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NASA CASE NO. LAR-13,996-1SB

PRINT FIG. #1

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(NASA-Case-LAR-13996-1-SB) IGNITABILITY
TEST METHOD AND APPARATUS Patent Application
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63/25 0256833

AWARDS ABSTRACT

IGNITABILITY TEST METHOD AND APPARATUS

NASA CASE NO. LAR-13996-1-SB

This invention relates generally to measuring and testing, and more particularly, to a method and apparatus for testing ignitability.

As illustrated in the drawings, an ignition material holder 30 has a hemispherical cavity 34 which receives ignition material to be ignited by an initiator. Pressure generated by ignition is sensed by a transducer 64 and a pressure trace is generated which reveals the ignitability characteristics of the initiator.

The invention is useful for testing percussion primers and other initiators for their ability to ignite ignition materials.

Inventor: Laurence J. Bement

Home Address: 46 Ramshaw Lane
Newport News, VA 23602

Employer: SS # [REDACTED]
NASA-Langley Research Center

Inventor: James W. Bailey
Home Address: 504 Tidemill Road
Tabb, VA 23602

Employer: SS # [REDACTED]
PRC Kentron

Inventor: Morry L. Schimmel
Home Address: 8127 Amherst Avenue
St. Louis, MO 63130

Employer: SS # [REDACTED]
Schimmel Company, St. Louis, MO

Initial Evaluator: William W. Fernald

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FIG. 1

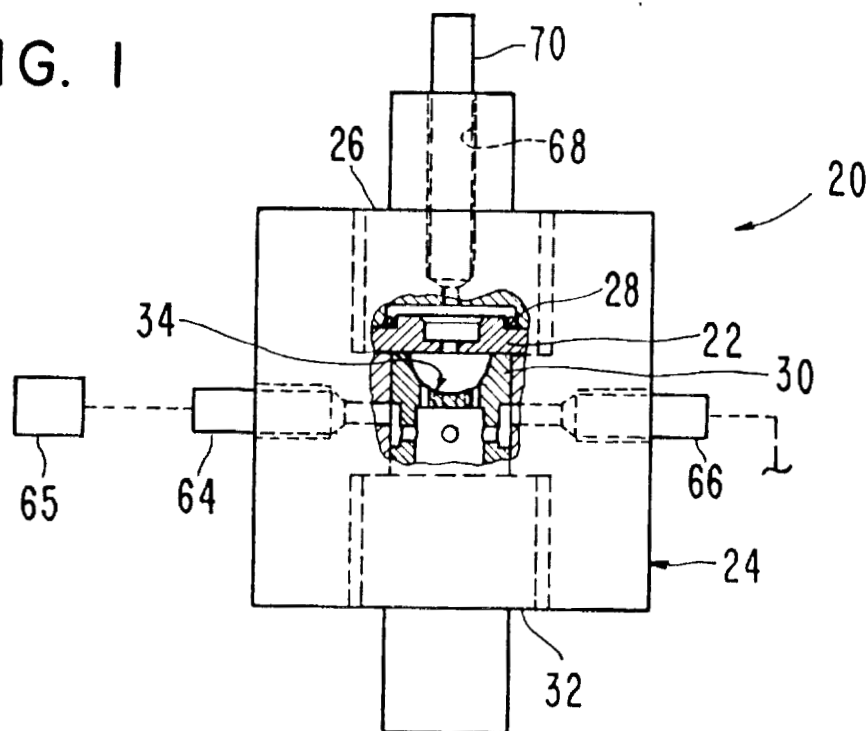


FIG. 2

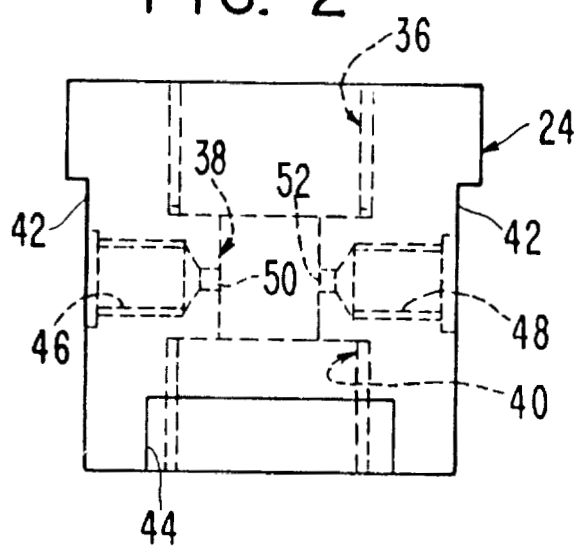


FIG. 3

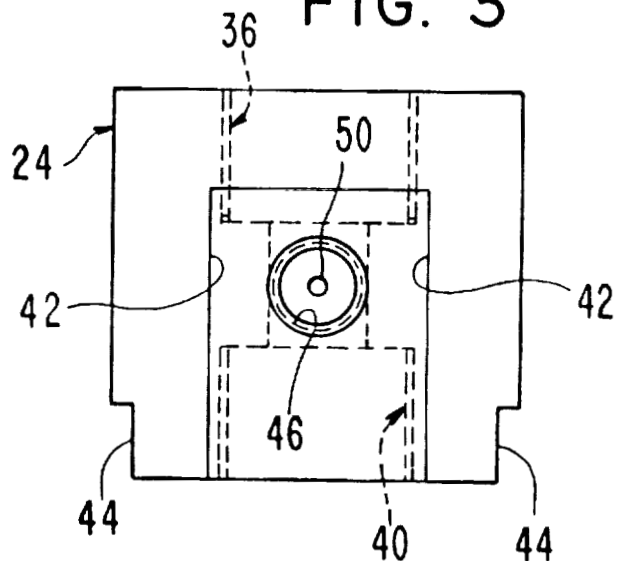


FIG. 4

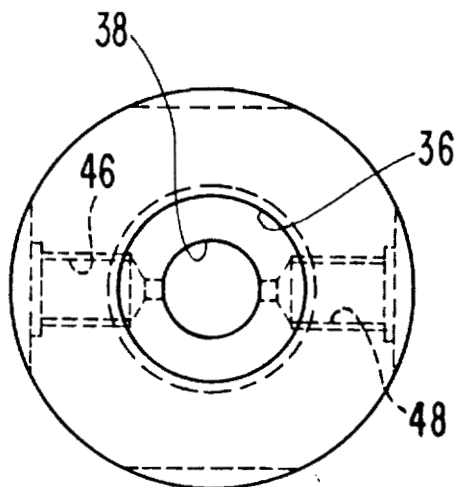


FIG. 6

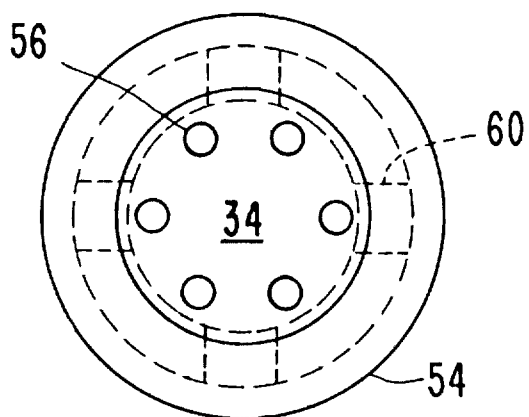


FIG. 5

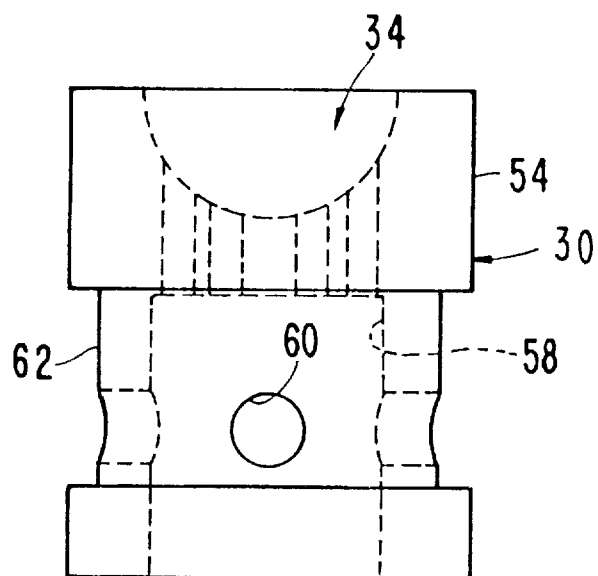


FIG. 7

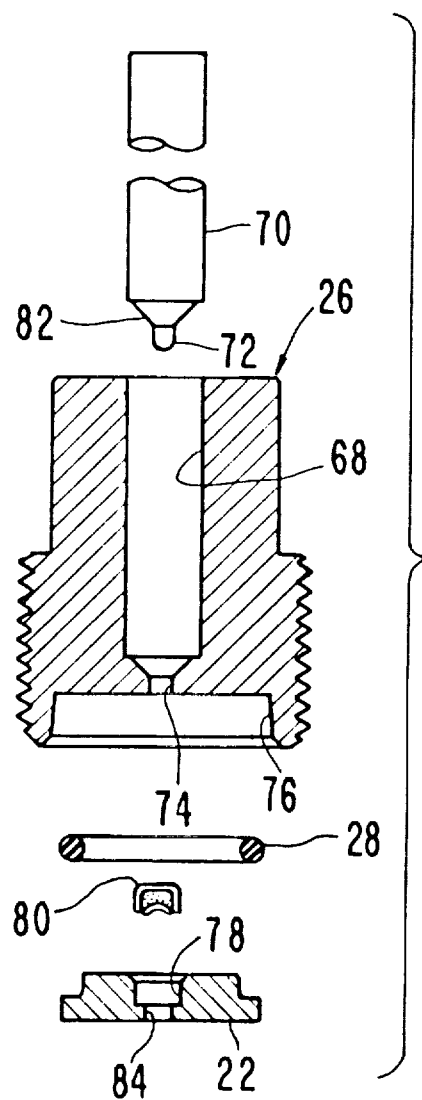


FIG. 8

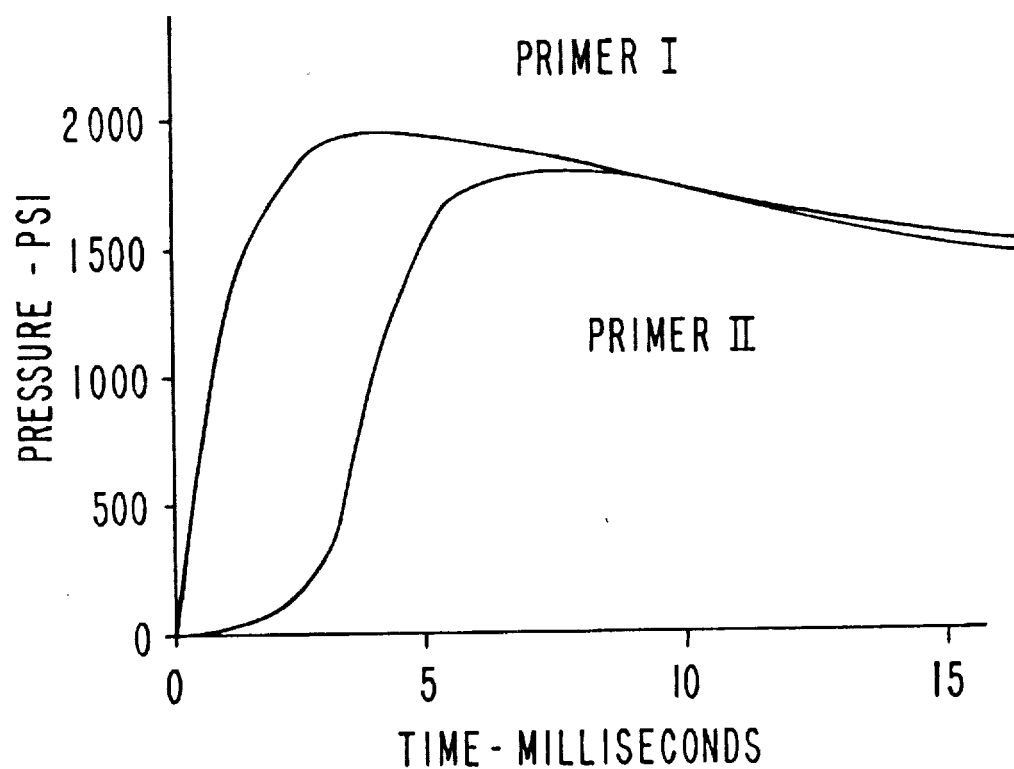


FIG. 9

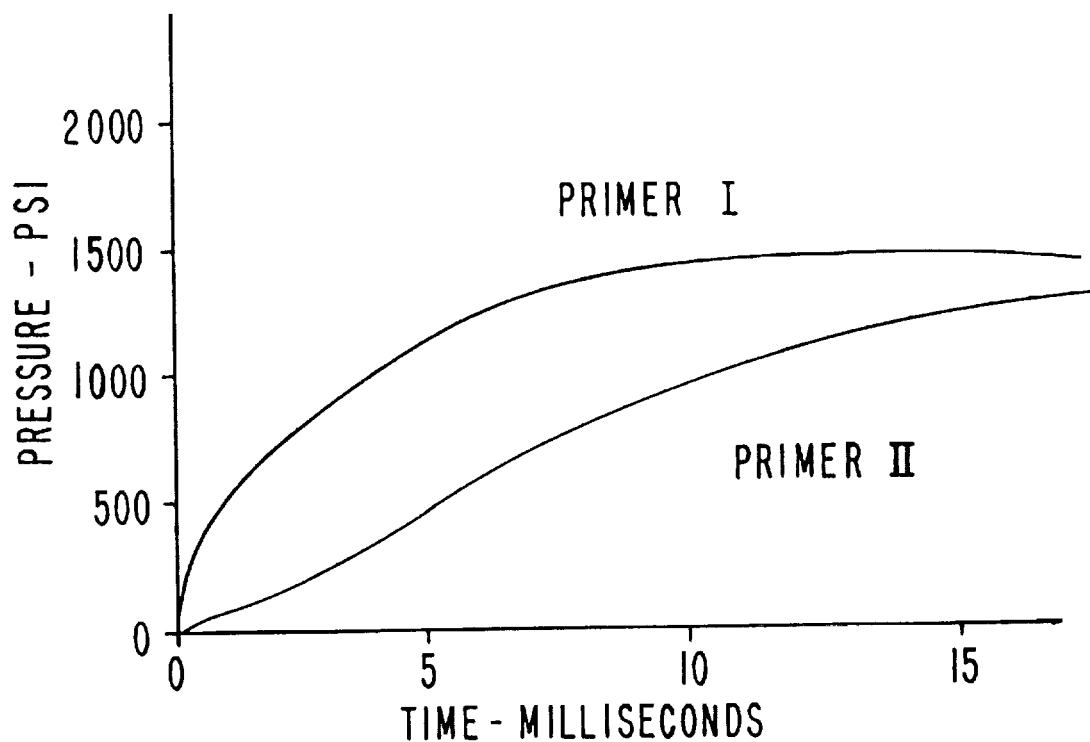


FIG. 10

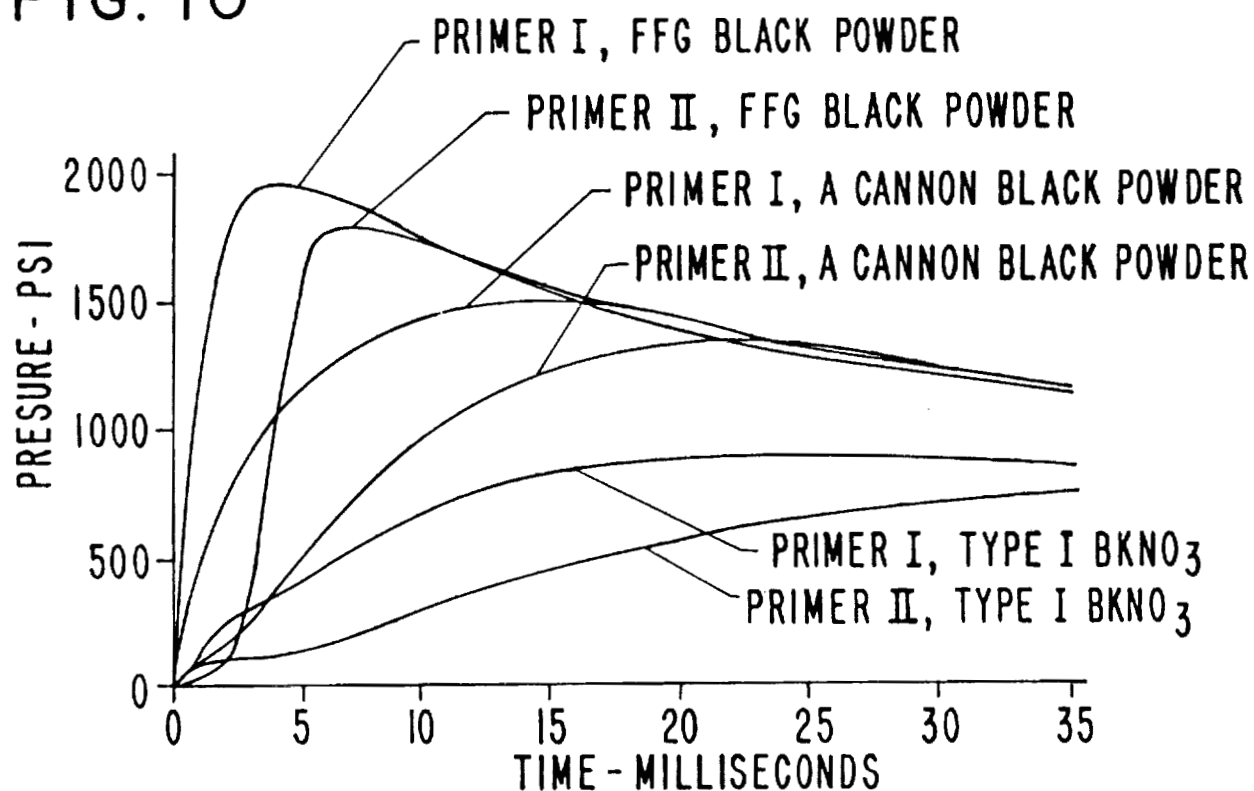
