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# Findings of the Joint Workshop on Evaluation of Impacts of Space Station Freedom Ground Configurations

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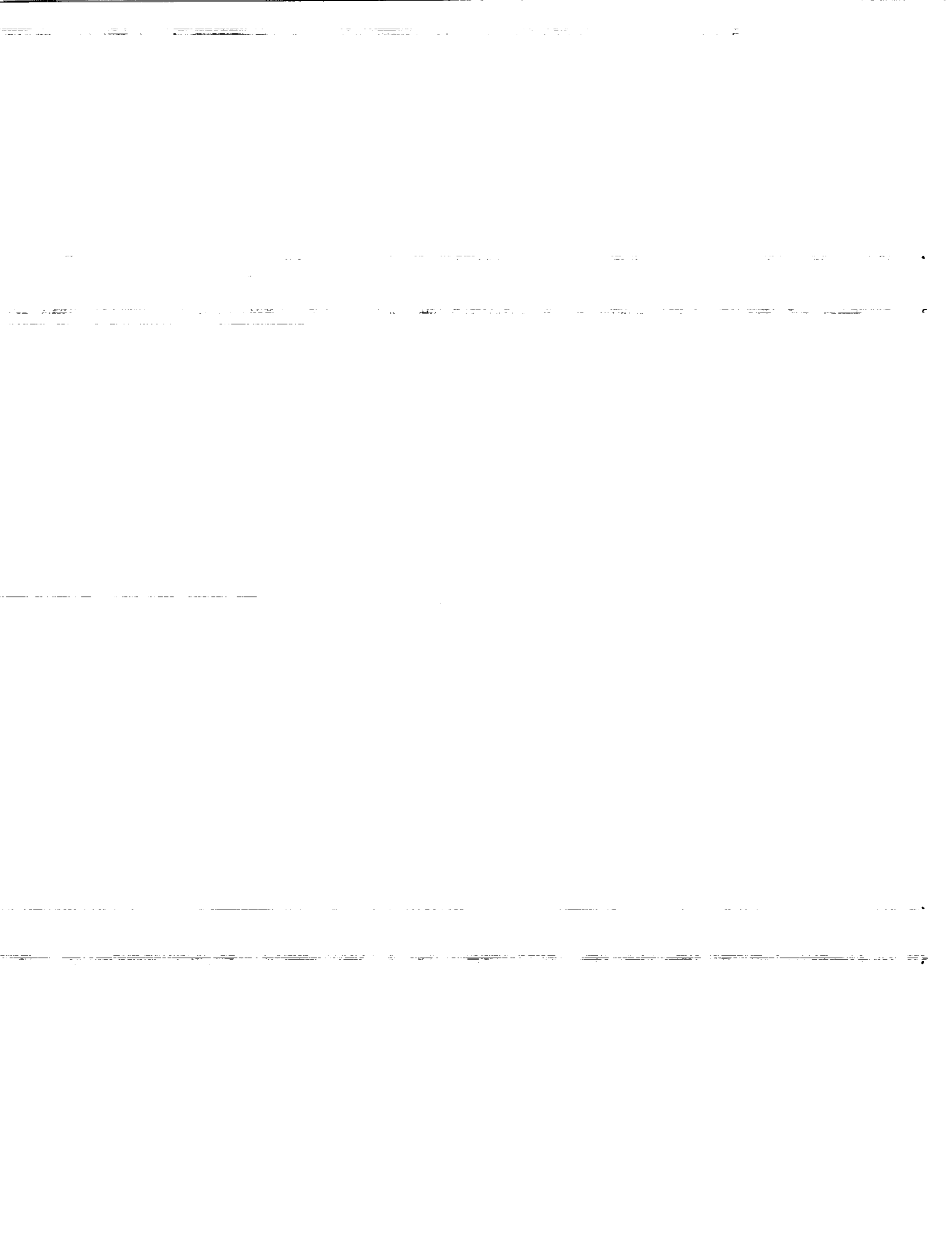
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FINDINGS OF THE JOINT WORKSHOP ON  
EVALUATION OF IMPACTS OF  
SPACE STATION FREEDOM GROUND CONFIGURATIONS

