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## MICROSTRUCTURAL ASPECTS OF ZIRCONIA THERMAL BARRIER COATINGS

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Various combinations of plasma-sprayed bond coatings and zirconia ceramic coatings on a nickel-based superalloy substrate were tested by static thermal exposure at 1200°C and cyclic thermal exposure to 1000°C. The bond coats were based on Ni-Cr-Al alloys with additions of rare earth elements and Si. The ceramic coats were various  $ZrO_2-Y_2O_3$  compositions, of which the optimum was found to be  $ZrO_2-8.9$ wt.  $x_{2}^{2}0_{3}^{3}$ . Microstructural analysis showed that resistance to crackiñg during thermal exposure is strongly related to deleterious phase changes. Zones depleted of Al formed at the bond coat/ceramic coat interface due to oxidation and at the bond coat/substrate interface due to interdiffusion, leading eventually to breakdown of the bond coat. The 8.9%  $Y_2O_3$  coating performed best because the as-sprayed metastable (high- $Y_2O_3$ ) tetragonal phase converted slowly into the low- $Y_2O_3$  tetragonal plus high- $Y_2O_3$  cubic-phase mixture, so that the deletérious monoclinic phase was inhibited from forming. Failure appeared to start with the formation of circumferential cracks in the zirconia, probably due to compressive stresses during cooling, followed by the formation of radial cracks due to tensile stresses during heating. Cracks appeared to initiate at the Al<sub>2</sub>O<sub>3</sub> scale/bond coat interface and propagate through the zirconia coating. Comparisons have been made with the behavior of bulk ZrO2-Y2O3 and the relationship between the microstructure of the tetragonal phase and the phase diagram. A separate investigation has also been made of the Zr0<sub>2</sub>-A1<sub>2</sub>0<sub>3</sub> interface.

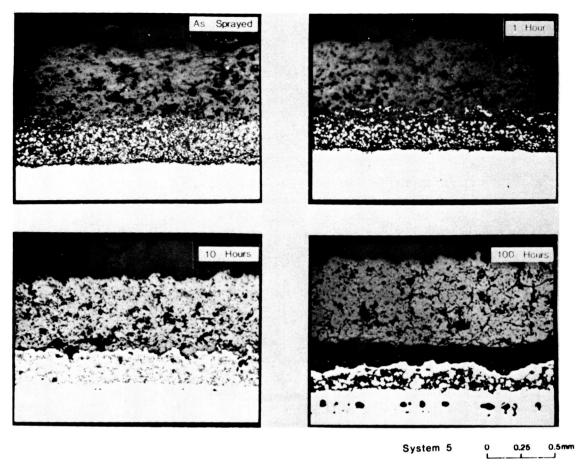


Fig. 1. Optical microstructures of an 8.9%  $Y_2O_3$  system, as-sprayed and after static thermal exposure for 1, 10, and 100 h at 1200°C.

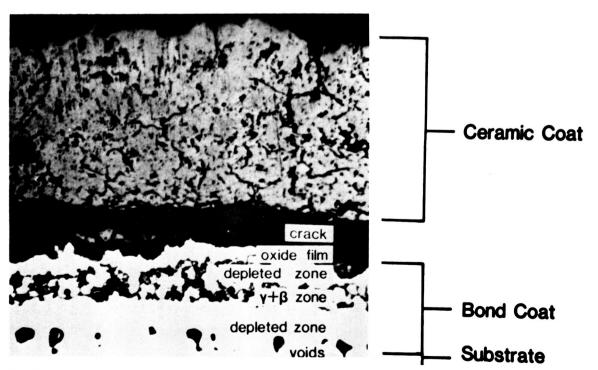


Fig. 2. General optical microstructure of an 8.9%  $Y_2O_3$  system after 100 h static thermal exposure at 1200°C.

