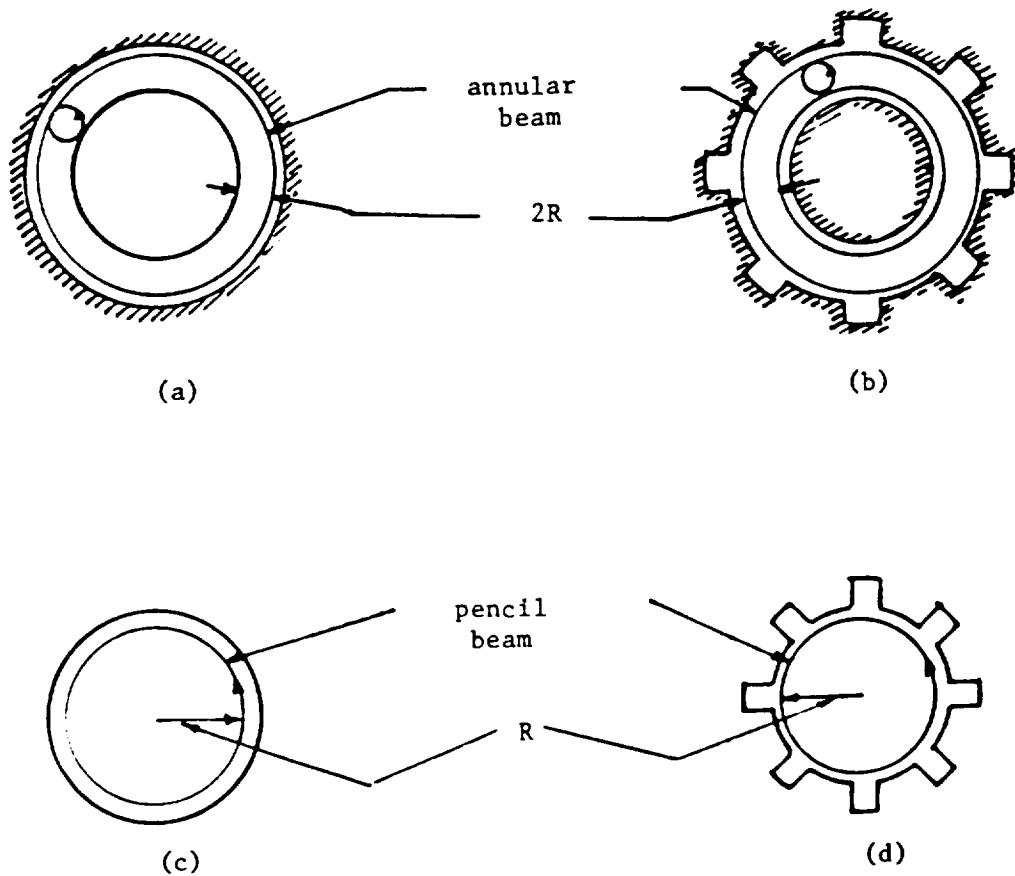


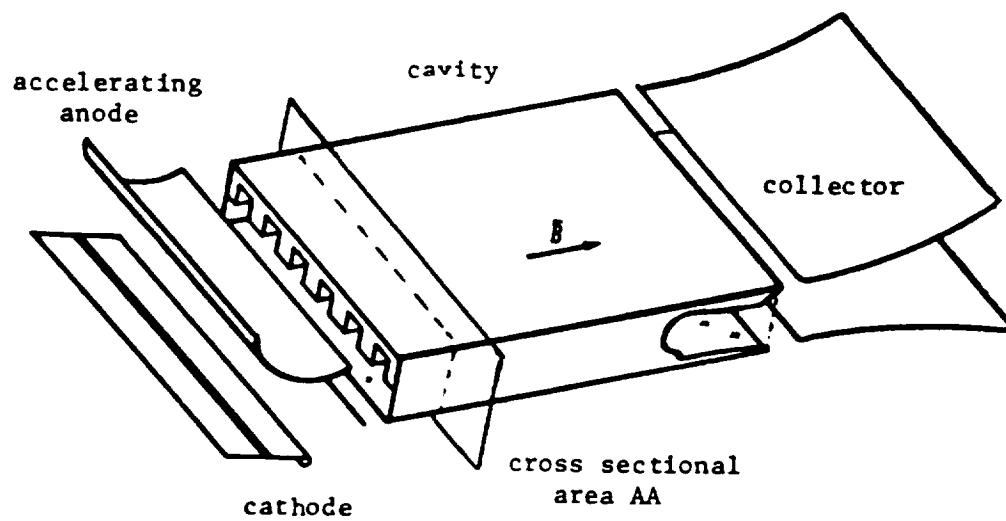
ANALYSIS OF A HIGH HARMONIC RECTANGULAR GYROTRON USING RIBBON BEAMS

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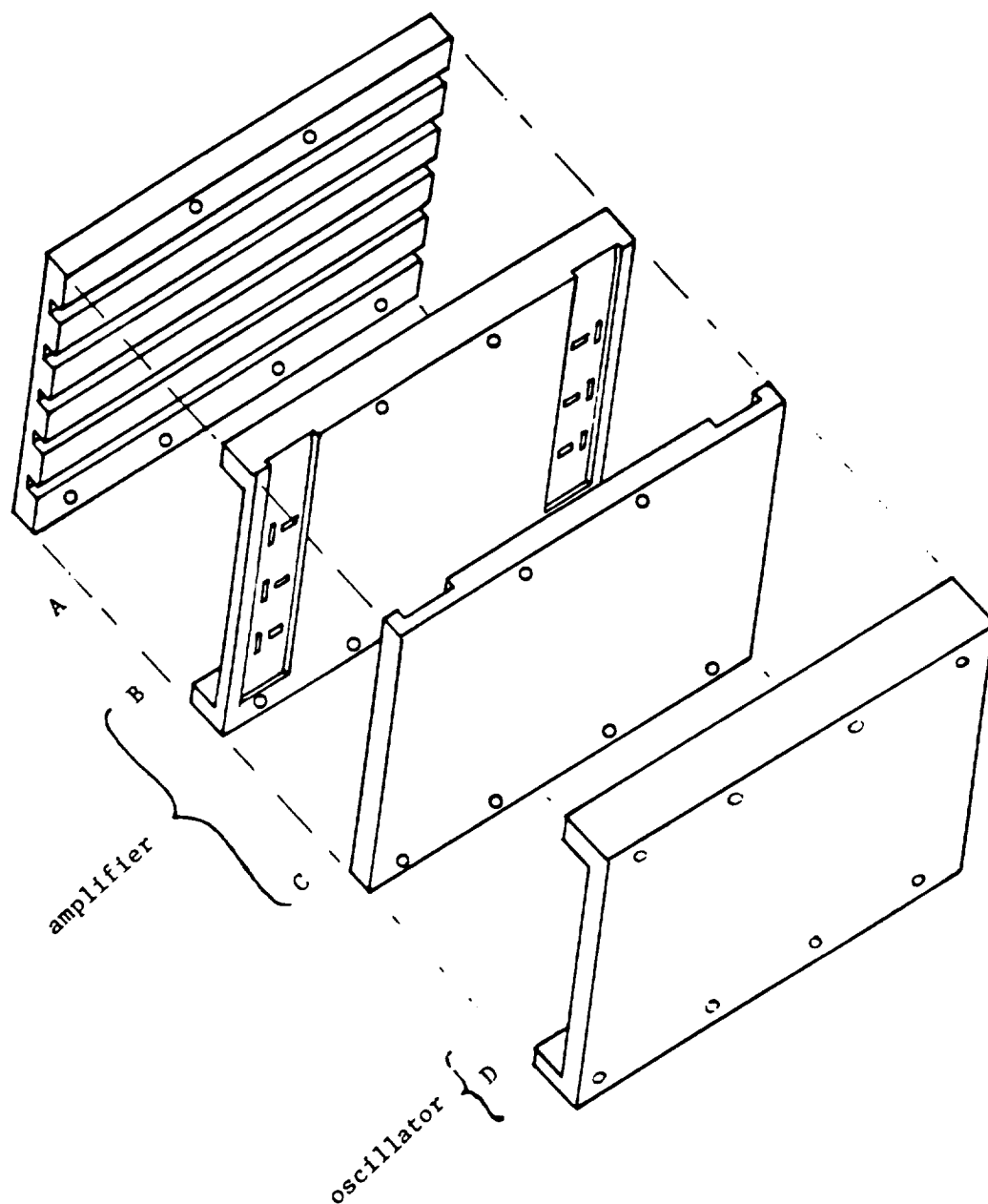


