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FINAL REPORT ORBIT TRANSFER ROCKET ENGINE TECHNOLOGY PROGRAM

AUTOMATED PREFLIGHT METHODS CONCEPT DEFINITION TASK E.7

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| Or the religing preling in equirements were defined and a range of possible preflight methods were proposed. Critical issues and benefits were also identified for each method and technology readiness and development costs addressed. It would be advantageous in a space based setting to minimize or entirely eliminate preflight engine checkouts requiring manual/extravehicular interaction with the hardware. Extravehicular activity not only introduces added safety risks for the astronauts, but is extremely costly. In this study the possibility of automating these checkouts was investigated. The minimum requirements in terms of information and processing necessary to assess the engine's integrity and readiness to perform its mission were first defined. A variety of ways of remotely obtaining that information, spanning a range of method sophistications were then generated. The sophistication of these approaches varied from a simple preliminary power up, where the engine is fired up for a short time, to the most advanced approach where the sensor and operational history data system alone indicates engine integrity. The critical issues and benefits of each of these methods were also identified, outlined, and prioritized. The technology readiness of these automated preflight methods were then rated on a NASA Office of Exploration Scale used for comparing technology options for future mission choices. Finally estimates were made of the remaining cost to advance the technology for each method to a level where the system validation models have been demonstrated in a simulated environment. | | | | |
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FOREWORD

The work reported herein was conducted by Advanced Programs and Engineering personnel of Rocketdyne, a division of Rockwell International Corporation, under Contract NAS3-23773 from December 1989 to April 1991. M. Millis, Lewis Research Center, was the NASA Project Manager. Mr. R. Pauckert was the Rocketdyne Project Manager, and T. Harmon was the Project Engineer. A. Martinez was responsible for the technical direction of the effort while C. Erickson, D. Hertzberg, K. Kramer, C. Meisl, and N. Gustafson made important technical contributions to the program. Secretarial support was provided by D. Senit.

INTRODUCTION

A space based chemical propulsion system capable of multiple starts and varied mission scenarios will require extensive preflight checkouts to assure crew safety and mission success. An automated approach for a space based system is highly desirable from the standpoint of feasibility. Performing preflight checkouts manually using modified ground-based techniques would require costly EVA and result in prohibitively high mission costs while also compromising reliability and safety.

Approaches to automating preflight readiness checkouts depend heavily on condition monitoring technology to provide the information required to assess the engine's readiness to fire. Condition monitoring sensors permit remote monitoring of critical components as the engine fires during normal operation. Based on the flight data obtained from these sensors, an assessment can be made on the condition or health of a particular component which in turn dictates the need for maintenance procedures or replacement.

OBJECTIVES

The objective of this study is to suggest and evaluate various methods of preflight readiness checkouts in the context of a space-based system. Where required, methods will incorporate advanced Integrated Control and Health Monitoring (ICHM) technologies enabling rapid and remote engine turnaround. Specific objectives of this task as defined by five separate subtasks in the statement of work (SOW) are summarized in Table 1.

SUMMARY OF ACCOMPLISHMENTS

Preflight readiness verification requirements were established for the engine. Requirements were based on previous logistics studies including the preliminary failure modes and effects analysis (Ref. 1) and the flow task analysis report. This report was generated in support of a prior NASA technology task (Ref. 2) to establish the operational flow of the engine and identify the applicable maintenance tasks for both current and advanced technologies. The operational flow tasks of interest to this study are those executed after delivery to the space station and before return to earth. Maintenance tasks were reviewed in light of the SSME



- Specify OTV engine preflight requirements.
- Suggest a range of possible preflight methods.
- Identify critical issues and benefits for each method.
- Estimate technology readiness for each method.
- Estimate the remaining development cost for each method.

Operations and Maintenance Requirements and Specifications Document (OMRSD - Ref. 3) which reflects the current inspection and checkout philosophy evolving from the Challenger incident. Thirty six preflight readiness verification requirements were identified for the engine. Requirements include 14 functional checks, 10 leak checks, 10 inspections, and 2 servicing tasks.

Several approaches for remotely performing readiness checkouts in space were outlined for each preflight requirement. The range of approaches reflect a variety of method sophistications. Three approaches for remotely obtaining data were considered -Preliminary power-up in which the engine is fired for a short time to acquire real time data, Automated component pre-cycling in which engine components are cycled in an inert gas medium to assess component integrity without hot firing the engine, and Automated static checkout in which an analysis of historical data and static checks are used to assess the engine's readiness to fire without the cycling of any components.

Where practical, alternate component designs were suggested to reduce criticality of component failure and hence delete or simplify preflight readiness requirements. This was particularly useful in the case of the Lox/H2 heat exchanger, in which a robust design was suggested to reduce the possibility of failure and eliminate the need for leak checks. Alternate designs were also suggested for the turbopump bearings and combustion/propellant systems joints.

Issues and benefits were generated for applicable preflight checkout approaches. Sensors and flight hardware, alternate component designs, and individual approaches were addressed separately. Issues and benefits were categorized into space basing, vehicle/infrastructure, and engine system impacts.

The technology readiness levels of the three preflight checkout methods were also evaluated. The scale used for comparing the methods was that used by the NASA office of exploration for evaluating options for future mission choices.

Estimates were also made for the remaining cost to advance the technology for each method to a level where the system validation models have been demonstrated in a simulated environment.

TECHNICAL DISCUSSION

SUBTASK 1 - Specification of Engine Preflight Requirements

Subtask 1 entailed the definition of the preflight readiness verification requirements for a space based engine. These requirements are the information and processing necessary to access the engine's integrity and readiness to perform its mission. The preflight requirements were generated by review and update of several completed studies. One of the primary sources was a similar study conducted under the Orbit Transfer Rocket Technology Program contract in 1987. In a subtask of the Advanced Engine Study (Ref. 4), maintenance and verification checks were identified for the space based engine.

In that effort a review of the Space Shuttle Main Engine (SSME) operations and maintenance manual was conducted with two purposes in mind: (1) to begin to outline the overall maintenance procedures for the engine, and (2) to identify technology requirements for streamlining space based operations. The original SSME document contained the requirements and specifications for the SSME at the organizational level (installed engines). Routine maintenance requirements (after each engine firing), periodic maintenance requirements (time/cycle oriented), and contingency requirements (unscheduled to isolate/rectify a condition) were covered.

It was then determined whether the individual tasks would be affected by an advanced integrated control and health monitoring (ICHM) system incorporating advanced sensors.

In order to update and expand the work completed under the Advanced Engine Study, additional documents were reviewed and integrated into the current study. These documents included:

- a. Operation and Maintenance Requirements and Specifications Document (OMRSD) for processing the SSME during STS launch operations at KSC. This OMRSD reflects the current inspection and checkout philosophy evolving from the Challenger incident (Ref. 3)
- b. RL10 Liquid Rocket Engine Service Manual prepared by United Technologies, Pratt and Whitney Aircraft Group (Ref. 5)

- c. Preliminary Failure Modes and Effects Analysis (FMEA) for the OTVE (Ref. 1)
- d. RL10 FMEA for Apollo missions (Ref. 6).

The results of this review constitute a current baseline list of preflight requirements. These redefined requirements for the engine in an operational space environment are presented in Table 2. These requirements are primarily based on Criticality 1 failure (major uncontained damage to an engine subsystem or component resulting in widespread engine damage) and Criticality 2 failure (significant contained damage to a vital engine subsystem or component sufficient to render it inoperative or its continued operation hazardous) modes identified in the OTVE FMEA.

Table 2 lists the preflight requirements to be performed between each engine start and also those requirements that are to be performed periodically at an interval to be determined as designs mature. The periodic requirements are those associated with damage, erosion, etc., that will propagate with time.

A total of thirty-six checkouts falling into four separate categories were identified. These included fourteen functional checks, ten leak checks, ten inspections, and two servicing tasks.

After a review of the available documentation, it was determined that additional information is required in order to substantiate the need for, or the possible deletion of, some of the requirements. These areas of concern are:

- (a) Hazards associated with simultaneously leaking hydrogen and oxygen in a space environment; how quickly do propellants dissipate in a space environment, and what combination of leakage rates constitute a hazardous combustible mixture? Additionally, some leak test requirements may be mission dependent; i.e., because of the possibility of hydrogen and oxygen combustion, more in-depth leak tests should be performed for engine starts in close proximity to the engine docking facility, than in a free space environment.
- (b) More information is needed on the dissipation characteristics of water in a spacebased environment to support the engine drying requirements listed in Table 2.
- (c) More information is needed on the probability of damage from debris, etc. in orbit and on the protection the vehicle affords the engine relative to encapsulation.

| | OTV Pr | eflight Requirements |
|-------------|---|---|
| | Functional Checks | Inspections |
| | Valve Actuator Check | 1. Exterior of Components for Damage/Security, etc. |
| Ś | Sensor Checkout/Calibration | 2. T/C Assembly for Evidence of Coolant Passage Blockage |
| ų | Pneumatic Component Checkout | 3. HPFTP Turbine Wheel/Blades for Cracks, Fatigue, and Damage |
| 4 | Operational Sequence Test (FRT) | 4. HPOTP Turbine Wheel/Blades for Cracks, Fatigue, and Damage |
| ы. | Control System Redundancy Verification | 5. LPFTP Turbine Wheel/Blades for Cracks, Fatigue, and Damage |
| Ô. | Controller Memory Verification | 6. LPOTP Turbine Wheel/Blades for Cracks, Fatigue, and Damage |
| Υ. | Contoller Pressurizatiion Verification | 7. HPOTP Bearings for Damage |
| œ | HPOTP Torque Check | 8. T/C Assembly Injector Faceplate, Igniter, and Lox Post Tips for Erosion, |
| ю. | HPFTP Torque Check | Burning, and Contamination. |
| 1 0. | LPOTP Torque Check | 9. Gimbal Bearings and TVC Attach Points for Evidence of Bearing Seizure |
| Ξ. | LPFTP Torque Check | and Fatigue. |
| 12. | Turbopump Axial Shaft Travel Check | 10. Heat Exchanger for Cracks, Evidence of Wear, and Damage |
| 13. | Extendible Nozzle Travel Check | Leak Checks |
| 14. | Igniter Operation | 1 HPOTP Primary I ox Seal |
| | Servicing Tasks | 2. HPOTP Lox/Turbine Drive Gas Seal |
| | | 3. Oxidizer Inlet Valve and MOV Ball Seals |
| | | 4. Fuel Inlet Valve and MFV Ball Seals |
| <u>.</u> | | 5. Propellant Valves Primary Shaft Seals |
| | a. iginter valves | 6. Pneumatic Control Assembly Internal Seals |
| | D. PC Jelisors | 7. Heat Exchanger Coil Leak Test |
| N | HPOTP Lox/Turbine Drive Gas Seal Pre-Start Purce | 8. Heat Exchanger Coil Proof Test |
| | | 9. Thrust Chamber Assembly Outer Walls |
| | | 10. Combustion and Propellant System Joints |

(d) Criticality assignments in the FMEA (Ref. 1) dated 2-22-85 should be reviewed/revised to reflect the current philosophies established after the Challenger incident. (Refer to the SSME FMEA).