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**ABSTRACT**

A workshop to consider the effects of various proposed Space Station Freedom (SSF) grounding schemes was held at NASA Lewis Research Center May 22-24, 1990. Experts from the plasma interactions community evaluated the impacts of environmental interactions on SSF under each of three proposed grounding schemes. The choice of grounding scheme for the SSF power system was found to have important implications for SSF design. Interactions of the SSF power system and structure with the low Earth orbit (LEO) plasma differ significantly between different grounding schemes. Environmental constraints will require modification of current SSF designs under any grounding scheme. Maintaining the present negative ground scheme may compromise SSF safety, structural integrity, and electromagnetic compatibility, and will increase contamination rates over alternate schemes. Positive grounding of the array requires redesign of the primary power system. Floating the array reduces the number of circuit changes in the primary power system but adds new hardware. Maintaining the present design will affect all parts of SSF. However, no impacts were identified on SSF systems outside of the electrical power system by positively grounding or floating the array.

**INTRODUCTION:**

Interactions of spacecraft with the natural environment have been of concern ever since docking events on the Gemini space program. Since that time, much has been learned of spacecraft environmental interactions, especially as new technology has been developed and flown.

SSF represents a significant increase in spacecraft size and power levels. Old rules of thumb must be re-examined and their validity retested before applying them to the new technology. In the 1980's, with the advent of the Space Shuttle, efforts were begun to understand how large spacecraft interact with the ionospheric plasma. In 1986, recommendations were made to ground SSF to the positive side of its arrays and a positively grounded array was baselined for an AC primary power distribution system. In 1989, when the primary power distribution system changed to DC, a negatively grounded system was assumed.

This change raised concerns among plasma interactions experts who made their concerns known in meetings of the Space Station Plasma Interactions and Effects Working Group. Finally, on May 22-24, 1990, a workshop was held at the NASA Lewis Research Center to evaluate the impacts of different proposed power system grounding schemes on Space Station Freedom. Because the interactions of SSF with the ambient LEO environment would be quite different for different grounding schemes, the impacts of these interactions on the safety, weight, feasibility, operating requirements, maintenance and reliability or risk of SSF were in need of evaluation to support a decision on the SSF grounding scheme. This paper is one result of that evaluation process. An attempt was made to bring to bear all known engineering and physical facts about interactions of spacecraft with the LEO environment to evaluate the impacts of three proposed grounding schemes. An effort was made to be as quantitative as possible. This report is one step in the necessary evaluation of the environmental issues regarding SSF grounding.

The first day of the Workshop was devoted to presentations about what one might

expect in the way of grounding-related SSF environmental interactions, how they may be estimated, and what kinds of answers need to be obtained. Ground rules for the next day's calculation sessions and the basic premises of the Workshop were presented. These basic premises are repeated here:

O SSF operations and designs can be optimized by including considerations of physical processes of environmental interactions.

O In LEO, current balance will be satisfied - positive and negative collected currents must balance.

O The grounding configuration chosen for the Space Station will influence all systems.

O Our understandings of the laws of physics (models, theories, equations, empirical guidelines) are sufficient that some predictions of the interactions and their impacts may be made.

O No one wants a SSF that won't work well.

On the following days, the Workshop split up into four working groups to pull together information and to perform calculations. The topics considered by the four working groups were:

1. Floating potentials and ground currents,
2. Atomic oxygen, sputtering, materials degradation and contamination,
3. Corona, arcing, and insulation,
4. Arc rates and effects, EMI, and Kapton pyrolyzation.

Results of their deliberations are reported in this paper.