Table I. Effect of Y<sub>2</sub>O<sub>3</sub> Content in the Ceramic Coat on the Number of 1000°C Cycles to Failure for Individual Specimens with a Given Bond Coat (Ni–Cr–Al with Y and Si Additions)

Y <sub>2</sub> O <sub>3</sub> (wt%)	No. of cycles to failure
4.3	7
	15
6.1	233
·	233
8.9	>500
	>500
	>500
19.6	321
	>500

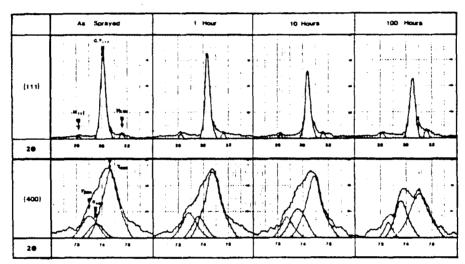


Fig. 3. Experimental X-ray diffraction patterns and deconvoluted peaks in the  $\{111\}$  and  $\{400\}$  regions for plasma-sprayed  $ZrO_2$ -8.9%  $Y_2O_3$  after 1, 10, and 100 h static thermal exposure at 1200°C.

Table II. Phase Analyses (mol%) after Thermal Exposure at 1200°C

System		Time (h)					
(%Y <sub>2</sub> O <sub>3</sub> )	Phase	As-sprayed	1	10	100		
4.3	Monoclinic	22	37	41	44		
	Cubic	4	5	4	3		
	Tetragonal	74	58	55	53		
6.1	Monoclinic	16	17	18	20		
	Cubic	6	9	10	11		
	Tetragonal	78	74	72	69		
8.9	Monoclinic	8	9	9	12		
	Cubic	13	15	22	31		
	Tetragonal	79	76	69	57		
19.6	Monoclinic	3	3	2	2		
	Cubic	70	76	84	88		
	Tetragonal	27	21	14	10		

Table III. Chemical Compositions (wt%) in the Bond Coat after Static Thermal Exposure at 1200  $^{\circ}\mathrm{C}$ 

Time	Al	Si	Cr	Со	Ni	Ti	Phase	Remark
As-sprayed	4.5	2.8	26.9	2.2	63.6		$\gamma/\gamma'$	
, ,	12.7	2.0	15.8	1.7	67.8		$eta/\gamma'$ $eta$	
1 h	2.5	1.1	19.7	2.8	73.9		$\gamma/\gamma'$	Depleted zone near ceramic coat
	6.1	1.0	11.6	1.9	79.4		β	Below depleted zone
	3.0	1.0	18.5	2.6	74.8		$\gamma/\gamma'$	Below depieted zone
	7.2	0.9	9.1	1.9	80.9		β	Near substrate
		1.6			67.8	0.4	$\gamma/\gamma'$	
	2.1	1.4	19.2	3.5	73.3	0.5	γ	Depleted zone near substrate
10 h	2.4	1.2	17.6	4.6	74.2		$\gamma/\gamma'$	Depleted zone near ceramic coat
		1.8			73.0		$\gamma/\gamma'$	Middle of bond coat
	8.5	1.4	9.8	3.8	75.6	0.9	β	Middle of bond coat
	3.4	2.2	17.4	4.8	71.5	0.7	γ/γ΄	Depleted zone near substrate
100 h	6.4	2.8	11.4	7.7	70.3	1.5	$\gamma/\gamma'$	Depleted zone near ceramic coat
	7.5	2.4	5.0	4.9	78.4	1.8	β	Middle of bond coat
							γ/γ'	Depleted zone near substrate

Table IV. Chemical Composition (wt%) of the Oxide Film Formed at the Ceramic Coat/Bond Coat Interface

Time at 1200°C (h)	Al <sub>2</sub> O <sub>3</sub>	Cr <sub>2</sub> O <sub>3</sub>	CoO	NiO
1	72.6	10.7	0.9	15.8
10	21.8	27.6	2.8	47.8
100	93.1	6.9		

