.947 241.C	C.948 241.5	0.946 241.1	C.949 242.C	0.948 241.5	
RUN	192	SEG	-	2	ŝ	4	ŝ	9	2	ω	ნ	10	11	12	6	14	15	16	NIId		N LO		~	~ 1)	4	Ś	9	2	¢	σ	10		12	2	14	15	16	
		4/V Co bE/p	0.032 1.020	0.031 1.020	0.022 1.014	0.012 1.008	0.007 1.004	0.001 1.000	-0-006 0-596	-0.007 0.996	-0.017 0.589	-0.021 0.987	-0.022 0.586	-0.017 0.589	-0.008 0.995	-0.011 0.593	0.004 1.002	0.041 1.026				4/V CP PF/P	C-037 1.C21	0.032 1.018	0.028 1.016	0.030 1.617	0.029 1.016	0.034 1.019	0.020 1.011	0.020 1.011	0.019 1.011	0.021 1.012	0.021 1.012	0.023 1.013	0.020 1.011	0.023 1.013	0.042 1.024	0.054 1.031
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ALPHA	20-00	DA/Q VF/V VA	616*0	179.0	0.974	0.939	0.927	0.922	0.928	0.909	0.905	0.900	0.874	0.876	0.916	0.960	0.979	0.980		ALFHA Do co		DA/U VF/V VA	0.928	0.933	0.427	0.905	0.902	0.888	0.884	0.884	0.878	0.881	0.879	0.875	0.896	u.919	0.937	0.965
TT	2 69.5	N GF/O	016-0	0.966	0.954	0.869	0.843	0.827	0.836	0.797	0.784	0.772	0.723	0.729	0.811	0.903	0.954	0.978	+	י ה	1.00 5	M 0F/0	0.860	0.869	0.854	0.808	0.803	0.778	0.763	0.763	0.751	0.758	0.755	0.747	0.786	0.835	0.880	0.949
D .	. 38	V MA/	LL \	6 0	0	œ	Q	5	6	4	0	4	ę	8	6 1)	(7)	ç	Ŷ	C	2 C		N *** V	æ	4	-	Ci	ሙ	C 11	υ.	Б	2	Ģ	4	ۍ ا	2	œ	~	Cr.
С ^у	4 242	NF /	C.97	C.97	C.97	0.92	0.91	0.90	0.916	C•85	C.891	C• 88.	C.85	C. 85	06.0	0.95	C.97	C-97	C	י ר י י			C.918	C.92	C.91	C•85	C . 88	C.97	C.86	0.86	C•86.	C.86(0.86/	0.85	0.88	0.901	C • 92	0.95
/r o1	74 68	27.0B	-2.03	-1.52	-1-02	-0-69	-0.52	-0-35	-0.19	-0.02	0.14	0.31	0.48	0.65	0.58	1.18	1.48	1.98				Z / DB	-2.05	-1.54	-1.04	-0.71	-0-55	-0 38	-0.21	-0.04	0.13	0.29	0.46	0. 63	16.0	1.17	1.46	1.96
H PN	2 1.4	Y/08	-0.45	-0-45	24-0-	-0.45	-0.45	-0.45	-0.45	-0-45	-0.45	-0.45	-0-45	-0.45	-0.45	-0-45	-0.45	-0-45				Y/CB	-0.03	£0°0-	-0.03	-0.03	-0-03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0-03	-0.03	-0.03	-0.03
F VAC	5 0.95	X/C8	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	£•49	8.49	8.49			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X/CB	1C.88	1C.88	1C.88	10.88	10.88	10.87	1C.88	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87
TST P TN CCN	571 1 66	MACH Q	0.952 242.3	0.955 243.4	0.955 243.4	0.956 243.9	0.956 243.9	0.956 243.9	0.955 243.4	0.955 243.4	0.954 242.9	0.954 242.9	0.954 242.9	0.954 242.9	0.954 242.9	0.952 242.3	0.953 242.5	0.954 243.4		101 F IN LLN		MACH	0.902 233.0	0.903 232.5	0.902 232.4	0.901 231.5	0.901 231.9	0.901 231.5	0.901 231.5	0.901 231.9	0.900 231.5	0.900 231.5	0.900 231.5	0.900 231.5	0.900 231.5	0.900 231.5	C.900 231.5	0.898 231.1
PUN	194	SEC	2	6 0	4	ŝ	9	~	æ	¢	2	11	12	13	14	15	16	17			140	SEG	2	m	4	ŝ	9	2	œ	6	10	1	12	5	14	5	16	17

		pF/P	072 1.041	068 1.038	024 1.013	006 1.003	018 1.010	012 1.007	008 1.005	011 1.006	.006 1.004	010 1.005	005 1.003	.005 1.003	.020 1.011	012 1.006	033 1.019	041 1.023			PE/P	054 1.027	049 1.025	036 1.018	025 1.012	018 1.009	005 1.003	008 0.996	016 0.992	010 0.995	004 1.002	018 1.009	012 1.006	015 1.008	019 1.010	027 1.014	036 1.018
		VA/V C	•0	0	•	•	•	•	0	•	0	0	•	•0	0.	•	0	•				•0	0.	•0	•0	•0	•	•01	•0-	•0	•0	•	•0	•0	•0	•0	•0
ALPHA	20.00	DA/Q VF/V	0.00.0	0.912	0.935	0.921	0.894	0.884	0.869	0.853	0.863	0.835	0.338	0.857	0.907	0.941	0.966	0.973	ALPHA	20-00	0A/Q VF/V	0.903	0.918	0.919	0.909	0.906	0.903	0.898	0.396	0.889	0.878	0.884	0.883	0.917	0.937	0.971	0.978
11	65.3	0F/0	0.818	0.842	0.867	0.830	0.783	0.760	C.729	0.702	0.717	0.668	0.672	0.707	0.809	0.875	0*6*0	0.961	11	67.2	9F / 9	0.816	0.844	0.840	0.817	0.807	797.0	0.781	0.775	0.763	0.747	0.765	0.759	0.827	0.871	0.948	0.967
٩	404	N/VN																	۵	451	M / M																
ى	231.5	NE / N	0.886	006-0	C.925	016.0	0.880	0.869	C.852	0.835	C.845	0.815	C.819	C.835	0.895	C.932	0.961	C.969	Ç	228.3	NF/N	0.851	C.907	0.909	C.858	C.894	C-851	0.886	0.884	0.876	C.864	C.871	0.865	c.906	0.929	0.967	C.975
- p1	159 !	2/58	-2.03	-1.53	-1.02	-0-69	-0.53	-0.36	-0.19	-0.02	0.15	0.31	0.47	0.64	0.98	1.18	1.47	1.58	p1	124	2/08	-2.04	-1.54	-1.04	11.0.	-0.54	-0.38	-0.21	-0-04	0.13	0.29	0.46	0.63	0.56	1.17	1.47	1.97
N/NA	1.474	Y/DB	0.01 -	- 10-0	- 10-0	- 10-0	- 10-0	- 10-0	- 10-0	- 10-0	C.CI	0.01	C.C1	10.0	0.01	c.c1	0.01	c.01	1/Na	1.500	7.0.B	C.C3 -	C.03 -	0.03 -	0.03 -	C•03 -	- 63 - C	0.03	C+ C3 -	0.03	C• 03	0.03	0.03	C• C3	0.03	0.00	C•03
F VACH	5 0.900	X/CP	- 64.3	8.49 -	8.49 -	8.49 -	8-49 -	8.49 -	8.49 -	E.49 -	- 64.3	8.49 -	8.49 -	8.49 -	E.49 -	8.49 -	8.49 -	E.49 -	F NACH	5 0.850	X / CB	10.87 -	1C-87 -	10.87 -	10.87 -	1C+87 -	10.87 -	10.87 -	10.87 -	10.87 -	IC.87 -	10.87 -	1C.87 -	10.87 -	10.87 -	10.87 -	10.87 -
TN CCN	66	0	231.5	229.9	230.5	232.3	231.9	231.5	231.9	231.5	231.5	233.1	233.1	232.7	232.7	232.3	232.3	233.2	TN CON	66	0	228.3	227.9	227.6	226.8	226.8	227.6	228.0	229.1	229.4	228.5	228.5	229.1	229.1	228.6	228.6	228.2
TST p	571 1	MACH	006.0	0.853	0.855	0.902	0.902	0.902	0.902	0.902	0.902	106.0	0.901	0.899	0.899	0.898	0.898	0.900	TST P	571 1	MACH	0.850	0.849	0.847	0.845	0.845	0.847	0.848	0.852	0.854	0.853	0.852	0.852	0.852	0.852	0.852	0.851
RUN	196	SEC	-	2	6 7)	4	ŋ	Ŷ	٢	ω	σ	10	11	12	13	14	15	16	RUN	197	SEO		2	רי ק	4	นา	\$	~	œ	6	2	11	12	<u> </u>	14	10 1	16

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		DF/	1.01	1.00	1.00	1.00	1-00	66.0	0.59	1.00	0.99	0.99	0.99	1.00	1.01	1.00	1.00	1.01			DE/	1.01	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
		5	0.026	0.017	0.008	0.005	0-004	-0.001	-0.004	0.001	-0.003	-0.006	-0.005	0.011	0.022	0.016	0-020	0.023			d C	0.023	0.019	0.018	500-0	600.0	0.001	100.0	0.012	0.013	0,009	0.006	0.011	0.010	0.016	0.020	
		V A /V																			V A / V																
ALPHA	20.00	CA/G VF/V	0.912	0.925	0.931	0.916	0.908	0.898	0.894	0.882	0.898	0.895	0.883	0.883	0.911	0.950	0.972	0.986	AL PHA	20.00	0A/0 VF/V	0.984	0.985	196.0	0.934	116.0	0.905	016.0	0.839	0.831	0.838	0.892	0.898	0.937	0.948	0.976	
11	68.6	0F/0	0.824	C.846	0.855	0.823	0.807	0.787	0.778	0.757	0.786	0.780	0.756	0.762	0.821	C.898	0.947	0.978	TT	69.1	0F/0	0.973	0.975	0.935	0.861	0.815	0.800	0.810	0.774	0.759	0.771	0.777	161.0	C. 868	0.893	0.955	
۵	458	M A / W																	C	456	NV/W																
ى	222.1	NF/N	£36°3	C.916	C.923	0.906	0.898	C.887	C.883	C.870	C.887	0.884	0.871	C.87C	C.902	C.544	0.969	C.984	ى ى	223.0	ME / N	C.981	C.983	0.963	C.926	0.901	0.894	c.900	0.877	0.869	C.876	0.881	0.887	0.929	0.942	0.973	
L pT	0 758	2/08	-2.04	-1.54	-1.04	-0.71	-0.54	-0.38	-0.21	-0.03	0.13	0.30	0.46	0.63	0.96	1.16	1.46	1.96	L p1	0 757	Z/C8	-2.04	-1.54	-1.04	-0.70	-0-54	- 12-0-	-0.20	-0-04	0.13	0.30	0.46	0.62	16.0	1.17	1.47	
H RN	8 1.52	Y/DB	- 0.03 -	-0.03	-0.03	- 0.03	-0-03	-0.03	-0-03	-0.03	-0-03	-0.03	-0-03	-0-03	-0.03	-0.03	-0.03	-0.03	H PN/	1 1.52(4/DB	-0-38 -	-0-38	- C. 38 -	-0-38 -	-0-38-	-0.38-	-0.38 -	- C. 38 -	-0-38	-0.38	-0-38	-0.38	-0.38	-0-38	-C•38	000
IF VAC	5 0.75	X / CB	1C.87	10.87	10.87	10.87	1C.87	1C.87	1C.87	10.87	10.87	10.87	1C.87	10.87	10.87	IC.87	10-87	1C.87	F NAC	5 0.80	X/CB	IC.87	10.87	1C.87	1C.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	1C.87	10.87	1 C • 87	1C.87	10 07
TN CON	66	G	222.1	222.6	223.1	223.1	223.5	223.5	223.5	223.5	223.0	223.0	224.C	224.5	224.C	224.C	224.1	224.1	TN CCN	66	e	223.0	223.C	222.5	222.5	223.C	223•C	223.C	223.5	224 . C	224.C	223.5	223.5	223.C	223.0	222.5	222 0
TST P	571 1	MACH	0.798	0.799	0.801	0.801	0-802	0.802	0.803	0.803	0.802	0.802	0.804	0.805	0.804	0-804	0.803	0.803	TST P	571 1	MACH	0.801	0.801	0.800	0.800	0.802	0.802	0.802	0.803	0.804	0.804	0.802	0.802	0.801	0.801	C. 800	100 0
RUN	200	SEC		r 1 1	(* 1	4	ŝ	Ŷ	~	ε	D			12	2	14	15	16	NUS	201	0 ± S		2	r 1	4	ŝ	Ŷ	~	∞	6	10	11	12	61	14	15	

1.009 .015 .005 L. C02 1.003 1.004 •000 ..004 1.012 1.008 1.002 1.000 0.594 966.0 79.597 1.000 1.005 r/D .000 .007 .008 1.006 1.014 ..004 1.001 .014 •004 .005 .007 DE/D .007 0.020 0.004 600°0 0.007 0.012 0.015 0.015 0.018 0.020 0.013 0.018 0.001 0.002 -0.013 0.032 0.012 0.032 0.026 -0.006 000.0-0.029 0.005 00000 0.009 0.008 -0.009 0.032 0.016 -0.010 0.015 0.012 e. O 8 V V V V V V 0.985 0.985 0.928 0.937 0.915 0.890 0.908 0.983 0.975 0.917 0.913 0.889 0.891 0.890 0.889 0.904 VF/V 0.983 0.938 0.928 0.916 0.954 VF/V 0.931 0.936 0.988 0.983 0.932 0.914 0.907 0.975 0.989 0.981 ALPHA 20.00 ALPHA 20.00 04/0 0A/Q 69**.**6 0F/0 0.972 0.975 0.870 0.853 0.866 0.822 0.816 0.769 0.803 C.950 C.856 C.824 0.918 0.823 C.774 0.777 0.778 0.977 0.969 0.821 0.900 69.3 0F/0 0.974 0.802 0.866 0.933 0.970 C.847 C.950 777.0 126.0 p 497 458 MA/M W V V W ۵ 222.C 223.1 C.980 C.983 C.981 C.931 ME / N 0.880 0.875 0.920 C.930 0.979 C.981 C.924 C.928 0.903 0.963 0.906 C.906 0.988 0.877 0.925 C-92C C.972 0.894 C.879 C.971 0.878 C.858 646.0 C-907 C.983 0.987 C.978 8 1.515 757 2 V/DR 2/DR W C.43 -2.03 C. 20 758 2 Z/CB 0.43 -1.53 0 0.43 -1.53 0 0.43 -1.04 0 0.43 -0.65 0 -C.48 -2.04 -C.48 -1.54 12. -0.53 -0.15 -1.04 -0.70 -0.37 0.13 0.25 0.46 0.64 96.0 1.16 1.47 F 0.14 0.31 0.49 0.65 0.98 1d -0.53 ထ ထ -0-04 œ 1.1 1 - 4 (1.95 F MACH RN/L 5 C+8C1 1+520 F NACH RN/L 5 0.758 1.515 -0.48 -0.48 -0.48 -0.48 -0.48 0.43 0.43 Y/DB 0.43 C.43 -C.48 -0.48 -C.48 ω -C.48 ω α 3 5 ന m **m** 3 -0-45 -0-48 -0.48 -0-41 0.4 0.4 0.4 0.4 0.4 4.0 0.4 -0.4
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		, , , , , , , , , , , , , , , , , , ,		1.00	1.00	1.00	1.00	65.0	0.99	1.00	0.99	0.99	55 ° 0	1.00	1.00	1.01	1.01			DF/	1.01	1.01	1.00	1.00	1.00	1.00	1.00	1.00	65 •0	0.99	1.00	1.CO	1.00	1.00	1.00
	ç	ر در د در د	0.025	0.019	0.007	-0.001	0.004	-0.006	-0.006	-0.001	-0.003	-0.006	-0.006	0.006	0.020	0.025	0.028			aC	0.028	0.031	0.015	0.007	0.003	0.003	0.001	0.004	-0.006	-0.005	0.002	0.007	0.002	100.07	0.019
		V A /																		V A /V															
		V F / V	1.912	0.930	.908	.896	.876	0.877	.872	.856	.853	.859	0.885	0.930	0.962	.979	.984			VF/V	.984	.982	.975	0.938	.901	j.893	.879	0.866	0.871	.875	.873	.898	.939	919.0	-986
ALPHA	20.00	UA/U			0	J)		U	J	J		0	0	0	7	ALPHA	20.00	0 A / O				J	0			U	0		9	0		Ú	J
	69 . 6	CF/0	0.823	0.858	0.809	0.782	0.746	0.746	0.735	0.709	0.703	0.713	0.760	0.853	0.925	496.0	0.977	TT	69.9	QF / Q	C.976	0.973	0.951	C.869	0.795	0.778	0.750	0.728	0.734	0.742	C.740	061.0	C.869	136.0	779-0
۵.	454	~ / ~ ~																o.	496	N V N															
ف	223.6	2 / J 2		0.922	0.858	C.884	0.863	0.865	C.859	C.842	C.839	C.845	0.873	0.922	0.958	C.976	0.982	0	223.0	NF /N	C.982	036°C	C-972	0.931	C. 89C	C.881	C.866	C.852	0.858	0.862	C.8€C	C.887	C.932	C.977	0.984
L d	759	E7.08		1.02	0.69	0.52	0.36	0.20	0.02	0.14	0.31	0.47	0.64	0.98	1.18	1.48	1.98	ld	757	Z/08	2.02	1.52	1.03	0.69	0.53	0.36	0.19	0.02	0.14	0.31	0.48	0.64	85.0	1.18	1.48
RN/L	1.521	/0B		- 10.	- 10.	- 10.	- 10.	- 10-	- C1 -	•01	• 01	.01	10.	•01	10.	•01	• 01	D/Nd	1.517	10.8	- 36 -	- 36 -	- 36 -	• 36 -	• 36 F	- 36 -	• 36	• 36	•36	• 10	• 16	• 30	9 6 1	•36	-36
VACH	C.802	/ [] 3	0- 67.	.49 -0	.49 -0	- 49 - C	.49 -0	- 49 - C	- 65.	.49 -0	.49 -0	- 49 - 0	.49 -0	- 49 - C	- 49 -0	.49 -0	- 49 - C	NACH N	0.801	/CB Y	.49 -0	.49 -0	<u>0</u> - 64.	0- 65.	<u>.</u> 49 – C	• 49 -0	.49 -0	- 49 -0	•49 -0	· 49 - C	.49 -0	•49 -C	- 49 - 0	•49 -0	- 49 -0
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TST F	571 1	MACH	0.802	0.799	0.799	0.799	0.799	0.758	0.758	0.800	0.800	0.800	C. 8CO	0.901	0.801	0.799	0.800	TST F	571 1	MACH	0.801	0.801	0.801	0.801	0.8CI	0.801	0.801	0.801	0.800	C•800	0.800	0.758	0.799	0.799	0.799
RUN	204	S T C		. m	4	ſ	N.	~	æ	6	10	11	12	2	14	15	16	RUN	205	SEQ	-	2	~	4	ي. س	¢	~	ω	σ	10		12	13	14	5

0.599 1.014 1.004 0**.** 598 1.008 1.009 1.003 1.000 1.000 1.003 .013 .005 .003 1.002 0.998 1.003 1.003 1.004 1.002 1.002 1.004 165.0 1.001 I.C04 799.0 1.001 110.1 1.C02 2007 DE/ 0.029 0.034 0.007 0.007 0000.0 0.008 0.011 0.034 0.015 0.010 0.015 0.031 0.018 0.011 0.004 -0.004 -0.005 100.0 -0.006 0.006 710.0 •024 0.011 -0.002 -0.007 0.004 0.044 0.014 -0.001 0.017 0.004 å Ō V A /V V A /V 0.983 0.982 0.982 0.975 0.929 0.909 0.872 0.886 0.975 0.933 0.920 0.867 0.964 0.934 0.926 0.920 0.923 0.976 VF/V 0.987 0.986 VF/V 0.897 0.909 0.894 0.960 0.978 0.993 0.936 0.942 0.969 0.983 AL PHA 20.00 ALPHA 20.00 QA/Q 0A/0 0.975 9.8 01 70 0.974 0.974 0.952 0.852 0.812 0.787 0.779 0.726 0.736 0.763 C.808 0.911 0.955 0.979 0.980 0.957 C.987 0.932 C.872 0.861 0.865 0.864 C.849 C.836 0.839 0.821 0.854 0.953 0.971 68.7 0F/0 0.885 750.0 0.776 496 MA/K 702 M / M D. 177.2 NE/N 222.5 NF / N 0.981 C.980 C.972 0.854 0.359 C•961 C•961 0.899 0.855 0.932 0.926 0.926 0.929 C.956 0.976 0.914 306-0 0.979 0.879 0.886 0.883 0.874 C-973 0.986 396-0 0.915 0.923 C. 939 0.967 C-921 0.975 C.98. 15 757 Z/DB X/CB Y/CB Z/DR E-49 -0.45 -2.03 C E-49 -0.45 -2.03 C B-49 -0.45 -1.53 C B-49 -0.45 -1.53 C 896 -2.05 -1.54 -1.05 -0.68 -0-36 -0.03 0.31 0.64 0.58 -0.54 -0.38 -0.19 0.48 0.12 0.47 0.63 0.96 ω -0.20 0.25 1.47 ω -0.71 1.17 F a -0.04 1.14 1.4 5 с. • 5 9.600 1.510 X/UB Y/UP Z/ 10.87 0.41 -24 RN/L 5 0.800 1.515 RN/L C • 41 O • 41 O • 41 -0.45 -0.45 -0-45 -0.45 -0.45 • 4 5 0.41 C.41 0.41 14.0 -0-45 -0.45 -0.45 -0-45 -C.45 -0.45 0.41 -0.45 0.41 C.41 C.41 0.41 0.4] 0.4] C • 4] 5-5 VACE NACH Е.49 Е.49 LC.87 LC.88 LC.88 8.49 8.49 8.49 ε.49 8.49 8.49 8.49 8.49 67*3 8.49 8.49 1 C • 87 1 C • 87 1 C - 87 1 C - 87 1 C - 87 1 C - 88 1 C - 88 1 C - 88 l C. 88 C-87 C-87 C. 87 C. 88 CONF P TN CONF 222 6 222 6 222 6 222 6 222 6 5 222 6 С 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 177.2 C 222.5 222.5 223.1 223.1 223.1 222•0 222•0 222•5 222 • 5 222 • 5 4 u١ 221.5 N N ŝ **N** N 221.5 2 223.] 571 1 66 221. 177.2 177. 177.5 177.2 177.2 177.2 ١. 177. 55 177. 571 1 MACH 0.800 0.759 0.800 0.758 MACH 0.600 0.600 0° + 6 0 0 0.800 0.800 0.600 0.600 TST C. 6 C O 0.801 0.758 0.758 561.0 0.799 0.800 0.800 0.800 •8C1 0.600 0.600 0.600 0.600 0.600 0.600 0.600 0.600 RUN 206 SFQ 4 ∞ σ C **^**: 3 4 ŝ Ś 207 SEC **(† 1)** RUN σ, \mathbf{o} 2 ∞ 4

PUN	ISI	P IN CC	NF NA	NA HU	1 PT	C	C	11	ALPHA				
208	571	1 66	5 0.6	02 1.5	13 89	6 177.8	101	68.4	20.00				
SEQ	MACH	c	X/DB	Y/DR	2/08	NF / N	N / N	0F / 0	QA/U VF/V	V A /V	a D	DF/D	
	0.602	177.8	IC.87	-0.03	-2.04	C.97C		0.851	0.925	•	0.019	1.005	
2	0.602	177.8	10.87	-0.03	-1.55	0.929		0.866	0.933		0.016	1.004	
m	0.602	177.8	IC. 88	-0.03	-1.04	C.925		C.859	0.929		0.019	1.905	
4	0.602	177.8	10.87	-0-03	-0.71	0.914		0.835	0.919		0.001	1-000	
ŝ	0.602	177.8	1C.87	-0.03	-0.54	C.857		0.804	0.903		0000-0-	1.000	
6	0.603	178.4	1C.87	-0-03	-0.38	0.888		0.792	0.895		0.012	1.003	
~	0.602	177.8	10.87	-0.03	-0.21	0.885		0.785	0.892		0.004	1.001	
ŝ	0.602	177.8	10.87	-0.03	-0.03	0.883		C.780	0.890		0.003	1001	
6	0.602	177.8	10.87	-0-03	0.13	0.871		0.762	0.878		0-018	1-005	
10	0.602	177.8	10.87	-0.03	0.30	0.854		0.798	0.400		-0.002	0.999	
11	0.602	177.8	10.87	-0.03	0.46	C.885		0.786	0.891		0-016	1-004	
12	0.602	177.8	10.87	-0.03	0.63	0.895		0.802	106-0		0.008	1,002	
13	0.602	177.8	10.87	-0.03	0.96	526-0		0.865	0.933			1.002	
14	0.602	177.8	10.87	-0.03	1.16	0-954		0-912	0.957			1 000	
5	0.600	177.2	1 5 . 87	F0-0-	74.	070		170.0					
							-		116.0		110.0	500•1	
C 1	0-602	111.8	IC-87	-0-03	1.97	C • 9 8 3		C.971	0.934		0.022	1.006	
RUN	151	F TN CC	NF WA	CE RN	11 PT	Ċ.	۵	11	VHU IV				
209	571	1 66	5 0.6(00 1.51	53 11	6 177.2	702	6.8.3	20.00				
SFC	MACH	U	X / L B	4 U D P	7 / 08	NE / N	N / N		DATO VEIN			01.0	
	0-600	177.2	1 C - 87	86.0-	-2-04	180.0					0,00		
5	0.000	177.2							707 • 0 0				
1 6									0. 202		CT0.0	1.004	
1 -								0.938	016.0		100.0	I.C02	
t I		7 - 1 - 7	12.11	2 1 1	11.0-	C•924	~	0.858	0.929		0.016	1.004	
^ '	0.602	177.8	1C•87	-C•38	-0.54	0.895	•	0.811	0.905		0.011	1.003	
Ø	0.602	177.8	l C. 87	-0.38	-0.37	0.894	•	0.801	0.900		0.007	1.002	
~	0.602	177.8	10.87	-0.38	-0.21	C.911	-	0.831	0.916		0.004	1.001	
æ	0.602	177.8	l C • 87	-0.38	-0.04	0.852	•	0.796	0.398		0.003	1.001	
σ	0.602	177. 5	1C.87	-C.38	0.13	0.885	C	0.792	0.895		0.013	1.003	
10	0.602	177.ε	1C•88	-C.38	0:00	C.885		167.0	0.895		0.006	1001	
	0.600	177.2	10.87	-0.38	0.47	0.900	Ŭ	0.812	0.906		0.004	1.001	
12	0-600	177.2	10.87	-0.38	0.63	C.9C2	•	0.817	0.908		0.017	1.004	
	0.602	177.8	1C.87	-0.38	0.96	0.927		0.863	0.931		0.019	1.005	
14	0.602	177.8	10.87	-6.38	1.17	C.938	Ŭ	0.884	0.942		0.016	1.004	
	0.600	177.2	10.87	-0.38	1.47	C.964	·	0.934	0.967		0.019	1.005	
16	C. 600	176.6	10.87	-0.38	1.96	0.985		0.976	0.986		0.020	1.005	

		pr/p	1.006	1.005	1.005	1.008	1.003	100.1	1.003	1.001	1.001	1.001	1.002	1.001	1.000	1.003	1.006	1.006			0/10	1-002	1.004	1.008	1.005	1.005	1.001	1.000	0.996	0.598	665.0	1.003	1.002	100.1	1.004	1.006	1.005
		Cb	0.024	610.0	0.019	0.031	0.013	0.004	0.011	0.003	0.003	0.003	0.010	0.003	0.000	0.011	0.023	0.024			a)	0.010	0.015	0.031	0.020	0.019	0.004	-0-001	-0.017	600.0-	-0.002	0.012	0.008	0.004	0.016	0.024	0-020
		V / V /																			V A /V	•						,		•	·						
PHA.	00.00	V/Q VF/V	0.984	0.987	0.965	0.921	0.914	0.909	0.900	0.906	0.904	0.904	0.901	0.921	0.945	0.972	0.976	0.986	PHA	.00	VIO VEIV	0.993	0.66.0	0.970	0.928	0.931	0.931	0.923	0.916	0.899	0.907	0.898	0.920	0.955	0.964	0.981	0.985
AL	2 20	QA QA	5	8	0	9	~	6	-	1	-	2	ŝ	Ģ	2	ŗ	4	9	٩L	1 20	0 07	8	ŝ	ŝ	8	Ç.	6	ņ,	ŝ	6	2	8	6	-	6	S.	4
	68.	QF /	10.97	0.97	0.93	0.84	0.82	C. 81	0-80	0.81	0.80	0.80	0.80	0.84	0.88	0.94	0.95	0.97	11	64.	QF/	C.98	0.98	0.94	0.85	0.85	0.85	0.34	0.82	0.79	0.81	0.79	0.83	0.90	0.92	0.96	0.97
٩	702	MA/M																	۵	691	M / M																
C	176.6	NF/V	C.983	0.986	0.962	c.916	0.908	C.9C3	C.854	006.0	C.898	0.898	0.895	0.916	C.942	c.97c	0.974	0.985	C	174.5	MF / N	256.0	0.985	0.968	0.924	C.926	C.92€	0.918	C.91C	0.893	c.9c1	0.852	0.915	C.952	0.962	0.979	0.984
Ld	895	Z/CB	2.04	1.53	1.05	0.71	0.54	0.37	0.21	0.04	0.12	0.29	0.47	0.63	0.96	1.17	1.47	1.56	La	882	Z/DB	2.03	1.53	1.03	01.0	0.52	0.36	0.19	0.02	0.14	0.31	3.48	0.64	0.97	1.17	1.48 I	- 98 - 1
RN/L	508	80	48 - 2	1 84	48 -	48 -(48 -(48 -(48 -(48 -(48 (48 (48	48 (48 (48	48	48	J/Ng	1.503	0.0	4.9	43 -	1 54	43 -(43 - (43 -(43 -(43 - (43 (4.3	43 (43	4.9	43	43	43
ACH	566	B </td <td>7 -0.</td> <td>8 -0.</td> <td>7 -0.</td> <td>7 - C</td> <td>-0- 2</td> <td>7 - 0.</td> <td>7 -0.</td> <td>7 -0.</td> <td>1 -0'</td> <td>7 -0.</td> <td>7 - 0.</td> <td>7 -0.</td> <td>7 -0.</td> <td>7 -0.</td> <td>7 -0.</td> <td>7 -0.</td> <td>ACH</td> <td>109</td> <td>B Y</td> <td>8.0.</td> <td>6</td> <td>8</td> <td>8.0.</td> <td>8</td> <td>8</td> <td>0. 8</td> <td>30.</td> <td>8</td> <td>с 8</td> <td>8</td> <td>8 0</td> <td>8 0</td> <td>с. 8</td> <td>6 0</td> <td>6 6</td>	7 -0.	8 -0.	7 -0.	7 - C	-0- 2	7 - 0.	7 -0.	7 -0.	1 -0'	7 -0.	7 - 0.	7 -0.	7 -0.	7 -0.	7 -0.	7 -0.	ACH	109	B Y	8.0.	6	8	8.0.	8	8	0. 8	30.	8	с 8	8	8 0	8 0	с. 8	6 0	6 6
N N N N	2. 5	2/X	10.8	1C.8	1 C. 8	10.8	1C.8	10.8	10.8	10.8	1 C. 8	10.8	1 C • 8	1C.8	1 C • 8	1C.8	1C.8	1C.8	N L N	5 0	0 / X	8.4	8•4	8•4	8.4	8.4	8.4	8•4	8.4	8.4	8.4	8.4	8•4	8.4	8•4	8.4	8.4
TN CO	66	0	176.6	176.6	177.2	177.2	177.8	177.2	177.2	177.2	177.2	177.2	177.2	177.2	176.6	176.6	177.2	177.2	TN CC	66	Q	174.5	173.9	174.5	173.9	174.0	173.4	174.6	174.6	175.1	175.1	174.5	173.9	173.5	173.9	173.5	173.9
TST P	571 1	MACH). 599	3.599	0.600	0.600	0.602	0.600	009.0	0.600	009.0	0.600	3.600	0.600	3.599	3.599	0.600	0.600	TST P	571 1	MACH	0.601	0.600	0.601	0.599	0.599	3.598	0.600	1.96.01	0.602	0.602	109.0	C+ 6 C O	0.600	0.599 	3.559	3.599
RUN	210	SEC	1	2 (3	4	Ś	6	-	8) 6	10 (11 (12 (13	14 (51	16 (RUN	211	SEO	2	m	4	ŝ	9	~	c	6	01		12 (14	5	10	17

		A/V CP PE/P	0.029 1.007	0.006 1.001	0.006 1.002	0.016 1.004	0.012 1.003	0.001 1.000	-0.002 0.999	0.002 1.000	-0.001 1.000	0.001 1.000	0.004 1.001	0.002 1.000	0.003 1.001	0.009 1.002	0.019 1.005	0.015 1.004			A/V CP PF/P	0.022 1.006	0.028 1.007	0.012 1.003	-0.002 0.999	0.005 1.001	-0.002 0.999	-0.002 0.599	0.007 1.002	0.006 1.001	0.001 1.000	0.004 1.001	0.001 1.000	-0.003 0.999	0.006 1.002	0.017 1.004	0.012 1.003
ALPHA	20.00	DA/Q VF/V VI	0.912	0.932	0.938	0.897	0.831	0.870	0.865	0.866	0.869	0.873	0.871	0.889	0.938	0.961	0.983	0.989	ALPHA	20.00	DA/Q VF/V VI	0.987	0.981	0.974	0.934	0.896	0.886	0.875	0.864	0.861	0.880	0.882	0.908	0•964	0.977	0.983	0.993
11	64.9	0F /0	0.828	0.862	0.873	797.0	0.766	0.744	0.735	0.738	0.741	0.749	0.746	C.779	0.872	0.920	0.969	0.980	TT	66.1	0F/0	0.978	0.957	0.948	0.864	0.792	0.772	0.753	0.735	0.728	0.762	0.767	0.815	0.923	0.953	0.967	0.987
٩	695	MA/M																	Q.	654	M A / M																
3	174.6	MF /N	0.907	0.928	656.0	C. 891	0.874	0.863	0.858	C.859	C.861	C.865	0.863	0.883	C.934	C.958	0.982	0.988	U	175.8	N L L N	C.9 86	036.0	0.972	066.0	0.889	0.879	0.868	0.856	C-853	0.873	0.875	0.903	C.961	c.976	0.981	C.992
Ld	886	Z/D8	2.02	1.53	1.03	0.69	0.53	0.36	0.19	0.02	0.14	0.31	0.48	0.64	96.0	1.18	1.48	1.98	1d	887	2/C8	-2.03	1.52	.1.03	01.0	-0.52	.0.36	-0.19	-0.02	0.15	0.31	0.48	0.65	0.98	1.18	1.45	I.98
RN/L	1.504	Y/CB	- 10.0	c.01 -	0.01 -	C.01 -	- 10-0	- 10.0	0.01 -	- 10.0	0.01	C.C1	0.01	0.CI	0.01	0.01	0.01	0.01	J/Ng		470P	0.36 -	0.36 -	0.36 -	0.36 -	0.36 -	C+36 -	0.36 -	0.36 -	0.ª36	0.36	0.36	0.36	0.36	0.36	0.36	C•36
NACH	0.5555	X/CB	E.49 -	8.49 -	8.49 -	8.49 -	- 64.8	E.49 -	E.49 -	- 64.8	E.48 -	8.48 -	E.48 -	E.49 -	E.49 -	8-48 -	E.49 -	- 64•3	NACE	0.602	X/CR	8.49 -	- 64.9	E.48 -	- 64.3	8•48 -	8.49 -	- 64.8	8.49 -	8.49 -	- 6 † •3	- 64•3	8.48 -	- 64 - 3	8 • 48 -	8.48 -	8.48 -
TST P TN CONF	571166 5	MACH Q	0.559 174.6	0.558 174.0	0.558 174.0	0.559 174.6	0.598 174.C	0.558 174.0	0.602 175.8	0.600 175.2	0.600 175.2	C-600 175.2	0.600 175.2	C.6C0 175.2	0.600 175.2	0.599 174.6	0.600 175.2	C.6C0 175.2	TST P TN CCNF	571 1 66 5	MACH C	0.602 175.8	0.602 175.8	0.600 175.2	9.600 175.2	0.559 174.6	0.559 174.6	0.559 174.6	0.600 175.2	0.601 175.8	0.559 174.6	0.599 174.6	0.599 174.6	0.599 174.6	0.599 174.6	0.599 174.6	0.558 174.C
RUN	212	SEC	1	2	~ ``	4	ŝ	Ŷ	2	8	6	10	11	12	13	14	51	16	RUN	212	SEC	1	2	6 1)	4	U N	¢	~	œ	6	10	11	12	F 1	14	ເກ 1	16

1.000 1.000 665.0 1.005 1.004 1.002 1.000 1.000 1.005 0.999 1.000 ..002 0.999 1.001 0.999 pr/p 1.000 0.999 666.0 0.999 C. 599 0.999 0.999 0.599 665.0 0.999 1.005 1.003 1.002 1.000 1.000 1.001 1.00 -Lud 0-007 0-001 0-016 0-002 0-010 0.006 0.002 -0.002 0.019 -0.010 -0.010 0.019 0.019 -0.010 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.028 -0.019 -0.010 0.011 0.007 0.002 0.003 0.032 -0.021 -0.021 -0.012 -0.021 d 0.000 000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.00.0 V A /V V V V . • 166.0 0.926 0.902 0.887 0.8888 0.979 0.950 0.940 0.939 0.939 395 0.899 0.950 619.0 0.945 0.983 0.987 0.879 0.8888 0.886 0.910 VF/V 0.991 0.932 0.932 0.961 0.987 VF/V 779.0 0.948 0.987 0.930 0.971 0.981 AL PHA 20.00 04/0 ALPHA 20.00 000.0 0.000 0A/Q 0.00.0 000.00 0.000 000-0 0.000 0.000 0.000 C.000 0.000 0.000 000-0 000.00 0.000 0.000 0.958 006.0 0.978 0.779 0.773 0.891 0.974 0.955 0.851 0.804 0.778 777.0 779.1 0.993 006.0 0.882 0.922 0.941 66.2 0/30 0.979 0.798 0.762 0.817 0.959 .965 01 10 0.981 0.881 0.379 0.867 0.867 0.836 0.989 0.893 65.1 0.000 .000 953 44/ N N V V N 000.000 000 000 1811 0.000 0.000 0000-0 0.000 0.000 0.000 0.00.00 0.000 00000 0.00.0 0.000 0 . 4. 5. 7. E. 7. E. 7. E. 7. C. 0 175.2 NF/N 0.893 C.9876 C.986 C.976 C.88C 516.0 C.882 0.879 C.945 C.944 0.856 0.856 C.872 0.904 0.945 0.980 156.0 156.0 C.949 C.931 C.961 0.881 C • 54 C 0.935 C.938 0.932 015-0 .587 0.975 C.914 0.98 UT UT . 1 887 Z/CB 5 C.250 1.523 1892 0.14 -0.53 -0.19 -0.54 -0.36 0.48 98. -1.54 -0.70 . 63 •64 .48 0.12 0.25 0.47 • 56 .16 .46 -0.45 -2.03 -0.45 -1.03 ω Z/DB -0.21 P 1 -0.45 -1.52 -0-02 PT -2.04 -1.05 -0.04 -0.37 σ. • 0 C 0 0 PN/L PN/L 5 0.600 1.503 4 / J, P -0.45 -0-45 Y/08 -0.45 -0.45 -0.45 -0.45 -0-45 -0.45 ŝ ŝ 0.41 C.41 C.41 C.41 C.41 -0.45 0.41 0.41 C.41 C-41 0.41 0.41 -0.45 C.4 -0-4-C. 4 C . 4 0.4 4. -0.4 ပို VACH VACH HUVN X/CB 8.49 8.49 8.49 8.49 8.49 8.49 e,49 8.49 8.49 8.49 x/CB 10.87 10.87 10.87 10.87 10.87 10.88 10.887 10.87 10.87 10.87 10.87 10.87 10.87 10.87 10.87 10.87 8.49 8.49 8.49 8•48 8.49 8.48 8.49 CONF **JUDU** 175.2 174.6 175.2 175.8 175.2 175.8 175.8 175.8 175.8 175.2 74.6 174.6 174.6 79.5 79.5 78.8 78.8 78.8 78.8 5.67 5.67 5.87 5.87 79.5 79.5 74.6 175.2 78.1 8°8 **u**n 5 - 51 .61 T.V 66 IN 66 O Ċ ۵ 571 1 ¢1 571 1 MACH 0.600 0.250 0.250 0.249 0.249 C.250 0.251 0.251 c.600 0.602 0.601 0.602 0.602 0.602 0.600 MACH 0.249 0.249 0-250 0-250 0-250 0-250 0-250 0.251 0.599 0.600 C.600 0.599 0.599 0.599 0.599 0.600 ST ST RUN 214 SEQ \mathbf{c} 13 14 12 215 SEQ 4 ഹ 9 $\boldsymbol{\omega}$ σ \underline{c} \$ RUN SUN 4 S 9 ∞ **O** 2 12 13 14 15 16

		pr/p	1.000	666.0	1.000	1.000	665*0	0.599	0.999	0.999	666.0	0.999	0.599	0.999	0.995	0.999	9.999	1.000		
		d U	-0.010	-0.019	-0.010	-0.010	-0.012	-0.021	-0.021	-0.021	-0.024	-0-021	-0.021	-0.021	-0.012	-0.021	-0.028	-0.008		
		V 0 / V	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		
		VF/V	0.946	0.951	0.950	0.913	0.904	0.915	0.905	0.847	0.903	0.903	0.888	0.896	0.944	0.959	0.992	0.992		
ALPHA	20.00	OA/O	000.0	0.000	0.000	0.000	c.000	0.00.0	0.000	000.0	000.0	c. J00	0.00.0	0.00.0	0.000	0.00.0	0.00.0	0.000		ALPHA
77	64.5	QF /0	0.893	0.902	006.0	0.832	0.815	0.834	0.817	0.803	0.813	0.813	0.785	0.801	0.889	0.919	C.9 82	0.983		TT 54.2
٩	1804	MA/W	000.0	000-00	0.00.0	0000.0	0.000	0.000	000.000	000.0	000 • 0	0.00.00	0.000	0.000	000.00	000.00	0.000	000.0		0 2 L 2 L 2 L 2 L 2 L 2 L 2 L 2 L 2 L 2
Q	78.8	ME /N	0.945	C.950	C.945	C.913	- 206-0	C.914	C • 504	0.896	C. 502	C.902	C.887	358.0	0.943	555.0	256*0	155.0		۵ ۲۵ ۲۰
۲q .	1884	Z / D8	-2.04	1.54	1.04	0.71	0.54 (0.37 (0.20	0.04 (0.13 (0.29	0.47	0.63 (0.96	1.16 (1.46	1.57		1884
RN/L	1.515	Y/C8	0.03 -	C.03 -	- E0.0	C•C3 -	0.03 -	- 60-0	0.03 -	0.03 -	C•03	0.03	0.03	0.03	c•03	0.03	0.03	C• C3		
MACH	C.250	X/CB	C.87 -	C.87 -	C.88 -	C. 88 -	C.87 -	C.87 -	C. 87 -	C.87 -	0.87 -	0.87 -	0.87 -	C. 88 –	C.88 -	C • 88 -	0.88 -	C. 87 -		VACH C - 7 FO
CONF	5		3.8	.8 1	3.8 <u>1</u>	- 8 ·	.8 1	1. 8 1	.8 1	.8	.8 1	.5 1	- 2 - 1	- 2 ·	• 5 T		1.8 1 (L C C N F
d L	1 66	C	~	78	28	78	78	28	2	18	28	52	5	5	~	52	78	5		2 4 4 4 4 4
TST	571	MACH	0.250	0.250	0.250	C.250	0.250	0.250	0.250	0.250	0.250	0.251	0.251	0.251	0.251	0.251	0.250	0.251		TST 571
PUN	216	SEQ	1	2	(*1	4	ŝ	9	-	80	¢	10	11	12	E I	14	1 2	16		NUN VIZ

		pF/p	0.999	0.999	665.0	665.0	1.000	666.0	0.999	0.999	666.0	665.0	666.0	665*0	666.0	666.0	1.000	1.000
		CD C	-0.019	-0.019	-0.019	-0.012	-0.010	-0.030	-0.030	-0.012	-0.012	-0.012	-0.021	-0.021	-0.019	-0.019	-0.010	-0.010
		V A /V	0.000	0-000	0000-0	0.000	0.000	0000.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0	0.000
	_	VF/V	1.001	0.992	0.978	0.936	0.910	0.900	0.902	0.915	U. 893	0.913	0.921	116.0	0.951	0.976	0.990	0.992
ALPHA	20.00	0 A / O	0000-0	0.000	0.000	c.000	C. 000	c.000	c.000	0.000	c. 000	0.000	c.000	c.000	0.000	c. 000	c.000	c.000
Ĩ	64.2	CF/Q	100.1	0.984	0.955	C.874	0.825	0.808	0.811	0.836	0.796	0.832	0.846	0.838	0.902	0.951	0.979	0.984
۵.	1804	NVN	0.000	0000.0	0.000	0.000	0000.0	0.000	000.0	0.000	0.000	000.0	0.000	0.000	0.00.0	0.000	0000.0	0.000
C	78.5	MF/N	1.001	C.952	C.978	C.935	506.0	C.855	C.901	C.914	C.892	c.912	C. 52C	916.0	C. 95C	C.976	056*0	C.592
۲ م	E 1884	Z/CP	-2.04	-1-53	-1.04	-0-71	-0.54	-0.37	-0.20	-0-04	0.13	0*30	0.47	0.63	0.56	1.16	1.46	1.96
T A A H	0 1.51	¥ / D B	-0-38-	-0-38	-0-38 -	-C•38 -	-0.38	-0.38 -	-0-38	-0-38	-0-38	-0.38	-0-38	-0.38	-0-38	-0.38	-0.38	-0-38
F VACI	5 0.25	X/CB	10.87	1C.87	1C.88 -	10.87	1 C • 88	10.87	10.88	1C.88 -	1C.88 -	1C.88 ·	10.87 -	1C.88 -	1C.88 -	10.88 -	1C.88 ·	1C.83 ·
TN CCN	66	e	78.8	78.8	79.5	2.67	79.5	78.8	78.1	79.5	79.5	3-62	78.8	78.8	78.8	78.8	19.5	2.61
ISI P	571 1	MACH	0.250	0.250	0.251	0.251	0.251	3.250).2 49	0.251	0.251	0.251	0.250	0.250). 250	0.250). 251	0.251
NUN	217	SEC	1	2	m	4	in.	6	~	0 0	6	10	11	12 (13	14 (15 (16 (

1.000 0.599 666 0.999 .000 .000 666 666 665 .000 999 665 0.999 665.0 0.999 0.999 č . 0 0 • ò 0 0 -0.010 -0.010 σ ¢ -0-019 -0.019 -0.021 -0.021 -0-012 -0-010 -0.010 -0.019 -0.019 -0.019 -0.021 -0.021 -0•019 -0-01 0.000 000 000 000 000 000 000 000 000 0000 A / V C C C 000 0.000 5 . --0 . 3 ే . . 0 • : 0.938 0.961 0.917 0.907 0.923 0.995 0.922 0.923 616 0.929 955 0.960 998 F/V 0.925 0.923 1.000 . 0 5 : 20.00 0.000 0.000 0 A / O 0.00.0 0.00.0 0.000 0.00.0 c.000 0.000 C.000 ALPHI 0.000 0.976 0.922 0.839 0.849 0.848 0.842 C.853 0.920 0.989 0.995 1.000 0.849 64.2 CF/0 0.820 0.862 0.849 016 0 1803 VA/N 0.000 0.000 0.000 0.000 0.000 0.000 000.000 0.00.0 0.000 0.000 0.00.0 000.0 0.00.0 0.000 8 2 U 2 • 8 2 U 2 • 8 0.988 C.96C 0.916 C.922 0.921 c.906 0.922 C.922 ω C-924 C.929 3 tr) œ 1.000 0.918 500 C.96(υ υ 555 ₽ Щ. ئ ి 0.250 1.515 1883 (/D8 Y/D8 Z/D8 -1.53 -0.70 -0.54 -0.21 0.13 0.30 0.46 0.63 1.16 1.47 -2.05 F d 1.1 g -RN/L -0•48 -0•48 -0.48 -0.48 -0.48 -0-48 ω œ ω -C.48 ω -0.48 ω ω ω ω -0-48 -0.45 -0-48 -0.48 -0.48 -0-48 -0.41 4 ٠ 0 NACH X/DB 0.88 C.88 C.88 C.87 C.88 C.88 C• 88 C• 88 C. 88 C.88 C.88 0.87 0.87 C.87 C.87 C.88 ഹ CONF 5-52 5-52 5-52 **w**h տտ 79. -62 571 1 671 1 0.250 0.251 0.251 0.251 0.251 0.251 0.251 0.251 0.251 0.251 **c** 0.251 0.251 0.251 0.251 0.251 S \sim m RUN 218 SEQ 0 m + 1 0 m 0 σ 0 4 S