Cylindrical cavity structures and electron orbits in
a) conventional, b) grooved coaxial, c) whispering
gallery mode gyrotron and d) gyromagnetron.
In b) the electrons see only a single ridge in their
complete orbit. In a) and c) the electrons do not
see any ridges at all during their complete orbit
but generate highly efficient interactions with the
electromagnetic fields.

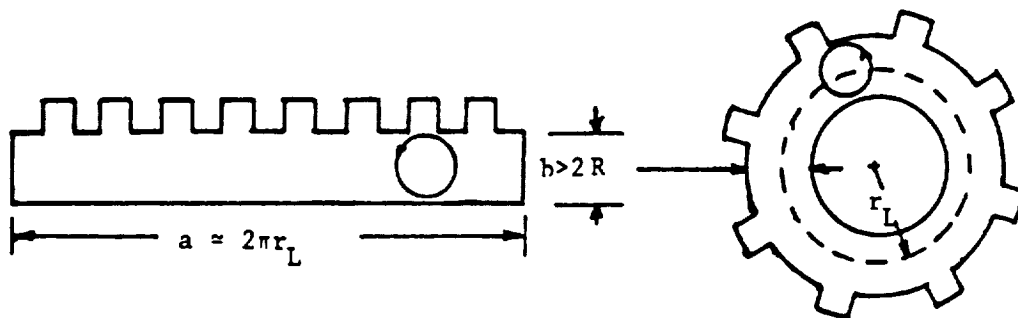
*Presently at Electrical & Computer Engineering Department,
University of Cincinnati, Cincinnati, Ohio, 45221.



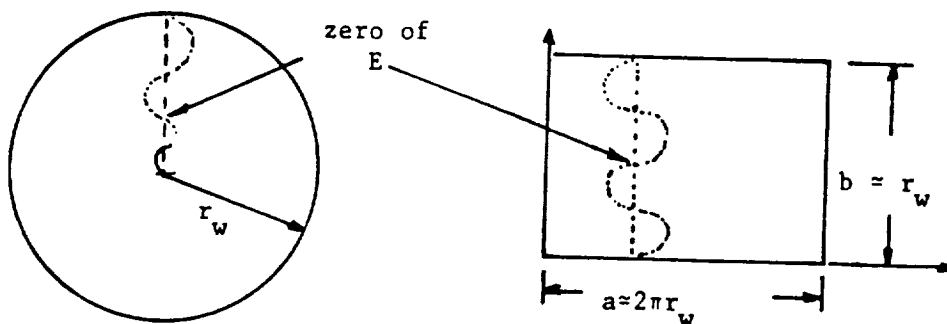
General schematic of an axially grooved gyrotron
using a ribbon beam.



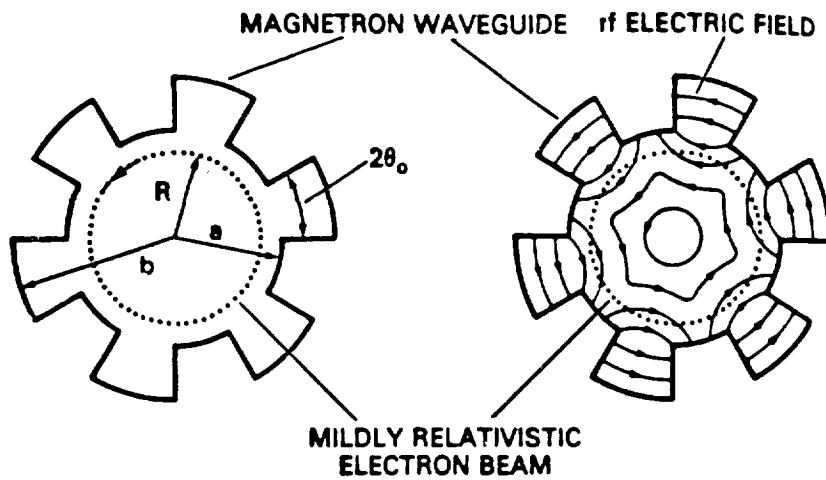
Constructional details. Upper grooved wall A is attached to the B and C for an amplifier or to D for an oscillator. B has coupling holes for input-output.



a - Folding a rectangular waveguide is equivalent to a coaxial waveguide.

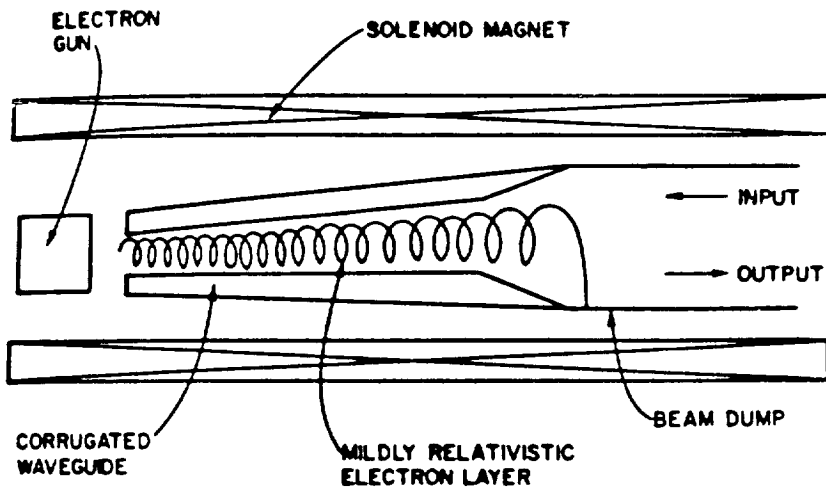


b - For fields to be compatible, only a rectangular waveguide with large dimensions but with small b/a ratio is equivalent to a circular waveguide having a few radial zeros.