This information may be acquired through quantitative modeling (i.e., item a), or by performing additional qualitative studies. Acquiring this information was beyond the scope of this task. Nevertheless, it is recommended that these issues be studied in subsequent tasks since they could impact the development and operation of the ICHM system.

Additional documentation substantiating these conclusions is presented in Appendix 1 and include:

Part A - Lists the SSME OMRSD and/or the OTVE FMEA failure mode references that were used to establish pre-flight requirements.

Part B - Defines the FMEA failure mode criticality assignments.

Part C - Comprehensive list of SSME OMRSD currently used to process the SSME/Shuttle at KSC and alternate landing sites. Entries in the column marked "OTV APPLIC - FUTURE" will be made after the engine component design becomes more firm.

Part D - Summary of RL-10 prelaunch checks extracted from the RL-10 service manual. It is assumed that these requirements are for ground launch activities and are for unmanned launch operations. This document was superficial and did not contain sufficient detail to influence the preflights methods study. The summary is provided for information only.

SUBTASK 2 - Generation of Range of Possible Preflight Methods

Introduction

The objective of Subtask 2 was to generate automated methods to accomplish the preflight checkouts identified in Subtask 1. Three sets of methods were generated, each reflecting a checkout philosophy which progressively relies on more ICHM monitored status checking of the component and system physical status, and less on component dynamic functional tests. The three levels of ICHM sophistication are reflected in the means by which the required data are remotely obtained. The methods include the following:

- (1) Preliminary power-up where the engine is fired for a short time (tankhead idle and a brief transition to pump idle). This represents the lowest level of ICHM sophistication.
- (2) Automated component pre-cycling where critical portions of the engine are physically cycled and monitored (such as pressurizing lines and spinning turbopumps). This represents an intermediate level of ICHM sophistication.
- (3) Automated static checkout where the sensors and operational data history are sophisticated enough to indicate engine integrity and readiness to fire without the need to cycle any part of the engine. This is the ultimate goal for preflight checkouts.

Preliminary Power-up

The preliminary power-up technique assumes required information is obtained through system operation. System conditions during the preliminary power-up phase permit detection of critical failures without catastrophic results, and subsequently permit safe shutdown of the engine. However, stress and pressure related potential failures might not be detectable. The engine system modes of operation which occur as part of the preliminary power-up phase include prestart, engine start, tank head idle, and pump idle mode. A brief description of each mode is provided below.

(1) Prestart: The controller performs a self-test and checkout of the ICHM. At the end of this phase, system temperatures are checked to assure that conditions are normal for engine start. A start-enable signal is sent to the vehicle.

- (2) Engine Start: The inlet valves are opened and propellants dropped to the main valves. The main fuel valve (MFV) is then opened. Hydrogen flows through the system, vaporizes, and enters the main injector. The gaseous oxidizer valve is then opened to circulate oxygen through the GOX heat exchanger and into the main injector. The igniter valves are then opened, the igniter sparks, and ignition is established in the augmented spark igniter. This initiates Tank Head Idle mode.
- (3) Tank Head Idle: Operation continues chilldown to thermally condition the engine system and provide some passive regulation of mixture ratio swings via H2 to O2 heat transfer. Transition to the next phase, pump idle mode, is determined by the appropriate component and propellant feed temperatures.
- (4) Pump Idle: Transition to pump idle begins as the controller opens the turbine shutoff valve. The main oxidizer valve (MOV) is ramped open approximately 40%. The oxidizer turbine bypass valve (OTBV) and the turbine bypass valve (TBV) are ramped closed 92% and 85% respectively. Closure of the turbine bypass valves increase hydrogen flow through the turbines which initiates pumping. The high pressure oxidizer pump discharge pressure rises and the gaseous oxidizer valve (GOV) is closed. Gaseous hydrogen and oxygen pass through the fuel tank check valve (FTCV), and the oxidizer tank check valve (OTCV) to the respective tanks elevating tank pressure and NPSH. The injector primes and combustion boosts the vaporization rate of the fuel in the cooling jacket providing additional power to the turbines. At the appropriate chamber pressure (approximately 8%), the controller initiates active control of mixture ratio and chamber pressure.

Advanced Design Recommendations

While determining preflight checkout methods, the possibility of deleting certain checkouts by incorporating advanced designs was considered. Advanced design features which may be available for proposed missions include hydrostatic bearings, which exhibit negligible wear, and welded joints, which reduce the overall number of leakage paths. A more complete list of advanced design recommendations is presented in Table 3. These features were not included in the OTVE preliminary design.

Advanced Design Features Recommended To Simplify Preflight Checkouts

- Welded engine system with the exception of inlet/outlet turbopump interface joints
- Robust heat exchanger design -Seamless heat exchanger design
- Robust thrust chamber design
- Hydrostatic bearings
- Addition of labyrinth seals and more durable seal materials to minimize seal wear and leakage

Sensors

The type and projected availability of sensors had a significant impact on the preflight checkout methods which were ultimately recommended. Where applicable, both current and advanced sensors were considered in the various approaches. Current ICHM sensor requirements were defined in the concurrent Task E.6 - ICHM Definition study (Ref. 7). These current ICHM measurements identified in E.6 are presented in Table 4.

Advanced sensor availability for the Lunar and Mars missions is shown in Table 5. Advanced sensors for the engine were determined in an earlier technology task (Advanced Engine Study Task D.1/D.3, Jan. 1986 - Ref. 8). Advanced sensor availability may also impact the nature of the checkout itself. For example, in the case of turbine wheel/blade inspection, remotely obtained blade fatigue data coupled with a life prediction model and trend analysis form the basis for an assessment of turbine condition. This differs from a manual boroscopic inspection which requires disassembly and does not lend itself to simple automation.

Groundrules and Assumptions

The groundrules as specified by NASA in the contract were:

- (1) Hydrogen/oxygen expander cycle
- (2) Space based
- (3) Man Rated
- (4) Designed for 100 starts/4 hours of operation (safety factor = 4)
- (5) No EVA available for preflight checks
- (6) Start cycle tankhead start (providing propellant settling and chilldown of components for thermal conditioning), pumped idle operation required for autogeneous tank pressurization
- (7) Preflight Checkout Technology development to readiness level 6

Current Technology ICHM Measurements

- Static Pressure
- Static Temperature
- Flow (Turbine flowmeter)
- Speed
- Modulating Valve Displacement (continuous)
- Shutoff Valve Displacement (on/off)
- Acceleration

Table 4

| | | aviiry |
|---|-------------------------------|-------------------------------|
| | Availabi | lity* |
| Advanced Sensor/Hardware | Technology Level 6 by 1996 | Technology Level 4 by 1996 |
| Ultrasonic Mass Flowmeter | × | |
| Fiberoptic Deflectometer | × | |
| Optical Leak Detection System | × | |
| Exo-Electron Fatigue Detector | | × |
| Isotope Wear Detector | × | |
| Plume Spectrometer | × | |
| Ferromagnetic Torque Meter | × | |
| Automated Visual Inspection | × | |
| * Based on current and projected funding levels | | |

Advanced Instrumentation Availability

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Table 5

Additional groundrules adopted which were not specifically stated in the contract were:

- (1) The following launch scenarios were applicable:
 - (a) Space station
 - (b) Lunar surface
 - (c) Martian surface
 - (d) Planetary orbit selected as most stringent
- (2) Engine system assumptions:
 - (a) Valves are electrically actuated with redundant motors
 - (b) Pneumatic system consists of LOX pump intermediate seal purge and injector shutdown purge

The OTV preliminary design incorporated an intermediate seal purge on the MK-49 Lox turbopump. The purpose of this purge is to assure that no intermixing of the GH_2 and Lox occur, thus preventing potentially dangerous combustible mixtures from forming. The injector shutdown purge is performed to expel any residual propellants from the injector and combustion chamber. This process also is to prevent the accumulation of a potentially explosive mixture. In a space based setting, the residual propellants would most likely diffuse rapidly to the surrounding vacuum of space. A detailed design and mass transfer analysis need to be conducted to verify this preliminary conclusion.

Methods

The approach taken in subtask 2 was to generate a range of preflight methods expanding the NASA suggested approaches into a detailed matrix to satisfy all preflight requirements. Based on the range of approaches, a preliminary recommendation of a particular approach for performing each check was made. Several advanced design concepts were also identified and are recommended to possibly reduce the number of checks. Sensors required for the preflight checkout approaches were identified and a preliminary assessment was made on the availability of sensors. A detailed table of the approaches developed in this subtask is presented in Appendix 2. The table in this appendix includes the approach for each of the three methods as applied to each preflight check required, the current and advanced hardware if needed, the recommended approach, and comments. A condensed version of Appendix 2 is provided in Table 6. This summary presents the preflight checks required and the recommended approach for accomplishing them.

A brief overview of the individual preflight checks will now be provided.

Functional Checks

Of the 14 checks specified, eight are currently automated and in use on operational engine systems and require little additional technology for implementation. Most are static checks which are driven by software. Precycling of valve actuators is necessary to assure system integrity. These engine valves are cycled before the upstream propellant shutoff valves at the exit of the supply tanks have been opened. Therefore, no propellant flow is required for this functional check.

Torque checks for all pumps can be performed in a similar manner using the automated component pre-cycling approach. Because of the extremely small breakaway torque values, this check may require the development of highly accurate sensors and special checkout procedures.

The turbopump axial shaft travel check may be substituted with other means of determining bearing health such as data from the bearing vibrational spectrum to indicate wear. There is also a possibility of deleting this check based on the use of hydrostatic bearings.

The extendible nozzle travel check will rely on data from any nozzle deployment/retraction during a previous mission. This is to avoid any additional cycling which may cause undue wear to the actuator mechanism.