665°0 0.999 0.999 666 DF/D 666.0 0.599 0.999 0.599 665.0 0.999 0.999 0.999 666.0 0.999 66 0 • -0.021 -0.021 -0.021 -0-017 610.0--0-019 -0-019 -0.019 -0.019 Φ -0.019 -0.021 -0.021 -0.021 -0.021 -0.021 •01. 9 0.000 0.00.0 0.000 0•000 0•000 000 000 000 000 0.000 0.000 0.000 0.000 0.000 0.000 e . > 5 • • 0.979 0.979 0.935 0.939 616.0 0.926 0.913 906 959 0.996 0.936 992 993 VF/V 0.903 0.913 981 0 5 . • ్ర 0 20.00 ALPHA QA/Q c. 000 c. 000 0.000 c. 000 c. 000 0.000 0.00.0 c.000 000-0 0.000 0.000 0.000 c.000 0.000 C.989 C.957 C.872 C.881 0.855 C.830 63.9 166.0 C.874 C. 983 0F/0 0.823 0.918 0.842 0.813 0.830 0.960 84 6.0 1803 MA/M 0.000 0.000 0.000 000 .000 0.000 0.000 000.0 0.00.00 0.00.0 0.000 0.00.0 0.000 000.000 0.00.0 . 75.5 MF /W 356.0 C. 534 C. 939 0.918 0.908 956*0 972.0 C.925 C.512 C.902 \sim 93 F 0 0.958 C m 0.980 56. 56 C.91 Ĵ 5 C+251 1+523 1884 X/CB Y/DE Z/DB + 8-49 0-43 -2-03 C 8-49 C+43 -1-52 C -0.68 -0.53 0.14 0.31 -0.35 ω ω 4 ω -0-02 -0.18 0.43 0.98 4. σ . PN/L • • 4 4 4 4 • 43 • 43 4.4. • 4 • • 4 • **(***) • 3 m 61 0.43 • 4 3 4. 4. 44 O \mathbf{O} \odot O \mathbf{O} 0 O 00 O NACH 8.49 8.49 8.49 8•49 8•49 49 ÷ w **L**ND 80.1 80.1 80.1 ٠ 2 66 C 80 0.252 0.252 0.252 0.252 0.252 0.2552 0.2552 219 5 F Q NATION 121 10 RUN ω 9 14 2

		pF/p	666.	666.	• 999	666.	• 599	666.	666.	665.	666.	665.	666.	666.	665.	666.	000.	666.			pF/p	666.	666.	666.	666.	665.	666.	666.	666.	666*	666.	666.	666.	666.	• 999	665 -
			0	0 6	0 1	20	0 1	0	0	000	0 1	30	2 0	20	0	1 0	0	7 0				4	0	0 6	0	10	1	8	0	2 0	10	0	0	10	0 6	0
		d C	-0-01	-0-01	-0.02	-0.01	-0-02	-0.01	-0-02	-0.03	-0.02	E0.0-	-0.02	-0.01	-0.02	-0.02	-0-01	-0.01			ð	-0-01	-0-01	-0-01	-0-01	-0.02	-0.02	-0.02	-0.02	-0-02	-0.02	-0.02	-0-02	-0.02	-0.01	10-01-
		V / J /	0000	000.0	• 000 • 0	000.0	000 •0	• 000	.000	000.	000.00	000.0	000.0	000.0	000.0	000.0	.000 .0	0000.			V A / V	• 000 • 0	. 000 .	.000	. 000 .	.000.	• 000 •	. 000.	• 000	000.0	.000	.000.	· 000 •	• 000 • (. 000 .	000 - 0
		VF/V	.935 0	. 940 C	.945 0	006.	.887 0	.858 C	.880 0	• 864 Ú	.864 0	.897 (.891 C	.892 (.940 0	.981 C	. 996	.995 0			/F/V	.993 0	996 0	.975 0	935 0	.898 0	.882 0	.902 C	.879 0	907 0	.894 C	.871 0	.927 0	. 943 C	.981 C	995
HA	00	<u></u>	0	000	0	0	0	0	0 0	0	0	0 0	0	0.0	0 0	000	0	0	HA	00	0	0	0	0 0	0 0	0	o o	0 0	o o	0 0	o o	00	0	000	0 0	0
ALP	20.	0A/	00 ° 0	00.0	00-0	0.00	0.00	0.00	c. 00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	ALP	20.	0A/	0.00	0.00	0.00	C-00	0.00	0.0	00.0	0.00	C- D	0.00	C. 00	0.0	C. 00	0.00	000
11	63.9	0F/0	0.872	0.882	0.891	0.808	0.784	0.733	177.0	0.744	0.744	0.801	161.0	0.792	0.882	0.960	166.0	0.989	11	63.7	CF/0	0.986	0.991	0.950	0.872	0.804	0.775	0.811	0.170	0.820	0.796	0.756	0.856	0.887	0.962	
٩	1803	MA/M	0.000	0.000	00000	0.00.00	000.0	0.000	000.0	0000.0	0.000	0.000	000.0	0.000.0	0.000	0.000	0.00.00	000.000	۵.	1803	NVVW	0.000	000.0	0.00.00	0.000.0	0000.0	0.000	000.00	000.00	0000.0	0000.0	0000.0	0000.0	000.000	0.000	
G	2.02	NF/N	0.534	0.940	3.944	C. 899	0.886	0.857	518.0	0.863	0.863	0.896	0.890	0.850	0.940	0.980	956.0	0.955	ı	3*5L	NF/N	£55 °0	956*0	0.975	\$25.0	0.897	C.881	106.0	0.878	0.906	0.892	C.87C	0.926	C+542	186.0	
μŢ	1884	2/DP	-2.03 (1.53	1.02 (.0.69	0.52	0.35 (. 51.0.	0.02	0.14	0.31 (0.47	0.65	9.98	1.18	1.48	1.98	1 d	1884	Z/DR	2.02	1.52 (1.03	0.69 (0.53 (0.36	0.19 (0.03 (0.15	0.31	0.48	0.65	0.98	1.18	~ ~ ~
PN/L	1.523	470B	0.01 -	c.01 -	- 10-0	- 10.0	- 10.0	0.01 -	- 10-0	- 10-0	C. C1	0.01	0.01	10.0	10.0	0.01	0.01	0.01	RN/L	1.524	Y/DB	0.36 -	0.36 -	0.36 -	0.36 -	0+36 -	0.36 -	0.36 -	0.36 -	3.36	0.36	0.36	0.36	0.36	0.36	20.00
NACH	0.251	/ 58	- 46 -	- 65.	- 65.	- 64.	- 65 -	- 49 -	- 44 -	- 49 -	- 64.	- 46 -	• 49	- 46 -	- 64.	- 64.	- 64.	- 65.	NACH	0.251	109	- 65.	- 64.	- 65.	- 49 -	- 46 -(- 65.	- 64.	- 64.	- 40	- 49 -	- 65.	- 64.	- 65.	- 65.	0
CNF	ŝ	×	ω	ω	æ	ω	æ	æ	ω	ω	æ	æ	ω	œ	ω	ω	ω	ω	CNF	r	×	ω	ω	e	œ	æ	œ	ω	ω	œ	ω	ω	ω	ω	æ	c
TN C	66	Q	2.97	2.91	79.5	80.1	79.5	79.5	79.5	2-61	2.95	2.91	79.5	80.1	79.5	79.5	79.5	5.61	TN C	66	C	79.5	79.5	79.5	79.5	79.5	3*62	3.91	2.91	2.61	2.91	79.5	5-61	79.5	5.95	u u u
IST P	571 1	MACH	.251	•251	.251	• 252	.251	.251	.251	.251	.251	.251	.251	.252	.251	.251	.251	.251	d ISI	571 1	MACH	.251	.251	.251	.251	.251	•251	.251	.251	.251	.251	.251	.251	.251	.251	1 1 1
RUN	220	SEQ	1 0	2 0	0	4	5 0	6 0	7 0	8	06	10 0	11 0	12 0	13 0	14 0	15 0	16 0	NNA	221	SFQ	1 0	2 0	30	4 0	5 0	60	7 0	8	06	10 0	11 0	12 0	13 0	14 0	15.0

• 000 • 000 1.000 0.999 665.0 665*0 666.0 0.999 .000 1.000 .000 000 665.0 0.999 665 0 0.999 'n • -0.010 -0.010 -0.012 -0-015 -0.013 -0.010 -0.010 -0.008 -0.010 -0.012 -0.012 -0.013 -0.012 -0.006 -0.012 -0.021 0• 000 0• 000 0.000 0.000 0.000 0.000 000 000 000 000 000 000 000 A V ే 0 • 3 .0 • • F/V 0.991 166.0 0.975 0.903 0.897 875 0.912 0.978 0.988 0.880 0.883 0.904 0+6+0 0.957 166 0 • -20.00 ALPHA 20.00 ALPHA 0.000 c. 000 0000 0.000 0.000 0.000 0.000 c.000 OA/U 0.00.0 000.0 c.000 c. 000 c.000 000.000 0.00.0 0.00.0 0.772 0.777 0.955 63.7 QF/0 0.981 0.981 C.950 0.815 0.813 0.834 186 66.3 0.803 0.763 0.830 0.882 0.914 0.000 0.000 . 1802 WA/M 0.000 0.00.0 000.000 0000.0 000.00 000.000 0.000 0.000 000.000 0.000 0.00.0 0.00.0 ۵ 80.1 MF/W 156°0 C.9C2 0.903 5:6.0 0.913 0.911 ω 0.896 0.879 0.882 C.874 s 0.978 166.0 156.0 C.95{ 85. 681 0.252 1.531 1884 (/DB Y/DP Z/DB 0.64 -1.52 0.14 -0.70 -0.51 0.48 0.98 •18 .47 -0.45 -2.03 -0.03 0 -0.18 P 1 5 1.9 RN/L C.954 1.480 DNNL DNNL -0.45 -0.45 -0-45 -0.45 -0.45 -0.45 -0.45 -0.45 -0.45 -0.45 -0.45 ŝ ŝ ŝ -0-45 -0.45 4 4.0ö VACH VA CH 5 0 • 2 \ X / DB 8 • 49 • 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 •49 8•49 • 49 - 49 α œ ഗ TN CLNF LADU UCNE 80.1 80.1 80.1 80.1 80.1 80.1 80.1 30.1 80.1 80.1 80.1 80.1 80.1 80.1 80.1 80.1 80.1 I.V 99 09 66 ۵. 571 1 ۵. 0.252 0.252 0.252 TST TST RUN 222 SFQ m 450N0 O 0 \sim 5 4 ഗ

.025 .019 •00 • • 004 .008 .004 .005 .005 .006 .009 •010 .021 .016 .025 . 032 F/P .038 0.040 0.030 0.010 0.007 0.008 0.014 0.032 0.039 0.050 .024 .060 0.012 0.008 0 V A V 0.975 0.972 0.961 0.917 0.893 0.894 0.883 0.883 0.887 0.887 0.887 0.887 0.887 0.953 0.953 0.953 0.971 VF/V 0.965 .96 OA/Q 0.824 0.775 0.768 0.764 0.763 0.790 0.912 0.966 0.959 0.794 0.957 0.966 C.964 QF /0 380 MA/M 241.7 NF/N 0.954 C.967 0.874 0.872 905 0.888 C.878 C.885 179.0 C.866 0.945 0.963 0.968 C.871 0.966 96 3 -1.54 0.12 10.97 -0.04 0.46 0.62 1.17 -2.04 -0.53 15.0 - 47 Z/08 -0.70 -0.37 -0.20 9 9 9 • **Y/CB** 0.41 0.41 0.41 C.41 C.41 C-41 0.41 C.41 C.41 0.41 C.4 C • 4] 0.4 C.4 4 4. 5 Ĵ C 833 X/CB C•83 C•88 C•88 C • 87 C • 87 C • 87 67 87 87 ω 3 3 00 241.7 242.8 242.8 242.8 242.8 242.8 242.8 242.8 242.8 242.8 242.E 241.7 42.8 ~ (7) ω **(7)** 241. 242. . . 42.4 C? Ň 571 1 MACH 0.957 0.957 0.957 0.957 0.957 0.957 0.957 0.957 0.957 0.957 0.955 0.955 0.955 0.957 0.957 0.956 RUN 223 SEC \sim m 4 ഗ \mathbf{Q} ~ ထ σ 10 2 (m 4 ŝ S 5 ω П

VA/V CP PF/P 0.036 1.023 0.036 1.023 0.012 1.008 0.012 1.008 0.011 1.007 0.011 1.007 0.011 1.003 0.011 1.003 0.011 1.003 0.013 1.008 0.013 1.008 0.013 1.008 0.014 1.003 0.014 1.003 0.014 1.003 0.014 1.003 0.014 1.003	V/V CP 0.053 1.033 0.053 1.033 0.027 1.021 0.027 1.021 0.021 1.001 0.013 1.008 0.013 1.008 0.013 1.008 0.014 1.002 0.014 1.002 0.015 1.014 0.015 0.014 1.002 0.014 1.002 0.015 0.014 0.002 0.014 0.002 0.014 0.002 0.015 0.014 0.002 0.014
T ALPHA • 6 -20.00 • 0 -903 • 0 -903 • 0 -925 • 0 -838 0 -848 0 -848 0 -848 0 -848 0 -848 0 -848 0 -856 0 -836 0 -836 0 -856 0 -8656 0 -8	ALPHA 20.00 74/0 VF/V VE 0.969 0.969 0.974 0.962 0.974 0.975 0.873 0.873 0.873 0.858 0.858 0.858 0.858 0.858 0.858 0.858 0.873 0.974 0.975 0.974 0.975 0.9774 0.9773 0.9774 0.9774 0.9773 0.9774 0.9773 0.9774 0.9773 0.9774 0.9774 0.9774 0.9774 0.97750 0.9774 0.9774 0.97740 0.97750 0.97750 0.97750 0.97750000000
88 88 88 88 88 88 88 88 88 88	P 11 383 68.8 - 0.957 0.957 0.731 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.737 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.735 0.773 0.773 0.735 0.773 0.735 0.773 0.773 0.735 0.773 0.774 0.773 0.774 0.773 0.774 0.773 0.774 0.773 0.774 0.774 0.774 0.774 0.774 0.774 0.774 0.774 0.775 0.774 0.775 0.774 0.7750 0.7750 0.7750 0.7750 0.7750 0.7750 0.7750 0.77500 0.7750000000000
F WACH PN/L PT 5 0.956 1.482 684 24 X/EB Y/DP Z/FB WF 10.87 -0.03 -1.55 C-9 0.87 -0.03 -0.54 0.82 0.87 -0.03 0.53 0.83 0.85 -0.03 0.53 0.83 0.95 -0.95 0.95 -0.9	ACH PN/L PT 950 1.475 684 241 8 Y/PR Z/D8 241 7 -0.38 -2.04 0.964 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -1.54 7.970 7 -0.38 -0.67 0.835 -0.38 -0.15 0.835 -0.38 0.13 0.835 -0.38 0.13 0.855 -0.38 0.63 0.835 -0.38 0.63 0.855 -0.38 0.915 0.855 -0.38 0.956 0.957 -0.38 0.956 0.955 -0.38 0.956 0.955 -0.38 0.956 0.955 -0.38 0.956 <t< th=""></t<>
RUN TST P TA CCA 224 571 1 66 1 0.955 243.4 2 0.955 243.4 4 0.955 243.4 5 0.955 243.4 6 0.953 242.9 7 0.953 242.9 1 0.951 242.4 10 0.951 245 245 1000000000000000000000000000000000000	RUN TST PTN CENF 225 571 66 5 0 1 0.950 241.8 10.8 2 0.950 241.8 10.8 4 0.950 241.8 10.8 5 0.952 242.3 10.8 6 0.952 242.3 10.8 7 0.952 242.3 10.8 7 0.952 242.3 10.8 7 0.952 242.3 10.8 7 0.949 243.1 10.87 8 0.949 243.1 10.87 8 0.949 243.1 10.87 0.949 243.1 10.87 0.949 243.1 10.87 0.948 242.7 10.87 0.948 242.7 10.87 0.948 242.7 10.87

		0.038 1.C24	0.038 1.024	0.020 1.013	0.013 1.008	0.009 1.006	0.003 1.002	0.004 1.003	0.006 1.004	0.003 1.002	0.002 1.001	0.007 1.005	0.020 1.012	0.033 1.021	0.039 1.024	0.049 1.C31	0.053 1.033				CP DF/D	0.035 1.022	0.033 1.021	0.025 1.016	0.006 I.004	0.003 0.598	3.010 0.994	0.010 0.593	.012 0.993	0.013 0.992	0.010 0.554	1.005 0.997	0.002 1.001	0.023 1.014	0.031 1.020	0.044 1.028	0.044 1.028
					•		~	0) _	2	•	Č	0		2	0				1 VA/V					Ĩ	Ĩ	ĩ	1) T) I	ĩ	~	_	0	•	
ALPHA	-20.00 00/0 VE/V	216.0	0.972	0.959	0.904	0.878	0.876	0.860	0.873	0.877	0 837	506 • 0	0.919	0.95(0.962	0.967	0.970		ALPHA	-20.00	04/0 VF/V	0.976	0.976	179.0	0.923	0.915	0.912	0.885	0.874	0-868	0.886	0.896	0 • 92	0.961	0.970	0.969	0.977
11	04.0	0.959	0.959	0.919	C.798	0.745	0.742	C.709	0.734	0.739	0.759	0.806	0.832	0.907	0.936	0.952	0.962	1		70.5	QF/Q	C.966	0.963	0.948	0.832	0.812	0.801	0.748	0.728	0.716	0.750	0.773	0.831	0.925	C.950	0.955	0.973
0 0 0																		(a	384	M / M																
5	N 4 4 • C	0.968	C.968	0.953	058°)	C.86C	C.860	C.841	0.855	0.859	C.871	0.855	0.907	C.94 2	C.956	C.961	0.965	ſ	Ċ	243.5	vF/v	C.972	0.971	C. 966	C.91C	c. 902	358.0	0.868	0.856	0.850	C.865	C.881	0.911	C.955	0.965	0.964	619.0
PT 200	7/0P	2.04	1.55	1.04	0.71	0.54	0.37	0.20	0.04	0.13	0.29	0.46	0.64	15.0	1.16	1.47	1.97	1	1 d	688	3/28	2.03	1.53	1.03	0.69	0.52	0.36	0.19	0.03	0.14	0.31	0.49	0.65	0.58	1.18	1.48	1.98
RN/L	1.4 C C	C • 48 -	C.48 -	0.48 -	C.48 –	C-48 -	C.48 -	C.48 -	C.48 -	C.48	0.48	C.48	C.48	0.48	C.48	C.48	C.48		RN/L	1.477	Y/DB	- 54.0	0.43 -	0.43 -	0.43 -	- 64.0	0.43 -	0.43 -	C.43 -	0.43	0.43	C.43	0.43	0.43	0.43	0.43	64-0
F VACH	x/ra	10.87 -	1C.87 -	10.87 -	10.88 -	10.87 -	10.87 -	10.87 -	10.87 -	1C.88 -	1C+88 -	1C.88 -	10.87 -	10.88 -	10.87 -	10.87 -	10.87 -			5 0.952	X / 0.8	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	E.49	8.49	E.49	E.49
Th CCN		244.C	244.0	243.5	243.5	243.5	243.C	243.C	243.C	243.5	243.5	243.5	243.5	242.6	242.2	242.2	241.8		TN CCNI	. 66	c	243.5	244.0	243.5	243.5	243.5	244.0	244.0	244.0	243.5	243.5	243.5	243.C	242.2	242.2	242.2	242.3
TSTF	MACH	0.953	0.953	0.952	0.952	0.952	0.950	0.950	0.950	0.951	0.951	0.951	0.951	0.948	0.947	0.947	0.945		TST F	571 1	MACH	0.952	0.953	0.952	0.951	0.951	0.952	0.952	0.952	0.951	0.951	0.951	0.949	0.947	0.947	0.947	0.946
RUN		. –	2	ŝ	4	ŝ	φ	-	ω	თ	10	11	27	13	14	15	16		КUN	227	SEQ		2	~ ~)	4	ŋ	¢	-	œ	ნ	10	11	12	13	14	15	16

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		d/	12	10	66	95	16	06	89	89	62	94	66	06	16	24	31	31			d/	20	19	08	98	94	92	06	92	95	76	66	02	18	22	28	C r
		L.	1.0	1.0	6. 0	0° 5	6.0	6 ° 0	6 •0	6.0	5 ° 0	6.0	0.9	1.0	1.0	1.0	1.0	1.0			u d	1.0	1.0	1.0	5°0	6.0	0.5	6 . 0	6.0	5 •0	6.0	6 •0	1.0	1.0	1.0	1.0	0 - 1
		٥٥	0.019	0.015	100.0-	-0.008	-0.015	-0.016	-0.017	-0.018	-0.013	-0.010	-0.002	0.010	0.026	0.038	0.049	0.049			C P	0.031	0.030	0.013	-0.004	-0°010	-0.012	-0.016	-0.013	-0.008	-0.004	-0.001	0.004	0.028	0.036	0.044	0.048
		V A /V																			V A /V																
PHA_	00.00	A/Q VF/V	0.912	0.939	0.939	0.902	0.871	0.826	0.807	0.807	0.818	0.840	0.859	0.387	0.954	0.969	0.966	0.974	۸H	00.00	AVO VEZV	0.909	0.975	0.972	0.918	0.866	0.839	0.835	0.836	0.833	0.853	J. 883	0.916	0.958	0.973	0.971	0.973
r Al	.7 -2(10 0/	17	11	52	34	0	68	96	36	52	55	33	5	60	52	10	70	۲ ۵۱	1 -20	0	17	19	5 † †	18	3	52	5	57	55	26	6	8	12	59	60	56
F	70.	CF.	0.8]	0.8	0.86	0.78	C. 72	0.6	0.60	0.60	0.62	0.66	0.70	0.76	0.90	0.95	0.95	0.9	F	71.	95	0.94	0.94	0.94	0.81	0.71	0.66	0.65	0.65	0.65	C. 65	0.74	0.81	0.92	6.0	0.9	0.96
۵.	385	M / M																	C	385	WA/W																
ø	243.0	NF / N	0.858	0.929	C.929	0.888	C.852	C.803	0.783	0.783	0.794	C.818	0.839	0.871	0.946	0.964	0.960	0.970	ري	245.1	NF / N	0.964	C.971	0.968	0.906	0.847	0.817	0.813	0.814	C.811	C-833	0.866	C.903	0.951	0.969	0.966	0.969
Ld	688	2/08	2.02	1. 52	1.C2	0.69	0.53	0.36	0.19	0.01	0.14	0.31	0.48	0.64	0.98	1.18	1.48	1 . 98	PT DT	691	Z/08	2.03	I.53	1.03	0.69	0.52	0.36	0.18	0.01	0.15	0.31	0.48	0.65	9.58	1.19	1.48	1.98
RNJL	1.475	(/DB	- 10-0	- 10•0	- 01 -	- 10-0	- I).CI -	- 10-0	0.01 -	- 10-0	10.0	0.01	10.0	0.01	10.0	10.0	10.0	10.0	RNJ	1.484	108	1.36 -		- 36 -	3.36 +	3-36 -	3.36 -			3.36	36	3.36		0.36	0 - 3 G	0.36	36
NACH	0.950	X/08)	8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(6 • 49 -(8.49 -(N D C H	0.953	X/C8 /	8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8.49 -(8-49 -(
TN CONF	56 5	G	43.0	5°64	+3 • 5	44.0	44.0	43.5	43.5	43.5	44.C	43.0	43.0	43.5	13.0	43.C	42.7	42.3		56 5	C.	+5. I	45.1	45.1	45.7	+5.7	+2-1	+5.7	44.6	44.6	44.6	44.6	44.6	44.6	44.6	44.2	44.2
TST P	571 1 (MACH	.950 24	1.952 24	.952 24	.954 24	1.954 21	1.952 24	.952 24	1.952 24	1.953 24	1.950 24	1-950 24	.951 24	949 24	.949 24	948 24	1.946 24		571 1 6	MACH	.953 24	1.953 24	.953 24	.954 24	1.954 24	.954 24	-954 24	1.951 24	- 651 24	.951 24	.951 24	1.951 24	.951 24	.951 24	-949 24	1-949 24
NNA	228	SFO	10	2 0	3	4	0 4	6 0	~	0 8	с 5	10 0	11 0	12 0	13 0	14	15 0	16 C		229	SEG	1 0	20	9	4 0	50	С У	7 0	0 8	6	10 0	11 0	12 C	13 0	14 0	15 0	16 0

.019 • 013 1.019 1.010 • 000 1.015 666.0 0.999 .024 1.019 0.995 0.992 165.0 .020 .028 ..026 • C15 1.001 .005 .017 .026 0.991 165.0 1.010 .028 bF/p 0.986 PF/P .034 066.0 966.0 .031 0.002 0.009 -0.001 0.030 0.030 0.016-0.002 -0.006 0.021 0.026 0.039 0+034 -0.014 -0.013 -0.004 •040 0.042 0.031 -0.016 0.032 0.044 0.059 0.046 0.027 0.017 -0.006 0.046 0.050 -0.021 0.001 e d C V A VV V A JV 0.926 0.889 0.871 0.856 0.846 0.895 0.937 0.974 0.923 0.966 0.932 0.860 0.959 VF/V 0.878 0.892 VF/V 0.976 0.360 0.853 0.858 0.865 0.926 0.922 0.879 0.864 0.869 **0.**884 0.967 0.978 0.973 0.971 0.974 0.970 20.00 ALPHA ALPHA -20.00 0 A V O 0 A / Q 0.967 71.6 0.730 0.767 0.879 0.925 0.950 0.958 0**.**948 0.828 0.733 0.837 0.934 0.957 QF/0 0.873 0.718 71.5 QF /0 0.964 0.759 0.687 0.766 0.842 0.756 0.737 0.701 0.684 0.706 0.795 0.969 0.866 0.707 0.959 0.696 417 W V N а 387 MV VM С. 237.0 244.1 C.915 C.923 C.863 C.854 O.838 0.828 MF/W C.974 0.969 C.910 C.873 0.860 C.915 C.852 C.962 0.972 NL IN C.927 0.841 0.838 0.846 0.376 C.960 C.968 0.969 C.847 C.865 C.833 0.966 C.911 C.842 0.381 0.965 C-952 180 691 3 Z/CP 32 1.483 706 Y/CP Z/CP 0.48 0.65 -0.53 -0.36 0.14 0.58 • 45 -0-65 •49 -0.71 0.13 0.30 0.95 1.16 1.96 ω -2.04 -1-55 -1.04 -0.55 -0.04 0.47 0.64 -0.19 -0.02 -0.21 -0.45 -1.03 F d -2.03 -0.45 -1.51 I.1 **1**•9 5 C.9C2 I.483 5 0.950 1.480 RN/I D/Na -C.45 -0.03 -0.45 -0-45 -0.45 -0.45 -0.03 -0.45 -0-03 -0.03 -0.03 Y/08 -0.45 -0.45 -0.45 U \ Ľ SU1 -0.03 -0.45 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0-45 -0.45 -0.45 -0.45 e e 01 NACH HUVN X/CP 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 X/CB 10.87 1C.87 1C.87 1C.87 1C.87 8.49 8.49 8.49 8.49 C.87 C.87 0.87 C.87 C.87 0.87 C. 87 C. 87 0.87 0.87 10.87 TN CONF TN CONF 237.C 237.1 236.7 237.C 236.5 237.1 237.5 237.5 236.7 236.6 245.1 245.1 S 236.2 235.8 236.1 236.1 244.1 245.1 245.1 245.1 245**.**] 245**.**] 245.1 244.1 245.1 244. 236.(245.1 245.1 244.(236 . 96 0 e 66 ۵. 571 1 ۵. 571 1 MACH 0.902 MACH 0.950 0.952 0.950 0.899 0.899 0.899 0.899 0.901 0.902 0.903 0.9003 0.9003 0°853 0°900 0.952 0.952 006.0 0.899 0.901 951 TST TST 0 29 0 PUN 230 SEC 2 12 14 Ś PUN 231 SEQ 5 14 5 M + 10 VO M ω $\boldsymbol{\sigma}$ m 4 Ŷ ~ ω σ 16

		ú∕sa dù	0.035 1.020	0.038 1.022	0.012 1.007	0.015 1.009	0.011 1.006	0.011 1.006	0.011 1.006	0.003 1.002	0.015 1.008	0.012 1.007	0.019 1.011	0.021 1.012	0.027 1.015	0.033 1.019	0.042 1.024	0.044 1.025			CP PF/P	0-030 1-015	0.030 1.015	0.019 1.010	0.014 1.007	0.010 1.005	0.014 1.007	0.016 1.008	0.010 1.005	0.013 1.007	0.014 1.007	0.008 1.004	0.011 1.006	0.022 1.011	0.025 1.013	0.028 1.014	0.039 1.020
		V A / V																			V A /V																
ALPHA	-20.00	0A/Q VF/V	0.930	0.932	0.936	0.896	0.863	0-824	0.817	0.823	0.822	0.851	0.859	0.891	0.950	0.970	0.973	0.973	ALPHA	-20.00	DA/Q VF/V	0.923	0.931	0.918	0.896	0.872	0 • 866	0.360	0.868	0.879	0.880	0.895	0.908	0.946	0.969	0.980	0.976
11	71.4	0F /0	C-863	0.870	0.865	0.784	0.719	C.649	0.638	0.644	0.647	0.698	0.715	111.0	0.903	0.948	0.962	0.961	LL	71.1	0F/0	0.848	C.864	0.832	0.785	C.738	0.728	0.719	167.0	0.753	0.756	0.781	0.809	0.891	0.944	0.967	0.964
۵	415	N/Vn																	٩	452	M / M																
G	5 237.4	N / LN	C.92C	0.923	C.927	0.882	0.845	0.803	0.796	C.8C2	0.801	C. 832	C.841	0.876	C.943	0.965	C.965	C.968	ى	225.3	MF /N	C.914	C-923	C•9C8	C. 883	0.857	C. 850	C.844	C.853	C. 865	C.866	0.882	0.857	0.939	C.965	116.0	C.972
- p1	102	Z / DB	-2.03	-1-53	-1.02	-0.69	-0-53	-0.36	-0-19	10.0-	0.16	0.33	0.48	0.64	0.98	1.18	1.48	56°1	Ъ1	2126	Z/CB	-2.04	-1.54	-1.04	-0.71	-0-55	-0-37	-0.20	-0-04	0.13	0.29	0•46	0.63	1.6.0	1.16	1.46	1.56
RNA	1.484	Y708	- 10-0	c.01 -	0.01 -	- 10-0	C. C1 -	- 10-0	C. C1 -	- 10-0	0.01	c. c1	0.01	0.01	C.C1	10.0	0.01	10.0	RN/I	1.452	4/DP	0.03 -	0.03 -	- 20-0	C• 03 -	C+C3+	0.03	0.03 -	0.03 -	0.03	0.03	0.03	0.03	0.03	c•03	c• c3	0.03
NACH	0.904	X/D3	8.49 -	6 49 -	8.49 -	8.49 -	8.49 -	8.49 -	E. 49 -	6.49 -	8.49 -	8.49 -	8.49 -	8.49 -	8.49 -	6.49 -	8.49 -	B.49 -	PACE VACE	0.851	X/C8	C. 87 -	C.87 -	C-87 -	C. 87 -	0.87 -	C-87 -	C-87 -	C.87 -	C. 87 -	C.87 -	C.87 -	0.87 -	0.87 -	0.87 -	C.87 -	c. 87 -
TA CONF	66 5	ç	37.4	37.4	37.4	37.4	37.C	36.6	36.6	36.6	36.1	36.2	35.7	35.3	36.2	36.2	35.3	35.3	TN CCNF	66 55	Ľ	29.3 1	29.3 1	29.8 1	29.8 I	29.8 1	29.8 1	29.4 1	29.4 1	29.1 1	29.5 1	29.5 1	30.2 1	30.2 1	30.1 I	30.5	30.C 1
TST P	571 1	MACH	0.904 2.	0.904 2	0.904 2	0.904 2	0.902 2	0.901 2:	0.901 2.	0.900 2	3. 899 2	0.899 2 .	0.898 2.	0.896 2	3.899 2	3.899 2.	0.896 2).896 2	TST P	571 1	MACH	3.851 2	3.851 2	0.852 2	0.852 2.	0.852 2.	3•852 24	0.850 2	J.850 2). 849 2.	7.850 2	3.851 2.	0.853 2.	0.853 2). 853 2.).854 2	0.854 2
RUN	232	SFO	7	2	m	4	5	9	~	8	6	10 (11	12 (13 (14 (15 (16 (RUN	233	SEC	1	2	m)	4	5	\$		8	6	0		12	13	14		16 (

1.005 1.011 1.007 1.007 1.010 .007 1.003 100.1 1.010 pF/p .003 1.001 1.C12 1.007 .010 ..016 ..005 ..006 ..003 1.005 .007 .001 .003 .010 .005 .004002 •000 .010 PF/P 018 1.013 0.005 0.013 0.011 0.002 0.002 0.003 0.006 0-020 0.013 0.021 0.028 0.021 0.025 0.039 0.035 0.014 0-020 0.022 0.006 0000.0 0.016 0.011 0.015 0.012 0.004 0.011 0.013 0.022 0.029 <u>a</u> å V A /V V A /V 0.859 0.839 0.835 0.835 0.842 0.842 0.858 0.870 0.917 0.881 0.890 0.955 0.988 VF/V 0.931 0.941 0.972 0.912 0.908 0.915 0.970 0.983 0.929 0.982 VF/V 0.978 0.919 316.0 0.916 0.913 0.930 0.980 0.964 ALPHA -20.00 -20.00 ALPHA 0 A V O 0 A O 0.715 0.678 71.0 0.669 0.959 70.9 0F/0 0.834 C.818 0.819 0F/0 0.874 0.760 0.681 0.853 0.854 0.925 0.681 0.711 0.777 0.912 0.980 978 0.970 0.825 0.811 0.822 0.941 0.972 0.853 0.834 0.736 0.967 0.947 0.821 0.972 F 452 WVVW 496 シント 0 ۵ 230.6 223.0 106.0 C.824 C.842 C.855 C.877 0.977 0.969 0.922 569.0 0.843 0.974 NF / N 216.0 NF /N C.817 C.949 C.986 016.0 906-0 C. 899 0.905 .867 0.984 0.902 0.904 0.922 .821 0.825 0.921 C.907 0.967 0.959 0.979 C.981 151 728 0.14 -1.54 • 48 0.99 -0.53 **Z/DB** -2.03 -1.53 -0-69 -0.19 0.64 1.18 •48 1.95 -2.04 -0.20 0.12 Fa -1.03 -0.53 -0.36 0.31 Z/08 0.25 0.46 -0.02 0.64 16.0 1.16 •46 10 -0.37 -0.04 • 6 5 0.854 1.497 5 0.801 1.513 PN/L X/CB Y/DB **RN/L** -0.01 -0.01 Y/DB 0.41 E.49 -C.CI -0.01 C.41 -0.01 -0.01 10.0-10.0-0.41 0.41 .41 0.41 -0.01 -0.01 -0-01 C-41 0.41 0.41 -0.01 -0-01 -0.01 C.41 0.41 0.41 -0.01 C.41 0.41 0-0-0.41 0.41 VACH N C H E.49 . 8.49 8.49 8.49 8.49 8.49 8.49 8.49 • 49 8.49 8.49 8.48 8.49 8.49 E.49 LC.87 LC.87 LC.87 X/CB 10.87 1C.87 1C.87 1C.87 .C.87 0.97 10.87 1 C. 87 10.87 10.87 C-87 0.87 TST P IN CONF CONF 229**.** E 229**.** 4 227.9 227.9 229.5 230.6 231.2 230.6 228.2 228.2 223•0 222•5 223•1 223.1 222.5 222.5 223.1 223.5 229.8 229.1 229.1 229.1 227.5 230.2 222.5 223.0 223.0 223.0 222.5 222.5 223.5 2 66 C 571 1 66 C c. 0.852 0.852 0.850 0.849 0.849 0.849 0.847 0.847 0.854 0.854 0.852 MACH 0.857 0.801 0.800 0.800 0.800 0.800 MACH 0.801 0.800 0.846 0.846 0.850 0.846 0.853 0.800 0.802 0.803 0.802 0.801 0.801 0.801 0.801 0.801 **TST** 571 234 234 550 4 ŝ Ø -Ø 6 C - \sim **6**13 4 W 235 SEQ N ŝ RUN .+ \mathbf{S} ~ œ 0 n 2 \$ ហ σ -Ś

		c/ ۲	315	908	005	100	004	03	100	204	100	202	204	008	600	010	015	014	
		ā		1.	1.(-	1.(-	1.	-			.	1.(.		1.(
		C b	0.034	0.017	0.011	0.003	0.008	0.006	0.003	0.008	0.002	0.005	0.010	0.018	0.021	0.023	0.033	0.030	
		VIEV																	
		VF/V	0.907	0.925	0.920	0.890	0.881	0.875	0.881	0.875	0.886	0.894	0.893	016.0	0.941	0.965	0.976	0.983	
ALPHA	-20.00	0A/0																	
11	70.8	0F /0	0.817	0.847	0.834	0.773	0.756	0.746	0.755	0.746	0.765	0.781	0.780	0.817	0.880	0.933	0.960	0.974	÷
٩	497	MA/M	-			-					-					-			C
9	222.5	ME / N	0.897	C.917	C.911	C.879	0.868	0.863	0.868	C-862	C.874	0.883	0.882	0.900	C.924	C.961	0.973	C • 980	c
Ld	757	Z/08	2.04	1.55	·1.04	.0.7I	0.54	0.37	0.20	0.04	0.13	0:30	0.46	0.63	0.96	1.15	1.47	1.97	10
RN/L	1.512	Y/DB	0.03 -	0.03 -	- 20.0	0.03 -	C. C3 -	0.03 -	C. 03 -	- 20-0	0.03	C• C3	C.03	C. 03	0.03	c. 03	C• C3	0.03	17 40
NACH	C.800	LCB	- 18.	- 18.	- 87 -	- 18.	- 13.	- 19 -	. 87 -	- 18.	- 87 -	- 73 -	. 87 -	- 19.	- 87 -	. 87 -	- 19-:	- 18.	
CONF	لا م	×	5 10	.1 10	.1 10	.1 10	.0 10	.0 10	•C 1C	.0 10	.0 10	.0 10	.0 10	• C 1 C	.0 10	.5 10	.5 10	.1 10	
F TN	1 66	Ċ	222,	223,	223,	223.	223,	223,	223.	223	223,	223.	223,	223.	223,	223.	223.	223,	i F
121	571	MACH	0.800	0.801	0.801	C.8C1	0.801	0.801	0.801	0.801	0.301	0.801	0.801	0.801	0.801	0.802	0.802	C.8C1	TCT
RUN	236	SEG		2	n	4	ŝ	9	٢	æ	6	10	11	12	13	14	15	16	

	0	RI E	GI PC	NA 002	AL R	P QU	A(JA	GE LI'	IS TY	5								
		pF∕p	1.020	1.016	1.007	1.004	1.002	1.001	1.003	1.006	1.008	1.003	1.010	1.007	1.010	1.007	1.006	1.007
		СЪ	0.044	0.035	0.016	0.009	0.004	0.001	0.006	0.013	0.018	0.007	0.023	0.016	0.022	0.015	0.013	0.016
		V A /V																
		VF/V	0.974	0.975	0.962	0.916	0.893	0.889	0.876	0.883	0.878	0.891	0.894	0.916	0.946	0.968	0.989	0.989
ALPHA	-20.00	OA/O																
	70.8	0F/0	0.962	0.959	0.924	0.825	0.778	0.770	0.747	0.762	0.754	0.777	0.787	0.828	0.891	0.935	0.981	0.982
a.	497	MA/M																
ى	222.5	ML / N	0.971	c.972	0.958	C.906	0.881	0.877	3.863	C.870	0.865	C.880	0.883	C-9C7	0.939	0.964	796.0	0.988
l d	2 757	Z/DB	-2.04	-1.54	-1.05	-0.71	-0-54	-0.37	-0-19	-0.03	0.13	0.30	0.47	0.63	0.96	1.17	1.47	1.96
	0 1.51	Y/DB	-0-38	-0.38 -	-0-38 -	-0.38 -	-0-38 -	-0-38 -	-0-38 -	-0.38 -	-0.38	-0.38	-0-38	-0.38	-0.38	-0-38	-0.38	-0.38
	5 C.8C	X/CB	1C.87 -	10.87	10.87	10.87 -	10.87	10.87 -	1C.87 .	10.87	10.87 -	1C.87 -	10.87 -	1C.87	10.87	1C.87 -	1C.87	10.87 -
	66	0	22.5	22.6	22.C	22.6	22.0	22.0	22.5	22.5	22.6	22.6	23.1	23.6	22.6	22.5	22.5	23.5
a ISI	571 1	MACH	.800 2	.799 2	.798 2	.799 2	.798 2	. 799 2	.800 2	.800 2	.799 2	. 799 2	.800 2	.801 2	. 759 2	.800 2	.800 2	.803 2
N N N N	237	U U V	0 1	2 0	9 8	4	50	9	7 0	о 8	6	10 0	11 0	12 0	13 0	14 0	15 0	16 0

		¢a b⊧/b	0.035 1.016	0.032 1.014	0.021 1.009	0.009 1.004	0.011 1.005	0.009 1.004	0.002 1.001	0.009 1.004	0.009 1.004	0.002 1.001	0.008 1.004	0.012 1.005	0.015 1.007	0.013 1.006	0.027 1.012	0.032 1.014			Cb bE/D	0.025 1.011	0.016 1.007	0.014 1.006	0.004 1.002	0.003 1.001	-0.001 1.000	965*0 600*0-	-0.014 0.993	0.001 1.001	0.014 1.006	0.010 1.004	0.009 1.004	0.019 1.009	0.023 1.010	0.022 1.010	0.025 1.011
		V VAV	0	•	.0	7				0	7	•	-	~	10	•		~			V VA/V	10	~	0	.+		` ~	' .0		.+	~	•	~		m	.0	10
AL PHA	-20.00	QA/Q VF/V	0.980	0.979	0.955	0.90	0.898	0.891	0.891	0•89(0 . 88	06*0	0.901	0.92	356•0	0.96	0.981	0.98	ALPHA	-20.00	DA/O VE/V	0.985	0.989	0.98(0.934	516*0	0.913	906*0	0 895	0 . 884	0 897	506 • 0	0.927	0.961	0.978	0.986	0.985
11	70.7	0F/0	179.0	0.968	0.910	C.8C8	161.0	0.777	0.774	0.775	C.770	0.792	0.808	0.841	0.908	0.938	016.0	0.975	11	7.07	0140	0.978	0.982	0.962	0.859	0-8-0	0.816	0.799	C.775	C•769	C•790	0.812	0.848	0.922	0.961	776.0	0.978
۵	154	W / M																	۵	197	w / Am																
ى	222.0	NF/N	C.978	776.0	C.95C	0.897	0.887	0.879	0.879	0.878	0.875	C•850	C.857	0.915	C.950	0.965	679.0	0.980	Ŀ	223.1	NF / N	C.983	C.988	C.978	0.926	0.910	C.9C4	0.896	0.883	0.872	0.886	658.0	0.919	C.956	0.975	C.984	0.983
L d	0 757	Z/08	-2.04	-1.55	-1.04	-0.70	-0.54	-0-36	-0.20	-0.04	0.13	0.29	0.47	0.63	0.96	1.16	1.47	1.97	Ld.	4 758	Z/D8	-2.03	-1.52	-1.03	-0-65	-0.52	-0.36	-0.19	-0.02	0.14	0.30	0.48	0.65	0.98	1.19	1.48	1.58
NA A	1.51(¥/08	- 34°-	- 84.0	C.48 -	- 84.0	0.48 -	C.48 -	- 84°-0	C.48 -	0.48	0.48	0.48	0.48	C.48	0.48	0.48	C.48	I/Na	1.514	Y / DB	0.43 -	C.43 -	0.43 -	C.43 -	C.43 -	0.43 -	0.43 -	C.43 -	0.43	0.43	64.0	C • 43	C + 3	0.43	0.43	0.43
F WACH	5 0.799	X / DB	10.87 -	10.87 -	1C.87 -	10.87 -	10.87 -	10.87 -	10.87 -	10.87 -	10.87 -	1C.87 -	10.87 -	10.87 -	10.87 -	10.87 -	10.87 -	10.87 -	F WACH	5 0.801	X / CB	8.49	8.49	8•48	8.49	8•48	<u>8</u> .48	8.49	8.49	8.49	8.49	8.49	e 4 4 9	E.49	٤•49	8•48	8.48
TST P IN CON	571 1 66	MACH 0	0.799 222.0	0.758 222.0	0.757 221.5	0.797 221.5	0.798 222.C	0.798 222.C	0.798 222.0	3.800 222.5	3.800 222.5	0.800 222.5	0.799 222.0	3.800 222.5	3.800 222.5	0.800 222.5	3.801 222.4	0.801 222.4	TST P IN CCN	571 1 66	MACH 0	0.801 223.1	0.801 223.1	0.801 223.0	3.803 223.5	0.803 223.5	3.803 223.5	J.804 224.0	0.804 224.C).804 224.C	0.802 223.C	0.801 223.0	2.8C0 222.5	3.800 222.5	3.799 222.6).758 222.C).758 222.C
RUN	238	SEQ	1	2	с С	4	ບ ທ	9	7 (8	6	10	11 (12 (13 (14	15	16 (NUA	239	SEC	-	2	3	4	ŝ	6 (7 (C) CD	6	10	11 (12 (13 (14	15 (16 (

		0 C / D	110 1				1.142	100.1	0.596	0.997	0.596	0.995	0.595	0.598	700				I - UU	1.C11				07.00		1.014	1.013	1.010	1.003	1.000	0.999	0.996	1.997	0.999	0.599	000.1	1.001	1.007	600-1	1-009	1.011
		a J						0.00	010-0-	-0.006	-0-010	110.0-	-0-011	+00-0-	0.008				010-0	0.025				c D			0.028	0.023	0.006	-0.000	-0.003	-0-010	-0.008	-0.003	-0.003	-0-00	0.003	0-015	0.019	0.021	0.025
		V A VV																						V V VV						•	•	•	,	,	•	,					
AH PHA	-20.00	DA/O VE/V	0.00	0.10 0	0.970	0.852		610-0		0. 643	0.838	0.347	0 - 868	0.877	0.901	0.955	0.976	0.985		0.986	-	ALPHA	-20.00	0A/0 VF/V	0.980			606.0	0.918	0.881	0.864	0.344	0.459	0.858	0.875	0.395	0.915	0.958	0.974	0.945	0.936
11	70-6	0F 70	0.806	0.875	0.837	0.800	0.751	112 0			0.013	0.689	C.727	0.745	0.796	0.907	C.952	0.977		0.979	,		70.5	0F/0	C.970	0.968					0. 723	0.684	111.0	0.712	0.742	0.782	0.821	0.914	0.950	.975	616.0
۵.	497	NV/N																			c	2	457	N V N										Ŭ	<u> </u>	Ŭ	Ŭ	U	0	U	0
U	222.0	MF / W	0.892	506-0	0.912	C.837	0-866	0.846	30.00		770.0	C • 8 3 Z	C•855	C.864	C.891	C.949	519.0	0.984		0•38 4	ç	و	222.5	N / L N	0.978	978°	965		070			570.	642.	.844	- 862	.884	•906	• 953	116.	• 983	• 584
L pT	0 757	Z / DB	-2.02	-1.53	-1.03	-0.69	-0-53	-0-36	0.0			C. I.)	15.0	0 . 48	0.65	76.0	1.17	1.48	1 C 0	04.1	FO	- 1	151	Z/08	2.03 (1.52 (1-03	0.69	0.52					0.14 0	0.32.0	0.48 0	0.65 C	0•58 C	1.19 0	1.48 U	1.58 U
Na t	1.51	Y/DB	. 10-0-	. 10-0-	- 10-0-	- 10-0.	0.01	- 10-0	10-0-				10.0	0.01	c.c1	10.0	c.01	0.01		10.0	IN NG		E1 - 1 - 1	Y/DB	0.36 -	0.36 -	C.36 -	C-36 -	- 36 -		2.0					9.99	1.36	0		0 1 11 1	0
NAC	0.799	X/08	6,49 -	8.49 -	8.49 -	- 64•3	8.49 -	- 64-3	8.49	8.40		7 (7 • 0	6 • 4 A	8•49 -	8.49 -	8.49 -	- 64.9	9.49 -	- 67 -		A C F		0.8CC	(/ LB	- 49 -	- 65 -	- 49 -	- 64-	- 49 -	- 67	- 07	07				. 49 -	- 65.	- 44	0- 65 .) - 54.	1 64.
LCNE	ŝ		0	0	44.1 •	u 1	u 1	u .	u v	u	، د		2	0	0	с ч	0	0	u		L N F			~	w	8	1	8	1		, α	- u) 0) 0	0 0 0 0	0 0 0 0	ນ (ເກີຍ	ຍ (ກ.ເ	ມ ເກ	00 0 4 1 U	υ c ι ι	ט זי
D T V	1 66	с т	9 222	9 222	3 221	222	222	222	222	222	000			223	223	223	223	223	222.	1	d I v	1 22	00	3	222	223.	223.	223.	223.	223	223.	222	, L C C	- C C C	222	• 222	• 277	• 7 7 7	.227	• • • • • •	•122
TST	571	MACI	52.0	0.79	0.79	0.80(0.800	C- 800	0.800	0-800	0.801				0.801	0.801	0.801	0.801	C-800		151	571		MACH	0.800	0.801	0.801	0.801	0.801	0.801	0.801	0.800	108-0								
RUN	240	SEC	1	2	3	4	ŝ	Ŷ	7	8	σ	È C		1;	17	-	14	5	16	•	RUN	170		9. 11 12	- (N	n	4	LL)	Ś	~	ŝ	σ						1 1		2

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		لأنه مداه	0.027 1.012	0.022 1.010	0.011 1.005	0.008 1.004	0.004 1.002	0.002 1.001	-0.005 0.998	0.004 1.002	-0.006 0.597	-0.000 1.000	0.006 1.003	0.006 1.003	0.015 1.007	0.009 1.004	0.015 1.007	0.021 1.009			Co pr/p	0.043 1.011	0.046 1.012	0.035 1.009	0.023 1.006	-9.005 0.999	0.002 1.2000	200.1 010.0		0.028 1.007	0.032 1.008	0.014 1.005	-0.001 1.000		0.00/ 1.002	0.015 1.004	0.032 1.008
A H	00	D VE/V VA/V	0.934	0.986	0.976	0.910	0.834	0.876	0.866	0.863	0.872	0.872	0.396	0.921	0.959	0.935	0.939	0.987	НА	00	Q VE/V VA/V	0.975	0.973	0.950	0.920	0.928	0.912	0.912	0.913	0.906	0.906	0.924	0.941	0.962	0.978	0.987	0.978
TT ALPI	70.6 -20.	CF/0 04/1	0.977	610.0	136-02	0.814	0.761	0.745	0.724	0.723	0.735	0.738	C.186	0.833	0.915	0.970	0.981	C.980	TT ALP	64.8 -20.	1 0F/0 0A/	0.957	0.955	0.905	0.842	0.852	0.821	0.824	0.828	0.816	C.818	0.847	0.878	0.922	0.955	0.975	0.961
C.	222.6 498	NE N NA/M	.982	.985	513	.900	.872	.863	.852	.850	.859	.859	.885	.912	.954	.983	.987	0.985	۹ ۵	175.8 695	ME /N MA /N	513	179.0	747 2	0.915	0.924	0.906	0.906	0.908	006-0	0.901	c.919	759.0	0.960	0.976	C.986	C.977
PU/L PT	1.514 758	/08 Z/08	.45 -2.03 C	.45 -1.53 0	.45 -1.04 0	.45 -0.67 0	.45 -0.53 0	.45 -0.36 0	.45 -0.19 0	.45 -0.02 0	.45 0.14 0	.45 0.31 0	.45 0.48 0	.45 0.65 0	.45 0.98 (.45 1.18 (.45 1.48 (.45 1.98 (PN/L PT	1.511 887	/DB Z/DB	.41 -2.05 (.41 -1.54 (.41 -1.04 (.41 -0.71	.41 -0.53 (.41 -0.37 (.41 -0.20	.41 -0.03	.41 0.13	.41 0.25	.41 0.47	.41 0.63	1.41 0.97	.41 1.16	.41 1.47	.41 1.96
CNF MACH	5 0.799 1	X/DB Y/	8.48 -0.	8.49 -0.	8.48 -0.	8.49 -0.	8.49 -0.	8.48 -0	8.49 -0.	8.49 -0.	8.49 -0	8.49 -0	8.49 -0	8.49 -0	E.49 -C	8-49-0	8-49 -C	8.49 -0	LNF WACH	5 0.601	X/DB Y	10.88 0	16-88 0	10.88 0	1C-88 C	10.88 0	1C.88 C	2 1C.88 C	1C.88 C	2 1C.88 C	1C.88 0	10.88 C	0 1C.88 C	2 IC.88 0	e 1C.88 C	2 IC.88 0	9 1C.88 0
TST P TN C	571 1 66	MACH 0	0.799 222.6	0.800 222.5	0.799 222.0	0.799 222.0	0.799 222.0	0-799 222-0	0-799 222-0	0.799 222.0	0.800 222.5	0.800 222.5	0.800 222.5	0-800 222.5	0.800 222.5	0.758 222.0	0-800 222.5	0.800 222.5	T A T A T A T	571 1 66		0-601 175-6	0.557 174.0	0.596 173 4	0.556 173.5	0.599 174.6	0.601 175.8	0.600 175.2	0.600 175.2	0.600 175.2	0.599 174.0	0.596 173.4	0.597 174.(0.600 175.2	0.602 175.1	0.600 175.2	0-602 175-1
RUN	242	C L V	, <u></u>	• •		4	ſ		-	· œ) o	10		1	: -	14	- 4C -	16	NIID	242		2	7 I	1 4	· u	\$	2	80	σ	10	11	12	13	14	15	16	17

		bF/⊅	1.000	1.001	1.004	1.004	1.002	1.005	1.005	1.002	1.002	1.003	1.004	1.003	1.003	1.005	1.005	1.010			pr/p	1.007	1.005	1.005	1.005	1.001	666*0	1.003	0.930	1.001	1.003	1.006	1.007	1.007	1.003	1.007	1.007
		d U	-0.001	0.005	0.014	0.015	0.007	0-020	0.020	0.010	0.008	0.011	0.018	0.013	0.011	0.022	0.019	0.038			CD	0.026	0.020	0.019	0.018	0.003	-0.002	0.011	-0.277	0.003	0.012	0.024	0.029	0.027	0.014	0.029	0.027
		VA/V																			V A /V																
ALPHA	-20.00	QA/U VF/V	0.936	0.934	0.926	0.893	0.894	0.873	0.869	0.880	0.892	0.892	0.890	0.916	0.946	0.950	0.983	0.978	ALPHA	-20.00	QA/Q VF/V	0.981	0.982	0.949	0.909	0.894	0.893	0.884	0.916	0.909	0.905	0.902	0.914	0.933	0.963	0.979	0.984
11	65.1	0F/0	0.868	0.865	0.852	0.789	061.0	0.752	0.745	0.765	0.785	0.786	0.784	0.833	0.892	0.901	0.969	0.963	T T	65.3	CF/0	0.967	0.967	0.899	C.820	0.788	0.786	0.772	0.771	0.816	0.812	0.808	0.832	0.869	0.926	0.963	0.972
D.	969	MA/M																	۵	695	NV N																
ى	175.2	MEZN	0.932	C •929	c.921	c. 886	0.888	C.865	C.861	0.873	C.886	0.886	C.884	C.911	0.943	C.946	C.982	C.977	C3	175.2	NF/N	C.98C	C.981	C. 946	C.903	0.887	0.887	0.878	C.910	C06*0	C.900	C. 856	506 ° 0	0.929	C.961	0.978	C-983
Ld .	883	2/08	-2.04	-1.54	-1-04	-0.71	-0.54	-0.37	-0.20	-0.04	0.13	0.30	0.46	0.63	0.98	1.15	1.46	1.96	Ld .	5 887	2/C8	-2.05	-1.53	-1-05	-0.70	-0.54	-0.38	-0.21	-0.05	0.12	0.30	0.46	0.63	0.96	1.16	1.47	1.96
LAN I	1.50	47.CB	· C• 03 -	- E0-0	- C. 03 -	- 60 • 0	0.03 -	· c. c3 -	- 20-0	· C• 03 -	E0 * 0.	.0.03	·0•03	0.03	0.03	·c. 03	-0-03	E0 • 0.	I RN/I	1.500	γ/08	- 35-0	0.38 -	- 38 - J	0.38 -	0.38 -	- 85.0	0.38 -	- 3 E • O	0.38	0.38	C.38	0.38	C. 38	0.38	0.38	C. 28
N A C H	0.500	X/CR	C. 83 -	0.88 -	C. 88 -	C. 88 -	C.88 -	C. 88 -	0.88 -	C. 88 -	C.88 -	C. 88 -	C. 88 -	C.88 -	C.88 -	C. 88 -	C. 88 -	C. 88 -	NACH	0.600	X/DR	0.88 -	C. 88 -	C • 83 -	C . 88 -	C. 83 -	C. 88 -	C. 88 -	C • 88 -	C 88 -	C • 88 -	C. 38 -	C-87 -	C • 87 -	C.87 -	C.87 -	C.87 -
UCNE	U)		• 2 1	•4 1	• 4	• 2 1	•2 1	• 8	• 8 1	۔ ع•	• € 1	• 0 1	• C]	•0	- - -	• ć 1	• € 1	• ć 1	UD0	ŝ		• 2	• € 1	• 8	• 2 1	• 2 1	• 2 1	•2 1	• 2 •	• 8	•2 1	• 2	• € 1	• 2 1	• €	• 8 •	- 2 -
D T V	1 66	U I	0 175	3 175	3 176	1 175	1 175	2 175	2 175	1 175	9 174	8 174	8 174	8 174	8 174	9 174	9 174	9 174	NL d	1 66	ю	0 175	9 174	2 175	0 175	0 175	0 175	1 175	1 175	2 175	0 175	0 175	9 174	0 175	9 174	1 175	0 175
TST	571	MACI	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.59	0.59	0.59	0.59	0.59	0.59	0.59	0.59	TST	571	MACI	0.60	0.55	0.60	0.60	0.60	C.60	0.60	0.60	0.60	0.60	0.60	0.55	C. 6C	0.59	0.60	0.60(
RUN	244	O H O	T	2	m	4	n	Ś	-	œ	6	10	11	12	13	14	15	16	RUN	245	SEO	-	~	(7 1)	4	רע	9	-	8	6	10	11	12	13	14	4) 	16

