

Solid Rocket Motors Morton Thiokol. Inc

## RSRM-3 (360L003) FINAL REPORT <br> BALLISTICS/MASS PROPERTIES

5 May 1989

Prepared for:

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Contract No. NAS8-30490
DR. No.
WBS.No.

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Aerospace Group

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## Space Booster: Proyr.an Morton Thiokul line

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TITLE
RSRM-3 (360L003) FINAL REPORT BALLISTICS/MASS PROPERTIES
5 May 1989
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### 1.0 INTRODUCTION

This report contains the propulsion performance and reconstructed mass properties data from Morton Thiokol's RSRM-3 motors which were assigned to the STS-29 launch. The Morton Thiokol manufacturing designation for the motors were $360 \mathrm{LOO3-A}, \mathrm{~B}$ which are referred in this report as RSRM-3A and RSRM-3B, respectively. The launch occurred on 13 March 1989 at the Eastern Test Range (ETR). The data contained herein was input to the STS-29 Flight Evaluation Report.

The SRM propellant, TP-H1148, is a composite type solid propellant, formulated of polybutadiene acrylic acid acryonitrile terpolymer binder (PBAN), epoxy curing agent, ammonium perchlorate oxidizer and aluminum powder fuel. A small amount of burning rate catalyst (iron oxide) was added to achieve the desired propellant burn rate. The propellant evaluation and raw material information for the RSRM-3 is included in the discussion section of this report.

The propellant grain design consists of a forward segment with an eleven point star with a transition into a tapered circular perforated (CP) configuration, two center segments that result in a double tapered CP configuration and an aft segment with a triple taper CP configuration, and a cutout for the partially submerged nozzle (Figure 1.1).

The ballistic performance presented in this report was based on the OFI 12.5 sample per second pressure data for the steady state and tailoff portion of the pressure trace. The OFI data on the left motor was adjusted down by 0.2 percent to closer match the magnitude of the real time data. The ignition buildup and maximum headend pressure was assessed using the 320 samples per second DFI data. The DFI data magnitudes were below that of the OFI and real time data, therefore, the left and right motor DFI data was adjusted up by 0.4 and 0.6 percent respectively.

### 2.0 SUMMARY

The delivered propellant burn rates were close to predicted. The delivered burn rates were $0.367 \mathrm{in} / \mathrm{sec}$ at 625 psia and $60^{\circ} \mathrm{F}$ and 0.368 for the left and right motors respectively. This was $0.001 \mathrm{in} / \mathrm{sec}$ lower than predicted for the left motor and the same as predicted for the right
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motor. The average of the two motors was $0.0005 \mathrm{in} / \mathrm{sec}$ below the target rate of $0.368 \mathrm{in} / \mathrm{sec}$ at 625 psia and $60^{\circ} \mathrm{F}$. The performance of the two motors were very close to the same as can be seen in Figure 2.2.

The performance of the pair of motors were compared to the following CEI Specification CPW1-3600 paragraphs for compliance: 3.2.1 Performance, 3.2.1.1 General Performance, 3.2.1.1.1 Ignition Characteristics, 3.2.1.1.1.1 Ignition Interval, 3.2.1.1.1.2 Pressure Rise Rate, 3.2.1.1.2 Motor Characteristics, 3.2.1.1.2.1 Nominal Thrust Time Curve, 3.2.1.1.2.2 Performance Tolerance and Limits, 3.2.1.1.2.3 Thrust Differential, 3.2.1.1.2.4 Impulse Gates. The performance from each motor as well as matched pair performance values were well within the CEI Specification requirements. The nominal thrust time curve and impulse gate information has been included. The historical average was well within the variation limits developed from the HPM Block prediction population at a burn rate of $0.368 \mathrm{in} / \mathrm{sec}$ at 625 psia and $60^{\circ} \mathrm{F}$. The historical population values are the average performance data from QM-4, SRM-8A, SRM-8B, SRM-9A, SRM-10A, SRM-10B, SRM-11B through SRM-19B, SRM-24A, SRM-24B, ETM-1A, DM-8, DM-9, QM-6, QM-7, PVM-1, RSRM-1, RSRM-2, and RSRM-3. The motors used in the HPM Block prediction population were $0 M-4$, SRM-8A, 8B, 9A, $10 \mathrm{~A}, 10 \mathrm{~B}, 11 \mathrm{~B}, 13 \mathrm{~A}$, and 13B.

Post flight reconstructed Redesigned Solid Rocket Motor (RSRM) mass properties are within expected values for the lightweight (RSRML) configuration and meet the following CEI paragraphs:3.2.2.2, 3.2.2.2.1, 3.2.2.2.2, and 3.2.2.2.3.

### 3.0 DISCUSSION AND RESULTS

3.1 RSRM-3 PROPELLANT MATERIALS

Both of the third flight motors were cast with primarily one evaluation of propellant, E63. The left motor contained two mixes from evaluation E64V in the center aft segment and two in the aft segment. The right motor was cast all from evaluation E63. Table 3.1 shows the raw material lots and vendors for the evaluations used.

TABLE 3.1
RAW MATERIAL EVALUATION SUMMARY

TP-H1148 PROPELLANT EVALUATION E63

| Ingredient |  | Stock-Lot |
| :--- | :--- | :--- |
| HB Polymer |  | $7227-0067$ |
|  | $7225-0075$ | Vendor |
| ECA | ASRC |  |
| Aluminum | $7228-0064$ | Dow Chemical |
| $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | $7226-0021$ | ALCAN |
| AP unground | $7229-0071$ | Charles Pfister |
| AP ground | $7229-0071$ | PEPCON |
|  |  | PEPCON |

TP-H1148 PROPELLANT EVALUATION E64 (VERIFICATION)

| Ingredient | $\frac{\text { Stock-Lot }}{}$ | Vendor |
| :--- | :--- | :--- |
| HB Polymer | $7227-0068$ | $\frac{\text { ASRC }}{}$ |
| ECA | $7225-0076$ | Dow Chemical |
| Aluminum | $7228-0065$ | ALCAN |
| $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | $7226-0021$ | Charles Pfister |
| $\mathrm{AP}^{2}$ unground | $7229-0074$ | Kerr McGee |
| AP ground | $7229-0074$ | Kerr McGee |

### 3.2 RSRM PROPULSION PERFORMANCE ANALYSIS

All times shown in this section, unless noted otherwise are referenced to the RSRM ignition command time at 1989:072:14:57:00:017 (EDT).