Leak checks

Turbopump and valve seal leakage can be monitored in flight with pressure transducers at the seal drain cavities. Leakage past valve ball seals can be monitored with external skin temperature sensors located just downstream of the ball. Valve shaft seal leakage can be monitored through the port just beyond the dynamic shaft seals.

| Preflight Checks and Recommended Methods | | |
|--|---------|--|
| Functional Checks | Method* | |
| 1. Valve Actuator Check | В | |
| 2. Sensor Checkout/Calibration | с | |
| 3. Pneumatic Component Checkout | С | |
| 4. Operational Sequence Test (FRT) | В | |
| 5. Control System Redundancy Verification | с | |
| 6. Controller Memory Verification | С | |
| 7. Controller Pressurization Verification | С | |
| 8. HPOTP Torque Check | В | |
| 9. HPFTP Torque Check | В | |
| 10. LPOTP Torque Check | В | |
| 11. LPFTP Torque Check | В | |
| 12. Turbopump Axial Shaft Travel Check | С | |
| 13. Extendible Nozzle Travel Check | В | |
| 14. Igniter Operation | В | |
| Leak Checks | Method* | |
| 1. HPOTP Primary Lox Seal | С | |
| 2. HPOTP Lox/Turbine Drive Gas Seal | С | |
| 3. Oxidizer Inlet Valve and MOV Ball Seals | С | |
| 4. Fuel Inlet Valve and MFV Ball Seals | С | |
| 5. Propellant Valves Primary Shaft Seals | С | |
| 6. Pneumatic Control Assembly Internal Seals | С | |
| 7. Heat Exchanger Coil Leak Test | В | |
| 8. Heat Exchanger Coil Proof Test | В | |
| 9. Thrust Chamber Assembly Outer Walls | С | |
| 10. Combustion and Propellant System Joints | С | |
| * A = Preliminary power-up B = Component Precycling | | |

- C = Automatic Static Checkout
- (Detailed description of approaches in Appendix 2)

| Preflight Checks | and Recommended |
|-------------------------|-----------------|
| Methods | (continued) |

| Inspections | Method* |
|--|---------|
| 1. Exterior of Components for Damage/Security, etc. | С |
| 2. T/C Assembly for Evidence of Coolant Passage Blockage | С |
| 3. HPFTP Turbine Wheel/Blades for Cracks, Fatigue and Damage | С |
| 4. HPOTP Turbine Wheel/Blades for Cracks, Fatigue and Damage | С |
| 5. LPFTP Turbine Wheel/Blades for Cracks, Fatigue and Damage | С |
| 6. LPOTP Turbine Wheel/Blades for Cracks, Fatigue and Damage | С |
| 7. HPOTP Bearings for Damage | С |
| 8. T/C Assembly Injector Faceplate, Igniter, and Lox Post Tips for Erosion, Burning, and Contamination | С |
| 9. Gimbal Bearings and TVC Attach Points for Evidence of Bearing Seizure and Fatigue | В |
| 10. Heat Exchanger for Cracks, Evidence of Wear, and Damage | с |
| Servicing Tasks | Method* |
| 1. Combustion Zone Drying a. Igniter Valves | В |
| b. P _C Sensors | |
| 2. HPOTP Lox/Turbine Drive Gas Seal Pre-Start Purge | В |
| * A = Preliminary power-up B = Component Precycling | L |

C = Automatic Static Checkout

(Detailed description of approaches in Appendix 2)

Table 6 (continued)

The heat exchanger is difficult to leak check since small internal leakage is difficult to detect remotely. Small undetectable leaks may develop into significantly larger leaks during full power operation; actual heat exchanger operating conditions may be difficult to simulate. A highly robust heat exchanger design is recommended as a means of deleting this check.

Hot gas system leaks may be difficult to detect since no throat plug is available. Remote inflight leak detection techniques present a viable option. Some leakage paths could be eliminated by welding combustion system joints.

Inspections

Remote high resolution visual techniques and thermally sensitive surface coatings (for the detection of hot spots) is a viable solution for exterior inspections. However, these techniques may be difficult to implement inside of the main combustion chamber because of inaccessibility and incompatibility of the coating with combustion products.

Turbine rotating element inspection can be accomplished by monitoring blade/disc fatigue and bearing wear. The blade/disc fatigue can be inferred from historical thermal data provided by optical pyrometers. Damage and fatigue is a function of both thermal transients and extended exposure to elevated temperature while under dynamic stress. Wear of the roller element bearings featured in the OTVE preliminary design would be monitored by isotopic wear detectors and fiberoptic deflectometers. Exhaust plume analysis may also be used to detect degradation.

Condition of the gimbal bearing and Thrust Vector Control (TVC) attach points can be deleted by using robust gimbal bearing design.

Servicing tasks

Drying of igniter and Pc sensors may not be required in a vacuum, but if needed, can be accomplished with an inert gas purge.

SUBTASK 3 - Issues and Benefits

The objective of Subtask 3 was to identify the issues and benefits associated with the range of automated preflight checkout methods developed in subtask 2. This task served the purpose of identifying technology areas and potential approaches for automating preflight checkouts, while providing a basis for more detailed preflight method definition studies.

The approach taken is illustrated in Figure 1. Each preflight checkout method was viewed as a composite of (1) the general approach and methodology of each suggested method, (2) the sensors which provide the required data, and (3) any alternate component designs considered to simplify or eliminate that particular preflight requirement. By viewing preflight checkouts in this manner, issues and benefits of each suggested method for satisfying preflight requirements were thoroughly identified.

As described above, three general approaches were considered in satisfying each preflight requirement. These approaches included preliminary power up, automated component precycling, and automated static checkout. Issues and benefits relating to each of these approaches were identified in a general sense as well as specifically in the context of the preflight requirements they satisfy. Issues and benefits were also identified for each sensor considered for preflight checkouts and for any alternate design recommendation where applicable. Where feasible, issues were categorized into space basing issues, vehicle / infrastructure issues, and system issues.

The results of subtask 3 are contained in Appendix 3 where a complete set of issues and benefits are presented. Part A of Appendix 3 identifies general issues and benefits for each of the three approaches listed above, Part B considers the range of methods suggested for satisfying each preflight requirement. Each entry in part B contains references to other applicable issues and benefits, specifically, issues relating to the general approach used (i.e., preliminary power up, component precycling, or static check), sensors and hardware considered for that particular method, and related alternate design recommendations where applicable. Preflight requirements that would be impacted by alternate design recommendations include heat exchanger leak checks and inspections, turbopump bearing checkouts, and hot gas system checkouts. ICHM sensor/hardware issues are identified in part C, and alternate design issues are discussed in part D of Appendix 3.

Issues and Benefits - Approach

RANGE OF PREFLIGHT REQUIREMENTS

Approaches:

- Preliminary Power-up
- Automated Component Pre-cycling
 Automated Static Checkout

| APPROACH | ICHM SENS |
|---|--------------------|
| METHODOLOGY | |
| | Issues relating to |
| • issues relating to each deneral approach | |
| | Speed sensor |
| Specific issues for each | Accelerometer |
| method based on general | Temperature se |
| approach and preflight | Pressure transc |
| requirement | Resolver positic |
| | Eddy Current pc |
| | Turbine flowmer |
| | Fiberoptic defle |
| | Ferromagnetic t |
| ISSILES AND BENEFITS CATECORIES | Isotope wear de |
| 1330E3 AND BENETI 3 CALEGONES | Optical leak det |
| | Optical Pyromet |
| Space Basing | Plume spectron |



Figure 1

Vehicle/infrastructure

Engine system

The scope of the methods presently used for satisfying preflight requirements will need to change as a result of the advanced ICHM sensors being considered. This applies particularly to visual inspections and leak checks - two of the most commonly practiced means of determining flight readiness - which would not be feasible in space using conventional ground based methods. Flight readiness assessments made on the basis of an operational history data base seem to be the simplest and safest approach, yet critical issues still need to be resolved. Of particular importance is a means to adequately monitor degradation of certain components during idle periods in space.

The issues identified for each automated preflight method reflected the current state of ICHM technology based on inputs provided by Rocketdyne experts. As ICHM development continues, some issues will be resolved while others will surface. Based on the evolving nature of the ICHM system and that of chemical transfer propulsion in general, it is recommended that this task be revisited as the ICHM definition firms.

SUBTASK 4 - Technology Readiness Assessment

In subtask 4, the technology readiness levels of the three preflight checkout methods defined in subtask 2 were evaluated. These are the preliminary power-up, automated component precycling, and automatic static checkout methods. Appendix 4 lists the 36 individual checkouts identified in subtask 1 to be accomplished by these methods for a successful preflight complete engine checkout. Appendix 4 also lists the sensors required for each of the three methods to complete these tests. Although the methods are fundamentally different, in many cases they use the same means to evaluate engine conditions. This table also gives the technology readiness of each of the sensors, allowing easy determination of overall method technology readiness as a sum of component readiness. The sensor readiness levels for the first six sensors were obtained from previous ICHM studies. Technology readiness rationales for the remaining seven sensors were established in conjunction with current E.6 efforts. A summary of the type and number of sensors used for each of the three methods is provided in Table 7.

Appendix 4 includes many checkout tasks from subtask 1 for which sensors were not required or are not applicable. Of those, the following checkout tasks do not require sensors: 1.2, 1.5, 1.6, 1.14, 4.1 and 4.2.

For steps 3.3, 3.4, 3.5, and 3.6, the turbine wheel and blade checks, there is no way at present to satisfactorily determine wear or damage using the automated component precycling method. In this case either the statistical techniques of the automated static checkout, application of a low life limit, or a preliminary power-up would have to be used to determine the turbine readiness.

It should be noted that components other than sensors needed for these methods are not included in Appendix 4. Among them are the engine controller, automation and control software, and a pressurized inert gas system for the precycling approach. These components, although integral parts of the preflight methods, are extensions of current, proven elements assumed to already exist in the engine system. They will, nevertheless, require significant development to incorporate the specific preflight functions and will be included in the overall method readiness assessment.





Table 7

Table 8 gives three indexes to show the level of technology readiness for each of the methods. The average readiness level of the sensors for each method along with the minimum level of sensor readiness is shown. The overall system readiness for each method is also given with the following rationales:

Preliminary Power-up: Level 5. There are many procedures performed to date which demonstrate elements of this method. Current engines such as the SSME and RS-27 are test fired before vehicle installation to check engine operation and performance against nominal values. The SSME block two controller performs a similar checkout of all systems without starting the engine before each firing. The J-2 was also fired, shut down and then fired again in an environment similar to that of a space based engine. In addition, the proposed advanced sensors have been demonstrated in ground tests. Together with component refinement, the efforts remaining are systems integration and validation.

Automated Component Precycling: Level 4. As with the previous method, all sensors have been ground tested in some form, but require varying degrees of further development. Evaluating engine readiness using cold flow tests is presently performed on components in preassembly ground tests only. This method would require the design of a substantially larger pressurized gas system with accompanying valves, engine ports and control system plus the design of a shaft drive mechanism.

Automatic Static Checkout: Level 4. This method is presently performed on most engines using available sensors; the only difference being the checkout is not done on board the vehicle. Measurements are remotely checked against the family of data for that engine type, and when possible against that engine's own previous data. Automating and moving these functions to the controller and further developing the designated sensors are efforts yet required to implement this method.

| | Average Sensor Readiness | Minimum Sensor Readiness | Overall System Readiness |
|------------------------------------|-----------------------------|-----------------------------|-----------------------------|
| Preliminary Power Up | 5.0 | 4 | 5 |
| Automated Component Pre-cycling | 4.9 | 4 | 4 |
| Automatic Static Checkout | 5.0 | 4 | 4 |

Table 8. Method Readiness Assessment

SUBTASK 5 - Remaining Development Cost for Automated Preflight Checkout Methods

This section describes the remaining development cost for each of the three preflight checkout categories; i.e., (1) Preliminary power-up (engine fired for short time), (2) Automated pre-cycling (cycling certain individual engine components without firing the engine), and (3) Automated static checkout (without cycling or hot firing engine). "Remaining" costs are understood to cover those costs which are required to bring the sensors and associated computer hardware and software to Technology Readiness Level 6, and to develop and demonstrate the entire automated preflight checkout process and system in a test bed engine (AETB). Activities which lead to a space flight ready system (Technology Readiness Level 7), i.e., qualification and reliability demonstration of the integrated automated preflight checkout system are excluded from the development cost reported in this section. Technical Readiness Levels definitions are listed in Table 9.