1.002 1.007 1.006 1.003 1.002 1.003 1.004 1.007 b F∕p 1.004 • 004 .006 ú∕ ⊐ 666*0 1.002 1.001 1.003 1.000 1.000 100.1 .001 .006 .007 .005 .003 .002 1.003 1.001 1.001 1.002 1.004 1.002 1.005 0.014 0.009 0.018 0.004 0.004 0.014 0.011 0.015 0.012 0.016 0.022 0.028 0.0011 0.007 0.006 0.024 0.007 0.003 0.014 0.028 0.024 0.028 0.020 0.005 -0.003 00000 -0.001 0.007 0.007 0.015 σ •01 C b 6 C V A /V V A /V 0.961 0.905 0.897 0.897 0.981 0.983 0.895 0.906 0.906 0.915 0.925 0.983 0.985 0.918 0.913 0.908 0.950 116.0 0.896 VF/V 0.934 VF/V 0.985 0.978 0.922 0.931 0.986 0.987 0.899 0.973 ALPHA -20.00 -20.00 AL PHA 0 A V O QA/C 0.967 0.971 0.971 0.921 0.796 0.793 0.792 0.812 0.812 65.7 0F/0 0.831 0.849 C.899 0.946 0.969 0.974 0.967 0.974 0.957 0.820 0.825 0.813 0.793 66.1 01 - 10 0.834 0.820 0.799 0.840 0.865 0.944 0.972 0.975 0.979 696 N / VN 695 M V M C ٥ 175.2 0•982 0•958 0•950 0•950 0.895 C.890 0.889 006-000 C-900 C.920 0.969 NF/N 0.910 0.946 C.980 C.984 O.977 C.912 0.908 0.908 C.9C2 0.905 0.852 026.0 0.985 C.982 0.984 0.917 C.890 179.0 C.98(¢ 6.0 0 1.503 887 V/DB Z/DB C-43 -2.03 C -0.20 -0.37 1.46 -0.65 -0.52 -0.36 0.12 0.30 0.47 0.63 1.17 -1.03 -0.15 0.15 70.97 79. -1.52 -0.54 -0.04 F a -0.71 0.45 0.66 σ ω œ ω .6•0 1.1 5.1 5 0.599 1.502 MACH RN/L C.6C0 1.5C3 C • 43 0 • 43 -C.48 0 • 43 0 • 43 0 • 43 -0.48 -0-48 -0-48 -0.48 -0.48 -0.48 -0.48 -0.48 -0.48 -0.48 0.43 -0.48 C+43 0.43 0.43 0-43 3 3 -0-4 0.4 0.4 0.4 C. 4 . 3 NACH HUVA X/CB 8.49 X/DR C.87 C.88 C.88 C.87 C.83 C.83 C.87 C.88 C.87 C.87 88 TST F TN C 571 1 66 4ACH 6 660 175-2 660 175-2 600 175-2 600 175-2 70 175-2 00 175-2 70 175-2 8 175-2 8 175-2 8 J CONF CONF 174.6 174.6 174.6 174.6 175.2 175.2 175.2 175.2 175.2 175.8 175.8 175.8 175.8 175.8 175.8 175.8 99 0 175.2 ω 175.1 N . دی 2 0 571 I MACH 0.599 0.599 0.559 0.559 0.660 0.660 0.660 0.660 0.660 0.660 0.602 0.602 0.559 0.602 0.602 0.602 0.602 0.602 0.600 TS1 0.600 0.602 60. RUN 246 SEQ m 45.00 20 113 RUN 247 SFC ω σ 4 ŝ 9 NMYUNNON 2 120452

	Cb bE/b	0.026 1.007	0.011 1.003	0.007 1.002	0.003 1.001	-0.004 0.999	0.000 1.000	0.001 1.000	665 0 200 0-	0.003 1.001	0.000 1.000	0.002 1.000	-0-003 0-999	0.009 1.002	0.015 1.004	0.029 1.007	0.028 1.007			CP OF/P	0.025 1.006	0.025 1.006	0.006 1.001	0.001 1.000	0.006 1.001	0.003 1.001	-0.004 0.999	-0.007 0.598	-0.003 0.999	-0.005 0.999	0.013 1.003	0.005 1.001	0.006 1.001	0.014 1.004	0.019 1.005	0.014 1.004
ALPHA -20.00	CA/Q VE/V VA/V	0.916	0.931	0.926	0.894	0.869	0.852	0.837	0.867	0 - 864	0.862	0.880	0.903	0.956	0.978	0.979	0.982	ALPHA	-20.00	CA/Q VE/V VA/V	0.945	0.983	0.972	0.922	0.882	Ú . 865	0 • 364	0.875	0.871	0.874	0.885	0.922	0.965	0.977	0.988	0.990
P TT 695 66.2	MA/M GF/Q	0.835	0.861	0.851	0.789	0.742	0.712	0.685	0.738	0.734	0.729	0.763	0.804	0.910	0.956	0.963	010.970	p TT	695 66.5	WA/W QF/Q	0.974	179.0	0.942	0.841	0.765	0.735	0.733	0.752	0.745	C•750	0.773	0.843	C.928	0.956	0.979	0.981
TN CONF MACH RN/L PT C 66 5 0.600 1.503 887 175.2	C X/DB Y/DP Z/CP MF/W	175.2 E.49 -C.01 -2.02 C.911	175.2 8.49 -0.01 -1.53 0.926	175.2 E.49 -C.C1 -1.C2 C.921	175.2 8.49 -0.01 -0.70 0.888	175.2 E.49 -0.01 -0.53 0.862	175.8 E.49 -C.Cl -O.36 C.844	175.8 8.49 -0.01 -0.19 C.828	175.8 8.49 -C.Cl -O.C2 C.859	175.8 8.49 -0.01 0.14 C.856	175.8 8.49 -0.01 0.32 0.854	175.8 E.49 -C.C1 0.47 C.873	175.8 8.49 -C.01 0.64 C.897	175.8 8.49 -C.Cl 0.98 C.953	175.E 8.49 -0.01 1.17 C.976	175.8 8.49 -0.01 1.48 0.978	175.8 8.49 -0.01 1.98 0.981	TN CONF MACH PN/L PT C	66 5 C.600 1.502 887 175.2	Q X/CB Y/DB Z/CB WF/M	175.2 8.49 -0.36 -2.02 C.984	175.2 8.49 -0.36 -1.52 0.982	175.2 8.49 -0.36 -1.03 C.970	175.2 8.49 -0.36 -0.70 C.917	175.2 8.49 -0.36 -0.52 0.875	175.2 8.49 -0.36 -0.36 0.857	175.2 8.49 -C.36 -O.17 C.856	175.2 8.49 -0.36/-0.02 C.868	175.2 8.49 -0.36 0.15 0.863	175.2 8.49 -C.36 0.32 0.867	175.8 8.49 -0.36 0.48 C.878	175.8 8.49 -0.36 0.65 0.918	175.8 8.49 -0.36 0.98 C.962	175.8 8.49 -0.36 1.18 0.976	175.8 8.49 -0.36 1.48 0.987	175.8 8.49 -0.36 1.98 C.989
RUN TST P 248 571 1	SEQ MACH	1 0.600]	2 0.600	3 0.600	4 0.600 1	5 0.600 1	6 0.602 1	7 0.602 1	8 0.602]	9 0.602]	10 0.602]	11 0.602 1	12 0.602]	13 0.602 1	14 0.602]	15 0.602]	16 0.602 1	RUN TST P	249 571 1	SEC MACH	1 0.600 1	2 0.600	3 0.600	4 0.600	5 0.600	6 0.600]	7 0.600	8 0.600 1	9 0.600	10 0.600	11 0.602 1	12 0.602	13 0.602 1	14 0.602 1	15 0.602]	16 0.602]

1.000 0.999 666.0 0.599 0.9999 0.9999 1.000 .005 .003 665.0 1.004 0.999 1.000 ..003 666.0 1.000 F00. .006 .003 1.001 .002 .005 pF/p 665.0 066 1.001 0.599 0.999 0.999 DF/1 õ ٠ -0.021 0.003 .019 -0.012 0.013 0.006 0.006 0.003 0.014 0.011 .011 0.002 -0-015 \sim -0.021 -0.010 0.002 4 5 0.025 0.021 0.002 0.007 -0.021 -0.021 -0.021 -0-01 -0.021 0.01 10. <u></u> 0 C 00 VA/V 0.000 0.000 000 000 000 0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 V A /V . ; • • •0 0.984 0.965 0.920 0.885 0.885 0.887 0.887 0.887 0.887 0.887 0.887 0.887 0.987 0.911 0.917 0.986 0.986 0.986 0.948 0.936 0.928 0.943 066 0.985 116 993 0.995 m 0.909 ŝ 0.949 F/V 0.996 0.931 0.980 VF/V 0.941 0.91 0.94 • • . > -20.00 04/9 ALPHA ALPHA -20.00 0A/Q 0.000 C.000 0.000 0.000 000.0 0.00.0 0.000 C• 000 0.00.0 0.000 C. 000 c.000 0.000 0.000 0.00.0 000.0 066.0 66.7 0F/9 0.974 0.972 0.930 0.840 0.774 0.777 0.777 0.777 0.777 0.777 0.753 0.819 0.819 0.819 0.923 0.923 0.968 0.969 0.969 0.969 65.1 QF/Q 0.991 0.898 0.874 0.832 0.859 0.824 0.887 0.864 0.883 0.979 0.961 986 C.899 0.392 0.941 T • 0.00.00 0.000 0000 0.000 0.000 0.000 0.000 000 694 Ma/m 000 79.4 1754 MF/W MA/W ٥. ۵. . 175.8 MF /N 0.955 0.982 0.985 0.985 6995 C•945 C•542 **C.915** C.878 O.872 O.891 O.905 525 0.878 870 930 s ω 3 ထ α) 0 Ø 0.963 0.879 0.912 0.984 C.983 955 0 0.948 16-0 C.928 0.901 94(C.94)12.0 C.98(66 56 ి . 0 3 ి 03 887 2708 -2.03 0 0.251 1.515 1875 (/CB Y/DE Z/DB -0.03 0.44 0.48 0.48 0.65 0.98 1.49 0.98 -0.69 -0.52 -2.05 -1.53 -1.04 -0.70 -0.54 -0.36 1.49 1.98 -0.22 0.63 0.12 0.29 0.47 79.0 1.16 •47 -1.52 -1.02 -0.18 РŢ -0.04 Ы σ RN/L 0.602 1.503 RN/L Y/DB -0.45 -0.45 -0.45 -0.45 -0.45 -0-45 C.41 -0-45 -0.45 -C • 45 .41 0.41 ŝ 0.41 0.41 0.41 0.41 41 ŝ 5 0.41 .41 •41 -0-45 -0-45 -0-45 -0.45 4. .4 . 4 4 • 4 4. 0.4 5 0 I \mathbf{c} O C \mathbf{O} 0 \mathbf{O} NACH NACH • 49 .49 X/TB C. 77 C. 83 C .49 ထတ ŝ CONF ŝ 175.2 75.4 778.8 779.4 779.4 778.8 778.8 778.8 778.8 778.8 80.1 80.1 8°.1 T N ľ 66 90 O Ó 571 I MACH ۵. ۵ ----TST F 571 1 MACH 0.600 0.600 0.602 0.600 0.249 0.250 0.600 TST 0.602 0.602 0.600 0.600 1264 22220 251 SFQ 2 50 2 50 5 F C 0 ŝ RUN 20450700 21

565-0 1.000 666.0 565.0 0.999 0.9999 0.9999 1.000 666 °0 666°0 666°0 665°0 1.000 0.599 666.0 .000 666.0 666 665 999 0/4 0.999 0.999 665.0 0.999 1.000 0.999 1.000 0 . . -0.010 -0.012 -0-021 -0.030 -0.012 -0-019 S C) -0.010 -0.030 -0.012 -0.012 -0.021 -0.017 -0.010 -0-014 -0.006 $\sim \sim$ 2 \$ 9 -0.001 -0.021 -0.021 -0.021 -0.021 00.00 -0.02 -0.01 -0-01 -0-01 -0-01 -0.02 -0-01 -0.01 8 8 0.000 0.000 0.000 0.000 0.000 0000 000 000 000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 V A /V 0 • • 0 • . • 0.927 0.66.0 0.980 0.983 0.991 VF/V 0.986 0.960 0.917 0.895 0.912 0.908 0.928 0.905 0.994 0.992 0.979 0.919 0.384 ŝ 0.922 0.928 3 0.937 VF/V 0.925 0.912 0.931 0.915 0.987 0.998 0.991 0.931 0.92 0.931 ALPHA -20.00 -20.00 ALPHA 0.000 0.00.0 QA/Q 000.0 000.0 0.000 0.000 0.00.0 000.0 0.00.0 C•000 0A/Q c. 000 0.000 0.000 0.000 0.000 0.000 0.00.0 0.000 0.000 c.000 c.000 0.000 0.000 0.000 0.000 000.0 c.000 0.000 0.00.0 0.000 0.000 63.5 GF/0 C.849 0.959 3.9 0.965 0.984 0.842 877 QF /0 0.859 C.857 0.981 876 0.972 0.920 0.852 0.838 0.829 0.799 0.829 0.822 0.864 0.930 m 0.979 0.958 0.866 0.836 0.778 0.854 0.859 0.974 0.995 0.981 0.988 0 0 6 0.000 0000.0 0.000 0.000 0.000 0000.0 0000.0 WA/W 0.000 000 000 0.00.0 0.00.0 M / M 0.00.0 • 000 1794 0.000 0.000 0.000 0.000 0.000 0.000 0.00.000 0.000 0.00.0 0.00.0 0000.0 0.000 0.000 00000 000. 0.000 1794 0.00.0 D č 0 ** 8 * 2 * 4 8 * / 4 8 Ó Ó 5.4 0.982 0.986 C.959 C.524 0.894 C•965 C.975 C.924 C.921 NH / N 122.0 .926 055 C.931 C.936 0.980 755 C.911 116.0 155 365 * 3 0.916 10.507 0:5:0 0.915 ω 0.882 0.927 1-98-U C.918 355.0 Ĵ . O 874 0.250 1.514 1874 (/CB Y/DB Z/DB 3.49 0.43 -2.03 Y/DP Z/CP -C.48 -2.05 -0.48 -1.53 -1.52 -1.03 0.29 0.46 -0.54 -0.37 -0.20 -0-45 -0-53 -0-35 -1.04 -0.04 0.63 .97 9 • 64 0.12 0.03 • 14 ÷ ω a) œ Р -0.19 5 • • .4 6. ** 35 *0 Ï, 40 00 -----5 0 - 2 - 5 2 1 - 5 1 - 5 1 - 5 1 - 5 1 - 5 2 - 5 2 1 - 5 1 0 0 \mathbf{O} PN/L RA JL 64. 0.43 0 • 4 3 0 • 4 3 0.43 -0.48 .48 .48 0.43 C. 43 0.43 C.43 -0.48 ω $\boldsymbol{\alpha}$ œ \mathbf{n} (m) m ~ 0.4 0.4 44 4. 4. 4 0.4 . о Т o 1 U I 0 1 O Ó NACH ļ VACH C•88 C•88 C•88 8.49 8.49 8.49 8.49 8.49 8.49 ビビン CCNF 78 • 8 78 • 8 78 • 8 78 • 8 78 • 1 78 • 1 78 • 1 78 • 1 78 • 1 4 4 5 5 78.1 1V 66 66 T N O O **Q** 571 1 p 0.249 0.249 0.249 0.249 MACH 249 249 249 249 248 249 248 248 248 571 . S ŝ 00 • • 1221 NONTOOF О 255 SEC nm 4m 50 10 12222 ω δ 5 16 S ω 0

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	bF∕0	0.999	0.9999	0.999	666*0	0.9999	665.0	0.9999	666*0	0.999	0.999	0.599	0.999	0.999	0° 595	1.000	1.000			bE/b	1.000	0.999	0.999	665.0	665.0	0.9999	0.9999	0.599	665.0	665°U	0.999	0.9999	1.000	0.998	665.0	0,099
	CD	-0.016	-0.014	-0.021	-0.012	120.0-	-0.012	-0.012	-0.021	-0.021	-0.021	-0.021	-0.012	-0.021	-0.017	-0.005	-0.010			٥Ĵ	-0.010	-0.015	-0.021	-0.012	-0.012	-0.021	-0.021	-0.023	-0.021	-0.012	-0.012	-0.012	-0.008	-0.039	-0.015	-0.014
	V / J / V	0.000	0.000	0.000	0* 0 00	0.000	0-000	0.000	0.000	0.000	0.000	0.000	0.000	0.009	0.000	0.000	0.000			V / V /	0.000	0.000	000.0	000.0	0.000	0.000	0.000	00000	0.000	0.000	000.0	0.000	0.000	0.000	0.000	00000
40	VF/V	0.935	0.942	0.941	0. 896	0.878	0.845	0.857	0.875	0.863	0.889	0.912	0.916	0.959	0.993	0.938	0.994	۵	0	VF/V	0.938	0.991	0.954	0.915	0.899	0.876	0.891	0.899	0.890	0.874	0.921	0.915	0.948	1.001	U. 996	0.995
ALPH	0A/0	0.000	0.000	c.000	0.000	0.00.0	0.000	0.000	C. UUO	0.000	0•000	0.000	0.000	0.000	0.000	0.00.0	0.000	ALPH	-20.0(0A/O	0.000	C. 000	0.000	0.000	0.000	0.000	c. 000	0.00.0	0.000	0.00.0	0.000	C. 000	0.000	C•000	0.000	0.000
11 63_3	0F/0	0.871	0.886	0.884	0.801	0.767	0.712	0.731	0.762	0.741	0.787	0.829	0.837	0.919	0.984	0.976	0.988	11	63.1	0F/0	0.975	199.0	0.908	0.836	0.806	0.764	C.790	0.806	0.789	0.761	0.846	0.836	0.898	1.000	166.0	0.989
d 1794	W/ 2W	0.000	0.00.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0	0	8 1794	MA/M	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0
34	MF /N	0.934	0.942	C.941	0.895	C. 876	0.844	0.855	C. E73	0.861	C.888	C.911	C.915	C.955	256.0	935.0	6.554	ى	78.	NF/N	C.988	156*0	0.554	0.914	0.898	C.875	0.885	0.898	0.385	0.873	C.920	C.914	C•948	1.001	956.0	0.955
L PT	Z/08	-2.03	-1.52	-1.01	-0.10	-0.53	-0.36	-0.19	-0.02	0.14	0.30	0.48	ŋ.65	10.97	1.18	1.48	1.95	L pT	6 1874	Z/DB	-2.02	-1.52	-1.03	-0.69	-0.52	-0.35	-0.19	-0.03	0.14	0.31	0.48	0.65	0.58	1.17	1.48	1.58
A H PV/	Y/DE	-0.01	10.0-	-0.01	-0.01	10.0-	-0.01	-0.01	-0.01	-0.01	-0.01	-0-01	-0.01	-0.01	-0.01	-0.01	10-0-	H RN	0 1.51	Y/DR	-0.36	-0.36	-0.36	-0.36	-0.36	-0-36	-0-36	-0-36	-0-36	-0.36	-0-36	-0.36	-0-36	-0-36	-0.36	-0-36
F NAC	X/08	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	F NAC	5 0.25	X/CB	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8-49
TA CCN	ge	78.1	77.4	78.1	78.8	78.1	78.8	78.8	78.1	78.8	78.8	78.8	79.4	79.4	79.4	79.4	78.8	TN CCN	66	0	78.8	78.8	78.1	4.61	78.8	78.8	78.8	78.8	79.4	79.4	79.4	4.67	4.97	77.4	78.8	78.8
TST P	MACH	3.249	0.248	3.249	0.250	3.249	0.250	0.250	0.249	0.250	0.250	0.250	0.252	0.252	0.252	0.252	3.250	TST P	571 1	MACH	0.250	0.250	0.249	0.252	0.250	0.250	0.250	3.250	0.252	0.252	0.252	0.251	3.251	0.248	2+250	3.250
RUN	S H C	-	2 (3) *	5	9	2	8	6	10 (11 (12 (13 (14 (15 (16 (RUN	257	SEG	1	2	m	4	ى د	0	2	υ Ω	6	10	11 (12 (13 (14 (15 (16 (

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571 166 5 0.245 TSL 1794 62.9 -20.00 0.991 0.007 PF/P 0.249 78.1 8.49 -0.45 -1.52 0.557 0.000 0.990 0.000 0.990 0.000 0.999 0.000	z	TST P	TN CCN	VH NA(CH RN	L PI	U L		٩	11	ALPHA				
MACH C X/CB Y/DB Z/CP VF/W MA/M GF/O GA/Q VF/V VA/V CP PF/P 0.2249 78.1 8.49 -C.45 -1.52 C.955 0.000 0.994 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.999 0.0999 0.0999 0.999		571 1	66	5.0	49 1.51	C 18	74 78	.1 17	94	62.9	-20.00	_			
0.249 78.1 8.49 -C.45 -2.03 C.55C 0.000 0.991 0.000 0.990 0.000 -0.001 1.000 0.256 78.8 8.49 -C.45 -1.52 C.59C 0.000 0.928 0.000 0.964 0.000 -0.021 0.999 0.256 78.8 8.49 -C.45 -0.70 C.894 0.000 C.779 0.000 0.881 0.007 -0.021 0.999 0.256 78.8 8.49 -C.45 -0.70 C.887 0.000 0.773 0.000 0.881 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.36 C.887 0.000 0.773 0.000 0.881 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.36 C.887 0.000 0.773 0.000 0.919 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.15 0.889 0.000 0.841 C.000 0.919 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.15 0.889 0.000 0.789 C.000 0.919 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.15 0.888 0.000 0.789 C.000 0.929 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.789 C.000 0.929 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.789 C.000 0.929 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.789 C.000 0.929 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.789 C.000 0.929 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 0.509 0.999 0.000 0.975 0.000 0.928 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 0.48 C.928 0.000 0.975 0.000 0.928 0.000 0.973 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 0.45 0.48 C.928 0.000 0.975 0.000 0.993 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 0.45 0.491 0.975 0.000 0.993 0.000 0.973 0.000 -0.021 0.993 0.249 78.1 8.49 -C.45 0.45 0.491 0.975 0.000 0.993 0.000 0.973 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 0.45 0.400 0.976 0.000 0.974 0.000 0.994 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 0.45 0.000 0.975 0.000 0.943 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 0.45 0.400 0.975 0.000 0.944 0.000 0.914 1.000 0.244 78.1 8.49 -C.45 0.914 0.976 0.000 0.945 0.000 0.914 1.074 0.004 0.954 242.3 10.88 0.41 -1.04 0.941 0.946 0.000 0.945 0.000 0.914 1.071		MACH	0	X/08	Y/08	10/2	AN S	N N	W/1	0F/0	04/0	VF/V	V A /V	c b	pF/p
0.249 78.1 8.49 -0.45 -1.52 C.990 0.979 C.000 0.990 0.000 -0.909 0.000 0.999 0.000 0.999 0.000 0.999 0.000 0.994 0.000 -0.021 0.999 0.299 0.200 0.894 0.000 -0.021 0.999 0.299 0.249 78.1 8.49 -0.45 -0.52 0.894 0.000 0.773 0.000 0.881 0.007 -0.021 0.999 0.299 0.2249 78.1 8.49 -0.45 -0.36 C.887 0.000 0.773 0.000 0.885 0.000 -0.919 0.000 -0.929 0.999 0.2249 78.1 8.49 -0.45 -0.19 0.918 0.000 0.919 0.000 -0.929 0.909 0.249 78.1 8.49 -0.45 -0.19 0.918 0.000 0.885 0.000 0.919 0.000 -0.929 0.999 0.249 78.1 8.49 -0.45 -0.19 0.918 0.000 0.789 0.000 0.919 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.11 0.928 0.000 0.789 0.000 0.919 0.000 -0.021 0.999 0.2249 78.1 8.49 -0.45 0.11 0.928 0.000 0.789 0.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.11 0.928 0.000 0.789 0.000 0.929 0.000 -0.021 0.999 0.299 0.200 0.249 78.1 8.49 -0.45 0.12 0.928 0.000 0.789 0.000 0.929 0.000 -0.021 0.999 0.299 0.200 0.249 78.1 8.49 -0.45 0.12 0.999 0.000 0.789 0.000 0.929 0.000 -0.021 0.999 0.299 0.200 0.249 78.1 8.49 -0.45 0.48 0.979 0.000 0.929 0.000 0.929 0.000 -0.021 0.999 0.299 0.200 0.249 78.1 8.49 -0.45 0.48 0.979 0.000 0.928 0.000 0.978 0.000 0.928 0.000 1.979 0.000 0.928 0.000 0.978 0.000 0.928 0.000 0.970 0.000 0.978 0.000 0.978 0.000 0.928 0.000 0.928 0.000 0.928 0.000 0.978 0.000 0.928 0.000 0.978 0.000 0.928 0.000 0.928 0.000 0.928 0.000 0.928 0.000 0.928 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.948 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.978 0.000 0.000 1.000 0.949 0.000 0.000 1.000 0.000 1.000 1.000 0.000 1.000 0.948 0.000 0.000 1.000 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.000 0.000 0.000		0.249	78.1	8.49	-0.45	-2.03	3 0* 55	0.0	002	0.581	0.000	0.990	000.000	-0.007	1.000
0.250 78.8 8.49 -C.45 -1.03 C.954 0.000 0.984 0.0021 0.999 0.249 78.1 8.49 -C.45 -0.879 0.000 0.884 0.0021 0.999 0.249 78.1 8.49 -C.45 -0.52 C.887 0.000 0.814 0.000 0.815 0.000 0.999 0.999 0.249 78.1 8.49 -C.45 -0.35 C.887 0.000 0.842 C.0001 0.999 0.999 0.249 78.1 8.49 -C.45 -0.15 C.818 0.000 0.842 C.0001 0.919 0.999 0.249 78.1 8.49 -C.45 -0.15 C.918 0.000 0.841 C.000 0.918 0.907 0.999 0.249 78.1 8.49 -C.45 0.15 C.928 0.000 0.929 0.000 0.918 0.999 0.000 0.999 0.999 0.000 0.929 0.001 0.999 0.999 0.000 0.918 0.999 0.000 0.918 0.999		0.249	78.1	8.49	-0-45	-1.52	2 C• 59	C 0.0	000	0.979	c.000	066.0	0.000	-0.010	1.000
0.2250 78.8 8.49 -C.45 -0.70 C.894 0.000 0.896 0.000 0.891 0.000 0.999 0.2249 78.1 8.49 -C.45 -0.52 0.879 0.000 0.811 0.000 0.999 0.2249 78.1 8.49 -C.45 -0.36 C.887 0.000 0.841 0.000 0.919 0.000 0.999 0.2249 78.1 8.49 -C.45 -0.15 C.818 0.000 0.841 0.000 0.919 0.000 0.999 0.2249 78.1 8.49 -C.45 0.31 C.928 0.000 0.841 0.000 0.999 0.000 0.999		0.250	78.8	8.49	-C.45	-1.03	3 0.96	4 0.0	000	0.928	0.000	0.964	0.000	-0.021	0.999
0.249 78.1 8.49 -C.45 -0.52 0.879 0.000 0.381 0.007 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.36 C.887 0.000 C.385 0.0021 0.999 0.250 78.1 8.49 -C.45 -0.36 C.887 0.000 0.841 C.000 0.919 0.070 -0.999 0.250 78.1 8.49 -C.45 -0.15 0.518 0.000 0.841 C.000 0.919 0.070 -999 0.249 78.1 8.49 -C.45 0.15 0.588 0.000 0.841 C.0021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.913 0.001 0.999 0.249 78.1 8.49 -C.45 0.48 C.921 0.996 0.001 0.993 0.001 0.993 0.001 0.999 0.249 78.1 8.49 -C.45 0.48 C.973 0.090 0.913 0.001 0.995 0.001 0.995 0.001 <td></td> <td>0.250</td> <td>78.8</td> <td>8.49</td> <td>-0-45</td> <td>-0-7(</td> <td>0 C.85</td> <td>4 0.0</td> <td>000</td> <td>0.799</td> <td>000.0</td> <td>0.896</td> <td>0.000</td> <td>-0.021</td> <td>0.999</td>		0.250	78.8	8.49	-0-45	-0-7(0 C.85	4 0.0	000	0.799	000.0	0.896	0.000	-0.021	0.999
0.249 78.1 8.49 -C.45 -0.36 C.883 0.000 C.780 C.000 0.885 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.19 0.918 0.000 0.847 C.000 0.919 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 -0.15 C.988 0.000 0.789 C.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.31 C.928 0.000 0.789 C.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.31 C.928 0.000 0.861 0.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.31 C.928 0.000 0.879 0.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 0.31 C.928 0.000 0.973 0.000 0.929 0.000 -0.021 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.973 0.000 0.928 0.000 1.0999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.928 0.000 1.0993 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.977 0.000 0.945 0.000 1.0003 1.000 0.249 78.1 8.49 -0.45 1.28 C.988 0.000 0.977 0.000 0.945 0.000 1.0003 1.000 0.249 78.1 8.49 -0.45 1.48 C.982 0.000 0.977 0.000 0.945 0.000 1.0003 1.000 0.249 78.1 8.49 -0.45 1.28 C.988 0.000 0.977 0.000 0.945 0.000 7.0003 1.000 0.249 78.1 8.49 -0.45 1.28 C.988 0.000 0.977 0.000 0.945 0.000 7.0003 1.000 0.249 78.1 8.49 -0.45 1.28 C.988 0.000 0.977 0.000 0.945 0.000 7.000 7.0003 1.000 0.244 78.1 8.49 -0.45 1.28 C.988 0.000 0.977 0.000 0.945 0.000 7.000 7.000 0.945 0.000 7.000 0.945 0.000 0.945 0.000 0.945 0.000 0.945 0.000 0.945 0.000 0.945 0.000 0.945 0.000 0.946 0.000 0.945 0.000 0.946 0.000 0.946 0.000 0.937 1.007 0.034 2.42.3 10.88 0.41 -1.034 0.946 0.000 0.946 0.000 0.946 0.000 0.00		0.249	78.1	8.49	-0.45	-0.52	2 0.87	9 0.0	000	0.773	0.000	0.881	0.000	-0.021	0.999
0.249 78.1 8.49 -C.45 -0.19 0.918 0.000 0.841 C.000 0.918 0.000 -0.021 0.999 0.250 78.8 8.49 -C.45 -0.02 C.518 0.000 0.841 C.000 0.918 0.000 -0.021 0.999 0.249 78.1 8.49 -C.45 0.31 C.928 0.000 0.789 C.000 0.929 0.000 -0.021 0.999 0.256 78.8 8.49 -C.45 0.31 C.925 0.000 0.929 0.000 -0.021 0.999 0.256 78.1 8.49 -C.45 0.31 C.925 0.000 0.973 0.000 -0.929 0.000 -0.999 0.249 78.1 8.49 -C.45 0.50 0.939 0.000 0.975 0.000 0.938 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 0.58 0.939 0.000 0.975 0.000 0.938 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 1.18 0.988 0.000 0.975 0.000 0.938 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 1.18 0.988 0.000 0.975 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.48 C.985 0.000 0.976 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.48 C.982 0.000 0.976 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.48 C.982 0.000 0.976 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.48 C.982 0.000 0.976 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.58 C.988 0.000 0.976 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.58 C.988 0.000 0.977 0.000 0.938 0.000 700 700 700 0.249 78.1 8.49 -C.45 1.58 C.988 0.000 0.977 0.000 0.938 0.000 1.0008 0.249 78.1 8.49 -C.45 1.98 C.988 0.000 0.977 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -C.45 1.98 C.988 0.000 0.977 0.000 0.945 0.000 0.945 0.000 0.945 0.000 0.941 1.000		0.249	78.1	8.49	-0-45	-0-36	5 C.88	0.0	000	C. 780	c. 000	0.385	0.000	-0.021	0.999
0.250 78.8 8.49 -C.45 -0.C2 C.518 0.000 0.841 C.000 0.918 U.0C0 -0.021 0.999 0.249 78.1 8.49 -C.45 0.15 C.888 0.000 0.789 C.000 0.929 0.0C0 -0.021 0.999 0.250 78.8 8.49 -0.45 0.31 C.928 0.000 0.861 0.000 0.929 0.0C0 -0.021 0.999 0.249 78.1 8.49 -0.45 0.48 C.577 0.000 0.861 0.000 0.928 0.0C0 -0.021 0.999 0.249 78.1 8.49 -0.45 0.65 0.939 0.000 0.973 0.0C0 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.973 0.0C0 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.939 0.0C0 -0.017 0.999 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.977 0.000 0.938 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.988 0.000 0.977 0.000 0.935 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.977 0.000 0.938 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.988 0.000 0.977 0.000 0.935 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.988 0.000 0.977 0.000 0.935 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.988 0.000 0.977 0.000 0.938 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.989 0.000 0.977 0.000 0.938 0.0C0 -0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.989 0.000 0.977 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.989 0.000 0.977 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.989 0.000 0.977 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.98 C.989 0.000 0.977 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.04 682 241.2 381 66.2 10.00 0.976 0.0976 0.975 0.000 0.976 0.076 0.074 1.0026 0.954 242.3 10.88 0.41 -1.04 C.964 0.975 0.995 0.0976 0.074 1.0026		0.249	78.1	8.49	-0.45	-0.1	9 0.91	8 0°0	000	3.842	c.000	0.919	0.000	-0.021	0.999
0.249 78.1 8.49 -0.45 0.15 0.888 0.000 0.789 0.000 0.929 0.000 -0.021 0.999 0.250 78.8 8.49 -0.45 0.31 0.928 0.000 0.928 0.000 -0.021 0.999 0.250 78.1 8.49 -0.45 0.48 0.577 0.090 0.928 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 0.65 0.939 0.000 0.978 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.973 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.975 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.975 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.975 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.975 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.976 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.588 0.000 0.976 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.588 0.000 0.976 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.588 0.000 0.976 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.588 0.000 0.976 0.000 0.948 0.000 1.000 0.249 78.1 8.49 -0.45 1.58 0.41 -0.500 0.976 0.000 0.948 0.000 0.976 0.000 1.000 0.954 242.3 10.88 0.41 -1.53 0.964 0.976 0.972 0.972 0.974 0.974 0.974 0.974		0-250	78.8	8.49	-0.45	-0.02	2 C.51	0°0 8	000	0.841	0.000	0.918	0.000	-0.021	0.999
0.249 78.1 8.49 -0.45 0.31 C.928 0.000 0.861 0.000 0.929 0.000 -0.021 0.999 0.250 78.8 8.49 -0.45 0.48 C.577 0.000 0.980 0.000 0.928 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 0.65 0.939 0.000 0.973 0.000 0.973 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.945 0.000 1.000 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.988 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.945 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.975 0.000 0.988 0.000 0.937 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.988 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.937 0.000 7.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.998 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.938 0.000 0.001 1.000 0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 0.000 0.938 0.000 0.001 1.000		0.249	78.1	8.49	-0.45	0.14	5 0.88	8 0.0	000	0.789	0.00.0	0.890	0.000	-0.021	0.999
0.250 78.8 8.49 -0.45 0.48 C.57 0.000 0.859 C.000 0.928 0.000 -0.071 0.999 0.249 78.1 8.49 -0.45 0.65 0.939 0.000 0.880 C.000 0.939 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.938 0.000 -0.008 1.000 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.938 0.000 -0.001 1.000 0.249 78.1 8.49 -0.45 1.48 C.985 0.000 0.975 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.985 0.000 0.975 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.989 0.000 0.975 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.976 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.989 0.000 0.976 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.989 0.000 0.976 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.989 0.000 0.977 0.000 0.938 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 C.988 0.000 0.976 0.093 0.000 1.000 0.951 1.66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH 0 X/CB Y/CB Z/DB MF/W MA/M 07/0 0.46 0.976 0.976 0.954 242.3 10.88 0.41 -1.53 C.967 0.959 0.0976 0.037 1.026 0.954 2422.3 10.88 0.41 -1.04 C.964 0.949 0.959		0.249	78.1	8.49	-0.45	0.31	1 C.92	8 0.0	000	0.861	0.000	0.929	0.000	-0-021	9,999
0.249 78.1 8.49 -0.45 0.65 0.939 0.000 0.880 0.000 0.939 0.000 -0.017 0.999 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.938 0.000 -0.008 1.000 0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.988 0.000 -0.003 1.000 0.249 78.1 8.49 -0.45 1.48 0.988 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.989 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.985 0.000 0.976 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.985 0.000 0.976 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.985 0.000 0.976 0.988 0.000 0.937 1.000 0.249 78.1 8.49 -0.45 1.480 682 241.2 381 66.2 10.00 MACH 0 X/UB Y/UB Z/DB MF/M 0F/0 0.966 0.976 0.976 0.037 1.026 0.951 241.2 10.88 0.41 -1.53 0.967 0.959 0.976 0.976 0.037 1.026 0.954 242.3 10.88 0.41 -1.04 0.964 0.971 0.959 0.976 0.976 0.037 1.026		0.250	78.8	8.49	-0.45	0.48	5.52 B	7 0.0	000	0.859	C.000	0.928	0.000	-0.021	0.999
0.249 78.1 8.49 -C.45 C.98 C.973 0.000 C.945 C.000 0.973 0.000 -0.017 0.999 0.249 78.1 8.49 -C.45 1.18 0.988 0.000 0.975 0.000 0.988 0.000 -0.003 1.000 0.249 78.1 8.49 -C.45 1.48 C.985 0.000 0.975 0.000 0.988 0.000 -0.001 1.000 0.249 78.1 8.49 -C.45 1.98 C.989 0.000 0.975 C.000 0.988 0.007 0.001 1.000 0.249 78.1 8.49 -C.45 1.98 C.589 0.000 0.975 C.000 0.988 0.007 0.001 1.000 0.249 78.1 8.49 -C.45 1.98 C.589 0.000 0.975 C.000 0.988 0.007 -0.003 1.000 0.249 78.1 8.49 -C.45 1.98 C.589 0.000 0.975 C.000 0.988 0.007 -0.003 1.000 0.249 78.1 8.49 -C.45 1.98 C.589 0.000 0.975 C.000 0.988 0.007 0.001 1.000 0.951 1 66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH 0 X/CB Y/CB Z/DB MF/W MA/M 0F/O 0A/Q VF/V VA/V CP 0.037 1.026 0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.976 0.037 1.026		0.249	78.1	8.49	-0.45	0.65	5 0.93	0.0 2	100	0.880	0.00.0	0.939	0.000	-0.012	0.599
0.249 78.1 8.49 -0.45 1.18 0.988 0.000 0.975 0.000 0.988 0.000 -0.008 1.000 0.249 78.1 8.49 -0.45 1.48 0.985 0.000 0.970 0.000 0.985 0.000 1.000 0.249 78.1 8.49 -0.45 1.48 0.985 0.000 0.975 0.000 0.988 0.000 1.000 0.249 78.1 8.49 -0.45 1.98 0.589 0.000 0.975 0.000 0.988 0.000 1.000 757 F Th CCNF MACH Ph/L PT G P TT ALPHA 571 1 66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH Q X/DB Y/DB MF/M MA/M 0F/0 0A/Q VF/V VA/V CP PF/P 0.951 241.2 10.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.954 242.3 10.88 0.41 -1.53 0.967 0.959 0.972 0.972 0.0141 1.076		0.249	78.1	8.49	-0.45	36 0	8 C.97	0.0	000	0.945	0.000	0.973	0.000	-0.017	0.999
0.249 78.1 8.49 -C.45 1.48 C.985 0.000 0.970 0.000 0.935 0.000 -0.003 1.000 0.249 78.1 8.49 -C.45 1.98 C.588 0.000 0.975 C.000 0.988 0.000 1.000 1.000 TST F Th CCNF MACH Ph/L PT C P TT ALPHA 571 1 66 5 C.951 1.480 682 241.2 381 66.2 10.00 MACH 0 X/CB Y/CB Z/DB MF/W MA/M 0F/0 0A/Q VF/V VA/V CP PF/P 0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.037 1.026 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.037 1.026		0.249	78.1	8.49	-0-45	1.18	3 0.98	0.0 8	000	0.975	0.000	0.988	0.000	-0-008	1.000
0.249 78.1 8.49 -0.45 1.58 C.589 0.000 0.975 C.000 0.988 0.000 1.000 TST P Th CCNF MACH Ph/L PT C P TT ALPHA 571 1 66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH Q X/CB Y/C9 2.708 MF/W MA/M 0F/0 0A/Q VF/V VA/V CP PF/P 0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.037 1.026 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.037 1.026		0.249	78.1	8.49	-0.45	1.48	8 C.98	5 0.0	000	0.970	0.000	0.935	0.000	-0.003	1.000
TST F Th CCNF MACH Ph/L PT C P TT ALPHA 571 1 66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH Q X/DB Y/DB Z/DB MF/W MA/M 0F/O 0A/Q VF/V VA/V CP PF/P 0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.037 1.026 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.072 0.034 1.021 0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.969 0.972		0.249	78.1	8.49	-0.45	1•9(8 C. 58	8 0°C	300	0.975	c. 000	0.988	0.000	0.001	1.000
TST F Th CCNF MACH Ph/L PT G FT ALPHA 571 1 66 5 0.951 1.480 682 241.2 381 66.2 10.00 MACH 0 X/CB Y/CB Z/DB MF/W 0A/M 0F/O 0A/Q VF/V VA/V CP PF/P MACH 0 X/CB Y/CB Z/DB MF/W 0A/M 0F/O 0A/Q VF/V CP PF/P 0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.071 0264 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.041 1.026 0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.969 0.0344 1.021															
571 I 66 5 0.951 I.480 682 241.2 381 66.2 10.00 MACH Q X/CB Y/CB Z/DB MF/N MA/M QF/O 0A/Q VF/V VA/V CP PF/P 0.951 241.2 IC.88 0.41 -2.04 0.971 0.966 0.976 0.976 0.037 I.C24 0.954 242.3 IC.88 C.41 -1.53 C.967 0.959 0.972 0.041 I.026 0.954 242.3 IC.88 0.41 -1.04 C.964 0.949 0.969 0.0372		TST P	TN CCN	VE NA	CH PN	L P	0		a.	11	ALPHA	_			
MACH Q X/CB Y/CB Z/DB MF/W MA/M QF/O QA/Q VF/V VA/V CP PF/P 0.951 241.2 1C.88 0.41 -2.04 0.971 0.956 0.976 0.037 1.024 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.041 1.026 0.954 242.3 1C.88 0.41 -1.53 C.967 0.959 0.972 0.041 1.026 0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.959 0.0349 0.0134 1.071		571 1	66	5 0.95	51 1.48	30 68	82 241	•~ 3	181	66.2	10.00	_			
0.951 241.2 1C.88 0.41 -2.04 0.971 0.966 0.976 0.037 1.C24 0.954 242.3 1C.88 C.41 -1.53 C.967 0.959 0.972 0.972 0.041 1.026 0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.969 0.969 0.034 1.021		MACH	o	X/DB	Y/09	Z / DE	3 MF/	N NA	W/	0F/0	0 A / O	VF/V	V 4 / V	د ن	br/b
0.954 242.3 1C.88 C.41 -1.53 C.967 0.959 0.972 0.041 1.026 0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.969 0.034 1.021		0.951	241.2	10.88	0.41	-2.04	4 0.97	1	~	0.966		0.976		0.037	1.024
0.954 242.3 1C.88 0.41 -1.04 C.964 0.949 0.969 0.969 0.034 1.021		0.954	242.3	1C.83	0.41	-1.55	3 C.96	7		0.959		0.972		0.041	1.026
		0.954	242.3	1C.88	0-41	-1.02	4 C.96	4	-	0.949		0.969		0-034	1-021

.

		pr/p	7 1.024	1.026	1.021	3 1.015	1.015	1.009	1.007	1.006	7 1.005	5 1.003	665.0 5	100.1	5 1.003	3 1.005	5 1.016	3 1. C31
		د م	0-03	0.041	0.034	0.023	0.024	0.014	0.011	0.010	0.00	00.00	-0.002	0.001	0.005	00.0	0.025	0.048
		V 4 / V																
		VF/V	0.976	0.972	0.969	0.930	0.938	0.938	0.929	0.921	0.909	0.892	0.902	0.883	0.400	0.931	0.960	0.972
ALPHA	10.00	0A/0																
1 L	66.2	0F/0	0.966	0.959	0.949	0.856	0.873	0.868	0.849	0.831	0.805	0.769	0.785	0.751	0.786	0.851	C.923	0.964
۵.	381	M / M																
0	241.2	MF /N	176.0	C.967	C.964	516.0	C.927	C.928	0.918	C.905	C. 895	C.876	C.887	0.866	C • 8 8 5	0.920	0.953	C.967
Ld	682	Z/08	2.04	1.53	1.04	0.70	0.54	16.0	0.20	0.04	0.13	0.25	0.46	0.63	0.96	1.17	1.47	1.96
D/Nd	1.480	K/DB	0.41 -	0.41 -	- 14.0	0.41 -	- 14-0	0.41 -	C.41 -	0.41 -	0.41	14.0	0.41	0.41	0.41	0.41	0.41	14.0
MACH	0.951	(/ CB	. 88	. 83	.88	. 88		. 83	.88	.88	. 88	.88	. 88	. 88	. 88	. 88	. 88	. 88
CONF	u n	×	2 10	10	3 10	В 10	8 10	3 10	10	3 10	3 10	3 10	8 IC	8 1C	.8 1C	8 1C	.8 IC	2 10
D TV	1 66	C	241.	242.	242.	242.	242.	242.	242.	242.	242.	242.	241.	241.	241.	241.	241.	241.
TST	571	MACH	0.951	0.954	0.954	0.956	0.956	0.955	0.955	0.955	0.955	0.955	0.953	0.953	0.953	0.953	0.953	0.951
5	56	С Ш	2	m	4	ŝ	φ	~~	ω	σ	10	11	12	13	14	5	16	17

		DF/D	1.027	1.024	020.1	210-1	1.009	1-006	1.003	1.003	1.002	1.000	0.999	1.003	1.010	1.019	1.029			pF/p	1.024	1.020	1.014	1.010	1.007	1.005	1.003	1.00.1	1.000	792.0	666.0	1.001	1.001	1.006	1.020	1.035
		<u>د</u>	0.042	150.0		0.017	0-014	0.009	0.004	0.004	0.003	-0.000	-0.002	0.005	0.016	0-030	0.047			d C	0.037	0.031	0.022	0.016	0.012	0.008	0.005	0.002	100.0-	-0.005	-0.002	0.002	0.002	0.010	0.031	0.055
		V A /V																		V A /V																
HA	00	Q VF/V	0.904	0.936	076-0	016-03	0.885	0.884	0.876	0.871	0.360	0.874	0.857	0.880	0.903	0.939	0.974	НА	00	Q VF/V	0.969	0.974	0.969	0.939	0.918	0.903	0.901	0.891	0.893	0.388	0.878	0.885	0.900	0.923	0.949	0.961
ALP	10.	OA/																٩LP	10.	0A/																
TT	61.3	QF/Q	0.815	0.857	ACA 0	0_798	0.760	0.756	0.739	0.729	0.709	0.732	C.701	0.746	0.798	0.880	0.967	TT	68.0	0F70	0.950	0.959	0.941	0.872	0.826	0.794	0.738	0.766	0.769	0.756	0.739	0.755	0.784	0.834	0.902	0.942
0	382	M A / M																۵	383	N/VH																
د	242.5	N / J N	0,036	C.017	C.00.7	0.889	C.868	C.867	0.858	C.852	0.841	0.856	C.838	0.363	0.885	0.929	0.969	ى	242.4	MF /N	C.963	C.970	C.964	0.925	0.906	C. 389	0.887	0.875	0.877	0.871	0.860	0.868	0.885	0.910	C.941	0.954
L PT	5 686	2012		1.04	02.0-	-0.54	-0-38	-0.20	-0-04	0.13	0.30	0.46	0.63	0.96	I.16	1. 46	1.96	L pT	0 685	2/08	-2.04	-1.54	-1.04	-0.71	-0-54	-0.37	-0.21	-0.03	0.12	0.30	0.46	0.63	0.97	1.17	1.46	1.97
H PN	2 1 - 4 8					-0-03	-0-03	£0.0-	-0.03	-0-03	-0.03	-0-03	-0.03	-0.03	-0.03	-0-03	-0-03	H RNJ	1 1.48	Y/DB	-0-38	-0.38	-0.38	-0.38	-0-38	-0.38	-0.38	-0-38	-0.38	-0-38	-C.38	-C.38	-0.38	-0-38	-0.38	-C•38
AF VAC	5 6 4 9 5	N 00			10.88	10.88	10.88	10.88	10.88	10.88	10.88	1C.88	1 C.88	10.88	1 C • 88	10.88	I C. 88	F NAC	56.03	X/CR	1C.88	10.88	1C.88	1 C • 88 ·	1C.88	10.88	1C.88	10.89	10.88	10.88	10.83	1 C . 88	10.88	1 C • 88	1C.88	1C.88
TN CC	0 0 0		242.5	242.4	242.4	242.4	241.5	241.9	241.5	241.5	241.9	241.9	241.5	241.5	241.5	241.1	241.1	TN CCN	66	C	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	242.4	241.9	241.4	241.C
TST P			0.051	156-0	126-0	0.951	0.950	0.950	0-950	0.950	0.950	0.950	0.948	0.948	0.948	0.946	0.946	TST P	571 1	MACH	0.951	0.951	0.951	0.951	0.951	0.951	0.951	0.951	2 156.0	0.951	0.951	0.951	0.951	0.950	0.949	. 1947
RUN		39 = L: />	- 0	1 60	4	ŝ	ç	7	ω	თ	10	11	12	-	14	15	16	RUN	261	C L S	H	2	m	4	ŝ	Ş	2	æ	6	10	11	12	1	14	15	16