As previously mentioned the $0 F I(12.5 \mathrm{~s} / \mathrm{s})$ data was used for the steady state and tailoff performance assessment. It compared well with the real time data although the left motor OFI data needed to be adjusted up 0.2 percent. The high sample rate DFI data ( $320 \mathrm{~s} / \mathrm{s}$ ) needed to be adjusted to match the magnitudes of the real time data. The DFI data for the left motor was adjusted up 0.4 percent and the right motor DFI data was adjusted up 0.6 percent. After the adjustments were made to the DFI data, it was used to assess the ignition characteristics and maximum headend pressure of each motor.

The ballistic performance was reconstructed using SCB04 steady state 1-D mass addition computer program, and SCA08 SRM modeling program. Both computer codes have been consistently used for predictions as well as
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reconstructions throughout the SRM program. Since thrust was not measured on the flight motors, average values of $\eta_{r}$ 's and $C_{m}$ 's, which are used for the pressure to thrust conversion, were taken from RSRM static test motors and applied to the measured headend pressure to determine the thrust values. The ignition characteristics of the motors were assessed using a 5-point running average smoothing method to reduce noise level in the raw pressure data.
3.3 RSRM DELIVERED PERFORMANCE
3.3.1 RSRM-3A/RSRM-3B Thrust and Pressure Comparison

The flight motor reconstructed thrust-time traces at the delivered temperature of $62^{\circ} \mathrm{F}$ are shown in figure 2.1. A comparison between the predicted thrust and reconstructed thrust for each motor can be seen in Figures 3.1, 3.2. Figure 2.2 shows the RSRM-3B igniter inside of the igniter lot acceptance specification.

The comparison of predicted and measured headend chamber pressure is shown in Figures 3.3, 3.4.

Figures 3.5 and 3.6 show how RSRM-3A and RSRM-3B compared with a nominal performance average for the RSRM at standard conditions of 0.368 burn rate and 60 degree $F$ PMBT. From the figures, it is evident that the RSRM design will continue to influence the shape of the average thrust time trace near 50 seconds.
3.3.2 RSRM Predicted Impulse, ISP, Burn Rate, Event Times, Separation, and PMBT Comparison
The reconstructed RSRM propulsion performance is compared to the predicted performance in Table 3.2. The actual values are very close to the predicted data for both motors and well within specification limits.

Figure 3.7 shows the high sample rate data points used to evaluate the ignition characteristics. Figure 3.8 shows the DP/DT or pressure rise rate curve. The calculated pressure rise rate for RSRM-3A was 82.7 psia/10 ms while that of RSRM-3B was 89.9 psia/ 10 ms . Table 3.3 lists the ignition history of all SRMs that were instrumented for high sample rate pressure data.

A comparison of actual and predicted propellant burn rates to the target burn rate for the flight RSRMs at a PMBT of $60^{\circ} \mathrm{F}$ is shown in Figure 3.9. The predicted scale factor of 1.0175 for conversions from 5

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inch CP burn rates to actual motor burn rate were based on an average scale factor from the HPM-RSRM population. The actual scale factors for left and right motors respectively were 1.0130 and 1.0177 .

The predicted propellant mean bulk temperature (PMBT) for both motors was $62^{\circ} \mathrm{F}$. This was based on predicted 2-D temperature gradients expected in the RSRMs. Table 3.4 shows the predicted gradient.


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TABLE 3.3
HISTORICAL THREE POINT AVERAGE thrust and pressure rise rate data

| MOTOR | $\begin{gathered} \text { OCCURRENCE } \\ \text { TIME } \\ \hline \end{gathered}$ | PRESSURE RISE RATE | OCCURRENCE TIME | THRUST RISE RATE | IGNITION <br> INTERVAL |
| :---: | :---: | :---: | :---: | :---: | :---: |
| STATIC |  | (PSI/10 ms) |  | (LBF/10 ms) |  |
| DM-2 | 0.1480 | 85.30 | 0.1480 | 245380 | 0.2330 |
| QM-1 | 0.1560 | 86.38 | 0.1560 | 246128 | 0.2362 |
| QM-2 | 0.1640 | 93.58 | 0.1720 | 234950 | 0.2391 |
| QM-3 | 0.1560 | 94.45 | 0.1520 | 245615 | 0.2287 |
| QM-4 | 0.1505 | 91.96 | 0.2225 | 234438 | 0.2192 |
| ETM-1A | 0.1520 | 86.72 | 0.1560 | 230023 | 0.2279 |

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| SRM-1A | 0.1530 | 87.58 | 0.2373 |
| :--- | ---: | ---: | ---: |
| SRM-1B | 0.1500 | 91.57 | 0.2358 |
| SRM-2A | 0.1530 | 90.74 | 0.2348 |
| SRM-2B | 0.1660 | 90.27 | 0.2345 |
| SRM-3A | 0.1500 | 91.05 | 0.2308 |
| SRM-3B | 0.1500 | 89.68 | 0.2271 |
| SRM-5A | 0.1530 | 95.10 | 0.2361 |
| SRM-5B | 0.1660 | 84.43 | 0.2380 |
| SRM-6A | 0.1530 | 92.72 | 0.2342 |
| SRM-6B | 0.1470 | 88.22 | 0.2329 |
| SRM-7A | 0.1500 | 99.90 | 0.2282 |
| SRM-7B | 0.1500 | 99.32 | 0.2276 |
| SRM-8A | 0.1530 | 106.29 | 0.2224 |
| SRM-8B | 0.1500 | 91.06 | 0.2196 |
| SRM-9A | 0.1530 | 92.31 | 0.2303 |
| SRM-10A | 0.1530 | 92.89 | 0.2373 |
| SRM-10B | 0.1500 | 84.56 | 0.2342 |
| SRM-13B | 0.1410 | 98.85 | 0.2115 |


| NUMBER | 24 |
| :--- | ---: |
| AVERAGE | 91.87 |
| STANDARD DEVIATION | 5.31 |


| 236,357 | 0.2307 |
| :---: | ---: |
| 11,977 | 0.0069 |
| 5.07 | 2.99 |


| DM-8 | 0.1680 | 77.00 | 0.1670 | 234,001 | 0.2424 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DM-9 | 0.1640 | 81.00 | 0.1720 | 275,525 | 0.2436 |
| QM-6 | 0.1480 | 87.40 | 0.1520 | 211,476 | 0.2321 |
| QM-7 | 0.1480 | 99.60 | NA | NA | 0.2230 |
| PVM-1 | 0.1520 | 92.80 | 0.1520 | 294,664 | 0.2338 |
| RSRM-1A | 0.1501 | 99.00 | NA | NA | 0.2296 |
| RSRM-1B | 0.1596 | 80.50 | NA | NA | 0.2310 |
| RSRM-2A | 0.1584 | 87.30 | NA | NA | 0.2410 |
| RSRM-2B | 0.1521 | 100.2 | NA | NA | 0.2360 |
| RSRM-3A | 0.1560 | 82.70 | NA | NA | 0.2414 |
| RSRM-3B | 0.1529 | 89.90 | NA Doc | NA | 0.2408 |
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# TABLE 3.4 <br> PREDICTED PROPELLANT <br> <br> TEMPERATURE GRADIENTS IN RSRM-3 

