

**FATIGUE CRACK GROWTH MODEL
RANDOM2 USER MANUAL**

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Prepared by :

Lola Boyce, Ph.D., P.E.
Thomas B. Lovelace

APPENDIX 1
of Annual Report
of Project Entitled
Development of Advanced Methodologies
for Probabilistic Constitutive Relationships
of Material Strength Models

NASA Grant No. NAG 3-867

Prepared for :

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Lewis Research Center
Cleveland, OH 44135

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The Division of Engineering
The University of Texas at San Antonio
San Antonio, TX 78285
January, 1989

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1.0 INTRODUCTION

This User Manual documents the FORTRAN program RANDOM2. RANDOM2 is based on fracture mechanics using a probabilistic fatigue crack growth model. It predicts the random lifetime of an engine component to reach a given crack size (see Section 2.0, Theoretical Background).

Included in this Manual are details regarding the theoretical background of RANDOM2, input data instructions and a sample problem illustrating the use of RANDOM2. Appendix A gives information on the physical quantities, their symbols, FORTRAN names, and both SI and U.S. Customary units. Appendix B includes photocopies of the actual computer printout corresponding to the sample problem. Appendices C and D detail the IMSL, Ver. 10¹, subroutines and functions called by RANDOM2 and a SAS/GRAPH² program that can be used to plot both the probability density function (p.d.f.) and the cumulative distribution function (c.d.f.).

2.0 THEORETICAL BACKGROUND

Fatigue crack growth data are usually presented as cycles, N , to reach a particular crack length, a . The initial crack size is a_i . It is generally accepted that under constant amplitude alternating stress, fatigue crack growth can be related to stress intensity through a first order differential equation.³

$$da/dN = C(\Delta K)^m \quad (1)$$

where C is a material parameter, m is a material property (often a constant) and ΔK is the stress intensity range. Stress intensity range is given by

$$\Delta K = Y\Delta\sigma\sqrt{\pi a}$$

where Y is a constant dependent upon component and crack geometry and $\Delta\sigma$ is the constant amplitude alternating stress. Therefore, equation (1) can be written as

$$da/dN = C(Y\Delta\sigma\sqrt{\pi a})^m$$

or,

$$da/dN = C Y^m \Delta\sigma^m \pi^{m/2} a^{m/2} \quad (2)$$

Equation (2) can be integrated, from the initial crack length, a_i , to the final crack length, a_f , to yield N , the number of cycles. The result is

$$N = \frac{1}{CY^m \pi^{m/2} \Delta\sigma^m} \left[\frac{a_f^{-m/2+1} - a_i^{-m/2+1}}{-m/2 + 1} \right] \quad (3)$$

Thus, equation (3) gives the "cycles to reach a given crack length."

Metallurgical evidence indicates that casting pores play a significant role in the high-cycle fatigue life of cast nickel base-superalloys, especially at high temperatures.⁴ The location and size of these fatigue crack-initiating pores vary greatly from one aerospace propulsion system component to another. This accounts for the large variability in fatigue life and leads to consideration of fatigue crack growth as a random phenomenon.

Fatigue life directly relates to casting pore size, and pore size can be used to determine initial crack size, a_i . Thus, utilizing principles of both probabilistic analysis and fatigue crack growth, a quantitative probabilistic constitutive relationship between fatigue life and fracture mechanics parameters can be developed. Using the "randomized equation" approach, the fatigue crack growth model, given by equation (3) has the following form:

$$N = f(C, m, \Delta\sigma, a_i, a_f, Y) \quad (4)$$

or, in general,

$$N = f(X_i), i = 1, \dots, 6, \quad (5)$$

where the X_i are the six independent variables in equations (3) and (4). Equation (3) is "randomized" by assuming the first four variables in equation (4) to be random. Assuming a small crack in a relatively large component leads to assuming $Y = 1.0$, a deterministic value. A deterministic final crack size was chosen since experimental evidence indicated that it was relatively unimportant.³

Probabilistic analysis, via simulation, yields the distribution of the dependent random variable, cycles, N . A probability density function (p.d.f.) of cycles is generated using the maximum penalized likelihood method. Maximum penalized likelihood generates the p.d.f. estimate using the method of maximum likelihood together with a penalty function to smooth it.⁵

3.0 INPUT DATA

Data input for RANDOM2 is user friendly and easy to manipulate (see, for example, the file entitled NORMAL.INP, in Section 4.0). The first five lines of input have the same format, namely 2E12.4, and the last two lines differ. The last two lines of input have the formats I3,2X,I3,2X,2E12.4,2X,I3 and I3, respectively. A brief line by line description is given along with an example for each line (Note: the ruler is to aid the user in formatting and is not a part of the input). A table listing the physical quantities, their units and symbols is given in Appendix A.