	A/V CP PF/P	0.036 1.023	0.035 1.022	0.025 1.016	0.019 1.012	0.015 1.010	0.008 1.005	0.004 1.003	0.000 1.000	-0.002 0.599	-0.003 0.998	0.005 1.003	0.007 1.004	0.012 1.008	0.017 1.011	0.028 1.018	0.050 1.032			A/V CP PF/P	0.032 1.020	0.030 1.019	0.023 1.015	0.015 1.012	0.008 1.005	0.011 1.007	0.007 1.005	0.002 1.001	-0.003 0.598	-0.010 0.993	-0.012 0.992	-0.021 0.987	-0.020 0.587	-0.006 0.596	0.012 1.007	0.044 1.627
AL PHA 10-00	QA/Q VE/V V	0.973	0.974	0.969	0.927	0.922	0.923	0.918	0.906	0.905	0.883	0.881	0.880	0.902	0.922	0.957	0.971	ALPHA	10.00	QA/Q VE/V V	176.0	0.977	0.971	0.924	0.938	0.936	0.925	0.910	0.836	0.874	0.870	0.878	0.926	0.959	0.973	0.974
71 C 383 68-6	MA/N CF/Q	0-960	0.960	C.944	0.848	0.837	0.334	0.822	0.795	0.792	0.749	0.748	0.747	0.794	0.836	0.918	0.962	LL d	382 69.4	MA/N OF/O	0.967	0.964	0*646	0.841	0.866	0.863	0.838	0-803	0.754	0.729	- C.720	0.730	0.826	0.902	0.944	0.965
CNF MACH PN/L PT C 5 0.951 1.478 685 242.4	X/08 Y/08 Z/08 MF/W	10.88 -0.48 -2.04 0.969	10.88 -C.48 -1.55 C.969	1C.88 -C.48 -1.04 C.964	IC.88 -C.48 -0.71 0.915	IC.88 -C.48 -0.54 C.9IC	I0.88 -C.48 -0.37 C.911	1C.88 -C.48 -O.21 C.9C5	10.88 -C.48 -0.04 0.852	1C.88 -C.48 0.13 C.890	IC+88 -C+48 0+29 0+866	1C.88 -0.48 0.47 0.864	1C.88 -C.48 0.64 0.862	10-88 -C.48 0.56 C.888	IC.88 -0.48 I.17 0.909	IC.88 -C.48 1.46 C.950	10.88 -0.48 1.97 C.966	NF WACH RN/L PT G	5 0.952 1.474 684 242.3	X/CB Y/CP Z/DB WF/W	E.49 0.43 -2.03 C.973	E.49 C.43 -1.52 C.972	E.49 0.43 -1.03 C.966	E.49 0.43 -0.68 C.912	8.49 0.43 -0.52 0.928	8.49 0.43 -0.35 0.926	8.49 C.43 -0.15 C.913	8.49 0.43 -0.03 0.896	8.49 C.43 O.14 O.869	8.49 C.43 O.31 C.856	8.49 0.43 0.48 C.852	8.49 0.43 0.64 C.86C	8.49 0.43 0.98 C.914	8.49 C.43 1.17 C.952	8.49 C.43 1.47 C.968	8.49 0.43 1.95 0.969
RUN TST P TN CC 262 571 1 66	SEG MACH O	1 0.951 242.4	2 0.953 242.5	3 0.952 242.3	4 0.954 242.5	5 0.953 242.3	6 0.953 242.3	7 0.953 242.3	8 0.955 242.8	9 0.955 242.8	10 0.955 242.8	11 0.953 242.3	12 0.955 243.4	13 0.953 242.9	14 0.951 242.4	15 0.950 242.4	16 0.949 242.C	RUN TST P TN CC	263 571 1 66	SEC MACH C	1 0.952 242.3	2 0.952 242.3	3 0.952 242.3	4 0.952 242.3	5 0.951 241.8	6 0.951 241.E	7 0.950 241.8	8 0.949 241.4	9 0.950 241.9	10 0.948 241.5	11 0.949 242.C	12 0.948 242.0	13 0.947 241.6	14 0.946 241.1	15 0.946 241.1	16 0.946 241.1

		CP DE/P	0.025 1.016	0-025 1-016	0.016 1.010	0.006 1.004	-0-01 1-000	465 U 600 U-	-0-015 0.990	-0-016 0-590	-0-019 0.988	-0-030 0-981	-0.022 0.586	-0-019 0.588	-0.008 0.995	0.008 1.005	0-024 1-015	0.050 1.031				CD DE/D	0.025 1.016	0.026 1.017	0.014 1.009	0.005 1.003	-0-000 1.000	-0-004 0-997	-0.004 0.597	-0.018 0.989	-0.021 0.987	0.014 0.991	-0-019 0-988	0.016 0.990	466 0 010 0.994	0.005 1.003	0.025 1.016	0.045 1.028
РНА	• 00	19 VE/V VA/V	0.907	0.938	0.934	0.925	- 606-0	0.893	0.870	0.854	0.857	0.050	0.820	0.847	0.487	0.923	0.965	0.972			00	U VE/V VA/V	0.972	0.978	0.977	0.948	0.925	- 106.0	- 068.0	0.877 -	0.857 -	0.840 -	0.848	0.863	- 606-0	0.945	0.969	0.976
D IT AL	385 69.6 10	MA/W QF/0 QA	0.810	0.874	0.861	C. 338	0.800	0.766	0.718	0.683	0.691	0.676	0.625	0.674	0.754	0.834	0.935	0.954	D TT AL			14/ 41/9 0A	166.0	0.964	C•956	0.886	0.834	0.782	0.761	0.130	0.692	0.663	0.676	0.705	0.796	0.878	0.943	0.972
WACH RN/L PT C	U+951 1+482 538 243.5	K/UB Y/UB Z/UB MF/W	8.49 - C. CI - 2.02 C. 893	8+49 -0.01 -1.54 C.927	3.49 -0.01 -1.02 0.923	3.49 -0.01 -0.65 C.914	3-49 -0.01 -0.52 0.895	3.49 -C.C1 -O.36 C.877	3.49 -0.01 -0.19 C.851	3.49 -0.CI -0.Cl 0.833	3.49 -C.CI 0.14 C.837	3.49 -0.01 0.31 C.830	3.49 -0.01 0.47 0.756	3.49 -0.01 0.65 C.826	9.49 -C.01 0.58 C.87C	3.49 -C.Cl 1.18 C.911	:.49 -0.01 1.48 0.959	3.49 -0.01 1.98 C.967	WACH RN/L PT C	0-951 1 480 488 242 E						443 TU-35 -0.454 (-940							-49 -U-30 U-48 U-827	•49 -U.56 U.65 U.844		•49 -0.36 I.I8 0.936	• 49 - 10 - 50 I - 48 U - 963	•43 -C.36 I.48 C.972
RUN TST P TN CCNF			1 0.951 243.5	2 0.951 243.5 8	3 0.951 243.5 8	4 0.952 244.C E	5 0.952 244.C 8	6 0.952 244.C 8	7 0.952 244.0 8	8 0.952 244.C 8	9 0.951 243.5 8	10 0.951 243.5 8	11 0.952 244.0 8	12 0.952 244.C 8	13 0.952 244.C 8	14 0.952 244.0 8	15 0.949 243.C 8	16 0.948 242.6 E	RUN TST P IN CONF	265 571 1 66 5	SEQ MACH Q X	1 0.951 243.5 8	2 0.952 243.5 8	3 0.957 243.5	4 0-954 244-C	5 0.954 244. C	6 0.954 244 C	7 0-954 244 C	8 0.952 243 5 P	9 0.952 243.5	10 0.952 243.5 8	11 0.952 243.5				15 0-950 243+0 84		
		۵	-	+ α) (> -	+ α	•	~ C	α	ົທ	<u>م</u> ،		~ r r	σ	. 4	0			a	_	• •	4	0	0	~	4	N	.+	*	•	~	Ċ,	ŝ	-	~	
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		/ Jd	1-02	10.1	10.1	00-1	00.4		00,00	00.00	0, 58	0.98	0.080	0.080	0.99	0.59	10.1	1.03			DF/	1.03	1.02	1.02	1.02(1.01(1.00	1.00	1.002	1.00	1.00	1.002	1.00	1.00	1.01	1.02	1.02	
		цЪ	0-033	0.078	0.020	0.010		-0-004	100-00-	-0-015		-0.074	400-01	-0.071	-0-011	100-0-	0.073	0.047			C D	0-054	0.048	0.042	0.035	0.018	0.005	0.008	0.003	0.007	0.007	0.004	0.012	0.016	0.026	0.038	0.041	
		VAVV																			V A /V																	
A	0	VF/V	0.976	0.978	0.976	0.942	0.918	0.919	106-0	0.889	0.875	0.861	0.863	0-864	0.919	0.954	0.971	0.975	4		VEIV	0.929	0.932	0.923	0.898	0.898	0.889	0.877	0.878	0.865	0.872	0.872	0.877	0.899	0.917	0.957	0.973	
ALPH	10.0	Q A Q																	ALPH	10.00	04/0																	
11	70.1	QF /Q	0.965	0.965	0.956	0.875	0.821	0.819	0.782	0.754	0.725	0.697	0.699	0.705	0.816	0.895	0.947	179.0	11	70.3	QF/0	0.871	0.873	0.853	0.798	0.790	0.766	0.744	0.744	0.723	0.735	0.733	0.746	161.0	0.832	0.924	0.959	
۵	385	N/VW																	٩	415	M / M																	
U	243.0	NE / N	0.972	C.974	0.972	0.932	0.906	0.906	0.886	0.872	C.857	0.841	0.843	0.845	0.906	0.946	0.966	179.0	G	235.5	MF / N	0.919	C-922	0.913	0.885	3.884	0.874	0.861	2.862	C.848	3.856	3.85 5	C.861	0.885	0.906	.951	3668	
۲d	688	/08	• 03	- 52	E0.	.69	.52	•35	.19	.02	.14	•31	• 48	• •	9 6 .	•18	47	76.	рŢ	703	/08	• 04	• 52	• 04	.71 (• 54 (• 30 •	.21	• 04	.13	• 29 (.46 (.63	.96	.17	•46 (.97 (
SN/L	479	2 80	+5 -2	1- 55	1- 51	15 -0	15 -0	15 -0	15 -0	15 -0	12	0	5	5	5	15	1 51	5	J/N	482	8 2	3 -2	1- 6	1- 6	01	0 m	01	9	0	0	0	0	0	0	~		-	
5	49 I.	1/2	-0-	-0-1	0-0-	0	0-0-	-0-	0-0-1	-0-	-0-	-0-	0-	-0-1	-0-	-0-	-0-1	-0-	H H U	01 1.	7/1	0.01	0•0-	0•0-	0.0-	0.01	0.0	0.0	0-0-	0.01	0-0-	-0 -0 -	0.0-	0.0	0.0	0.0-	0.0	
F VA	5 0.9	X/CB	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	F NA(5 0.9(X/LB	10.88	1 C. 88	l C • 88	10.87	I C - 88	1C.88	10.83	l C. 88	10.88	l C - 88	1 C • 8 8	10.88	LC. 88	10.88	l C • 88	lC.88	
N CCN	S	•	3•C	3.0	۲. ۳.	un •	۲. ۳.	ມ ອີ	۹. ۳.	0.	••0		0.	u، •	م	u \ •	0.5	.	CCN			6.0	K n	• •	•	2	Q	0	4N •	5	U.	5	4	4	0	5	•	
1	1 6	-	3 24	24	24	24	24	24	24	247	241	241	24	24	24	24	243	243	P T	1 66	Ç	235	235	234	234	23	235	236	235	235	235	235	236	236	236	236	236	
TST	571	MACF	0.945	0.94	0.951	0.951	0.951	0.951	0.951	0.952	0.952	0.952	0.952	0.951	0.951	0.951	0.950	0.950	TST	571	MACH	0.901	0.900	0.897	0.857	0.898	0.899	006.0	006.0	106.0	0.901	106.0	206.0	206.0	0.900	0.900	0.900	
RUN	266	SEQ	-	~	m i	4	ŝ	ų.	~	œ	6	10	11	12	13	14	5 	16	NDa	267	SEC	-	2	m	4	in i	01	-	ω i	6			12	<u> </u>	14	4 T	16	

	pr/p	1.032	1.033	1.021	1.020	1.012	1.008	1.C04	0.994	0.996	0.595	0.998	799.0	0.999	1.006	1.015	1.022				DE/D	1.024	1.020	1.015	1.012	1.013	1.C09	1.007	1.006	1.005	1.004	1.006	1.008	1.010	1.010	
	a C	0.057	0.058	0.038	0.036	0.021	0.014	0.007	-0.011	-0.007	-0.008	-0.004	-0.005	-0.001	0.011	0.025	0.038				d C D	0.048	0*0*0	0.030	0.024	0.025	0.017	0.014	0.012	0.010	0.008	0.012	0.015	0.021	0.019	
	V A / V	•																			V A / V															
ALPHA	04/0 VF/V	0.917	0.922	0.932	0.900	0.883	0.870	0.855	0.850	0.836	0.816	0.637	0.845	916	0.932	0.969	0.975		ALPHA	10.00	0A/Q VF/V	0.914	0.928	0.925	0.903	0.885	0.878	0.871	0.365	0 - 868	0.872	0.859	0.370	0.912	0.941	
11	0F/0	0.847	C.858	0.869	0.802	0.763	0.734	0.704	0.687	0.664	0.628	0.667	0.681	0.813	0.857	0.943	0.963	ł	11	70.0	0F/0	0.835	0.861	0.851	0.803	0.769	0.753	0.739	0.726	0.732	0.738	0.716	0.737	0.821	0.880	1
a	× 1 4 1 4	•																(0	452	N V N															
0 0 0 0 0	N - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	C. 9C6	116.0	0.923	C. 886	0.868	C.854	0.838	C.832	C.816	0.795	C.818	0.827	0.902	0.923	C. 964	C.971		U	230.1	NF / N	C.9C3	C.918	C.916	168.0	C.872	C.864	C.856	C.85C	C.853	0.858	C.844	C. 855	C.9C1	C-934	
L pT	2/DB	-2.03	-1.53	-1.02	-0.69	-0.52	-0.36	-0.19	-0.02	0.15	0.31	0.48	0.64	85.0	1.18	L.48	1.98		Lol	9 727	Z/08	-2.04	-1.55	-1.04	-0.71	-0-53	-0-38	-0.20	-0.03	0.13	0.29	0.46	0.63	95*0	1-16	-
H RN/	2 I.48 7/DP	-0.01	-0-01	-0.01	-0.01	-0.01	-0.01	10.0-	-0.01	-0-01	-0.01	-0.01	10.2-	-0.01	-0.01	-0.01	-0.01		NA H	3 1.49	Y/DB	-0.03	-0.03	-0.03	-0-03	-0.03	-0.03	-0.03	-0.03	-0-03	-0.03	-0.03	-0-03	-0.03	-0-03)
F NAC	0.60 c X/CB	8.49	8.49	8.49	8.49	8.49	8.49	8.49	£• 49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49		E VAC	5 0.85	X/CR	10.88	10.88	10.88	1C.88	10.88	10.83	10.88	10.88	10.88	10.88	1C.88	1C.88	10.88	10.88	
TN CON	000	235.8	235.0	234.6	234.7	234.7	234.7	234.8	235.2	236.1	236.1	235.6	236.0	235.9	235.5	235.C	235.0		TN CCN	66	c	230.1	229.8	229.8	229.4	229.4	229.1	229.1	229.1	229.1	229.1	229.1	229.1	228.6	228.6	
TST P	MACH	0.902	0.899	0.897	0.897	0.897	0.897	0.896	0.898	006-0	006.0	0.899	0.900	0.901	006.0	0.899	0.899		TST P	571 1	MACH	0.853	0.852	0.852	0.850	0.850	0.849	0.845	0.849	0.849	0.845	0.849	0.849	0.848	0.845	
RUN	SFO	, 	2	m	4	U I	9	7	œ	ς,	10	11	12	13	14	15	16		NDA	269	SEQ		2	m	4	ŝ	9	٢	œ	6	10	11	12	5	14	•

1.015 1.018 1.018 1.007 965.0 1.004 166.0 0.994 0.998 0.998 1.006 1.009 1.015 F/D 1.017 pr/p -0-008 0.035 0.037 0.036 0.020 0.014 0.008 0.012 0.018 0.029 0.034 0.028 -0.005 -0-011 -0.004 0.038 3 9 V A /V V A /V 0.918 0.924 0.922 0.893 0.874 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.857 0.972 0.972 0.972 0.979 VF/V VF/V 10.00 ALPHA 10.00 ALPHA 0 A / 0 QA/U 70.0 0F/0 0.851 0.847 0.788 0.747 0.747 0.747 0.721 0.701 0.704 C.657 C.657 C.6580 C.717 C.6580 C.6580 C.6580 C.6580 C.6571 C.657 0.836 69.7 0130 0.969 MA / M 495 M / M 451 2 C 230.5 MF/N 223.5 NF / N C.912 C.88C C.88C C.866 C.846 C.876 C.876 C.815 0.9C8 0.914 C.813 0.826 0.950 C.968 0.977 613 ω C.848 ē 2/08 -2.02 -1.03 -0.19 0.14 0.32 0.48 0.98 -0.53 0.64 1.17 1.48 1.58 -0.02 h VACH PN/L C.854 1.500 X/DB Y/DP Z 1/Nd 0.803 1.519 -0.01 Y/DB 0.41 -0-01 -0-01 -C.C1 -0.01 -0-01 -0.01 -0.01 10.01 10.01 -0.01 -0.01 -0.01 0.0-NACE X/FB 8.49 8.49 8.49 8.49 8.49 .49 • 49 49. 8.49 • 49 • 49 •49 •49 •49 • 49 ω αu æ ∞ ∞ ထေ ω œ L. CONF w 229.8 229.8 229.8 Mage
 <l 0.852 0.803 852 0.852 0 NE469FB60HNB RUN 270 SEC 12 9

1.009 1.010 1.012 .003 1.005 1.014 .003 .002 • 004 .003 001 .011 .010 10. ٠ 0.023 0.025 0.025 0.020 0.006 0.010 0.009 0.003 0.006 0.023 0.016 0.030 0.004 0.023 0.927 0.930 0.931 0.926 0.926 0.983 0.908 0.895 0.913 0.907 0.940 179.0 0.955 0.976 .980 0.975 0.854 0.857 0.857 0.853 0.853 0.853 0.853 0.853 0.853 0.810 0.818 0.818 0.959 0.876 0.957 0.912 0.976 0.980 0.974 C.923 C.919 C.922 C.918 0.858 0.884 c.9c3 c.896 0.933 0.896 0.950 579.0 16 19 757 2 Z/DP 5 1 -1.54 (1 -1.54 (: -0.72 0.13 -0.04 • 63 .47 -0.21 0.47 .97 .16 -0.37 σ ٠, 0 0.41 C.41 0.41 0.41 C.41 0.41 .41 0.41 C.41 C.41 0.41 0.4 0.4] 0.4] X (1)
< The Find Content of the Content of t 223 5 223 5 222.5 0.801 0.801 0.801 0.801 0.801 0.801 0.801 0.801 0.801 0.801 0.802 300 0.802 0.802 0.800 01204 271 SEC 2 m + 10 0 m 00 0 NNa 10

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	DE /	1.01	1.01	1.00	1.00	1.00	1.00	0.95	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.01	1.01			010	1.00	1.01	1.00	1.01	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0(1.00	5
		0.031	0.025	0.013	0.013	0.006	-0.001	-0.003	0.003	0.003	0.009	0.010	0.010	0.014	0.012	0.023	0.032			ن د	0.021	0.022	0.017	0.025	0.014	0.009	0.006	0.001	0.003	£00°0	0.016	0.010	0.020	0.018	C C C
	VA/V																			V / V V															
PHA	.00 /0 VF/V	0.908	0.922	0.929	0.911	0.902	0.386	0.883	0.865	0.874	0.879	0.878	0.876	0.919	0.945	0.909	0.981	VIQ	00	VE/V	0.987	0.983	0.973	0.920	0.6.0	0.892	0.892	0.839	0.871	0.386	0.888	0.399	0.923	0.949	
TT AL	54.6 IU 2F/0 0A	818	.842	.853	.817	797.	. 763	.757.	.725	. 742	.753	.752	.749	.834	. 385	.942	179.	11 11	69.3 10	CF/O OA	.980	179.	.948	.840	795	.778	.778	.771	.736	. 765	.770	-792	.855	.897	
n (154 N/Vñ	0	ō	õ	0	ō	o	c	c	0	0	0	0	0	0	0	C	0	498	WA/W	Û	0	0	Ű	0	0	0	0	0	0	C	C	0	0	•
ں ب رب ر	1 • 2 2 Z U	0.858	0.913	C.921	0.901	C.891	C.874	0.871	0.851	C.861	0.866	C.865	0.863	016.0	0.935	c.966	0.578	c	222.0	NF / N	0.985	0.980	C.970	116.0	0.889	0.880	0.881	C.878	0.957	C.874	0.876	0.888	C.920	0.943	
L PT	101 01	-2.04	-1.54	-1.04	-0.71	-0-55	-0.37	-0.20	-0.04	0.14	0.29	0.46	0.63	0.96	1.17	1.47	1.97	10 11	16 757	2/08	-2.04	-1.54	-1.04	-0.71	-0.54	-0.37	-0.21	-0-04	0.13	0.29	0.47	0.63	16.0	1.16	1
NA HU	8477 8477	-0.03	-0-03	-0.03	-0.03	-0-03	10.03	-0.03	-0.03	-0.03	-0-03	-0.03	-0-03	-0-03	-0.03	-0.03	-0-03	n a	98 1.5	Y/DB	-0.38	-0-38	-0.38	-0.38	-0.38	-0.38	-C.38	-0-38	-0.38	-0-38	-0-38	-0.38	-0-38	-0-38	
NF VA	8.0 C	IC.88	10.88	1C.88	1C.88	10.88	IC.88	1 C. 88	1C.88	1C.88	1C.88	10.88	1 C.88	1C•88	1C-33	10.88	1C.88	NE	5 0.7	X/08	10.88	10.88	10.88	I C - 83	1C.88	1C.88	1C.88	1C.88	1C.88	10.88	1 C. 88	1C.88	1C.88	1C•88	000
DU VI d	1 66 0	222.5	222.6	222.5	222.5	222.5	223.0	223.C	223. C	223.C	223.0	223.0	222.5	222.5	222.5	223.C	222.4		1 66	C	222.0	222 C	222 • C	222.5	222.5	222.5	222.5	222.5	222.5	223.0	223.0	223.0	223.0	222.5	
TST	MACH	0.800	0.799	0.800	0.800	0.800	0.801	0.801	0.801	0.801	0.802	0.802	0.800	C. 800	0.800	0.802	0.801	TCT	571	MACH	0.758	0.759	0.799	0.800	0.800	0.800	0.800	0.800	0.800	0.801	0.801	0.801	0.801	C.8C0	
NUN NUN	212	, "	2	m	4	ŝ	9	2	æ	σ	10	11	12	13	14	15	16	NIId	273	SEQ	-	2	m	4	۲U	9	-	œ		10	11	12	13	14	

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1.014 1.012 .009 1.005 1.005 1.005 1.001 1.005 .001 1.003 1.002 1.003 •000 1.002 • 004 1.010 • 00 5 1.005 1.009 1.C09 PF/P .004 1.000 1.007 1.003 1-004 1.004 1.010 1.012 1.014 1.009 0.999 1.01/ 0.010 0.006 110.0 0.006 0.010 0.011 0.004 600*0 0.015 0.032 0.028 0.020 0.020 0-020 0.023 0.023 0.026 0.020 0.016 0.001 600.0 0.012 0.004 0.020 0.011 -0.003 0.008 0.031 ۵ ن ĉ V A /V V A /V 0.967 0.903 0.397 0.836 VF/V 0.894 0.889 VF/V 0.975 0.933 0.876 0.842 0.386 0.939 0.954 0.954 0.941 0.983 0.925 0.908 0.936 **0.982** 0.930 0.913 0.892 0.979 0.982 0.894 0.956 981 0.987 0.927 0.901 0.936 10.00 0A/0 10.00 QA/Q **NLPHA ALPHA** 0F/0 0.974 0.844 0.810 0.799 0.786 0.859 0.913 0.958 0.854 0.854 0.856 0.848 0.815 0.815 0.815 0.759 0.751 0.759 0.759 0.903 **1.**69 0.773 0.766 0.782 0.796 0.972 C.936 C.781 0.956 579.0 0.980 C.980 0F/0 69.I 0.924 0.963 р 498 МД/М 154 M / M ۵ 19 758 222.6 2/08 wr 5 0.800 1.518 757 222.5 X/CB Y/CP 2/CB MF/W 0.979 C. 981 C.898 0.892 0.963 C.886 C.883 C.883 C.877 0.874 0.883 c.890 C.92E 0.972 C.986 C.985 0.980 C.922 0.925 0.919 C.903 C.870 C.874 C.917 0.859 C.957 0.976 516.0 0.880 C.864 0.948 0.979 0.29 1.17 -0.54 -0.38 -0.21 0.13 0.63 0.96 C-88 -C-48 -2-04 -0.48 -1.54 . 47 1.97 -1-04 -0.71 -0-04 0.43 -2.03 -1.52 -1.03 -0-10 -0.52 -0.19 0.14 0.48 F 0.64 0.98 1.47 1.58 -0-35 0.31 U١ -0.01 1.1 F WACH RN/L 5 0.799 1.519 TST P TN CCNF MACH RN/L 0.43 0.43 C.43 0.43 -0-48 Y/JB -0.48 -0.48 -C.48 -C.48 -0-48 -C.48 0.43 -C.4P -0.48 -C.48 -C.48 α 0.43 0.43 C.43 C.43 -0-45 -0-48 -0.48 444 0.4 X/CB 1 C. 88 1 C. 88 10.88 1C.88 1C.88 1C.88 1C.88 1C.88 1C.88 1C.88 IC.88 L C • 88 **C.** 88 8 49 8 49 8 49 8 49 1C.88 C.83 8.49 8.49 8.49 8.49 8.49 8.49 £.49 8.49 8.49 8.49 8.49 E.49 E TN CCNF C 222.6 222.6 222.5 222.5 222.5 222.5 222.5 223.0 223.0 223•0 223•0 223•0 223. C 223.0 223.5 223.0 223. Ċ 571 1 66 LL. 571 1 MACH 667.0 0.800 0.798 0•799 0•800 0.801 0.801 0.800 0.800 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.758 MACH C.8CO 0.801 0.801 0.801 0.801 0.802 0.801 0.800 0•799 0•799 0.801 0.801 0.801 0.801 661 • 8 UN 2 7 4 5 F C 2 m 2 50 ω Ø 212 275 SEC C 4 m 2 R UN NMANO ~ ω δ 2 1313 5 4 2

	CP PF/P 0.029 1.013	0.028 1.013	0.024 1.011	0.015 1.007	0.006 1.003	0.004 1.002	0.009 1.004	0.003 1.001	265 0 200 0	0.006 0.597	0.003 0.999	0.001 1.001	0.012 1.005	0.016 1.007	0.025 1.011	0.034 1.015			Co belo	0.029 1.013	0.030 1.013	0.013 1.006	0.008 1.003	0.000 1.000	0.006 1.003	0.006 0.597	0.006 0.997	0.005 0.998	0.009 0.996	0.004 1.002	0.009 1.004	0-013 1-006	シンシャイ トインマン
ALPHA 10.00	0A/Q VF/V VA/V 0.900	0.915	0.924	0 03	0.877	0.864	0.847	0.839	0.853	0.847	0.854 -1	0.863	0.924	0.953	0.979	0.981	ALPHA	10-00	DA/D VF/V VA/V	0.982	0.979	0.976	0.926	0.897 -	0.872	0.858	0.861	0.867	0.852 -	0.861	0.885	0.942	
453 69.2	A/M 0F/0	0.830	0.848	C.803	0.748	0.724	0.696	0.679	0.700	0.691	0.704	0.722	0.842	0.904	0.963	0.972	11	494 69.1	A/N CF/O	126-0	0.965	0.952	0.846	0.785	0.739	0.710	0.716	0.727	0.698	0.718	0.764	0.879	
F WACH RN/L PT C 5 0.802 1.513 754 222.3	X/DB Y/DB Z/DP MF/W 1 8.49 -0.01 -2.02 C.850	8.49 -0.01 -1.52 C.9C6	8.49 -0.01 -1.03 0.916	8.49 -0.01 -0.69 C.853	E.49 -C.01 -O.53 C.864	E-49 -C.C1 -0.36 C.850	8.49 -0.01 -0.19 0.833	8.49 -C.CI -O.O2 C.824	8.49 -0.01 0.14 0.838	E.49 -0.01 0.31 C.832	E.49 -C.C1 0.47 C.835	8.49 -0.01 0.65 C.849	8.49 -0.01 0.97 0.915	8.49 -0.01 1.18 C.947	E.49 -C.01 I.4E C.976	E.49 -C.Cl 1.98 0.978	VF WACH RN/L PT Q	5 0.801 1.512 754 221.8	X/08 Y/08 Z/08 VE/V	8.49 -0.36 -2.02 0.979	8.490.36 -1.52 C.976	8.49 -C.36 -I.C2 C.973	E.49 -0.36 -0.69 0.918	E.49 -C.36 -0.51 0.885	8-49 -0.36 -0.36 0.855	8.49 -C.36 -O.18 C.844	8.49 -C.36 -O.C3 C.847	8.49 -0.36 0.14 0.854	8.49 -C.36 0.32 C.837	8.49 -0.36 0.48 0.847	E.49 -C.26 0.64 0.873	E.49 -C.36 0.95 C.935	
N TST P TN CCN 6 571 1 66	C MACH Q 1 0-8C2 222-3	2 0.801 221.8	3 0.801 221.E	4 0.801 221.8	5 0.801 221.8	6 0.801 221.8	7 C.8C1 221.E	8 0.860 221.2	9 0.800 221.2	0 C.800 221.2	.1 0.800 221.2	.2 C.8C0 221.2	3 0.800 221.2	4 0.800 221.2	5 0.800 221.2	6 0.800 221.2	UN TST P TN CCN	17 571 1 66	C HACH D	1 0.801 221.8	2 0.801 221.6	3 0.801 221.6	4 0.802 222.3	5 0.802 222.3	6 0.804 222.8	7 0.301 221.8	8 0.8015,221.8	9 0.804 222.8	10 0.804 222.8	.1 0.804 222.8	.2 0.802 222.3	3 0.802 222.3	

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		CP DF/P	0-034 1-015	0.025 1.011	0.020 1.009	0.013 1.006	0.006 1.003	0.001 1.001	-0-000 1-000	-0-002 0-566 -0-002 0-566	-0-006 0-997	-0-006 0.997	0.006 1.003	0-005 1-002	0-016 1-007	0.019 1.009	0-026 1-012	0.031 1.014				0 033 1 000		0.028 1 0.07	0.015 1.004	0-010 1-003	0.009 1.002	0.010 1.003	0.008 1.002	0.012 1.003	0.008 1.002	0.016 1.004	0.006 1.001	0.017 1.004	0.028 1.007	0.019 1.005	0.029 1.007
		F/V V1/V	940	985	116	92 <i>5</i>	900	894	878	862 -	368	870	834	392	950	967	981	981			E/V VA/V		000 0 H D	96.7	93.7	934	923	1.66	116	900	913	905	918	934	950	186	616
ALPHA	10.00	DA/Q V	•0	•0	•0	•	•0	•0	•0	•0	0	.0	•0	0	•0	•0	•	•0	AH PHA	10.00	04/0						0	0	•0	0.	0	0	•0	0	0	0	0
T T	69.1	0r /0	0.969	779.0	0.957	0.844	0.793	0.781	0.748	0.719	0.729	0.732	0.761	0.778	0.897	0.935	0.968	0.972	11	67.8	0F/0	0.965	049.0	0.937	0.874	0.867	0.846	0.861	0.822	0.801	0.825	0.812	C•834	0.868	206.0	0.963	C.964
٩	464	N V N																	0	703	M / M																
U	3 221.3	MF / N	179.0	C.983	0.974	C.916	0.889	C.883	0.865	0.949	0.855	0.857	0.871	0.881	C.944	C.963	0.978	0.979	ى	176.0	NL /N	C.978	0.981	0.965	C.933	0.930	516.0	C.927	0.906	C.854	0.908	C • 899	0.913	0.930	0.946	0.979	0.578
Lbl	0 753	27.08	-2.03	-1.52	-1.03	-0.69	-0.52	-0-35	-0.18	-0.07	0.14	0.30	0.48	0.65	0.98	1.18	1.44	1.99	L PT	8 896	Z/CB	-2.04	-1.54	-1.04	-0.71	-0.54	-0.38	-0.20	-0.04	0.13	0.29	0.46	0.63	0.96	1.17	1.46	1.97
Ч И И И И И	0 1.51	Y/5B	-0.45	-0.45	-0-45	-0.45	-0-45	-0.45	-0.45	-0-45	-0.45	-C.45	-0.45	-0.45	-0.45	-0.45	-0-45	-0.45	H PN	8 1.5C	Y/CB	0.41	0.41	0.41	C.41	0.41	0.41	0.41	0.41	0.41	0.41	14.0	14.0	0.41	C.41	0.41	0.41
	5 0.80	X/CB	8.49	8.49	8.49	8.49	64.9	8.49 -	- 64° -	64.9	E. 49 .	- 64.3	E.49 -	E.49 -	8.49	E.49 -	- 64.3	6 49 -	F NACI	5 0.59	X/ER	1 C. 88	10.88	1C.88	1C.88	1 C. 88	1 C. 88	10.88	10.88	10.83	I C. 88	10.88	1C.38	1C.88	10.88	10.88	I C • 88
	. 66	C	221.3	221.3	221.3	221.8	221.5	221.6	222.3	222.3	222.3	222.3	222.3	222.3	222.3	222.8	222.3	222.3	The CEN	66	ۍ ا	176.C	176.0	176.C	176.0	176.C	176.€	176.C	176.C	176.6	1/6.5	1/6.6	1/6.0	1/0.5	1/0.5		111.2
151	271]	MACH	C. 800	0.800	0.800	0.801	0.801	0.801	0.803	0.303	0.803	0.803	0.803	0.803	0.303	0.804	0.802	0.802	1 IST	571 1	MACH	0.558	0.598	0.558	0.598	0.598	0.559	0.598	0.558	0.559	0. 7 44 7 7 7 0	2.5.2.2. 2.2.2.0 2.2.2.0		0. 5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -		010.0
RUN	278			n :	ς ·	4 1	ŝ	Q	2	œ	5	10	11	12	13	14	۲ ^۰	16	PUN	579	SFR		2	6 1	4	in '	91	- (ω (ר ה ה	2.			C 1	t u 	0 7 1	с Т

	Co pE/b	0.009 1.007	0.008 1.002	0.019 1.005	0.000 1.000	0.016 1.004	0.015 1.004	0.017 1.004	0.008 1.002	0.004 1.001	0.015 1.004	0.011 1.003	0.019 1.005	0.019 1.005	0.020 1.005	0.036 1.009			1	CP Pr/p	0.028 1.007	0.014 1.004	0.024 1.006	0.012 1.003	0.008 1.002	0.015 1.004	0.008 1.002	0.026 1.007	0.012 1.003	0.027 1.007	0.007 1.002	0.008 1.002	0.007 1.002	0.004 1.001	0.029 1.007	0.032 1.008
АЦРНА 10-00	04/0 VF/V VA/V 0.919	0.935	0.934	206 *0	0.907	0.882	0.876	0.880	0.889	0.899	0.887	0.897	0.917	0.950	0.970	0.974				VA/U VE/V VA/V	0.931	0.985	0.945	0.919	0.910	0.885	0.893	0.871	0.892	0.888	0.396	0.903	0.938	0.952	0.975	0.931
P TT 703 67.2	MA/N 0F/0 C.840	0.868	0.866	0.816	0.812	U. 758	807 °D	0. 705	081.0	861.0	111.0	0.196	0.836	0.00.0	0.941	0.954	P 11	702 44 9				1/6.0	168-0	0.858	0.819	0.13	181.0		0.186	287.0	261.0	U•815	0+873	106.0	0.954	0.967
JE WACH RN/L PT C 5 C+600 1-516 896 177-2	10.88 -0.03 -2.04 C.913	IC-88 -0.03 -1.55 C.930	10.88 -0.03 -0.71 0 001	1C-88 -C.C3 -0.54 C.901	10.88 -0.03 -0.37 0.876	1C-88 -C-03 -0.21 C-840			1C-88 -C-C3 0.30 0.803	1C-88 -0.03 0.46 r por						10+00 -0+07 I+36 C+315	F WACH RN/L PT C	5 0.599 1.514 896 176.6	X/CB Y/D8 Z/CB MF/N	LC.88 -0.38 -2.04 0.979	LC-88 -C-38 -1-54 C.564		10-88 -0.38 -0.71 C 012													KIK IN DE T ON IN ON ON
PUN TST PTN CCA 280 571 1 66 SFC MACH O	1 0.600 177.2	3 0.599 176.6	4 0.602 177.8	5 0.6C2 177.8	6 0.6C3 178.4	7 0.602 177.8	8 0.602 177.8	9 0.602 177.8	10 0.602 177.8	11 0.602 177.8	12 0.602 177.8	13 0.603 178.4	14 0.602 177.8	15 0.603 178.4	16 0-603 178.4		KUN TST P TN CCNI	281 571 1 66	SEC MACH Q	1 0-559 176.6 1	2 0.602 177.8 1	3 0.602 177.8 1	4 0.6C1 177.2 1	5 0.602 177.8	6 0-6C1 177-2 1	7 0.602 177.8 1	8 0.602 177.8 1	9 0.603 178.4 1	10 0.503 178.4 1	11 0.603 178.4 1	12 0.602 177.8 1	13 0.601 177.2 1	14 0.601 177.2 1	15 0.602 177.8 1	16 0.602 177.8 1	

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		/ CP PF/P	0.051 1.013	0.035 1.009	0.026 1.007	0.022 1.005	0.013 1.003	0.009 1.002	0.010 1.003	0.007 1.002	0.007 1.002	0.007 1.002	0.005 1.001	0.004 1.001	0.022 1.005	0.023 1.006	0.033 1.008	0.016 1.004			/ Co bt/b	0.019 1.005	0.022 1.005	0.009 1.002	0.011 1.003	0.004 1.001	0.002 1.001	0.006 1.001	-0.004 0.999	-0.015 0.996	865.0 600.0-	0.003 1.001	-0.004 0.999	-0.004 9.599	0.009 1.002	0.019 1.005	0.021 1.005
ALPHA	10.00	DA/Q VF/V VA/V	0.970	0.976	0.962	0.914	0.906	0.904	0.901	0.888	0.905	0.894	106-0	0.914	0.930	0.949	0•969	0.988	ALPHA	10.00	DA/D VF/V VA/V	0.936	0.984	0.977	0.929	0.928	0.919	0.909	0.910	0.906	0.899	0.897	0.910	0.960	0.977	0.980	0.982
P 11	696 66.1	MA/M QF/Q	0.949	C.957	0.927	0.831	0.812	0.808	0.804	617.0	0.810	0.790	0.803	0.826	0.861	006 0	0.942	0.979	b II	703 68.1	WA/N GE/O	0.975	179.0	0.953	0.858	0.854	0.835	0.816	0.816	0.808	0.795	0.793	0.816	0.916	0.953	0.963	0.967
U	1 177.7	NF / N	C. 968	C.974	C.96C	506.0	006.0	0.858	0.895	0.882	0.855	0.888	0.895 0	0.908	C.925	0.946	0.967	C.987	Q	6 176.6	MF / N	C.985	0.983	C.975	0.925	C.924	C.914	0.903	0.904	006-0	C.893	0.890	0.904	C.957	616.0	0.979	C.981
PN/L PT	1.517 89	/CB Z/DB	.48 -2.04	.48 -1.54	•48 -I.04	.48 -0.70	.48 -0.53	.48 -0.37	.48 -0.20	.48 -0.05	.48 0.12	.48 0.29	.48 0.47	.48 0.63	.48 0.96	.48 1.17	.48 1.48	•48 1. 96	RN/L PT	1.509 89	/D9 Z/CB	.43 -2.03	•43 -1•53	.43 -1.03	.43 -0.69	.43 -0.53	.43 -0.35	.43 -0.19	.43 -0.02	.43 0.14	.43 0.31	.43 0.48	.43 0.65	.43 0.98	.43 1.18	.43 I.48	.43 1.95
NF NACH	5 0.604	X/08 Y	1C.87 -C	1C.87 -0	1C-88 -0	1C.88 -C	10.83 -0	10.88 -C	10.88 -0	IC.88 -C	1C.88 -C	1C.88 -C	1C-88 -C	1C.88 -0	1C.88 -C	1C-88-C	1C.88 -C	IC.88 -C	NF NACH	5 0.599	X/CB Y	8.49 0	8.49 0	8.49 0	8.49 0	8.49 C	8.49 0	8.49 0	8.49 C	8.49 0	8.49 C	8.49 0	8.49 0	8.49 0	8.49 0	8.49 C	8.49 0
TST P TN CC	571 1 66	MACH G	0.604 177.7	0.601 176.5	0.600 175.9	0.600 175.9	0.598 175.3	C.558 175.3	0.558 175.3	0.558 175.3	0.600 175.9	0.600 175.9	0.600 175.9	0.600 175.9	0.600 175.9	0.600 175.9	0.600 175.5	0.602 177.1	TST P TN CO	571 1 66	MACH 9	0.559 176.6	0.600 177.2	0.600 177.2	0.602 177.8	0.602 177.8	0.603 178.4	0.602 177.8	0.602 177.8	0.602 177.8	0.602 177.8	0.602 177.8	0.602 177.8	0.601 177.2	0.602 177.8	0.602 177.8	0.603 178.4
RUN	282	SFO	2	r 1	4	U D	9	2	œ	6	10	11	12	6 1	14	15	16	17	NUA	283	SFQ	H	2	m	4	ŝ	9	٢	8		01	11	12	13	14	15	16

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	0670	1.008	1.004	1.003	1.000	766.0	0.599	666.0	0.598	665.0	1.000	1.001	0.598	0.598	1.002	1.005	1.006			pF/p	1.007	1.006	1.002	1.003	1.001	666*0	0.999	0.998	0.998	0.599	0.998	1.000	1.000	1.001	1.004	1.005
	مر	0.031	0.015	0.014	0.002	110.0-	-0.004	-0.002	-0.007	-0.004	-0.001	0.005	-0.006	-0.008	0.007	0.018	0.023			CD	0.026	0.025	0.007	0.011	0.004	-0.002	-0.005	600.0-	-0.007	-0.003	-0.009	-0.001	-0.001	0.004	0.014	0.019
	~ ~ ~																			VA/V																
) VF/V	0.907	0.925	0.926	0.901	0.882	0.864	0.867	0.858	0.858	0.861	0.870	0.886	0.942	0.959	0.979	0.981		_	VF/V	0.981	0.982	176.0	0.919	0.891	0.884	0.866	0.871	0.874	0.864	0.886	0.901	0.935	0.962	0.984	0.985
ALPHA	10.00																	ALPHA	10.00	0A/Q																
11	68.8 0F/0	0.819	C.850	0.852	0.801	0.764	0.733	0.738	0.721	0.721	0.727	0.746	0.771	0.879	0.916	0.959	0.966	11	69.1	0F/0	0.966	0.967	0.952	C.837	0.784	0.768	0.735	0.743	0.750	0.733	0.772	0.802	0.867	0.922	0.969	0.973
с ;	10/ W/WW																	۵	101	WV/W																
0 0 1 1	1 / /•8 MF /N	106.0	0.920	c. 922	0.895	3.875	0.857	C.855	0-850	0.850	0.853	0.863	0.879	656*3	0.956	116.0	086.0	ى ئ	177.8	MF/W	086.0	386.3	0.975	.914	.885	0.877	.858	.863	.867	.856	3.875	3-895	1:6*	0.960	.983	.984
PT 200	7 / DB	2.03	1.53 (.1.02 (-0-69	0.53 (0.36 (0.19	0.02 (0.15 (0.31 (0.48 (0.64 (66*0	1.18	1.48 (1.98 (PT .	896	Z/DB	.2.02	1.52 (·1.03 () 59*0.	0.52 (0.36 (0.19 (0.02	0.15 (0.32 (0.48	0.65 (0.97 (1.18 (1.48 (1.98 (
RN/L	. 1•512 Y/DB	0.01 -	- 10-0.	- 10-0	- 10-0	- 10 · J	- 10-0	- C. C. L	- 10-0	0.01	·0. C1	10-0.	0.01	10.0	.0.01	10-0-	0.01	RN/L	1.510	Y/CB	0.36 -	C.36 -	0.36 -	C+36 +	0.36 -	0.36 -	0.36 -	0.36 -	0.36	0.36	0.36	0.36	0.36	0.35	0.36	0.36
VACT.	. U•6U2 X/E8	8.49 -	- 64.3	8.49 -	£•49 -	- 64.3	- 64*3	E.49 -	- 64. 3	8.49 -	E.49 -	8.49 -	- 64•3	8.49 -	- 65*3	E.49 -	E 49 -	N A C H	0.602	X/5B	8.49 -	8.49 -	8.49 -	8.49 -	8.49 -	- 64.8	8.49 -	6 • 49 -	- 64.8	- 64•3	- 64•3	- 65-8	8.49 -	6 • 49 -	8.49 -	8.49 -
N CONF	n o G	7.6	7.2	7.2	7.2	7.2	7.8	7.8	7.2	7.8	7.8	7.8	7.2	7.2	7.2	7.8	7.8	N CONF	41 50	Cł	7.8	7.8	7.8	7.8	1.8	7.2	7.2	7.2	7.2	7.2	5.6	7.2	1.2	7.2	7.8	7.8
	0 - H	02 17	11 10	01 17	01 17	11 10	02 17	C2 17	.21 10	02 17	02 17	02 17	01 17	11 10	CI 12	02 17	C2 17	T P T	1 1 6	E	02 17	02 17	02 17	02 17	02 17	CO 17	00 17	CO 17	11 00	C0 17	66 17(00 17	CI 17	.21 10	02 17	02 17
ST ST	4 U U U U U U U U U U U U U U U U U U U	1 0.6	2 0.6	3 0.6	4 0.6	5 0.6	6 0.6	7 0.6	8 0.6	9 0 6	0 0.6	1 0.6	2 0.6	3 0.6	4 0.6	5 0.6	6 0.6	IN TS	15 57	AM Q	1 0.6	2 0.6	3 0.6	4 0.6	5 0.6	6 C.6	7 0.6	8 0.6	9.0.6	0 0.6	1 0.5	2 0.6	3 0.6	4 0.6	5 0.6	6 0.6
a a	N V	>									-		_		-			J L	28	5											-			••••	1	