 <br> <br> TEMPERATURE GRADIENTS IN RSRM-3}

| WEB DIST(1) | DEGREE LOCATIONS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 45 | 90 | 135 | 180 | 225 | 270 | 315 |
| 2.63 | 66.7 | 57.5 | 56.3 | 56.5 | 56.5 | 56.8 | 66.5 | 71.5 |
| 7.88 | 64.1 | 59.0 | 57.9 | 58.0 | 58.0 | 58.5 | 63.9 | 67.5 |
| 14.19 | 65.1 | 60.5 | 59.2 | 59.2 | 59.2 | 60.1 | 64.9 | 68.1 |
| 21.56 | 65.7 | 61.8 | 60.5 | 60.4 | 60.5 | 61.5 | 65.6 | 68.2 |
| 28.94 | 66.2 | 62.8 | 61.4 | 61.2 | 61.4 | 62.5 | 66.0 | 68.3 |
| 36.31 | 66.4 | 63.3 | 61.9 | 61.7 | 61.9 | 63.0 | 66.2 | 68.2 |

(1) MEASURED FROM CASE WALL TOWARD CENTER OF SEGMENT (INCHES)

### 3.3.3 RSRM-3 Pressure Distribution

Tables 3.5 and 3.6 show RSRM-3 reconstructed pressure distribution during ignition and steady state at a Propellant Mean Bulk Temperature (PMBT) of 62 degrees F. Figure 3.10 shows the location points referenced in the pressure distribution tables. The pressure distribution was reconstructed theoretically, since, no internal pressures are measured other than headend pressure. The pressures were reconstructed using Caveny-Kuo ignition transient program, SCBO4 steady state 1-D mass addition, and SCA08 SRM modeling program.
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NOZZLE
STAGNATION
PRESSURE





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TABLE 3.5 (CONTINUED)
RSRM-3A MOTOR PRESSURE DISTRIBUTION SUMMARY AT 60 DEGREES F
















 MRNTNRNNRNNO



 NT













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IME
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 HEADEND PRESSURE

NOZZLE
STAGNATION
PRESSURE
185.6
169.4
153.9
140.0
128.0
117.2
106.2
94.4
82.7
72.5
64.3

| HEADEND PRESSURE <br> (489.9) | 530.0 | 689.3 | 851.2 | 1012.1 | 1171.2 | 1332.1 | 1491.2 | 1511.0 | 1577.5 | 1697.5 | 1816.7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 186.5 | 186.5 | 186.5 | 186.3 | 185.9 | 185.8 | 185.0 | 184.7 | 184.7 | 184.7 | 184.7 | 184.7 |
| 170.2 | 170.2 | 170.2 | 170.1 | 169.6 | 169.6 | 168.8 | 168.6 | 168.6 | 168.6 | 168.6 | 168.6 |
| 154.6 | 154.6 | 154.6 | 154.5 | 154.1 | 154.1 | 153.3 | 153.2 | 153.2 | 153.2 | 153.2 | 153.2 |
| 140.7 | 140.7 | 140.7 | 140.6 | 140.2 | 140.2 | 139.5 | 139.4 | 139.4 | 139.4 | 139.4 | 139.4 |
| 128.6 | 128.6 | 128.6 | 128.5 | 128. 2 | 128.2 | 127.5 | 127.4 | 127.4 | 127.4 | 127.4 | 127.4 |
| 117.8 | 117.8 | 117.8 | 117.7 | 117.3 | 117.3 | 116.6 | 116.7 | 116.7 | 116.7 | 116.7 | 116.7 |
| 106.7 | 106.7 | 106.7 | 106.6 | 106.3 | 106.3 | 105.7 | 105.7 | 105.7 | 105.7 | 105.7 | 105.7 |
| 94.8 | 94.8 | 94.8 | 94.7 | 94.5 | 94.5 | 93.9 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 |
| 83.1 | 83.1 | 83.1 | 83.0 | 82.8 | 82.8 | 82.3 | 82. 3 | 82. 3 | 82.3 | 82. 3 | 82. 3 |
| 72.8 | 72.8 | 72.8 | 72.7 | 72.5 | 72.5 | 72.1 | 72.1 | 72. 1 | 72.1 | 72.1 | 72.1 |
| 64.6 | 64.6 | 64.6 | 64.5 | 64.3 | 64.3 | 64.0 | 64.0 | 64.0 | 64.0 | 64.0 | 64.0 |

























































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$$
\begin{gathered}
\text { NOZZLE } \\
\text { STAGNATION } \\
\text { PRESSURE } \\
187.3 \\
171.9 \\
155.7 \\
139.9 \\
126.0 \\
114.2 \\
103.6 \\
93.5 \\
83.9 \\
75.3 \\
67.9
\end{gathered}
$$
\]

### 3.3.4 RSRM-3 Pressure Oscillations

Both boosters used on STS-29 were instrumented with a special channel for measuring chamber pressure oscillations. The measurement was accomplished by electrically A-C coupling the data acquired from the OPTs. This gage is identical to the POO1 gage used in static test, and in fact is very similar to the A-C coupled gage used on static test motors, P016. The P016 gage is also an A-C coupled mean pressure gage, is the same make as the OPTs, uses the same operating principles as the OPT, and externally appears identical to the OPTs. Though they are not exactly the same gage, they are extremely similar. Bit resolution and sample rate were adequate for measuring the low level 1-L and 2-L mode pressure oscillations anticipated in the combustion chambers of the boosters. The measurement system used on STS-29 should be comparable to that used during static testing.