Groundrules and Assumptions

For definition purposes, "preflight checkout" was defined as that part of a space-based mission timeline which encompasses both engine preflight condition and engine postflight condition assessment. The mission time difference between postflight and preflight may be short, several days, or long, a year or more. Both checkout conditions will draw heavily on data accumulated by the ICHM during the actual flight phase. These data are assumed to be stored and processed by a ground-based maintenance data base. Table 10 lists additional operational requirements above those mentioned in Subtask 2 which implicitly affect the automated preflight checkout method development program and cost. Table 11 lists all other groundrules and assumptions used in establishing the cost estimates.

| Techno | ology Readiness Levels: Definition |
|---------|--|
| Level 7 | System validation model demonstrated in space; system ready for space-based applications |
| Level 6 | System validation model demonstrated in simulated environment; test of an equivalent of the final system configuration |
| Level 5 | Component and/or breadboard demonstrated in relevant environment |
| Level 4 | Component and/or breadboard demonstrated in laboratory |
| Level 3 | Analytical and experimental proof-of-concept for critical function and/or characteristic; conceptual design test |
| Level 2 | Technology concept/application formulated; conceptual design drafted |
| Level 1 | Basic principles observed and reported |



- Fail operational/fail safe
- High reliability
- Service free life for 100 starts and four hours
- Entire engine is Orbital Replacement Unit (ORU), except: sensors can be replaced at space base by EVA or robotic
- Extendable nozzle
- 10:1 to 20:1 continuously throttleable

Costing Groundrules and Assumptions

- Development program covers all phases of automated preflight checkout from advanced sensor development to system validation in terrestrial simulation of actual flight environment in advanced expander test bed (AETB).
- Development program includes the cost of a comprehensive maintenance data base, though this data base will also be required for the flight parameter data analysis.
- Already spent technology acquisition costs for sensors and software not considered (relatively small sunk costs).
- All costs in 1991 constant dollars.
- Sensor, software and computer costs are incremental above those reported in Task E.6 for a minimal ICHM system (\$46M).
- All costs are Rough Order of Magnitude (ROM), based on analogies, parametrics and expert information, not on detailed program schedules and manpower loadings.

Approach

There are many alternative preflight checkout development programs possible since three candidate checkout methods have been identified, for 36 measurement parameters with several sensor alternatives of different technology readiness levels. In order to reduce this large number of possible development programs to a manageable size, the following approach was taken, illustrated in Figure 2. Two engine design alternatives were postulated:

- (1) An advanced engine is optimized for space based operations and as many design precautions as possible have been taken to minimize the necessary amount of preflight condition monitoring. These include, e.g., hydrostatic bearings on both turbopumps, an external tubular, seamless, weldless heat exchanger and welded engine component interfaces. This approach assumes a design philosophy which is analogous to that of the ALS booster engine concept, i.e., optimization of the engine design with respect to operability with performance as a close but secondary design criterion. It was further assumed that two approaches are feasible: one maximizing the use of current state-of-the-art sensors, the second one maximizing the use of advanced sensors. Current sensors may be somewhat limited in their attributes such as life expectancy, drift characteristics, reliability, repeatability, measurement directness, etc. Advanced sensors will have improved such attributes. In addition, non-intrusiveness and new direct measurement capabilities, as described in the previous section of this report and in the appendices, will be available.
- (2) The engine is not optimized for space base operations, but rather a modification of a ground based engine (such as an RL-10 derivative). It may have features like ball or roller bearings, a heat exchanger with welds in the coils, and flanged engine component interfaces. This design approach necessitates a maximum amount of preflight checkout operations. As in Alternative (1), it was also assumed that either a maximum number of current sensors, or a maximum number of advanced sensors can be used. In this design approach, the engine will need some modifications to accommodate the turbopump spin-up for preflight torque measurement, and for checking turbopump seals with inert gas.



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Figure 3 presents the "building blocks" of a generic development program for the automated preflight checkout methods. The development cost of each building block was determined. For the case in which advanced sensors are used, the program starts with sensor development to advance the sensor technologies to readiness level 6, system validation model demonstrated in simulated environment, i.e., one level before validation in space. Parallel with the sensor technology, the computer hardware and software has to be developed. The computer hardware includes memory and processors in addition to those identified for flight parameter measurements in Task E.6. The software includes the processing logic and algorithms for the preflight checkout sensors, and a (presumably ground based) centralized maintenance data base for engine history information. It will accumulate all flight, preflight and postflight data, and will be used for trend analysis and statistical process control techniques as the basis for maintenance actions. The software costs were determined as those in addition to Task E.6 software costs. The cost estimates of Task E.6 did not include development of a centralized maintenance data base.

Sensors and software have to be integrated into a preflight checkout system and "tested" in an engine. This can be best accomplished first in a "Soft Simulation" (i.e., analytical) task. In this task all engine parameters and sensor parameters will be simulated by time dependent functions and algorithms. This could be performed with support of Rocketdyne's transient engine performance model which encompasses analytical representation of engine hardware. Engine component and sensor failures can be introduced into a Monte Carlo-type soft simulation in order to understand the time and functional interdependencies of the sensor/software/engine component system.

The next set of activities, shown in parallel in Figure 3, are "Hard Simulation" and "Integrated Sensor/Computer System Brassboard Simulation." The Hard Simulation of engine components and preflight checkout sensors involves instrumenting real engine components with real sensors required for preflight checkout, and testing the engine components by flow testing (turbopumps, valves, pneumatic subsystem) or hot firing (main combustion chamber with nozzle, gimbal/TVC). Vibration testing (shaker table) may also be required. The engine components should be of flight configuration, but need not be the same as those for an OTVE or STVE. These component and sensor tests will be performed using six separate component brass boards and will establish the viability of the sensors in an engine component environment.





* "Delta" means additional development over that discussed in Task E.6 for the ICHM

The next task, "Integrated Sensor/Computer System Brassboard Simulation" includes real sensors and processors, prototype software and a suitable existing computer platform. The engine components will be simulated by digital or analog signals driving the sensors or processors. This simulation will address systems aspects of the automated preflight checkout method, sensor time behavior, real processor characteristics, data base functioning, etc.

The final task of the development program consists of instrumenting an engine with sensors, integrating all preflight checkout sensors, software and computer with the engine and flight ICHM system, and statically hotfiring the engine (e.g. the Advanced Expander Test Bed [AETB]). Successful completion of this task will establish the system validation in simulated (i.e. ground) environment. For this task, only that cost was estimated which is due to contractor instrumentation, software and systems engineering support, while engine testing costs (both labor, hardware and propellants) are assumed to be government furnished.

Sensor reliability demonstration and qualification of the engine/sensor/ computer/software system are considered to be outside technology level 6 and constitute necessary tasks for advancing to level 7. The costs of these tasks were, therefore, not determined.

Figure 4 is a generic program schedule for the preflight checkout method tasks discussed above, to establish the timeframe of activities. Development costs were based on this schedule. The schedule (4 years to first AETB test) is consistent with a reasonably paced development program and would allow time for integration of the automated preflight checkout system with an engine ready for an Initial Operating Capability (IOC) near the end of the decade.

Development Program Cost Evaluation

After dividing the development program into 7 tasks, the cost of each task was determined separately, based on parametrics, analysis, modification of Task E.6 costs and some preliminary manpower loading estimates.

Generic Development Schedule for Automated Preflight Checkout Program

| Task | | | 7 | ear | | |
|---|---|---|---|-----|---|---|
| | t | 2 | с | 4 | £ | 9 |
| Advanced Sensor Development | | | | | | |
| Delta ICHM Software Development | | | | | | |
| Delta ICHM Computer Development | | | Π | | | |
| Soft Simulation | | | | | | |
| Hard Simulation | | | | | | |
| Integrated Sensor/Computer Brassboard | | | | | | |
| Engine Modification (for Method 2 only) | | | | | | ~ |
| AETB Test Support | | | | | | Π |
| First AETB Test | | | | | | |
| | | | | | | |

Figure 4

The logic for sensor development costs is as follows: Current technology ICHM sensors (see Table 4) need a minimum of development, and a nominal cost of \$0.5M was assumed for the sum of all sensors. This was based on the cost estimate provided in Task E.6. Advanced sensors (see Appendix 4) currently at a technology level of 4 were estimated to require \$1M for each type to bring them to level 6. Sensors currently at level 5 were estimated to require \$0.5M for each type to bring them to level 6. These approximate, averaged costs were based on extensive discussions with instrumentation experts.

The development rationales for the other tasks shown in Figure 2, plus required engine modifications for Category 2 (component precycling), are listed in Table 12. The costs of the individual development tasks are summarized in Table 13.

Development Program Costs for Each Preflight Checkout Method

As discussed previously, the preflight development costs were determined for two alternatives: (1) an advanced design engine optimized for space based operations, and (2) an engine with minimum modifications to an existing ground based engine.

(1) Engine Optimized for Space Basing

For this alternative, the design assumptions shown in Table 3 are presumed to be incorporated into the engine. The following engine preflight checkout requirements can be eliminated (see also Table 2):

| | sumate |
|--------|---------|
| | |
| 1 mont | binetit |
| David | הפעפור |

| Task | Task Cost Elements | Cost (1991M\$) | Rationale |
|--|--|----------------|---|
| Sensor Development 2. Delta Software | Current state-of-the-art sensors Advanced state-of-the-art sensors Maintenance Data Base | 0.5 8.0 | Adaptation of existing sensor sulte, see Task E.6. Sum of advanced sensor development costs for sensors shown in Appendix 4, using rule described in text. |
| Development | Space Base Optimized Engine Design | 3.5 | 3000 Source Line of Code (SLOC) (average of 17 military ground and mobile data bases, non-ADA) x 7.6 hrs/SLOC for manned filght related computers x 2.0 (complexity factor for ADA). |
| | Non-Space Base Optimized Engine Process Software | 4.6 | 30% more SLOC than above due to more sensors, more data reduction and data storage. |
| | Space Base Optimized Engine | 2.4 | 16,000 man hours (from Task E.6 for pre-start operations) x 2 (complexity factor to account for more extensive checkout processes). |
| | Non-Space Base Optimized Engine | 3.6 | 50% more SLOC than above due to more sensors, and more complex process logic. |
| 3. Delta Computer Hardware Development | • Labor | 2.5 | 354,000 man hours (from Task E.6 for ICHM computer) x 0.1 (10% detta cost for additional capability). |
| 4. Soft Simulation (Analytical Tool) | • Labor | 0.6 | Development and documentation of a complete simulation analysis tool where all sensors and engine components are simulated by characteristics functions. Possible use of "Transient Engine Model." 2 man years. |
| | Software | 0.1 | Simulation software shell and training. |
| | | Table 12 | |