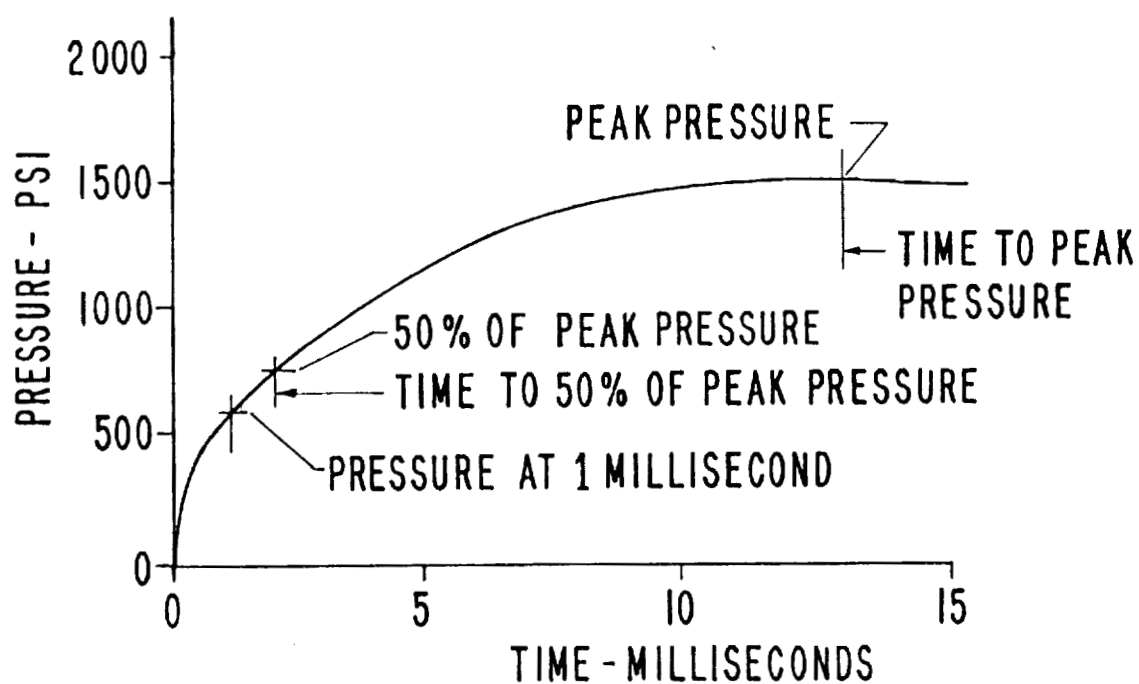


FIG. 11



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IGNITABILITY TEST METHOD AND APPARATUS

Origin of the Invention

The invention described herein was made in the performance of work under a NASA contract and is subject to the provisions of Section 305 of the National Aeronautics and Space Act of 1958, as amended,
5 Public Law 85-568 (72 Stat. 435; 42 USC 2457).

Background of the Invention

Field of the Invention

The present invention relates generally to the field of measuring and testing, and more specifically, to a test apparatus and method for
10 determining the ignition performance of ignition devices, i.e., devices that produce flame.

Description of the Related Art

Ignition of propellant materials used in rocket motors, or munitions, or even automobile air bags, all start with an igniter or initiator which can
15 be fired either electrically or mechanically. Percussion primers are one type of munitions application. Percussion primers are small brass cups, loaded with friction-sensitive pyrotechnic compositions and an internal anvil. An impact on the cup's bottom ignites these compositions by compression between the cup and anvil to produce an output of heat,
20 light, gas and burning particles.

Percussion primers have been in use for over one hundred years. Over this time, test methods and apparatuses have been devised to measure different aspects of an ignition output, such as heat, light, pressure, and burning particles. Heat output has been measured with
25 calorimeters and light output has been measured with photocells and photographs of an ignition output's light and burning particles in a darkened room and with the aid of vented test volumes. Pressure

measurements have been made by simply having an operator listen to relative sound of the output in vented test fixtures, and by measuring the pressure in closed test volumes.