Data acquired from the A-C coupled OPTs are displayed in a waterfall plot format in Figures 3.11 (left booster) and 3.12 (right booster). The first longitudinal (1-L) and second longitudinal (2-L) acoustic modes of the combustion cavity can be observed at about 15 and 30 Hz , respectively. Maximum oscillation amplitudes for the left motor were 0.31 psi 0-to-peak at 15.5 Hz and 86 seconds (1-L mode) and 0.44 psi at 28 Hz and 89 seconds (2-L mode). The right motor experienced a maximum 1-L mode amplitude of 0.38 psi 0 -to-peak at 15.5 Hz and 85 seconds. The maximum 2-L mode amplitude for the right motor was 0.54 psi 0-to-peak at 29.5 Hz and 83 seconds. Figures 3.13 through 3.16 describe running, instantaneous, peak-to-peak oscillations amplitudes in the 1-L and 2-L modes for the left and right motors, respectively, during the last half of operation. This type of analysis is more representative of instantaneous oscillations than are the time averaged oscillations presented in a waterfall plot. Figure 3.13 shows maximum peak-to-peak 1-L mode oscillations of 1.26 psi for the left motor. The corresponding number for the right motor is 1.24 psi.

Several observations about the two STS-29 solid rocket boosters can be made:

Both motors have strikingly similar acoustic signatures.
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The STS-29 waterfall plots are very similar to those from STS-27 and STS-26, though $2-L$ mode activity is somewhat less.

The general appearance of the STS 29 waterfall plots more closely resembles HPM behavior than recent $\bar{R} S R M$ static test behavior.

Oscillation amplitudes for RSRM flight motors continue to be significantly lower than for RSRM static test motors.

When using waterfall plots to compare oscillation amplitudes, it is important to remember that this format uses an averaging method of analysis. This presents no difficulty for steady state signals but has an attenuating effect on transient signals. Since most of the data obtained from a solid rocket motor are transient, any oscillation magnitudes referred to as maxima are, in fact, not true but averaged values over a given time slice. These numbers are, nonetheless, very useful for comparison. Table 3.7 shows such a comparison for the STS-29, STS-27, STS-26 motors and recent static test motors. DM-6 and DM-7 were Filament Wound Case (FWC) motors.

In conclusion, both STS-29 motors exhibited chamber pressure oscillations similar to previous RSRM flight motors and previous HPM designs. The high amplitude $1-\mathrm{L}$ mode oscillations experienced late in operation in the RSRM static test motors was not present in any of the 6 RSRM flight motors used to date.

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TABLE 3.7
Maximum Pressure Oscillation Amplitude Comparison

| Motor | Source of Measurement | Mode | Time of Measurement | Frequency ( Hz ) | Max Pressure (psi 0-to-peak) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { STS-29 } \\ & \text { (left) } \end{aligned}$ | Waterfall | 1-L | 86 | 15.5 | $\frac{0.31}{}$ |
|  |  | 2-L | 89 | 28.0 | 0.44 |
| STS-29 Waterfall <br> (right) AC OPT |  | 1-L | 85 | 15.5 | 0.38 |
|  |  | 2-L | 83 | 29.5 | 0.54 |
| TEM-02 | Waterfall | 1-L | 78 | 16.0 | 0.40 |
|  |  | 2-L | 100 | 29.5 | 0.59 |


| QM-8 Waterfall | 1-L | 104 | 14.5 | 1.11 |
| :--- | :--- | :--- | :--- | :--- |
|  | 2-L | 55 | 27.5 | 0.45 |
| TEM-01 Waterfall | 1-L | 79 | 15.5 | 0.53 |
|  | 2-L | 95 | 29.5 | 1.07 |

STS-27 Waterfall 1-L 82 (left) AC OPT

2-L 82
15.5
0.37
29.5
0.60

STS-27 Waterfall
1-L 82 (right) AC OPT

2-L
83
STS-26 Waterfall 1-L 79 (left) AC OPT

2-L
95
15.5
0.57

|  | 2-L | 95 |
| :--- | :--- | :--- |
| STS-26 Waterfall <br> (right) AC 0PT | 1-L | 83 |
|  |  | 94 |

29.5
0.72
16.0
0.70
29.5
0.87 (right) AC OPT

2-L
94
15.0
0.54
30.0
0.47

PVM-1 Waterfall
1-L
99
14.5
1.76

2-L
79
29.5
1.05
QM-7 Waterfall 1-L 93
14.5
1.40

2-L 79
29.5
0.95

QM-6 Waterfall
1-L 107
2-L 83
14.5
1.50
29.5
0.65
$\qquad$


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| Source <br> Motor | of Measurement | Mode | Time of Measurement | Frequency ( Hz ) | Max Pressure (psi 0-to-peak) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DM-9 | Waterfall | 1-L | 107 | 14.5 | 1.15 |
|  |  | 2-L | 96 | 30.0 | 0.88 |
| DM-8 | Waterfall | 1-L | 78 | 16.0 | 0.83 |
|  |  | 2-L | 97 | 29.5 | 0.85 |
| ETM-1A | Waterfall | 1-L | 83 | 15.5 | 0.47 |
|  |  | 2-L | 100 | 29.5 | 0.55 |
| DM-7 | Waterfall | 1-L | 77 | 15.5 | 1.29 |
|  |  | 2-L | 93, 96 | 29.5 | 0.86 |
| DM-6 | Waterfall | 1-L | 76 | 15.5 | 0.51 |
|  |  | 2-L | 86 | 29 | 0.78 |
| QM-4 | Waterfall | 1-L | 93 | 14 | 0.41 |
|  |  | 2-L | 83 | 29 | 0.35 |

### 3.4 CEI SPECIFICATION PERFORMANCE REQUIREMENTS

### 3.4.1 Performance Tolerances

The parameter variations of the total population of RSRMs about a nominal value are constrained by the requirements defined in the CEI Specification paragraph 3.2.1.1.2.2, Table II. A comparison of the RSRM-3A and RSRM-3B calculated and reconstructed parameters at PMBT of $60^{\circ} \mathrm{F}$ with respect to the nominal values and the CEI Specification maximum 3 sigma requirements is shown on the following two tables.
$\qquad$