#### SPACECRAFT/PLASMA INTERACTIONS BACKGROUND:

The ionospheric plasma in LEO is conductive. Any spacecraft placed in this environment will come to an equilibrium potential relative to the plasma such that no net current is collected. If the spacecraft has a distributed voltage (e.g. an illuminated solar array) which permits currents to be collected from the plasma, then part of the spacecraft will be positive relative to the plasma potential (defined as zero volts), collecting electrons, and the rest will be negative relative to the plasma, collecting ions. The electrons are very light, mobile, and easily collected. The ions are massive, slower moving, and difficult to collect. Therefore, the total spacecraft voltage relative to the plasma will be such that most of its area will be negative with respect to the plasma potential and only a small part will be positive. Figure 1 illustrates these points. It also shows that if a spacecraft structure is grounded to the positive side of the solar array then it will be near zero volts because its surface area adds to the surface area which can collect electrons. If the spacecraft is grounded to the negative side of the solar array it will be driven negative by most of the array-generated voltage. Many experiments on the Space Shuttle and free-flying LEO spacecraft verify these concepts.

In the past, these effects have been seen on spacecraft in LEO conditions, but the voltages and spacecraft sizes were sufficiently small that they only had to be considered in correcting and interpreting results of scientific experiments. However, the physical size and voltage level of the SSF power system require that plasma effects be considered in the design.

#### BASIC CONSIDERATIONS ABOUT THE SSF POWER SYSTEM:

The purpose of this workshop was to investigate the consequences of various grounding schemes. Details of the power system are discussed in reference 1. With this background three possible grounding configurations were identified.

Although additional configurations are possible, their consequences are covered in this set, and they may be less practical.

The first configuration identified has the solar array grounded with the primary power distribution on its negative side and the secondary power distribution also grounded on the negative side. This is the concept presently being used to design the power distribution system [Fig. 2].

If the structure is grounded to the negative side of the array, the structure/array will float nearly the entire array voltage negative in the daytime (about -150 to -130 V negative of the ionospheric plasma). This is to balance the positive ion collection by the structure and array with the electrons collected by the array [Figure 2]. At night, when no voltage is generated by the array, the structure will be near plasma potential.

The second configuration grounds the array and the primary power system positive, and grounds the secondary power distribution negative. The ground reference would change sign across the transformer in the DC to DC Converter Units (DDCUs). The primary power distribution system would have positive referenced circuitry [Fig. 3].

With the structure grounded to the positive side of the array, the positive structure is electron collecting, while nearly the entire array must be ion collecting to balance this [Figure 3]. As a result the structure is only slightly positive relative to the plasma. However, the negative side of the array now floats nearly 160 V negative relative to plasma.

The third configuration would float the solar arrays and negatively ground both the primary and secondary power distribution systems. For this configuration a DDCU would have to be added outside the alpha joint, either in the DC Switching Unit (DCSU) or just after the Sequential Shunt Unit (SSU). This requires an additional DDCU for each solar array mast. Such a DDCU would have different requirements than the DDCUs which convert to the secondary power system and, in general, will not be interchangeable. This would permit most of the power distribution circuitry to have a negative ground. But the SSU and some support circuitry might need to be grounded separately and electrically isolated from the rest of the system [Fig. 4].

A floating array would permit the array to float relative to plasma, and permit the structure to float near plasma potential [Figure 4]. This option combines some environment interactions advantages with a slightly reduced arc probability due to the slightly more positive floating array.

#### IMPACTS OF THE THREE GROUNDING SCHEMES ON SSF:

Some of the relevant effects of these configurations are presented in matrix form in Table I. This table gives both advantageous and disadvantageous impacts. Additional details of the impacts, the methods used to quantify and evaluate them, and detailed recommendations for implementing the different grounding schemes can be found in reference 1.

#### SUMMARY:

All identified grounding schemes create technical issues that may affect SSF costs and/or schedule. The problems arise for a variety of reasons and involve design changes to accommodate identified problems in the current design or to accommodate the alternate grounding schemes and are discussed below. References and relevant calculations may be found in reference 1.

##### Present design (Negative Ground):

The present design grounds all systems negative, and ties the ground to the

negative side of the array. This will cause SSF ground and structure to float 130 to 150 V below plasma. Safety concerns are raised because of the 140 V difference between SSF and free flying bodies such as the docking of Shuttle or astronauts on EVA. Interlock mechanisms may be required to prevent thruster firings or venting events while these other bodies are connected to or touching SSF for such events will cause currents through the spacecraft body or the Extravehicular Mobility Unit (EMU) of about 10 amps. Alternatively, active charge control systems (hollow cathodes or other plasma contactors) could be used to limit potentials. However, these will increase the plasma density around the entire SSF and will exacerbate other interactions (such as array current collection).