Tests of the effect of burning particles are made in a vented
5 volume and by a "standoff" method. In the latter, a primer is fired into a large, deep volume with a test propellant at the base. The depth is varied until ignition fails to occur.

One of the disadvantages common to the above-mentioned test methods and apparatuses is that virtually all system-level tests have been
10 performed on a go/no-go basis. That is, a system or sub-system is assembled and then initiated. The results will show that the tested initiator, such as a percussion primer, either did or did not work properly. Thus, the tests do not provide sufficient information on actual ignition interfaces used in ignition system designs. Consequently, little technical
15 understanding has been achieved in determining the relative importance of system variables and functional margins. Individual measurements of heat, light, pressure, and burning particles cannot be adequately extrapolated to a system-level performance. For example, the large volumes in all of the above-mentioned test apparatuses are not
20 representative of actual applications. The volumes reduce the available pressure and allow heat to dissipate, even to the point of quenching the burning particles.

Generally, the known methods and apparatuses discussed above only provide relative comparisons, which often depend on operator
25 judgment. These tests are incapable of measuring ignition within the first millisecond.

Ignitability has particular significance to aerospace applications where there is a need to measure how well an initiating element can ignite other materials. Specifications require that igniters fire when
30 supplied with sufficient electrical or mechanical input energy. For some devices, such as the NASA standard initiator, (NSI), output is controlled by specifying pressure performance limits when fired into a closed volume

(known as a "bomb") with no requirement for ignition by its output. However, no military specification or other generally accepted tests exist for measuring primer output, which is used only for ignition.

5 Percussion primers are generally about 0.2 inch or less in diameter and consist of thin wall brass cups containing blended pyrotechnic compositions and an internal anvil. Impacting and deflecting the bottom of the cup compresses the friction-sensitive pyrotechnic composition against the anvil to achieve ignition, thereby outputting a quantity of heat, light, gas and burning particles.

10 One specific test method and apparatus was developed for measuring energy output for many different kinds of explosive devices, including percussioned primers. The apparatus included a piston/cylinder energy sensor containing a strength-calibrated, crushable honeycomb element. The output of a percussion primer was measured as the work
15 done in stroking the piston to crush the honeycomb. Output was equated to the distance crushed multiplied by the crush strength of the honeycomb, and was expressed in units of inch-pounds.

Significantly, the most important percussion primer output parameter is not energy output to stroke a piston, but is instead the ignitability
20 performance. A need exists to develop a test method and apparatus which will determine whether the primer will ignite the next item in the train, and with what margin. The apparatus, however, was not capable of providing information with regard to ignition efficiency or time delay for achieving initiation.

25 Summary of the Invention

An object of the present invention is to provide a test method and apparatus capable of providing quantitative measurements of the efficiency of all types of initiators, one type thereof being percussion primers.

Another object of the invention is to provide a relatively simple method of comparing output performance of percussion primers and other initiators in terms of ability to ignite typical propellant materials.

In a preferred embodiment, an apparatus for testing ignitability of an
5 initiator includes a body having a central cavity, an initiator holder for holding the initiator over the central cavity of the body, an ignition material holder disposed in the central cavity of the body and having a cavity facing the initiator holder which receives a measured quantity of ignition
10 material to be ignited by the initiator and a chamber in communication with the cavity of the ignition material holder and the central cavity of the body, and means in communication with the central cavity of the body for measuring, recording and analyzing pressure characteristics generated by ignition of the ignition material by the initiator. Firing the initiator into the
15 ignition material causes the ignition material to ignite, and the pressure generated in the closed chamber is measured as a function of time to generate a pressure trace. Preferably, the method includes measuring pressure at one millisecond, time to reach 50 percent peak pressure, and time to reach peak pressure. "Ignitability" is then expressed as the ratio
20 of one millisecond pressure to peak pressure. This ratio can be compared to ratios similarly devised using other materials to provide comparative results.

These objects, together with other objects and advantages which will be subsequently apparent reside in the details of construction and operation of the apparatus and method steps as more fully hereinafter
25 described and claimed, reference being had to the accompanying drawings forming a part hereof, wherein like reference numerals refer to like parts throughout.

Brief Description of the Drawings

Fig. 1 is a cross-sectional view of an apparatus for testing
30 ignitability of an initiator according to the present invention;

Fig. 2 is a cross-sectional view of a portion of the apparatus illustrated in Fig. 1;

Fig. 3 is a view similar to Fig. 2, turned 90 degrees;

Fig. 4 is a top plan view of the portion illustrated in Fig. 2;

5 Fig. 5 is an enlarged, cross-sectional view of another portion of the apparatus of Fig. 1;

Fig. 6 is a top plan view of the portion illustrated in Fig. 5;

Fig. 7 is an exploded view of a sub-assembly of the apparatus of Fig. 1;

10 Fig. 8 is a graph illustrating a pressure trace of two different primer types (Primer I = M42C1 and Primer II = M42C2), both using the same type of ignition material (FFG black powder);

Fig. 9 is a graph showing a comparison of pressure traces produced by Primer I and Primer II percussion primers using A-Cannon
15 black powder ignition material;

Fig. 10 is a graph showing typical pressure traces produced by the Type I and Type II percussion primers, using 200 mg each of three different ignition materials; and

Fig. 11 is a graph illustrating a pressure trace, and data point
20 selected for numerical description and analysis of ignitability according to the method of the present invention.