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TABLE 3.8
COMPARISON OF RSRM-3A VARIATIONS
AT PMBT $=60^{\circ} \mathrm{F}$ ABOUT THE NOMINAL TO THE
CEI SPECIFICATION REQUIREMENTS
CEI
MAX 3 SIGMA NOMINAL RSRM-3A RSRM-3A
PARAMETER
(1)

|  |  |  |  |  |
| :--- | :--- | :--- | :--- | ---: |
| WEB TIME | $\pm 5.0$ | 111.7 | 111.4 | -0.27 |
| ACTION TIME | $\pm 6.5$ | 123.4 | 124.1 | 0.57 |
| WEB TIME AVG PRESSURE | $\pm 5.3$ | 660.8 | 659.8 | -0.15 |
| MAX PRESSURE | $\pm 6.5$ | 918.4 | 895.0 | -2.55 |
| MAX SEA LEVEL THRUST | $\pm 6.2$ | 3.06 | 3.04 | -0.65 |
| WEB TIME AVG VAC THRUST | $\pm 5.3$ | 2.59 | 2.58 | -0.39 |
| VAC DEL SPECIFIC IMPULSE | $\pm 0.7$ | 267.1 | 267.5 | 0.15 |
| WEB TIME VAC TOTAL IMPULSE | $\pm 1.0$ | 288.9 | 287.8 | -0.0 |
| ACTION TIME TOTAL IMPULSE | $\pm 1.0$ | 296.3 | 295.4 | -0.0 |
|  |  |  |  |  |

PRESSURE VALUES IN PSIA, THRUST VALUES IN MLBF, IMPULSE VALUES IN MLBF-SEC
(1) CEI PARAGRAPH 3.2.1.1.2.2, TABLE II
(2) QM-4 STATIC TEST AND SRM-8A AND B, SRM-9A, SRM-10A, SRM-10B, SRM-11A, SRM-13A AND SRM-13B FLIGHT AVERAGE AT STANDARD CONDITIONS.
(3) RSRM-3A AT PMBT $=60^{\circ} \mathrm{F}$
(4) DELTA $=(($ RSRM $-3 A-$ NOMINAL $) /$ NOMINAL $) * 100$
$\qquad$

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| TABLE 3.9 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| COMPARISON OF RSRM-3B VARIATIONS <br> AT PMBT $=60^{\circ} \mathrm{F}$ ABOUT THE NOMINAL TO THE CEI SPECIFICATION REOUIREMENTS |  |  |  |  |
| PARAMETER |  | nominal <br> VALUE(2) | $\begin{aligned} & \text { RSRM-3B } \\ & \text { VALUE (3) } \end{aligned}$ | $\begin{aligned} & \text { RSRM-3B } \\ & \text { DELTA\% (4) } \end{aligned}$ |
| VEB TIME | $\pm 5.0$ | 111.7 | 111.4 | -0.27 |
| ACTION TIME | $\pm 6.5$ | 123.4 | 123.8 | 0.32 |
| WEB TIME AVG PRESSURE | $\pm 5.3$ | 660.8 | 660.8 | 0.00 |
| MaX PRESSURE | $\pm 6.5$ | 918.4 | 890.0 | -3.09 |
| MaX SEA LEVEL THRUST | $\pm 6.2$ | 3.06 | 3.05 | -0.33 |
| WEB TIME AVG VAC THRUST | $\pm 5.3$ | 2.59 | 2.59 | 0.00 |
| VAC DEL SPECIFIC IMPULSE | $\pm 0.7$ | 267.1 | 267.8 | 0.26 |
| WEB TIME VAC TOTAL IMPULSE | $\pm 1.0$ | 288.9 | 288.2 | -0.24 |
| ACTION TIME TOTAL IMPULSE | $\pm 1.0$ | 296.3 | 295.9 | -0.13 | IMPULSE VALUES IN MLBF-SEC

(1) CEI PARAGRAPH 3.2.1.1.1, TABLE II
(2) OM-4 STATIC TEST AND SRM-8A AND B, SRM-9A, SRM-10A, SRM-10B, SRM-11A, SRM-13A AND SRM-13B FLIGHT AVERAGE AT STANDARD CONDITIONS.
(3) $\quad$ RSRM-3B AT PMBT $=60 \mathrm{~F}$
(4) DELTA $=(($ RSRM $-3 B-$ NOMINAL $) /$ NOMINAL $) * 100$

### 3.4.2 RSRM Nominal Thrust-Time Performance

The nominal RSRM-HPM performance is defined as the average performance of the HPM and RSRM static test and flight motor series at standard conditions. The standard conditions consist of the propellant burn rate of $0.368 \mathrm{in} / \mathrm{sec}$ at 625 psia and a PMBT of $60^{\circ} \mathrm{F}$. The flight motor reconstructed thrust-time traces are normalized to standard conditions and averaged with past flight and static test data at standard conditions to form the RSRM-HPM population nominal thrust-time trace. This nominal RSRM-HPM performance will be continually updated during the
$\qquad$

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Shuttle program. It is the current estimate of the total population nominal. The nominal performance for the thrust time trace and impulse gate requirements is based on the performance of $0 M-4$, SRM-8A, SRM-8B, SRM-9A, SRM-10A, SRM-10B, SRM-11B through SRM-19B, SRM-24A, SRM-24B, ETM-1A, DM-8, DM-9, QM-6, QM-7, PVM-1, RSRM-1, RSRM-2, and RSRM-3. The delivered RSRM-HPM population nominal performance is compared to the CEI Specification paragraph 3.2.1.1.2.1, Table I requirements on Figure 3.17. 3.4.3 Impulse at Standard Conditions VS Requirement Gates

The vacuum impulse at standard conditions at each of the gates is compared to the CEI Specification paragraph 3.2.1.1.2.4 requirements on the following table. The population making up the standard nominal for the impulse requirements are the same as those in the nominal thrust time trace (Figure 3.17).

| TABLE 3.10 |  |  |
| :---: | :---: | :---: |
| RSRM-HPM POPULATION IMPULSE GATES |  |  |
| IMPULSE | REQUIREMENT <br> (1) | STANDARD NOMINAL (2) |
| Impulse at 20 sec (10**6 LBF-SEC) | 63.1 (MIN) | 64.5 |
| Impulse at 60 sec (10**6 LBF-SEC) | $\begin{array}{rl} 172.9 & 178.1(+3 \%) \\ & 171.2(-1 \%) \end{array}$ | 172.5 |
| Impulse at ACTION TIME ( $10 * * 6$ LBF-SEC) | 293.8 (MIN) | 296.3 |

(1) CEI PARAGRAPH 3.2.1.1.2.4
(2) NORMALIZED TO STANDARD CONDITIONS-BURN RATE OF 0.368 IN/SEC. POPULATION IS SAME AS USED TO COMPARE NOMINAL THRUST TRACE, Figure 3.17 .

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### 3.4.4 Matched Pair Thrust Differential

The maximum thrust imbalance assessment is shown on the following table. Figure 3.18 through Figure 3.21 shows the thrust differential during ignition, steady state, and tailoff. All the thrust differential values were near the nominal values experienced by previous flight SRMs and were well within the CEI Specification paragraph 3.2.1.1.2.3, Table III limits. The thrust values used for the assessment were reconstructed at the delivered conditions of each motor.

