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DESTABILIZATION OF YTTRIA-STABILIZED ZIRCONIA INDUCED BY  
MOLTEN SODIUM VANADATE-SODIUM SULFATE MELTS\*

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The extent of surface destabilization of  $\text{ZrO}_2$  - 8 wt %  $\text{Y}_2\text{O}_3$  ceramic disks was determined after exposure to molten salt mixtures of sodium sulfate containing up to 15 mole% sodium metavanadate ( $\text{NaVO}_3$ ) at 1173 K. The ceramic surface was observed to transform from the cubic/tetragonal to monoclinic phase, concurrent with chemical changes in the molten salt layer in contact with the ceramic. Significant attack rates were observed in both pure sulfate and metavanadate-sulfate melts. The rate of attack was found to be quite sensitive to the mole fraction of vanadate in the molten salt solution and the partial pressure of sulfur trioxide ( $1 \times 10^6$  to  $1 \times 10^{-3}$  atm) in equilibrium with the salt melt. The observed parabolic rate of attack is interpreted to be caused by a reaction controlled by diffusion in the salt that penetrates into the porous layer formed by the destabilization. The parabolic rate constant in mixed sodium metavanadate - sodium sulfate melts was found to be proportional to the  $\text{SO}_3$  partial pressure and the square of the metavanadate concentration. In-situ Raman spectroscopic measurements allowed simultaneous observations of the ceramic phases and salt chemistry during the attack process.

<sup>1</sup> This work supported by the U.S. Dept. of Energy, Office of Basic Energy Sciences.

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Table I  
Exposure Environment Composition  
( percent )

Initial Gas Composition		Equilibrium Composition at 1173 K		
O <sub>2</sub>	SO <sub>2</sub>	O <sub>2</sub>	SO <sub>2</sub>	SO <sub>3</sub>
90	10	90	7.7	2.4
99	1	99	.76	.24
99.9	0.1	99.9	$7.6 \times 10^{-2}$	$2.5 \times 10^{-2}$
99.985	0.015	99.99	$1.1 \times 10^{-2}$	$3.7 \times 10^{-3}$
1	99	.25	97.	.15

Table II  
Parabolic Rate Constants

(  $P_{SO_3} = 2.4 \times 10^{-3}$  )

NaVO3 Concentration ( mole percent )	Parabolic Rate Constant ( cm <sup>2</sup> /sec )
0.0	$1 \times 10^{-11}$
0.2%	$1 \times 10^{-11}$
1.0%	$1.7 \times 10^{-10}$
2.0%	$5.4 \times 10^{-10}$
3.9%	$1.5 \times 10^{-9}$

## RAMAN EFFECT

$$\omega_i - \omega_s = \omega_{\text{VIB}}$$

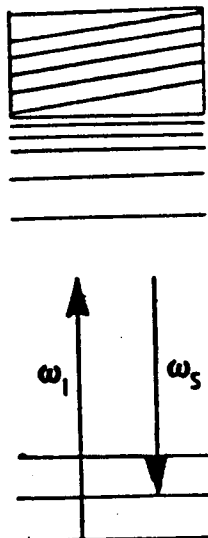


Figure 1.

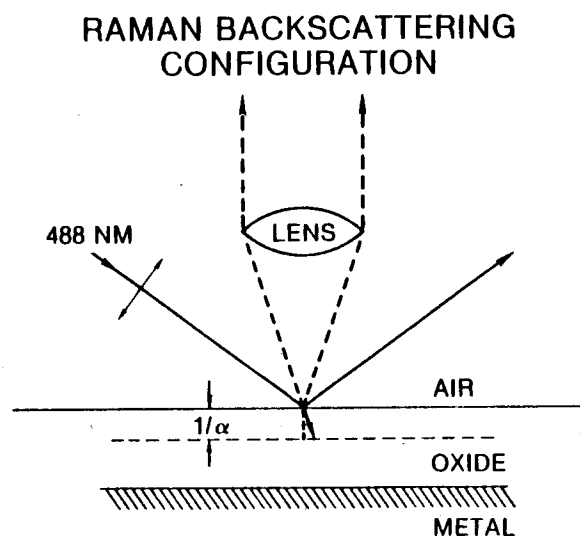


Figure 2.

## RAMAN ADVANTAGES

1. NON-PERTURBING
2. IN SITU
3. QUANTITATIVE CHEMICAL COMPOUND IDENTIFICATION
4. SENSITIVE TO LATTICE SYMMETRY
5. LATERAL RESOLUTION - 1  $\mu\text{m}$
6. DEPTH RESOLUTION - (100  $\text{\AA}$  - 100  $\mu\text{m}$ )
7. GAS ENVIRONMENT CHARACTERIZATION
8. SAMPLE/GAS TEMPERATURE
9. TEMPORAL RESOLUTION (ms - hs)

Figure 3.

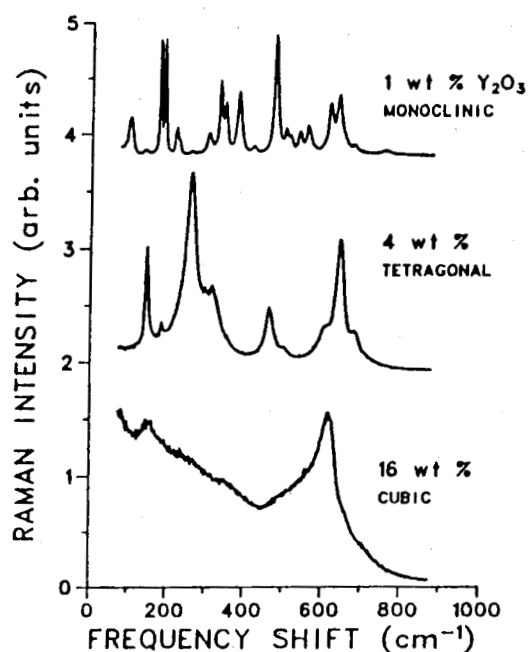
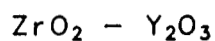


Figure 4.