1. Random Number Generator Seed, ISEED, and Sample Size, NTOT

EXAMPLE:

```
123456789012345678901234567890
      1                      40
```

2. Material Property, RMM

EXAMPLE:

```
123456789012345678901234567890
      28.0E-01          1.4E-01
```

3. Initial Crack Size (Pore Diameter), RAI

EXAMPLE:

```
123456789012345678901234567890
      300.0E-06        45.0E-06
```

4. Material Property, RCC

EXAMPLE:

```
123456789012345678901234567890
      2.20E-11         0.22E-11
```

5. Stress Range, DELSIG

EXAMPLE:

```
123456789012345678901234567890
      6.2E+02          6.2E+01
```

6. The DESPL ¹ parameters are NODE, INIT, ALPHA, EPS, MAXIT and are entered in that order as follows:

EXAMPLE:

1234567890123456789012345678901234567890
21 0 50.0E-01 10.0E-05 30

7. The DESPL parameter, IOPT, is entered as follows:

EXAMPLE:

1234567890
2

4.0 SAMPLE PROBLEM FOR RANDOM2

The objective of this program is to predict the random lifetime, to reach a given crack size for an engine component . The theory is based on fracture mechanics, using a probabilistic fatigue crack growth model (see Section 2.0, Theoretical Background). RANDOM2 input parameters are given in Table A1.1. Note that the first four parameters are random. Their means and standard deviations are input by the user. The last two parameters, A_f and Y , are deterministic and are fixed internally by the program. They are equal to the values shown in Table A1.1.

Table A1.1 RANDOM2 sample problem input (SI units)

FORTRAN Name	Distribution Type	Mean	Standard Deviation	
			(Value)	(% of Mean)
RMM	normal	28.0E-01	1.4E-01	(5%)
AI	lognormal	300.0E-06	45.0E-06	(15%)
RCC	lognormal	2.20E-11	0.22E-11	(10%)
DELSIG	lognormal	6.2E+02	6.2E+01	(10%)
AF	N/A	2.0E-03	N/A	
YY	N/A	1.0	N/A	

The input is entered in the following format in a file entitled NORMAL.INP.

```

1234567890123456789012345678901234567890
      1              40
28.0E-01      1.4E-01
300.0E-06      45.0E-06
2.20E-11      0.22E-11
6.2E+02      6.2E+01
21  0      50.0E-01      10.0E-05      30
  2
    
```

Execution of RANDOM2 (source code entitled NR2.FOR) produces an output file entitled RANDM22 giving intermediate results (see Appendix B). Execution also produces the plotfiles OUT1 and OUT2 (see Appendix B). These files are used to plot the X and Y axes of the probability density function (p.d.f.) and the cumulative distribution function (c.d.f.), respectively, generated by RANDOM2. The plots are drawn from the plotfiles by the SAS/GRAPH graphing program (see Appendix C). These plots for the sample problem are shown in Figures A1.1 and A1.2.

This same sample problem has been reported in Boyce and Chamis.⁶ There, however, it utilized U.S. Customary units and an older version of RANDOM2 (IMSL Version 9.2 subroutines).

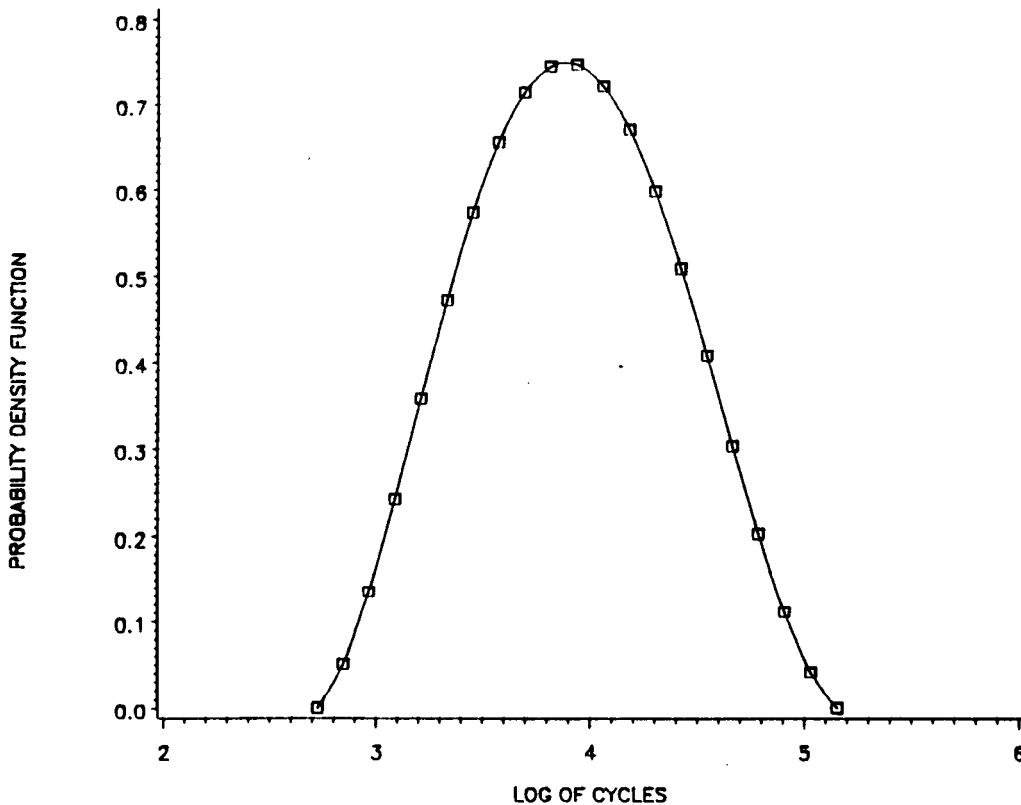


Fig. A1.1 p.d.f. of log of mechanical cycles for fatigue crack growth model, using maximum penalized likelihood.