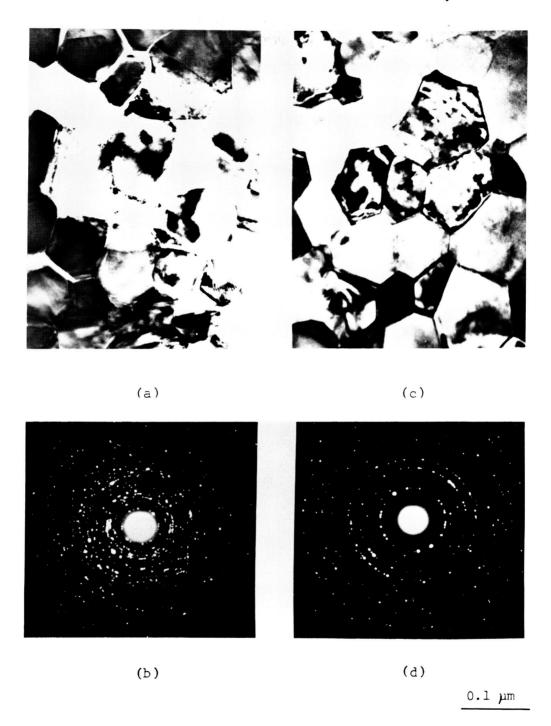
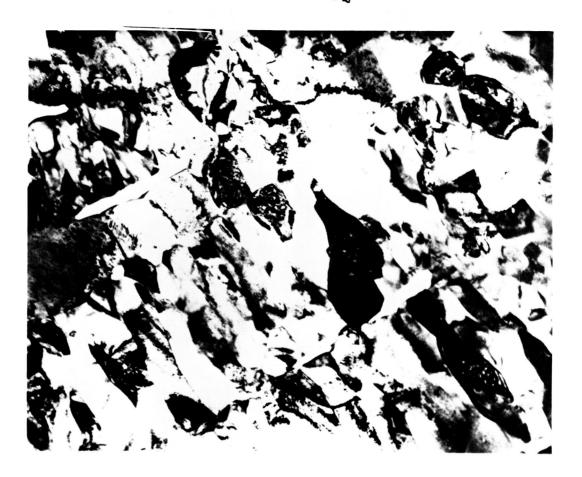


Fig. 4. (a)-(d) TEM micrographs of the as-sprayed  $4.3\% \text{ Y}_2\text{O}_3$  ceramic coating showing the separated regions of monoclinic and tetragonal (T') grains and their SAD ring pattern, (a)-(b) monoclinic; (c)-(d) tetragonal (T')



0.1  $\mu m$ 

Fig. 5. TEM micrograph of the as-sprayed 6.1%  $\rm Y_2O_3$  ceramic coating showing the non-equilibrium tetragonal (T') columnar grains.



 $0.5 \mu m$ 

Fig. 6. TEM bright-field image showing the  $ZrO_2$ - $Y_2O_3$  splat morphology with columnar tetragonal grains which have grown perpendicular to the splat boundary (6.1%  $Y_2O_3$ ) ceramic coat after 100 h at 1200°C.

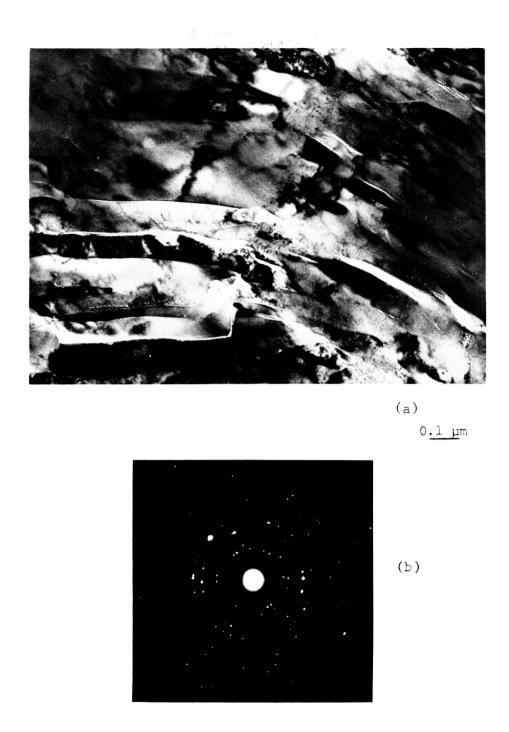


Fig. 7. (a)-(b) TEM micrograph of the columnar cubic grains within as-sprayed 19.6%  $Y_2O_3$  ceramic coating showing intergranular microcracking (a) and the SAD ring pattern (b).