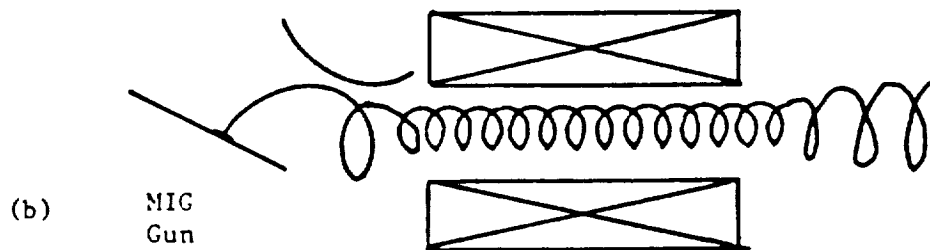
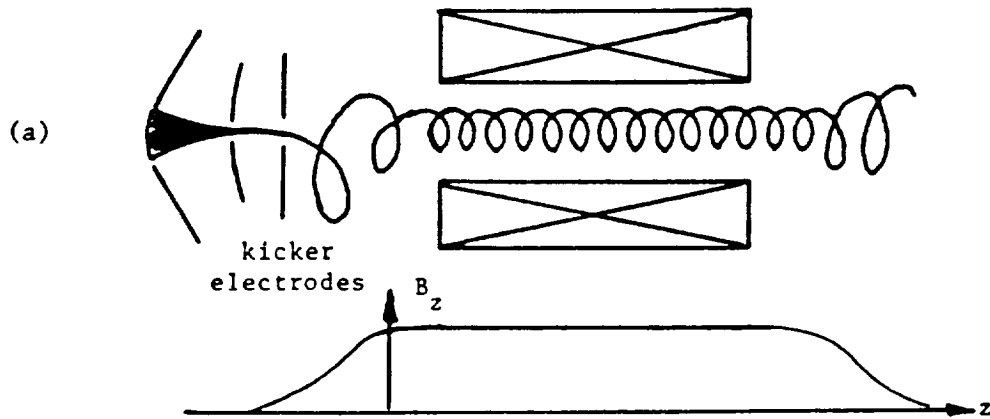
(a) Left. The cross-sectional view of a gyromagnetron with six vanes. (b) Right. Sketch of the rf electric fields of the 2π mode.

Low Magnetic Field Gyrotrotron

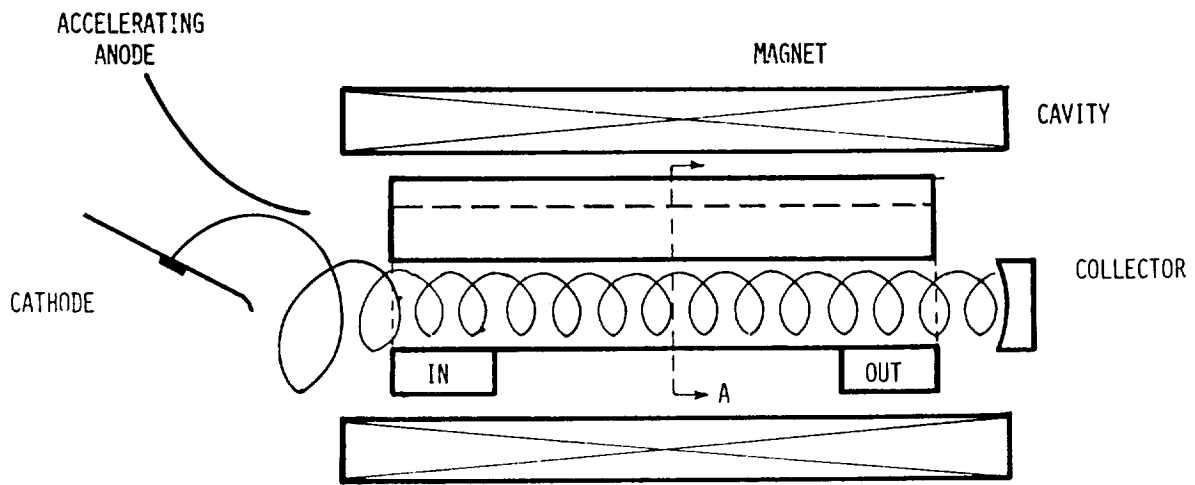


A schematic drawing of a low magnetic field, broad band, gyromagnetron amplifier

Pierce
Gun



a) Ribbon beam using a conventional Pierce gun and kicker fields. b) Ribbon beam generated by a planar version of the MIG gun.