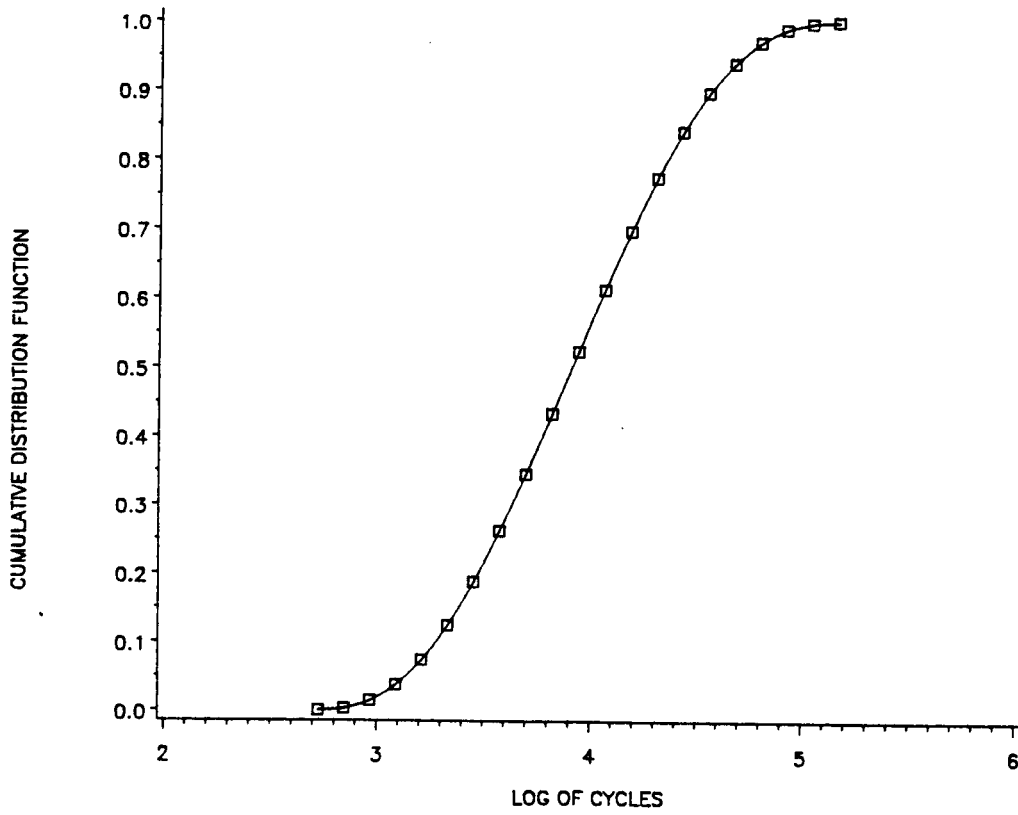


Fig. A1.2 c.d.f. of log of mechanical cycles for fatigue crack growth model, using maximum penalized likelihood.

5.0 REFERENCES

- ¹IMSL, "STAT/LIBRARY, FORTRAN Subroutines for Statistical Analysis", Houston, Texas, 1987.
- ² SAS Institute, Inc. SAS/GRAPH User's Guide, Version 5 Edition, Cary, NC: SAS Institute, Inc., 1985, p. 596.
- ³ Kozin, F. and Bogdanoff, J.K., "A Critical Analysis of Some Probabilistic Models of Fatigue Crack Growth," Engineering Fracture Mechanics, Vol. 14, 1981, pp. 55-89.
- ⁴ Hoffeler, W., "High-Cycle Fatigue-Life of the Cast Nickel Base-Superalloys in 738 LC and IN 939," Metallurgical Transactions A, Vol. 13A, July, 1982, pp. 1245-1255.
- ⁵ Scott, D.W., "Nonparametric Probability Density Estimation by Optimization Theoretic Techniques," NASA CR-147763, April, 1976.
- ⁶ Boyce, L. and Chamis, C.C., "Probabilistic Constitutive Relations for Cyclic Material Strength Models," Proceedings, 29th Structures, Structural Dynamics and Materials Conference, Williamsburg, VA, 1988.

6.0 APPENDIX A

PHYSICAL QUANTITIES, SYMBOLS, AND UNITS

The physical quantities, their symbols, and units for the fatigue crack growth model are given in the following table.

Table A1.2 Physical quantities, symbols, and units
for fatigue crack growth model for RANDOM2

Physical Quantity	Theory Symbol	FORTRAN Name	Units	
			SI	U.S.
Material Property	m	RMM	m/cycle/M Pa	m in/cycle/ksi
Initial Crack Size	A_i	RAI	m	in
Material Property	C	RCC	m/cycle	in/cycle
Alternating Stress	$\Delta\sigma$	DELSIG	M Pa	ksi
Final Crack Size	A_f	AF	m	in
Geometry Dependent Constant	Y	YY	(dimensionless)	