## Experimental Procedure

- Stabilized zirconia ceramics immersed in sulfate-vanadate melts contained in platinum crucibles.
- Temperature, sulfur dioxide and sulfur trioxide content varied.
- Post-exposure analysis by electron microscopy, electron microprobe and Raman spectroscopy.

Figure 5.

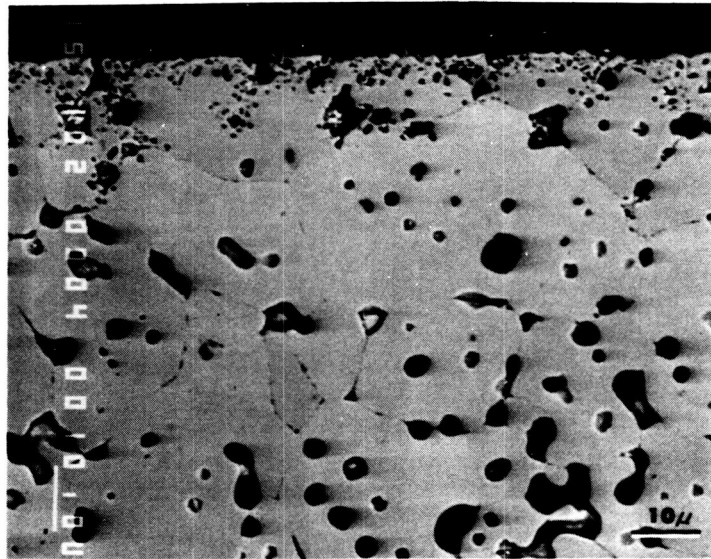


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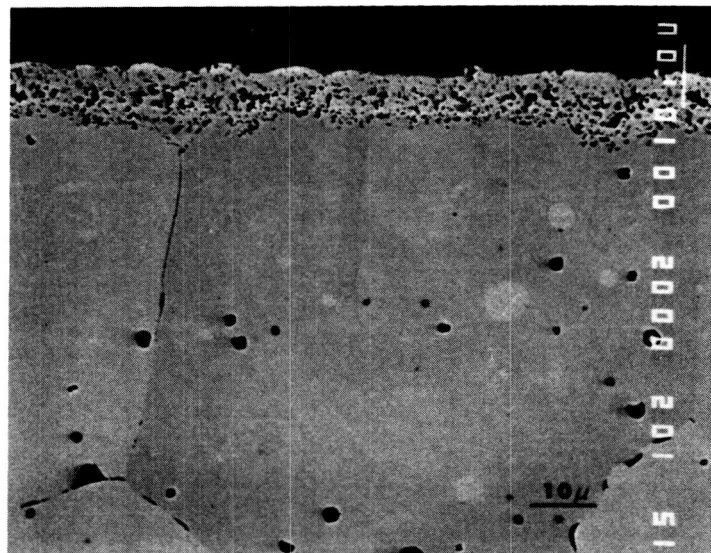
$\text{ZrO}_2 - 8 \text{ wt\% } \text{Y}_2\text{O}_3$

Exposure: 900°C

Pure  $\text{Na}_2\text{V}_2\text{O}_6$



10 min.



1 hr.

Figure 6.

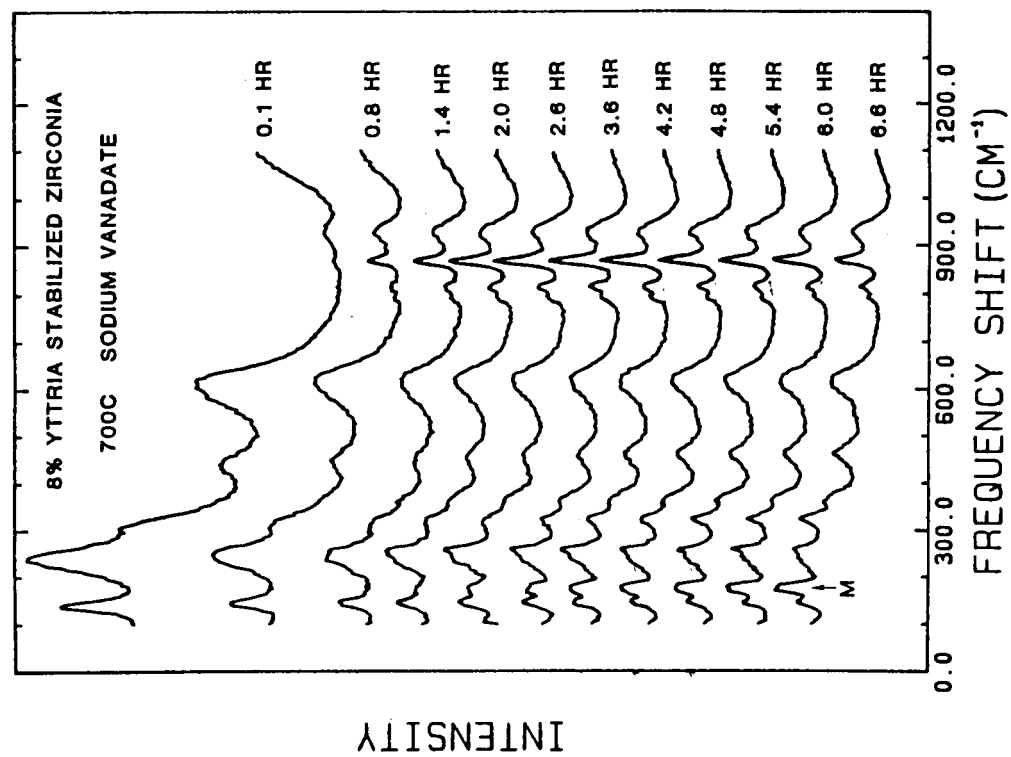


Figure 7.