LONGITUDINAL CROSS SECTION OF GYROTRON AMPLIFIER

RESULTS

OPERATING FREQUENCY = 90 GHz

HARMONIC NUMBER 5

$V_1 = 0.4 \text{ C}$

$V_2 = 0.267 \text{ C}$

$\nu = 2.2 \times 10^{-3} \text{ (9.5 A)}$

$P_b \text{ (BEAM CURRENT)} = 670 \text{ KW}$

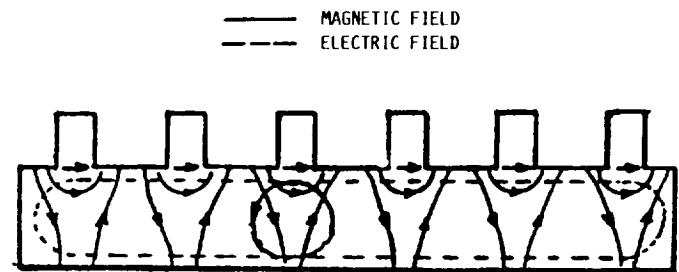
$N = 3$

$\alpha = 0.64 \text{ cm}$

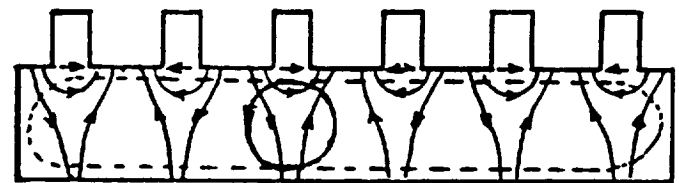
$b = 0.2928 \text{ cm}$

$R_w = 0.15$

$R_d = 0.19$

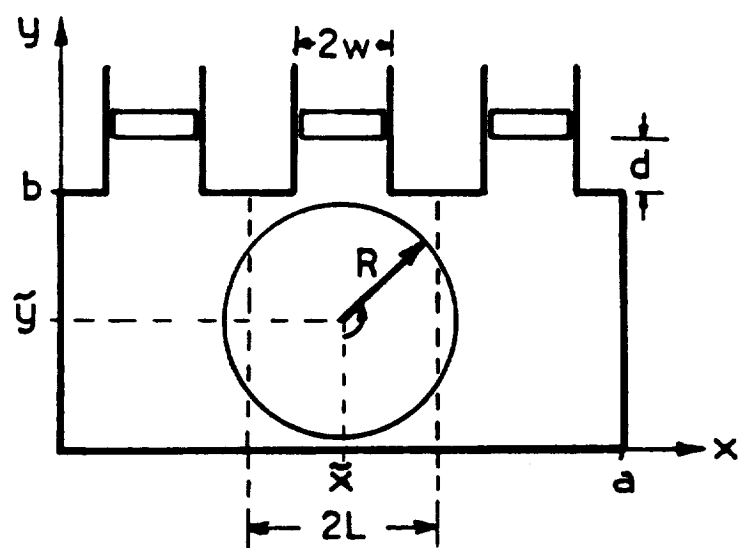


2π Mode

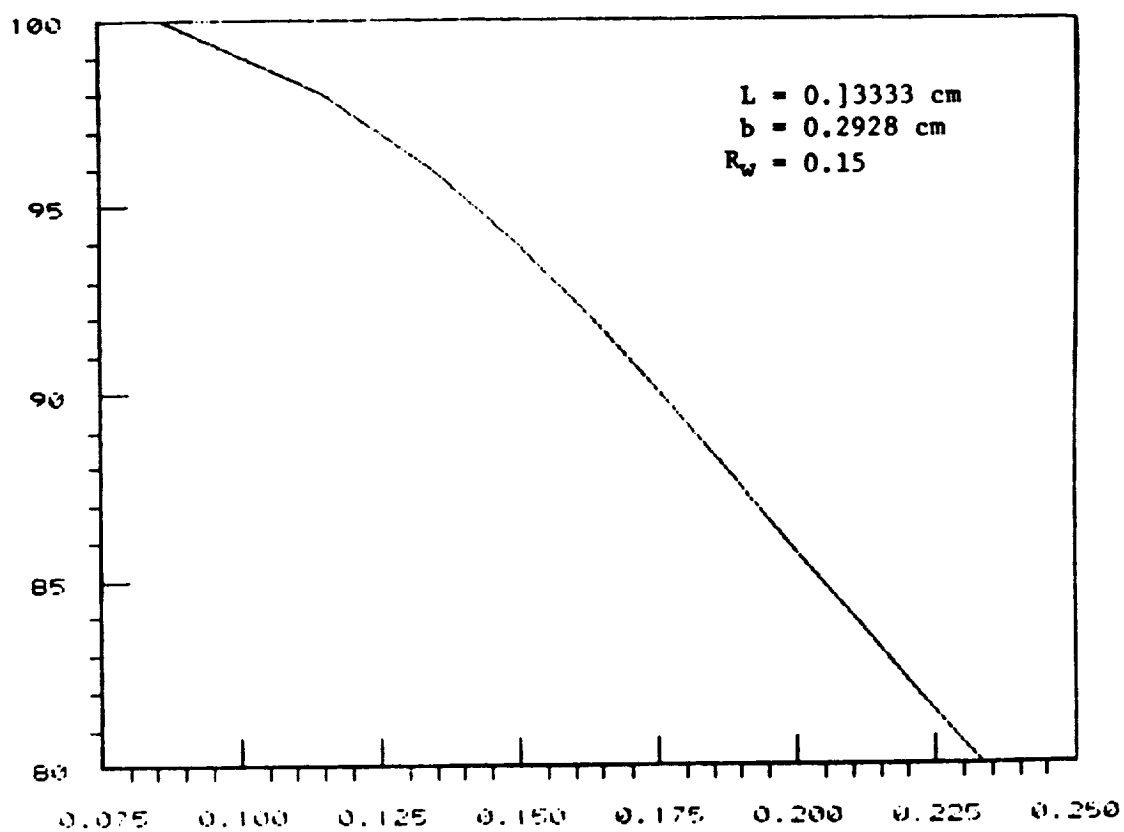


π Mode

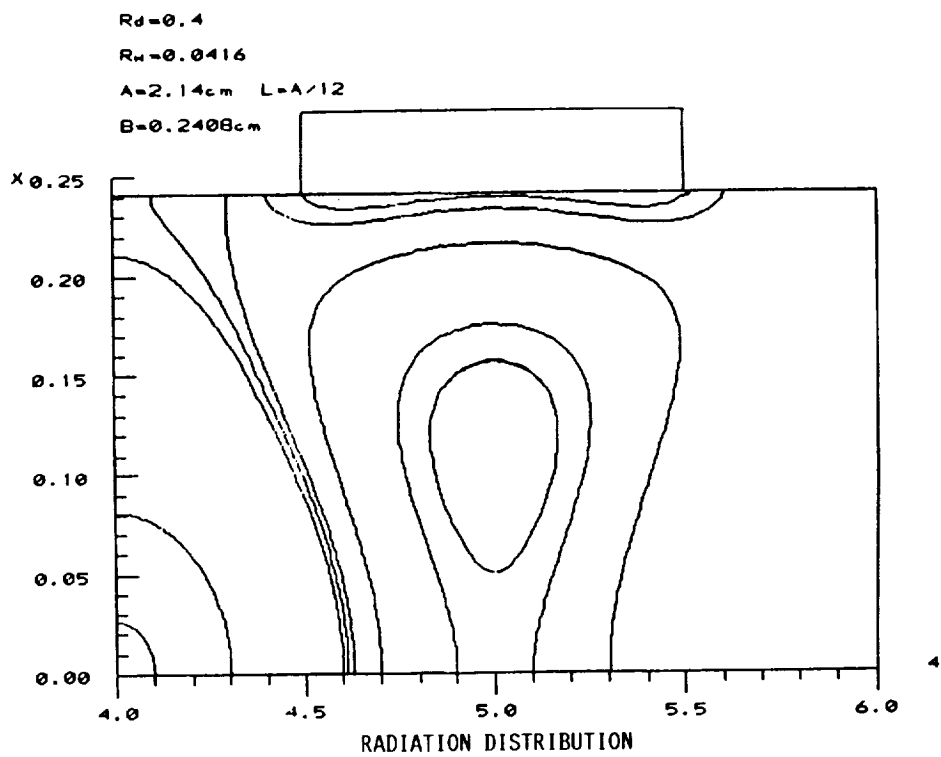
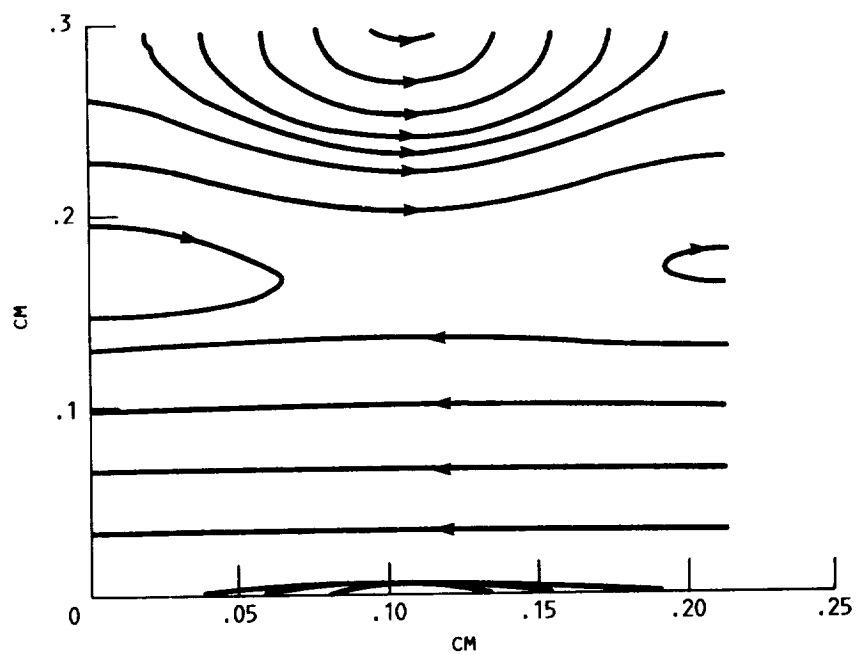
RADIATION PATTERN IN RECTANGULAR GYROTRON