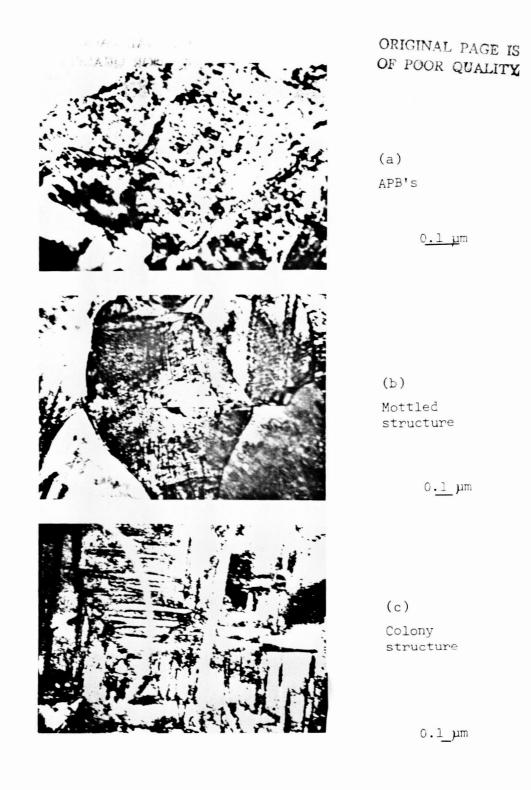


Fig. 8. (a)-(c) Three kinds of tetragonal phase TEM microstructure

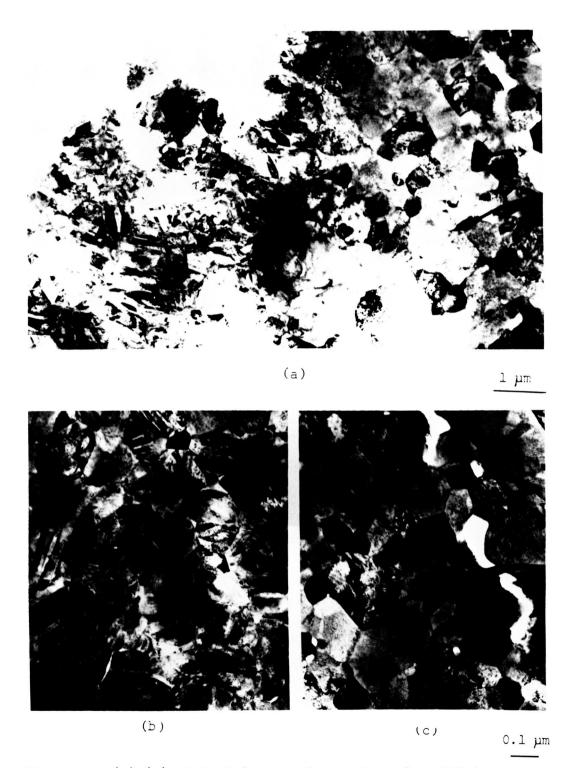


Fig. 9. (a)-(c)  $4.3\%~\rm Y_2O_3$  ceramic coating after 100 hours exposure at  $1200^{\circ}$  C showing separate regions of monoclinic and tetragonal grains.



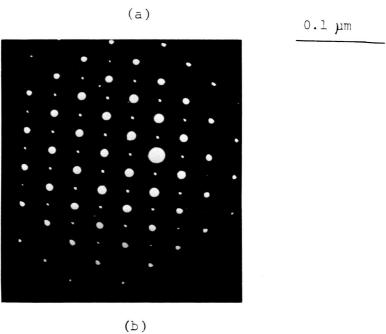
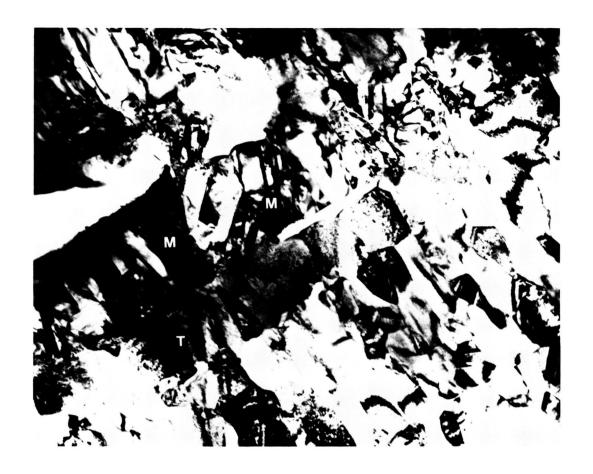