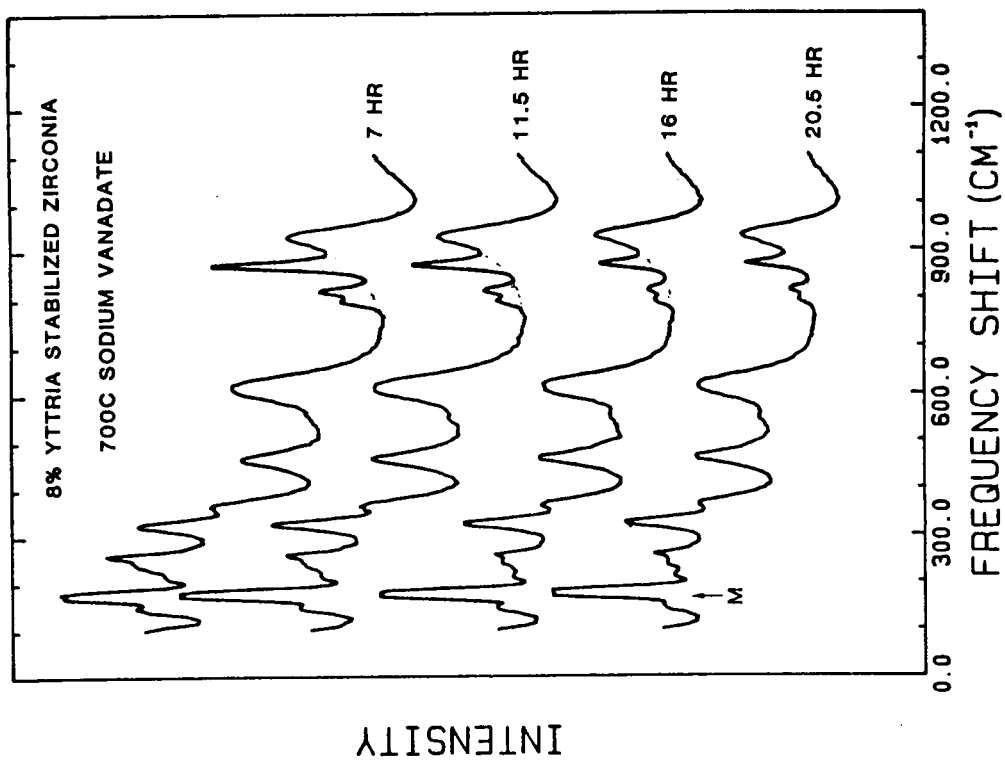


Figure 8.

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$\text{ZrO}_2 - 8\text{wt}\% \text{Y}_2\text{O}_3$   
 $\text{NaVO}_3$  24hr  $700^\circ\text{C}$

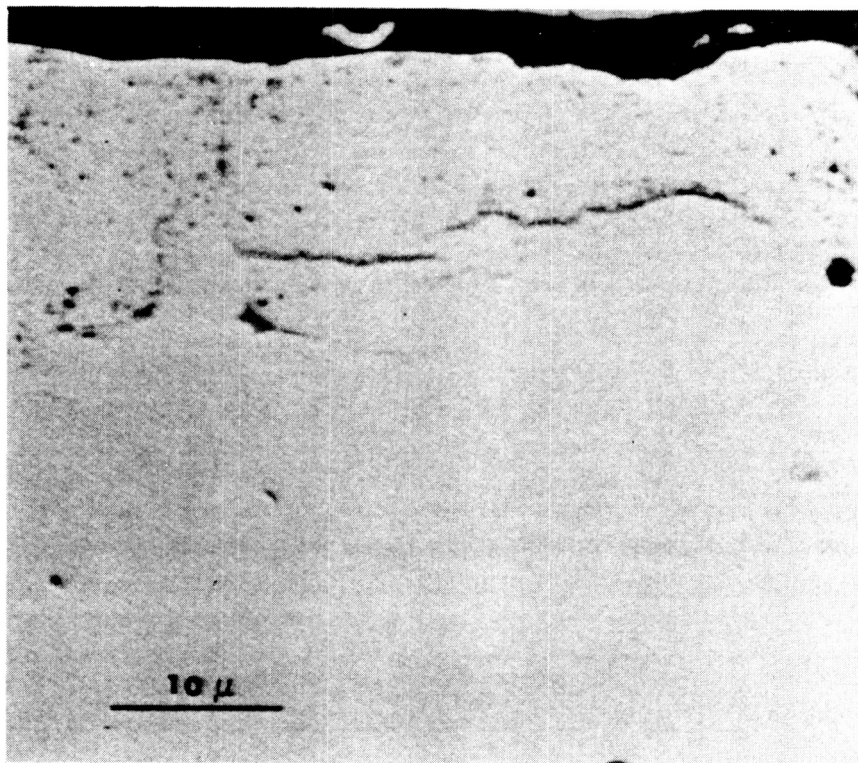


Figure 9.