7.0 APPENDIX B

SAMPLE PROBLEM: SOURCE, INPUT AND OUTPUT FILES


```

CALL RNSSET(ISEED)
CALL RNLN(NTOT, YM, YS, RCC)
WRITE(6, 2021)
2021 FORMAT(5, 1001) MATERIAL PROPERTY, C'
C LOGNORMAL STRESS RANGE, DELSIG
WRITE(6, 1002) ISEED, NTOT
READ(5, 1011) XM, XS
WRITE(6, 1011) XM, XS
XS = 0.62E+02
XM = 5.2E+02
YS = SQRT(LOG(1.0+(YS/XM)**2))
YM = LOG(XM) - 0.5*YS**2
CALL RNSSET(ISEED)
CALL RNLN(NTOT, YM, YS, DELSIG)
WRITE(6, 2022)
2022 FORMAT(5, 1001) STRESS RANGE, DELSIG'
C DEFINE DETERMINISTIC PARAMETERS
C PI
PI = 3.1415926535897932384626433
C COMPONENT AND CRACK SHAPE PARAMETER, YY
YY = 1.0
C FINAL CRACK SIZE, AF
AF = 2.0E-03
C CALCULATE CYCLES TO REACH CRACK SIZE 2.0E-03M
XNF(1) = 0/(RCC(I))*PI**RMM(I)/2.*DELSIG(I)**
1 RMM(I) = ((AF**2 - RMM(I)/2.) - RAI(I)**(1 - RMM(I)/2.)) /
1 (1 - RMM(I)/2.)
XNF(I) = XNF1**XNF2
C CALCULATE LOG OF CYCLES TO REACH CRACK SIZE 2.0E-03M
XNF(I) = ALOG10(XNF(I))
101 CONTINUE
2023 FORMAT(5, 1001) LOG OF CYCLES TO REACH CRACK SIZE=2.0E-03M, '/,
1, GIVEN STRESS MEAN AMPLITUDE=6.2E+02MPA'
WRITE(6, 1001) XNF(I), I=1, NTOT)
C SORT LOG OF CYCLES
CALL SORT(XNF, NTOT)
WRITE(6, 2024)
2024 FORMAT(5, 1001) SORTED LOG OF CYCLES'
C XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
C CALCULATE PDF OF LOG OF CURRENT CYCLES, LOG XNF
WRITE(6, 985)
985 FORMAT(5, 1001) DESPL PARAMETERS'
WRITE(6, 1002) NODE, INIT, ALPHA, EPS, MAXIT
BND(2) = XNF(NTOT) + 0.05*XNF(NTOT)
WRITE(6, 979) BND(1), BND(2)
979 FORMAT(6, 980) BND(1), BND(2) = ,E12.4, I,X,E12.4)
CALL DESPL(NTOT, XNF, NODE, BND, INIT, ALPHA, MAXIT, EPS, DENS, STAT,
1 NMIS)
WRITE(6, 980)
980 FORMAT(5, 1001) PDF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDE PLOT'
WRITE(6, 981)
981 FORMAT(5, 1001) OUTPUT STATISTICS'
WRITE(6, 982)
982 FORMAT(5, 982) NUMBER OF MISSING VALUES'

```

```

WRITE(6,1010)NMISS
CC CALCULATE WINDOW WIDTH, HH
      HH=(BND5(2)-BND5(1))/(NODE-1)
CC CALCULATE VALUES OF LOG OF CURRENT CYCLES AT WHICH PDF IS ESTIMATED;
CC ALSO CALLED "NODE" VALUES
DO 6001, I=1, NODE-2
      BND5(I+2)=BND5(1) + (I*HH)
6001 CONTINUE
      WRITE(6,983)
983 FORMAT(7,983)
      WRITE(6,1001)(BND5(I), I=1, NODE)
CC REORDER BND5 FOR PLOTTING
      SAVE1 = BND5(2)
      SAVE2 = BND5(NODE)
      BND5(NODE)=BND5(2)
      DO 6002, I=1, NODE-2
      BND5(I+1)=BND5(I+2)
6002 CONTINUE
      BND5(NODE-1)=SAVE1
      BND5(NODE) =SAVE2
      WRITE(6,984)
984 FORMAT(7,984)
      1X AXIS PDF, ORDERED LOG OF CURRENT CYCLES, LOG XNF,
      WRITE(6,1002)(BND5(I), I=1, NODE)
CC WRITE LOG OF CURRENT CYCLES AND PDF OF LOG OF CURRENT CYCLES,
      LOG XNF TO PLOT FILES
990 WRITE(34,990) (E12, 4, 1X, E12, 4)
991 FORMAT(34,991) (BND5(J), DENS(J), J=1, NODE)
CC CALCULATE CDF OF LOG OF CURRENT CYCLES
      READ(5,1010)IOPT
      WRITE(6,992)
992 FORMAT(7,992)
      WRITE(6,1010)IOPT
      X0=BND5(1)
      DO 6003, I=1, NODE
      P=GCDF(X0, IOPT, NODE, BND5, DENS)
      BND5X(I)=X0
      X0=X0+HH
      DISTX(I)=P
6003 CONTINUE
      WRITE(6,994)
994 FORMAT(7,994)
      1X AXIS OF CDF, CDF, PLOT,
      WRITE(6,1001)(DISTX(I), I=1, NODE)
CC
      WRITE(6,993)
993 FORMAT(7,993)
      1X AXIS OF PDF, CDF PLOT,
      WRITE(6,1001)(BND5(I), I=1, NODE)
      WRITE(6,1001)(BND5X(I), I=1, NODE)
CC WRITE LOG OF CURRENT CYCLES AND CDF OF LOG OF CURRENT
      TO THE PLOT FILES

```

```

WRITE (35,990)
WRITE (35,991) (BNDS(J),DISTX(J),J=1,NODE)
STOP
END
CXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
C SUBROUTINE SORT (Y,N)
C DIMENSION Y(10000)
C Y IS THE ARRAY TO BE SORTED
C AT COMPLETION Y(1) IS SMALLEST VALUE
C AT COMPLETION Y(N) IS LARGEST VALUE
DO 1 I=1,N-1
  DO 2 J=I+1,N
    IF (Y(I).GT.Y(J)) GO TO 2
    TEMP = Y(I)
    Y(I) = Y(J)
    Y(J) = TEMP
  2 CONTINUE
1 CONTINUE
END