TABLE 3.11
RSRM-3 THRUST IMBALANCE SUMMARY
SPEC IMBALANCE TIME

|  | SPEC | IMBALANCE | TIME |
| :--- | :--- | :--- | :--- |
| IGNITION (0 SEC TO 1.0 SEC, LBF) | 300 K | -88.8 K | 0.094 |
| STEADY STATE ( 1.0 SEC TO FIRST | 85 K | -39.0 K | 90.0 |
| WEB TIME MINUS 4.5 SEC, LBF) |  |  |  |
| TRANSITION (FIRST WEB TIME $85 \mathrm{~K}-268 \mathrm{~K}$ | +30.8 K | 111.0 |  |
| MINUS 4.5 SEC TO FIRST WEB <br> TIME, LBF) | linear |  |  |
| TAILOFF (FIRST WEB TIME TO LAST <br> ACTION TIME, LBF) | 710K | +46.1 K | 112.0 |

```
IMBALANCE = LEFT SRM - RIGHT SRM
```


### 3.4.5 Matched Pair Performance Requirements

The CEI Specification requires that the performance of a matched pair of motors on a flight set have similar performance according to table 3.12. The RSRMs for STS-27 were well within the matched pair specification requirements.

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TABLE 3.12
MATCHED PAIR PERFORMANCE LIMITS

CEI SPECIFICATION DELIVERED
PARAMETER

## VEB TIME

ACTION TIME
WEB TIME AVG PRESSURE
MAX PRESSURE
MAX SEA LEVEL THRUST
WEB TIME AVG VAC THRUST
VAC DEL SPECIFIC IMPULSE
WEB TIME VAC TOTAL IMPULSE
ACTION TIME TOTAL IMPULSE

MAX DIFFERENCE(\%)(1) \% DIFFERENCE(2)

PRESSURE VALUES IN PSIA, THRUST VALUES IN MLBF, ImpULSE VALUES IN MLBF-SEC
(1) CEI SPECIFICATION PARAGRAPH 3.2.1.1.2.2, TABLE II
(2) DIFFERENCE $=(($ RSRM $-3 B-$ RSRM 3 A $) /$ RSRM -3 AVERAGE $) * 100$ DATA AT PMBT OF 60 DEG F

### 3.4.6 Ignition Characteristics

The ignition characteristics of both motors are shown in Table 3.13 compared with the limits from CEI Specification paragraphs 3.2.1.1.1.1 and 3.2.1.1.1.2. All the values were well within the limits.

TABLE 3.13
RSRM-3 Ignition Characteristics

| Parameter | CEI Requirement | RSRM-3A | RSRM-3B |
| :--- | :--- | :--- | :--- |
| Ignition Interval | $202-262 \mathrm{~ms}$ | 241 ms | 241 ms |
| Pressure Rise Rate | $115.9 \mathrm{psi} / 10 \mathrm{~ms}$ | 82.7 | 89.9 |

$\qquad$

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### 3.5 RECONSTRUCTED MASS PROPERTIES

The Morton Thiokol manufacturing designation, 360L003, along with STS-29 have been used, by Mass Properties, to identify the RSRMs used on this flight. The left and right hand RSRMs for the flight will be designated as $A$ and $B$.

Tables 3.14 and 3.15 provide $S T S-29 A$ and STS-29B reconstructed sequential mass properties, respectively.

Table 3.16 and 3.17 compares RSRML predicted sequential weight and center of gravity (cg) data against post flight reconstructed data. A $1,518 \mathrm{lbm}$ slag weight was used for both prefire and postfire sequential predictions. Actual STS-29 mass properties may be obtained from Mass Properties History Log Space Shuttle 360L003-LH (TWR-17338), dated 25 October 1988, and 360L003-RH (TWR-17339), dated 25 0ctober 1988. Post flight reconstructed data reflects Ballistics mass flow data from the 320 sample per second measured pressure traces. Tables 3.18 and 3.19 present CEI requirements, predicted, and actual weight comparisons. The actual weights are in close agreement with predicted values. Mass Properties data for both RSRMs comply with CEI requirements.
$\qquad$
TABLE 3.14
SEQUENTIAL MASS PROPERTIES