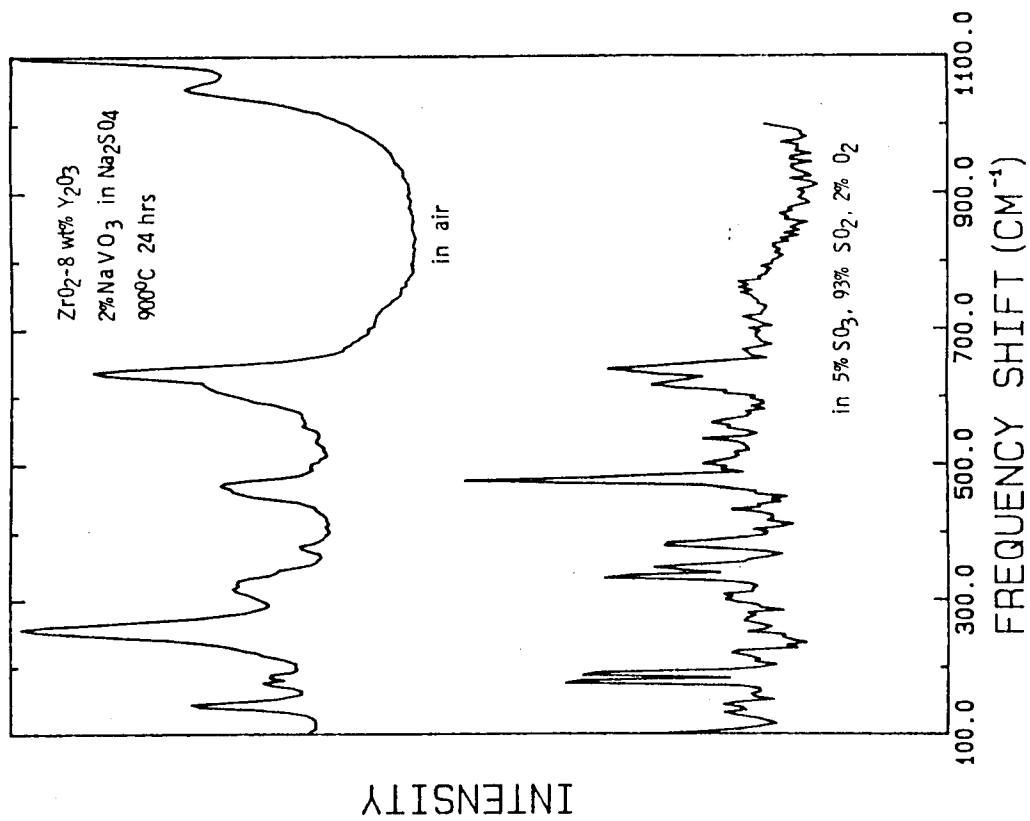


Figure 11.

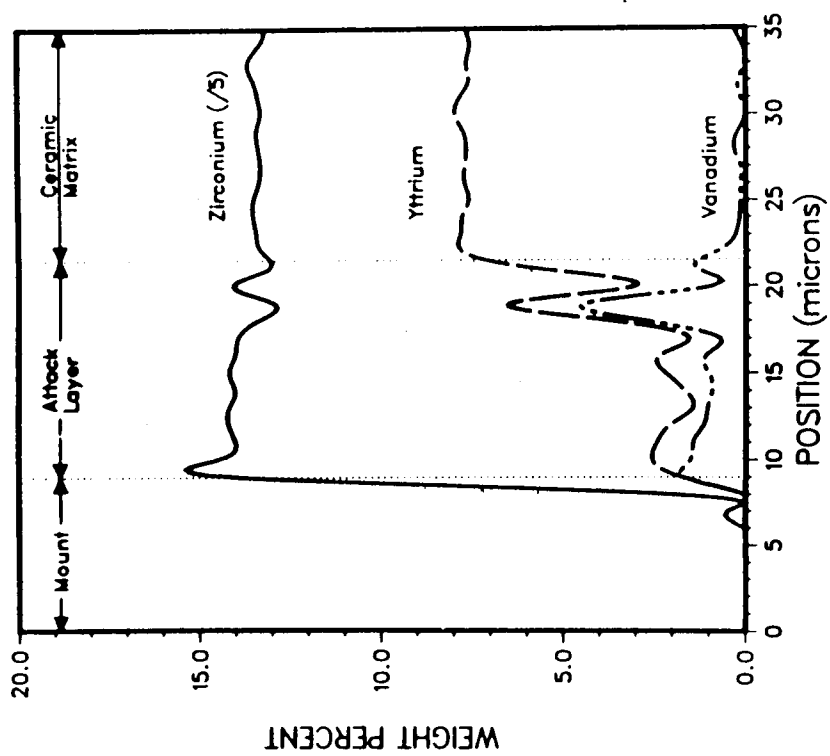
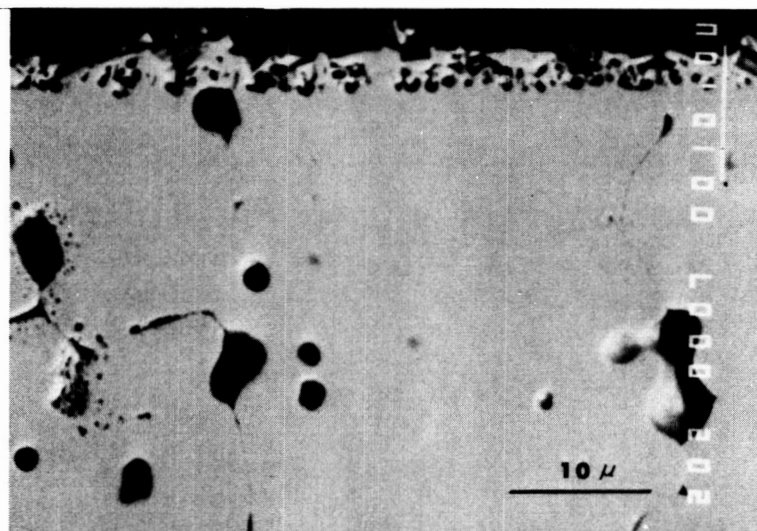