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0.999 1.006 1.003 0.999 0.999 0.998 1.000 1.005 0.999 0.598 0.999 666 1.007 1.002 1.000 666.0 666 005 0.999 666.0 665.0 665.0 0.999 0.999 1.001 0.999 0.999 0.999 666.0 pr/p 0.997 0.998 1.002 . . -0.005 0.003 0.002 0.007 0.023 0.014 0.019 0.027 -0.009 -0.013 -0.015 -0-039 -0.030 -0.019 -0.030 -0.030 -0.030 -0.028 -0.022 0.010 -0.003 -0.007 -0.024 -0.021 100.0--0.021 -0.011 -0.021 -0.021 -0.02 8 0.000 0.000 0.000 0.000 000 0.000 000 A/V 0.000 0.000 0.000 0.000 0.000 0.000 V A /V . 0.951 0.830 0.879 0.871 0.871 0.882 0.885 0.885 0.895 0.952 0.952 0.928 0.983 0.985 0.979 972 975 266 0.975 U.922 0.903 0.891 0.994 0.954 0.907 0.927 0.928 0.935 0.983 0.984 0.934 0.941 VF/V VF/V 0.980 ం . 0 10.00 0A/0 AL PHA 10.00 ALPHA 0.000 c.000 0.000 c. 000 c.000 0.00.00 c. 000 c. 000 000.0 0.000 0.000 QA/Q 000-000 000-0 000.0 C.000 100.00 0.903 0.816 0.901 0.935 68.4 0F/0 C.9888 0.967 0.957 C.820 O.856 O.858 0.853 69.4 GF/0 0.972 C.843 0.804 C.780 0.761 0.759 0.743 0.766 0.789 0.969 0.974 0.872 0.950 **C.**882 0.859 0.965 0.943 C.950 0.993 0.965 0.000 0.000 0.000 000 000 0.000 0.000 0.000 0.000 0000.0 0.000 702 M / M 80.2 1811 WF/N MA/N 0.000 0000.0 0.00.0 C. . 177.2 MF/W C.979 0.954 C.984 0.953 0.940 C.9C6 C.926 C.927 0.951 C.924 0.935 0.875 0.889 0.927 0.583 0.983 0.973 0.897 0.864 0.872 0.863 0.982 C.9E4 C.979 0.971 0.903 0.949 0.873 0.966 C.917 5-5-7 . 56° 896 0.251 1.517 1893 (/CB Y/DB Z/DB -0.20 -0.02 0.15 0.31 0.48 -0.70 -0.36 -0.20 0.12 0.29 0.46 0.63 -0-35 0.58 l.48 X/08 Y/09 Z/08 8.49 -0.45 -2.03 -1.53 0.65 -2.05 • 63 .17 -0-65 -0.53 ω F. -1.03 F d -1.54 -1.04 - 40 6. ç . **RN/L** F WACH RN/L 5 0.600 1.507 -0.45 -0.45 -0.45 0.41 0.41 0.41 0.41 -0.45 -0.45 -0.45 -0.45 C.41 C.41 0.41 0.41 0.41 SC) ŝ ŝ S 0.41 C.41 -0.45 -0-45 .41 -0.45 -0.45 -0-45 C • 4] 0.41 4 MACH 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 X/08 TN CONF S CONF 177-2 5.61 78.8 78.8 78.8 78.8 75.5 79.5 . ω 2 66 C 571 1 672 0 6750 0 7500 0 750 000000 571 1 MACH ٥ 0.600 0.600 0.600 0.600 0.600 0.600 0.601 0.601 250 249 249 249 0.250 0.6C1 0.6C1 0.601 . 602 .602 **TST** 49 50 0.601 0.601 TST 0.2 ~ 0 \odot 0 4 $\underline{\nabla}$ 287 SEG PUN 286 SEQ **u**h 450000 \mathbf{O} \mathbf{n} (m 4 ŝ m + m o r o σ Σ RUN Ξ **N**