Development Cost Estimate (continued)

| Task | Task Cost Elements | Cost (1991M\$) | Rationale |
|--|-------------------------------------|-------------------|--|
| 5. Hard Simulation (Component Brassboards) | | | Sensors mounted on engine components, tested by cold flow, vibration and/or test fire. |
| Lox Turbopump | Test Labor | 0.2 | (20 tests/3 tests/wk) x 10 EP x 40 hrs/wk |
| Fuel Turbopump | _ | 0.2 | (20 tests/3 tests/wk) x 10 EP x 40 hrs/wk |
| Main Combustion Chamber | | 0.8 | (40 tests/3 tests/wk) x 20 EP x 40 hrs/wk |
| Valves | | 0.2 | (8 valves x 10 tests/valve/5 tests/wk) x 5 EP x 40 hrs/wk |
| Pneumatic Subsystem | | 0.05 | (10 tests/3 tests/wk) x 5 EP x 40 hrs/wk |
| 6 Component Brassboards | Engineering and Management Labor | 0.05 3.0 | (10 tests/3 tests/wk) x 5 EP x 40 hrs/wk 2 yrs x 10 EP x 2000 hr/yr |
| 6 Component Brassboards | Hardware | 3.5 | Cost of 70% of new OTVE 0.7 x \$5M |
| 6. Integrated Sensor/Computer System Brassboard | | | System integration of actual sensors and simulated engine component hardware |
| Sensors | Hardware | 0.6 | 40 sensors at \$15K/sensor in the average |
| Engine Component Simulation | Software | 0.2 | Equivalent to "Translent Engine Model," 2000 man hrs |
| Computer | Hardware | 0.5 | Engineering estimate of special purpose computer |
| Sensor/Component Integration | Software | 1.2 | 50% of Item 2 process software |
| Brassboard Test and Design | Labor | 1.5 | 1 yr x 10 EP x 2000 hr/yr |
| 7. OTVE Modification | | | Turbine spin and seal inert gas supply subsystem |
| Valves and Press. Tanks Design, Test and Checkout | Hardware Labor | 0.3 2.0 | 5% of OTVE First Unit Cost, 0.05 x \$6M 1% of OTVE DDT&E core effort. 0.01 x \$200M |
| 8. AETB Test Support | Labor | 2.4 | 2 yrs x 8 EP (Instrumentation, software and systems engineers) |

Note: EP = equivalent person

Table 12 (continued)

| Summary of Development (Elements by Task* | Cost |
|--|------------|
| | (M\$, 91) |
| Sensor Development | 0.5 to 8.0 |
| Delta Software Development | |
| Maintenance Data Base • Optimized engine • Not optimized engine | 3.5 4.6 |
| Process Software Optimized engine Not optimized engine | 2.4 3.6 |
| Delta Computer Hardware Development | 2.5 |
| Soft Simulation | 0.7 |
| Hard Simulation | 8.0 |
| Integrated Sensor/Computer System Brassboard | 4.0 |
| OTVE Modification (for Cat. 2 only) | 2.3 |
| AETB Test Support | 2.4 |
| | |

* These costs are not additive. The proper elements are combined for 4 different cases as shown in Table 14.

- Functional Checks
 - HPOTP Torque Check
 - HPFTP Torque Check
 - LPOTP Torque Check
 - LPFTP Torque Check
 - Turbopump axial shaft travel
- Leak Checks
 - HPOTP Primary Lox Seal
 - HPOTP Lox/Turbine Drive Gas Seal
 - Heat Exchange Coil Leak Test
 - Heat Exchange Coil Proof Test
 - <u>Component</u> Interface Joints (but not <u>engine/vehicle</u> fluid interfaces)
- Inspections
 - HPOTP Bearings for Damage
 - · Heat Exchanger for Cracks, Evidence of Wear and Damage
- · Servicing Tasks None to be eliminated

(2) Engine not Optimized for Space Basing

This assumes that an engine with a basically ground based design concept, such as the current RL-10, is used for space based operations. In this instance, all or most of the 36 preflight checkout parameters listed in Table 2 need to be addressed.

The development program costs for the two engine design alternatives are summarized in Table 13. The total program costs range from about \$26M to \$35M. This range is relatively small due to the fact that a large part of the costs are contained in software, hardware simulation and brassboard efforts which were assumed to be basically invariant to the selection of particular sensor concepts. Software costs for engines which are optimized for space basing are different than those for engines not optimized for space basing. The maintenance data base software for non-optimized engines was assumed to be 30% larger, and the process software 50% larger compared to those for optimized engines. The 30% increase is due to the larger amount of sensors and the associated larger data base requirement for maintenance. The 50% increase is also partly due to the higher amount of sensors, and partly because of the additional more complex process logic requirements. A

more detailed development program analysis, however, may show more differentiation, especially with regard to sensor algorithm software. The cases which use advanced stateof-the-art sensors are more costly than those with existing qualified sensors; however, the capability, quality and reliability of the preflight checkout information is also higher for these cases. The use of current state-of-the-art sensors may lead to higher operating costs (due to lower sensor life and reliability expectations) and to lower quality information (due to more reliance on trend analysis instead of direct measurements).

Preflight checkout Category 2 (automated precycling) for engines which are not optimized for space base operations may introduce substantial reliability and safety issues connected with the addition of valves, lines, inert gas tanks, etc. which may degrade the overall reliability and safety and may also lead to larger life cycle costs.

All development program costs shown in Table 14 are in addition to those which were given for Task E.6, as previously noted.

110 Development Program Costs (M\$.

| L | | • | | | | | | | |
|----------------------|--|--------------------------------|----------------------------------|-------------------------|-------------------------------------|------------------------------|------------------------|--------------------------------------|-----------------|
| | Engine Ol Space Base | otimized fo Operatio | Jr IIS | | Engi Spac | ne <u>Not</u> O ce Base (| ptimized f | or s | |
| | Max. Use of Current Sensors (Cat. 1, 2, 3) | Max. L Advanced (Cat. 1) | lse of Sensors (Cat. 2, 3) | Ma Curre (Cat. 1) | tx. Use of ent Senso (Cat. 2) | rs (Cat. 3) | M Advar (Cat. 1) | ax. Use of iced Sens((Cat. 2) | ors (Cat. 3) |
| Sensors | 95 | CV | ŭ | u u | | u c | L P | | |
| | 7 .7 | 2 | с. г | C .C | <u>.</u> | C'N | c.) | 6.5 | 5.5 |
| △ Software | 1 5.9 | | 4 | V | | ® | 6 | | |
| A Computer | 2.4 | | | ¥ | | 7 | 4 | | |
| Soft Simulation | ▲ 0.7 | | ▲ | ¥ | | 0 | | | 4 |
| Hard Simulation | ●●●●● | | • | ¥ | | 8 | 0. | | 4 |
| Integrated Brassboa | rd ▲ 4.0 | | Å | ¥ | | 4 | 0 | | |
| Engine Modifications | | | ≜ | I | 2.3 | 1 | ł | 2.3 | 1 |
| AETB Test Supp. | 2.4 | | A | ¥ | | 7 | 4 | | 4 |
| | | | | | | | | | |
| Total | \$25.9M | \$27.4M | \$28.9M | \$31.2M | \$29.5M | \$28.2M | \$33.2M | \$34.5M | \$31.2M |
| Note: Preflight ch | neckout category (| l) = prelimir | ary power up | o, (2) = auto | mated pro | scycling, (| 3) = automa | ited static | checkout |

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Table 14

References

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- 4. Advanced Engine Study Task D.4, Orbit Transfer Rocket Engine Technology Program, NAS3-23773, Rocketdyne, 1987.
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- 8. Advanced Engine Study Task D.1/D.3, Orbit Transfer Rocket Engine Technology Program, NAS3-23773, Rocketdyne, 1986.

Appendix 1

OTVE Preflight Requirements (References)

| quence check (FRT) X V41ASO.030 1 redundancy verification X V41AN0.030 1 ory verification X V41AV0.010 - |
|--|
| redundancy verification X V41AND.030 1 Ory verification X V41AVD.010 |
| ory verification X V41AV0.010 |
| |

OTVE PREFLIGHT REQUIREMENTS - REFERENCES (Sheet 1 of 6)

Part A

| | NOTES | | | | | | | |
|-------------------------|-------------------------------|-------------------|-------------------------------|---|-----------------------|--|--|--|
| | FMEA | CRIT. | | | 2/8 | 2/6 2/8 2/6 2/6 | 2/8 1/6 1/6 1/6 1/8 | |
| ES | OTVE | REF. ND. | | • | 050302 | 050304 060304 060304 060304 060304 060307 | 050202 050203 050203 070302 070303 070305 | 050402 050403 050404 050404 050406 050202 060204 060204 060204 |
| FERENC | 0 | CRIT. | | - | - | | - | - |
| RE | SSME OMRS | REF. ND. | | 040.0NA18V | V41BS0.040 | | V41BS0.020 | V41BS0,030 |
| | | Periodic (TBD) | | | | | | |
| | | Routine | | × | × | | × | × |
| ATVE DDEEL TEUT DEALURE | מואב דארו בושוון הבקטותרחבאוס | REQUIREMENT | FUNCTIONAL CHECKS (continued) | 7. Controller pressurization verification | B. NPDTP torque check | | 9. HPFTP torque check | 10. LP01P torque check |

OTVE PREFLIGHT REQUIREMENTS - REFERENCES (Sheet 2 of 6)

Part A

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.

| | NOTES | | | | | | | See FMEA reference for turbopump lorque checks. | ~ | | |
|---------------------------|-----------------------------|-------------------|-------------------------------------|-----------------------|-------|------------|-----------------|--|-----------------------------------|----------------------|--|
| | FMEA | CR11. | | 2/B | 2/C | 2/B 2/H | 2/C 2/C 2 | | 2 | ME | |
| ES | 01VE | REF. NO. | | 050102 | 01050 | 070202 | 070204 | (NDTES) | 020502 | 101040 | |
| FERENC | 0 | CR11. | | | | | | | 1 | ~ ~ | |
| RE | SSME OMRS | REF. ND. | | V41BS0.010 | | | | V41BS0.032 V41BS0.044 V41BS0.020 | 1 | V41AQ0.010 | |
| | | Periodic (TBD) | | | | | | | | | |
| | _ | Rout Ine | | × | | | | × | × | × | |
| ATVE DDEELTEUT DEPUTOENTE | OLVE FACTLISHT REQUIREMENTS | REQUIREMENT | <u>UNCTIONAL CHECKS</u> (continued) | 1. LPF1P torque check | | | | Turbopump axial shaft travel check | 3. Extendable nozzle travel check | 4. Igniter operation | |
| | | | الک | - | | | | - | - | <u> </u> | |

OTVE PREFLIGHT REQUIREMENTS - REFERENCES (Sheet 3 of 6)

Part A

OTVE PREFLIGHT REQUIREMENTS - REFERENCES (Sheet 4 of 6)

Part A

mediate seal pressure. Frequency of test TBD. SSME monitors inter-NOTES CR11. 27B 33322 1/A 1/A 2/B М OTVE FMEA \sim ı 1 1 1 1 Μ I CRII. REF. NO. 060506 060507 060104 060105 060106 070104 070105 070106 060302 050306 020202 020201 020301 020401 11 ł ł REFERENCES J.R I _ _ - --SSME OMRSD V41BQ0.090 V41BQ0.091 V41BQ0.020 V41BQ0.040 V41BQ0.110 V41800.120 V418Q0.010 V41BPB.020 V41BPB.030 V41BQ0.160 N0. V41AY0.221 (NOTES) REF. Periodic (TBD) × Rout Ine × × × × × × × × × **OTVE PREFLIGHT REQUIREMENTS** Propellant valves primary shaft seals Fuel inlet valve and MFV ball seals Pneumatic control assembly internal Thrust chamber assembly outer wall Oxidizer inlet valve and MOV ball seals Combustion and propellant system HPOTP LOX/turbine drive gas seal (intermediate seal) Heat exchanger coils proof test Heat exchanger coils leak test REQUIREMENT HPOTP primary LOX seal Joints LEAK CHECKS seals -10. 2. 4. 5. . б . . **e** . -8.