Figure 10.

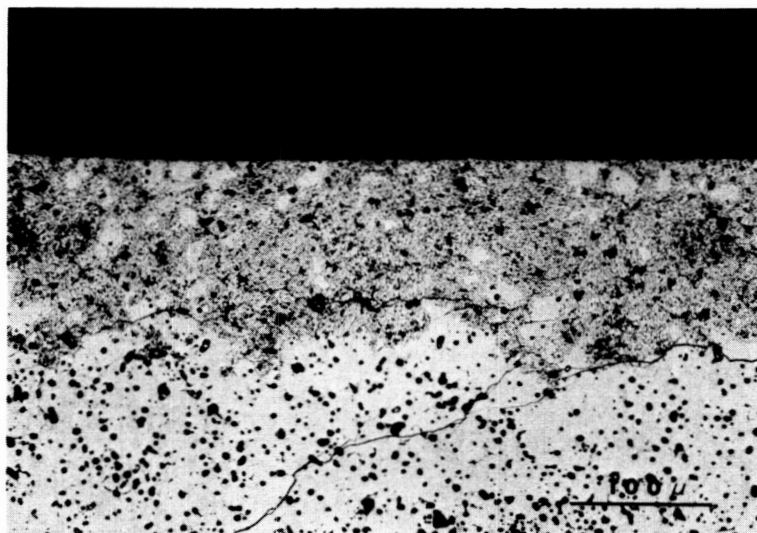
$\text{ZrO}_2 - 8 \text{ wt\% } \text{Y}_2\text{O}_3$

Exposure: 900°C 24 hr.

2 mol%  $\text{Na}_2\text{V}_2\text{O}_6$  in  $\text{Na}_2\text{SO}_4$



Exposed in air



Exposed to 93%  $\text{SO}_2$  5%  $\text{SO}_3$  2%  $\text{O}_2$

Figure 12.

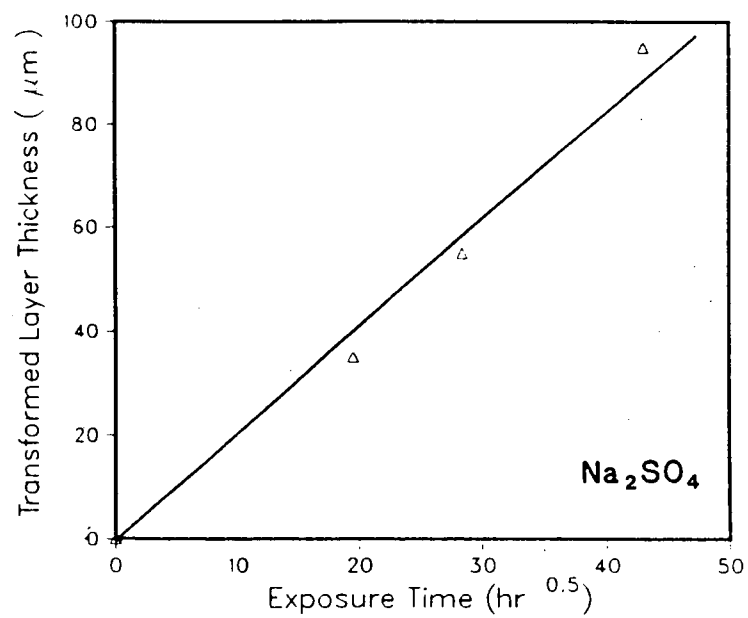


Figure 13.