```

```

-----
IMSL Name: D3SPL/DD3SPL (Single/Double precision version)
Computer: IBM/SINGLE
Revised: November 1, 1985
Purpose: Nonparametric probability density function estimation
         estimation by the penalized likelihood method.
Usage:   CALL D3SPL (NOBS, X, NODE, BNDS, INIT, ALPHA, MAXIT, EPS,
         DENS, STAT, HESS, LDHES, ILOHI, DENEST, IPVT, WK2)

```

- Arguments:
- NOBS: Number of observations. (Input)
 - X: Vector of length NOBS containing the random sample of responses. (Input)
 - NODE: Number of mesh nodes for the discrete Pdf estimate. (Input)
 - BNDS: Vector of length 2 containing the minimum and maximum values for X(i) in BNDS(1) and BNDS(2), respectively. (Input)
 - INIT: Initialization option. (Input)
 - ALPHA: Positive penalty weighting factor which controls the smoothness of the estimate. (Input)
 - MAXIT: Maximum number of iterations allowed in the iterative procedure. (Input)
 - EPS: Convergence criterion. (Input)
 - DENS: Vector of length NODE containing the estimated values of the discrete Pdf at the NODE equally spaced mesh nodes. (Input/output if INIT=1, Output otherwise)
 - STAT: Vector of length 4 containing the log-likelihood and the log-penalty terms, respectively. STAT(3) and STAT(4) contain the estimated mean and variance for the estimated distribution. (Output)
 - HESS: Seven by NODE-2 hessian matrix (and its factorization). (Output)
 - LDHES: Leading dimension of HESS exactly as specified in the dimension statement in the calling program. (Input)
 - ILOHI: I-NOBE by 2 matrix containing the indices for the risk set

at each node value. (Output)
 DENEST - NODE by matrix containing the gradient vector, among
 other quantities. (Output)
 B - Vector of length NODE containing the NODE values.
 IPVT - Pivot vector of length NODE-2. (Output)
 WK2 - Work vector of length NODE-2. (Output)

Chapter: STAT/LIBRARY Density and Hazard Estimation

Copyright: 1985 by IMSL, Inc. All Rights Reserved.

Warranty: IMSL warrants only that IMSL testing has been applied
 to this code. No other warranty, expressed or implied,
 is applicable.

SUBROUTINE D3SPL (NOBS, X, NODE, BNDS, INIT, ALPHA, MAXIT, EPS,
 DENS, STAT, HESS, LDHES, ILOHI, DENEST, B,
 IPVT, WK2)

INTEGER NOBS, NODE, INIT, MAXIT, LDHES, ILOHI(*),
 IPVT(*)
 REAL ALPHA, EPS, X(*), BNDS(2), DENS(*), STAT(4),
 HESS(LDHES,*), DENEST(NODE), B(*), WK2(*)
 INTEGER I, IMPTR, IPTR, ITER, K, KMI, KM2, KPF1, H, H2, H3,
 KX, KVAL, BSMALL, CK, CKM1, CKM2, CKMCM1, CKP1, CKP2,
 CONS, LEPS1, FACTOR, FK, FKM1, FKM2, FKP1, H, H2, H3,
 SUM, TEMP, WK(4)
 DOUBLE PRECISION SUM1, SUM2, SUM3

INTEGER MINCR(8)
 SAVE MINCR

INTRINSIC ALOG, AMAX1, MAX0, MIN0, MOD, SORT
 INTEGER MAX0, MIN0, MOD
 REAL ALOG, AMAX1, SORT

EXTERNAL EIMES, EIFOP, EIFSH, EISTI, EISTR, SADD, SAXFY,
 SCOPY, SHPROB, SSCAL, D2SFT, L2TRB, LFSRB

EXTERNAL ISMIN, NIKRCD, SDOT, SNRM2, SSUM
 INTEGER ISMIN, NIKRCD
 REAL SDOT, SNRM2, SSUM

DATA MINCR/5, 9, 17, 33, 65, 129, 253, 100001/
 CALL EIFSH ('D3SPL')

NER = 1
 IF (NOBS .LT. 1) THEN
 CALL EIMES (5, 1, 'After removing all missing (NaN, not a
 ,number) values from X there are no valid
 ,observations. At least one valid observation
 ,is necessary.')

END IF
 IF (NODE .LE. 4) THEN
 CALL EISTI (1, NODE)
 CALL EIMES (5, 2, 'NODE = Z(I1). The number of mesh
 ,nodes, NODE, must be an odd integer greater
 ,')

ENDIF
 Error checks

Specifications for Intrinsic
 Specifications for Subroutines
 Specifications for Functions