OTVE PREFLIGHT REQUIREMENTS - REFERENCES (Sheet 5 of 6)

| OTVE PREFLIGHT REQUIREMENTS REFERENCES OTVE PREFLIGHT REQUIREMENTS REFERENCES ROUTREMENT ROUTREMENT REFERENCES ACTURE ACTUREMENT ROUTREMENT IL SECTIONS CITLI REGUIREMENT 1. Exterior of components for damage, security, clearances, etc. X V411010.030 1 - 1 1 1 1 1 <t< th=""><th></th><th>NDTES</th><th></th><th></th><th>re information needed probability of damage om orbital debris, etc.</th><th></th><th>equency of inspection</th><th>equency of inspection D.</th><th>equency of inspection D.</th><th>equency of inspection D.</th><th>equency of inspection D.</th><th></th><th>equency of inspection D.</th><th>equency of inspection D.</th></t<> | | NDTES | | | re information needed probability of damage om orbital debris, etc. | | equency of inspection | equency of inspection D. | equency of inspection D. | equency of inspection D. | equency of inspection D. | | equency of inspection D. | equency of inspection D. |
|---|------------------------------|---------|-------------------|------------|---|--|--|--|--|---|-----------------------------|--|--|--|
| OTVE PREFLIGHT REQUIREMENTS REFERENCES FOUREMENT REQUIREMENT REQUIREMENT REFERENCES REQUIREMENT REQUIREMENT REQUIREMENT REQUIREMENT REQUIREMENT ROUTINE REQUIREMENT ROUTINE REQUIREMENT ROUTINE REQUIREMENT ROUTINE REQUIREMENT ROUTINE REQUIREMENTS ROUTINE REQUIREMENTS ROUTINE REQUIREMENTS ROUTINE REQUIREMENT ROUTINE REQUIREMENT ROUTINE RECUIREMEES CITIT. REFERENCES REFORENCES CITIT. REFERENCES SHE OWESD OTVE RETURNES X VAIBSO.0B0 R | _ | IEA | RIT. | | - Fr | - <u>1</u> 8 | - | 2 1B | - | 2 Fr 18 | IA Fr IC IB | 2B | 1/8 1 18 | |
| REFERENCE OTVE PREFLIGHT REQUIREMENTS REQUIREMENT X VAIBIO X VAIBSO.0080 To assembly for evidence of coolant X VAIBSO.0080 FETT turbine wheel/blades for cracks, X VAIBSO.0080 <td>S</td> <td>01VE FM</td> <td>REF. NO. C</td> <td></td> <td>1</td> <td>030101 030102</td> <td>050205</td> <td>050105</td> <td>050305</td> <td>050405</td> <td>060303 060304</td> <td>020101 020105</td> <td>090304</td> <td>030201</td> | S | 01VE FM | REF. NO. C | | 1 | 030101 030102 | 050205 | 050105 | 050305 | 050405 | 060303 060304 | 020101 020105 | 090304 | 030201 |
| NTVE PREFLIGHT REQUIREMENTS REF OUREMENT REQUIREMENT REQUIREMENT REQUIREMENT RETOR REQUIREMENT RETOR REQUIREMENT RETOR REQUIREMENT RETOR INSPECTIONS INSPECTIONS I. Exterior of components for damage, x X V411810.030 SEME OMEST X V411850.080 FATTO turbine wheel/blades for cracks, x V411850.080 FATTO turbine wheel/blades for cracks, x <tr< td=""><td>ERENCE</td><td>_</td><td>CR11.</td><td></td><td>-</td><td>1</td><td>~</td><td>1</td><td>-</td><td>1</td><td>-</td><td>-</td><td>1</td><td></td></tr<> | ERENCE | _ | CR11. | | - | 1 | ~ | 1 | - | 1 | - | - | 1 | |
| OTVE PREFLIGHT REQUIREMENTS OTVE PREFLIGHT REQUIREMENTS REQUIREMENT Routine Periodic REQUIREMENT Routine Periodic INSPECTIONS 1. Exterior of components for damage, security, clearances, etc. X 3. HPFIP turbine wheel/blades for cracks, fatigue, and damage X 4. LPFIP turbine wheel/blades for cracks, fatigue, and damage X 5. HDOTP turbine wheel/blades for cracks, fatigue, and damage X 6. LDOTP turbine wheel/blades for cracks, fatigue, and damage X 6. LDOTP turbine area for evidence of fatigue or damage X 7. HPOTP bearings for damage X 6. LDOTP turbine area for evidence of fatigue or damage X 7. HPOTP bearings for damage X 6. LDOTP turbine area for evidence of fatigue or damage X 7. HPOTP bearings for damage X 9. Gimbal bearing and contamination Y 9. Gimbal bearing seture and famage X 9. Gimbal bearing set weldence of weat, and damage X 9. Gimbal bearing set well cracks, etc. X 9. Gimbal bearing set well cracks, etc. X 9. Gimbal bearing | REF SSME OMRSD | | REF. NO. | | V41BUD.030 | 1 | V41BS0.080 | 1 | V41BS0.082 | 1 | V41BS0.082 | V41BU0.040 | i i | V41BU0.040 V41BU0.086 |
| OTVE PREFI.IGHT REQUIREMENTS OTVE PREFI.IGHT REQUIREMENTS REQUIREMENT Routine REQUIREMENT Routine INSPECTIONS 1. Exterior of components for damage, security, clearances, etc. x 2. TC assembly for evidence of coolant passage blockage (hot spots) x 3. HPFIP turbine wheel/blades for cracks, fatigue, and damage x 4. LPFIP turbine wheel/blades for cracks, fatigue, and damage x 5. HPOTP turbine wheel/blades for cracks, fatigue, and damage x 6. LPOTP turbine wheel/blades for cracks, fatigue, and damage x 7. HPOTP turbine wheel/blades for cracks, fatigue, and damage x 9. HPOTP turbine area for evidence of fatigue or damage x 10. HPOTP bearings for damage x 9. Gimbal bearings for damage x 10. Heat exchanger for weld cracks, etc. x 10. Heat exchanger for weld cracks, etc. x | <u> </u> | | Periodic (TBD) | | | | × | × | × | × | × | | × | × |
| DIVE PREFLIGHT REQUIREMENTS REQUIREMENT REQUIREMENT REQUIREMENT INSPECTIONS I. Exterior of components for damage, security, clearances, etc. 1. Exterior of components for damage, security, clearances, etc. 2. TC assembly for evidence of coolant passage blockage (hot spots) 3. HPFIP turbine wheel/blades for cracks, fatigue, and damage 4. LPFIP turbine wheel/blades for cracks, fatigue, and damage 5. HPOTP turbine wheel/blades for cracks, fatigue, and damage 6. LPOTP turbine area for evidence of fatigue, and damage 7. HPOTP bearings for damage 8. TC assembly injector faceplate, igniter, and LOX post tips for evidence of bearing seizure and fatigue 9. Gimbal bearing and TVC attach points for evidence of bearing seizure and fatigue 9. Gimbal bearing and TVC attach points for evidence of bearing seizure and fatigue 9. Gimbal bearing and TVC attack points for evidence of bearing seizure and fatigue 9. Gimbal bearing and TVC attack points for evidence of bearing seizure and fatigue 9. Hoat exchanger for weld cracks, evidence of bearing seizure and famage | | | Routine | | × | × | | | | | | × | | |
| | OTVE DREFLIGHT REALLIGEMENTS | | REQUIREMENT | NSPECTIONS | . Exterior of components for damage, security, clearances, etc. | . TC assembly for evidence of coolant passage blockage (hot spots) | . HPFIP turbine wheel/blades for cracks, fatigue, and damage | . LPFTP turbine wheel/blades for cracks, fatigue, and damage | . HPOTP turbine wheel/blades for cracks, fatigue, and damage | . LPOTP turbine area for evidence of fatigue or damage | . HPOTP bearings for damage | . TC assembly injector faceplate, igniter, and LOX post tips for erosion, burning, and contamination | . Gimbal bearing and IVC attach points for evidence of bearing seizure and fatigue | 0. Heat exchanger for weld cracks, evidence of wear, and damage |
| | | | | YI | <u> </u> | 2. | | ₹ | -2. | | ٦. | | 5 1 1 4 5 | 2 |

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Part B

BASIC FAILURE MODE EFFECTS AND CRITICALITY

| Number | Engine Effect | Vehicle Effect | Mission Effect |
|--------|---|--|---|
| 1 | Major uncontained damage to an engine subsystem or component resulting in widespread engine damage. | Significant damage to adjacent equip- ment and/or vehicle probable. | Mission abort(1) Low probability of vehi- cle loss, crew death or injury |
| 2 | Significant contained damage to a vital engine subsystem or component sufficient to render it inoperative or its continued operation hazardous. | Damage to adjacent equipment or vehicle highly improbable. | Mission abort(1) |
| 3 | Performance degradation or notable damage to component/ subsystem. Continued opera- tion conditionally acceptable. | None | Mission abort(1) Conditionally dependent |
| 4 | Minor failures fully tolerated by continued operation at an acceptable hazard level. Minor propellant leakage from flanged joints. | None | Delay until resolved at mission start |
| 5 | Nuisance failures. | None | Correct at next routine maintenance |

ICHM MODIFIED FAILURE MODE EFFECTS AND CRITICALITY

| Criticality Number | Engine Effect | Vehicle Effect | Mission Effect |
|-----------------------|---|----------------|---|
| A | Safe shutdown of engine before uncontained damage results. | None | Mission abort(1) |
| B | Safe shutdown of engine before significant contained damage results. | None | Mission abort(1) |
| C | Reduced power level operation. | None | Mission abort(1) Conditionally dependent |
| D | Parallel or standby redundant system assumes function; normal engine operation continues. | None | Delay until resolved at mission start |

- (1) Mission abort for criticality 1 through 3 and A through C failures applies only on outbound phases prior to OTV payload disposition. After abort, emphasis is placed on safe return of the vehicle/crew regardless of payload disposition.
- NOTE: Basic failure modes requiring multiple failures to produce the specified criticality are indicated by a suffixed M after the criticality number.