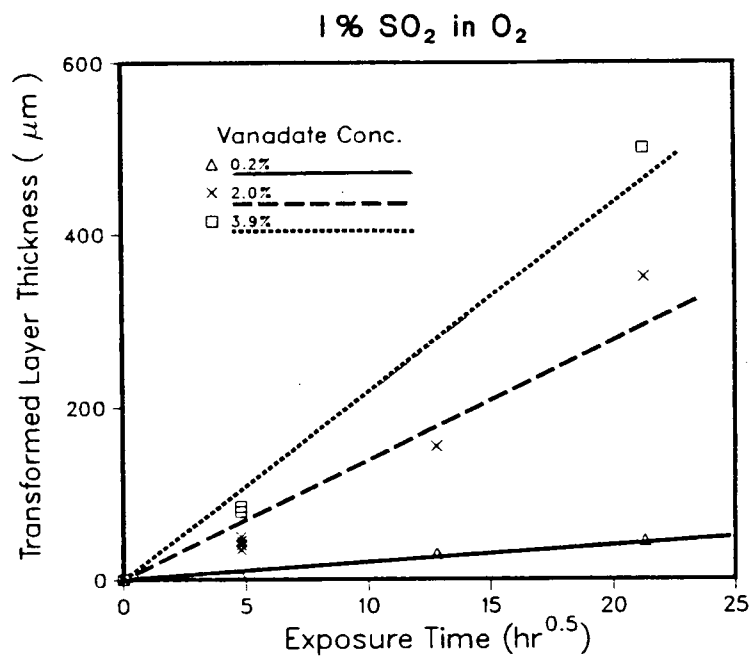
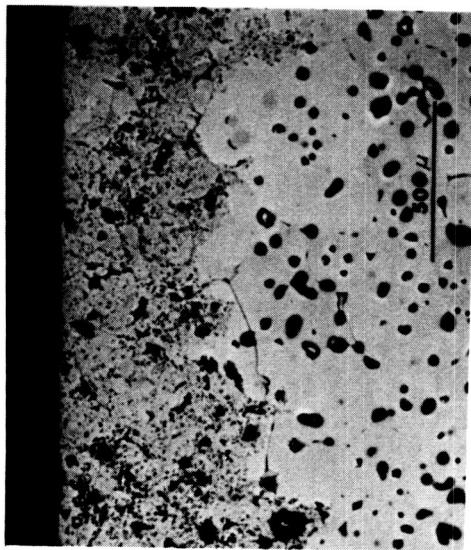


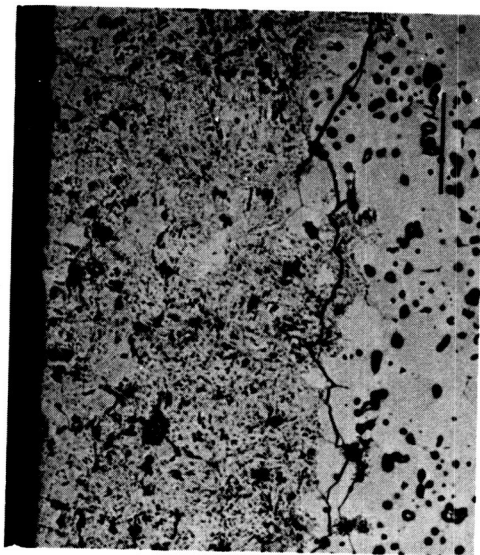
Figure 14.

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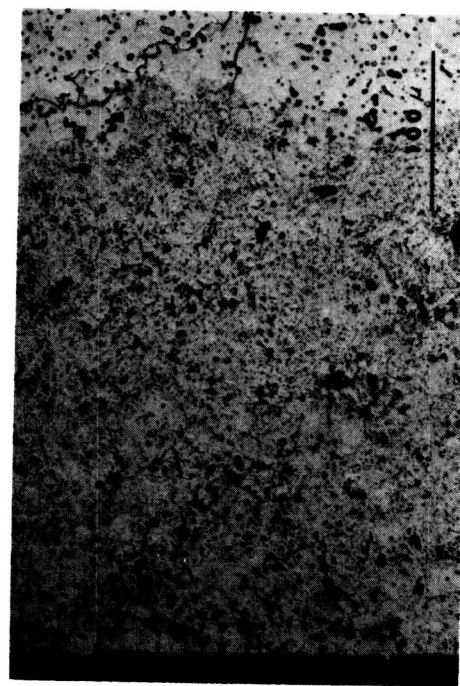
1173 K 1% SO<sub>2</sub> in O<sub>2</sub>



24 hr



164 hr



452 hr

Figure 15.

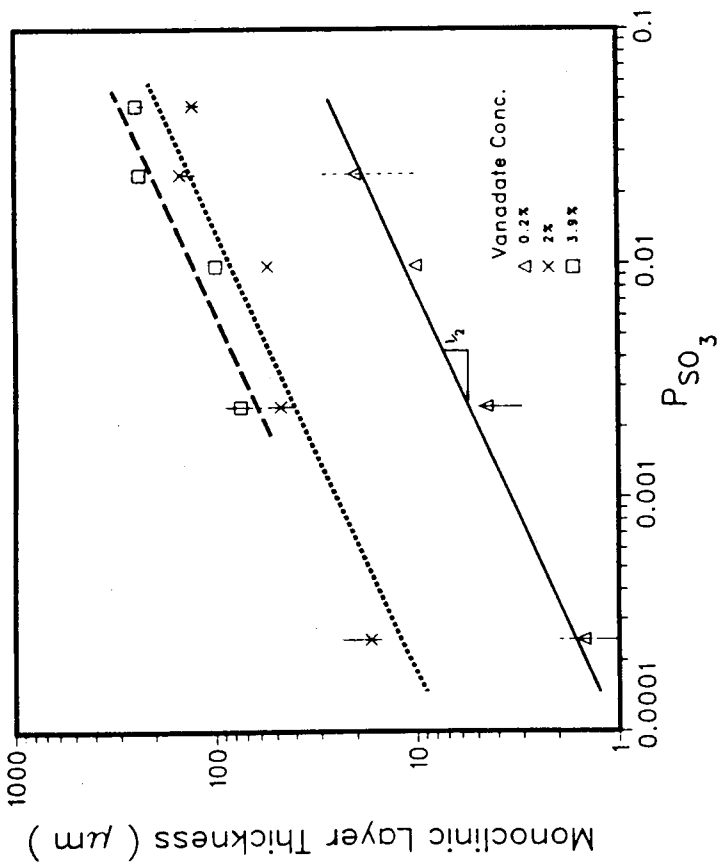


Figure 17.