Specifications for Save Variables

```

1 ELSE IF (MOD(NODE,2) .EQ. 0) THEN
2   CALL EISTI (1, NODE)
3   CALL EINES (5, 3, 'NODE = Z(I) must be an odd integer' //
4     'greater than 4.')
```

```

5 END IF
6 IF (ALPHA .LE. 0.0) THEN
7   CALL EISTR (1, ALPHA)
8   CALL EINES (5, 4, 'ALPHA = Z(R1). The penalty weighting' //
9     'factor which controls smoothness, ALPHA, must' //
10    'be greater than 0.')
```

```

11 END IF
12 IF (MAXIT .LE. 0.0) THEN
13   CALL EISTI (1, MAXIT)
14   CALL EINES (5, 5, 'MAXIT = Z(I1). The maximum number' //
15     'of iterations, MAXIT, must be greater than 0.')
```

```

16 END IF
17 IF (BNDS(1) .GT. BNDS(2)) THEN
18   CALL EISTR (1, BNDS(1))
19   CALL EISTR (2, BNDS(2))
20   CALL EINES (5, 6, 'BNDS(1) = Z(R1) and BNDS(2) = ' //
21     'Z(R2). The minimum value for X, BNDS(1), must' //
22     'be less than, or equal to the maximum value for' //
23     'X, BNDS(2).')
```

```

24 END IF
25 IF (INIT .NE. 0) THEN
26   CALL EISTR (1, 'NE, 0')
27   CALL EISTR (2, 'DENS(NODE), NE, 0')
28   CALL EISTR (3, 'DENS(1)')
29   CALL EISTR (4, 'DENS(NODE)')
30   CALL EISTR (5, 'DENS(2)')
31   CALL EISTR (6, 'DENS(1) = Z(R1) and DENS(NODE)=Z(I1)' //
32     'estimates of the density must be zero.')
```

```

33 END IF
34 IF (DENS(TSMIN(NODE, DENS(1))) .LT. 0) THEN
35   CALL EINES (5, 8, 'The initial estimates of the' //
36     'density, DENS, must be greater than or' //
37     'equal to 0.')
```

```

38 END IF
39 NOB1 = 0
40 DO I=1, NOBS
41   IF (X(I) .LT. BNDS(1) .OR. X(I) .GT. BNDS(2)) THEN
42     NOB1 = NOB1 + 1
43   END IF
44 END DO
45 IF (NOB1 .EQ. NOBS) THEN
46   CALL EINES (5, 9, 'All elements in X lie outside the' //
47     'interval BNDS(1) to BNDS(2). At least one' //
48     'element of X must lie in this interval.')
```

```

49 END IF
50 IF (EPS .LE. 0.0) THEN
51   EPS1 = 1.0E-4
52 ELSE
53   EPS1 = EPS
54 END IF
55 IF (NIRCD(0) .NE. 0) GO TO 9000
56 IMPTR = 0
57 IF (INIT .EQ. 0) THEN
58   DENS(1) = 0.0
59   DENS(2) = 2.0/(BNDS(2)-BNDS(1))
60   DENS(3) = 0.0

```

```

M = 3
ELSE M = NODE
END IF
C 20 IF (INIT.EQ. 0) THEN
      Refine mesh
      HOLD = M
      IMPTR = IMPTR + 1
      M = MINO(NODE, MINCR(IMPTR))
      END IF
      H = (BND(2) - BND(1)) / (M - 1)
      H2 = H * H
      H3 = H2 * H
      IF (INIT.NE. 0) THEN
        Make initial DENS integrate to 1.
        CALL SSCAL(NODE, 1.0 / (H * SSUM(NODE, DENS, 1)), DENS, 1)
      END IF
      Set mesh nodes
      B(1) = BND(1)
      DO 30 I = 2, M
        B(I) = B(I-1) + H
      30 CONTINUE
      Set B indices for interpolating X
      IPTR = 0
      IF (X(IPTR), LT, BND(1)) GO TO 40
      DO 60 N = 1, M - 1
        ILOHI(K, 1) = IPTR
        ILOHI(K, 2) = IPTR - 1
        IF (X(IPTR), LE, NOBS) THEN
          IF (X(IPTR), LT, B(K+1)) THEN
            ILOHI(K, 2) = ILOHI(K, 2) + 1
            IPTR = IPTR + 1
          IF (IPTR, LE, NOBS) GO TO 50
        END IF
      END IF
      60 CONTINUE
      70 FACTOR = 2.0 * ALPHA / H3
      IF (INIT.EQ. 0) THEN
        Initialize mesh node densities
        CALL D2SPT(M-2, B(2), 1, MOLD, BND, DENS, DENEST, WK, WK,
          &
          TEMP = 1.0 / (M * H * H)
          DO 80 I = 2, M - 1
            DENS(I) = AMAX1(TEMP, SQRT(DENEST(I-1, 1)))
          80 CONTINUE
        ELSE
          DO 90 I = 2, M - 1
            Via the initial estimates
            DENS(I) = SQRT(DENS(I))
          END IF
          DENS(M) = 0.0
          Maximize
          DO 140 ITER = 1, MAXIT
            Get Hessian - Lagrangian
            HESS(1, 1) = 0.0
            HESS(1, 2) = 0.0
            HESS(2, 1) = 0.0
            HESS(2, 2) = 0.0
            SUM = 0.0
          140 CONTINUE
          CN** are true estimates = FK**2