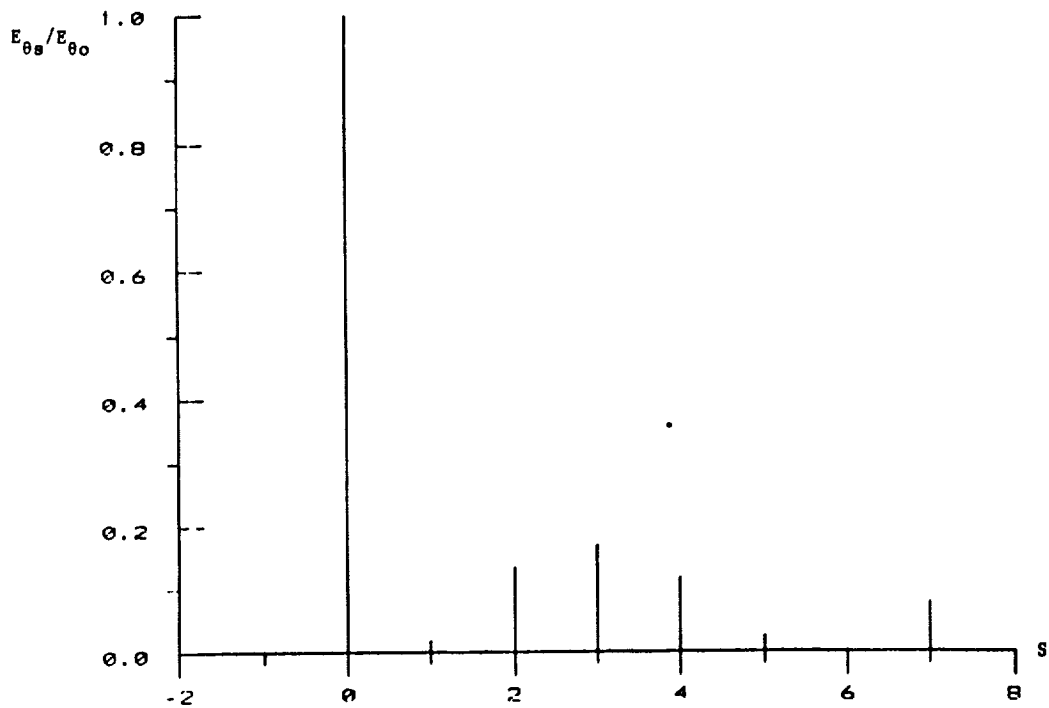


f (GHz)

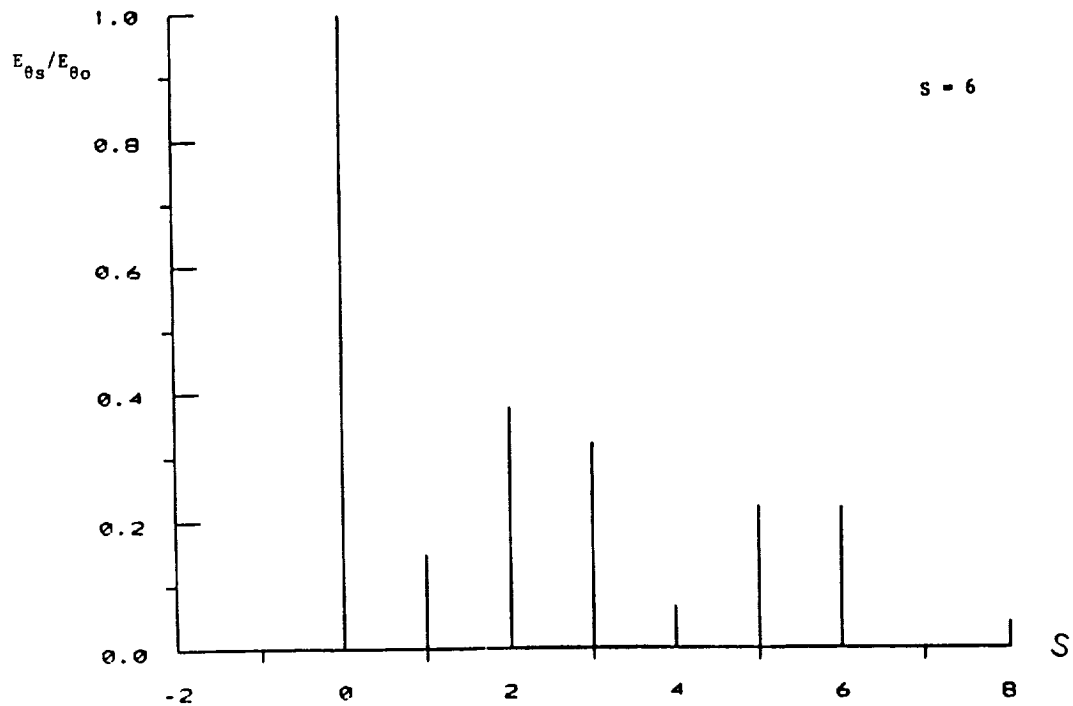


$R_d = d/b$

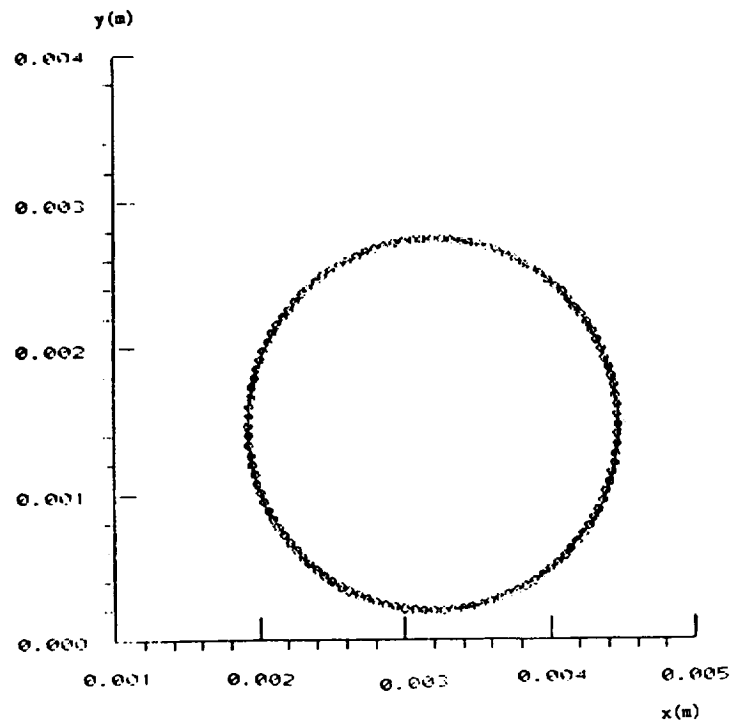




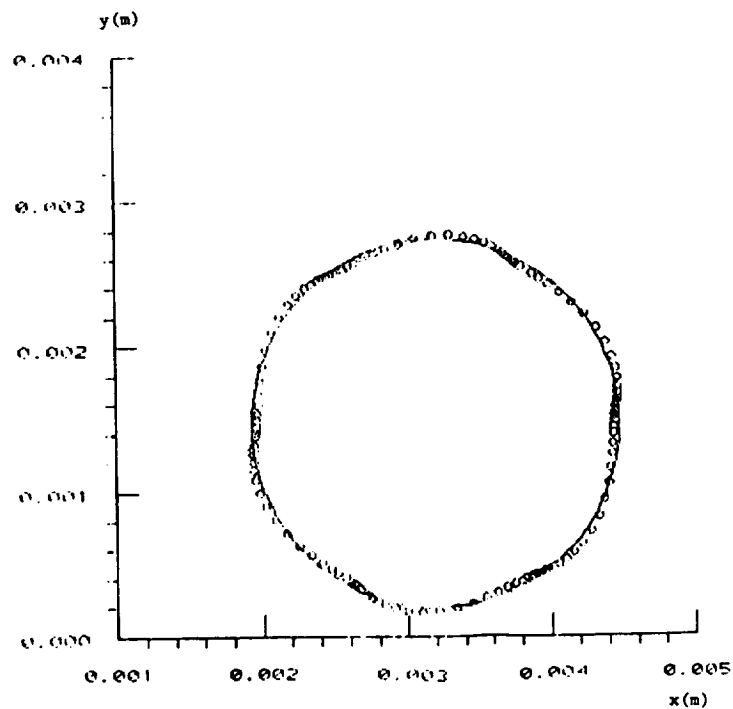
Fourier component spectrum of the tangential electric field