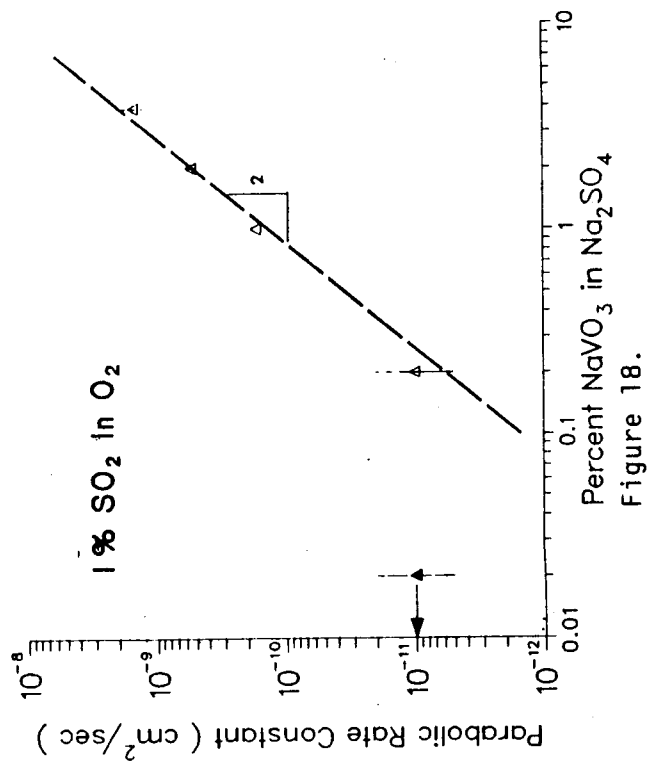


Figure 18.

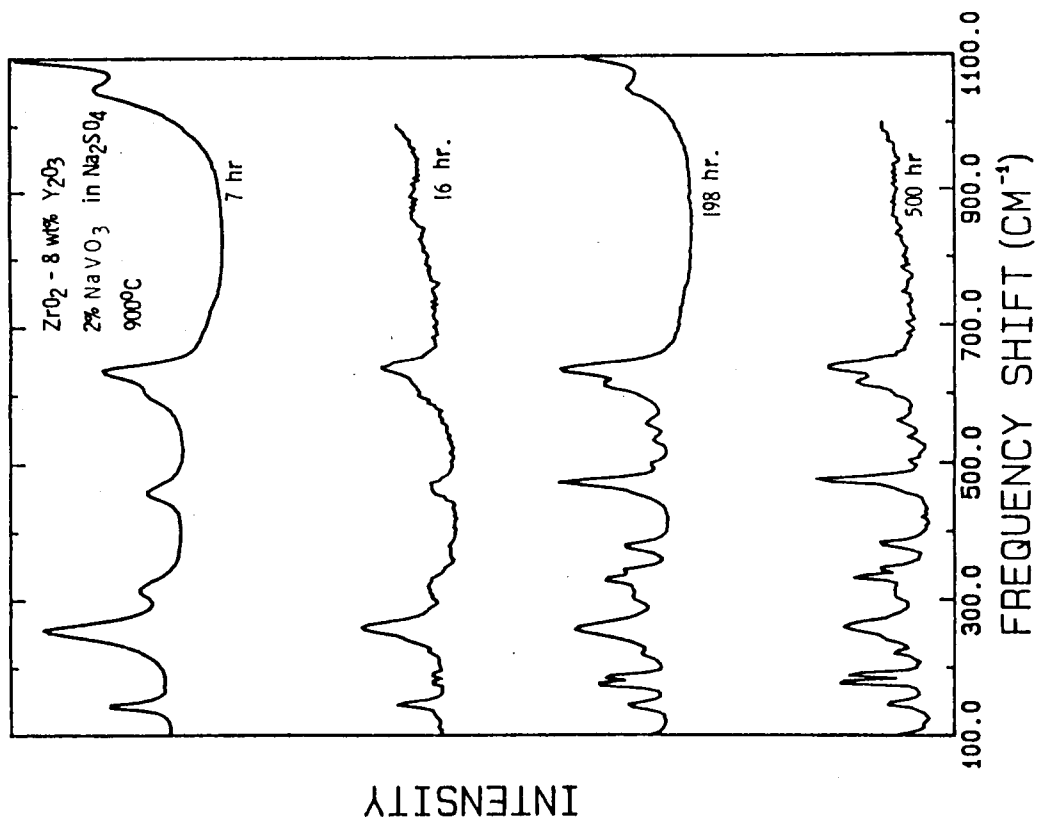
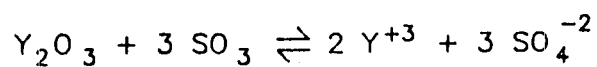


Figure 16.



## YTTRIUM LEACHING REACTIONS

– in sulfate melts



– in sulfate–vanadate melts

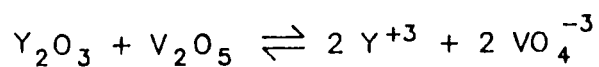
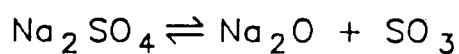
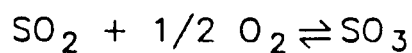
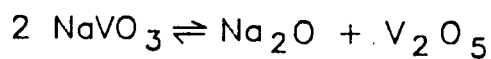


Figure 19.



$$a_{\text{Na}_2\text{O}} = \frac{K_2}{p_{\text{SO}_3}} a_{\text{Na}_2\text{SO}_4}$$



$$\begin{aligned} a_{\text{V}_2\text{O}_5} &= \frac{K_3 a_{\text{NaVO}_3}^2}{a_{\text{Na}_2\text{O}}} \\ &= \frac{K_3 p_{\text{SO}_3} a_{\text{NaVO}_3}^2}{K_2 a_{\text{Na}_2\text{SO}_4}} \end{aligned}$$

Figure 20.