Fig. 10. 4.3% Y 0 ceramic coating after 100 hours at  $1200^{\circ}$  C : (a) TEM micrograph of the tetragonal colony structure within large ( ~ 1.0  $\mu$ m) grain and (b) corresponding [011] diffraction pattern.



0.2 µm

Fig. 11. 6.1%  $Y_2O_3$  ceramic coating after 100 hours exposure at  $1200^{\circ}$  C showing splats formed by low  $Y_2O_3$  concentration particle consisting of many twined monoclinic grain and splats formed by high  $Y_2O_3$  concentration particle consisting of tetragonal grains.

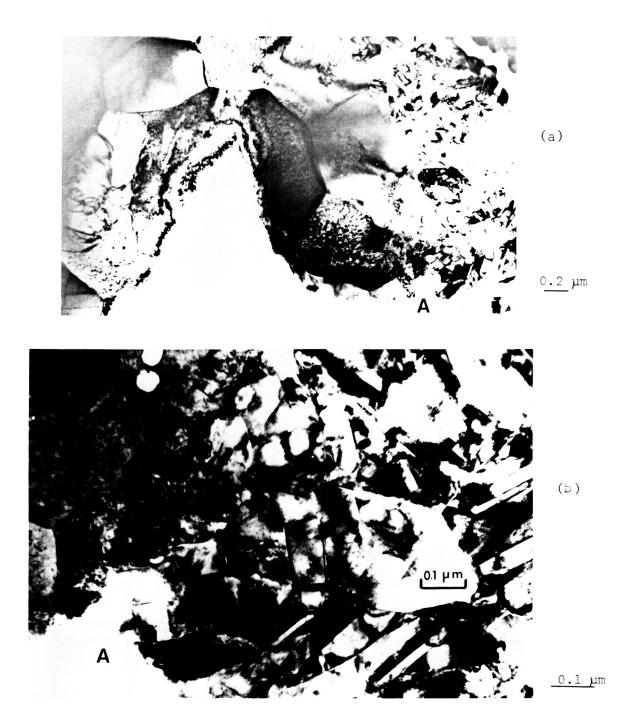
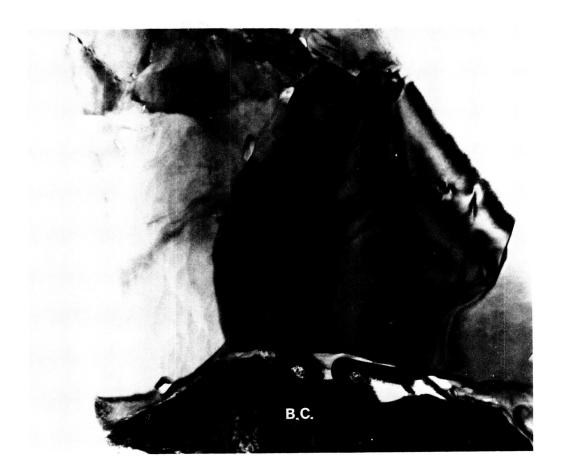


Fig.12. (a)-(b)  $19.6\%~Y_2O_3$  ceramic coating after 100 hours exposure at  $1200^{\circ}$  C (a) monoclinic and cubic grains (b)higher magnification micrograph showing tetragonal grains(A) formed at the interface between monoclinic and cubic grains due to yttrium diffusion.



					0.25 jun	_
Position	<u>A1203</u>	SiO <sub>2</sub>	Cr <sub>2</sub> 0 <sub>3</sub>	<u>Co0</u>	NiO	
1	2.2	43.1	9.3	4.3	41.1	
2	5.7	55.2	6.9	2.8	29.3	
3	25.0	3.3	65.2	0.6	5.8	

Fig. 13. TEM micrograph of oxide scale after 1 hour thermal exposure at 1200°C and the result of point EDAX analyses (system 5). The oxide scale is adherent to the bond coating, however pores are present at the oxide scale/ceramic coating interface.