| EVENTS/TIMES | WEIGHT (LBS) | CENTER LONG. | OF GRAVITY LAT. VERT. |  | ITCH MOMENT OFINERTIA ${ }^{\text {ROLL }}$ YAW |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PRE-LAUNCH | 1255040.6 | 1171.588 | 0.072 | 0.008 | 42391.866 | 878.095 | 42392.895 |
| LIFT-OFF ${ }_{\text {TIME }}=0.00$ | 1254345.7 | 1171.724 | 0.072 | 0.008 | 42348.459 | 876.758 | 42349.488 |
| TIME $=0.24$ INTERMEDIATE BURN | 1016525.6 | 1207.942 | 0.089 | 0.010 | 30830.782 | 761.675 | 30831.809 |
| TIME = 20.00 |  |  |  |  |  |  |  |
| INTERMEDIATE BURN | 796537.3 | 1231.709 | 0.112 | 0.013 | 21792.256 | 627.629 | 21793.278 |
| MAX "Q"ME $=40.00$ | 666485.7 | 1229.527 | 0.134 | 0.015 | 18079.433 | 550.529 | 18080.447 |
| TIME $=54.00$ <br> INTERMEDIATE BURN | 611980.3 | 12R7.097 | 0.145 | 0.017 | 16688.611 | 515.470 | 16689.622 |
| TIME $=660.00$ INTERMEDIATE BURN |  |  |  |  | 12011.826 | 381.793 | 12012.826 |
| INTERMEDIATE BURN | 420936.3 | 1215.124 | 0.209 | 0.024 | 12011.826 | 381.793 | 12012.826 |
| MAX "G" | 356591.9 | 1213.719 | 0.247 | 0.029 | 10609.358 | 331.180 | 10610.352 |
| TIME $=88.00$ | 251397.2 | 1225.183 | 0.348 | 0.041 | 8605.563 | 242.987 | 8606.549 |
| WEB TURN ${ }_{\text {THE }}=100.00$ | 174250.5 | 1266.459 | 0.499 | 0.059 | 7272.103 | 173.124 | 7273.080 |
| $\text { TIME }=111.44$ |  |  |  |  |  |  |  |
| end of action time $\text { TIME }=124.08$ | 144582.6 | 1313.361 | 0.600 | 0.071 | 6568.299 | 146.845 | 6569.271 |
| SEPARAIION. | 144008.7 | 1314.840 | 0.603 | 0.070 | 6542.600 | 146.436 | 6543.575 |
| TIME $=125.83$ <br> NOZZLE JETTISONED | 141429.0 | 1305.149 | 0.604 | 0.070 | 6323.230 | 141.664 | 6324.185 |
| TIME $=195.83$ |  |  |  |  |  |  |  |
| max reentry "q" | 141211.1 | 1305.045 | 0.605 | 0.070 | 6311.820 | 141.471 | 6312.776 |
| NOSE TIME P = ${ }_{\text {P PLOYMENT }}$ | 141158.8 | 1305.022 | 0.605 | 0.070 | 6309.031 | 141.425 | 6309.987 |
| DROGUE CHE $=350.83$ | 141157.8 | 1305.022 | 0.605 | 0.070 | 6308.976 | 141.424 | 6309.931 |
| $\text { TIME }=351.43$ | 11787.8 | 1305.022 | 0.605 | 0.070 |  |  |  |
| frustum release | 141121.0 | 1305.006 | 0.605 | 0.070 | 6307.001 | 141.391 | 6307.957 |
| TIIME $=372.53$ | 141118.7 | 1305.005 | 0.605 | 0.070 | 6306.880 | 141.389 | 6307.835 |
| $\text { TMME }=373.83$ |  |  |  |  |  |  |  |
| MAIN CHUTE 1ST DISREEFING | 141101.1 | 1304.998 | 0.605 | 0.070 | 6305.930 | 141.374 | 6306.885 |
| MAIN CHUTE $=383.93$ DISREEFING | 141090.8 | 1304.994 | 0.605 | 0.070 | 6305.376 | 141.365 | 6306.331 |
| $\underset{\text { SPLASHDOWN }}{\text { TIME }}=389.83$ | 141046.6 | 1304.974 | 0.605 | 0.070 | 6302.947 | 141.326 | 6303.903 |
| TIME $=415.83$ |  |  |  |  |  |  |  | EVENTS/TIMES

TABLE 3.15
SEQUENTIAL MASS PROPERTIES
STS-29 RIGHT HAND

| EVENTS/TIMES | (LBS) | $\begin{aligned} & \text { CENTER } \\ & \text { LONG. } \end{aligned}$ | Of GRAVITY |  | MOMENT OFINERTIA |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PRE-LAUNCH <br> TIME $=0.00$ | 1255967.6 | 1171.614 | 0.072 | 0.007 | 42439.683 | 877.956 | 42440.705 |
| LIFT-OFF $=0.00$ | 1255262.7 | 1171.753 | 0.072 | 0.007 | 42395.714 | 876.621 | 42396.736 |
| INTERMEDIATE BURN | 1017869.0 | 1207.998 | 0.089 | 0.009 | 30903.479 | 761.890 | 30904.499 |
| INTERMEDIATE $\begin{array}{r}\text { 20.00 } \\ \text { BURN }\end{array}$ | 797566.8 | 1231.878 | 0.113 | 0.011 | 21854.650 | 627.715 | 21855.664 |
| $\text { Max "TIME }=40.00$ | 667488.4 | 1229.801 | 0.135 | 0.013 | 18140.952 | 550.484 | 18141.958 |
| TIME $=54.00$ |  |  |  |  |  |  |  |
| INTERMEDIATE BURN | 612997.9 | 1227.476 | 0.146 | 0.015 | 16756.976 | 515.980 | 16757.980 |
| INTERMEDIATE BURN | 421936.0 | 1215.855 | 0.211 | 0.021 | 12077.750 | 381.788 | 12078.742 |
| $\text { MAX "G"ME }=80.00$ | 357146.9 | 1214.734 | 0.249 | 0.025 | 10665. 221 | 330.832 | 10666. 209 |
| TIME $=87.00$ INTERMEDIATE BURN TIME $=100.00$ | 251180.6 | 1227.119 | 0.352 | 0.035 | 8644.564 | 241.953 | 8645.543 |
| WEB BURN | 174637.2 | 1267.562 | 0.503 | 0.051 | 7313.501 | 172.451 | 7314.471 |
| END OF ACTION TIME | 144862.4 | 1314.842 | 0.605 | 0.061 | 6591.180 | 146.265 | 6592.145 |
| TIME SEPARATION | $144235.5^{\circ}$ | 1316.690 | 0.608 | 0.061 | 6559.568 | 145.837 | 6560.535 |
| TIME $=125.83$ |  |  |  |  |  |  |  |
| NOZZLE JETTISONED | 141679.1 | 1306.972 | 0.609 | 0.061 | 6373.431 | 141.125 | 6374.385 |
|  | 141461.2 | 1306.870 | 0.610 | 0.061 | 6362.032 | 140.932 | 6362.987 |
| MAX TIME $=320.83$ |  |  |  |  |  |  |  |
| NOSE CAP DEPLOYNENT | 141408.9 | 1306.848 | 0.610 | 0.061 | 6359.244 | 140.886 | 6360.199 |
| TIME $=350.83$ | 141407.9 | 1306.847 | 0.610 | 0.061 | 6359.190 | 140.885 | 6360.143 |
| TIME $=351.43$ |  |  |  |  |  |  |  |
| FRUSTUM RELEASE | 141371.1 | 1306.832 | 0.610 | 0.060 | 6357.216 | 140.852 | 6358.171 |
| TIHE $=372.53$ MAIN CHUTE LINE STRETCH | 141368.9 | 1306.831 | 0.610 | 0.060 | 6357.095 | 140.850 | 6358.049 |
| TIME $=373.83$ |  |  |  |  |  |  |  |
| MAIN CIIUTE 1ST DISREEFING | 141351.2 | 1306.824 | 0.610 | 0.060 | 6356.145 | 140.835 | 6357.100 |
| MAIN TIHUE $=383.93$ 2ND DISREEFING | 141341.0 | 1306.820 | 0.610 | 0.060 | 6355.592 | 140.826 | 6356.547 |
| TIME $=389.83$ |  |  |  |  |  |  |  |
| SPLASHDOWN | 141296.7 | 1306.801 | 0.610 | 0.060 | 6353.165 | 140.787 | 6354.120 |

$$
\begin{aligned}
& \text { Event } \\
& \text { Pre-Ignition } \\
& \text { Liftoff } \\
& \text { Action Time } \\
& \text { Separation }{ }^{2} \\
& \text { Nozzle Jettison } \\
& \text { Nose Cap Deployment } \\
& \text { Drogue Chute Deployment } \\
& \text { Main Chute Line Stretch } \\
& \text { Main Chute 1st Disreefing } \\
& \text { Main Chute 2nd Disreefing } \\
& \text { Splash Down }
\end{aligned}
$$