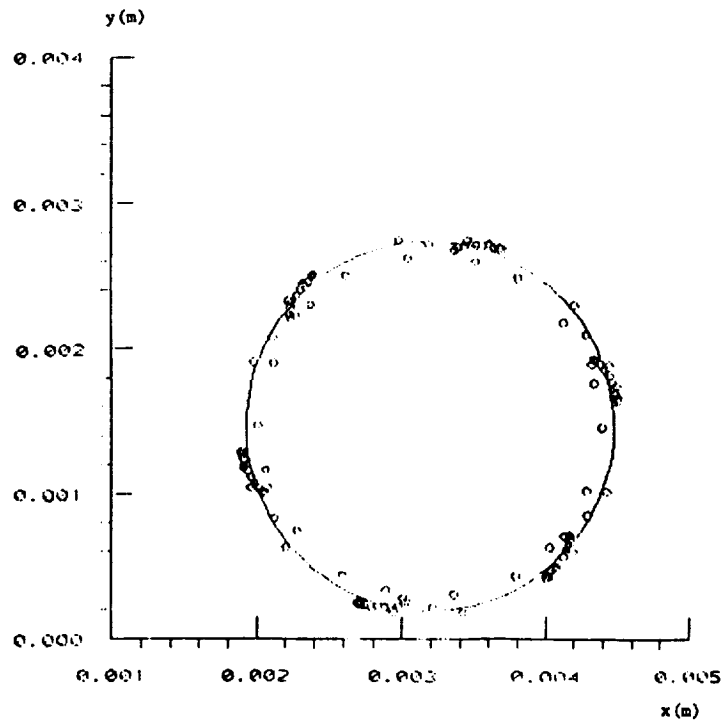
Fourier component spectrum of the tangential electric field



The initial phase distribution of an annular pencil beam which includes 120 electrons.

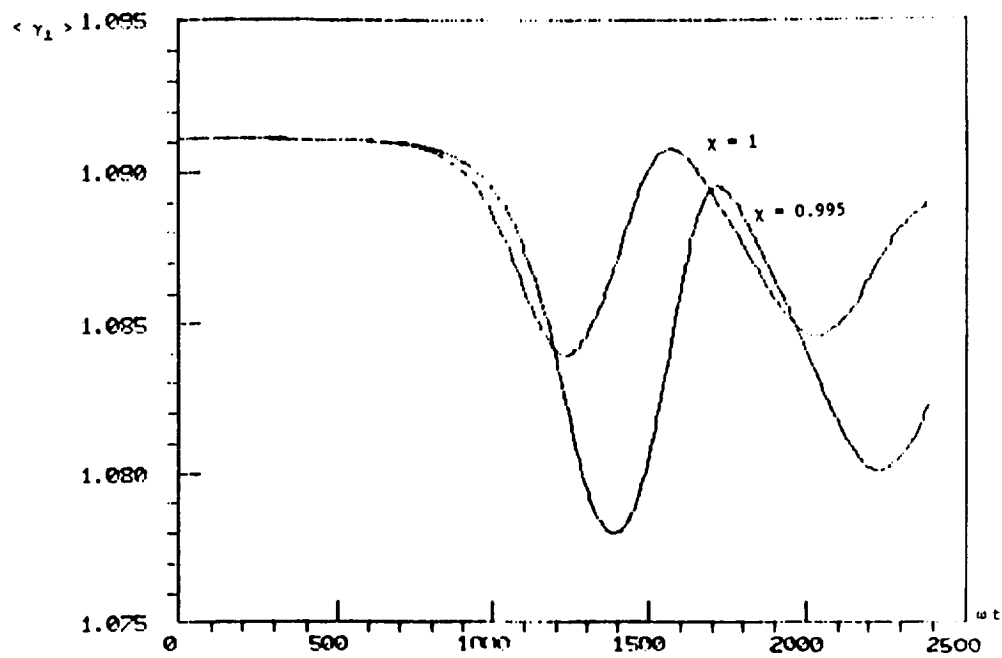


The phase distribution of the ensembled 120 electrons in linear region.

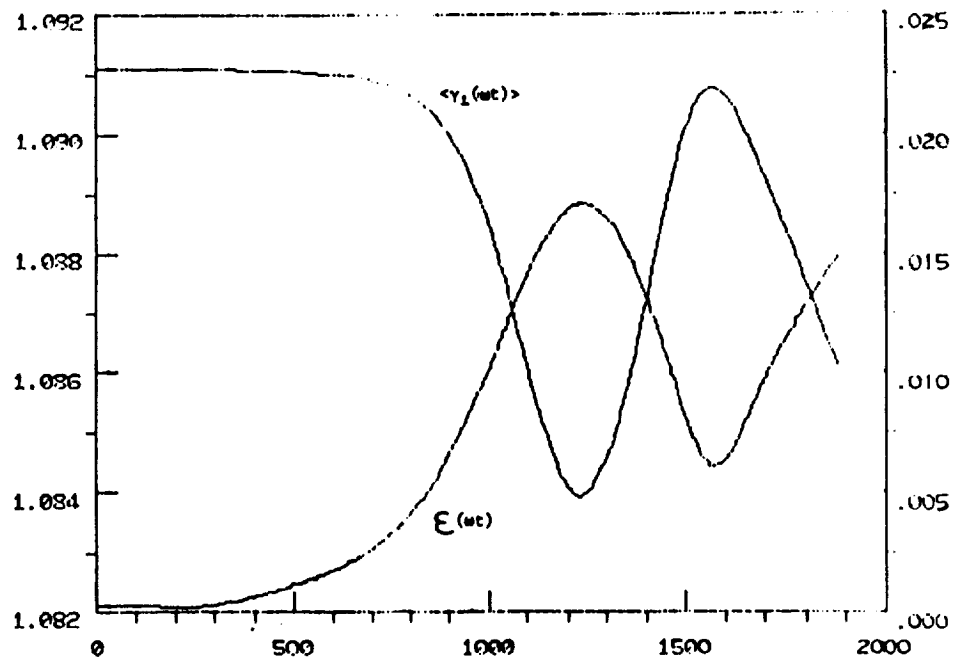


The phase distribution of the ensembled 120 electrons when the electrons regain energy from the field after saturation.