Arcs are likely to occur on the structure. The present anodized surface will break down under the electric field imposed on it. Arcs will be triggered by micrometeoroid impacts, but their characteristics are unknown. Arcs analogous to solar array arcs may occur on the structure.

Erosion rates of the SSF structure may be increased due to sputtering by ions accelerated by the -140 V structure potential to holes in the anodization that may be caused by dielectric breakdown or debris impacts. This may compromise the structural integrity of the trusses in from five to thirteen years.

Large currents that violate present EMI requirements are likely. In addition to the solar array related currents, a current of about one Ampere DC is expected because of leakage currents through the structure anodization. This will increase over the lifetime of SSF. Voltage transients of 160 V and current transients of about 10 Amps are expected during thruster firings. During arcs, similar voltage swings and transient currents up to 100 Amps may occur. Additional shielding may be required for equipment.

Finally, contamination rates on solar arrays, thermal coatings, and optics will be increased with increased sputtering of the structure.

#### Positive ground:

In order to ground the solar array and primary power distribution positively while maintaining negative ground on the secondary power system, a redesign of the primary power distribution system is required. Either NPN technology must be replaced with PNP technology or circuits must be more complicated. Also the DDCUs will need minor modifications for their insulation to survive increased corona occurrence, as will multiwire connectors. Solar array arcs have a slightly higher risk of occurring because of the -160 V maximum negative potential rather than the -140 V on the negative grounded system. The sputtering problem on the solar arrays will be slightly increased.

#### Floating:

In order to float the array, new hardware will be needed. New additional DDCUs will be required. These DDCUs will not be parts-compatible with the other DDCUs because they must tolerate higher voltages, higher power levels, and higher corona levels.

#### Summary of impacts:

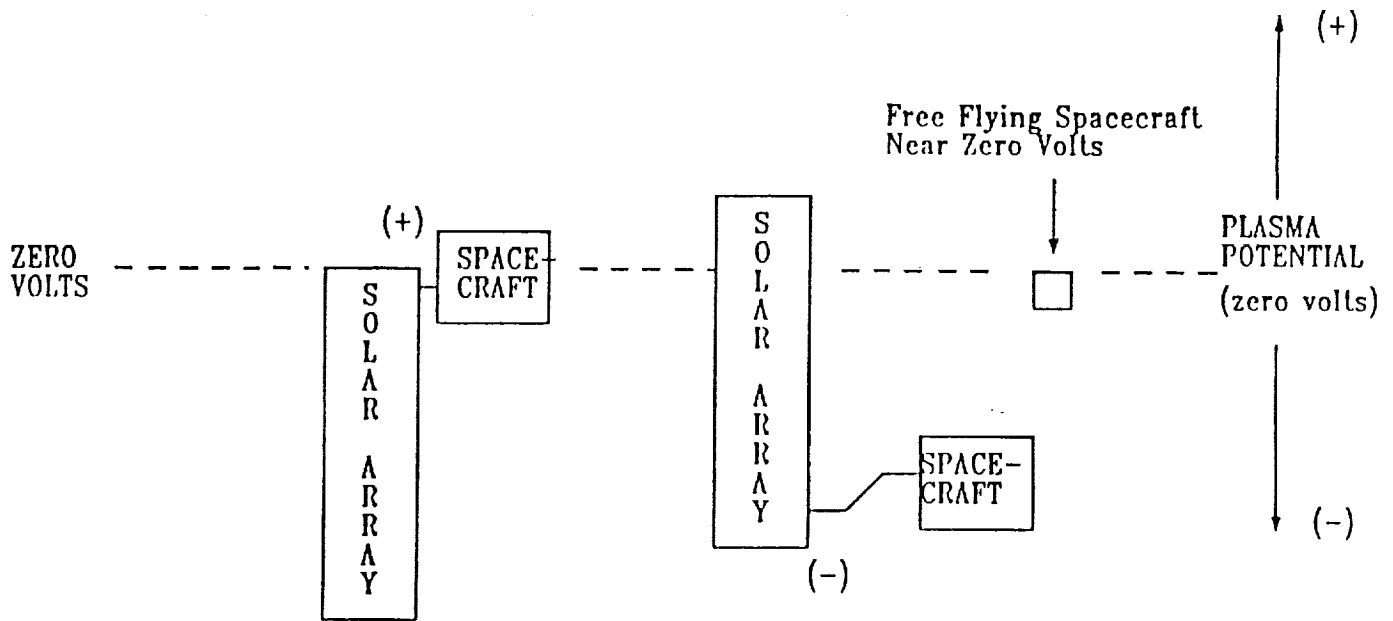
Environmental constraints suggest modification of present SSF designs. Maintaining the current grounding scheme may compromise safety, structural integrity, electromagnetic compatibility, and will increase contamination rates. Positive grounding of the array requires reworking of the primary power system. Floating the array reduces the number of circuit changes but adds new hardware. Maintaining the present negative ground design will affect all parts of SSF. However, no impacts were identified on SSF systems outside of the electrical power system by positively grounding or floating the array.