Detailed Description of the Preferred Embodiments

The aforementioned drawings will be discussed with reference to examples of test materials, such as percussion primers and ignition
25 materials. In conducting tests using the apparatus and method of the present invention, the following percussion primers were used:

Percussion Primer I

Diameter - 0.1748 to 0.1756 inch; Height - 0.111 to 0.119 inch

Composition

	<u>Ingredients</u>	<u>Percentage by Weight</u>
5	Lead Styphnate	53
	Barium Nitrate	22
	Antimony Sulfate	10
	Aluminum (powdered)	10
	Tetracene	5

10

Percussion Primer II

Diameter - 0.1748 to 0.1756 inch; Height - 0.111 to 0.119 inch

Composition

	<u>Ingredients</u>	<u>Percentage by Weight</u>
	Lead Thiocyanate	25
15	Potassium Chlorate	33
	Antimony Trisulfide	25
	TNT	3
	Calcium Silicide	14

20 The two primers I and II, are available as percussion primers M42C1-PA101 and M42C2-793, respectively, and were selected for their markedly different output performances. The output of Primer I is considerably more brisant than Primer II, due to Primer I's lead styphnate content.

Ignition Materials used for testing are identified as follows:

	<u>Nomen- clature</u>	<u>Material</u>	<u>Physical Description</u>
	FFFG	Black Powder	0.020 to 0.030 in. granules
5	FFG	Black Powder	0.020 to 0.060 in. granules
	A-Cannon	Black Powder	0.125 to 0.250 in. platelets (0.60 in thickness)
10	20/40	Boron-Potassium Nitrate (BKNO ₃)	Salt to flour consistency
	Type I (6/12)	(BKNO ₃)	0.60 to 0.130 granules
15	Type 2R Pellets	(BKNO ₃)	0.125 DIA x 0.100 height, domed ends

The ignition materials were selected to provide a wide range of initiation sensitivities and burning rates. That is, the finer powders and granules would be expected to ignite more easily and burn more rapidly than the larger granules and pellets. Black powder and boron-potassium nitrate are the most extensively used ignition materials.

The test apparatus of the present invention is generally referred to in Fig. 1 by the numeral 20.

A percussion primer is pressed into a primer holder 22 which is placed into an upper cavity of a body 24. An adapter 26 threads down onto the primer holder 22 in order to firmly hold the primer holder in the upper cavity of the body 24 and over a central cavity. An O-ring 28 provides a pressure seal between the adapter 26 and the primer holder 22.

An ignition material holder 30 is disposed in a central cavity of the body between the primer holder 22 and a plug 32 threaded into a lower cavity provided in the body 24. The material holder 30 has a hemispherical cavity 34 facing the primer holder 22 which, when

performing a test, is designed to receive a quantity of ignition material (in one embodiment about 200 mg). The ignition material is weighed out and inserted into the hemispherical cavity 34 prior to assembly of the apparatus. In the embodiment of the invention which uses about 200 mg
5 of material, the hemispherical cavity 34 has a diameter of 0.435.

The body 24 is illustrated in Figs. 2-4 prior to assembly with the other parts. These figures illustrate the upper cavity 36, the central cavity 38, and the lower cavity 40. The three cavities collectively form a longitudinal passageway through the body 24 which, upon assembly,
10 receives the adapter 26, the material holder 30, and the plug 32, all of which are in end-to-end contact at opposite ends of the central cavity 38. The body 24 is substantially cylindrical in shape, except for parallel flattened surfaces 42 and 44.

A pair of sockets 46 and 48 extend transversely through the body
15 24 from diametrically opposite sides of the central cavity 38. The sockets 46 and 48 have bores 50 and 52, respectively, which extend into communication with the central cavity 38.

Referring to Figs. 5 and 6, the material holder 30 is shown in greater detail by enlargement. The material holder 30 has an upper
20 portion 54 in which the hemispherical cavity 34 is formed. Six axially oriented holes 56 extend from an outer region of the hemispherical surface of the hemispherical cavity to an axially disposed cylindrical chamber 58 formed in the material holder 30 below the upper portion 54. Four lateral holes 60, which are substantially horizontally coplanar, extend
25 from the cylindrical chamber 58 to an annular recess 62 formed externally around the outer cylindrical surface of the material holder 30. Expanding hot gas and burning particles which pass through the six vertical holes 56 enter the cylindrical chamber 58 and exit therefrom through the lateral holes 60. When assembled into the body 24 of the
30 test apparatus, the lateral holes 60 are disposed in a horizontal plane beneath the bores 50 and 52 so as to protect the transducers 64 and 66 (Fig. 1) which are fitted into the sockets 46 and 48, respectively. The

annular recess 62 allows the hot gas and thus the pressure generated by ignition, to be communicated to the transducers.

When assembled, the hemispherical cavity 34 and the cylindrical chamber 58, which are in communication with each other by virtue of the vertical holes 56, are sealed at opposite ends by the primer holder 22 and the plug 32.

Referring to Fig. 7, the adapter 26 has a central bore 68 slidably receiving a firing pin mechanism 70 having a pin 72 at a proximal end thereof. Upon actuation of the firing pin mechanism, the pin 72 passes through an opening 74 to strike a primer held in the primer holder 22 which is received in a space 76.

The primer holder 22 has a cavity 78 which receives a percussion primer 80. When the firing pin mechanism is thrust downwardly to the full extent, the pin 72 will strike the upper portion of the percussion primer thus firing the same. The percussion primer acts as a seal to prevent venting of pressure created during the burning of the ignition material.