```

```

DO 120 K=2, M-1
  KMI = K
  KX0(1,K-2)
  KP1 = K + 1
  KP2 = MINS(M,K+2)
  FK = DENS(K)
  FKM1 = DENS(KMI)
  FKM2 = DENS(KM2)
  CKM1 = FKM1**2
  CKM2 = FKM2**2
  CKP1 = DENS(KP1)**2
  CKP2 = DENS(KP2)**2
  BK = B(K)
  BKMI = B(KMI)
  SUM = SUM + CK
  IF (K.GE.4) HESS(1,KMI) = 4.0*FK*FKM2*FACTOR
  SUM1 = 0.0D0
  SUM2 = 0.0D0
  SUM3 = 0.0D0
  DO 100 I=ILOHI(K,1), ILOHI(K,2)
    TEMP = (X(I)-BK)/H
    CONS = (1.0-TEMP)/(CK+(CKP1-CK)*TEMP)
    SUM1 = SUM1 + CONS
    SUM2 = SUM2 + CONS*CONS
  CONTINUE
  CKMCHI = CK*CKM1
  DO 110 I=ILOHI(KMI,1), ILOHI(KMI,2)
    CONS = (X(I)-BKMI)/H
    TEMP = CKMI + CKMCHI*CONS
    SUM1 = SUM1 + CONS/TEMP
    TEMP = TEMP*TEMP
    SUM2 = SUM2 + (CONS*CONS)/TEMP
    SUM3 = SUM3 + CONS*(1.0-CONS)/TEMP
  CONTINUE
  TEMP = 2.0*TEMP
  RSMALL = RSMALL + 2.0*CK*TEMP
  HESS(3,KMI) = TEMP + 4.0*CK**6.0*FACTOR*SUM2)
  IF (K.NE.2) HESS(2,KMI) = 4.0*FK*FKM1*(-4.0*FACTOR+SUM3)
  DENEST(KMI,1) = FK*TEMP
  DENEST(KMI,2) = -2.0*FK
  CONTINUE
  RSMALL = 1.0/H - SUM + RSMALL
  CALL SCOPY (M-2, DENEST(1,2), 1, DENEST(1,3), 1)
  CALL SADD (M-2, -RSMALL/(2.0*SUM), HESS(3,1), LDHES)
  CALL SCOPY (M-4, HESS(1,3), LDHES, HESS(5,1), LDHES)
  HESS(2,M-3) = 0.0
  HESS(3,M-2) = 0.0
  CALL SCOPY (M-3, HESS(2,2), LDHES, HESS(4,1), LDHES)
  CALL L2TRB (M-2, HESS, LDHES, 2, 2, HESS, LDHES, IPVT, WK2)
  CALL LFSRB (M-2, HESS, LDHES, 2, 2, IPVT, DENEST, 1, DENEST)
  CALL LFSRB (M-2, HESS, LDHES, 2, 2, IPVT, DENEST(1,2), 1, DENEST(1,2))
  IF (NIRCD(1).NE.0) GO TO 9000
  CONS = SDOT(M-2, DENEST(1,3), DENEST(1,2), 1)
  CONS = (1.0/H-SUM-SDOT(M-2, DENEST(1,3), DENEST(1,1), 1))/CONS
  Update the gradient

```

```

100 C CALL SAXPY (M-2, CONS, DENEST(1,2), 1, DENEST(1,1), 1)
101 C CALL SAXPY (M-2, -1.0, DENEST(1,1), 1, DENEST(2), 1)
102 C TEMP = SNRM2(M-2, DENEST(2), 1)
103 C IF (SNRM2(M-2, DENEST(1), 1) .GT. EPS1*TEMP) GO TO 150
104 C TEMP = TEMP*1.0E-4/SQRT(M-2.0)
105 C DO 130 I=2, M-1
106 C DENEST(I) = AMAX1(TEMP, DENEST(I))
107 C CONTINUE
108 C CALL EISHT (1, MAXIT)
109 C CALL EIHES (3, 1)
110 C IF (MAXIT=2(I)) GO TO 150
111 C IF (M.NE. NODE).GO TO 20
112 C SUM1 = 0.0
113 C DO 160 K=1, M
114 C KMI = MAX0(K-1, 1)
115 C KPI = MIN0(K+1, M)
116 C SUM1 = SUM1 + (DENS(KMI)-2.0*DENS(K)+DENS(KPI))**2
117 C CONTINUE
118 C SUM2 = -0.5*FACTOR*SUM1
119 C STAT(2) = 0.0
120 C DO 170 I=1, NORS
121 C IF (X(I).GE.BNDS(1) .AND. X(I).LE.BNDS(2)) THEN
122 C CALL D2SPT (1, X(I), 1, NODE, BNDS, DENS, DENEST, WK, WK,
123 C & SUM2 = SUM2 + ALOG(DENEST(1,1))
124 C END IF
125 C STAT(1) = SUM2
126 C SUM1 = 0.0
127 C SUM2 = 0.0
128 C DO 180 K=1, M-1
129 C FKPI = DENS(K)
130 C BK = B(K)
131 C CONS = FK + FKPI
132 C TEMP = CONS + FKPI
133 C SUM1 = SUM1 + H2*TEMP/6.0 + 0.5*H*BK*CONS
134 C SUM2 = SUM2 + H3*(TEMP+FKPI)/12.0 + H2*BK*TEMP/3.0 +
135 C & 0.5*H*BK*BK*CONS
136 C CONTINUE
137 C STAT(3) = SUM1
138 C STAT(4) = SUM2 - SUM1*SUM1
139 C CALL E1POF ('D3SPL ')
140 C RETURN
141 C /EOF