REFERENCES:

1. Ferguson, D.C., Snyder, D.B., and Carruth, R., *Report of the Joint Workshop of the Space Station Freedom Plasma Interactions and Effects Working Group, the Space Station Freedom Plasma Working Group, and the Space Station Freedom EMI/EMC and Electromagnetic Effects Working Group on Evaluation of Impacts of Space Station Freedom Grounding Configurations, May 22-24, 1990, in publication.*

TABLE I. PRIMARY POWER GROUNDING CONFIGURATION ASSESSMENT

CONFIGURATION	IMPACTS	ADVANTAGEOUS IMPACT	DISADVANTAGEOUS IMPACT
	Modules/Truss grounded to negative end of solar array (current design approach - see Fig. 2)	<ul style="list-style-type: none"> <li>o -140 V vs -180 V max potential on solar array with respect to plasma (a minimal advantage)</li> </ul>	<ul style="list-style-type: none"> <li>o All Work Packages impacted by plasma effects</li> <li>o Safety (EVA/Docking) compromised by induced voltages and 10 amp current through EMU vents</li> <li>o Thermal control materials must be re-evaluated, redesigned or substituted</li> <li>o Truss structure seriously questionable in 5-13 years</li> <li>o Large plasma-induced currents and voltages to be accommodated</li> <li>o Contamination increased by sputtering</li> <li>o Conducted EMI requirement not met</li> </ul>
	Modules/Truss grounded to positive end of solar array (see Fig. 3)	<ul style="list-style-type: none"> <li>o Module/Truss voltage near plasma potential eliminates structural sputtering, insulation req.</li> <li>o Thermal coatings: no change</li> <li>o Minimum plasma/structure current</li> <li>o No new EVA/Docking safety problems</li> <li>o Keeps impacts &amp; redesign issues in a single Work Package</li> </ul>	<ul style="list-style-type: none"> <li>o 280 V vs 180 V maximum DC potential in power connectors to DDCU</li> <li>o Redesign of DC-DC Converters required</li> <li>o Corona design requirements increased in DDCU</li> <li>o Redesign of primary power control circuitry</li> </ul>
	Modules/Truss floating with respect to solar array (see Fig. 4)	Same as above	<ul style="list-style-type: none"> <li>o Corona design requirements slightly increased in new, additional DDCU</li> <li>o Design new DDCU (180 V to 160 V)</li> <li>o Redesign of solar panel power control circuits</li> </ul>



- Spacecraft Near Zero Volts
- Only Solar Array Must Consider Plasma Effects
- Spacecraft Negative and Must Consider Plasma Effects
  - Sputtering and Arcing
  - Docking and Safety
  - Structure Currents and EMI

Figure 1. How a spacecraft with High Voltage Solar Arrays floats in the plasma.