In operation, the percussion primer 80 is initiated by impacting the firing pin with about 100 inch-ounces of striking energy. Primer ruptures, caused by excessively deep penetration of the firing pin into the primer, are prevented by restricting the firing pin penetration to about 0.030 inch. The output of the percussion primer transfers through a spit hole 84 of the primer holder 22 onto the ignition material received in the hemispherical cavity 34. The high pressure gases, generated by the combustion of the ignition material vent through the six vertical holes 56 in the holder 30 into the cylindrical chamber 58 and subsequently to the pressure transducers 64 and 66. The transducer outputs are measured with an oscillograph 65 and recorded on magnetic tape and permanent records are created.

After testing, the apparatus is easily disassembled for cleaning to assure the same initial conditions exist for each firing.

The pressure transducers 64 and 66 are preferably piezoelectric type transducers, which are well known and commercially available. One such transducer is the KISTLER MODEL 601A. An associated measurement system measures pressure sensed by the transducers, and
5 can include known components such as charge amplifiers, voltage amplifiers, a tape recorder and oscillograph, which has a frequency response that is preferably flat to 40 kHz.

The system will facilitate the creation of a "pressure trace" which is a graphical illustration of a pressure wave plotted on X and Y axes, with
10 pressure on the Y-axis and time on the X-axis. These pressure traces are illustrated in Figs. 8-11.

Tests performed with the ignition materials in the bottom of the central cavity 38 (thus resting on the upper surface of the plug 32 in the absence of the material holder 30) produced very little performance
15 differences. To evaluate the ignition and burning rate extremes afforded by very fine to very coarse ignition materials, the 20/40 and 2R BKNO₃ materials were tested. Quantities were doubled to exaggerate potential differences of burning rate and peak pressures achieved. The pressure traces generated by either primer indicated poor ignition characteristics,
20 that is, very slow (100 millisecond time frame) non-reproducible build-up of pressure. The material holder of the present invention was found to facilitate a better presentation of the ignition material to the output of the percussion primer, and provide a more controlled burning of the ignition material.

25 In using the ignition material holder 30 in the central cavity 38, the initiation and combustion characteristics improved immediately. Pressures rose quickly and the powdered ignition material was consumed in less than 10 milliseconds. The 20/40 BKNO₃ and FFFG black powder ignited very quickly, so that little differentiation could be made between the
30 ignition performance of these two primers. Conversely, the 2R BKNO₃ pellets ignited so slowly that, again, differentiation could not be recognized between primers.

The first successful differentiation was achieved in using the FFG black powder, as shown in the graph of Fig. 8. The pressure produced by primer I rose immediately, and primer II produced an initial gradual increase, followed by a rapid rise in comparison to primer I.

5 Fig. 9 shows the pressure traces produced when using the A-cannon ignition material. As before, the differences are significant.

Two percussion primers, Primer I and Primer II were used in five tests, with each of the FFG and A-Cannon black powder and the Type I BKNO_3 . Typical pressure traces generated by the parametric
10 investigation were plotted on the same coordinate system and then analyzed to determine a statistical compilation and comparison of the performances achieved. A compilation of typical pressure traces produced by primer I and primer II percussion primers, using 200 mg each of the three different ignition materials is shown in Fig. 10 (which
15 has a reduced time scale, compared to the preceding graphs).

The data points selected to provide a numerical description and analysis of the pressure traces for the ignitability test method are shown in Fig. 11. Logical descriptives are the time to reach peak pressure, the time to reach 50% of peak pressure, and the peak pressure achieved.
20 Another significant measurement is the pressure achieved at one millisecond. Since the major portion of both primers I and II heat contribution is achieved within the first millisecond, this time interval is significant for measuring primer initiation capability. According to the present invention, the ratio of the pressure at one millisecond to the peak
25 pressure defines ignitability.

The following tables I-VI summarize test data obtained using the aforementioned descriptives. The initial comparison for each ignition material reveals that primer I achieved ignition sooner and more rapidly than did primer II. Secondly, the FFG black powder, using either primer
30 (according to Tables I and II) produced the highest ignitability values (the ratio of pressure achieved at one millisecond over the peak pressure).

The A-cannon black powder (Tables III and IV) was second, and the Type I BKNO_3 , Tables V and VI, was third.

TABLE I.- FUNCTIONAL DATA ON THE M42C1 PERCUSSION PRIMER USING 200 MG FFG BLACK POWDER IGNITION MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P \text{ PEAK}}$ (%)
1	3.1	.9	2080	1340	64
2	3.1	.8	2090	1255	60
3	3.0	.7	2060	1305	63
4	2.8	.8	2045	1255	61
5	3.2	.7	1955	1200	61
AVE	3.0	.78	2046	1271	61.8
STD DEV	.15	.08	53.7	53.5	1.6

TABLE II.- FUNCTIONAL DATA ON THE M42C2 PERCUSSION
PRIMER USING 200 MG FFG BLACK POWDER
IGNITION MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P \text{ PEAK}}$ (%)
1	5.2	3.0	1795	155	8.6
2	5.5	2.8	1785	90	5.0
3	4.3	1.7	1800	360	20.0
4	5.0	2.5	1775	125	7.0
5	5.6	2.9	1800	55	3.0
AVE	5.1	2.5	1791	157	8.7
STD DEV	.51	.52	10.8	119.5	2.7

TABLE III.- FUNCTIONAL DATA ON THE M42C1
PERCUSSION PRIMER USING 200 MG OF
A-CANNON BLACK POWDER IGNITION
MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P \text{ PEAK}}$ (%)
1	8.9	1.0	1465	800	54.6
2	9.2	1.1	1695	730	43.1
3	15.1	1.6	1225	490	40.0
4	7.7	2.0	1465	570	38.9
5	12.0	1.1	1395	630	45.2
AVE	10.6	1.4	1449	644	44.4
STD DEV	2.9	.42	168.9	123.6	6.2