TABLE 3.16
SEDUENITAL MASS PROPERTIES PREDICLED/ACIUAL COMPARISONS
STS-29 left Aand

| Weight (b) |  |  |  | Longitudinal $\sigma_{\text {( }}(\mathrm{in})$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Predicted ${ }^{1}$ | Actual | Delta | \% Error | Predicted ${ }^{1}$ | Actual | Delta | \% Error |
| 1,255,041 | 1,255,041 | 0 | 0.00 | 1,171.588 | 1,171.588 | 0.000 | 0.00 |
| 1,254,412 | 1,254,346 | -66 | 0.01 | 1,171.715 | 1,171.724 | +0.009 | 0.00 |
| 144,707 | 144,583 | -124 | 0.09 | 1,312.994 | 1,313.361 | +0.367 | 0.03 |
| 143,974 | 144,009 | +35 | 0.02 | 1,314.957 | 1,314.840 | -0.117 | 0.01 |
| 141,420 | 141,429 | $1+9$ | 0.01 | 1,305.146 | 1,305.149 | +0.003 | 0.00 |
| 141,161 | 141,159 | -2 | 0.00 | 1,305.022 | 1,305.022 | 0.000 | 0.00 |
| 141,146 | 141,158 | +12 | 0.01 | 1,305.015 | 1,305.022 | +0.007 | 0.00 |
| 141,119 | 141,119 | 0 | 0.00 | 1,305.004 | 1,305.005 | +0.001 | 0.00 |
| 141,107 | 141,101 | -6 | 0.00 | 1,304.999 | 1,304.998 | -0.001 | 0.00 |
| 141,100 | 141,091 | -9 | 0.01 | 1,304.996 | 1,304.994 | -0.002 | 0.00 |
| 141,047 | 141,047 | 0 | 0.00 | 1,304.974 | 1,304.974 | 0.000 | 0.00 |

[^1] Event
Pre-Ignition
Liftoff
Action Time
Separation 2
Nozzle Jettison
Nose Cap Deployment
Drogue Chute Deployment
Main Chute Line Stretch
Main Chute 1st Disreefing
Main Chute 2nd Disreefing
Splash Down

RREDICTED/ACTUAL VEIGAT (lb) COMPARISONS
SIS-29 LEFT RAND

| Iten | Minimum | Maximum | Predicted ${ }^{3}$ | Actual | Delta | \% Error | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inerts |  |  |  |  |  |  |  |
| Prefire, Controlled |  | 150,076 | 148,968 | 148,968 | 0 | 0.00 | 1 |
| Propellant | 1,104,714 |  | 1,104,894 | 1,104,894 | 0 | 0.00 | 1 |
| Usable |  |  | 1,104,037 | 1,104,157 | +120 | 0.01 | 2 |
| To Liftoff |  |  | 533 | 597 | $+64$ | 10.72 |  |
| Liftoff to Action |  |  | 1,103,504 | 1,103,560 | +56 | 0.01 | 2 |
| Unusable |  |  | 857 | 737 | -120 | 16.28 |  |
| Action to Separation |  |  | 667 | 508 | -159 | 31.30 |  |
| After Separation | - |  | 190 | 229 | +39 | 17.03 |  |
| Slag |  |  | 1,518 | 1,518 | 0 | 0.00 | 2 |

Notes:

1. Requirenent per CPVI-3600A, Addendum G, Part I, (RSRM CEI Specification).
2. Slag included in usable propellant, liftoff to action.
3. Based on 25 October 1988, Mass Properties History Log Space Shuttle 3601003-1H (TWR-17338).

PREDCIED/ACTIAL WETGHT (lb) COMPARISANS
STS-29 RIGEII BAND

| Iten | Miniman | Maxinum | Predicted ${ }^{3}$ | Actual | Delta | \% Error | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inerts |  |  |  |  |  |  |  |
| Prefire, Controlled |  | 150,076 | 149,231 | 149,231 | 0 | 0.00 | 1 |
| Propellent | 1,104,714 |  | 1,105,565 | 1,105,565 | 0 | 0.00 | 1 |
| Usable |  |  | 1,104,707 | 1,104,804 | +97 | 0.01 | 2 |
| To Liftoff |  |  | 534 | 607 | +73 | 12.03 |  |
| Liftoff to Action |  |  | 1,104,173 | 1,104,197 | +24 | 0.00 | 2 |
| Unusable |  |  | 858 | 761 | -97 | 12.75 |  |
| Action to Separation |  |  | 668 | 561 | -107 | 19.07 |  |
| After Separation | - | - | 190 | 200 | +10 | 5.00 |  |
| Slag |  |  | 1,518 | 1,518 | 0 | 0.00 | 2 |

Notes:

1. Requirement per CPMI-3600A, Addendum G, Part I, (RSRM CEI Specification).
2. Slag included in usable propellant, liftoff to action.
3. Based on 25 October 1988, Mass Properties History Log Space Stuttle 360003-RH (TWR-17339).

revision $\qquad$


Figure 2.1 RSRM- 3A AND 3B RECONSTRUCTED VACUUM THRUST-TIME TRACE

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Figure 3.3 RSRM-3A PREDICTED VS. MEASURED HEADEND PRESSURE

TWR-17542-10

Figure 3.4 RSRM-3B PREDICTED VS. MEASURED HEADEND PRESSURE


TVR-17542-10


TVR-17542-10




TWR-17542-10
-

Figure 3.10 RSRM Axial Station Lncation Summary



TIME (SEC)
TEST - STS-29 LEFT 80 P

## (d-d ISd) דצя


TIME (SEC)

tIME (SEC)

TEST —— STS-29 RHT 80 PT
ST•E $31 n 8 \mathrm{FA}$

TIME (SEC)


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Figure 3.19 RSRM-3 STEADY STATE THRUST IMBALANCE (INSTANTANEOUS)


[^0]:    JW11
    
    

[^1]:    Notes:

    1. Based on Mass Properties History Log Space Stuttle 3601003-LH, 25 October 1988 (TWR-17338).
    2. The separation longitudinal center of gravity of $1,314.840$ is $69 \%$ of the vehicle length.