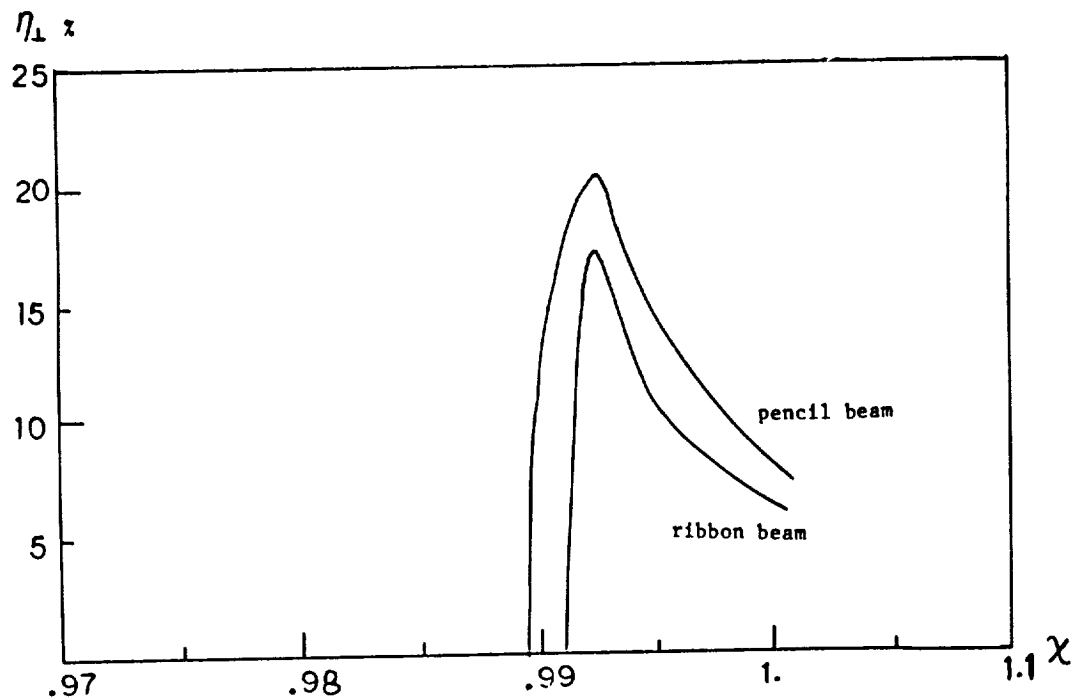
ORIGINAL PAGE IS
OF POOR QUALITY



Energy curves with $\chi = 0.995$ and $\chi = 1$ respectively for a pencil beam at $s=6$.



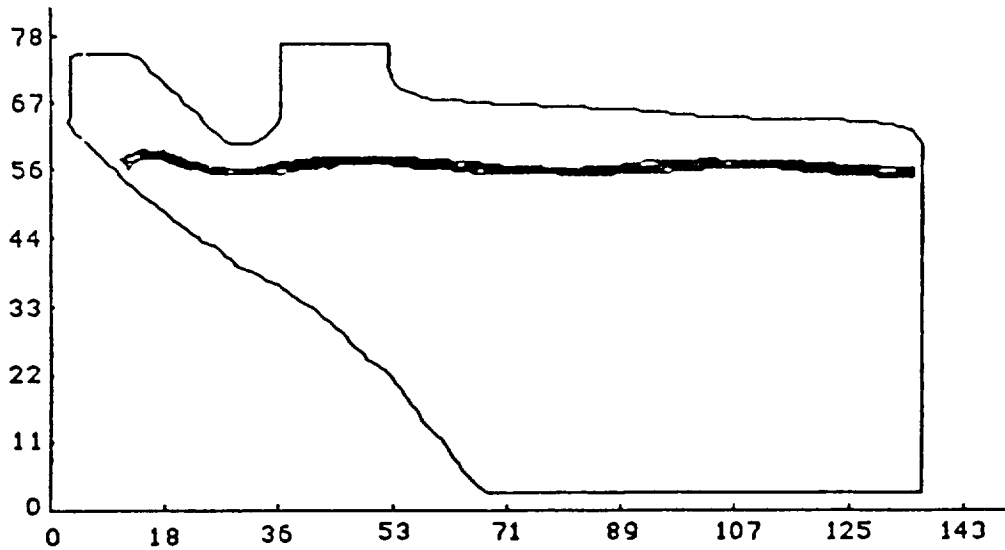
The field amplitude and average beam γ as a function of ωt for a typical nonlinear simulation.



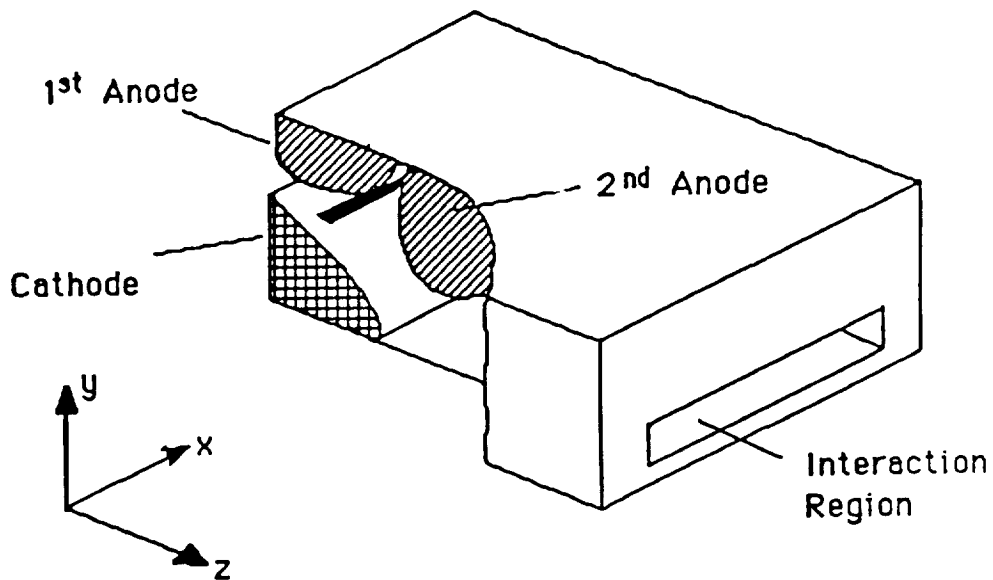
The energy conversion efficiencies of sixth cyclotron harmonic operation vs. χ for a pencil beam with its guiding center $(a/2, b/2)$ and a ribbon beam at $y=b/2$.

ADVANTAGES

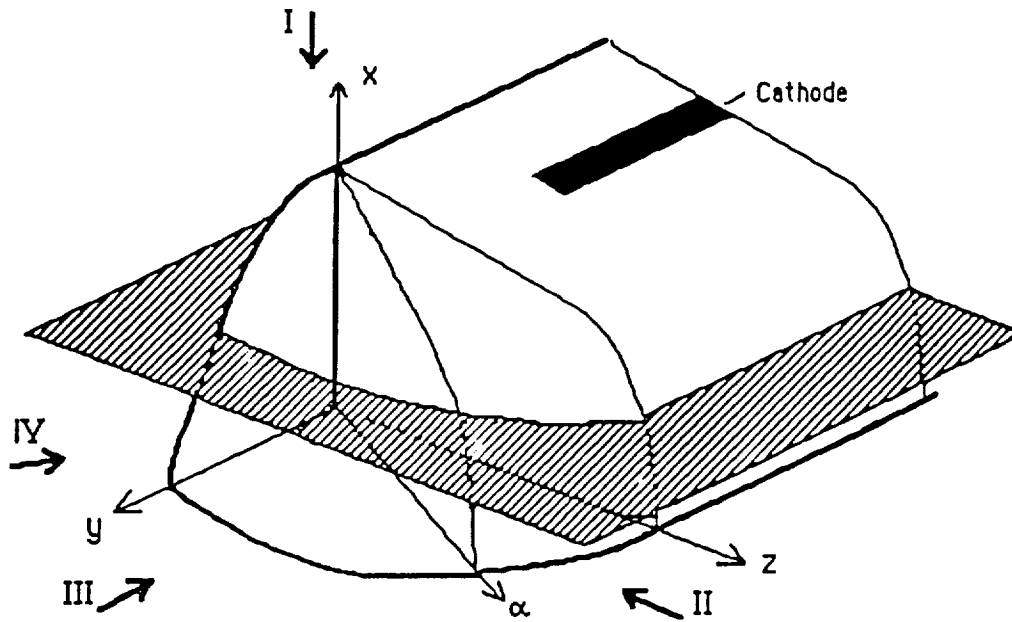
- 1 - ELIMINATION OF SUPERCONDUCTING MAGNETS
- 2 - REDUCED MODE COMPETITION PROBLEMS
- 3 - HIGHER POWER HANDLING CAPABILITY
- 4 - REDUCTION OF SPACE CHARGE FORCES
- 5 - EASE OF MODIFICATION AS AN AMPLIFIER AND OSCILLATOR
- 6 - EASE OF MACHINING
- 7 - SEPARATE INPUT-OUTPUT PORTS FOR AN AMPLIFIER
- 8 - BETTER EFFICIENCY AT HIGHER HARMONICS