TABLE IV.- FUNCTIONAL DATA ON THE M42C2
PERCUSSION PRIMER USING 200 MG OF
A-CANNON BLACK POWDER IGNITION
MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P \text{ PEAK}}$ (%)
1	13.8	3.9	1380	180	13.0
2	16.7	3.9	1410	260	18.4
3	15.8	5.8	1195	120	10.0
4	19.1	6.4	1320	110	8.3
5	16.8	5.3	1250	180	14.4
AVE	16.4	5.1	1311	170	12.8
STD DEV	1.9	1.1	89.1	60	3.9

TABLE V.- FUNCTIONAL DATA ON THE M42C2 PERCUSSION
PRIMER USING 200 MG OF TYPE I BORON-
POTASSIUM NITRATE IGNITION MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P \text{ PEAK}}$ (%)
1	32.2	4.92	845	345	45.8
2	32.5	7.6	786	156	19.8
3	28.3	7.8	880	104	11.8
4	23.5	5.0	904	144	15.9
5	32.9	8.6	804	100	12.4
AVE	29.8	6.7	843	169	20.1
STD DEV	4	1.7	49.6	100.9	11.9

TABLE VI.- FUNCTIONAL DATA ON THE M42C2 PERCUSSION
PRIMER USING 200 MG OF TYPE I BORON
POTASSIUM NITRATE IGNITION MATERIAL

TEST NUMBER	TIME TO PEAK PRESSURE (ms)	TIME TO 50% PEAK (ms)	PEAK PRESSURE (psi)	PRESSURE @ 1ms (psi)	$\frac{P @ 1ms}{P PEAK}$ (%)
1	33.4	10.9	785	25	3.1
2	42.2	14.2	756	16	2.1
3	37.3	13.2	742	66	8.8
4	31.4	9.5	744	56	7.5
5	39.2	12.3	748	74	9.8
AVE	36.7	12.02	755	47.4	6.6
STD DEV	4.3	1.8	17.6	25.5	3.4

Finally, and most importantly, ratioing the ignitability of the two primers for each ignition material, the FFG black powder indicated the most differentiation in performance. The FFG black powder ignitability for primer I was 61.8 (Table I) and for primer II, 8.7 (Table II) producing a ratio of 7.1. For the A-cannon black powder, the ratio was 3.5, and for the Type I $BKNO_3$, the ratio was 3.0.

Although ignition is a major requirement for systems such as aerospace rocket motors, munitions and even automobile air bags, no method currently exists, other than the present invention, to measure relative ignition efficiency, or "ignitability." Consequently, no specification

exists on ignitability, and surprisingly, there are no output test requirements in any military specification for percussion primers which are used only for initiation.

5 The key parameters for achieving a successful test methodology and bomb configuration and acceptable pressure performance differentiation between primers were determining the proper ignition material and its confinement. The fine ignition materials, which were easily initiated and exhibited very high burn rates, produced similar pressure traces with either primer. Conversely, the large pellet ignition
10 materials initiated and burned so slowly that the pressure traces were again similar with either primer. The ignition material had to be confined in a holder at the top of the test bomb cavity, facing the percussion primer, rather than in the bottom of the cavity to achieve reproducible pressure performances. This confinement provided highly reproducible
15 initial conditions and allowed primer output to penetrate and mix with the igniter material to achieve ignition. Furthermore, the small initial volume sustained the initial primer output pressure, supporting the conditions needed for stable combustion. This configuration has the added benefit of providing a good simulation of actual design interfaces.

20 The present method clearly differentiates the ignition performances of two different percussion primers. The pressure traces produced by each primer, test-fired with FFG black powder, A-cannon black powder and Type I boron-potassium nitrate (BKNO_3), were markedly different in any combination. Recorded for statistical comparisons were the times to
25 peak and 50 percent of peak pressure, the peak pressure, and a term defined herein as "ignitability." Ignitability is defined as the ratio of the pressure achieved within the first millisecond over the peak pressure. The first millisecond is when the major portion of primer output is produced to initiate the ignition materials.

30 The FFG black powder proved to be the best ignition material in the test, followed by A-cannon black powder and Type I BKNO_3 , to evaluate the differences in output performance of the two percussion

primers. The most dramatic single data point comparator was ignitability. The ignitability of primer I, using the FFG black powder, was 7.1 times greater than that produced by the primer II.

5 The many features and advantages of the present invention are apparent from the detailed specification, and thus, it is intended by the appended claims to cover all such features and advantages of the ignitability test method and apparatus which fall within the true spirit and scope of the invention. Further, since numerous modifications and changes will readily occur to those skilled in the art based upon the
10 disclosure herein, it is not desired to limit the invention to the exact construction and operation illustrated and described. Accordingly, all suitable modifications and equivalents may be resorted to falling within the scope and the spirit of the invention.

What is claimed is:

IGNITABILITY TEST METHOD AND APPARATUS**Abstract of the Disclosure**

5 An apparatus for testing ignitability of an initiator includes a body
having a central cavity, initiator holder for holding the initiator over the
central cavity of the body, an ignition material holder disposed in the
central cavity of the body and having a cavity facing the initiator holder
which receives a measured quantity of ignition material to be ignited by
the initiator and a chamber in communication with the cavity of the
10 ignition material holder and the central cavity of the body, and a
measuring system for analyzing pressure characteristics generated by
ignition of the ignition material by the initiator. The measuring system
includes at least one transducer coupled to an oscillograph for recording
pressure traces generated by ignition.