		pr/p	0.999	0.999	665°0	665 0	0.599	665 0	0.999	666.0	665°0	0.999	0.598	665*0	0.599	665*0	0. 999	665*0			DF/D	665.0	665°U	0.9999	0.999	
		с С	-0.022	-0.022	-0.922	-0.030	-0-030	-0-030	-0.030	-0.030	-0.030	-0.030	-0-039	-0.014	-0.021	-0.025	-0.026	-0.017			Ċ	-0.017	610.0-	-0.030	-0.030	
		V A /V	0.000	0.000	0.000	0.000	U. 0CO	0.000	0.000	0.000	0.000	0-000	0.000	6.000	0.000	0.000	0.000	0.000			V A /V	0.000	0.000	0.000	0.000	
~~~	~	VF/V	0.941	0.946	0.941	0.916	0.914	0.902	0.893	0.891	0.903	0.899	0.925	0.914	0.956	0.946	0.940	0.991	_	~	VF/V	0.992	0.986	0.975	0.921	
AL PHA	10.00	0A/Q	c.000	0.00.0	c.00.	c.000	000.0	0.00.0	000.0	0000.0	C.000	000.0	0.000	000.0	0.000	0.000	000-0	000.0	AL PHA	10.0C	0A/G	0.000	0.000	0.000	c.000	
11	68.1	QF /0	0.884	0.893	C.884	0.836	0.832	0.811	0.794	0.790	0.813	0.806	0.853	0.834	0.913	C.892	612.0	0.981	ŢŢ	68.0	0F/0	<b>C.982</b>	0.972	0.948	0.846	
۵.	5 1811	M / M	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0000*0	c	1181	NVN	0.000	0000.0	0.000	000.000	
G	19.	MF /N	0.941	C. 945	C.941	C.915	C-913	105.0	C.892	C.89C	C.902	C.858	C.925	C12.0	C.556	C.945	055 * 0	156.3	U	- 52	NF/N	C.952	<b>c.</b> 586	C.974	C.92C	1
L PT	1 1892	Z / DB	-2.04	-1.55	-1.04	-0.71	-0.54	-0.38	-0.20	-0.03	0.13	0.29	0.46	0.63	10.97	1.16	1.47	1.56	L pT	2 1892	2/08	-2.04	-1-54	-1.05	-0.71	1
CH RN/	0 1.51	Y/D8	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0-03	-0.03	-0-03	-0+03	-0.03	-C.03	-0.03	-C.03	INA H	10 1.51	Y/DB	-0-38	-0-38	-0.38	-0.38	1
F VAC	5 C•25	X/CB	1C.88	1C.88	10.88	1C-88	10.88	10.88	10.88	10.88	10.88	10.88	10.88	10.88	1C.88	10.88	10.88	10.88	F VAC	5 0.25	X/CB	10.88	10.88	10.88	10.88	•
TN CCN	66	U	79.5	2.91	79.5	2*6L	79.5	19.5	78.8	78.8	78.8	78.8	18.8	79.5	78.8	78.1	78.1	78.8	TN CCN	66	c	2.91	79.5	2*61	79.5	1
TST P	571 1	MACH	0.250	0.250	0.250	0.250	0.250	0.250	0.749	0.249	0.249	0.749	0.249	0.250	0.249	0.248	0.248	0.249	TST P	571 1	MACH	0.250	0.250	0.250	0.250	

**AL PHA** 

ORI OE	GII PO	VA OR	L	₽4 QU	AG AI	e Lij	IS V			
	4	66	66	66	66	66	99	66	66	(

TST F	> TN CC	NF VA	CH RN	/r p1	U L	c	TT	<b>AL PHA</b>				
571	1 66	5 0.2	50 1.5	12 189	32 79.	5 1811	68.0	10.0C				
MACH	c	X / CB	Y/DB	Z/D8	N/JN i	NVN	QF/0	0A/G	VF/V	V / V / V	Ċ,	DF/D
0.250	79.5	10.88	-0-38	-2.04	C.952	0.000	C.982	0.000	0.992	0.000	-0.017	0.599
0.250	19.5	1C-88	-0.38	-1-54	• C.586	00000	0.972	0.000	0.986	0.000	610.0-	665°U
0.250	79.5	10.88	-0.38	-1.05	5 C.974	0.000	0.948	0.000	0.975	0.000	-0.030	0.9999
0.250	79.5	10.88	-0.38	-0.71	. C.92C	0.000	0.846	C.000	0.921	0.000	-0.030	0.999
0.250	2.91	1C.88	-0.38	-0-54	· C.912	0.000	0.830	0.000	0.913	0.000	-0.030	0.999
0.250	79.5	10.88	-0.38	-0-38	128.0	0.000	0.804	c. 000	0.898	0.000	-0.021	665.0
0.250	79.5	10.88	-0-38	-0.21	0.916	0.000	0.839	0.000	1.16.0	0.000	-0.021	0.599
0.250	79.5	1C.88	-0.38	-0.04	+ C.914	0.000	0.834	0.000	0.915	0.000	-0.021	0.9999
0.250	79.5	10.88	-0-38	0.13	116.0	0.000	C.839	c. UOO	0.917	0.000	-0.030	0.999
0.250	79.5	1 C. 88	-0.38	0.30	0.888	000.0	0.787	0.000	0.889	0.000	-0.030	0.999
0.250	79.5	10.88	-0-38	0.46	005°0 S	0.000	C.810	C• 000	106.0	0.000	-0.030	665.0
0.250	79.5	10.88	-0.38	0.64	0.921	0.000	0.848	000.0	0.922	0.000	-0.030	665.0
0.250	79.5	10.88	-0.38	0.96	C.950	0.000.0	0.901	0.000	0.951	0.000	-0.030	0.9999
0.250	79.5	1C.88	-0.38	1.16	0.966	0.000	0.932	C. UUU	0.966	0.000	-0.022	0.999
0.250	2.21	1 C • 88	-0-38	1.46	0.983	0.000	0.965	0.000	0.983	0.000	-0.019	0.5999
0.250	2.97	10.88	95.0-	15°1	0.988	0.000	0.976	0.000	0.938	0.000	-0.006	1.000

1.000 0.999 665*0 665*0 0.599 0.9999 666.0 665 0.9999 666 666 0.999 0.999 665.0 665.0 665 1 0 ě 0 -0.023 -0.030 -0.030 -0.030 -0.030 -0.030 -0.030 -0.021 -0.030 -0.024 -0.017 C -0.021 -0.02 -0.00 -0-01 0.000 VA/V 0.0000 0.000 0.00 0.00 0.00 0.000 0.000 0.000 0.000 0.000 0.000 000 0.000 0.909 968 979 0.989 967 0.958 VF/V 934 924 0.917 0.926 0.906 0.918 990 0.994 0.931 0.903 . . • • 0 0 . 10.00 ALPHA 0.000 0.000 0.000 000.0 c.000 000.0 0 A / Q 0.00.0 0.000 0.000 c.000 c.000 000.0 0.000 0.000 .000 .988 0.852 0.838 0.855 67.9 CF/Q 0.934 0.87I C.841 C.841 .934 616 0.824 0.818 0.865 0.915 • Ó  $\mathbf{O}$ 0 000.0 000 • 0 0.000 MA/W 0.0000 0.0000 0.000 0*000 0.000 000.000 1811 000.0 0.000 0.000 0000.0 78.8 MF /N 0.989 0.954 0.957 0.934 C.923 C.916 C.925 C.925 C.928 C.905 L16*0 0.967 056°) 525°) C.902 C.957 5 0.249 1.506 1891 -0.21 -0.03 0.12 0.25 0.48 -1.54 -1-05 -0.71 -0.54 -2.04 0.63 2/08 PT 0 PNJL -C.48 -C.48 -0.48 X/DB -0.48 -0.48 -0.48 α ω ω ω ω ω ω ω 8 Ω -0-48 -0-45 -0-48 -0-48 -0-48 -0.41 -0-48 -0-41 4 4 . 00 MACH CONF 79.5 20.01 20.01 20.01 20.01 17 66 571 1 a. 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.250 0.250 0.250 0.250 MACH 0.249 0.250 0.250 0.250 S RUN 290 SEG 2 N m + 1 0 ~  $\boldsymbol{\infty}$ σ  $\mathbf{N}$ 3 4 S

0.999 666.0 0.999 999 666*0 665 DF/D 665 999 0.999 0.999 665 °0 665.0 0.999 0.999 666.0 0.999 č 0 -0.021 -0.030 -0.030 -0.030 -0.030 -0.015 -0.019 -0.017 -0.017 -0.024 -0.021 -0.021 -0.014 -0.021 -0-05 3 0.0000 0.000 0.000 000 000 0.000 0000 <u>v / v</u> 0.000 • . . > 0.929 0.918 0.940 968 965 0.993 0.913 0.901 0.990 934 902 933 166 VF/V **0.**984 0.913 0.994 • • 0 0 0. 0 10.00 0A/0 ALPHA 0.000 0.000 0.000 000.0 0.000 0.000 C-000 c. 000 c. 000 0.000 0.000 C.000 0.000 0.000 0.000 0.979 0.986 0.967 .929 67.8 QF/0 0.841 0.870 0.831 0.811 C.810 0.868 .936 .981 0.830 0.830 0.860 986  $\circ$ 0 • 000 0 • 000 0.000 0000-0 0.000 0.00.00 N/VN 0.000 000.0 0.000 0.000 1811 0.00.0 0.000 0000.0 79.5 NF / N C.993 0.984 0.918 0.933 0.535 0.912 C.900 C.912 C.928 265°0 166°0 796°0 066-0 C.932 C.968 -1.53 5 0.250 1.512 1892 X/CB Y/CB Z/DB -0.52 -0.35 -0.15 -0.02 0.45 0.45 0.14 0.65 0.98 F d -2.03 ¢  $\boldsymbol{\omega}$ ω 3**5**•1 1.1 PN/L 0.43 0.43 0.43 C•43 O•43 O•43 0.43 m (7) **C**1 **6**73 (m) m ក្រា 0.4 0.4 0.4 4.4 0-4 4 0.4 N A CH TN CONF -62 .61 571 1 MACH Ω. 0.250 0.249 0.250 250 250 250 250 TST 0 • 5 0 291 SFQ PUN 4 10 V M 00 σ O  $\mathbf{n}$ m 4 5 0

	۵	. 0	σ	6	6	σ	σ	σ	ç	σ	6	σ	ō	5	ç	6	ō			٩	σ	φ	σ	σ	6	6	δ	6	6	<u>ь</u>	σ	6	6	6	c
	DF /	0.99	0.59	65*0	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.59	55°0	0.99	0.99	0° 33	0.99			DF/	0.59	0.59	0.99	0.99	65.0	0.59	65 • 0	0.99	0.99	0.99	0.59	0.99	0.99	0.99	
	a J	-0.017	-0.021	-0.022	-0.030	-0.030	-0.030	-0.030	-0.030	-0.030	-0.030	-0.030	-0.030	-0-024	-0.028	-0.028	610.0-			a C	-0.026	-0.017	-0.024	-0.026	-0.030	-0.030	-0.032	120.0-	-0.021	-0.021	-0.021	-0.021	-0.021	-0.019	
	~ ~ ~	0000.0	0.000	0.000	0.000	0• 000	0-000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0-000			VAIV	0.000	0.000	0.000	0.000	0.000	0-000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
~~ ~	, VE/V	0.927	0.945	0.937	0.889	0.883	0.863	0.874	0.386	0.873	0.866	0.899	0.912	0.944	0.980	0.987	0.997			VEZV	0.994	0.980	0.971	0.938	0.905	0.899	0.901	0.883	0.879	0.879	0.302	0.917	0.960	0.984	200 0
ALPHI		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0	c.000	0.000	0.000	0.000	0.000	c. 000	0.000	000 •0		10.00	04/0	0.000	0.000	000-0	0.000	0.000	0.00.0	0.00.0	0.00.0	C-000	0.000	C• 000	0.00.0	0.000	C•000	
TT,	0 - 1 0 0 - 1 0	0-856	0.891	0.875	0.787	0.777	0.742	0.761	0.782	0.759	0.747	0.806	C.829	0.888	0.958	0.974	0.993	Ĩ	67.7	0F/0	0.987	0.960	0.941	0.878	0.817	C.8C6	0.810	0.776	0.769	0.770	0.811	0.839	0.920	0.967	
d	1181 MV/W	0000-0	0.000	0.000	0.000	000.0	0.000	0000.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00.0	000.000	۵	1811	NA/W	0.000	0.000	0000-0	0.000	000.000	0.000	0000.0	0.00.00	0.00.0	0.000	000 * 0	0.000	000.000	0000.0	
U (	1 • 7 · 1 N	C-926	C.944	0.936	0.888	C.882	<b>C.</b> 862	C.873	0.885	C.872	C. 865	0.858	116.0	C.943	0.979	0.987	L 56 ° 0	C	78.8	NF / N	0.954	C.980	172.0	C.937	C.904	C.858	C• 500	C.881	0.878	C.878	105*0	c.916	095-0	C.984	
L PT	3 1892 7 / N B	- 2,00		-1.03	-0.69	-0.53	-0.36	-0.19	-0.01	0.14	0.32	0.47	0.65	0.98	1.17	1.48	1.98	Id	1991 4	Z/08	-2.03	-1.52	-1.02	-0.10	-0.52	-0.36	-0.15	-0-03	0.15	16.0	0.48	0.64	9.580	1.18	•
		- 10-0-	-0-01	-0-01 -	- 0.01	- 10-0-	-0.C1	- 10-0-	-0-01	-0-01	-0-01	-0-01	-0-01	-0.01	10.0-	-0.01	-0.01	Nd	1.50	Y/DB	-0-36 -	-0-36 -	-0-36 -	-0-36 -	-C.36 -	-0-36 -	- 0-36 -	- 92.0-	-0.36	-0-36	-0-36	-0-36	-0-36	-0-36	
LACI		01/4 8/40	8.49	E 49 .	- 64•3	8.49 -	8.49 -	6.49	. 49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	8.49	M D C I	0-24	×/08	. 64. 6.	8.49 -	£ • 4 9 -	8.49 -	8.49 -	8.49 -	8.49 -	8.49 -	64.49	- 64•3	64.6	8.49	- 64.8	6.49	(
IN CONF	φ c	∋ č "	5.0	2.6	3*61	19.5	3.61	19.5	79 <b>.</b> 5	8.8	78.8	78.8	78.8	79.8	78.8	78.8	78.8		9	e e	8.8	9.5.5	10. E	8.8	8.8	8.8	8.8	8.8	8.8	5*6	9 <b>.</b> 5	5°5	·9.5	5.5	•
I d I S I			250 7	.250	.250	.250	.250	.250 1	.250	.249	. 249	.249	.249	.249	- 249	.249	.249	1 0 1 2 1	571 1 6	ACH	.249 7	.250 7	.250 7	.249 7	.249 7	.249 7	,249 7	.249 7	249 7	.250 7	,250 7	.250 7	,250 7	.250 7	
RUN	292	5 C 3 F	10	30	4 0,	5 0	6 0	-0 -	ບ 8	°0 6	10 0.	11 0.	12 0.	13 0.	14 0.	15 0.	16 0.	L NIId	292	SEC.	10	2 0,	30.	۰ ۲	2 0	6 0.	7 0.	8	•0 6	10 0.	11 0.	12 0.	13 0.	14 0.	( (

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666 • 0 0.999 0.999 666.0 0.599 000 665 • 0 6665.0 665 °0 0.999 666.0 0.599 0.999 666.0 0.599 666.0 PF/I -0.024 -0.019 -0.022 -0.019 -0.014ŝ -0.015 -0.021 -0.021 -0.021 -0.021 -0.021 -0.021 -0-021 -0-02 00.0å V ∆ /V 0.0C0 0.000 0.000 0.000 0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 U. 0C0 0.000 0.000 0.988 0.922 0.902 0.880 893 987 0.993 0.980 VF/V 0.990 0.889 0.908 0.933 0.961 0.992 0.892 0.887 . • 10.00 ALPHA 0A/Q 0.00.0 0.000 0.00.0 000.0 0.000 0.00.0 0.00.0 0.000 000-0 0.000 0.000 0.000 0.000 C.000 0.00.0 0.000 1.982 0.868 0.960 0.979 C.848 0.811 0.792 0.772 0.794 67.6 0F/0 C.974 0.784 0.923 0.787 0.821 0.986 .974 Ó 000.000 0000 0.000 0.000 0.000 0.000 .000 0.00.00 0.000 0.000 1812 M / M 0.000 0.000 ۵. C 78.8 MF/N 69930 C•990 C•987 C•921 C•921 C•921 0.875 0.886 0.907 0.961 0.892 C.888 c.932 C.980 C-987 U C.249 1.507 1892 X/CB Y/CP Z/DB 8.49 -C.45 -2.03 ( 0.65 0.98 1.18 -1.53 -0.52 -0.35 0.14 ω -0.18 -0.02 16.0 La La 0.48 • 4 5. PN/L - C • 45 -0-45 -0-45 -0.45 34.0--0-45 -0.45 -0.45 -0-45 -0.45 -0.45 -0-45 S ŝ -0-45 4. NACH VACH 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 ŝ LUN F 80.2 80.2 80.2 79.5 80.2 80.2 80.2 779.5 779.5 80.2 80.2 4n N 6 80. 2 ۵. 571 1 MACH 0.249 5 15 010m4 8 UN 294 SF0 RUN NW400000

.027 1.000 1.009 1.025 1.034 1.031 1.010 1.000 .013 .006 .017 1.005 1.002 762.0 0.596 0.016 0.039 0.054 0.043 0.038 0000.0 0.049 -0.006 -0.006 0.007 0.003 0.00.0 0.015 0.027 0.021 ð V V V 0.971 0.962 0.916 0.916 0.918 0.877 0.877 0.933 0.973 0.973 0.973 0.971 VF/V 971 . ALPHA -10.00 QA/Q 68.1 QF/0 0.959 0.935 0.935 0.836 0.823 0.823 0.823 0.823 0.823 0.823 0.761 0.751 0.759 0.799 0.897 0.954 0.969 0.965 0.961 382 M / MN ۵ 243.4 MF/N 0.965 0.966 0.955 0.958 0.903 C.882 0.871 0.874 0.859 0.877 106.0 C.394 0.942 C.969 16.0 96 1 686 2 2/08 -0.54 -0.21 0.13 0.29 0.47 0.63 -1.53 -1.05 -0.70 -0.38 -0.03 76.0 1.17 ω 1.97 1.48 RNJ 0.954 1.483 Y/DB C.41 0.41 C.41 0.41 0.41 C.41 .41 0.41 0.41 0.41 .41 .41 4. 4. 4. 4. ò లి  $\mathbf{O}$  $\mathbf{C}$ VACH X/TB C 888 C 8888 C 888 C 888 C 888 C 8888 C 888 C 888 C 888 C 888 C 888 C 888 C • 88 C • 88 C • 88 88 **u**n **HNUU** 241.9 241.9 241.9 241.9 241.9 241.9 241.5 241.9 241.9 241. Z 1 66 ۵. 571 ] MACH 0.954 0.952 0.952 0.950 0.950 0.950 0.950 0.950 0.954 0.950 676 0.950 0.950 0.950 TST . 295 SEQ 2 3 450000 2 <u>-2</u> 4527

		bF/p	1.023	1.023	1.013	1.008	1.006	1.003	1.003	666.0	966.0	0.999	1.002	1.008	1.015	1.018	1.024	1.030					pc/p	1.025	1.021	1.014	1.006	1.001	0.9999	199.0	0.992	0.992	9994	0.598	1.004	1.013	1.018	1.028	i 1.035
		C D	0.036	0.036	0.021	0.013	0.010	0.005	0.005	-0.002	-0.009	-0.001	0.003	0.012	0.024	0.028	0.038	0.048					e C	0.039	0.033	0.022	0.010	0.001	-0.001	-0.004	-0.012	-0.013	-0.010	-0.003	0.006	0-020	0.028	0.045	0.055
		V A /V																					V N / V																
ALPHA	-10.00	0A/Q VF/V	0.907	0.937	0.934	0.895	0.876	0.858	0.346	0.847	0.851	0.856	0.864	0.877	0.927	0.954	0.978	0.975			ALPHA	-10.00	QA/Q VF/V	0.966	0.972	0.965	0.918	0.891	0.872	0.364	0.857	0.863	0.361	0.874	0.894	0.940	0.967	0.969	0.973
11	69.6	0140	0.815	0.878	0.863	0.780	0.741	0.705	0.684	0.681	0.686	0.698	0.715	0.745	0.850	0.912	179.0	116.0		ļ		70.7	0F/0	0.944	0.956	0.933	0.824	0.765	0.727	0.712	0.695	0.705	0.703	1.732	0.774	0.877	0.941	0.955	016-0
۵	382	NA/N																		(	ם	381	MV/W																
U	242.9	NF/N	0.852	C.927	c.923	0.875	0.858	0.838	0.826	0.826	0.831	0.836	C.845	<b>C.</b> 860	C.915	C.947	C.974	179.0		Ċ	2	243.4	NF /N	C.96C	196.0	C•959	0.905	C.874	0.853	C•845	0.837	0.843	0.841	0.356	0.878	0.931	296.0	C.964	0.968
Ld .	5 685	2/08	-2.04	-1-55	-1.04	11.0.	-0.54	-0.37	-0.20	-0.04	0.13	0.30	0.46	0.63	0.96	1.16	1.46	1.96		ł	n.	685	Z / 0.8	-2.04	-1.54	-1.04	12-0-	-0.53	-0.38	0.20	-0-04	0.13	0.30	0.47	0.63	0.96	1.16	1.47	1.96
RNA	1.476	Y/08	- 60.0-	-0.03 -	- 0.03	- 60.0-	-0.03 -	- 60-0-	-0-03 -	- 0- 03 -	-0*03	E0 • 0 •	-0-03	-0-03	-0-03	-0-03	-0-03	£0•0-	*			5 1.473	Y/DB	-0.38 -	-0-38 -	-0-38-0-	- 0.38 -	0.38	0.38	- C* 38 -	-0-38 -	-0.38	·C. 38	-0.38	·C•38	• <b>0</b> •38	•0•38	•0•38	•0•38
WACH	0.953	X/DB	C. 88 -	C. 88 -	C.88 -	C.88 -	0. 88 -	0.88 -	C. 88 -	C . 88 -	0.88 -	C. 88 -	C 88 -	C 88 -	0.88 -	0.88 -	C. 87 -	C . 88 -		2	NACH	0.955	X/DB	0.87 -	0.87 -	C.87 -	C.87 -	C.87 -	C.87 -	C.87 -	C.87 -	C-87 -	0.87 -	C.87 -	C. 87 -	0.87 -	C.87 -	0.87 -	0.87 -
CONF	ŝ		1 6.	- 6	.4 1	.4	1 5.	1 5.		• 0		- C	•0	-0	• 1	• 6	• ć 1				CONF	ŝ		• 4 1	• 4 1	- 2	1 1.			• 1 1	- 7 - 1	-7 1	•6 1	• 1 1		• 7 I	- 1	•6	• •
P TN	1 66	C -	242	242	242	242	241	241	241	242	242	242	242	242	241	241	241	241		i F	2	1 66	0	243	243	244	244	244	244	244	244	244	244	244	244	243	243	244	244
<b>TST</b>	115	MACH	0.953	0.953	0.951	0.951	0.950	0.950	346-0	0.945	0.945	0.945	0.945	576-0	0.946	0.947	0.947	0.948		۴ د ۴	121	571	MACH	0.955	0.955	576*0	056-0	0.950	0-950	0.950	0-950	0.950	0.951	0-950	0.950	576-0	0.945	0.951	0-951
NUN	296	SEQ	T	2	<b>m</b>	4	ĥ	9	-	ω	σ	10	11	12	<b>7</b>	14	15	16			2 D ¥	297	SEQ	-1	2	<b>6</b> 1)	4	ŝ	9	~	œ	σ	10	11	12	6	14	15	16

	CP PF/P	0.036 1.023	0.031 1.019	0.019 1.012	0.007 1.005	0.010 1.006	0.002 1.001	-0.004 0.998	-0.004 0.598	-0.002 0.999	0.032 1.001	0.005 1.003	0.006 1.004	0.016 1.010	0.033 1.021	0.045 1.028	0.053 1.034			CD DE/D	0.028 1.018	0.027 1.017	0.020 1.013	0.007 1.004	-0.001 0.599	-0.007 0.996	-0.010 0.994	-0,010 0,993	-0.013 0.992	-0.011 0.593	-0.010 0.994	-0.003 0.598	0.009 1.006	0.019 1.012	0.033 1.021	0.047 1.029
ALPHA	04/0 VF/V VA/V	0.975	0.977	0.965	0.917	0.901	0.891	0 • 885	0.875	0.876	0.878	0.386	0.911	0.954	0.961	0.969	0.973	АЦРНА	-10.00	DA/Q VF/V VA/V	0.980	0.979	0.975	0.926	0.926	0.909	0.897	0.884	0.870	0.874	0 • 384	216.0	0.964	0•930	0.980	0.976
71 q 71 485	MA/M QF/Q	0.963	0.966	166.0	0.820	0.790	0.766	0.751	0.733	0.736	0.741	0.757	0.809	0.904	0.930	C.956	0.969	11 d	385 72.4	MA/M CF/0	179.0	0.967	0.955	C•840	0.835	0.798	0.773	0.746	0.719	0.728	0.746	0.806	0.923	0.965	0.974	179.0
CNF MACH RN/L PT C 5 0.962 1.483 692 245.1	X/CB Y/CE Z/CB MF/N	1C.87 -C.48 -2.C4 C.970	10.87 -0.48 -1.54 0.973	IC.87 -0.48 -1.04 0.959	10.87 -0.48 -0.71 0.904	10.87 -0.48 -0.54 0.886	1C.87 -C.48 -0.38 0.875	10.87 - 0.48 - 0.20 0.868	IC-87 -0.48 -0.04 0.857	IC.87 -C.48 O.12 C.855	1C.87 -0.48 0.28 C.86C	10.87 -0.48 0.46 C.869	IC.87 -C.48 0.63 0.857	IC.87 - C.48 0.96 0.946	10.87 -0.48 1.16 C.954	10.87 -0.48 1.46 C.964	1C.87 -C.48 1.97 C.968	CNF MACH RN/L PT C	5 0.954 1.481 692 245.7	X/D9 Y/D8 Z/D8 MF/M	8.48 C.43 -2.C3 C.977	8.49 0.43 -1.52 C.975	8.48 C.43 -1.C3 C.971	8.48 0.43 -0.65 C.915	8.48 0.43 -0.52 C.914	8.48 C.43 -0.34 C.855	8.48 0.43 -0.19 0.882	8.48 C.43 -0.02 0.867	8.48 0.43 0.14 C.852	8.48 0.43 0.31 0.856	8.48 0.43 0.48 C.867	8.48 0.43 0.66 0.899	8.48 C.43 C.97 C.958	8.48 0.43 1.18 C.977	8.48 0.43 1.48 C.976	8.48 C.43 1.58 C.971
RUN TST P TN CC 298 571 1 66	SFG MACH Q	1 0.952 245.1	2 0.952 245.1	3 0.954 245.7	4 0.954 245.7	5 0.954 245.7	6 0.954 245.7	7 0.954 245.7	8 0.954 245.7	9 0.954 245.7	10 0.954 245.7	11 0.954 245.7	12 0.952 245.1	13 0.954 245.7	14 0.952 245.1	15 0.951 244.6	16 0.949 244.2	PUN TST P TN CC	299 571 1 66	SEG MACH Q	1 0.954 245.7	2 0.954 245.7	3 0.956 246.2	4 0.956 246.2	5 0.954 245.7	6 0.953 245.1	7 0.953 245.1	8 0.953 245.1	9 0.952 245.1	10 0.954 245.7	11 0.952 245.2	12 0.952 245.2	13 0.952 245.2	14 0.949 244.2	15 0.949 244.2	16 0.950 244.7

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1.020 0.993 0.986 1.006 1.017 1.025 1.028 1.020 1.007 1.004 1.007 1.010 799. 797 0.990 DF/D 1.001 1.024 .013 1.001 .008 1.022 1.021 0.988 0.588 pr/p . 027 066.0 0.998 1.003 1.004 1.005 1.017 1.020 .02( -0.005 0.033 0.002 0.007 0.013 0.009 -0.015-0.018 -0.018 -0.015 -0.003 0.026 0.039 0.036 0.008 0.030 0.016 -0.021 0.045 0.036 0.038 0.031 0.002 0.043 0.023 0.005 0.013 0.007 0.047 0.046 ð ٥ V A /V V A / V 0.975 0.897 0.877 0.862 0.879 0.901 766.0 0.873 VF/V 0.923 0.932 0.854 0.886 0.974 0.978 0.864 0.846 0.345 0.973 0.975 VF/V 0.938 0.945 0.898 0.870 0.860 0.851 0.845 0.857 0.927 0.953 0.968 779.0 974 ALPHA -10.00 -10.00ALPHA 0A/Q 0 A / Q 0F/0 0/ 40 0.885 0.740 73.6 0.831 0.733 0.707 0.671 0.907 73.8 0.862 0.785 0.744 0.694 0.685 0.708 0.703 0.857 0.914 0.953 0.969 0.672 0.701 0.895 964 0.953 0.961 0.774 0.735 0.783 0.954 0.965 0.974 0.771 387 419 W/ VN MV/W ¢ 0 246.3 MF/X 0.975 0.965 c.936 c.922 C.836 C.857 176.0 C.950 0.970 C•973 0.839 C.911 1.862 C.842 0.946 C.964 C.97C 0.881 0.859 0.845 0.825 0.824 0.842 0.886 C.929 0.885 0.833 C.826 0.871 970 0.860 C.916 O 695 -0.45 -1.52 -0.45 -1.03 0.13 0.48 0.64 -0.20 0.13 Y/CB Z/CB -0.45 -2.03 -0.45 -0.68 ω •18 •49 -C.03 -2.04 -1.55 -1.04 -0.54 10.97 -0.36 -0.18 0.30 •46 0.62 .16 -0.03 0.31 •46 F -0.71 **6**•0 ŏ. <u></u>6. RN/L 5 C.9CC 1.482 5 0.953 1.482 RN/L -0-45 -0-45 -0.45 -0-45 -0.45 -0.45 -0.45 -0.45 -0.45 -0.03 -0.03 -0.03 -0-45 -0.45 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0.03 -0-03 -0.03 -0.03 -0.03 HUV2 HUVN X/CB E.48 -8.48 8.43 8.48 8.48 8.48 10.87 C.87 C.87 C 87 C 87 C 87 C 87 C 87 C 87 C. 87 C. 87 8.48 8.48 8•48 8.48 C.87 8.48 8.48 8.48 8.48 8.48 C-87 C-87 C-87 C.87 œ 88 8.4 ి P TN CCNF D TN CCNF 237.8 237.8 237.8 238.7 237.3 m 246.8 246.8 246.8 246.3 245.8 245.8 ω 238.2 236.9 4 **6**1 238.7 238.7 239.2 238.2 2 ų U I 246. 245. 238. 238. 236. 236. \$ ٩ 571 1 66 C ٩ 571 1 MACH 0.953 0.954 0.954 0.954 0.954 0.953 0.953 0.952 0.953 0.953 0.900 0.900 0.952 C.950 0.950 MACH 0.901 0.902 0.902 C. 902 949 TST 0.900 0.901 0.901 896 0.953 0.950 0.899 0.858 0.901 0.901 0.896 89 TST . ċ . RUN 302 SEQ 20 303 S S S S * ¢ σ 2 4 5 2 213 14 5 t NNA 4 JU. ŝ

		0/30	1.017	1.017	1.013	1.005	1.003	1.C05	1.004	1.003	1.002	100.1	I.005	1.013	1.017	1.020	1.021	1.017			p⊧/p	1.009	1.009	1.005	1.001	0.996	1.000	0.996	0.596	C. 598	0.996	1.000	1.003	I. CO8	1.013	1.020	1.021
		e)	0.030	0.030	0.023	0.009	0.005	600°0	0.096	0.006	0.003	100.0	500°0	0.023	0.030	0.036	0.037	160.0			СÞ	0.018	0.019	0.010	0.002	-0-007	-0.001	-0.007	-0.009	-0.004	-0.007	-0.001	0.005	0.015	0.025	0.039	0.042
		V A / V																			V A /V					•	•	•	•	•	·	•					
ALPHA	-10.00	DA/Q VF/V	0.939	0.941	0.933	0.893	0.864	0.835	0.820	0.834	0.813	0.320	0.344	0.873	0.933	0.962	0.976	0.980	ALPHA	-10.00	CA/G VE/V	0.926	0.937	0.931	0.895	0.865	0 • 843	0.830	0.831	0.437	0.852	0. 359	0.887	0.942	0.967	0.975	0.979
1 i	74.0	QF / 0	0.879	0.885	0.864	0.775	0.720	0.668	0.640	0.665	0.637	0.640	0.634	0.743	0.866	0.933	0.965	179.0	TT	73.8	CF/0	0.348	0.870	0.355	0.779	0.720	0.682	0.657	0.659	0.670	0.696	0.710	0.766	0.879	0.937	0.964	0.972
۵	417	MA/W																	٩	459	NV VN																
0	238.5	NF /N	0:030	0.933	<b>C.9</b> 24	0.878	0.847	C.816	C.799	C.814	197.0	0.800	0.825	0.856	0.923	0.956	C.972	172.0	G	231.1	MF / N	0.917	C.929	<b>C.</b> 922	C.882	0.850	0.826	C.812	C.814	C.919	C.836	C•843	C.874	0.934	<b>C</b> •962	0.972	0.976
LPT	2 709	Z/08	-2.03	-1.52	10.1-	-0.69	-0.53	-0.35	-0.19	-0.01	0.15	0.32	0.47	0.65	0.58	1.18	1.48	1.98	L b1	8 735	2/08	-2.03	-1.52	-1.02	-0-69	-0.52	-0-37	-0-18	-0.02	0.14	0.31	0.47	0.65	0.98	1.18	L.48	1.98
Na H	4 1.48	Y/DB	-0.01	-0.01	-0-0-	-0-01	-0-01	-0-01	-0-01	-0-01	10.0-	-0.01	10.0-	-0-01	-0-01	10-0-	-0.01	10.0-	F RN/	8 1.45	Y/L8	- 10-0-	- 0.0.1 -	-0.01	- 0.01	- 0-01 -	-0-01	- 10-0-	-0-01	-0-01	-0-01	10-0-	-0.01	-0-01	-0-01	-0.01	-0-01
E WAC	0.00	X / DB	8.49	8.49	- 67 · 8	8.49	8.49	8.49	8.49	E. 49 -	8.49	8.49 -	8.49	8.49	8.49	8.49	£ • 49 ·	8.49		5 0.841	X/CB	8.49 -	- 61.3	8.49 -	E.49 -	E.49 -	- 64.3	8.49 -	8.49	8.49 -	8.49 -	E • 49	- 64.8	8.49	E. 49 .	E. 49 -	5 49 ·
T P TN CON	1 1 66	0 н;	04 238.5	34 238.5	14 239.0	34 235.0	33 238.6	33 238.6	01 238.2	30 237.8	<b>JO 237.E</b>	30 237.8	99 237.4	39 237.4	37 237.0	57 237.C	36 236.5	38 237.4	P TN CCNF	1 66	c,	18 231.1	9 231.5	1 232.4	11 232.3	12 232.2	:2 232.2	1 231.7	1 231.7	1.2.232.1	12 232.1	1.2 232.1	3 232.5	13 232.5	3 232.5	11 231.6	0 231.3
RUN TST	304 571	SEQ MAC	1 0.90	2 0.90	3 0.90	4 0.90	5 0.90	6 0.90	16.0 7	8 0.90	36°0 6	10 0.90	11 0.85	12 0.85	13 0.85	14 0.85	15 0.85	16 0.85	RUN TST	305 571	SEC MAC	1 0.84	2 0.84	3 0.85	4 0.85	5 0.85	6 0.85	7 0.85	8 0.85	9 0.85	10 0.85	11 0.85	12 0.85	13 0.85	14 0.85	15 0.85	16 0.85
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		4	14	14	5	07	05	10	00	02	03	90	05	05	08	60	14	18			d/	0.8	101	90	03	05	00	66	10	10	101	10	lC	06	101	12	
		u a	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.1		1.0	1.0	1.0	1.0	1.0			ц С	1.0	1.0	1.0	1.0	1.0	1.0	<b>6</b> •0	1.0	1.0	1.0		1•0		1.0	1.0	1.0
		C P	0.027	0.029	0.026	0.015	0.009	0.002	0.000	0.005	0.006	0.012	0.009	0.011	0.016	0.019	0.027	0.036			a	0.018	0.015	0.013	0.008	0.004	0.001	-0.003	0.001	0.002	0.003	0.003	0.003	0.013	0.016	0.027	0.024
		V A /V																			V A / V																
		VF/V	0.930	0.935	0.920	0.890	0.879	0.868	0.868	0.864	0.883	0.871	0.889	0.898	0.945	0.966	176.0	0.981			V F/V	0.990	166.0	0.977	0.933	0.921	0.925	<b>0.914</b>	0.906	0.911	0.909	0.918	0.931	0.960	0.976	0.983	0.986
ALPHA	-10.00	QA/Q																	ALPHA	-10.00	Q/AQ																
TT	74.0	QF /Q	0.860	C.870	0.839	0.775	0.752	0.728	0.728	0.722	0.758	7.57.0	177.0	0.788	0.886	0.933	0.961	0.974	11	73.8	QF/0	0.986	0.986	0.955	0.859	0.834	0.840	0.816	0.803	0.812	0.810	0.826	0.852	0.919	0.953	679.0	0.980
۵	457	MVV.																	C.	503	M / M																
ۍ	231.7	MF/N	C.921	C.926	c.910	C.877	0.865	0.853	0.853	0.848	0.865	0.856	0.876	C.886	C.937	C.962	0.974	C.978	Ç	223.4	NF/N	C.985	056.0	0.974	0.925	0.912	<b>C.916</b>	0.904	0.356	106.0	<b>C.</b> 899	0.908	0.923	C.956	C-973	0.980	0.985
10	734	Z/58	-2.04	1.54	-1.04	11.0.	0.54 (	0.38	0.21	0.04 (	0.13	0.29	0.47	0.63	10.97	1.17	1.47	1.97	μ	764	Z/CR	-2.04	-1-54	·1.05	01.0.	0.55	0.38	0.20	-0-C4 -	0.13	0.29	0.47	0.63	0.58	1.16	1.46	1.97
RN/L	1.457	<b>Y/DB</b>	C.03 -	C.03 -	c.03 -	0.03 -	0.03 -	C. C3 -	C.03 -	C. C3 -	c.03	0.03	c.c3	0.03	0.03	0.03	0.03	C•03	RN/L	1.512	Y/08	0.41 -	0.41 -	C.41 -	0.41 -	C-41 -	C.41 -	0.41 -	C.41 -	0.41	0.41	C.41	0.41	C.41	0.41	C.41	C.41
MACH	0.851	X/C8	C.E7 -	0.87 -	C.87 -	0.87 -	0.87 -	C.87 -	0.87 -	c. 87 -	0.87 -	C.87 -	0.87 -	0.87 -	C. 87 -	0.87 -	C.87 -	C. 87 -	NACH	0.796	X/DB	C.87	C.87	C. 87	c.87	<b>C.</b> 87	<b>C.</b> 87	<b>C.87</b>	C.87	C.87	C. 87	C.87	<b>C.87</b>	C. 87	C.87	C. 87	C.87
CONF	K V	• ,	1 -		-	<b>–</b>	i o	-	5	Ē	Ĩ	i D	ີ ບ	0	4	4 1	1	-	CONF	ŝ		4	-1-5	4	4 I	4	4 1	9	5	- - 	с 5	- - -	4 1	Ĩ 5	4	4	- - -
11	1 66	0	231.	231.	230.	230.	231.	231.0	231.	231.	231.	231.	231.	231.	231.	231.	231.	231.	D TN	1 66	o	223 .	223.	224.	224 .	224.	224.	224.	224.	224.	224.	224.	225.	225.	225.	225.	224.
TST	571	MACH	0.851	0.850	0.848	0.847	0.848	0.848	0.849	0.849	0.849	0.848	0.848	0.848	0.849	0.849	0.851	0.850	TST	571	MACH	0.796	0.798	0.799	0.799	661.0	0.799	0.801	0.801	0.801	0.801	0.801	0.802	0.803	0.802	C•802	0.801
RUN	306	SEC	-	2	m	4	ŝ	Ŷ	~	ω	6	10	11	12	13	14	15	16	RUN	307	SEQ		2	m	4	Ś	\$	2	80	σ	10	11	12	13	14	5	16

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..004 ..009 • 000 0 • 598 0 • 598 665*0 • 00 • 0.999 .008 .017 .011 • C04 **797** ..005 .007 .006 .014 .012 .000 •004 PF/D ...001 ..001 .001 .001 1.009 F/p .011 .013 012 -0.004 0.008 0.002 0.002 0.021 0.001 0.000 0.002 010-0 0.018 0.025 010.0 -0.007 0.016 0.021 -0.003 .028 0.008 0.009 0.024 0.030 0.002 -0.003 0.026 0.011 0.014 0.031 0.038 C V A /V V A / V VF/V 0.981 0.899 0.938 0.975 0.926 0.9256 0.899 0.893 0.893 0.893 0.893 0.892 0.888 0.916 0.916 0.963 0.969 0.897 0.893 0.887 0.895 0.892 VF/V 0.984 0.986 **U.** 983 0.896 0.966 .979 0.985 0.951 0.981 0.981 -10.00 ALPHA ALPHA -10.00 0A/Q OA/Q 0.974 0.935 0.819 0.982 GF/0 0.784 0.777 0.767 0.783 0.783 0.778 0.792 0.897 0.968 0.975 0.955 0.846 C.840 C.795 0.778 0.777 0.774 0.767 0.794 0.826 0.926 7.97 0.936 76.8 QF /0 779.0 176.0 0.822 010.070 0.963 0.979 SC5 MA/W 504 N/Vn ۵ C 769 226.1 /DB WF/W 225.7 MF/N 0.885 C.982 C.982 C.918 C.918 C.916 C.888 0.882 C.882 C.881 0.975 C-981 C-965 0.882 0.875 C. 888 536*0 0.904 0.886 0.884 C.880 C-9C3 0.945 0.962 0.979 0.876 C.893 0.907 C.97 C.978 C•984 0.98 C.755 1.513 769 X/CR Y/DP Z/CR C.87 -C.48 -2.C4 ( -2.03 -0.53 -1-53 -1.04 -0.71 -0-53 -0.38 0.29 0.46 -0.02 0.13 0.63 16.0 1.17 1.47 1.96 F d -1.03 0.31 0.48 0.65 85.0 Fo 69.0œ ch ω -0.04 Z / DB . 4 0.801 1.513 F WACH PN/L CCNF MACH PN/L 0.4 0.4 0.4 0.0 -0.48 -0.48 Y / D B -0-48 0.43 0.43 0.43 -0.48 -0.48 -0.48 -0.48 C+43 -0.48 -0.48 C.43 0.43 0.43 C+43 -0.48 -0.48 œ ω **6**00 -C.48 œ m -C.45 -0.48 -C.4 0.4 5-5 0.4 C • 4 0.4 X (7) X C 87 C.87 C.87 C.87 C 88 C 88 C 83 C.87 8•48 8•48 8 • 4 8 8 • 4 8 8 • 4 9 •49 • 49 • 49 C. 87 • 49 αÛ a. ഗ JNLU UNK 226.6 227.2 226.1 227.2 227.2 227.2 226.7 227.3 225.8 225.8 2255.7 2255.7 2255.7 226.1 226**.**1 225**.**6 226.7 226.7 227.2 226.6 226.6 227.2 227.2 226.8 226.8 226.8 226.8 m 226.8 226.1 226.2 1.2 226. -C **T**N 66 571 1 66 25 ۵. 571 1 ۵ MACH 551.0 0.49 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.803 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0.802 0 0.803 0.803 0.803 0.803 0.800 0.800 0.800 0.800 0.800 0.499 0.499 0.798 0.800 MACH 0.801 0.801 0.799 0.801 TST 800 801 TST ð . S F C 500 12 2 14 ഹ 21 14 310 SFQ 4 α 0 ŝ N 4 Ś ω G  $\subseteq$ ŝ N 3  $\mathbf{\sigma}$ Ś

		pr/p	1.008	1.007	1.005	1.000	166.0	0.596	1.000	0.598	1.000	1.001	0.999	1.000	1.000	666.0	1.003	1.012				p∈/p	1.012	1.009	1.008	1.003	0.598	166.0	0.998	<b>765.</b> 0	166.0	0.999	0.996	1.002	1.008	1.010	1.010	1.010
		d D	0.019	0.015	0.010	000000	-0.007	600.0-	0000.0	-0.004	-0.001	0.002	-0.002	-0.01	100.0	-0-001	0.007	0.027				C D	0.027	0.021	0.013	0.006	-0.003	-0.007	-0.005	-0.013	-0.007	-0.003	-0.010	0.005	0.018	0.021	0.021	0.023
		V / V /					·			ŗ	·		·									VA/V								-			·					
٩	0	VF/V	0.906	0.922	0.918	0.389	0.873	0.854	0.829	0.842	0.849	0.835	0.869	0.891	0.949	0.983	0.988	0.934		A	о О	VF/V	0.983	0.944	0.964	0.916	0.879	0.370	0.844	0.348	0.857	0.867	0.890	0.906	746.0	0.977	0.987	0.987
ALPH	-10.0	0 A V O																		ALPH	-10.0	0A/G																
11	77.2	0F/0	0.810	0.839	0.830	0.769	7.57.0	0.702	0.661	0.683	0-696	0.673	0.732	0.773	0.889	0.961	0.975	0.976	!	1 1	77.4	QF/0	974.0	C.974	0.929	0.824	0.749	0.732	0.686	069.0	0.709	0.727	0.767	0.804	619.0	0.958	0.979	0.980
۵.	507	WV/VN																		۵.	506	N/VN																
J	22.7.4	NF / N	3.896	51913	0.909	0.877	0.860	0.839	0.813	0.827	0.834	0.820	0.856	<b>c.</b> 875	0.943	0.981	3.986	3.982		ں	227.3	VF /N	186.0	3.982	096.0	106.0	3.866	0.857	3.829	0.833	0.843	<b>3.</b> 853	3.878	3-855	0.952	.974	3.985	3.985
١d	774	Z / DB	2.02	1.53	1.02 (	0.69 (	0.53 (	0.36 (	0.19	0.02 (	0.14 (	0.32 (	0.48 (	0.65 (	0.98 (	1.17 (	1.48	1.98 (	1	L d	772	2/08	2.02	1.52	1.03	0.65 (	0.52 (	0.36	0.19 (	0.03 (	0.14 (	3.31 (	0.48 (	3.64 (	0.98 (	1.17	1.48 (	1.58 (
PNL	1.521	/0 ^B	- 10-	- 10.	- 10-	- 10-	- 10-	•01 -(	- 10-	- 10 -	-01	•01	•01	• 01	-01	10.	•01	•01		FN/L	1.518	/ D.B	- 36 -	+ 900 •	- 36 -	- 36 -	- 36 -	• 36 -(	•36 -(	• 36 <u>-</u> [	• 36	• 36	• 36	•36	•36 (	- 36	• 36	96.
MACH	C.8CO	/08 \	- 64.	- 49 -0	.49 -0	- 49 -0	.49 -0	.48 -0	.48 -0	- 65.	.48 -0	.48 -0	.49 -0	.49 -0	.48 -0	.48 -0	•48 -0	• 48 -0		NACH	0.801	/CB Y	.48 -0	.48 -0	-48 -0	.48 -0	•48 -0	.48 -0	•48 -0	.48 -0	.48 -0	.48 -0	.49 -0	•48 -0	•48 -0	•48 -0	• 48 -0	.48 -0
CONF	<b>u</b> n	×	<b>4</b> 8	4 8	<b>4</b> 8	4 8	4 8	4 8	4	4 8	<b>4</b> 8	9 8	4 8	8	<b>5</b>	ς, Ω	8 8	7 8		CONF	ሆነ	×	en en	8	8 8	e B	<b>6</b> 0	3	3	3	8 8	8	е В	8	8 3	4 8	4 8	8 8
N H d	1 66	C T	227.	1 227.	227.	227.	227.	1 227.	227.	227.	1 227.	226.	226.	226.	1 226.	228.	5 228.	227.	-		1 66	0	. 227.	226.	1 226.	227.	227.	227.	227.	. 227.	226.	226.	1 226.	226.	. 226.	1 227.	226.	225.
IST	571	MACH	0.800	0.800	0.800	0.800	0.800	C. 800	0.800	0.800	0.800	0.795	151.0	0.795	552.0	0.804	0.805	0-804		TST	571	MACH	0.801	0.800	0.800	0.801	9-801	0.801	0.801	0.801	0.800	0-800	0.800	0.801	0.801	0.800	861.0	151.0
RUN	312	SFC	<b></b>	2	<b>m</b>	4	ŝ	9	2	α	σ	10	11	12	13	14	12	16		NUN	313	SEC	1	2	<b>(</b> 7)	4	ŝ	9		ຒ	6	10	11	12	13	14	12	16

	0F/D	1.015	1.013	1.006	1.006	0.999	1.997	0.996	0.993	1997	0.595	666.0	1.000	1.003	1.007	1.012	1.014			pF/p	1-004	1. CO4	1.005	1.004	1.000	1.001	1.002	666*0	1.001	1.003	1.001	1.003	1.003	1.004	1.005	1.004
	CP	0.035	0.030	0.013	0.013	-0.002	-0.07	-0.009	-0.015	-0.097	-0.011	-0.002	-0-001	0.007	0.015	0.026	0.030			ď	0.018	0.018	0.013	0.015	0.002	0.006	0.007	-0.003	0.004	0.014	0.003	0.014	0.013	0.018	0.019	0.016
	V A / V																			V A / V																
٩c	VF/V	0.981	0.982	0.971	0.915	0.332	0.865	0.365	0.867	0.365	0.869	0.895	0.911	0.961	0.978	0.985	0.981	٨	0	VF/V	0.989	0.985	0.966	0.920	0.925	0.921	0.912	0.914	0.907	0.906	0.920	0.926	0.955	0.972	0.985	0.991
ALPH -10-0	0 A / Q																	Ηdη	-10.0	0 A / Q																
77.6	0140	0.973	0.973	0.941	0.824	0.755	0.722	0.721	0.724	0.723	0.729	0.781	0.811	0.917	0.958	0.977	179.0	11	76.5	CF/0	0.980	0.972	0.934	0.840	0.845	0.841	0.824	0.825	0.814	0.814	0.837	0.852	0.909	0.945	0.974	0.984
р 507	M / M																	۵.	118	M A / W																
C 226.0	N L L N	516.0	0.980	0.967	206.0	C.870	0.851	0.851	0.854	0.852	0.856	0.884	106.0	C.956	C.976	0.983	516.0	C	182.4	NF / N	0.988	0.984	0.964	0.915	C.920	0.916	C.907	0.908	0.902	0.901	0.914	0.922	C.952	010.0	C. 984	066.0
L PT	2/08	-2.03	-1.46	-1.03	-0.69	-0.52	-0-35	-0.19	-0.02	0.14	0.31	0.48	0.65	0.98	1.17	1.48	1.98	LpT	1 918	Z/08	-2.05	-1.54	-1.04	-0.70	-0.54	-0-37	-0.21	-0.04	0.13	0.29	0.46	0.64	0.96	1.16	1.46	1.97
H PN/ 9 1.51	Y/DB	-0.45	-0-45	-0.45	-0.45	-0-45	-0-45	-0.45	-0.45	-0-45	-0-45	-0.45	-0.45	-0-45	-0.45	-0.45	-0.45	H RN/	2 1.52	Y/08	0.41	0.41	0.41	C.41	0.41	0.41	0.41	0.41	0.41	C.41	0.41	0.41	0.41	0.41	0.41	0.41
F NAC 5 0.79	X/LB	8•48	8*48	8•48	8•48	8•48	8 • 48	8+48	8 • 48	8,48	E.48	8.48	8.48	8•48	8.48	£•48	8•48	F VAC	5 0.60	X / DB	10.87	10.87	10.87	1 C . 87	10.87	1C.87	10.87	10.87	10.87	10.87	10.87	10.87	10.87	1C•87	10.87	1 C • 87
TN CON	0	26.9	26.9	26.9	26.5	26.4	26.8	26.8	26.8	27.3	27.3	27.8	27.8	27.8	27.8	27.3	27.3	TN CON	66	C	82.4	82.4	82.4	81.8	81.2	81.2	81.2	81.2	81.2	81.2	81.2	81.2	81.2	81.2	81.8	81.8
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MACH	.799 2	• 799 2	5 661.	.799 2	.758 2	.800 2	.800 2	.800 2	.801 2	.801 2	.803 2	.803 2	.803 2	.803 2	.802 2	.802 2	TST P	571 1	MACH	.602 1	.602 1	.602 1	.601 1	•600 1	•600 1	• 600 1	.600 1	• 600 1	•600 1	•600 1	.600 1	•600 L	• 600 1	.601 1	•601 1
AUN 314	SEQ	1 0	2 0	30	4	50	60	2 0	8	06	10 0	11 0	12 0	13 0	14 0	15 0	16 0	RUN	315	SEQ	1 0	2 0	9	4	C S	60	7 0	8	06	10 0	11 0	12 0	13 0	14 0	150	16 0

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		1.005	1.003	1.002	1.001	1.002	1.002	1.001	0.999	1.001	1.002	666.0	1.001	1.002	1.002	1.004	1.005			bF/p	1.008	1.005	1.003	1.002	1.001	0.9999	1.002	1.000	0.598	1.001	1.001	1.000	1.002	1.003	1.C04	700-1
	c (	0.018	0.014	0.008	0.003	0.006	0.010	0.003	-0-003	0.002	0.008	-0.003	0.004	0.010	0.006	0.015	0.022			C b	0.032	0.022	0.014	0.006	0.005	-0.003	0-006	-0.002	-0.007	0.002	0.004	-0.002	0.006	0.013	0.018	0.076
		A 1 4 A																		V A /V																
ALPHA	-10.00	U.926	0.937	0.926	0.899	0.894	0.884	0.888	0.894	0.384	0.905	0.907	0.921	0.953	0.960	0.985	066 • 0	ALPHA	-10.00	0A/Q VF/V	0.982	0.985	0.960	0.921	0.903	0.903	0.892	0.901	0.893	0.902	0.915	0.920	0.955	0.974	0.983	0.986
11	76.1	0.853	C.872	c.850	797.0	0.788	0.771	0.778	0.787	0.770	C.810	0.812	0.839	0.904	0.919	0.972	0.983	ŢŢ	76.1 -	0F/0	176.0	0.974	0.920	0.841	0.805	0.804	0.786	0.800	0.784	0.804	0.831	0.836	106.0	0.947	0.968	0.976
٩	617 1																	a	719	W/VW																
3	181.8	0.921	<b>C.9</b> 32	C.921	C.892	0.887	0.877	<b>C.</b> 882	C.888	C.877	C.899	0.902	C.916	0.945	0.958	C.984	0.989	<del>ن</del>	182.4	NL/N	C.981	C.984	0.958	c.916	0.897	1.857	0.886	0.894	C.886	0.896	0.911	<b>C.915</b>	0.952	0.972	<b>C.</b> 982	0.985
L PT	0 518	-2.04	-1.54	-1.05	-0.71	-0-54	-0.38	-0.20	-0.03	0.14	0:30	0.47	0.63	0.98	1.16	1.46	1.96	L pT	3 518	2708	-2.04	-1.54	-1.05	-0.71	-0-54	-0.38	-0.20	-0.04	0.13	0.30	0.46	0.63	0.96	1.17	1.47	1.96
H RN/	1 1.52	-0.03	-C.03	-0-03	-0.03	-0.03	-0.03	-0-03	-0.03	-0.03	-0.03	-0-03	-0.03	-0.03	-0-03	-0.03	-0.03	H RN/	2 1.52	Y/CB	-0.38	-0-38	-0.38	-0.38	-0-38	-0.38	-0-38	-0.38	-0.38	-0-38	-0.38	-0-38	-0.38	80.01	-0-38	96-0-
	5 U.6U	10.87	10.87	10.87	1C. 87	10.87	10.87	10.67	10.87	10.87	10.87	1C.87	10.87	1 C • 87	10.87	1C.87	10.87		5 0.60	X/CP	10.87	10.87	1 C. 87	10.87	1 C • 87	10.87	10.87	1 C • 87	10.87	10.87	10.87	10.87	10.87	1C.87	1C.87	1C_ P7
TN CCP		181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	TN CCM	66	G	182.4	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.6	181.8	181.8	181.8	181.8	181.8
TST P		0.601	0.601	0.601	0.601	0.601	0.601	C.6C1	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	TST P	571 1	MACH	0.602	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601	0.601
NUA V		8 <b>—</b>	2	n	4	In.	Ŷ	٢	တ	<del>о</del>	10	11	12	13	14	<u>لار،</u>	16	КUN	317	SEQ		2	<b>ה</b> ש	4	<b>u</b> n	9	•	ထ	9	10	11	12	61	4	1 1	16

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1.005 1.006 1.002 1.000 1.002 pF/p 1.006 1.004 1.005 1.002 1.002 1.004 1.003 1.001 . 002 666.0 1.001 I. C03 1.001 1.000 1.002 1.006 1.000 1.002 1.004 1.005 1.004 OF/D 1.001 0.999 1.003 1.004 1.001 L. C04 0.019 0.008 0.010 0.013 0.025 0.023 0.010 0.003 0.020 0.018 0.007 0.006 0.019 -0.002 100.0-0.005 0.002 0.018 -0.004 0.010 0.015 0.016 110.0 0.016 -0.001 0.004 0.007 e. V A /V V A /V 0.914 0.899 0.903 0.962 VF/V 0.990 0.982 0.956 0.990 0.922 0.920 0.903 0.915 0.903 0.908 0.912 0.919 VF/V 0.978 0.980 0.901 0.965 186.0 166.0 0.985 0.931 0.901 0.906 0.883 0.903 0.928 0.958 0.992 -10.00 ALPHA ALPHA -10.00 0 A V O 0 A / O 75.8 QF/0 0.968 75.4 0F/0 0.914 0.807 0.985 0.829 0.808 0.804 0.817 0.824 0.920 0:630 0.965 0.956 0.810 0.984 0.860 0.770 0.804 0.827 C.798 0.802 0.835 0.854 0.913 0.961 0.985 0.986 0.974 0.843 0.339 0.982 0.801 611 716 MA/W W / M ۵. ۵ 912 179.3 /DB MF/W 918 181.8 MF/N C.981 C.9C8 0.857 0.913 C-984 C-584 C-577 0.989 C.953 0.853 C-897 558-0 0.903 906-0 C.980 C.927 C.915 0.895 0.877 0.897 0.955 C.917 C.924 0.962 0.989 006-0 0.897 506*0 C.9555 9.978 156.0 C.99] -0.53 -1.55 0.25 0.43 -2.03 -1.03 X/CB Y/DP Z/CB -0.48 -2.04 -0.48 -1.55 0.12 0.47 .47 0.14 0.48 **C.** 58 -0.38 0.63 0.96 .17 Z/08 10 -0.54 -0.04 0.65 -0.71 -0.21 -1.52 -0.35 -0.18 -0.02 0.31 6. 1.99 1.18 • 4 5 0.601 1.521 5 0.598 1.508 RN/L NACH PN/L -0.48 -0.48 -0.48 -C.48 0.43 0.43 -0.48 -0.48 Y/DP 0.43 0.43 -0.48 -0.48 -0.48 -C.48 -0.48 -C.48 -0.48 -C.48 64.0 C.43 0.43 0.43 0.43 C - 43 C • 43 .43 0.4 VACH IC.87 10.87 C.87 C.87 C . E7 C . B7 C . 88 X/DR 1 C . 87 1 C. 88 **C •** 88 **C.** 88 C. 87 10.87 C. 87 C. 88 8.49 8.49 8.49 8•49 8•49 C.87 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 8.49 **JUDU** TA CONF 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 181.8 179.5 181.8 181.8 5.971 2.99.5 179.5 179.3 179.5 79.5 5.971 179.9 179.5 179.9 179.3 131.8 79.5 79.3 σ 179. N L C 571 1 66 66 C ٥ TST P 571 1 MACH 0.6C1 0.6C1 MACH 0.601 0.555 0.558 0.558 0.558 0.559 0.559 0.601 0.601 0.601 0.601 0.601 0.601 0.601 0.601 0.558 0.599 0.599 0.601 0.601 0.595 599 0.601 0.601 0.601 0.599 0.559 599 599 TST 53 0 . . • RUN 318 SFC  $\sim$ n) 4 **u**n 9 ~ œ 0 11 21 2 σ 4 **u**n RUN 319 SEC J ഹ 0 9 ω σ 12 13 14 51 9

		pF∕p	• 004	.003	• 002	.002	666.	665.	. 998	. 598	• 000	.998	665 •	• 000	.001	.002	• 004	.003				bE/D	- 003	-004	.001	100.	.002	.001	. 598	. 598	866.	• 002	. 999	.000	• CO3	•006	.006	• 005
		СЪ	0.018 1	0.012 1	0.010	0.006 1	-0.002 0	-0.004 0	0 600.0-	0 600-0-	1 100.0-	0 600.0-	-0.004 0	0.000 1	0.003 1	1 010.0	0.015 1	0.013 1				ۍ C	1 510.0	0.017 1	0.006 1	0.004 1	0.010 1	0.005 1	0.008 0	-0.006 0	-0.008 0	0.009	-0.004 0	0.001 1	0.014 1	0.023 1	0.022 1	1 610.0
		V A /V						•														VA/V																
VLPHA	10.00	0A/Q VF/V	0.921	0.933	0.933	0.893	0.879	0.801	0.860	0.858	<b>U</b> •366	0.874	0.835	0.902	0.946	0.981	0.986	0.990		ALPHA	10.00	CA/U VF/V	0.988	0.986	0.909	0.916	0.890	0.871	0.873	0.868	0.809	0.873	006*0	0.913	0.963	0.975	J. 985	0.438
11	75.4 -	QF /0	0.842	0.865	0.864	0.787	<b>C.7</b> 59	0.727	0.724	0.722	0.737	C.750	0.771	0.803	0.889	0.962	0.974	0.983		11	75.4 -	0F/0	0.978	C.975	0.936	0.830	0.783	0.747	0.749	0.738	0.741	0.752	0.798	0.824	0.925	C.953	0.973	0.980
۵	716	MA/W																		<b>D</b> .	716	MA/M																
y	E-971	NL /N	0.916	3.928	3 <b>.</b> 92£	3.887	2.871	3.853	<b>c.</b> 852	C.85C	0.858	0.867	c.879	3.856	0.942	0.980	3.985	056.0		ى ع	179.9	NF/N	C.987	C.985	0.967	010.0	3.884	C. 864	0.866	c.860	0.862	3.866	0.854	C.9C7	0.960	0.973	3.984	C.987
μ	216	Z/DB	2.02	1.53	1.02	0.70	0.52 (	0.36	0.19	0.02 (	0.14 (	0.31 (	0.48	0.64	86.0	1.17	1.48	1.98		b	515	2/DB	2.03	1.53	1.03	59.0	0.53	0.35	0.19	0.03	0.14	0.32	0.48	0.65	0•58	1.15	1.48 (	1.98
RN/L	1.508	UCB	.01 -	- 10.0	- 10-0	- 10.0	- 10.0	- 10-0	0.01 -	- 10.0	0.01	0.01	10.0	10.0	10.0	0.01	0.01	10.01		RN/L	1.511	1/EB	0.36 -	0.36 -	0.36 -	3+36 -	0.36 -	0.36 -	0.36 -	0-36 -	0.36	0.36	3.36	0.36	36	0.36	36	9.90
NACH	0.558	(/CB )	- 65.	- 65 -(	- 49 -(	)- 65*	- 65-	• 49 -(	- 65 -(	- 65 - (	- 49 -(	- 65.	- 65 - (	- 64 -(	- 65 -(	• 49 -(	- 65 - (	- 65-1		X A C H	0.559	(/CB	- 65 - 6	- 65 - 6	9-49-(	- 65 - (	- 64•	- 65 - (	• 49 -(	.48 -(	- 48 -(	• 48 -(	.48 -(	.48 -(	.48 -(	•48 -(	- 65.	• 49 - (
CONF	ŝ	×	<b>6</b>	<b>m</b>	60 61	<b>m</b>	с. Ф	e G	<b>6</b> )	3	сл Ф	5 2 2	e B	<b>m</b>	<b>m</b>	<b>6</b>	<b>6</b>	8			<b>u</b> n	•	в 6-	ŝ	8 5	ŝ	۳ ۳	ω. 	6 6	ω σ	<b>m</b>	ω S	с С	<b>5</b>	ۍ ۵	S S	ພ	ŝ
P TN	l 66	С Н	E 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	8 179.	6 179.	i	d T	1 66	с Ч	5 179.	0 180	641 5	0 180.	0 180.	C 180.	6116	6 179.	8 179	6 1 1 9	5 I79.	6 179	C 18C.	6116	0 180.	0 180.
151	571	MAC	0.59	0.55	0.59	0.55	0.59	0.55	0.59	0.59	0.55	0.59	0.59	0.59	0.59	0.55	0.59	0-55		ISI	571	MAC	0.55	0.60	0.55	0.60	0•60	0.60	C• 59	0.55	0.59	0.55	0.59	0.59	0• 60	0.59	0.60	0.60
RUN	320	SFC	-	<b>r</b> :	ŝ	4	ŝ	9	-	œ	6	10	11	12	13	14	15	16		R C N	321	SEQ		2	<b>m</b>	4	LC.	\$		œ	5	10		12		41		16

1.003 1.002 • 006 666*0 r /p 1.001 799.0 .006 .005 • 003 .000 .002 DF/D 0.999 0.999 .001 .001 .005 666 0.598 0.998 1.000 665.0 665.0 665.0 665.0 665.0 666.0 666.0 0.599 665.0 666.0 0.999 0.999 -0.006 -0.024 -0.024 -0.024 0.007 0.001 0.022 0.025 0.014 0.004 -0.008 -0.002 700.0 0.022 0.022 -0-014 -0.014-0.024 -0.024 -0.024 -0.024 -0.024 -0.015 -0.015 -0.019-0-019 -0.019 -0-019 0.012 0. 0C0 0. 0C0 0.000 0. 0CC 0. 0CC 000 0.000 V A /V 0.000 0.000 0.000 0.000 0.000 0.000 0.000 000.000 V A / V 0.998 0.956 993 0.919 0.882 0.880 0.900 0.903 0.929 0.389 0.985 0.939 0.930 0.914 0.924 0.938 0.967 0.984 0.891 0.989 0.987 VF/V 0.995 0.942 0.983 VF/V **3.**984 0.988 0.969 0.885 0.926 964 0.969 0.995 -10.00 -10.00 ALPHA ALPHA 0.000 0 A / O c. 000 0.00.0 04/0 000.000 000.0 000.0 0.000 c. 000 0.000 0.00.0 C-000 0.000 000.0 0.000 c.000 0.996 0.968 C.886 0.879 0.912 C.972 0.980 0.938 0.835 0.780 0.767 0.798 0.805 0.926 CF/O 0.834 75.4 0.761 0.779 72.8 0.861 0.989 994 0F70 176.0 0.989 0.863 0.877 0.934 0.967 0.965 0.848 0.851 0.772 0.979 16 0000.0 0.000 0000.0 0.000 00000 0.000 000 716 000.000 0.00.0 0.000 0.000 WA/N 79.5 1829 NV VW 0.000 0.000 0.000 0.000 ۵ 0 913 186.5 C.985 0.983 C.938 0.955 C.937 0.967 0.875 0.873 0.894 0.878 **256**.0 C.925 956 NF / N £86.0 199.0 0.882 0.921 とくよう 356.0 0.942 C.930 C10.0 C.923 C.967 C. 955 C.913 0.584 C.884 0.897 C.967 0.988 C.961 5.98 L 0.249 1.502 1910 -0.69 0.14 0.48 1.98 -0.54 0.29 0.65 0.98 •48 0.12 0.46 X/UB Y/UE Z/UE 8.49 -0.45 -2.03 -0.19 0.30 1.18 -1.53 -0.71 0.63 0.96 l.46 -1.52 -1.03 -0.02 -2.05 -0.20 •17 **79.** L d -0.36 Y/NB Z/DB -1.04 -0.04 F a PN/L RN/L 0.600 1.514 -0.45 -0-45 -0-45 -0+45 0.41 -0-45 -0-45 .41 0.41 -0-45 -0.45 -0-45 -C.45 -0-45 -0-45 -0.45 .41 14. .41 .41 14. .41 .41 .41 .41 .41 -0-45 .4] -0-4 • 4  $\mathbf{C}$ MACH NUCH 8.49 8.49 • 49 .49 •49 •49 8.49 8.49 8.49 •49 8.49 • 49 C 87 C 88 C 87 C 87 C 87 C. 88 C. 88 8.49 8.49 • 49 C . 87 C.87 X/08 0.87 C.87 0.87 C.87 C. 88 C•88 C•88 0.88 œ œ œ a  $\alpha$ ഹ ŝ TN CONF P TN CONF 180.5 179.9 179.3 80.5 179.9 179.9 179.9 181.1 181.1 80.5 180.5 79.5 2°62 79.5 181.1 180.5 79.5 79.5 2.61 2.91 79.5 79.5 79.5 79.5 80.5 79.5 С 66 C 571 1 66 STP 571 1 0.600 0.598 C.6CC 0.599 MACH 0.599 0.599 MACH 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.249 0.599 0.599 0.601 0.600 0.600 0.249 0.599 0.600 0.600 0.249 0.249 0.249 49 0.601 0.601 0.249 TST . 12 2 323 SEQ RUN 322 SFQ 450 10 2 15 3 œ σ NUN SON 00 <u>o</u> N m st <u>_</u> 4 2 9

## ORIGINAL PAGE IS OF POOR QUALITY

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NUA	TST p		L L	N A CH	RN/	L PT	U	۵.	11	VLPH/				
324	571 1	66	о N	•249	1.50	3 191	. 61 0	5 1829	72.5	-10.00	~			
SEQ	MACH	Ç	×	5.0	118	Z / DB	NL / N	W/ AN	0F/0	0 A / O	VF/V	V A / V	d C	bF∕p
	0.249	2°51	1 C • 1	87 -(	0.03	-2.04	0.949	000 * 0	0.899	c.000	0.949	0.000	-0.019	0.999
2	0.250	80.2	10.	87 - (	0.03	-1-54	C.951	0.000	0.904	0.000	0.952	0.000	-0.015	666.0
m	0.249	79.5	10.	87 -(	•03	-1.04	C-933	0.000	C.870	c.000	0.934	0.000	-0.024	0.999
4	0.249	5*52	10.	87 -(	0.03	-0.71	506*0	0.000	0.825	000.0	016.0	0.000	-0.024	666*0
Ś	0.249	79.5	10.1	87 -0	0.03	-0-54	C.892	0.000	0.796	0.000	0.893	0.000	-0.024	666.0
\$	0.249	2.97	- C -	87 -(	0.03	-0.38	C.893	000.0	797.0	0.000	0.894	0.000	-0.024	665*0
-	0.249	79.5	10.	87 -(		-0.21	C.889	0.000	0.790	c.000	0.891	0.000	-0.024	666.0
ω	0.249	79.5	10.	87 -C	.03	-0.03	0.904	000000	0.816	0.000	0.905	0.000	-0.024	0.999
¢	0.249	79.5	10.	87 - (	03	0.13	0.905	000000	0.818	000.0	0.906	000.0	-0-024	666.0
01	0.250	80.2	10.	87 -0	50°C	0.29	C.9C8	0.000	0.825	c.000	0.909	0.000	-0-015	0.999
11	0.250	80.2	10.	87 -(	- C3	0.46	C.906	0.000	0.820	0.00.0	0.907	0.000	-0.010	1.000
12	0.250	80.2	10.	87 -(	0.C3	0.63	C.937	0.000.0	0.978	0.00.0	0.938	0.000	-0.024	0.999
13	0.250	80.2	-01	87 –C	0.03	0.96	0.546	000.0	0.893	0.000	0.946	0.000	-0.024	665 •0
14	0.250	80.2	10.	87 -(	0.03	1.16	0.973	0.000	0.946	C. 000	0.974	0.000	-0.021	666.0
15	0.250	80.2	10.	87 -0	0.03	1-46	0.988	0.000	0.976	0.00.0	0.988	0.000	-0.019	666.0
16	0.249	79.5	10.	87 -(	0.03	1.57	1.004	000.0	1.006	0.000	1.004	0.000	-0.019	0.999
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RUN	TST p	TN CC	L N F	NACH	RN/	L b L	ى	D	11	ALPHI	4			
325	571 1	66	0 40	•245	1.50	161 4	1 79.	5 1830	72.1	-10.00				
0 Li S	MACH	C	/ ×	CR	109	Z/CB	NF / N	n/Vn	0F70	0A/C	VF/V	V A /V	٥	pr/p
ga-4	0.249	79.5	10.	87 -(	0.38	-2.05	455 ° J	0.000	0.987	C. 000	<b>964</b>	0.000	-0.014	666.0
~	0.248	78.8	10.	87 -(	3.38	-1.54	856*0	0.000	0.996	0.000	0.998	0.000	-0.017	0.599
61	0.248	78.8	10.	87 -(	0.38	-1.04	C.948	00000	0.898	0.000	0.949	0.000	-0.024	665.0
4	0.249	2.9T	10.	87 -(	C• 38	-0.71	C.922	0.000	0.849	C. UOD	0.923	0.000	-0.024	666*0
n	0.249	2*62	10.	87 -(	3.38	-0-54	0.895	0.000	0.808	0.000	0.900	0000.0	-0.024	0.999
9	0.248	78.8	10.	87 -(	3•38	-0.37	C• 891	0.000	0.794	<b>c.</b> 000	0.892	0.000	-0.024	666.0
-	0.249	79.5	10.	87 -(	3•38	-0-20	C.905	0.000	0.818	c. 000	0.906	0.000	-0.024	0.999
æ	0.245	19.5	10.	87 -(		-0.04	C.91C	0.000	0.827	0.000	0.911	0.000	-0.024	666.0
6	0.248	78.8	-01	87 -(		0.13	0.915	0.000	0.836	c.000	0.916	0.000	-0-024	666 0
10	0.248	78.8	10.	87 -(	3.38	0.29	0.915	0.00	0.836	0.00.0	0.916	00000	-0.024	0. 599
11	0.249	79.5	10.	87 -(		0.47	C.919	0.000	0.844	c.000	0.920	0.000	-0.024	0.999
12	0.249	<b>19.5</b>	10.	87 -(	9.38	0.63	0.931	0.000	0.867	000.0	0.932	0.000	-0.015	0.999
2	0.248	78.8	10.	87 -(	3•38	0.96	<b>C.</b> 96 <b>C</b>	0.000	0.921	0.000	0.961	0.000	-0.033	0.9999
14	0.249	79.5	10.	87 -(	3.38	1.17	C 8 5 8 3	0.000	0.965	C. UOO	0.983	0.000	-0.010	1-000
15	0.249	5-51	10.	87 -(	3.38	1.47	0.587	0.000	0.974	0.000	0.987	0.000	-0.010	1.000
16	0.249	19.5	10.	87 –(	3.38	1.56	255*0	0.000	0.984	0.00.0	0.992	0.000	-0.014	665.0