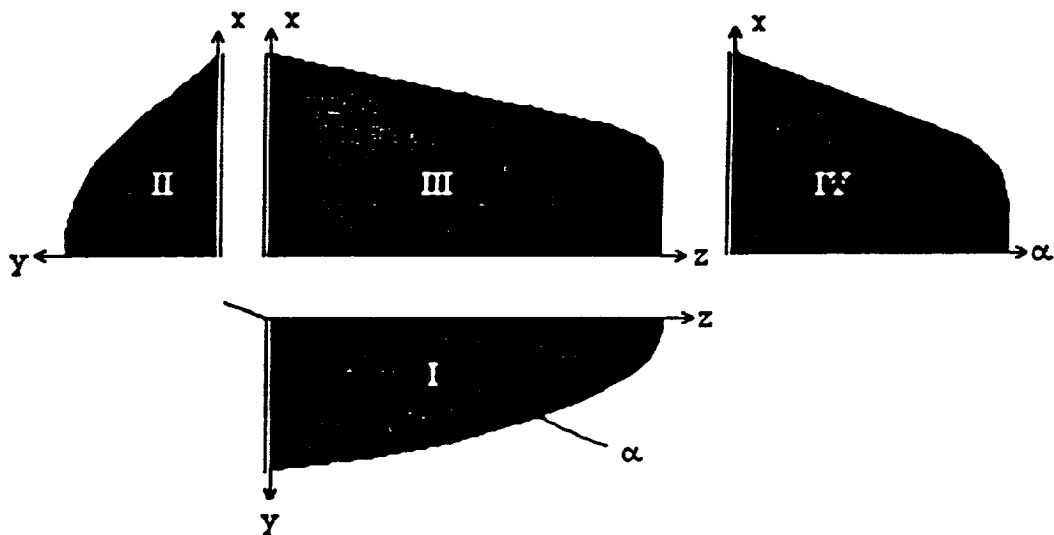
Simulation of the MIG gun whose boundaries are determined by computer bit mapping the boundaries of Fig.6. First anode potential $V_1 = 40$ kV and the final electrode potential $V_2 = 80$ KV. $B_0 = 1$ KG in the axial direction.



Boundary identification is made by bit mapping the projections of the different electrodes onto different mutually perpendicular coordinate planes.



(a)

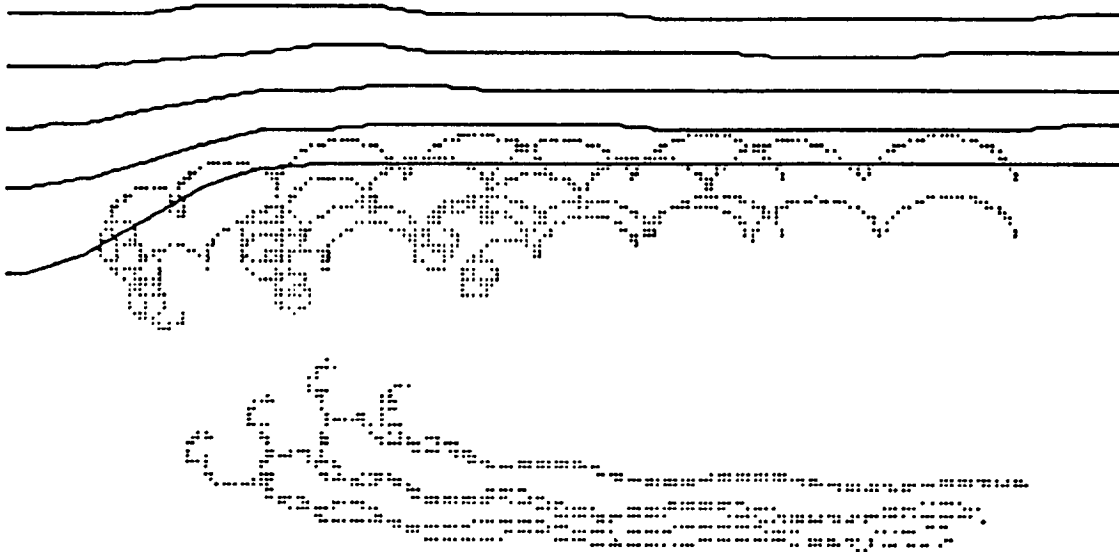
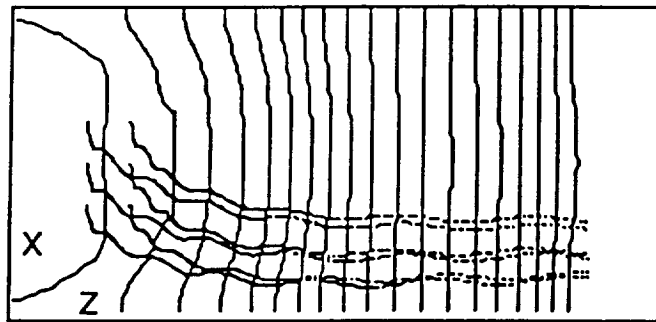
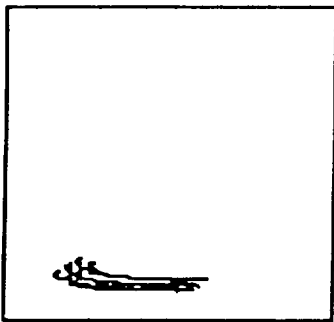
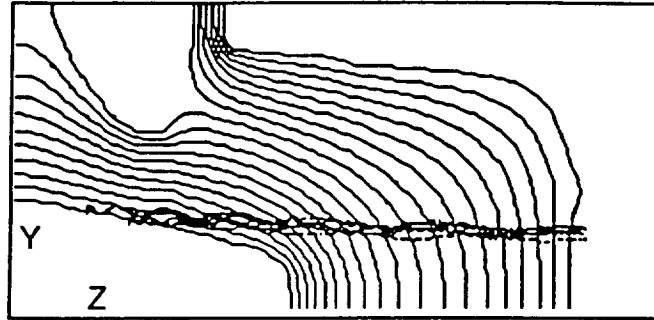
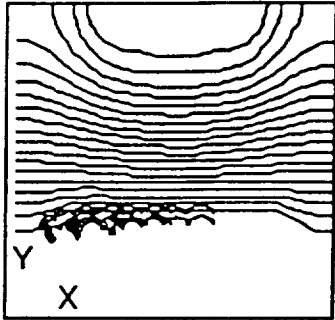


(b)

The projections of the cathode electrode at different planes. Projections I is in (y,z) plane, II is in (x,y) plane, and III is in (x,z) plane and IV is in an intermediate plane perpendicular to the (y,z) plane. Plane I is not necessary for many electrode profiles.

$X_c = -10 \text{ mm.}$
 $Y_c = -5 \text{ mm.}$
 $Z_c = 65 \text{ mm.}$

3D Electric field
 3D Magnetic field



$X_c = -10 \text{ mm}$
 $Y_c = -5 \text{ mm}$
 $Z_c = 65 \text{ mm}$

2-Dimensional Electric field
 2-Dimensional Mag. field