 $0.5 \, \mu \text{m}$ 

Fig.14. TEM micrograph of oxide film after 10 hours thermal exposure at  $1200^{\circ}$  C showing the columnar grains of Al $_2$ 0 $_3$  and the void formation at the oxide film/bond coating interface.

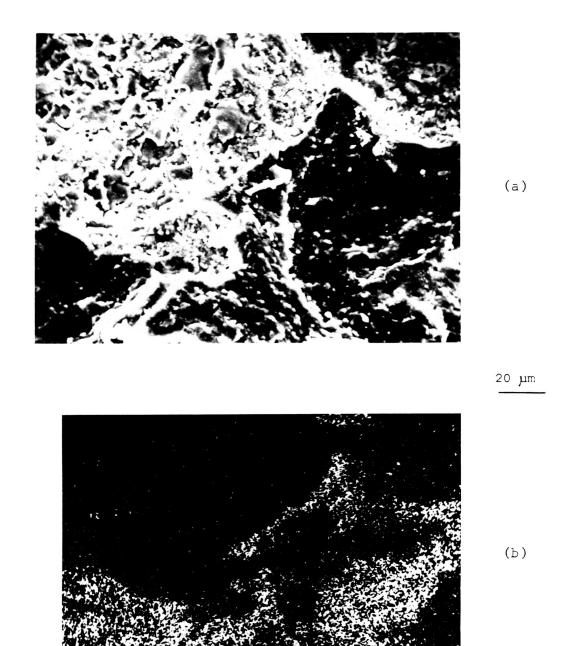


Fig. 15. (a)-(b); (a) SEM micrograph of the bottom-side of ceramic coating (system 10) that had failed after 100 hours exposure and (b) microprobe X-ray map for Al.

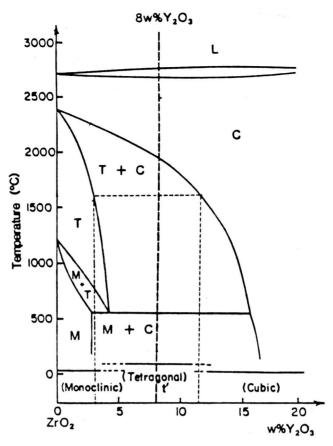


Fig. 16. Phase diagram of the  $ZrO_2$ -rich region of the system  $ZrO_2$ - $Y_2O_3$  (Ref. 4).

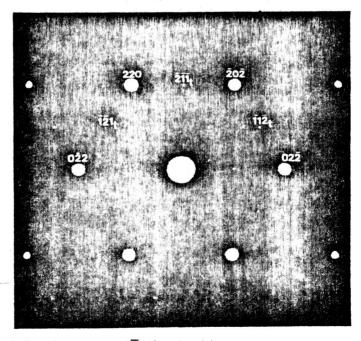


Fig. 17. Diffraction pattern, [111] zone axis.

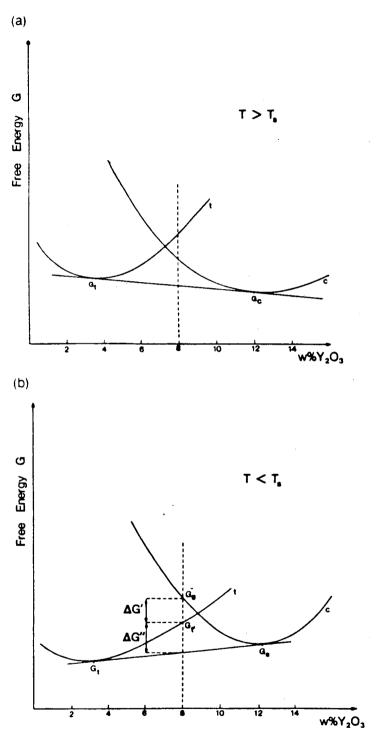


Fig.18. Free energy vs composition curves: (a) above the critical temperature  $\mathcal{T}_0$  and (b) below the critical temperature  $\mathcal{T}_0$ .