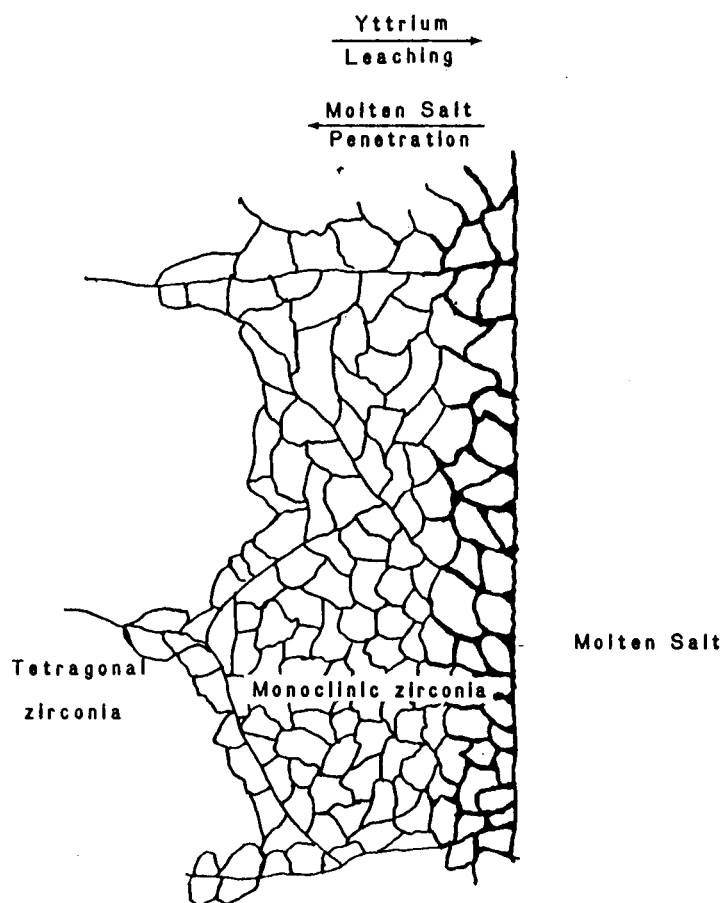
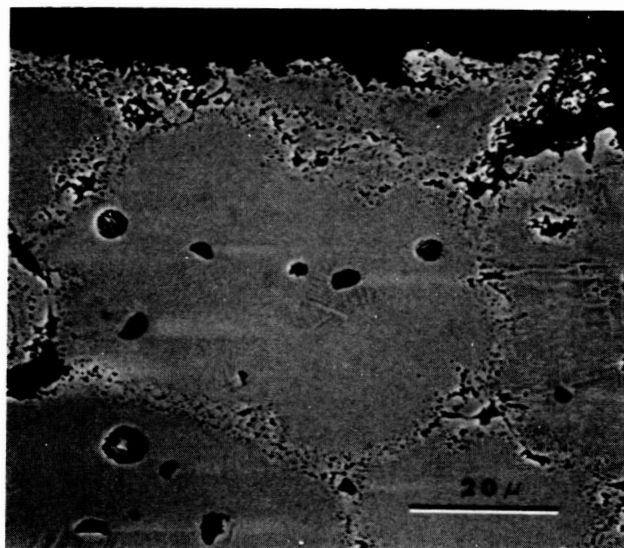


Figure 21.

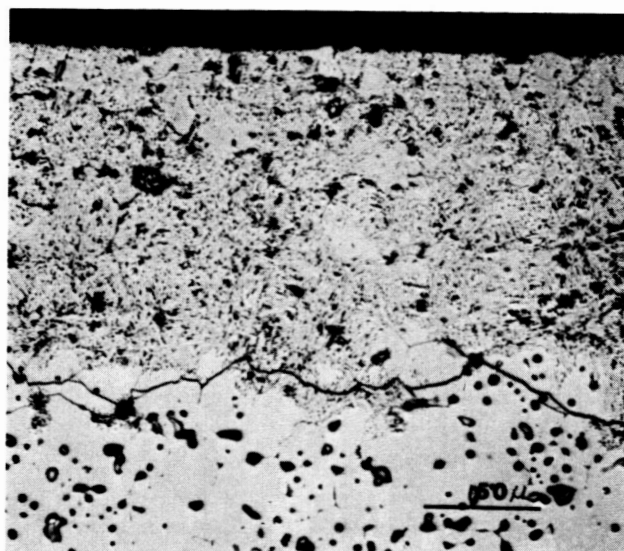
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1173 K 1% SO<sub>2</sub> in O<sub>2</sub>



ZrO<sub>2</sub> - 1.5 wt% MgO

96 hr



ZrO<sub>2</sub> - 8 wt% Y<sub>2</sub>O<sub>3</sub>

164 hr

Figure 22.

## Summary

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- Attack of zirconia ceramics is sensitive to sodium metavanadate concentration, and thus to vanadium impurity level in fuel.
- The attack is also sensitive to sulfur dioxide content of the environment.
- The attack follows parabolic kinetics and is proportional to the square root of the sulfur trioxide partial pressure.

Figure 23.