| CDITICAL | DEDUTERT | SSME P | VPPL1CA1 | NC | OTV API | LICATION | | <u> </u> |
|----------|---|-----------------------|----------|----------|---------|----------|---|----------|
| 117 | | POST- INSTALLATION | ROUT INE | PERIODIC | 0661 | FUTURE | NULES | |
| | FUNCTIONAL CHECKS | | | | | | | |
| 1 | Controller memory dump/compare | × | × | | × | | | |
| ~ | Valve actuator checkout | × | × | | × | | | |
| - | Pneumatic component checkout | × | × | | × | | | |
| - | Sensor checkout | × | × | | × | | | |
| - | Redundancy verification | × | × | | × | _ | | |
| L | Controller heater verification | × | × | <u></u> | | | | |
| - | Operational sequence check (FRT) | × | × | | × | | | |
| - | Controller pressurization verification | × | × | | × | | <u>^</u> | |
| E | MFV heater checkout | × | | | | | | |
| e | Gimbal electrical bonding test | × | | | | | | |
| ß | Interface electrical bonding test | × | | | | | | |
| e | Gimbal actuator electrical bonding test | × | | | | | | |
| - | Controller power/internal temperature verification | × | × | | | <u></u> | | |
| ~ | Operational instrumentation verification | × | × | | | | Includes skin temperalures and accelerometers | - |
| ~ | Skin temperature instrument channelization | × | | <u> </u> | | | | |
| | | | | | _ | | | |

Part C SSME OMRSD (Sheet 1 of 11)

| | OTTO | NULES | | | | | | | | | | | |
|---|-----------|-----------------------|-------------------------------|-------------------|-------------------|-------------------|-------------------------|---|-------------------------|-----------------------------|--|----------------------------------|---|
| | LICATION | FUTURE | | | | | | | | | | | |
| | OTV APF | 0661 | | × | × | × | × | × | × | | | × | |
| | NO | PERIODIC | | <u> </u> | <u> </u> | <u> </u> | | | <u></u> | | | | |
| | VPPLICATI | ROUTINE | | × | × | × | × | × | × | | × | × | |
| _ | SSME / | POST- INSTALLATION | | × | × | × | × | × | | × | | | |
| | | KEQUIKEMENI | FUNCTIONAL CHECKS (continued) | LPFTP torque test | HPFTP torque test | LPOTP torque test | LPOTP shaft travel test | HPOTP torque test/impeller lock verification | HPOTP shaft travel test | HPOTP shaft travel baseline | Antiflood valve cracking pressure test | Pre-cryogenics load requirements | Load and execute sensor checkout module Load and execute redundancy checkout module Load and execute pneumatic checkout module (partial) Load flight software Dump and compare controller memory contents |
| | 11011100 | LTY LTY LTY | | - | - | - | - | ~ | - | 1 | - | - | |

Part C SSME OMRSD (Sheet 2 of 11)

| CRITICAL- | RFOULTRFMENT | SSME | APPLICAT | NOI | OTV APP | LICATION | |
|-----------|--|-----------------------|----------|--------------|-------------|-------------|----------------------|
| 11Y | | POST- INSTALLATION | ROUT INE | PERIODIC | 0661 | FUTURE | NOTES |
| | LEAK CHECKS | | | | | | |
| - | HPFTP liftoff nose/piston seals | × | × | | | | |
| ~ | LPFTP liftoff nose/piston and Naflex seals | × | × | - <u>-</u> | | | |
| - | HPOTP primary oxidizer seal | | × | | × | | |
| - | Heat exchanger coil leak test | | × | | × | | |
| - | Heat exchanger coll proof test | | | 3500 3500 | × | <u></u> | During HPOIP recycle |
| - | MFV ball seal | × | × | | × | | |
| - | MFV primary shaft seal | | × | <u> </u> | × | | , |
| - | MOV ball seal | × | × | | × | | |
| ~ | MOV primary shaft seal | | × | | × | | |
| | FPOV ball seal | × | × | | | <u> </u> | |
| ~ | FPOV primary shaft seal | - | × | <u></u> | <u> </u> | | |
| ~ | OPOV ball seal | × | × | | | | |
| , | OPOV primary shaft seal | | × | | | | |
| - | CCV primary shaft seal | | × | | | | |
| - | Propellant valve actuators pneumatic seals | | × | | | | |
| JR | Fuel bleed valve seat | | × | | | | |
| | | | <u> </u> | | | | |

Part C SSME OMRSD (Sheet 3 of 11)

| REQUIREMENT | | SSME A | PPLICA1 | N | OTV API | PLICATION | NOTES |
|--|----------|-----------------------|----------|----------|---------|-----------|------------------------------|
| | | POST- INSTALLATION | ROUTINE | PERIODIC | 0661 | FUTURE | |
| <u>LEAK CHECKS</u> (continued) | | | | <u> </u> | | | |
| Oxidizer bleed valve seat | | | × | | | | |
| Antiflood valve seat/shaft seal | | | × | | | | |
| Pneumatic control assembly internal s | eals | | × | <u> </u> | × | | |
| Thrust chamber interior/exterior wall | s | | × | | × | | |
| MCC-to-nozzle seal | | | × | | | | |
| MCC liner decay-pressure check | | | × | | | | ÷ |
| Main injector LOX posts | | | × | | | | Unsupported plugged posts |
| System purge check valves (7) | | | × | | | | |
| Systems gross leakage (signature leak check) | | | × | <u></u> | | | |
| Oxidizer, fuel, hot gas system violate joints | Ð | × | × | , | × | | |
| Pneumatic interface connections | <u> </u> | × | | | | | |
| | <u> </u> | | <u> </u> | | | | |
| | | | | | | | |
| | | | <u>-</u> | | | | |

Part C SSME OMRSD (Sheet 4 of 11)

| | NULES | | | | Pump removed from engine | More white pump is removed, detailed inspections are con- ducted on powerhead, MCC injector, and tuel prehurner. |
|------------|-----------------------|-------------|---|------------------------------------|---|---|
| PLICATION | FUTURE | | | | | |
| 0TV AP | 0661 | | × | | × × | < |
| NOI | PERIODIC | | | | 3 starts | |
| APPL I CAT | ROUTINE | | × | × | I | |
| SSME | POST- INSTALLATION | | × | | | |
| OFALLER | | INSPECTIONS | Exterior of components for damage, security, clearances, corrosion, etc. | Interior of components (borescope) | Main injector faceplate, baffles, injector elements, flow/heatshields, film coolant holes, LOX posts, ASI chambers/orifices, igniters, and LOX dome Fuel preburner Oxidizer preburner Oxidizer preburner Main combustion chamber liner and acoustic chambers Heat exchanger Hot gas manifold First- and second-stage furbine | blades Tip seals and platforms Dampers Dampers Bellows shield (dye penetrant) Sheet metal, struts, vanes Coolant orifices |
| CDITICAL_ | LTY | | - | ~ | - | |

Part C SSME OMRSD (Sheet 5 of 11)

RI/RD 91-145

. ...

Part C SSME OMRSD (Sheet 6 of 11)

MCC injector, oxidiz-5000 seconds initial-Prior to pump instal-Concurrent with HPFIP Concurrent with HPOTP is removed, detailed inspections are con-ducted on powerhead, Eddy-current testing Rocketdyne for inand HPOIP removals NOLE: While pump er preburner, and Pump returned to ly, 2400 seconds heat exchanger. to detect wall NOTES thereafter spection thinning removal lation **OTV APPLICATION** FUTURE 0661 × × × POSI-INSTALLATION ROUTINE PERIODIC seconds seconds (see notes) (see notes) notes) 3,000 starts 3500 (see SSME APPLICATION I × i I ł I ۱ Hot gas manifold transfer tube liner welds and support pins (dye penetrant) First- and second-stage turbine Fuel preburner LOX post support pins Fuel preburner oxidizer ASI orifice Tubes, brackets, turning vanes Oxidizer preburner LOX posts (eddy HPFTP bellows height verification Coil eddy-current test
 Coil welds (borescope) REQUIREMENT INSPECTIONS (continued) Pump end bearings Heat exchanger blades current) HPOTP CRITICALä JR ITΥ ~

Part C SSME OMRSD (Sheet 7 of 11)

| APPLICATION | P FUTURE NOTES |
|--------------|-----------------------|
| DTV AP | 0661 |
| ION | PERIODIC |
| APPLICAT | ROUTINE |
| SSME | POST- INSTALLATION |
| DECULTOENENT | ислотистени |
| | 117 |

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| | NOTES | | | | | See attached purge | flow charts | |
|-----------------|-----------------------|--|--|---------------------------------------|--|--------------------|--|--|
| LICATION | FUTURE | | | | | | | |
| OTV API | 0661 | | _ | | × | | × | |
| NOI | PERIODIC | | | | | | | |
| APPLICAT | ROUTINE | × | | × | | × | | |
| SSME | POST- INSTALLATION | × | | | | | | |
| DE DITI DE MENT | | <u>SERVICING</u> Install protective covers and closures | Nozzle/MCC Drain line exits TC exit Bellows MFV heater Critical sensors | Propellant system drying/verification | HPFTP turbine bearing HPOTP turbine seals/drains Uxidizer purge system MCC and nozzle HPOTP secondary turbine seal pressure sense line MCC pressure sensors | Purges, pre-start | Oxidizer dome (GN₂) HPOTP intermediate seal (GN₂/He) Fuel system (He) Component fuel drain (He) Preburner shutdown (He) LP fuel duct helium barrier (He) Controller coolant (air/GN₂) Oxidizer inlet feed system (GN₂/He) | |
| CRITICA1- | 117 | 1 | | - | | - | | |

Part C SSME OMRSD (Sheet 8 of 11)



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SSME OMRSD

(Sheet 9 of 11)

1

SSME Purges

FUEL SYSTEM PURGE ON 3 MINUTES FOR EACH 50 MINUTES IN PSN 3

(11+12016)

973

11.7

OXID INLET FEED SYB

(Sheet 10 of 11)

SSME OMRSD

Part C



RL10 Purges

| | REQUIREMENT | SSME A | PPLICATI | NO | 01V APP | I. I CAT I ON | NOTES |
|------|--|--------------|----------|----------|---------|---------------|--|
| | | INSTALLATION | ROUT INE | PERIODIC | 0661 | FUTURE | |
| | | | | | | | |
| me | ntal closures | | × | | | | Post-landing |
| Ξ | ght set | | 1 | | | | Prior to orbiter |
| ပမ | losure xit closures | | | | | | terry |
| ່ຍ | llant and hot gas systems | | I | | | | Prior to orbiter ferry |
|]e | bumpers | | 1 | | × | | Post-landing if en- gines have not been positioned down. Possible application to OTVE in a multi- engine configuration. |
| | | | | | | | |
| EQ | JIREMENTS | | | | | | |
| പ്പം | pplicable PERIODIC required to return the condition. | | | | | | |
| t t | is defined as ignition the SSME. | | | | | | |
| | | | <u></u> | | | | |

| DEFLECTOR TEST - DIAL INDICATOR VALVE ACTUATION VALVE ACTUATION SOLENDID VALVES (3) - VERIFY ACTUATION AUDIBLY AND BY TOUCH PROPFILANT VALVES (5) - VEBIEV ACTUATION AUDIBLY AND BY TOUCH | <u>LEAK CHECKS</u> <u>LEAK CHECKS</u> <u>OXIDIZER FLOW CONTROL AND PURGE CHECK VALVE LEAKAGE</u> OXIDIZER FLOWMETER AT TEST FIXTURE OXIDIZER AND FUEL SYSTEM EXTERNAL LEAKAGE LEAK DETECTION SOLUTION HELIUM SYSTEM INTERNAL LEAKAGE IN-LINE FLOWMETER AT SOLENOID VALVE VENTS | VISUAL INSPECTIONS OBVIDUS DAMAGE AND CONTAMINATION LOOSE CONNECTORS PROTECTIVE COVER, CLOSURE, AND DESICCANT REMOVAL | SUMMARY TOTALLY MANUAL - NO AUTOMATION REQUIRES SYSTEM VIOLATION AND EXTERNAL HODRIDS |
|---|---|--|---|
|---|---|--|---|