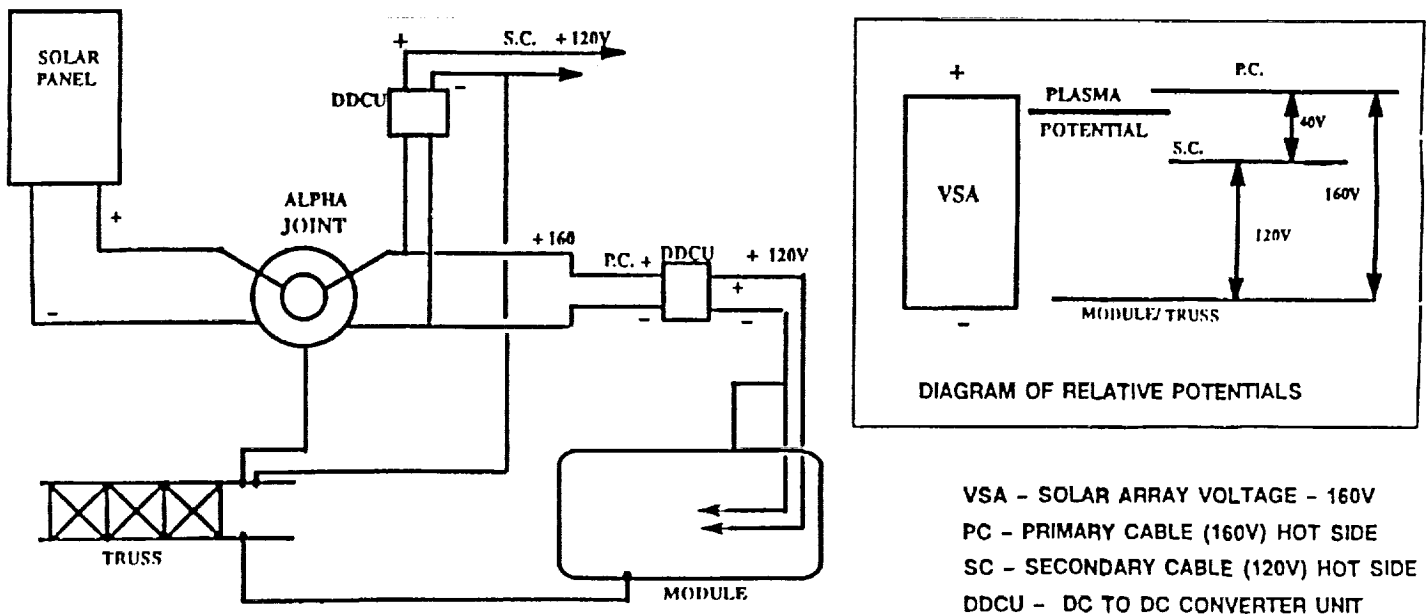
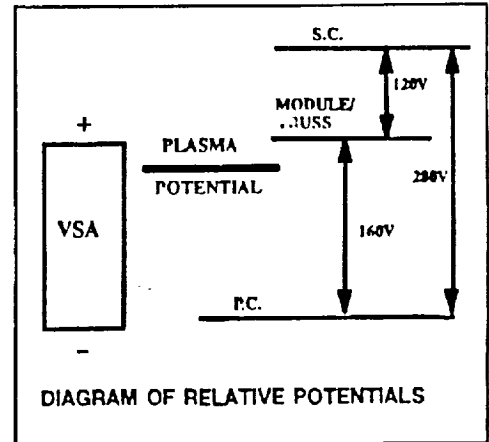
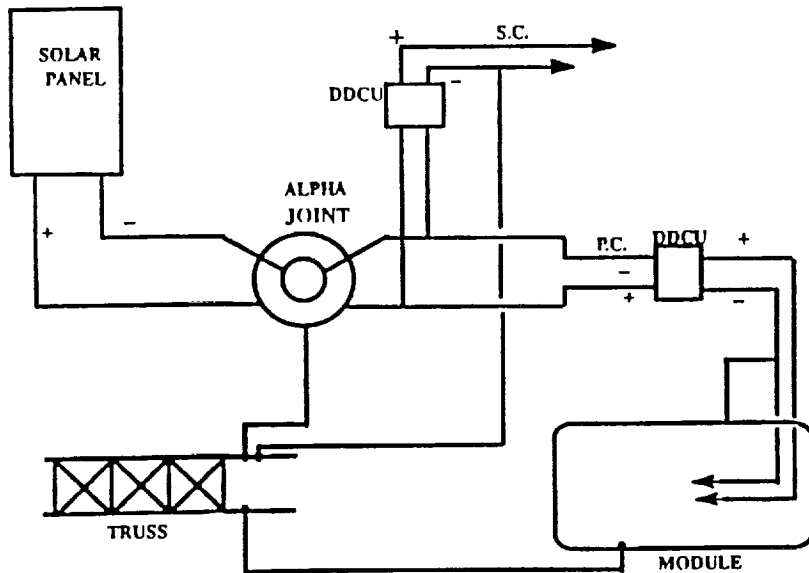