```


1
28.0E-01
300.0E-06
2.20E-11
6.2E+02
21

40
1.4E-01
45.0E-06
0.22E-11
50.0E-01
22

10.0E-05 30


```

21 0.5000E+01 0.1000E-03 0.5153E+01 0.3725E-01 0.3089E+01 0.3210E+01
MDS(1), RMS(2)= 0.2724E+01 0.5153E+01 0.3725E-01 0.3089E+01 0.3210E+01
DF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF PLOT 0.3696E+01
0.0000E+00 0.5049E-01 0.1355E+00 0.2417E+00 0.3572E+00
0.4790E+00 0.5719E+00 0.6542E+00 0.7124E+00 0.7426E+00
0.7450E+00 0.7193E+00 0.6683E+00 0.5957E+00 0.5055E+00
0.4067E+00 0.3027E+00 0.2019E+00 0.1118E+00 0.4101E-01
0.0000E+00
OUTPUT STATISTICS
-0.2267E+02 -0.3434E+02 0.3913E+01 0.2276E+00
NUMBER OF MISSING VALUES
LOG OF CURRENT CYCLES, LOG XNF 0.3846E+01 0.3967E+01 0.3089E+01
0.3221E+01 0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01
0.3817E+01 0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01
0.4424E+01 0.4546E+01 0.4667E+01 0.4789E+01 0.4910E+01
0.5031E+01
DRIVER LOG OF CURRENT CYCLES, LOG XNF, X AXIS PDF, CDF PLOT 0.3089E+01
0.2724E+01 0.2346E+01 0.2967E+01 0.3089E+01 0.3210E+01
0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01 0.3817E+01
0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01 0.4424E+01
0.4546E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
CDF PARAMETERS
CDF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF, CDF PLOT
0.0000E+00 0.3089E-02 0.1435E-01 0.3725E-01 0.7362E-01
0.1239E+00 0.1872E+00 0.2616E+00 0.3446E+00 0.4329E+00
0.5232E+00 0.6121E+00 0.6969E+00 0.7731E+00 0.8400E+00
0.8955E+00 0.9385E+00 0.9699E+00 0.9882E+00 0.9975E+00
1.0000E+01
ORDERED LOG OF CURRENT CYCLES, LOG XNF, X AXIS OF PDF, CDF PLOT
0.2724E+01 0.2346E+01 0.2967E+01 0.3089E+01 0.3210E+01
0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01 0.3817E+01
0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01 0.4424E+01
0.4546E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
0.5153E+01
CDF PARAMETERS
CDF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF, CDF PLOT
0.0000E+00 0.3089E-02 0.1435E-01 0.3725E-01 0.7362E-01
0.1239E+00 0.1872E+00 0.2616E+00 0.3446E+00 0.4329E+00
0.5232E+00 0.6121E+00 0.6969E+00 0.7731E+00 0.8400E+00
0.8955E+00 0.9385E+00 0.9699E+00 0.9882E+00 0.9975E+00
1.0000E+01
ORDERED LOG OF CURRENT CYCLES, LOG XNF, X AXIS OF PDF, CDF PLOT
0.2724E+01 0.2346E+01 0.2967E+01 0.3089E+01 0.3210E+01
0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01 0.3817E+01
0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01 0.4424E+01
0.4546E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
0.5153E+01
CDF PARAMETERS

```


1118:03:1152	7.6744	USER	TEMPORARY DATASET SECTORS USED -	5
1118:03:1155	7.6744	USER	PERMANENT DATASET SECTORS ACCESSED -	4792
1118:03:1161	7.6744	USER	SECTORS QUEUED TO FRONT END -	1
1118:03:1164	7.6744	USER	SECTORS QUEUED TO FRONT END -	1
1118:03:1170	7.6744	USER	7.6742 CPU seconds =	5.7557 RT seconds (82%)
1118:03:1177	7.6744	USER	467 I/O requests =	0.1401 RT seconds (2%)
1118:03:1180	7.6744	USER	1.7996 CHXCPU mwd\$sec =	0.5399 RT seconds (8%)
1118:03:1185	7.6744	USER	1.8168 CHX I/O requests =	0.5450 RT seconds (8%)
1118:03:1186	7.6747	USER	Total =	6.9807 RT seconds
1118:03:1189	7.6747	USER	RT cost at bid priority 2 = \$	0.97
1118:03:1192	7.6747	USER		

8.0 APPENDIX C

IMSL SUBROUTINE CALLS FROM RANDOM2

1. RNSET - Initializes a random seed for use in the IMSL random number generators.
2. RNNOR - Generates pseudorandom numbers from a standard normal distribution using an inverse CDF method.
3. RNLNL - Generates pseudorandom numbers from a lognormal distribution.
4. DESPL - Performs nonparametric probability density function estimation by the penalized likelihood method.
5. GCDF - Evaluates a general continuous cumulative distribution function given ordinates of the density.

9.0 APPENDIX D

SAMPLE SAS/GRAPH (VER. 5.16) PROGRAM FOR RANDOM2

```
data a;
INFILE 'OUT1.CPR' FIRSTOBS=2;input x y;
GOPTIONS DEVICE=HP7470;
proc gplot;
  axis1 label=(h=1 f=simplex 'LOG OF CYCLES')
        value=(h=1 f=simplex);
  axis2 value=(h=1 f=simplex) label=none;
  plot y*x / haxis=axis1 vaxis=axis2;
  TITLE H=1 A=90 F=SIMPLEX 'PROBABILITY DENSITY FUNCTION';
  symbol i=spline v=square;
data B;
INFILE 'OUT2.CPR' FIRSTOBS=2;input x y;
proc gplot;
  axis1 label=(h=1 f=simplex 'LOG OF CYCLES')
        value=(h=1 f=simplex);
  axis2 value=(h=1 f=simplex) label=none;
  plot y*x / haxis=axis1 vaxis=axis2;
  TITLE H=1 A=90 F=SIMPLEX 'CUMULATIVE DISTRIBUTION FUNCTION';
  symbol i=spline v=square;
```