• 000 0.9999 0.9999 665 .000 666. 666 665 .999 665 .999 665 665 665.0 0.999 . 5 . . 6 . • 0 0  $\mathbf{o}$ 00 C -0.026 -0.015 -0.021 -0.014 -0.024 -0.001 -0.015-0-015 -0-015 -0.008 -0.024 -0.024 -0.015-0.024 6 A / V 0 0 0 0 000 0000 0000 000 000 000 0000 0 ं 00000 • 0 000 0 0 • > 0.988 0.979 0.979 0.926 0.921 0.921 0.921 0.927 0.945 0.959 988 979 0.982 VF/V 779 994 1.001 • • 4 -10.00 c. 000 c. 000 c. 000 AL PH 0.975 0.957 0.957 0.844 0.844 0.851 0.851 0.838 0.838 0.838 0.857 0.953 0.953 1.001 0.987 72.0 0F/0 840 918 00 р 1829 МД/ч 0000-0 0.000 80.2 WF/W 0.988 C.978 C-977 C-982 C-954 C-954 ç 5 0•959 045 MACH PN/L PT 0.250 1.512 1911 X/DB Y/DB Z/DB 7 0.87 -0.48 -2.04 0 0.87 -0.48 -1.54 0 -1.54 -1.04 -0.71 -0.54 -0.37 -0.04 0.12 0.25 0.47 0.47 0.47 0.63 0.63 0.63 1.17 1.17 Š, œ -0.48 œ ω ωωω Ø ω  $\infty \infty$ ဆဆ -0-45 -0-48 -0-48 -C.48 -0.48 -0-48 -0.48 -C-41 4 . 0 X
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8.49       -0.01       -0.317       0.000       0.931       0.000       -0.948       0.000       -0.012         8.49       -0.01       -1.53       0.344       0.000       0.344       0.000       -0.012         8.49       -0.01       -1.53       0.344       0.000       0.345       0.000       0.345       0.000       -0.012         8.49       -0.01       -0.53       0.317       0.000       0.756       0.000       0.345       0.000       -0.024         8.49       -0.01       0.387       0.000       0.756       0.000       0.387       0.000       -0.024         8.49       -0.01       0.387       0.000       0.756       0.000       0.384       0.000       -0.012         8.49       -0.01       0.35       0.377       0.000       0.756       0.000       0.397       0.000       -0.012         8.49       -0.01       0.376       0.000       0.376       0.000       0.376       0.000       -0.012         8.49       -0.01       0.377       0.000       0.394       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000	Ø		X/CB	1/0	<u>a</u> n	Z/08	N L N	M / M	CF/Q	OA/O	VF/V	V A /V	d C	DF/D
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<pre>E 6.49 -0.01 -1.03 C.914 0.000 0.834 0.000 0.914 0.000 -0.024 E 4.9 -0.01 -0.53 C.817 0.000 0.756 0.000 0.868 0.000 -0.012 E 4.9 -0.01 -0.53 C.817 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.756 0.000 0.871 0.000 -0.012 E 4.9 -0.01 0.877 0.000 0.775 0.000 0.871 0.000 -0.012 E 4.9 -0.01 1.48 0.998 0.000 0.975 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.48 0.998 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.48 0.998 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.48 0.998 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.48 0.998 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.58 0.572 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.01 1.58 0.572 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.36 -1.53 0.591 0.000 0.992 0.000 0.992 0.000 -0.012 E 4.9 -0.36 -1.53 0.591 0.000 0.992 0.000 0.991 0.000 -0.012 E 4.9 -0.36 -1.53 0.591 0.000 0.983 0.000 0.991 0.000 -0.012 E 4.9 -0.36 -0.130 0.991 0.000 0.912 0.000 0.991 0.000 -0.012 E 4.9 -0.36 -0.130 0.991 0.000 0.912 0.000 0.991 0.000 -0.012 E 4.9 -0.36 0.147 0.000 0.913 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.000 0.913 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.931 0.000 0.922 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.773 0.000 0.924 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.993 0.000 0.912 0.000 0.924 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.913 0.000 0.924 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.910 0.912 0.000 0.924 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.910 0.912 0.000 0.924 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.912 0.000 0.924 0.000 0.914 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.910 0.912 0.000 0.924 0.000 0.914 0.000 -0.012 E 4.9 -0.36 0.147 0.910 0.917 0.910 0.912 0.000 0.914 0.000 0.914 0.000 0.010 E 4.9 -0.</pre>	-62		8.49	0.01		1.53	0.947	0.000	0.896	0.000	0.948	0.000	-0.019	0.999
E .49 -C.C1       -C.C5 C .000 0.895 0.000 0.817 0.000 -0.024         E .49 -C.C1       -C.10 -0.55 C .876 0.000 0.817 0.000 -0.024         E .49 -C.C1       -C.11 -0.56 C .877 0.000 0.817 0.000 -0.024         E .49 -C.C1       0.15 C .817 0.000 0.756 C.000 0.817 0.000 -0.024         E .49 -C.C1       0.15 C .817 0.000 0.756 C.000 0.817 0.000 -0.024         E .49 -C.C1       0.15 C .817 0.000 0.756 C.000 0.817 0.000 -0.021         E .49 -C.C1       0.17 C .877 0.000 0.756 C.000 0.817 0.000 -0.011         E .49 -C.C1       0.17 C .877 0.000 0.917 0.000 0.817 0.000 -0.012         E .49 -C.C1       0.17 C .975 0.000 0.917 0.000 0.918 0.000 -0.012         E .49 -C.C1       0.17 C .975 0.000 0.918 0.000 0.918 0.000 0.918 0.000 -0.012         E .49 -C.C1       0.17 C .975 0.000 0.991 0.000 0.918 0.000 0.918 0.000 0.000         E .49 -C.C1       0.14 C .975 0.000 0.991 0.000 0.992 0.000 -0.012         E .49 -C.01       1.48 0.976 0.000 0.991 0.000 0.992 0.000 -0.012         E .49 -C.21       0.51 0.970 0.991 0.000 0.991 0.000 0.914 0.000 0.024         E .49 -C.25       0.900 0.983 0.000 0.983 0.000 0.991 0.000 0.024         E .49 -C.25       0.900 0.991 0.900 0.991 0.000 0.991 0.000 0.914 0.000 0.991 0.000         E .49 -C.26       0.900 0.991 0.900 0.991 0.000 0.991 0.000 0.914 0.000 0.991 0.000         E .49 -C.26       0.900 0.991 0.900 0.991 0.0000 0.914 0.000 0.991 0.000	-61	<b>B</b> CA	8.49	-0-0		1.03	0.914	0.00.0	0.834	0.000	0.914	0000-0	-0.024	665.0
<pre>8.49 -0.01 -0.53 C.875 0.000 0.766 0.000 0.877 0.000 -0.024 8.49 -0.01 0.877 0.000 0.756 0.000 0.878 0.000 -0.024 8.49 -0.01 0.877 0.000 0.756 0.000 0.878 0.000 -0.024 8.49 -0.01 0.33 0.877 0.000 0.756 0.000 0.874 0.000 -0.015 8.49 -0.01 0.33 0.877 0.000 0.756 0.000 0.894 0.000 -0.015 8.49 -0.01 0.33 0.877 0.000 0.776 0.000 0.894 0.000 -0.015 8.49 -0.01 1.48 0.978 0.000 0.776 0.000 0.894 0.000 -0.015 8.49 -0.01 1.48 0.978 0.000 0.776 0.000 0.992 0.000 -0.015 8.49 -0.01 1.48 0.988 0.000 0.977 0.000 0.992 0.000 -0.015 8.49 -0.01 1.48 0.988 0.000 0.977 0.000 0.992 0.000 -0.015 8.49 -0.01 1.48 0.988 0.000 0.977 0.000 0.992 0.000 -0.015 8.49 -0.01 1.48 0.988 0.000 0.992 0.000 0.992 0.000 0.002 8.49 -0.01 1.48 0.989 0.000 0.992 0.000 0.992 0.000 -0.025 8.49 -0.36 -1.53 0.991 0.000 0.992 0.000 0.992 0.000 -0.015 8.49 -0.36 -1.63 0.910 0.992 0.000 0.992 0.000 -0.025 8.49 -0.36 -0.69 0.914 0.000 0.992 0.000 0.992 0.000 -0.015 8.49 -0.36 -0.69 0.914 0.000 0.992 0.000 0.991 0.000 -0.012 8.49 -0.36 -0.69 0.910 0.993 0.000 0.992 0.000 0.000 0.902 0.000 8.49 -0.36 -0.03 0.983 0.000 0.983 0.000 0.991 0.000 -0.012 8.49 -0.36 -0.19 0.000 0.983 0.000 0.994 0.000 -0.012 8.49 -0.36 0.149 0.000 0.983 0.000 0.914 0.000 0.914 0.000 -0.012 8.49 -0.36 0.140 0.990 0.766 0.773 0.000 0.944 0.000 -0.012 8.49 -0.36 0.190 0.918 0.000 0.914 0.000 0.914 0.000 -0.012 8.49 -0.36 0.190 0.916 0.773 0.000 0.924 0.000 -0.012 8.49 -0.36 0.140 0.900 0.765 0.791 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.900 0.765 0.000 0.914 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.900 0.765 0.000 0.914 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.000 0.765 0.000 0.914 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.900 0.765 0.000 0.914 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.970 0.918 0.000 0.914 0.000 0.914 0.000 -0.012 8.48 -0.36 0.914 0.000 0.916 0.797 0.000 0.914 0.000 0.012 -0.012 8.48 -0.36 0.914 0.000 0.755 0.000 0.914 0.000 0.914 0.000 0.012 -0.012 8.48 -0.36 0.914 0.900 0.755 0.000 0.994 0.000 0.000 0.012 -0.012 8.48 -0.36 0.914 0.900 0.755 0.000 0.</pre>	-61	u۱	8.49	0.0-	T	0.69	0.894	000.0	0.799	c• 000	0.895	0.000	-0.024	666.0
8.49 -C.CI -0.36 C.867 0.0759 C.750 C.000 0.868 0.000 -0.024 8.49 -C.CI -0.19 0.877 0.000 0.768 0.000 0.878 0.000 -0.017 8.49 -C.CI 0.15 C.877 0.000 0.756 0.000 0.871 0.000 -0.017 8.49 -C.CI 0.47 C.895 0.000 0.756 0.000 0.897 0.000 -0.017 8.49 -C.CI 0.47 C.895 0.000 0.992 0.000 -0.017 8.49 -C.CI 1.17 C.976 0.000 0.992 0.000 -0.015 8.49 -0.01 1.48 0.988 0.000 0.992 0.000 -0.012 8.49 -0.01 1.51 C.976 0.000 0.992 0.000 -0.012 8.49 -0.01 1.51 C.976 0.000 0.992 0.000 -0.012 8.49 -0.01 1.51 C.976 0.000 0.992 0.000 0.992 0.000 8.49 -0.01 1.51 C.976 0.000 0.992 0.000 0.992 0.000 8.49 -0.01 1.51 C.914 0.000 0.992 0.000 0.992 0.000 8.49 -0.35 0.911 0.000 0.992 0.000 0.992 0.000 8.49 -0.36 0.52 C.500 0.912 0.000 0.992 0.000 -0.012 8.49 -0.36 0.52 C.500 0.912 0.000 0.992 0.000 0.914 0.000 8.49 -0.36 0.152 C.555 0.000 0.983 0.000 0.992 0.000 8.49 -0.36 0.013 0.883 0.000 0.983 0.000 0.914 0.000 -0.012 8.49 -0.36 0.914 0.000 0.912 0.000 0.924 0.000 -0.012 8.49 -0.36 0.914 0.000 0.938 0.000 0.914 0.000 -0.012 8.49 -0.36 0.914 0.000 0.918 0.000 0.914 0.000 -0.012 8.49 -0.36 0.120 0.883 0.000 0.938 0.000 0.924 0.000 -0.012 8.49 -0.36 0.140 0.930 0.000 0.914 0.000 -0.012 8.49 -0.36 0.140 0.930 0.000 0.914 0.000 -0.012 8.49 -0.36 0.140 0.900 0.918 0.000 0.924 0.000 -0.012 8.49 -0.36 0.140 0.930 0.000 0.914 0.000 -0.012 8.49 -0.36 0.140 0.930 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.000 0.918 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.000 0.918 0.000 0.914 0.000 -0.012 8.48 -0.36 0.140 0.900 0.918 0.000 0.914 0.000 -0.012 8.48 -0.36 0.914 0.000 0.918 0.000 0.924 0.000 0.012 8.48 -0.36 0.914 0.000 0.918 0.000 0.924 0.000 0.000 0.012 8.48 -0.36 0.914 0.9000 0.918 0.0000 0.924 0.000 0	79.	<b>K</b> A	8.49	0.0-	ĭ -	0.53	0.876	000.0	0.766	0.00.0	0.877	0.000	-0.024	0.599
5       8.49       -0.011       0.877       0.000       0.756       0.000       0.871       0.000       -0.012         2       6.49       -0.01       0.877       0.000       0.756       0.000       0.871       0.000       -0.011         2       6.49       -0.01       0.877       0.000       0.756       0.000       0.871       0.000       -0.011         2       8.49       -0.01       0.877       0.000       0.975       0.001       0.976       -0.011         2       8.49       -0.01       0.877       0.000       0.975       0.000       -0.972       0.001       -0.011         2       8.49       -0.01       1.7       0.975       0.000       0.975       0.001       0.976       -0.011         2       8.49       -0.01       1.7       0.976       0.000       0.975       0.001       0.075       -0.012         2       8.49       -0.01       1.7       0.976       0.000       0.975       0.001       0.075       -0.012         2       8.49       -0.01       1.48       0.988       0.000       0.976       0.075       -0.012         8.49       -0.01	79.	ŝ	8.49	0-0-	T T	0.36	C.867	0.000	0.750	C•000	0.868	0.000	-0-054	665.0
2       6.49       -C.C1       -0.01       C.877       0.000       0.756       C.000       0.878       0.000       -0.017         2       E.49       -C.C1       0.47       C.897       0.000       0.576       C.000       0.877       0.000       -0.017         2       E.49       -C.C1       0.47       C.897       0.000       0.575       C.000       0.871       0.000       -0.011         2       E.49       -C.C1       0.47       C.897       0.000       0.597       0.000       -0.015         2       E.49       -C.C1       0.47       C.897       0.000       0.975       0.000       0.975       0.000       -0.015         2       E.49       -0.01       1.41       C.976       0.000       0.975       0.000       0.975       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       <	79.	<b>k</b> n	8.49	0.0-	Ť H	0.19	0.877	0.000	0.768	0.000	0.873	0.000	-0.024	0.599
2       8.49       -C.C1       0.15       C.877       0.000       0.876       0.000       0.876       0.001         2       8.49       -0.01       0.33       0.877       0.000       0.897       0.000       -0.015         2       8.49       -0.01       0.47       C.873       0.000       0.897       0.000       -0.011         2       8.49       -0.01       0.47       C.873       0.000       0.995       0.000       -0.011         2       8.49       -0.01       1.48       0.988       0.000       0.995       0.000       -0.012         2       8.49       -0.01       1.48       0.988       0.000       0.995       0.000       -0.012         2       8.49       -0.01       1.48       0.988       0.000       0.995       0.000       -0.012         2       8.49       -0.01       1.48       0.900       0.992       0.000       -0.012         2       8.49       -0.01       1.514       191       80.7       0.000       -0.992       0.000         2       8.49       -0.01       1.514       9.000       0.992       0.000       0.902         2	80.	2	E • 49	0.0	- -	0.01	0.870	0000.0	0.756	0.000	0.871	0.000	-0.024	0.599
2       E.49       -0.01       0.33       0.877       0.000       0.897       0.000       -0.017         2       E.49       -0.01       0.47       C.895       0.000       0.992       0.000       -0.017         2       E.49       -0.01       1.17       C.975       0.000       0.955       0.000       0.955       0.000       0.955       0.000       0.976       0.010         2       E.49       -0.01       1.48       0.988       0.000       0.975       0.000       0.975       0.000       0.910       0.010       0.020         2       E.49       -0.01       1.48       0.988       0.000       0.995       0.000       0.995       0.000       0.910       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.020       0.010       0.010       0.010       0.010       0.010       0.010	80.	2	8.49	-0.0	-	0.15	C.877	0.000	0.768	c. 000	0.878	0.000	-0.017	666.0
2       8.49       -C.C1       0.47       C.895       0.000       0.897       0.000       0.894       0.000       -0.015         2       8.49       -C.C1       0.47       C.875       0.000       0.975       0.000       0.975       0.000       0.976       0.000       -0.015         2       8.49       -C.C1       0.47       C.975       0.000       0.975       0.000       0.976       0.000       -0.010         2       8.49       -C.C1       1.41       C.975       0.000       0.975       0.000       0.976       0.000       -0.010         2       8.49       -C.01       1.417       C.975       0.000       0.975       0.000       0.946       0.000       -0.012         2       8.49       -0.01       1.417       C.975       0.000       0.946       0.000       -0.012         5       0.514       191       8C       47       0.000       0.946       0.000       -0.012         5       0.514       191       8C       7       10.000       0.949       0.000       -0.012         5       0.514       191       8C       829       711       10.000       0.949	80.	2	E.49	0.0-	-	0.33	0.870	0.000	0.756	000.0	0.871	0.000	-0.015	0.999
<ul> <li>2 8.49 -0.01 0.64 0.853 0.000 0.952 0.000 0.952 0.000 -0.015</li> <li>2 8.49 -0.01 1.48 0.988 0.000 0.955 0.000 0.998 0.000 -0.028</li> <li>2 8.49 -0.01 1.48 0.988 0.000 0.994 0.000 0.992 0.000 -0.028</li> <li>2 8.49 -0.01 1.58 0.552 0.000 0.984 0.000 0.992 0.000 -0.028</li> <li>2 8.49 -0.01 1.58 0.552 0.000 0.984 0.000 0.992 0.000 -0.028</li> <li>2 0.250 1.514 191 80.2 1829 71.1 -10.00</li> <li>3 0.250 1.514 191 80.2 1829 71.1 -10.00</li> <li>5 0.250 1.514 191 80.2 1829 71.1 -10.00</li> <li>2 8.49 -0.36 -1.53 0.951 0.000 0.992 0.000 0.992 0.000</li> <li>2 8.49 -0.36 -1.53 0.951 0.000 0.992 0.000 0.904 0.000</li> <li>2 8.49 -0.36 -0.69 0.914 0.000 0.992 0.000 0.901 0.022</li> <li>3 49 -0.36 -0.69 0.914 0.000 0.982 0.000 0.991 0.000 -0.015</li> <li>8 49 -0.36 -0.63 0.991 0.000 0.992 0.000 0.901 0.001</li> <li>2 8 49 -0.36 -0.63 0.900 0.913 0.000 0.991 0.000 0.914</li> <li>3 49 -0.36 -0.63 0.000 0.913 0.000 0.924 0.000 0.024</li> <li>3 49 -0.36 0.014 0.893 0.000 0.938 0.000 0.920 0.000</li> <li>4 9 -0.36 0.037 0.893 0.000 0.924 0.000 0.901 0.0015</li> <li>8 49 -0.36 0.047 0.900 0.938 0.000 0.924 0.000 0.915</li> <li>8 49 -0.36 0.937 0.000 0.944 0.000 0.924 0.000</li> <li>2 8 48 -0.36 0.936 0.000 0.948 0.000 0.900 0.0015</li> <li>3 48 -0.36 0.447 0.000 0.944 0.000 0.901 0.0015</li> <li>4 49 -0.36 0.447 0.900 0.900 0.900 0.901 0.0015</li> <li>4 49 -0.36 0.447 0.900 0.900 0.900 0.900 0.000 0.924 0.000</li> <li>5 8 48 -0.36 0.457 0.000 0.946 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.456 0.000 0.991 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.457 0.000 0.991 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.935 0.000 0.991 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.944 0.000 0.904 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.964 0.000 0.994 0.000 0.901 0.0015</li> <li>5 8 48 -0.36 0.900 0.900 0.994 0.000 0.901</li> <li>5 8 48 -0.36 0.900 0.900 0.994 0.000 0.901</li> <li>5 8 48 -0.36 0.900 0.991 0.000 0.994 0.000 0.0015</li> <li>5 8 48 -0.36 0.900 0.991 0.000 0.994 0.000 0.0015</li> </ul>	80.	2	8.49	0°0-	-	0.47	C.896	0.000	0.802	C• 000	0.897	0.000	-0-017	0.999
2       8.49       -0.011       0.977       0.972       0.000       0.992       0.000       -0.010         2       8.49       -0.011       1.48       0.988       0.000       0.992       0.000       -0.012         2       8.49       -0.01       1.48       0.988       0.000       0.945       0.000       0.946       0.000       -0.012         2       8.49       -0.01       1.58       C.572       0.000       0.948       0.000       -948       0.000       -0.922       0.000         5       0.250       1.514       191       86.2       1829       71.1       -10.00       -0.923       0.000       -949       -0.001       -0.923       0.000       -0.923       0.000       -0.923       0.000       -0.923       0.000       -0.012       849       -0.023       -1.53       0.971       0.000       0.943       0.000       -0.943       0.000       -0.923       0.000       -0.012       849       -0.023       -1.023       0.925       0.000       0.943       0.000       -0.943       0.000       -0.012       849       -0.023       -1.023       0.923       0.000       0.946       0.000       -0.023       849       -0	80	~.	8.49	0.01	-	0.64	C*853	0.00.0	0.797	0.000	0.894	0.000	-0.015	0.5999
<ul> <li>E 6.49 -C.GI 1.17 C.976 0.000 C.952 C.000 0.996 0.007 -0.010</li> <li>E 8.49 -0.01 1.48 0.988 0.007 0.975 0.000 0.996 0.007 -0.003</li> <li>CCNF WACH PN/L PT C P TT ALPHA</li> <li>CCNF WACH PN/L PT C P TT ALPHA</li> <li>F 0.256 1.514 1911 80.2 1829 71.1 -10.00</li> <li>S 0.256 1.514 1911 80.2 1829 71.1 -10.00</li> <li>E 4.9 -0.36 -2.03 0.951 0.000 0.982 0.000 0.992 0.007 -0.023</li> <li>E 4.9 -0.36 -2.03 0.597 0.000 0.982 0.000 0.992 0.007 -0.024</li> <li>E 4.9 -0.36 -1.53 0.951 0.000 0.982 0.000 0.994 0.007 -0.024</li> <li>E 4.9 -0.36 -0.19 0.887 0.000 0.983 0.000 0.994 0.000 -0.024</li> <li>E 4.9 -0.36 0.14 0.895 0.000 0.988 0.000 0.994 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.895 0.000 0.912 0.000 0.991 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.895 0.000 0.908 0.000 0.914 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.897 0.000 0.918 0.000 0.914 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.897 0.000 0.918 0.000 0.914 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.897 0.000 0.918 0.000 0.914 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.900 0.778 0.000 0.924 0.000 -0.024</li> <li>E 4.9 -0.36 0.47 0.000 0.938 0.000 0.924 0.000 -0.024</li> <li>E 4.49 -0.36 0.47 0.000 0.936 0.000 0.914 0.000 -0.024</li> <li>E 4.49 -0.36 0.47 0.000 0.938 0.000 0.924 0.000 -0.024</li> <li>E 4.49 -0.36 0.47 0.000 0.936 0.000 0.924 0.000 -0.024</li> <li>E 4.48 -0.36 0.47 0.000 0.937 0.000 0.924 0.000 -0.012</li> <li>E 4.48 -0.36 0.47 0.000 0.947 0.000 0.914 0.000 -0.012</li> <li>E 4.48 -0.36 0.47 0.000 0.947 0.000 0.914 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.947 0.000 0.904 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.947 0.000 0.904 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.947 0.000 0.904 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.947 0.000 0.994 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.947 0.000 0.994 0.000 -0.012</li> <li>E 4.48 -0.36 0.497 0.000 0.9487 0.000 0.994 0.000 -0.012</li> <li>E 4.48 -0.36 0.000 0.994 0.000 0.994 0.000 -0.012</li> </ul>	80	• 2	8.49	-0-0	-	15.0	C.952	000.0	0.905	0.000	0.952	0.000	-0.015	0.599
<ul> <li>E 8.49 -0.01 1.48 0.988 0.000 0.984 0.000 0.992 0.000 -0.0028</li> <li>E 8.49 -0.01 1.58 0.572 0.000 0.984 0.000 0.992 0.000 -0.0028</li> <li>CCNF wACF PN/L PT C P T ALPHA</li> <li>5 0.250 1.514 1911 80.2 1829 TT ALPHA</li> <li>5 0.250 1.514 1911 80.2 1829 TT 1.1 -10.00</li> <li>V/DB Z/DB WF/W WA/M GF/O 0.493 0.000 -0.992 0.000</li> <li>2 8.49 -0.36 -1.53 0.991 0.000 0.982 0.000 0.992 0.000 -0.015</li> <li>2 8.49 -0.36 -1.02 0.589 0.000 0.982 0.000 0.992 0.000 -0.015</li> <li>2 8.49 -0.36 -1.02 0.589 0.000 0.982 0.000 0.9914 0.000 -0.015</li> <li>2 8.49 -0.36 -0.52 0.595 0.000 0.982 0.000 0.9914 0.000 -0.015</li> <li>2 8.49 -0.36 -0.19 0.867 0.000 0.982 0.000 0.9914 0.000 -0.015</li> <li>2 8.49 -0.36 -0.19 0.867 0.000 0.980 0.000 0.9914 0.000 -0.015</li> <li>2 8.49 -0.36 0.19 0.867 0.000 0.980 0.000 0.9914 0.000 -0.015</li> <li>2 8.49 -0.36 0.19 0.867 0.000 0.9814 0.000 0.901 0.024</li> <li>2 8.49 -0.36 0.19 0.867 0.000 0.992 0.000 0.914 0.000 -0.015</li> <li>2 8.49 -0.35 0.114 0.867 0.000 0.9308 0.000 0.924 0.000 -0.015</li> <li>2 8.49 -0.35 0.119 0.867 0.000 0.920 0.900 0.914 0.000 -0.015</li> <li>2 8.49 -0.35 0.19 0.867 0.000 0.926 0.000 0.924 0.000 -0.015</li> <li>2 8.49 -0.35 0.14 0.900 0.900 0.900 0.914 0.000 -0.015</li> <li>2 8.49 -0.35 0.14 0.900 0.900 0.900 0.914 0.000 -0.015</li> <li>2 8.49 -0.35 0.14 0.900 0.900 0.916 0.000 0.924 0.000 -0.015</li> <li>2 8.48 -0.35 0.14 0.900 0.994 0.000 -0.916 0.001</li> <li>3 4.48 -0.35 1.19 0.974 0.000 0.994 0.000 -0.015</li> <li>3 4.48 -0.35 1.998 0.000 0.994 0.000 -0.015</li> <li>3 4.48 -0.35 1.998 0.000 0.994 0.000 -0.015</li> <li>3 4.48 -0.35 1.998 0.000 0.994 0.000 -0.015</li> <li>4 4.8 -0.35 1.998 0.000 0.994 0.000 -0.015</li> <li>4 4.8 -0.35 1.998 0.000 0.994 0.000 -0.011</li> <li>5 4.48 -0.35 1.998 0.000 0.994 0.000 -0.011</li> <li>5 4.48 -0.35 1.998 0.0000 0.994 0.000 0.994 0.000 -0.011</li> </ul>	80	2.	6 <b>4 •</b> 3	0.0-		1.17	0.976	0.000	0.952	0.000	0.976	0.000	-0.010	1.000
<ul> <li>2 8.49 -0.01 1.58 C.552 0.000 0.984 0.000 0.992 0.000 -0.003</li> <li>CCNF WACH PN/L PT C P TT ALPHA</li> <li>5 0.250 1.514 1911 80.2 1829 71.1 -10.00</li> <li>5 0.250 1.514 1911 80.2 1829 71.1 -10.00</li> <li>7 N/DB Z/DB MF/W MA/M QF/C 0.000 0.992 0.000 -0.015</li> <li>8 49 -0.36 -1.02 0.991 0.000 0.982 0.000 0.992 0.000 -0.012</li> <li>8 49 -0.36 -1.02 0.555 0.091 0.991 0.000 0.992 0.000 -0.012</li> <li>8 49 -0.36 -1.02 0.555 0.090 0.981 0.000 0.994 0.000 -0.012</li> <li>8 49 -0.36 -0.15 0.991 0.000 0.982 0.000 0.992 0.000 -0.012</li> <li>8 49 -0.36 -0.19 0.867 0.000 0.981 0.000 0.944 0.000 -0.024</li> <li>2 8 49 -0.36 0.14 0.000 0.980 0.000 0.944 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.000 0.980 0.000 0.944 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.893 0.000 0.917 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.893 0.000 0.918 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.893 0.000 0.918 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.893 0.000 0.918 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.900 0.900 0.914 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.900 0.900 0.918 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.900 0.914 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.900 0.914 0.000 0.914 0.000 -0.012</li> <li>8 49 -0.36 0.14 0.900 0.914 0.000 0.917 0.000 0.917 0.001</li> <li>8 48 -0.36 0.14 0.900 0.952 0.000 0.914 0.000 -0.015</li> <li>8 48 -0.36 1.19 0.914 0.000 0.952 0.000 0.914 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.952 0.000 0.914 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.952 0.000 0.914 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.952 0.000 0.914 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.994 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.994 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.994 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.950 0.900 0.994 0.000 -0.015</li> <li>8 48 -0.36 1.99 0.000 0.994 0.000 0.900 0.000</li> </ul>	79	41 •	8.49	0.0-		1.48	0.988	0.000	0.975	0.000	0.988	0.000	-0.028	0.999
CCNF       WACH       PN/L       PT       ALPHA         5       0.250       1.514       1911       80.2       1829       71.1       -10.00         5       0.256       1.514       1911       80.2       1829       71.1       -10.00         2       8.49       -0.36       -7.03       0.589       0.700       0.949       U.000       -0.949         2       8.49       -0.36       -1.53       0.951       0.000       0.982       0.000       0.949       U.000       -0.025         5       8.49       -0.36       -1.02       C.555       0.000       0.942       0.000       -9949       U.000       -0.024         5       8.49       -0.36       -1.02       C.555       0.000       0.933       0.000       0.934       0.000       -0.024         6       8.49       -0.36       0.102       0.833       0.000       0.914       0.007       -0.024         7       8.49       -0.36       0.14       0.800       0.778       0.000       0.924       0.007       -0.024         8       49       -0.36       0.14       0.800       0.778       0.000       -0.024 <t< td=""><td>80</td><td>~</td><td>8.49</td><td>0.0-</td><td></td><td>1.58</td><td>255 ° 0</td><td>0.000</td><td>0.984</td><td>0.000</td><td>0.992</td><td>0.000</td><td>200.0-</td><td>1.000</td></t<>	80	~	8.49	0.0-		1.58	255 ° 0	0.000	0.984	0.000	0.992	0.000	200.0-	1.000
5       0.250       1.514       191       80.2       1829       71.1       -10.00       VF/V       VA/V       CP         0.2       8.49       -0.36       -7.03       0.589       0.000       0.992       0.000       -0.992       0.000       -0.015         0.2       8.49       -0.36       -1.53       0.589       0.000       0.992       0.000       -0.992       0.000       -0.992       0.000       -0.015         0.2       8.49       -0.36       -1.02       0.5955       0.000       0.992       0.000       -0.992       0.000       -0.023         0.2       8.49       -0.36       -0.52       0.5900       0.000       0.9914       0.000       0.9914       0.000       0.9914       0.000       0.9914       0.000       0.9914       0.000       0.9914       0.000       0.9914       0.000       0.991       0.000       0.991       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000       0.000	-		ž	a ر		10	ر	0	11		<			
x / DB       Y / DB       Z / DB       MF / M       QF / D       QF / D       QF / V       V / V / V       V / V / V       V / V / V / V       V / V / V / V / V / V / V / V / V / V /		; ; ;	ייין כ ע	-					 		<b>T</b> (			
2.2 $8.49$ $-0.36$ $-2.03$ $0.589$ $0.000$ $0.982$ $0.000$ $0.932$ $0.000$ $-0.020$ $3.5$ $8.49$ $-0.26$ $-1.53$ $0.991$ $0.000$ $0.982$ $0.000$ $-0.922$ $0.000$ $-0.020$ $3.5$ $8.49$ $-0.26$ $-1.53$ $0.991$ $0.000$ $0.912$ $0.000$ $-0.922$ $0.000$ $-0.023$ $3.5$ $8.49$ $-0.26$ $-1.62$ $C.955$ $0.000$ $0.912$ $0.000$ $0.914$ $0.000$ $-0.023$ $3.6$ $-0.52$ $C.900$ $0.000$ $0.912$ $0.000$ $0.914$ $0.000$ $-0.023$ $3.49$ $-0.26$ $-0.52$ $C.900$ $0.000$ $0.914$ $0.000$ $-0.023$ $3.49$ $-0.26$ $-0.36$ $C.882$ $0.000$ $0.783$ $C.000$ $0.914$ $0.000$ $3.49$ $-0.26$ $-0.14$ $0.887$ $0.000$ $0.914$ $0.000$ $0.024$ $3.49$ $-0.26$ $0.14$ $0.887$ $0.000$ $0.817$ $0.000$ $0.027$ $3.49$ $-0.26$ $0.14$ $0.887$ $0.000$ $0.926$ $-0.022$ $3.49$ $-0.26$ $0.14$ $0.887$ $0.000$ $0.926$ $-0.022$ $3.49$ $-0.26$ $0.326$ $0.000$ $0.766$ $0.000$ $0.926$ $-0.022$ $3.49$ $-0.26$ $0.926$ $0.000$ $0.766$ $0.000$ $0.924$ $0.000$ $3.49$ $-0.26$ $0.926$ $0.926$ $0.000$				• T		171		4701 7					Ċ	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	, <del>0</del>	.2	8.49	0	ا مورو	2.03	0.589	000-000	0.977	0.000	0.989		-0.003	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	80	2	8.49	0.01	9	1.53	0.991	0.000	0.982	0.000	0.992	0.000	-0.015	
<ul> <li>E 8.49 -0.36 -0.69 C.914 0.000 0.834 0.000 0.914 0.000 -0.024</li> <li>E 8.49 -C.36 -0.52 C.900 0.000 C.809 C.000 0.901 0.000 -0.015</li> <li>E 8.49 -C.36 -0.36 C.883 0.000 0.778 C.000 0.944 0.000 -0.015</li> <li>E 8.49 -C.36 -0.19 0.867 0.000 0.778 C.000 0.887 0.000 -0.015</li> <li>E 8.49 -C.36 -0.19 0.867 0.000 0.778 C.000 0.887 0.000 -0.024</li> <li>E 8.49 -C.36 -0.19 0.867 0.000 0.766 C.000 0.887 0.000 -0.015</li> <li>E 8.49 -0.36 0.14 C.893 0.000 0.766 C.000 0.887 0.000 -0.075</li> <li>E 8.49 -0.36 0.47 C.893 0.000 0.766 C.000 0.877 0.000 -0.075</li> <li>E 8.48 -0.36 0.47 C.893 0.000 0.852 0.000 0.924 0.000 -0.075</li> <li>E 8.48 -0.36 1.19 C.974 0.000 0.852 0.000 0.976 0.000 0.976 0.001</li> <li>E 8.48 -0.36 1.19 C.974 0.000 0.957 C.000 0.976 0.000 0.976 0.001</li> <li>E 8.48 -0.36 1.19 C.974 0.000 0.957 C.000 0.976 0.000 0.976 0.001</li> </ul>	79	นา •	8.49	-0-	9	1.02	5 ° 2 2 2	0.000	0.912	0.000	0.956	0.000	-0-022	0.999
<ul> <li>2 8.49 -C. 36 -0.52 C. 90C 0.000 C. 809 C.000 U. 9UI U. 000 -0.024</li> <li>2 8.49 -0.36 -0.36 C. 883 0.000 0.778 C. 000 U. 834 0.000 -0.015</li> <li>2 8.49 -C. 36 -0.19 C. 867 0.000 0.751 0.000 0.868 0.000 -0.024</li> <li>2 8.49 -C. 36 -0.19 C. 867 0.000 0.783 C. 000 0.887 0.000 -0.024</li> <li>2 8.49 -C. 36 0.14 C. 899 0.000 0.766 C. 000 0.887 0.000 -0.024</li> <li>2 8.49 -C. 36 0.14 C. 893 0.000 0.766 C. 000 0.877 0.000 -0.024</li> <li>2 8.49 -C. 36 0.47 C. 893 0.000 0.766 C. 000 0.877 0.000 -0.024</li> <li>2 8.49 -C. 36 0.47 C. 893 0.000 0.766 C. 000 0.924 0.000 -0.024</li> <li>2 8.48 -C. 36 0.64 C.973 0.000 0.952 0.000 0.924 0.000 -0.015</li> <li>2 8.48 -C. 36 1.19 C.974 0.000 0.952 0.000 0.974 0.000 -0.015</li> <li>2 8.48 -C. 36 1.98 C.974 0.000 0.948 0.000 0.974 0.000 -0.015</li> <li>2 8.48 -C. 36 1.98 C.974 0.000 0.948 0.000 0.974 0.000 -0.015</li> <li>3 8.48 -C. 36 1.98 C.974 0.000 0.948 0.000 0.976 0.000 0.976 0.000 -0.015</li> </ul>	79	ឋ <u>ា</u>	8.49	-0-3	ī 9	0.69	0.914	0.000	0.834	0.000	0.914	0.000	-0.024	0.999
1.2       8.49       -0.36      883       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.864       0.000       0.887       0.000       0.000       0.887       0.000       0.002         2       8.49       -0.36       0.14       0.865       0.000       0.887       0.000       0.887       0.000       0.024         2       8.49       -0.36       0.14       0.895       0.000       0.887       0.000       0.877       0.000       0.024       0.024       0.024       0.024       0.0224       0.002       0.002       0.024       0.002       0.002       0.002       0.002       0.002       0.002       0.000       0.877       0.000       0.000       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002       0.002	80	~ 5	8 49	-0-3	ī 9	0.52	C. 90C	0.000	C.809	0.000	0.901	0.000	-0.024	0.999
8.49       -C.36       -0.19       0.867       0.000       0.751       0.000       0.868       0.000       -0.024         8.49       -C.36       0.14       C.885       C.000       0.887       0.000       -0.024         8.49       -C.36       0.14       C.885       C.000       0.887       0.000       -0.024         8.49       -C.36       0.14       C.885       C.000       0.887       0.000       -0.024         8.49       -0.36       0.14       C.889       0.000       0.783       C.000       0.887       0.000       -0.024         8.49       -0.36       0.14       C.899       0.000       0.766       C.000       0.877       0.000       -0.024         8.49       -0.36       0.47       C.893       0.000       0.766       C.000       0.877       0.000       -0.024         8.48       -0.36       0.47       C.976       0.000       0.976       0.000       -0.015         8.48       -0.36       1.19       C.974       0.000       0.948       0.000       -0.017         8.48       -0.36       1.49       C.985       0.000       0.948       0.000       -0.017      <	30	•2	8.49	-0-	T 9	0.36	C•883	0.000	0.778	C. J00	0.834	0.000	-0-015	0.999
1-2       8-49       -C-36       -0-C3       C-885       0-000       0-783       C.000       0.887       0.000       -0.024         1-2       8-49       -0.35       0-14       C-899       0.000       0-808       0.000       0-900       0-074         1-2       8-49       -0.35       0-14       C-899       0.000       0-808       0.000       0-764       0-900       0-764       -0-024         1-2       8-49       -0.36       0-47       C-893       0-000       0-766       C-000       0-874       0-002       -0-024         1-2       8-49       -0.36       0-47       C-893       0-000       C-797       C-000       0-874       0-001       024       -0-024         1-2       8-48       -0-36       0-64       C-923       0-000       0-852       0-001       0-24       0-024       0-024         1-2       8-48       -0-36       0-94       0-057       0-001       0-924       0-0024       0-024         1-2       8-48       -0-36       1-19       C-973       0-000       0-924       0-002       0-024       0-0024         1-2       8-48       -0-36       1-19       C-985	80	2.	8.49	- C • 3	Ĩ 9	0.19	0.867	0.000	0.751	0.00.0	0.868	0.000	-0.024	665 0
1-2       8-49       -0.36       0.14       0.899       0.000       0.808       0.000       0.877       0.900       -0.24         1-2       8-49       -0.36       0.32       0.875       0.000       0.766       0.000       0.877       0.900       -0.024         1-2       8-49       -0.36       0.47       0.893       0.000       0.766       0.000       0.877       0.900       -0.024         1-2       8-49       -0.36       0.47       0.893       0.000       0.852       0.000       0.894       0.000       -0.024         1-2       8-48       -0.36       0.64       0.973       0.000       0.852       0.000       0.924       0.000       -0.024         1-2       8-48       -0.36       0.974       0.900       0.948       0.000       -0.024         1-2       8-48       -0.36       1.19       0.974       0.900       0.976       -0.027         1-2       8-48       -0.36       1.49       0.900       0.948       0.000       0.976       -0.017         1-2       8-48       -0.36       1.49       0.900       0.976       0.001       0.926       0.001       0.027	30	- 2	8•49	-0.1	٦ بو	0.03	0.385	0.000	0.783	C.000	0.887	0.000	-0.015	666.0
<ul> <li>2 8.49 -0.36 0.32 C.876 0.000 0.766 C.000 0.877 0.000 -0.024</li> <li>2 8.49 -0.36 0.47 C.893 0.000 C.797 C.000 0.894 0.000 -0.024</li> <li>2 8.48 -0.36 0.64 C.923 0.000 0.852 0.000 0.924 0.000 -0.015</li> <li>2 8.48 -0.36 0.98 C.976 0.000 0.852 0.000 0.976 0.000 -0.014</li> <li>2 8.48 -0.36 1.19 C.974 0.000 0.948 0.000 0.974 0.000 -0.013</li> <li>2 8.48 -0.36 1.49 C.985 0.000 0.948 0.000 0.974 0.000 -0.013</li> <li>2 8.48 -0.36 1.49 C.974 0.000 0.948 0.000 0.976 0.000 -0.013</li> <li>2 8.48 -0.36 1.49 C.974 0.000 0.948 0.000 0.976 0.000 -0.013</li> <li>2 8.48 -0.36 1.49 C.985 0.000 0.948 0.000 0.976 0.000 -0.013</li> </ul>	80	• 2	8.49	-0-3	\$	0.14	0.899	0000.0	0.808	0.000	0.6.00	0.000	-0.024	665*0
<ul> <li>2 8.49 -0.36 0.47 0.893 0.000 0.797 0.000 0.894 0.000 -0.024</li> <li>2 8.48 -0.36 0.64 0.923 0.000 0.852 0.000 0.924 0.000 -0.015</li> <li>2 8.48 -0.36 0.98 0.976 0.000 0.948 0.000 0.976 0.000 -0.017</li> <li>2 8.48 -0.36 1.19 0.974 0.000 0.948 0.000 0.974 0.000 -0.017</li> <li>2 8.48 -0.36 1.49 0.974 0.000 0.948 0.000 0.974 0.000 -0.017</li> <li>3 8.48 -0.36 1.49 0.974 0.000 0.948 0.000 0.946 0.000 -0.012</li> <li>5 8.48 -0.36 1.98 0.954 0.000 0.947 0.000 0.946 0.000 0.976 0.000 -0.012</li> </ul>	80	• 2	8 • 49	2-0-	9	0.32	0.876	0.000	0.766	C. UUO	0.877	0.000	-0-024	0.599
1.2       8.48       -0.36       0.64       0.923       0.000       0.852       0.000       0.924       0.000       -0.015         .2       8.48       -0.36       0.98       0.976       0.070       -0.024         .2       8.48       -0.36       0.98       0.976       0.000       -0.074         .2       8.48       -0.36       1.19       0.974       0.000       0.948       0.000         .2       8.48       -0.36       1.19       0.974       0.000       0.948       0.000       0.974       0.001         .2       8.48       -0.36       1.45       0.985       0.000       0.978       0.000       -0.011         .2       8.48       -0.36       1.45       C.985       0.000       0.948       0.000       -0.011         .2       8.48       -0.36       1.49       C.985       0.000       0.946       0.000       -0.011	80	•2	8.49	-0-	9	0.47	0.893	0.000	197.0	C• U00	0.894	0.000	-0.024	665 0
<ul> <li>2 8.48 -0.36 0.98 C.976 0.000 C.952 0.000 0.976 0.000 -0.024</li> <li>2 8.48 -0.36 1.19 C.974 0.000 0.948 0.000 0.974 0.000 -0.017</li> <li>2 8.48 -C.36 1.49 C.985 0.000 0.970 C.000 0.946 0.000 -0.012</li> <li>5 8.48 -0.36 1.98 C.954 0.000 0.987 0.000 0.994 0.000 -0.012</li> </ul>	80	• 2	8•48	E 0-	50	0.64	C.923	0.000	0.852	0.000	0.924	0.000	-0.015	665.0
<ul> <li>2 8.48 -0.36 1.19 0.974 0.000 0.948 0.000 0.974 0.000 -0.017</li> <li>2 8.48 -0.36 1.45 0.985 0.000 0.970 0.000 0.946 0.000 -0.013</li> <li>5 8.48 -0.36 1.98 0.954 0.000 0.987 0.000 0.994 0.000 -0.012</li> </ul>	80	2.	8.48	0-0-	9	96.0	C.976	000°u	C. 952	0.00.0	0.976	0.000	-0.024	0.999
•2 8•48 -C.36 1•45 C•985 0•070 0•970 C•000 0•936 0•060 -0•013 •5 8•48 -0•36 1•98 C•954 0•C0C C•987 0•000 0•994 0•0C0 -0•012	80	•2	8*48	-0-3	9	1.19	0.974	0.000	0.948	0.000	0.974	0.000	-0.017	0.999
•5 8.48 -0.36 1.98 C.954 0.606 0.987 0.000 0.994 0.060 -0.012	80	•2	8.48		9	1.45	<b>C.</b> 985	0.0.0	0.970	C. 000	0.936	0.000	-0.013	0.999
	79	un.	8•48	-0-3	Ŷ	1.98	C.954	0.000	0.987	0.000	0.994	0-000	-0.012	565.0

0.9999 665 •0 665°0 665°0 6665°0 6666°0 666°0 E/0 .000 665.0 665 0.999 666 65 . ē • -0.024 -0.024 -0.024 -0.024 -0.024 -0.024 -0.024 -0.024 -0.012 -0.022 -0.019 .017 -0.003 Ŷ 000 8 C • • VF/V 0.989 0.985 0.965 0.904 0.892 0.894 0.908 0.883 0.888 0.891 0.916 0.938 906 916 998 998 00 . 0 ALPHA -10.00 0A/Q 0.000 c.000 c.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 71.2 0F70 0.977 0.977 0.970 0.979 0.929 0.797 0.822 0.775 0.797 0.837 0.837 0.932 0.951 0.994 0.996 0.000 .000 C 855 855 . . U F MACH RN/L PT 5 0.250 1.514 1911 8.49 -0.45 -2.03 0 8.49 -0.45 -1.52 0 8.49 -0.45 -1.52 0 8.49 -0.45 -1.52 0 8.49 -0.45 -0.55 0 8.49 -0.45 0.35 0 8.49 -0.45 0.19 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0.98 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.49 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 -0.45 0 8.40 0 8.40 -0.45 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 8.40 0 Ś CONF Ľ١ ណ 5 ហ -62 -61 -61 2 D 571 1 249 249 σ 4 Ś N . 0 . RUN 330 SFQ 65543210983655432

## TABLE 2(b)

Configuration 6 – Ballast-profile model as supported in Configuration 5.

1.241 1.225 1.071 1.134 1.023 1.029 1.026 1.049 1.054 pF/p 1.078 1.096 1.174 1.202 1.213 1.222 1.226 1.234 1.067 0.282 0.263 0.083 0.083 0.083 0.083 0.083 0.083 0.024 0.024 0.058 0.064 0.079 0.092 0.113 0.205 0.233 0.237 0.237 0.260 0.266 0.275 9 V A /V 0.856 0.866 0.955 0.917 0.972 0.984 0.980 0.976 0.976 0.958 0.951 0.965 VF/V 0.360 0.831 0.941 0.895 805 0.879 0.873 0.367 . ALPHA 0.00 0.01 0.865 0.852 0.956 0.919 0.971 0.983 0.979 0.975 0.967 74.4 QF/O 0.966 096.0 0.944 0.898 0.879 863 0.954 0.882 0.874 0.367 0.857 320 WA/M 272.5 WF/W 0.825 C-840 C-945 C-945 C.966 C.966 C.970 C.949 0.858 C.855 0.958 0.875 C.834 C.834 0.976 C.960 0.928 C-845 C.842 C-941 2/CB 2/CB 1.95 ( 1.95 1.95 1.96 1.96 **1**6. 1.96 1.96 1.96 •96 .96 -97 •96 - 97 .97 -97 - 51 72**.** NF WACH RN/L 6 1.104 1.513 X/CB Y/DE Z 7.18 -0.02 1 -0.01 -0.01 -0.01 -0.01 00°00 0°00 0°00 -0-00 -0.00 C-01 C-01 C-01 0.01 00 6.93 6.76 6.60 6.44 6.27 6.09 5.94 5.26 5.09 4.53 4.76 4.59 5.76 5.60 5.44 4.42 4.10 P IN CONF 66 C 272.9 272.5 272.2 271.9 272.2 271.5 271.8 271.8 271.7 272.2 271.8 272.1 272.3 272.3 272.3 272.1 272.1 272. 571 1 MACH 1.105 1.058 1.059 1.101 1.104 1.099 1.104 1.104 1.101 1.100 TST 1.101 650.1 1.100 1.102 1.100 1.102 1.104 1.102 RUN 331 SEQ n m 4 50000 10 12 14 15 16 17 18 19 2023

1.031 1.069 1.066 • 0.65 .068 1.062 DE/I 0.037 0.080 0.080 0.078 0.076 0.076 0.076 đ V A /V 0.921 0.896 0.748 0.705 0.677 0.706 0.765 VF/V 0.00 04/0 **ALPHA** 0570 0.843 0.843 0.818 0.539 0.473 0.473 0.473 75.7 0.565 0.885 319 M / M ۵ 6 1.1C5 1.507 686 272.7 M X/CB Y/DE Z/DE MF/M M 5.49 0.000 -1.04 0.9024 5.49 0.00 -0.03 0.710 5.49 0.00 0.12 0.6666 5.49 0.00 0.12 0.6666 5.49 0.00 0.29 0.636 5.49 0.00 0.46 0.636 PN/L WACH TST P IN CONF 272.7 272.7 273.1 273.1 272.9 272.6 270.8 270.8 271.7 571 1 66 MACH Q 1.105 1.105 1.105 1.102 1.105 1.098 1.053 1.093 332 SEQ - nin + u o r o RUN

	DE/D	1.027	1.016	0.998	166.0	0.598	666.0	1.005	1.022			DF/D	1.003	1.007	0.996	995.0	1.000	666.0	1.000	1.008	
	<u>د</u> ه ۲	0.043	0.025	-0.00	-0.004	+00.0-	-0.002	0.007	0.035			60	0.008	0.015	600.0-	010-0-	-0-001	-0.002	100.0-	0.018	
	V A / V											V A /V									
AL PHA 0.00	PA/U VF/V	0.911	0.873	0.712	0.685	0.678	0.712	0.768	0.924	ALPHA	0.00	0A/4 VF/V	0.918	0.853	0.744	0.742	0.749	0.793	0.344	0.948	
11 75.8	CF/0	0.828	0.752	0.465	0.428	0.419	0.465	0.553	C.851	11	75.4	QF /0	0.830	0.708	0.521	0.518	0.531	0.600	0.685	0.895	
9 C D K	N / VN									۵	505	W V V									
247-0	NF/N	C.858	0.860	0.683	C.655	0.648	0.683	0.742	C.913	C.	226.2	N L J N	0.909	0.838	0.723	0.722	0.729	0.775	0.829	0.942	
14	Z/CB	1.04	0.55	0.04	0.14	0.29	0.46	0.63	0.56	Τd	169	7/08	-1 - 04	-0-54	-0-04	0.12	0.29	0.46	0.63	0.96	
1/14 1/14	108	0.00 -	- 00-0	0.00	00.00	00.00	0.00	00-00	00.00	17 N R	1.510	Y / D.P.	- 00-0	- 00 - 0	- 00 - 0	00-00	0.00	0.00	0.00	00.0	
NACH 0.040	X/08	5.49	5.49 (	5.49	5.49	5.49	5.49	5.48	5.49		008 0	X/FB	67 s	5.48	5.49	67 - 3	5.49	5.49	5.49	5.49	
T P TN CCNF		49 247.0	48 246.6	46 246.2	47 246.1	45 245.7	45 245.7	46 246.2	45 245.8	SNUT AT 0 T			100 276.7	101 226.1	100 224-2	100 226.2	102 226.7	102 226.7	202 226.7	301 226.1	
RUN TS	VW CAS	1 0.9	2 0.9	0.0	4 0.9	5 0.9	6 0 9	6-0 2	8 0.9											0°0	

1.000 0.598 0.998 0.598 0.998 0.9999 665 0 1.000 DE/0 -0.036 -0.029 -0.026 -0.010 -0.045 -0.043 -0.036 -0.010 3 0.909 0.889 0.819 0.814 0.814 0.854 0.856 VF/V 0.892 0.944 ALPHA 0.00 04/0 C.000 0.000 0.000 **c.**000 0.000 000-0 0.787 0.667 0.659 0.726 0.729 0.792 C.889 71.1 CF/7 0.825 F 0°000 0°0000 0.000 0.000 0.000 0.000 1828 NA/N 0.000 С. 80.9 MF /N C.9C8 C.888 C.817 O.813 C.853 O.854 C.891 0.943 C 1151 Z/CB L d F WACH RN/L X/FB Y/DB Z 5.49 C.C0 -0 5.49 C.C0 -0 5.49 C.C0 -0 5.49 0.00 0 5.49 0.00 0 5.49 0.00 0 5.49 0.00 0 CONF Ś TA C( 66 66 80.5 80.5 80.5 80.5 80.5 80.5 80.5 80.5 80.5 **ド う S** し 3 E と S G = O M 4 E S C 8

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Table 2(c)

Configuration 5 – Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section: forward-facing pitot-static probe.

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		PF/P	1.010	1.047	1.067	1.071	1.065	1.062	1.063	1.065	1.070	1.079			pt/p	1.065	1.066	1.066	1.061	1.067	1.069	1.069	1.081			a/id	1.036	1.074	1.073	1.078	1.076	1.067	1.065	1.066	1.070	1.085
		d C	0.012	0.055	0.079	0.083	0.077	0.074	0.074	770.0	0.083	0.094			CD	0.076	0.079	0.078	0.072	0.079	0.082	0.083	0.096			<u>6</u>	0.042	0.087	0.085	160.0	0.088	0.078	0.076	0.079	0.084	0.101
		V A /V													V A /V											V A /V										
ALPHA	0.00	0A/Q VF/V	0.985	0.907	0.929	0.901	0.861	0.816	161.0	0.813	0.851	0.934	ALPHA	0.00	QA/Q VF/V	0.902	0.895	0•746	0.707	0•663	0.684	0.757	0.914	ALPHA	0.00	CA/Q VF/V	0.967	0.933	0.879	0.879	0.842	0.800	0.779	0.807	0.864	0.934
11	70.6	QF/Q	0.973	0.826	0.891	0.832	0.743	0.654	C.610	0.651	C.727	0.913	11	72.0	0F 10	0.928	0.816	0.536	0.473	C.412	0.444	0.5555	0.868	11	72.8	GF / Q	C.954	0.906	0.785	0.190	0.712	0.627	0.591	C.640	0.754	0.918
٩	317	W V V											۵.	319	MV VN									<b>C</b> .	319	N V V N										
G	269.3	ME/N	C•982	0.988	C.914	<b>C.</b> 882	0.835	C.785	0.757	0.782	0.824	0-920	U	270.7	NE / N	0.882	C.875	0.705	C.668	<b>C.622</b>	0.644	c.721	0.896	C	271.0	NF / N	0.960	616.0	0.855	0.856	0.814	0.767	0.745	0.775	0.839	C.92C
D L	8 678	2/CB	-1.05	-070	-0-54	-0.21	-0-04	0.12	0.29	0.46	0.63	0•96	Fq .	2 682	Z/08	-1.04	-0.54	-0-04	0.13	0:00	0.47	0.62	0.96	1 d	9 682	2/0B	-1.04	-0.71	-0.54	-0.21	-0.04	0.13	0.29	0.46	0.63	0.96
LNN H	1.50	X/08	C.44 -	- 44 -0	C.44 -	0.44 -	0.44	C.44	0.44	C.44	0.44	0.44	RN/I	1.512	Y/DB	00.00	- 00 - 0	00.00	0.00	00.0	00-00	0.00	00-00	INA .	1.50°	۲/09	- 6 - 4 4 -	- 644 -0-	- 644 -	- 44 - 0	- 644 -	-0.44	-0-44	-C.44	-0-44	-0.44
MACH	1.10	X/08	5.49	5.49	5.49	5.49	5.49	64.5	5.49	5.49	5.49	5.49	NACH	1.100	X/CB	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49	NACH	1.102	X/C9	5.49 -	5.49 -	5.49 -	5.49 -	- 64•5	5.49 -	5.49 -	5.49 -	5.49	5.49 -
TST P IN CONF	571 1 66 5	MACH 0	1.102 269.3	1.106 269.9	1.101 269.1	1.101 269.1	1.101 269.1	1.098 268.4	1.058 268.4	1.056 268.1	1.096 268.1	1.054 268.C	TST P TN CCNF	571 1 66 5	MACH C	1.100 270.7	1.058 270.6	1.098 270.6	1.098 270.6	1.099 270.4	1.097 270.2	1.094 269.6	1.059 270.4	TST P IN CONF	571 1 66 5	MACH Q	1.102 271.0	1.102 271.C	1.105 271.6	1.108 272.2	1.110 272.4	1.102 271.0	1.100 270.7	1.097 270.2	1.095 269.9	1.058 270.C