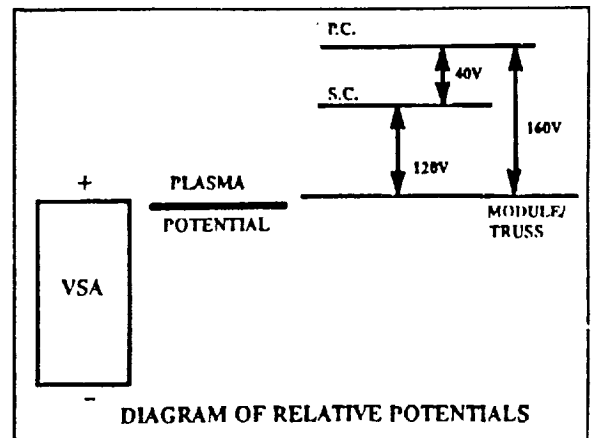
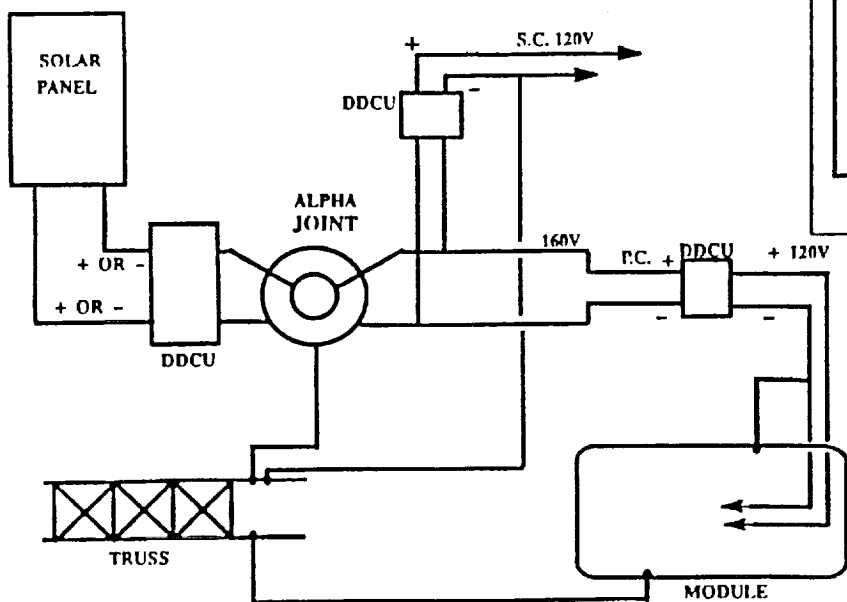
Figure 2. The presently baselined SSF Negative Ground Configuration.





VSA - SOLAR ARRAY VOLTAGE - 160V  
 PC - PRIMARY CABLE (160V) HOT SIDE  
 SC - SECONDARY CABLE (120V) HOT SIDE  
 DDCU - DC TO DC CONVERTER UNIT

Figure 3. A Positively Grounded Solar Array with Negatively Grounded Secondary.



VSA - SOLAR ARRAY VOLTAGE - 160V  
 PC - PRIMARY CABLE (160V) HOT SIDE  
 SC - SECONDARY CABLE (120V) HOT SIDE  
 DDCU - DC TO DC CONVERTER UNIT

Figure 4. Floating the Solar Array and Negatively Grounding the Secondary Power.



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