RUN	336	SEQ	~	r	4	S	9	-	ထ	σ	10	11	RUN	155	SEC	-	<i>د</i>	<b>f</b> r	4	ŝ	9	~	80	RUN	338	SEQ	7	2	m	4	<b>u</b> n	Q	~	ω	σ	10

		CP PF/P	0.185 1.158	0.177 1.150	0.156 1.132	0.153 1.129	0.159 1.135	0.159 1.135	0.155 1.131	0.220 1.185				CP PF/P	0.054 1.034	0.053 1.034	0.041 1.026	0.043 1.027	0.038 1.024	0.029 1.018	0.023 1.014	0.055 1.034				Cp pF/p	0.046 1.029	0.038 1.024	0.028 1.018	0.016 1.010	0.006 1.004	-0.005 0.997	-0-001 0-999	0.001 1.001	0.005 1.003	0.028 1.018
		VA/V												V A / V												V A /V						•	•			
ALPHA	0.00	0A/Q VF/V	0.888	0.836	0.282	0.150	0.134	0.358	0.650	0.382		ALPHA	0.00	CA/Q VE/V	0*646	0.848	0.117			0.243	0.566	0.947		ALPHA	0.00	QA/Q VF/V	0.963	0.892	0.936	0.875	0.838	0.802	0.783	0.806	0.852	0.955
11	73.9	0F/0	0.868	0.749	0.074	0.021	0.016	0.120	0.420	0.874		11	73.8	CF/O	0.915	0.708	0.012			0.051	0.290	0.911		11	74.1	GF/0	0.941	0.786	0.873	0.743	0.668	0.602	0.573	0.612	C.694	0.914
<u>م</u>	320	M / M										۵.	388	M / M										۵	387	n/vn										
ى	272.5	NL / N	C.866	C.8C7	C.256	C.135	c.121	C.325	0.605	0.859		U	245+7	NF / N	C.941	C.827	0.108			C.224	C.534	526.0		ى	246.3	NF/N	<b>C.</b> 956	C.876	C.926	C.857	0.816	C.777	0.757	0.782	0.832	0.948
Ld -	686	2/08	-1.03	-0.53	-0-02	0.14	0.31	0.47	0.64	9.98		1d	0 695	2/08	-1.03	-0.53	-0.03	0.14	0.31	0.47	0.64	35*0	)   	L PT	0 695	2/DB	-1.04	-0.70	-0.54	-0.21	-0.04	0.12	0.29	0.46	0.63	0.96
I/Vd	1.51	×/08	c. C2 -	C.C2 -	C.02 -	c.c2	<b>C°</b> C2	<b>C-</b> C2	C - C 2	0-02		L/NA	1.480	۲/PB	0.02 -	c. C2	C.C2 -	C. C2	C. C.2	0.02	C. C2	C• C2	, , ,	INA I	1.48	Y/DR	0.44 -	0.44 -	0.44 -	0.44 -	0.44	C.44	0.44	0.44	0.44	0.44
N N C H	5 <b>1.1</b> 03	X/CB	3.52	3.52	3.52	3.52	3.52	2.52	3.57	3.57		- NACH	0.951	X/CB	3.52	5.52	3.52	3.52	3.52	5.57	1 2 2	C 1	1	E NACH	5 0 .953	X / 0.B	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49
TST P IN CONF	571 1 66 5	MACH C	.103 272.5	.101 272.2	.058 271.7	.099 272.1	100 272 3	100 272 3	7.17C 800	064 271.4	- - - - - - - - - - - - - - - - - - -	TST P IN CONF	571 1 66 5	MACH C	951 245.7	951 245-7	1.950 745.8	949 245 4	949 245 4	0-245 745	1.947 245.0	947 245 0		TST P TN CCNF	571 1 66	MACH Q	1.953 246.3	.954 246.8	0.952 246.3	0.951 245.7	.951 245.7	0.951 245.7	1.951 245.7	1.949 245.3	.949 245.3	0.949 245.3
RUN	6	C E C		2 1		4	י ר י גי	· -		- a	>	RUN	340	U L V		10	2 F	1	, c 			- α	2	RUN	341	S E C		2	ŝ	4	u	9	-	8	5	10 (

OR	IGINAL	PAGE	IS
OF	POOR	QUALI'	Γ <b>Y</b> ;

CP °F/P 0.036 1.023 0.022 1.014 0.002 1.011 -0.010 0.594 -0.007 0.995 -0.004 0.598 -0.004 0.598 0.030 1.019	CP PF/P 0.046 1.029 0.032 1.029 0.005 1.029 0.001 1.001 0.001 1.001 0.001 1.001 0.001 1.001 0.003 1.006 0.031 1.020	CP PF/P 0.016 1.010 0.008 1.005 -0.016 0.993 -0.016 0.993 -0.015 0.991 -0.006 0.995 0.009 1.006 0.014 1.009
V A / V	V A / V	N N N
ALPHA 0.00 0.400 0.910 0.879 0.879 0.879 0.879 0.661 0.661 0.661 0.661 0.705 0.726	ALPHA 0.00 0.4/0 VF/V 0.955 0.834 0.837 0.837 0.837 0.837 0.855 0.855 0.855 0.855	ALPHA 0.00 0.400 0.830 0.830 0.830 0.779 0.767 0.767 0.762 0.763 0.917
74.4 0.822 0.457 0.457 0.457 0.457 0.457 0.457 0.457 0.457 0.457 0.852 0.852 0.852	TT 74.5 74.5 74.5 0.870 0.870 0.870 0.870 0.870 0.595 0.595 0.595 0.529 0.529 0.503 0.909	11 74-7 74-7 0-856 0-8563 0-5535 0-5335 0-5335 0-5335 0-5335 0-5335 0-825
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	388 7 4 7 4	2 0 0 7 0 0 7 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
CCNF MACH RN/L PT C 5 0.952 1.480 695 246.3 X/DB Y/DB Z/DB WF/N X/DB 7/DB 2/DB WF/N 5.49 0.00 -1.04 0.896 6 5.49 0.00 -0.54 0.861 8 5.49 0.00 0.13 0.636 8 5.49 0.00 0.13 0.636 8 5.49 0.00 0.13 0.636 8 5.49 0.00 0.13 0.637 3 5.49 0.00 0.29 0.631 8 5.49 0.00 0.13 0.637 8 5.49 0.00 0.13 0.631 8 5.49 0.00 0.52 0.740	CFNF WACH RN/L PT C 5 0.952 1.480 695 246.3 X/FB Y/DB Z/DB WF/N X/FB -0.44 -1.05 C.960 5 49 -0.44 -0.70 C.924 5 49 -0.44 -0.20 C.816 771 5 49 -0.44 0.25 C.777 8 5 49 -0.44 0.25 C.777 8 5 49 -0.44 0.96 0.944 5 49 -0.44 0.96 0.944	CCNF MACH RN/L PT C 5 0.953 1.481 596 246.8 X/CB V/DB Z/DB MF/W K/CB C 2002 -1.05 C.920 6.99 -0.02 -1.05 C.920 6.99 -0.02 0.12 0.753 6.99 -0.02 0.12 0.774 6.99 -0.02 0.44 C.735 6.98 -0.02 0.44 C.735 6.98 -0.02 0.44 C.735
T P TN C CH 245 52245 50245 50245 50245 50245 50245 50245 50245 50245 50245	ST P TN 71 1 66 952 246 952 246 952 246 952 245 950 245 949 245 949 245 950 245	ST P TN 71 1 66 953 246 954 246 954 246 953 246 953 246 953 246
N 24 2 N 24 2	и	<b>Ν Ψ Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν Ν</b>

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PF/P 1.014 1.014 1.004 0.993 0.998 0.998 0.998 1.001 1.001 1.001 1.001	95770 1.0017 1.0017 1.0017 1.0003 1.0003 1.0005 1.0005 1.0005 1.0005
CP 0.024 0.0064 -0.012 -0.003 -0.003 0.003 0.003 0.003 0.036	0.038 0.038 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
∧ ∧ ∨ ∧ ∧	∧ v v
ALPHA 0.00 0.00 0.932 0.370 0.794 0.765 0.765 0.779 0.837 0.922	AL PHA 0.00 0.00 0.920 0.861 0.690 0.691 0.691 0.796 0.729 0.729
7 1 1 7 4 5 0 6 7 7 0 0 6 7 3 1 0 6 5 7 9 0 6 5 7 9 0 8 4 8 0 8 4 8	741 741 00.8744 00.4244 00.4244 00.4441 00.4440 00.4441 00.884
р 421 МА/М	423 47.3
<pre>MACH RN/L FT C MACH RN/L FT C 0.902 1.489 714 235.8 X/CB Y/DP Z/CP MF/W 6.99 -0.02 -1.05 C.922 6.99 -0.02 -0.05 C.854 6.98 -0.02 -0.04 C.771 6.98 -0.02 0.12 C.74C 6.98 -0.02 0.12 C.74C 6.98 -0.02 0.45 C.711 6.58 -0.02 0.63 C.817 6.58 -0.02 0.63 C.817 6.58 -0.02 0.63 C.817 </pre>	<pre>*ACH RN/L PT G 0.897 1.485 713 238.1 X/CB Y/CE Z/DB MF/W 5.49 C.00 -1.04 0.909 5.49 C.00 -1.04 0.909 5.49 C.00 -1.04 0.909 5.49 C.00 0.13 0.663 5.49 C.00 0.30 C.651 5.49 C.00 0.30 C.651 5.49 C.00 0.30 C.651 5.49 C.00 0.30 C.651</pre>
RUN TST P TN CONF 345 571 1 66 5 560 MACH 0 1 0.902 239.8 2 0.904 240.2 4 0.904 240.2 5 0.904 239.6 6 0.903 239.2 7 0.905 240.0 8 0.905 240.0	RUN TST P TN CCNF 346 571 1 66 5 510.897 238.1 2 0.896 237.6 3 0.898 238.0 4 0.898 238.6 6 0.900 238.4 7 0.900 238.4 8 0.901 238.4

	0 E / D	1-046	1-040	1.044	1 - 0 - 1	1-037	1.030	1.018	1 . 042
	e	0-081	0.071	0.078	620.0	0.065	0-053	0.032	0-074
	V A / V	•							
	VF/V	0.939	0.776	0.000		0.115	0.341	0.613	0.940
0.00	0 A / O	1							
74.7	QF / Q	0.904	0.588	0000-0		0.012	0.105	0.348	0.903
421	MAJW								
238.5	NF / N	C.930	c.752	C-00C		c.107	0.319	C.585	156.0
5 713	Z / DB	-1.03	-0.53	-0-03	0.15	0.30	0.47	0.64	0.58
1.480	Y/DB	0.02 -	c. C2 -	0.02 -	0.02	C• C 2	0.02	<b>C • C</b> 2	c.c2
006*0	X / 0B	3.52	3.52	3.52	3.52	3.52	3.52	3.52	3.52
50	C	38.9	38.9	38.5	38.0	18.0	18.0	<b>5</b> •8	5 <b>9.</b> 4
7116	IACH	900 23	,900 23	899 23	898 21	.898 23	898 23	900 23	<b>901 2</b> 3
	71 1 66 5 0.900 1.486 713 238.9 421 74.7 0.00	71 1 66 5 0.900 1.486 713 238.9 421 74.7 0.00 ICH Q X/DB Y/DB Z/DB MF/M MA/M GF/Q QA/Q VF/V VA/V CP DF/D	71 1 66 5 0.900 1.486 713 238.9 421 74.7 0.00 1CH Q X/DB Y/DB Z/DB MF/M MA/M QF/Q QA/Q VF/V VA/V CP DF/D 100 238.9 3.52 0.02 -1.03 0.930 0.9064 0.939 0.081 1.046	71 1 66 5 C.900 1.486 713 238.9 421 74.7 0.00 CH Q X/DB Y/DB Z/DB MF/M MA/M GF/Q QA/Q VF/V VA/V CP DF/D 100 238.9 3.52 0.02 -1.03 C.930 0.904 0.939 0.081 1.646 100 238.9 3.52 C.C2 -0.53 C.752 0.588 0.776 0.071 1.640	71 1 66 5 C.900 1.486 713 238.9 421 74.7 0.00 CH Q X/DB Y/DB Z/DB WF/W MA/M GF/Q QA/Q VF/V VA/V CP PF/P 100 238.9 3.52 0.02 -1.03 C.930 0.904 0.939 0.776 0.031 1.646 100 238.9 3.52 C.C2 -0.53 C.752 0.588 0.776 0.071 1.640 199 238.5 3.52 C.C2 -0.63 C.000 0.000 0.000 0.078 1.644	71 1 66 5 C.900 1.486 713 238.9 421 74.7 0.00 CH Q X/DB Y/DB Z/DB WF/M MA/M GF/Q QA/Q VF/V VA/V CP PF/P 100 238.9 3.52 0.02 -1.03 C.930 0.904 0.939 0.031 1.046 100 238.9 3.52 C.C2 -0.53 C.752 0.588 0.776 0.031 1.040 199 238.5 3.52 C.C2 -0.03 C.000 0.078 1.044 198 238.6 3.52 C.02 0.15	71 1 66 5 0.900 1.486 713 238.5 421 74.7 0.00 CH 0 X/DB Y/DB Z/DB MF/M MA/M QF/Q 0A/Q VF/V VA/V CP PF/P 100 238.9 3.52 0.02 -1.03 0.930 0.904 0.939 0.071 1.046 100 238.5 3.52 0.02 -1.03 0.930 0.9588 0.776 0.939 0.071 1.046 100 238.5 3.52 0.02 -0.03 0.772 0.588 0.776 0.073 1.044 198 238.0 3.52 0.02 0.15 198 238.0 3.52 0.02 0.15 100 0.012 0.012 0.015 0.073 1.041	1       66       5       0.900       1.486       713       238.5       4.21       74.7       0.000         1       0       X/DB       Y/DB       Z/DB       MF/M       QF/Q       0.40       VA/V       CP       PF/P         1       0       X/DB       Y/DB       Z/DB       MF/M       QF/Q       0.40       VA/V       CP       PF/P         100       238.9       3.52       0.02       -1.03       C.930       0.939       0.071       1.646         100       238.9       3.52       0.053       C.752       0.568       0.776       0.071       1.646         100       238.5       3.52       C.023       C.752       0.588       0.776       0.071       1.646         199       238.6       3.52       C.02       0.105       0.105       0.015       0.073       1.641         198       238.0       3.52       C.62       0.36       0.47       0.319       0.053       1.037         198       238.0       3.52       0.47       0.319       0.105       0.341       0.053       1.037	1       66       5       C.900       1.486       713       238.9       421       74.7       0.000         1       0       X/DB       Y/DB       Z/DB       WF/W       MA/W       GF/G       0.400         1       0       X/DB       Y/DB       Z/DB       WF/W       MA/W       GF/G       0.00         100       238.9       3.52       0.02       -1.03       C.930       0.939       0.071       1.646         100       238.9       3.52       0.053       C.752       0.588       0.776       0.071       1.646         100       238.5       3.52       C.022       -0.053       C.752       0.588       0.776       0.071       1.646         199       238.6       3.52       C.022       0.15       0.015       0.012       0.073       1.641         198       238.0       3.52       C.027       0.35       0.015       0.015       0.013       1.641         198       238.0       3.52       C.027       0.365       0.015       0.015       1.037         198       238.0       3.52       C.02       0.364       0.341       0.032       1.037         198<

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CP 0.279 0.2843 0.2843 0.2845 0.2845 0.2845 0.2845 0.2845 0.2851 0.2770 0.2770 0.2770	CP CP 0.033 0.008 0.003 0.003 0.003 0.003 0.003 0.015 0.015	CP 0.043 0.0055 0.001 0.013 0.013 0.013
V A / V	~~~~	V A/V
ALPHA 0.00 VF/V 0.459 0.859 0.859 0.857 0.856 0.858 0.858 0.864 0.864 0.864 0.864	ALPHA 0.00 04/0 VF/V 0.914 0.851 0.784 0.782 0.782 0.800 0.846 0.846 0.846	ALPHA 0.00 0.00 0.910 0.846 0.846 0.846 0.846 0.846 0.693 0.693 0.693 0.693 0.693 0.693
11 75.8 0.857 0.857 0.855 0.855 0.855 0.855 0.855 0.855 0.856 0.871 0.871	74.7 74.7 74.7 74.7 0.939 0.939 0.939 0.939 0.585 0.580 0.580 0.610 0.886 0.886	74.3 677,0 677,0 0.696 0.696 0.447 0.447 0.533 0.533 0.661 0.885
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		V A /V											V A /V											V A /V					,					
ALPHA	0.00	QA/Q VF/V	0.934	0.734	0.179	0.057	0.249	0.388	0.678	0.942	ALPHA	0.00	DA/Q VF/V	0.915	0.140	0.261	0.232	0.318	0.511	0.717	0*6*0	ALPHA	0.00	DA/Q VF/V	0.980	0.898	0.921	0.851	0.838	0.819	0.834	0.862	0.907	0 0 U
ŢŢ	74.2	0F/0	0.889	0.525	0.029	0.003	0.056	0.138	0.439	0.910	11	74.0	0 L 10	0.847	0.536	0.063	0.049	0.093	0.244	0.495	106*0	11	73.9	QF / Q	0.970	0.796	C.840	0.705	0.676	0.645	0.670	0.720	0.809	200 0
٩	457	MA/M									۵.	500	MA/M									٩	500	MA/N										
U	231.6	ME/N	<b>C.</b> 926	c.711	0.168	C.054	0.233	C.366	0.653	C•934	(J	225.4	MF / N	<b>C.</b> 906	C.720	C•247	0.219	C.3C1	0.488	C.696	C.934	U	225.4	NF/N	0.978	C.887	0.912	0.836	0.823	0.802	0.818	C.848	0.897	130 0
L PT	6 733	Z/08	-1.03	-0.53	-0.02	0.14	0.31	0.47	0.64	0.98	L PT	6 764	2/08	-1.03	-0-53	-0-03	0.14	0.31	0.47	0.64	10.97	L PT	7 764	Z/CP	-1.04	-0.71	-0.54	-0.21	-0.04	0.13	0.29	0.46	0.63	
- RN	1.1.49	Y/08	C. 02 -	C. C2 -	C•02	<b>c.</b> c2	C.02	C• C2	0.02	0.02	IN a F	2 1.51	Y/DB	C.02	C• C2 ·	C.02	C.02	C•C2	0.02	<b>C•</b> C2	20.02	I/Va +	1.51	Y/08	C.44 -	0.44	0.44	0.44 -	0.44	0.44	0.44	C.44	0.44	17 U
	0.85	X/CB	3.52	3.52	3.52	3.52	3.52	3.52	3.52	3.52	IDVN :	5 0.801	X/D8	3.52	3.52	3.52	3+52	3.52	3.52	3.52	3.52	: NACH	0.802	X/08	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49	5.49	27
TST P TN CCNI	571 1 66	MACH Q	0.851 231.6	0.851 231.6	0.851 231.6	0.850 231.3	0.850 231.3	0.850 231.2	0.850 231.3	0.849 230.5	TST P IN CONF	571 1 66	MACH C	0.802 225.4	0.801 224.9	C.8C0 224.4	0.800 224.4	0.801 224.9	0.802 225.4	0.801 224.9	0.800 224.4	TST P TN CONF	571 1 66	MACH Q	C.802 225.4	0.802 225.4	C.8C1 224.5	C.8CI 224.9	0.799 224.4	0.799 224.4	0.758 223.9	0.758 223.5	0.798 223.5	0 700 777 0
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	VA/V	2 A / 2
LPHA 0.00 VF/V 0.903 0.720 0.720 0.720 0.768 0.768 0.832 0.832	ALPHA 0.00 0.00 0.978 0.938 0.868 0.810 0.868 0.810 0.779 0.779 0.843 0.843 0.901 0.966	ALPHA 0.00 0.00 0.360 0.360 0.360 0.300 0.307 0.307 0.307 0.319 0.319 0.319 0.354
TT A 73.7 0.67.0 0.696 0.696 0.6485 0.485 0.485 0.668 0.564 0.564 0.564 0.564	71 73-8 73-8 0-965 0-965 0-876 0-876 0-627 0-576 0-576 0-533 0-937	P TT 500 73.6 0.825 0.825 0.612 0.622 0.646 0.622 0.646 0.622 0.646 0.622 0.646 0.622 0.646 0.622
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V CP PE/P	0.019 1.005	0.006 1.002 -0.006 0 690	-0-008 0-998	-0.001 1.000	-0.009 0.598	-0.010 0.998	0.013 1.003			V CP PF/P	0.017 1.004	0.006 1.002	0.002 1.000	-0.006 0.598	-0.004 0.599	0.002 1.000	0.014 1.003	0.012 1.003	0.012 1.002	0.010 1.002			V CP PF/P	0.013 1.003	0.013 1.003	-0.006 0.598	-0.007 0.598	-0.006 0.598	-0.004 0.599	0.007 1.002	0.008 1.002
ALPHA 0.00 04/0 VF/V VA/	0.924	0.866 0.817	0.817	0.840	0.851	0.877	0.932	ALPHA	0.00	CA/Q VE/V VA/	0.982	0.909	0.922	0.869	0.840	0.843	0.838	0.866	0.689	0.968	ALPHA	0.00	DA/Q VF/V VA/	0.925	0.846	0.758	0.772	0.785	0.327	0.845	0.953
P TT 700 64.6 MA/M 0F/0	0.850	0.651	0.650	0.690	C.708	0.755	0.863	LL d	697 65.0	MA/N OF/Q	0.965	0.817	0.841	0.741	0.691	169.0	C• € 89	0.740	0.782	0.935	11 c	698 65.3	MA/N QF/0	0.849	0.703	0.557	0.578	0.558	0.668	0.702	0* 603
NF MACH RN/L PT C 5 0.597 1.510 891 174.7 X/CB Y/CB Z/DB MF/M	6.99 -0.02 -1.05 C.920	728-0 44.01 20-01 44.00 728-0 40-01 20-01 44.00	6.99 -0.02 0.12 0.807	6.99 -C.C2 0.29 C.831	6.99 -0.02 0.45 C.842	6.99 -0.02 0.61 C.870	6.99 -C.C2 0.96 C.928	NF MACH RN/L PT C	5 0.602 1.519 891 177.1	X/CB Y/DB Z/CE MF/N	5.49 C.44 -1.C4 C.98C	5.49 0.44 -0.71 C.903	5.49 0.44 -0.54 C.917	5.49 C.44 -0.21 C.862	5.49 0.44 -0.04 C.831	5.49 C.44 O.12 C.835	5.49 0.44 0.29 C.829	5.49 0.44 0.47 C.859	5.49 C.44 0.63 C.883	5.49 0.44 0.97 C.966	NF WACH RN/L PT Q	5 0.601 1.515 891 176.5	X/DB Y/DB Z/DB MF/M	5-49 0.00 -1.04 0.920	5.49 C.CO -0.54 C.837	5.49 0.00 -0.04 0.747	5.49 0.00 0.13 0.761	5.49 C.CC 0.30 C.774	5.49 0.00 0.46 C.818	5.49 0.00 0.62 0.837	5.49 0.00 0.96 0.949
RUN TST P TN COI 357 571 1 66 SEQ MACH 0	2 0.557 174.7	4 0-557 174.7	5 0.598 175.3	6 0.601 176.5	7 0.600 175.9	8 C.6C0 175.5	9 0.600 175.9	RUN TST P TN CCI	358 571 1 66	SEC MACH C	1 0.602 177.1	2 0.602 177.1	3 0.601 176.5	4 0.603 177.1	5 0.603 177.1	6 0.601 176.5	7 0.600 175.9	8 0.557 174.7	9 0.598 175.3	10 0.598 175.3	RUN TST P TN CCI	359 571 1 66	SEC MACH Q	1 0.601 176.5	2 0.601 176.5	3 0.601 176.5	4 0.601 176.5	5 0.601 176.5	6 0.601 176.5	7 0.601 176.5	8 0.601 176.5

. . ......

		0F / D	1 - 002	1.000	1.000	1.000	0.999	0.999	0.999	1.00.1	1.00.1	1.003		
		đ	0-008	0.002	0.002	-0.001	-0.003	-0.002	-0-004	0.003	0-003	0.013		
		VAVV												
		VF/V	0.983	0.935	0.873	0.820	0.806	0.811	0.835	0.864	0.892	0.958		
AL PHA	0.00	0A/0	1				-	-		-	-			
11	65.6	QF/Q	0.965	0.867	0.750	0.657	0.633	0.642	0.681	0.733	0.785	0.915		t t
٩	698	MA/M												c
ى	176.5	NF/N	196.0	:.931	3.866	C.81C	.796	0.801	3.826	.856	3.886	.955		¢
Ld	891	2/CB	1.04 (	0.71 (	0.54 (	0.20	0.04 (	0.13 (	0.29 (	0.47 (	0.63 (	0.97 (		10
PN/L	1.514	(/08	0.44 -	- 44 -	- 44 -	- 55*(	)•44 -	.44	.44		.44	.44		0 1/ 1/
NACH	0.601	(/0B	- 65*	- 65 -:	- 65 -	- 65 - 9	- 65*:	- 65*	- 49 -(	- 65 -	- 49 -(	)- 65*		N N L
CCNF	<b>U</b> T	Ŷ	ي در			<u>د</u> ،	ur •	ŝ	<u>ب</u>	un un	5	5		U N U U
NL d .	1 66	о Н	1 176	2 177	2 177	1 176	1 176	1 176	1 176	1 176.	0 175	0 175.		DTA
TST	571	MAC	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	C• 60		TCT
RUN	360	S E C E C		<b>∼</b> ∶	( <b>7</b> 7)	4	Ľ	Ŷ	~	œ	σ.	10		A LA

.00 /0 VF/V V	10 VF/V V
0.00 04/0 VF/ 0-94	24/0 VF/ 0-94
0 0 0 0.	10 0A/
65.9 0F/0 1.901	ηF/Ω 1.901
29 00 24 26	200
69 MA/	N A /
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	d/∃u	1.000	1.000	1.000	0 <b>•</b> 999	1.000	1.000	1.000	1.000
	d C	0.001	-0.010	-0.001	-0.012	-0.010	-0.008	-0.010	-0.001
	V A /V	0•000	0.000	0.000	0-000	0.000	0.000	0.000	0.000
	VF/V	0.960	0.806	0.538	0.616	0.670	0.754	0.824	0.970
ALPHA 0.000		0.000	0.00.0	000.0	c. 000	0.000	c.000	0.000	000.0
11 64_8	0E/0	0.920	0.647	0.287	0.376	0.445	0.566	0.676	0.941
0 1794	N V N	0.00.00	000.0	000.0	0.000	000.000	0000-0	000.0	000.00
74 74 7	N L / N	C. 955	0.804	C.536	0.614	9.668	c. 752	0.823	C. 97C
1975	Z/CB	1.03	0.53	0.02	0.14	0.31 (	0.48	0.64	0.58
RN/L	Y708	c.c2 -	C.02 -	c. c2 -	<b>C</b> •02	C• C2	0.02	c. 02	<b>c.</b> 02
NACH 0-251	x/58	3.52	3.52	3.52	3.52	3.52	3.52	3.52	2.52
N CCNF	0	9.4	8•8	9.4	8•8	8•8	8.8	8.8	8°8
ST P T 71 1 6	IACH C	251 7	250 7	252 7	250 7	250 7	250 7	250 7	250 7
RUN T 342 5	SEQ M	1 0.	2 0.	ວ ຕ	4 C.	о. А	6 0 <b>.</b>	7 0.	8 0 8

1.000 666.0 665 °0 665 °0 865 °0 865 °0 865 °0 865 °0 865 °0 L -0.032 -0.025 -0.025 -0.010 -0.041 -0.034 -0.021 СÞ 0.976.0 0.915 0.864 0.834 0.837 0.804 0.389 0.920 0.946 VF/V ALPHA 0.00 0.000 C. 000 0A/Q 0.000 0.0000 0.0000 TT 64.6 0F/0 0.951 0.825 0.825 0.834 0.443 0.443 0.443 0.443 0.443 0.8592 0.8592 0.8592 0.8592 0.8593 0.853 р 1794 Мд/м 78.8 MF/8.8 MF/8.6 C.975 C.975 C.914 C.914 C 833 C 833 C 833 C 833 C 853 NF MACF PN/L PT 5 C-250 1.51C 1874 X/CB Y/CB 2/CB 5.49 C-44 -1.04 0 5.49 C-44 -0.70 0 5.49 C-44 -0.70 0 5.49 C-44 0.12 0 5.49 C-44 0.12 0 5.49 C-44 0.12 0 5.49 C-44 0.29 0 5.49 C-44 0.47 0 5.49 C-44 0.47 0 4 エンじじ  $\mathbf{x} = \mathbf{x} =$ 571 1 571 1 571 1 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 

665°0 6666°0 866°0 866°0 666°0 666°0 0.999 -0.028 -0.024 -0.032 -0.019 -0.024 СР -0.014 -0.040 0.928 0.849 0.799 0.800 0.800 0.808 0.833 0.833 0.833 VF/V 64.6 6770 0.850 0.718 0.634 0.636 0.6536 0.6536 0.731 0.731 4 75.4 1794 MF/N MA/W C.928 0.000 C.928 0.000 C.928 0.000 C.398 0.000 C.398 0.000 C.831 0.000 C.831 0.000 0.000 0.000 0, 757 C, 758 C, 758 C, 831 C, 831 C, 530 C, 530 NF WACH RN/L PT 5 0.252 1.517 1874 X/DB Y/DB 7/D8 7/D8 5.49 0.00 -0.54 0 5.49 0.00 0.13 0 5.49 0.00 0.13 0 5.49 0.00 0.29 0 5.49 0.00 0.29 0 5.49 0.00 0.29 0 TST P 571 1 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 0.252 8 U N 3 6 4 5 E Q -1 n n n n n n n n n

		06 10	000	000	000		000		000	000			665*0				DF/D	999	665	998	598	.598	665	666	666
		a	-0-014 (	-0-0-									-0-016				съ С	-0-014 0	-0-034 0	-0-039 0	-0-043 0	-0-046 0	0-034 0	-0-032 0	-0.028
		V / / V	0.000	0.000		0.000							- CCC - O				VAVV	0.000	0.000	0.000 -	0.000	0.000-0	0.000	0.000-0	0.000
		VF/V	0.967	0.917	0.44.8	0.821	0 - 841		1 1 0 - 0 0 - 3 4 0	0.851	320.0		0.908				VE/V	0.930	0.856	0.331	0.830	0.374	0.867	0. 304	0.935
AL PHA	0.00	OA/O	0.000	0.000	C-000	0.000	0.000	0.000	0.000	0,000	00000		0.000		ALPHA	0.00	O/A/O	c.000	0.000	0.000	000.0	c. 000	0.00.0	0.000	C.000
Ŧ	64.5	QF/Q	0.934	C. 829	0.715	0.670	2-704	0.654	0.718	0.721	0.878		0.935		1 T	64.4	0F70	C.862	0.729	0.686	<b>C.</b> 684	0.761	0.748	0.743	C.871
۵	1794	M V M	0.000	0.000	0.000	0.000	0.00.0	0.000	0000-0	0.000	000000		0.000		۵.	1794	M / M	0.000	0.00.0	0.000	0.000	000.0	0.000	0.000	0.000
G	78.8	MF/W	C.967	C.911	0.846	0.815	0.835	0.809	0.848	0.850	0.528		<b>7.</b> 568		e	78.8	NF / N	C.929	<b>C.85</b> 4	C.825	C.828	C.873	0.866	C.863	C.934
t pŢ	1 1874	2/28	-1.05	-0.71	-0-54	-0.20	-0.04	0-12	0.29	0.46	0.63		0•96		L of	1 1874	Z/08	-1.05	-0.56	-0-05	0.12	0.29	0.45	0.61	0.95
H RN/	0 1.51	X/CB	-0.44	-0-44	-0.44	-0.44	-0-44	-0-44	-0-44	-0.44	-C.44		-C - 4 4		INd H	0 1.51	Y/DB	-0.02	-0-02 -	-0-02 -	-0.02	-0.02	-0.02	-0-02	-0-92
F NAC	5 0.25	X/CB	5.48	5.48	5.49	64 • 5	5.49	1. 19	5.49	5.49	5.49		84 87		LAN -	5 0.25(	X / 5.8	6.98	<b>6.98</b> -	- 85 - 9	ۥ 58 -	6.98 -	6.98 -	- 85 -3	<b>6.</b> 98 -
TN CCNI	56	Q	78.8	78.8	78.8	78.8	79.4	78.8	19.4	79.4	78.8	0 0	2.2		IN CONF	56	o	<b>18.</b> 8	18.1	1.8.1	18.1	8.8	8.8	8.8	8.8
TST P	571 1	MACH	1.250	1.250	. 250	.250	1.252	. 250	.252	.252	1.250	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0524		TST P	571 1 6	MACH	.250	.249	.249	- 249	.250	.250	.250	.250 3
RUN	365	SEG	1	20	5	4	5	9	7 0	8	6				NUN	366	SEC	1 0	2 0	0	4	5	6 0	7 0	8

Table 2(d)

 $\label{eq:configuration} \begin{array}{l} \text{Configuration 7}-\text{Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section} \\ & \text{aft-facing pitot-static probe.} \end{array}$ 

		pF/p	0-740		+TI •0	0.698	0.697	0-704		101.0	0.795	0.847	016		0.2.0	1.008	1.026		0 30 • 1
		c b	-0-411		164.0-	-0.477	-0.479	944-0-		-0.424	-0.325	-0-242		20 T • 0 -	-0.40	0.012	170 0		**0*0
		V A / V	rrc 0		622.0	0.171	0.239	216		0.401	0.372	0.368		0.200	0.044	0.00.0			0.000
		VF/V	L 76 0	-+7+0	0.334	0.340	0.381	292.0	0.400	114.0	0.460	0 408		662.0	0.000			0.000	0.00
ALPHA	0.00	O V O		n+0 •0	0.031	0.017	0.034		100.0	0.105	0-095		C+C2-2	C.051	0.002	0000			000-0
11	66.2	06/0		C. U34	0.069	0-069	C 80 0		0.134	0.168	0-147		C71.0	c.050	0.000			0.000	0.000
D	381	2 / 2		0.256	0.208	0-157	0 221	100.0	+62.0	0.379	0.346		0.342	0.236	0.040	VUC O			0.000
ى	241.7	NE / N		0.228	0.310	215			0.436	0.480	064 0		C.381	0.234	0000-0			0000	c• 000
١d	683		2772	0.18	0.18 (			01-10	0.18 (	0.18 (	~ ~ ~ ~		0-11	0.17	0.17		0.17	0.16	0.16
PN/L	1 480		202		1010			00.0	00.00	0.01			<b>c. c1</b>	0.01	0-02		0.02	0.02	0.03
N O C H	051		GB</td <td>- - - - - - - - - - - - - - - </td> <td>Ca c</td> <td></td> <td>1.1.4</td> <td>1.40</td> <td>1.69 -</td> <td>1.98 -</td> <td></td> <td>07.07</td> <td>2.55 -</td> <td>2.85 -</td> <td>- 13 -</td> <td></td> <td>3.44 -</td> <td>3.72 -</td> <td>- 10.4</td>	- - - - - - - - - - - - - - - 	Ca c		1.1.4	1.40	1.69 -	1.98 -		07.07	2.55 -	2.85 -	- 13 -		3.44 -	3.72 -	- 10.4
L L N F	-	-		~		. r	- 1	•	<b>m</b>		• •	7.	۲۷ •	-2		•	•	- 1	• 2
DIN			с н	1 241	1 2 1		0.47 0	0 240	9 240	1 241		1 241	1 241	1 241	176 1	113 1	51 241	51 240	52 241
TCT		1 6	M A C	0,05			C • 4 2	36°0	0-94	000		0.45	0.95	50.0		1 1 2	0.9	0.95	0.95
NIIG		367	500	5	16	<b>.</b> .	4	S	9		-	æ	σ		•		27	13	14

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		DF/D	<b>727 0</b>		0.708	0.692	202 0	0000	0.699	1272		0.184	0.849		225.0	176-0		1.03	1.024	1 022	7 7 7 7 7 7
		2		1 1 + • 0 -	-0.462	-0-488		-0.440	-0.476	124 0-		-0.341	020 0-		-0.124	-0-045		G00°0	0.038	320 0	
					0.256	0.178			0.250	C C C C		0.380	222		0.218	0.045		0.000			
		V L J V		117.0	0.362	308		0.362	0.395	077 0	104-0	0.434	C0C 0	000-0	0.233	0.00.0		0.000	0.000		000-0
ALPHA	0.00	0770		0.045	0.040	010		620.0	c. 050	F 00 0	1 20.0	0.098		010.0	0.037	000	2.00	0.000			
11	61.6			0.048	0.080		0.0	0.078	0.095		0.140	0.129		0.108	0.043			0.000	000		000.0
٩	381	MA AM		0.247	0.236		-01-0	0.191	0.269		0.346	0.354		0.300	0.201		1+0-0	0.000			
e	240.7		~~~	0.257	2220		1.22.0	0.337	872.0		C.439	2020		0.356	0.215		0.00.0	0000-0		2000-2	0000
La	681		2113	0.25	0.05		67.0	0.25	70 74	• •	0.24	76 0		0.24	0.74		0.23	0.23		07.0	0.23
PN/L	1.473		X / 13 H	0-01			00.00	00-00		00.0	0.01		1 · · ·	0.01	10.0		0.02	0.02		2.0 2	0.03
NACH	0.950		X/ 0B	0.53		(• 0 C	1.11	1-40	- 07 -	1.00.1	1.98 -		- 12.2	2.55 -	1 22 0	• •	3.14	- 44 -		1. 13	4.01 -
CCNF CCNF	-	•		2	- r	•		~	• 1 C	2.	~ ~ ~	1 6	7•1	-2		•	<b>1</b>	~		Z • ]	1.0
TPTN	1 1 44		HU	150 740		147 041	150 240	151 241		147 IG	151 241		147 ICF	151 241		113 004	348 241	151 74		951 24	950 24(
ALIN TS	720 57	10 000	SFQ MA			2 0.4	3 0.9			5 U•9	A 0,9		5 °C	8 0.9		い し ひ	10 0.9			12 0.5	13 0.9

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0.774 0.774 0.845 0.907 0.553 0.688 0.694 0.722 C19 0.995 1.019 0.694 PF/P -0.029 0.029 -0.485 -0.437 -0.358 -0.246 -0.147 -0.008 -0.495 -0-407 -0.485 -0.441 9 0.000 0.187 0.322 0.319 0.252 0.141 0.000 0.000 0.159 0.000 V & /V 0.289 0.263 0.065 0.000 0.286 0.272 0.184 0.221 .000 VF/V 0.289 0.00 ALPHA 0.025 C.000 C.021 **C.**063 c.015 c.000 0.005 0.046 0.00.0 0.000 0.020 0.029 0.052 0.052 0.000 0.053 0.026 0.003 68.8 0F/0 0.051 0.044 000 0.000 0.173 0.299 0.236 385 MA/M 0.000 0.184 0.000 0.130 ษา • 0.267 C.265 0.251 0.165 0.204 0.268 0.060 0.243 0.177 • 000 MF/N 000 243 6 0,38 0,38 0,38 ω F d . . 0.3  $\mathbf{O}$ F NACH RN/L Y/DP -0.02 -C.C2 -6.62 0.82 1.11 1.41 1.69 1.69 2.56 2.85 2.27 X/CB C.53 CCNF 243.1 243.6 243.6 243.6 243.0 243.0 243.5 243.5 243.5 243.0 243.0 243.0 243.1 2 Q L Q L Q 571 1 MACH α 0.949 0.949 0.949 0.949 0.949 0.949 0.949 0.949 0.949 0.949 0.949 0.950 0.952 0.952 0.950 51 0 m 4 6 9 4 9 9 7 m 1 m 1 m 1 m R U N 3 6 9 5 E Q

0.748 0.845 0.505 0.956 0.993 1.012 1.014 0.689 0.698 0.727 0.784 DF/D 0.721 0.696 -01--0.246 0.019 0.022 -0.434 -0.070 -0+402 -0-444 -0.484 -0-495 -0.479 -0.342 -0.011 ð 0.200 0.200 0.119 0.045 V A /V 0.151 0.000 0.212 0.177 0.160 0.000 0.070 0.053 000 VF/V 0 ALPHA 0.00 0.025 0.027 0.010 Q A A 0.002 69.6 67/0 0.029 0.019 0+015 0+000 0+003 C.014 0.000 0.185 0.184 0.109 0.042 386 VA/V ---C.148 C.000 D.064 00000 NF/W 0.196 0.164 0.139 . 049 000-242 C 2 688 2 7 0 8 0 • 5 0 0 • 5 0 0 • 5 0 0.49 0.49 0.49 0.49 0.49 ω F C. 0.48 0.48 0.48 4 . Ö F MACH RN/L 7 0.948 1.480 Y/nB -0.01 -0.02 -0.02 -0.02 1.11 1.41 1.69 0.53 C.82 1.98 2.27 2.55 2.55 2.85 2.44 2.44 X / CB 3.73 CONF ... 242.1 242.1 242.1 242.7 243.1 243.1 243.5 243.6 243.6 243.6 243.6 243.0 242.5 242.9 242.7 242.1 D TN 9 C 9 571 1 MACH 0.948 0.947 0.947 0.947 0.948 0.948 0.949 0.950 0.959 0.959 056-0 c 949 ST 5 O 370 SF0 120 NNa

7 0.899 1.4 X/CB Y/DB C.53 C.01 C.82 C.01 L.11 C.00	82 704 Z/DP 0.13 0.18 0.18 0.18	235.6 MF / M	416			~			
X/CB Y/DB C.53 C.01 C.82 C.01 L.11 C.00	Z/DP 0.13 0.18 0.18 0.18	<b>メ / エ</b> ズ	+	-	ノントン				
C.53 C.01 C.82 C.C1 L.11 C.00	0.18 0.18 0.18 0.18 0.18		MA / M	0F/0	QA/Q	VF/V	V 4 / V	CD	0/3d
C.82 C.C1 1.11 C.00	0.18 0.18 0.18	0.248	0.257	0.048	0.051	0.206	0.276	-0.395	0.777
1.11 C.00	0.18 0.18	C.298	0.173	0.066	0.022	0.319	0.186	-0.442	0.748
	0.18	0.345	0.168	0.087	C.021	0.368	0.181	-C.460	0.736
1.41 0.00		0.411	0.242	0.124	0.043	0.437	0.260	-0.461	0.736
1.69 -0.00	0.18	0.474	0.300	0.168	0.067	0.502	0.321	-0-447	0.746
1.58 -0.01	0.18	C.484	0.386	0.181	0.115	0.512	0.411	-0.398	0.774
2.27 -0.01	0.17	C.456	0.359	0.174	0.108	0.434	0.383	162.0-	0.835
2.56 -0.01	0.17	0.352	0.301	0.111	C.081	0.375	0.322	-0.182	0.897
2.85 - C. C1	0.17	C.207	0.201	0.041	C.038	0.222	0.216	-0.082	0.954
3.14 -0.02	0.17	0.054	0.070	0.003	0.005	0.059	0.076	-0.012	0.993
3.44 -0.02	0.17	c.000		00000		0.00.0		0.035	1.C20
3.73 -C.C2	0.16	0000		C.000		0.000		0.052	1.029
4.01 -0.03	0.16	0000-0		000.0		0.000		0.057	1.033

PF/D	0.789	0.743 0.743	0.731	0.736	0.766	0.820	0.873	0*6*0	0.982	1.019	1.035	1.039
٥	-0.370	-0.417	-0.475	-0.468	-0.414	-0.320	-0.224	-0.106	-0.032	0.034	0.062	0.068
V A /V	0.240	0.258	0.265	0.335	0.351	0.3£2	0.328	0.135	0.050			
VF/V	0.256	0.389 0.400	0.430	0.430	0.469	6.455	0.331	0.136	0.025			0.000
ALPHA 0.00 04/0	c. 039	0.059 0.032	C.045	0.072	0.082	C.U94	0.082	0.015	0.007			
TT 70.5 01/0	0.045	0.101 0.104	C.119	0.151	0.150	0.150	0.112	0.028	0.001			00000
4 1 4 4 1 4 7 4 1 4	0.224	0.279 0.208	0.247	0.313	0.328	0.339	0.306	0.126	0.033			
235.8 87.8	C. 239	0.365	0.404	0.453	C.442	C.428	0.357	0.173	C.023			0.000
PT 2702 2708	0.25	0.25	0.24	0.24	0.24	0.24	0.24	0.24	0.23	0.23	0.23	0.23
PN/1 1.479 7.08	C+ C1	0.01 0.00	00-0	0.00	10*0	0.01	0.01	0.01	0.02	C•C2	0.02	c• 03
WACH 0.902 X703	c - 53	C•82 L•11	1.41	1.69 -	1.58 -	2.27 -	2.56 +	2.85 -	3.14 -	3.44 -	3.73 -	4.01 -
CCNF 7	ω. •	4 U	•	• Ç	•6	• 0	•6	\$ •	0	4.	ω •	ω
P 11 1 66	2 235	1 235 9 235	9 235	8 234	8 234	8 234	8 234	8 234	9 235	1 235	2 235	2 235
TST 571 MACH	0-90	0.890	0.89	0.85	0.891	0.89	0.89	0.89	0.89	06.0	0.90	06 0
N C S S S S S S S S S S S S S S S S S S		ne pri	4	S	9	2	ധ	6	10	11	12	13

C.785 0.762 0.720 0.727 0.752 0.807 9.870 0.535 .986 0.736 1.019 m 0.785 DF/1 •03 1.031 o 0.058 0.033 -0.419 -0.466 -0-493 -0.436 -0.340 -0.229 -0.115 -0.025 -0.481-0.381 8 0.158 0.258 0.258 0.122 042 0.327 000 0.244 V V V . . o 0.314 0.206 0.299 0.295 0.233 0.200 0.193 6.318 VF/V 0.000 0.00.0 0.00 0.4/0 ALPHA 0.027 0.001 0.038 0.070 0.063 C.050 0.00.0 0.012 0.058 0.058 0.065 0.062 0.052 0.052 0.052 0.052 70.9 0F/0 0.061 000.000 000-0 0.039 0.278 MA/M 415 0.241 0.306 0.278 0.134 0.113 000.0 ٥ 235.0 MF/V C.276 C.297 0.293 C.179 C.192 00000 0.279 0.269 0.243 0000 702 Z/DB 0.40 0.40 0.40 F MACH RN/L 0.859 1.475 0.01 00.00 α C.01 -0.00 -0.02 115 X/DB • 69 . 58 2.56 2.85 .14 3.44 C.53 C.82 1.11 1.41 . 73 -01 5 **61** CONF ~ 235.4 235.4 235.4 234.5 234.9 234.9 2 Ē a 571 1 0•859 0•900 MACH 0.901 0.898 0.901 S T uvudvøvønvu Ling SEC SEC

0.753 0.872 OF/D 0.932 0.932 1.613 1.613 1.025 0.793 0.742 0.741 0.728 0.810 0.767 -0.433 -0.332 -0.224 -0.120 -0.029 0.023 0.043 -0.412 -0.367 -0.455 -0.458 -0.480 d C 0.217 0.226 V A /V 0.159 0.000 0.122 0.154 VF/V 0.155 0.295 0.191 0.083 0.140 0.000 ALPHA 0.00 0A/Q 0.016 0.039 C.033 C.U00 C.058 C.024 0.013 0.013 71.1 0.016 0.010 0.018 0.000 0.202 0.210 415 MA/M 0.147 0.00.00 n <u>ب</u> 234. MF/V C.082 C.130 0.144 C.275 0.113  $\infty$ m C C-143 0.178 20 5 7C1 Z/CB 0.50 0.50 0.50 0.49 0.49 C.49 0.49 0.50 54.0 0.48 0.48 0.48 P 4 Ö RN/L 7 0.858 1.473 -0.00 Y/CB 0.01 0.01 0.00 -C•C1 -0•01 -0.01 -0.02 -0-01 -0.02 -0-02 0.0-VACE X/CB C.53 C.82 L.11 • 69 • 99 -27 • 85 .14 • 44 .41 • 73 5 CCNF 235•1 235•5 235.5 235.5 235.5 235.5 235.5 235.1 235.8 235.1 236.3 234.5 236.7 66 4 C TST F 571 I 0.899 MACH 0.858 006 0-902 0.902 • RUN 374 SEQ HNM450PB5 110

		0110	0.792	0.773	0.760	0.765	0.774	0.810	0.859	606*0	172.0	1.011	1.029	1.033	1.031
		دە	-0-411	-0-447	-0.471	-0.462	-0-445	-0.375	-0.280	-0.180	-0.058	0-022	0.058	0.066	0.063
		V 8 / V	0.193	0.202	0.215	0.257	0.358	0.419	0.379	0.254	0.155	0.000	0.000		
		VF/V	0.254	0.316	0.443	0.466	0.538	0.544	0.481	0.364	661.0	0.000	0.00.0	0.000	0•000
ALPHA	0.00	0A/0	C. 026	0.028	0.031	0.045	0.088	0.127	0.110	0.069	<b>C.</b> 020	0.00.0	C•000		
11	71.5	0/30	0.045	0.068	0.133	0.149	0.203	C.218	0.179	C.107	0.034	0.000	c. coo	0000.0	<b>c</b> •000
۵.	455	WVVW	0.181	0.189	0.202	0.242	0.337	0.396	0.357	0.276	0.145	0000.0	00000		
C	230.1	NL / N	0.238	0.297	C.415	0.441	0.512	(.519	0.457	C.343	0.186	000.0	000-0	0000.0	0000
L b1	7 730	2/08	0.18	0.18	0.18	0.18	0.18	0.18	0.17	0.17	0.17	0.17	0.17	0.16	0.16
INT H	1.49	Y/08	0.01	0.01	0.00	00-00	-0.00	10.0-	10.0	.c.c1	-0-01	·C•C2	0.02	·C•02	-C• C3
MACF	0.850	X / DB	0.53	<b>C.</b> 82	1.11	1.40	1.69 -	1.98 -	2.27 -	2.56 -	2.85 -	3.14 -	3.44 -	3.73 -	4.01 -
N CONF	5 7	•	1.1	ຍ ເ	3.8	5•0	6°0	1.1	3.4	5. • • •	1.7	0.1	0.2	5.0	5 <b>°</b> 6
Ē	1 6	<b>.</b>	23	23(	23(	23(	23(	23(	22	23	23(	23(	23(	22	22
TST	571	MACH	0.850	0.852	0.852	0.852	C.852	0.850	0-847	0.845	0.850	0.850	0.849	C.848	0.848
۸Na	375	SEQ	<b></b> 1	2	m	4	un.	φ	~	æ	σ	10	11	12	13

		pF/p	0.802	0.781	0.761	0.754	0.759	0.785	0.834	0.894	0.964	1.006	1.024	1.033	1.030
		СÞ	-0.394	-0.433	-0.472	-0-483	-0.476	-0.424	-0.327	-0-207	-0.070	0.012	0.048	0.065	0.059
		V A /V	0.271	0.264	0.181	0.271	0.341	0.359	0.373	0.302	0.131	0.043			
	_	VF/V	0.270	0.361	0.387	0.432	0.494	0.481	0.429	0.307	0.145	0.000	0.00.0	0.00.0	
ALPHA	0.00	0A/0	0.052	0.048	0.022	0.049	C. U78	0.090	0.103	0.072	0.015	<b>C.002</b>			
TT	71.6	0F/0	0.052	C• C90	0.101	C.126	0.167	0.164	0.137	0.074	0.018	c. coo	000.0	0.000	
G.	457	MA/M	0.254	0.248	0.169	0.255	0.321	0.338	0.351	0.284	0.123	0-040			
G	229.9	ME / N	0.254	0.340	0.365	0.408	0.465	C.457	C.4C6	0.288	0.135	0000	000.0	0000-0	
FT.	151	Z/Ca	0.25	0.25	0.25	0.24	0.24	0.24	0.24	0.24	0.24	0.23	0.23	0.23	0.23
RN/L	1.457	Y/CB	0.01	c. c1	c.00	c•00	0.00	c.c1	c.c1	0.01	c. c1	0.02	c. c2	c.02	0.03
NACH	0.848	X / Г.В.	C. 53	0.80	1.11	14.1	1.69 -	1.98 -	2.27 -	2.56 -	2.85 -	3.13 -	2.44 -	- 61.5	4.01 -
V CONF	-	<i>.</i> .	5°C	۲.0	٥.6	5.0	.6	ۍ • د	5.0	•	2•]	5	0.6	0	) <b>.</b> 6
TPT	. I 66	U H	18 229	50 230	1 230	:2 230	EL 230	:2 23(	12 230	3 231	14 231	11 230	1 230	51 231	1 230
151	571	MAC	0.84	0.35	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
RUN	376	SEC		2	m	4	ŝ	Ś	~	æ	O.	10		12	13

125

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pE/P 0.810 0.749 0.756 0.783 0.836 0.836 0.766 0.956 1.003 1.023 1.023 1.029 0.788 -0.429 -0.324 -0.198 -0.498-0.482 0.045 0.058 0.058 -0-465 -0.088 0.006 -0.374 -0.418 0.000 0.000 0.000 0.155 0.322 0.330 0.258 V A /V 0.186 0.180 0.267 0.323 0.280 0.150 VF/V 0.237 0.233 0.283 0.340 0.039 0.00 ALPHA 04/0 C.025 c.000 c.016 c.072 c.072 c.072 c.053 0.000 0.034 C. 027 69.0 GF/0 0.039 0.053 0.078 C.051 C. C72 0.058 0.018 0.007 0.075 0.303 0.000 0.243 0.168 M 4 52 M 4 52 0.174 0.145 C.3C4 C.263 0.140 C.C84 L d F WACH RN/L 7 0.853 1.502 Y/DP -C.C2 -0.03 -C.02 -0.01 1.69 1.58 2.27 X/CB C.53 C.81 1.10 1.41 3.13 2.56 2.85 2.44 . 72 4.01 L N L TN CI 66 0 230-1 229-4 228.6 228.6 229.0 228.9 229.3 ωω 17 αU 229.8 229.8 229.8 229.8 229.8 229.8 229. 571 1 MACH 0.853 0.850 0.848 0.848 0.856 0.850 0.850 0.850 0.851 0.852 0.852 0.852 0.852 RUN 377 SFG NMJUON ωo 2 1213

0.758 0.789 0.841 0.995 1.020 1.023 0.792 0.767 0.745 0.554 0.814 0.040 0.045 0.039 -0.500 -0.185 -0.090 -0.368 -0.414 -0.413 -0.313 -0.461 -0.474 -0.011 a C 0.000 0.249 0.266 0.122 0.000 V 4 /V 0.122 0.174 0.133 0.240 0.216 0.212 VF/V 0.035 0.167 0.00 04/0 ALPHA 0.000 0.052 C.012 0.000 0.013 0.040 0.032 0.029 0.010 0.021 69.8 0F/0 0.021 c. cc1 453 MA/M 0.000 0.249 0.114 0.000 4 726 228.5 2/DB MF/W 0.50 0.124 0.50 0.225 0.50 0.223 0.50 0.223 0.50 0.223 0.49 0.124 0 0.49 0.163 0 0.156 0.033 0.49 0.49 0.49 ω F. œ 0.4 0.48 0.4 4. Ó F WACH PA/L -0.01 C.02 () () () -0.02 -0.02 -0.01 -0.01 0 X/CB C • 53 C • 53 C • 81 L • 11 L • 11 L • 11 L • 40 L • 69 L • 69 L • 69 Z • 55 Z • 555 2.85 3.14 3.44 3.73 4.01 TST F TN CCNF 571 1 66 7 MACH C X 0.849 228.5 C 228.5 228.5 229.1 230.5 230.5 229.7 230.C 229.7 229.8 Ç 230. C 230-0.848 851 851 53 œ ់ • Ó 570 570 ω Ø 2 I 218

RUN	<b>TST</b>	<b>D</b>	TN O	L N U	VAC	F RN/	ة ب	+	U	۵	11	AL PHI	4			
379	571	<b></b> 1	66	-	0.75	9 1.52	0	62 2	23.3	500	70.5	0.0				
SEQ	MACH	r	0		X/CB	Y/DB	0/2	2	F/N	MA/M	QF/0	0 A / 0	VF/V	V A /V	СÞ	bF∕p
<b>,</b>	351.0	80	23.3	-	0.53	0.01	0.1	8 0	237	0.185	0.046	0.030	0.251	0.201	-0-389	0.827
2	0.795	6	23.8	-	C•82	C.C1	0.1	່. ວ ອ	371	0.203	0.110	C. 033	0.390	0.215	-0-442	0.802
ŝ	0.798	80	:23.3		1.11	0.00	0.1	80.0	444	0.252	0.155	C.050	0.465	0.267	-0.484	C. 784
4	0.797	2	22.8		1.41	00.00	0.1	ີ ບ ຍ	475	0.306	0.177	0.073	0.497	0.323	-0.490	0.782
ŝ	552 -0	6	23.2		1.69 ·	-0.00	0.13	0.0	512 (	0.394	0.208	0.123	3,5.0	0.414	-0-461	0.794
9	0.796	-~- ∞	22.7		. 58 .	-0-01	0.1	ບ ຍ	452	0.381	0.200	0.120	0.515	0.401	-0.390	0.826
2	0.795	8	22.7	• •	2.27	-0.01	0.1	-0 -	332	0.269	C. C58	C.Uo5	0.350	0.284	-0.235	0.895
æ	0.798	8	22.7	, v	2.56	-0.01	0.1	7 0.	257 (	0.244	0.963	0.056	0.272	0.258	-0.127	645 0
σ	351.0	5	22.7	•~	2.85	-0.01	0.1	· 0 ~	000	000.000	0.000	0.00.0	ú.000	0.000	-0.008	0.996
10	351.0	8	22.7	<b>1</b> • 1	3.13	-0.02	0.1	1 0.	000	00000	0.000	0.00.00	0.000	0.003	0.036	1.016
11	C•796	8	22.7	•	- 44 -	-0.02	0.1	~							0.067	1.030
17	367.0	ດ. ຄ	22.7	• • 1	3.73	-0.02	0.10	ς. Υ	000		0.000		0.000		0.053	1.024
13	0.797	2	22.7	-	4. CI	-0-03	0.16	5							0.050	1.022

		0 ⊑ / D	0.820	101.0 6.	2 0.787	11 0.780	3 9.792	0 0.824	4 9.877	2 0.936	0.986	8 1.012	11.023	
		1 Co	4 -0-40	4 -0.44	3 -0.47	4 -0-49	1 -0.46	0 -0.39	3 -0.27	7 -0.14	9 -0.03	20°0 C	0.05	
		VAV	. 0.18	0.24	0.245	0.25	0.36	0.37	+ 0.37	5 0.24	0.08	0.00		
۲I اع	0	V L L V	0.241	: 0.395	0.397	0.481	0.467	0.444	0.384	. 0.205	0.00	0.000	0-000	
ALPH	0.0	OA/C	0.025	C.042	0.043	0.060	0.093	C.102	0.110	C. 051	0.001	0.000	-	
1 I	70.8	0/ 10	0.042	0.114	0.112	0.164	0.157	C.147	0.116	0.035	0.000	0.000	C.00C	
۵.	2 497	VA/V	0.173	0.231	0.235	0.278	0.343	0.351	0.354	0.233	0.084	0.000		
C	224.	NF / N	0.227	C.378	0.377	0.459	7.445	6.423	0.364	C.154	C.000	C- 30C	C.00C	
L pT	0 760	Z / DB	0.25	0.25	0.25	0.24	0.24	0.24	0.24	0.24	0.24	0.23	0.23	
INA H	2 1.52	Y / D B	0.01	0.01	0.00	0.00	-0.00	-0.01	-0.01	-0.01	-0.01	-0.02	-0.02	
F MAC	7 0.80	X / 08	0.53	0.82	1.11	14.1	1.69	1.99	2.27	2.55	2.85	3.14	3.44	
TN CON	66	e	224.2	224.6	224.6	223.6	723.7	224.2	223.7	224.2	223.2	223.2	223.2	
TST P	571 1	MACH	0.802	0.804	0.804	0.801	0.801	0.802	0.800	0.301	0.799	0.799	0.799	
RUN	380	SEQ	1	2	m	4	<b>L</b> n	Ŷ	2	œ	σ	10	11	

0.780 0.984 1.C12 1.C17 1.017 1.017 0.782 0.876 0.936 0.775 bF/p 0.824 0.811 0.028 0.037 0.039 CP -0.391 -0-493 -0.408 -0.276 -0.143 -0-036 -0.594 -0-488 -0.424 0.078 0.000 0.000 0.000 0.032 0.247 0.337 0.337 0.134 V A /V 0.000 VF/V 0.323 0.255 0.155 0.000 0.000 0.246 0.233 0.364 0.301 0.00.0 0.00 AL PHA QA/Q 0.004 0.000 0.001 0.042 0.015 080.080 c.059 0.000 0.060 0.044 0.063 0.047 0.019 0.000 71.1 QF/Q C. COO 0.000 0.233 498 MA/M 0.030 0.312 0.127 0.074 0.259 0.00.0 0 223.7 MF/N C.273 0.346 C.285 C.3C6 C.241 C.146 0.000 c. ccc ..000 0.232 .000 760 7/DB 0.40 0.40 0.39 0.39 0.39 0.39 0.38 0.38 0.38 0.38 0.38 P P F WACH RN/L 7 0-801 1-517 Y/DB C.C1 0.00 00.00 -0.01 -0.01 -C.CI -0-02 -0.02 10-0--0-07 -0-03 X/CB C-53 C-82 L-11 • 84 .14 3.44 . 72 .01 3 CONF 224•2 223•7 223•2 223•1 223•1 223•1 ۵. 571 1 MACH 0.8C1 0.799 0.799 0.799 0.799 0.800 0.800 0.800 0.800 0.800 0.800 0.800 0.799 0.801 0.800 ST N.WANOP@DOHNW RUN 381 SEQ

0.876 0.879 0.900 0.977 1.004 1.012 1.006 £05 • 0 0.937 000 pF/p 0.883 1.008 110.1 -0.486 -0.401 -0.252 -0.090 0.015 0.048 0.043 0.030 -0.382 -0.466 -0-496 0.023 -0-001 80 VA/V 0.252 0.371 0.381 0.381 0.381 0.385 0.000 0.165 0.308 0.422 0.515 0.549 0.547 0.384 0.00.0 0.000 VF/V 0.000 0.000 0.145 0.00 ALPHA C-120 0-137 0.126 c.109 0A/Q 0.054 0.114 0.025 0.000 0.000 0F/0 0.148 C.221 0.130 0.019 70.3 c. 000 0.253 c.220 000.0 0.000 00000 0.244 0.360 0.370 0.394 0.375 0.340 .000 705 MA/M 0.159 0.000 O 5 MF / W 0.298 c.5c2 c.536 0.373 0.410 00000 0-140 0.000 0.000 C.000 PT C 500 178. Z/DB 0.18 0.18 0.18 0.18 0.18 0.18 0.17 0.17 0.17 0.17 0.16 .16 ~ 0.1 0 MACH RN/L 0.601 1.513 -0.00 -0.02 -0.03 -0.01 -0.01 10.0--0.01 -0.02 X/FB C.53 C.82 L.10 L.41 1.69 1.99 2.56 2.85 2.85 3.13 3.72 3.43 2 CCNF 178.5 176.7 176.7 176.7 177.9 177.3 177.5 177.5 177.5 176.7 ທີ່ຫ 178.1 2 66 Q C) 571 1 0.557 0.557 0.557 0.557 0.557 0.557 0.559 0.559 MACH 0.601 0.559 0.600 0.600 0.601 0.601 E S RUN SEO SEO - NM + LA N 00 11 2 3

	pF/p	0.890	0.889	0.871	0.875	0.902	0.939	179.0	1.002	1.010	1.012	1.010	1.003	1.003
	СЪ	-0.435	-0-474	-0.510	-0.494	-0.388	-0.245	-0.115	0.008	0.038	0.047	0.041	0.011	0.011
	V A /V	0.197	0.244	0.304	0.373	0.323	0.341	0.308	0.000	0.000				
	VF/V	0.280	0.372	0.503	0.506	0.459	0.334	0.170	0.000	0.000	0.000	0.000	0.000	
ALPHA 0.00	0 A / O	0.032	C.049	0.075	0.115	0.088	0.103	C.087	0.00.0	0.000				
11 70.0	0F/0	0.066	0.115	0.209	0.213	0.180	0.098	0.026	000.0	c.000	000.0	000.0	000.0	
705	N V V	0.191	0.236	0.294	0.362	0.313	0.331	0.299	0.000	0.000				
5-171 3	N / 1 N	C.271	0.361	0.490	654.0	3.446	C.324	0.165	0.000	0000	C.000	C.0CC	0000	
14 J	2/08	0.25	0.25	0.25	0.24	0.24	0.24	0.24	0.24	0.24	0.23	0.23	0.23	0.23
1/121	Y/DB	C.01	0.01	0.00	00.0	-0.00	-0.01	-0-01	-0.01	-0.01	-0.02	-c.c2	-0.02	-0-03
2 MACH	X/CB	C.53	C.82	1.11	1.41	1.69 -	- 85 • I	2.27 -	2.56 -	2.85 -	3.13 -	3.44	3.73	4.C1 -
TN CCNF	90	5-12	78.5	78.5	78.5	77.5	5-11	77.3	76.7	77.9	5-12	78.5	6.17	78.5
TST P	MACH	0.600 1	0.602 1	2.6C1 1	0.601 1	3.600 1	0.559 1	0.599 1	1.597 1	<b>J.600 I</b>	0.600 1	0.601 1	0.600 1	0.602 1
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1.005 0.999 1.007 0.897 0.880 0.864 .998 0.893 0.935 666.0 1.008 0.862 772.0 0 -0.256 0.029 -0.549 -0.542 0.021 -0.002 -0.006 -0.423 -0.004 -0.408 -0.476 d C VA/V 6.126 0.0000 0.120 0.335 0.335 0.319 0.319 000 • VF/V 0.245 0.371 0.327 0.377 0.236 0.134 0.000 0.000 0.000.0 0.000 0.000 0.00 0.4/0 0.013 ALPHA 0.00.0 0.012 0.042 0.094 c.089 0.004 c. 000 0000°0 0000°0 0000°0 0.115 0.047 0.016 0/30 0E/0 C. C87 0.051 00000 0.000 0.114 0.309 0.060 0.000 706 MA/M 0.000 0.219 0.325 0.116 0.122 ۵ 177.9 NF/N C.237 0.365 0.228 0.130 0.000 C.360 C.317 000-0 0.000 000.0 0.39 F C RN/L 0.600 1.51 -0.02 -0-02 10°01 -0°01 MU MN 3.72 2.13 3.43 ~ CONF CONF 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171.9 2.171. 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.771 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7712 2.7717 2 9 C TST P MACH MACH MACH C. 6000 C. 6000 C. 6000 C. 6000 C. 6000 C. 599 C. 5000 C. 500 0.599 0.600 .600 0.600 C こう よう そう きゅう こう 8 UN 3 8 5 5 F 0

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		or /p	0.578	0.575	0.976	0.978	0.586	199.0	1.000	1.001	1.000	1.000	0.998	0.598	865.0
		من	-0-496	-0.554	-0.550	-0.510	-0-309	-0.078	0.006	0.015	100.0-	100.0	-0.042	-0.055	-0-046
		V A / V	0.352	0.407	0.370	0.458	0.383	0.137	0.000	0.000	0.003	0.000	0.000	0.000	0.000
		VF/V	0.402	0.469	0.527	0.531	0.347	0.000	0.000	0.000	0.000	0.000	0.00.0	0.00.0	0.00.0
ALPHA	0.00	0 A / Q	0.120	0.160	0.132	C.203	0.143	C.018	c.J00	c.000.0	0.00.0	0.00.00	c.000	c.000	c.000
11	66.4	CF/0	0.156	0.212	0.269	6.273	9.118	0.00.00	0.00.0	0.000	000.0	000.00	000.0	0.000	c•000
С.	1802	NVV.	0.350	0.405	0.368	0.456	0.381	0.136	0000.0	0.000	0000-0	0.000	0.000	000.0	0.000
۲	8 <b>C</b> •9	NE/N	552.0	C.466	0.525	0.528	C.346	0000-0	0.000	0.000	0.000	000 • 0	0000	0000-0	000-0
L b L	7 1884	2/0P	0.18	0.18	0.18	0.18	0.18	0.18	0.17	0.17	0.17	0.17	0.17	0.16	0.16
ENVI FNV	1.52	Y/DB	10.0	10-0	00 • 00	00-00	0.00	.0.01	.0.01	·c• c1	0.01	·c. c2	-0.02	-0-02	·0•03
NACH	0.253	X / 5.B	0.53	0.82	1.11	1•41	I. 69 -	1.98 -	2.27 -	2+56 -	2.85 -	3.13 -	3.43 -	3.72 -	4.00 -
TN CCNF	66 7	c	80.8	30.1	80.1	3*61	79.5	79.5	80.1	80.1	80.1	80.1	79.5	79.5	5*62
TST P	1112	HUAM	0.253	0.252	0.252	0.251	0.251	0.251	0.252	0.252	0.252	0.252	0.251	0.251	0.251
PUN PUN	387	SEC	<b>,</b>	2	m	4	S	¢	2	ω	σ	10		12	13

		0/1d	0.579	0.975	0.975	0.578	0.985	0.596	0.999	0.999	665*0	1.000	0.598	199.0	265.0
		d D	-0-474	-0.561	-0.573	-0.503	-0.329	-0.093	-0.023	-0.012	-0.019	-0.010	-0.043	-0*060	-0-060
		V A /V	0.336	0.265	0.251	0.343	<b>0.356</b>	0.145	0.121	0.000	0.000	0.000	0.000	0.000	0.000
		VF/V	0.246	0.404	0.531	0.502	0.290	0.135	0.042	0.000	0.074	0.000	0.00.00	0.00.0	0.00.00
ALPHA	00.00	0/A/Q	C.109	0.067	C.061	0.114	0.124	0.021	0.014	c.000	000.0	c.000	c.000.0	0.00.0	0.00.0
1	65.8	01 - 0	0.059	0.157	0.272	0.245	0.082	0.018	0.002	0.000	0.005	000.0	005.0	0.000	C.000
đ	1872	MV/M	0.334	0.263	0.249	0.342	0.354	0.144	0.120	0.000	0000.0	0.000	0.00.0	0.000	0.000
U	19.5	NL JN	0.245	C.4C2	C.528	C.50C	0.289	0.134	0.042	0.000	C.073	0.000	00000	0000-0	000.0
LPT	6 1883	2.158	0.25	0.25	0.25	0.24	0.24	0.24	0.24	0.24	0.24	0.23	0.23	0.23	0.23
I/Nd r	1.1.51	Y/08	0.01	0.01	00.00	c. co	-0-00	-0.01	-0.01	10-0-	-0.01	-0.02	-0.02	-0-02	-0-03
NACt	0.25	X / 5.B	C. 53	<b>C.</b> 82	1.11	1.41	1.69 -	1.58	2.26 -	2.55 -	2.85 -	3.13 -	3.43 -	2.73 -	4.01 -
A CONF	6 7	C C	9. E	0.1	0.1	8 <b>•</b> 8	9 <b>.</b> 5	8°8	9 <b>.</b> 5	9.5	8•8	8.8	8°8	9.5	9.5
L L	1 6		~	8	8	~	2	~	~	-	~	~	~	~	~
TST	571	HUVW	0.251	0.252	0.252	0.250	0.251	0.250	C+251	0.251	0.250	0.250	0.250	0.251	0.251
NNA	388	SFO	<b></b>	~	n	4	ſ	Ś	2	8	σ	10	11	12	13

0.993 1.000 1.000 1.999 0.976 0.973 0.976 0.985 F/P 979 . ē. -0.555 -0.555 -0.5555 -0.155 -0.010 -0.010 CP •470 Ŷ VA/V 0.2221 0.0222 0.050 0.3333 0.3333 0.050 0.050 0.050 0.050 0.050 0.246 0.121 0.000 0.000 0.000 0.000 0.201 0.111 0.303 VF/V TT 65.4 67.4 0.012 0.012 0.012 0.012 0.014 0.014 0.000 0.000 0.000 0.219 0.000 0.133 0.396 0.3371 0.371 0.371 0.332 0.232 0.000 0.000 1802 MA/M ۵ 12010 C.11C C.31C C.35C 8 u ₹ NACH NACH C. 553 C. 555 C. 553 C. 555 C. 553 C. 555 CONF 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 0 -

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MODEL DIAMETER = 6 in.

Figure 1.- Scale models tested in 6- by 6-ft transonic wind tunnel. (a) Ablated configuration. (b) Ballasted configuration.



ALL DIMENSIONS NORMALIZED TO MODEL DIAMETER MODEL DIAMETER = 6 in.





a) FAR-WAKE CONFIGURATION



b) NEAR-WAKE CONFIGURATION (CONFIGURATION "A" MODIFIED BY BENDING)

Figure 3.- Pitot-static probe.



Figure 4.- Test setup.



Figure 5.– Radial profiles of dynamic pressure.  $X/D_B = 5.5$ ,  $Y/D_B = 0$ , R = 0.75 million,  $\alpha = 0^\circ$ .



Figure 6.– Axial profile and spatial contours of dynamic pressure in wake of ablated Galileo probe.  $\alpha = 0.0^{\circ}$ ,  $R_D = 0.75$  Million.



Figure 6.- Concluded.



Figure 7.- Effect of angle of attack on dynamic-pressure profiles,  $X/D_B = 8.5$ , M = 0.80,  $R_D = 0.75$  million.



Figure 8.– Contours of constant reverse dynamic pressure in near wake of ablated model,  $\alpha = 0$ ,  $R_D = 0.75$  million,  $Y/D_B = 0$ .



Figure 8.- Continued.



Figure 8.- Concluded.

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