RL10 PRELAUNCH CHECKS - SUMMARY

Part D

- LEAK AND FUNCTIONAL CHECKS
- IGNITION SYSTEM
- ENERGIZE SYSTEM VISILALLY INSPECT END SOADK FONSTSTENCY

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Appendix 2

OTV Automated Preflight Methods - Approaches

I. Functional Checks

| Check | Approach | Sensors | /hardware | Selection | Comments |
|---------------------------------------|--|--|-------------|-----------|---|
| 1. Velve Actuator Checkout | A. Prelim Power Up Hardware conditioning has occurred Steedy state bank head idle conditions achieved Steedy state bank head idle conditions achieved Check made on transient to pump idle. Varily proper valve sequence occurs at power up Checks performed by sensors and computer Checks performed by sensors and computer Component pre-cycling Cycle valves electrically to verily actuator integrity Performed by sensors and controller C. Automated atatic checkout Historical data base for every valve Valve actuation at prior engine operation Electrical resistance measurements to verily actuator integrity | Current: - VDT, on/off Desition Sensor | :peour | ۵ | Currently automated on the SSME. A combination of approaches Band C will provide a high degree of confidence. |
| 2. Sensor checkout/ calibration | A. Prelim Power Up A. Prelim Power Up Hardware conditioning has occurred Steady state bank head idle conditions achieved Steady state on transient to pump ide. Verify normal searcers and computer Verify normal searcers and computer Clecks performed by sensors and computer Clecks performed by sensors and computer Component pre-cycling Precycling of sensors is considered a static check approach not applicable to this check Uses historical data bear Programmed inputs trom prior engine operation Performed by sensors and controller | urrent: | . pequanceq | U | Currently automated on the SSME. Note that checkout capab lifty needs to be designed into sensor. Approach C is a valid check and minimizes expended resources. |

I. Functional Checks (contd)

| Check | Approach | Sensors | /hardware | Selection | Comments |
|------------------------|---|---|-----------|-----------|--|
| 3. Drovenski | A. Prelim Power Up | Current: | Advanced: | U | Currently automated on the |
| component checkout | Hardwere conditioning has occurred Steady state tank head idle conditions achieved | ressure transducers, oressurized | | | check depends on the pneumatic system. Ideally this would be the |
| | Check made on parsent to pump role. Verify nominal pneumatic component functioning at power up Checks performed by sensors and controller | source. gas | | | iox pump intermediate seal purge and the injector shutdown purge. The checkout may not require |
| | B. Component pre-cycling | | | | anyming more man a look at me previous flight's valve actuation and ressure data |
| | programmed cycling sequence of pneumatic components performed by sensors and controller | | | <u></u> | |
| | C. Automated static checkout | | | | |
| | Historical data base pneumatic system operation from prior engine operation. | | | | |
| 4. Opera- tional | A. Prelim Power Up | Current: Pressure | Advanced: | 8 | Currently automated on the SSME. Simple sequence check |
| sequence test (FRT) | Hardware conditioning has occurred Steady state tark head idle conditions achieved Steedy state tark head idle conditions achieved Check medo on transient to pump idle. Veity nominal controller function (valve sequencing) at power up to assess fight readiness Checks performed by sensors and controller | transducers, LVDT, on/off position sensor | | | done with computer in combination with past history data would be sufficient. |
| | B. Component pre-cycling | | | | |
| | Verity nominal controller function through cycling of electrical valves and Prevunatic system Check performed by sensors and computer | | | | |
| | C. Automated statle checkout | | | | |
| | Historical data base Controller operation from prior engine operation Static controller electrical check | | | | |

I. Functional Checks (contd)

| Check | Approach | Sanaora | /hardwara | | |
|--|--|----------|-----------|-----------|---|
| 5. Control | A. Prelim Power Up | 202020 | | Calection | Comments |
| system re- dundancy verification | Hardware conditioning has occurred Steady state tank head idle conditions achieved Check made at pump idle. Include an interval of redundant tunctions Verify nominal controller redundant functions Checks performed by sensors and controller | | | 5 | Currently automated on the SSME. Uses an automated self-test. |
| | B. Component pre-cycling | | | | |
| | Redundant controller functions are checked statically Approach not applicable to check | | | | |
| | C. Automated static checkout | | | | |
| | Historical data base controller redundancy output from prior engine operation Programmed inputs to evaluate redundant control system integrity Performed by sensors and computer | | | | |
| 6. Controller | A. Prelim Power Up | Current: | Advanced: | U | Currentiv automated on the |
| memory verification | Controller memory check is performed statically Approach not applicable to check | | | | SSME. Uses an automated self- test. |
| | B. Component pre-cycling | | | - | |
| | Controller memory check is performed statically Approach not applicable to check | | | <u> </u> | |
| | C. Automated static checkout | | <u> </u> | | |
| | Historical data base Varify norminal behavior from prior engine operation Program to evaluate controller memory integrity performed by computer | | <u> </u> | | |
| | | | | | |

I. Functional Checks (contd)

| Check | Approach | Sensors | /hardware | Selection | Comments |
|--|--|---|---|-----------|--|
| 7. Controller zatiosuri- zatification verification | A. Prelim Power Up Hardware conditioning has occurred Steady state tank head kile conditions achieved Steady state tank head kile conditions achieved Check made at pump idla. Verity that controller casing is pressurized to corract level Checks performed by sensors B. Component pre-cycling Controller is factory sealed with inert gas at prescribed pressure Approach not applicable in performing check Automated static checkout Historical data base performed by sensors and computer performed by sensors and computer | Current: | Advanced: | υ | Currently automated on SSME. Controller will be factory sealed with inert gas. Simply check the internal pressure. |
| 8. HPOTP torque check | A. Prelim Power Up Hardware conditioning has occurred Hardware conditioning has occurred Seady state tarn's home of the conditions achieved Evaluate rpm vs. expected rpm at inlevant conditions Evaluate rpm vs. expected rpm at inlevant conditions Hardware of a constrained to the tarneose to home the home of the conditions Any result in damage or bootstrap to hall Pump ide check parformed by sensors and computer check parformed by sensors and computer check parformed by sensors and computer B. Component pre-cycling B. Component pre-cycling Transle incremental blasts of inent gas of increasing pressure until treateway brque measured frant gas spin system required may require electro mechanical system to broque the shaft increased weight and computer increased weight and computer increased weight and computer franting as spin system required increased weight and computer increased weight and complexity increased weight and computer increased weight and computer increased weight and computer increased weight and complexity increased weight and computer | Current: Pressure temperaturer sensor, speed sensor, pressurized in ert source. source. | Advanced: Ferturmspretic fiberophic deflectometer. deflectometer. | α | Use a torque meler and measure brque as the engine provers down from its prior run. This approach on its own however presents a problem with measuring an problem with measuring an torque which is why approach B is selected. |
I. Functional Checks (contd)

| Check | Approach | Senaore | hardwara/ | | |
|-------------------------------|--|---|---------------------------------|-----------|--|
| 9. HPFTP | See functional check #8 | 0 1001100 | | Selection | Comments |
| Check | | | | | |
| 10.LPOTP Torque Check - | See functional check #8 | | | | |
| 11.LPFTP Tornue | See functional check #8 | | | | |
| Check - | | | | | |
| 12. Turbo- | A. Prelim Power Up | | | | |
| pump axial shaft travel | • Hammers conditioning has a second | LVDT, | Advanced: Fiberoptic | U | Design bearing with deflectometer |
| check. | Steady state tank head ide conditions achieved Chock and control of the conditions achieved | accelerometer | deflectometer, isotopic wear | | this check may be deleted if |
| | Check performed by sensors appointed check performed by sensors and computer | | detector | | These bearings would accumulate negligible wear during start and |
| | B. Component pre-cycling | | | | shutdown. Contact for thrust bearings is minimal since they are |
| | Remotely move shaft axially to induce travel requires mechanical actuation avian | | | | used during transient periods only. |
| | performed by sensors and controller increased weight and complexity | | | | |
| | C. Automated static checkout | | | | |
| | Historical data base Bearing vibrational spectrum at prior engine operation Real time monitored bearing wear | | | | |
| 13. Eutorite | A. Prelim Power Up | Current: | Advanced. | | |
| cteck | Hardware conditioning has occurred Steady state tank head idle conditions achieved Check made on transient to pump idle Check performed by sensors and computer Check performed by sensors and computer Extendible nozzle deployed or not deployed during this time | ocelerometer, on/off position tensors | | 0 | Should need to axtend only when required during mission. Simple alignment sensors will provide necessary data. A robust gimballing mechanism should be employed to permit cycling for checkout purposes. |
| | B. Component pre-cycling | | | | |
| | Activate extendible nozzle actuation system Programmed gimballing sequence may be initiated as dynamic source to check travel performed by sensors and controller | | | | |
| | C. Automated Static Checkout | | | | |
| | Historical data base Extendible nozzle deployment/retraction at prior engine operation Verify correct positioning of extendible nozzle in current configuration | | | | |

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I. Functional Checks (contd)

| 14. Ignite: A. Prailin Power Up Pre-cycling is the bear static electrical transmerses to the conditioning has occurred Pre-cycling is the bear static electrical transmerses to the conditioning has occurred • Hardware conditioning has occurred • Hardware conditioning has occurred • Electrical transmerses to the condition achieved • Fre-cycling is the bear static electrical transmersion at power up • Unmated • Seedy state tank head idle conditions achieved • Check made on transient to pump idle. • Check partmerses and computer • Check performed by sensors and computer • Check performed by sensors and computer • Check performed by sensors and computer B. Component pre-cycling • Cycle igniter to verity intagrity • Cycle igniter to verity intagrity • Historical data bese • Igniter integrity • Igniter integrity • Historical data bese • igniter integrity • igniter integrity | Check | Approach | Sensors | /hardware | Selection | Comments |
|---|-------------|---|----------|-----------|-----------|---|
| Hardware conditioning has occurred currently Hardware conditioning has occurred currently Steady state tank head idle conditions achieved Check performed by sensors and computer Check performed by sensors and computer Component pre-cycling Cycle igniter to verify integrity Performed by sensors and computer C. Automated attatic checkout Historical data base Electrical resistance measurements to verify integrity Electrical resistance measurements to verify integrity | 14. Igniter | A. Prelim Power Up | Current: | Advanced: | 0 | Pre-cycling is the best approach |
| Check made on transient the purp dia. Check made on transient to purp dia. Verify igniter operation at power up Checks performed by sensors and computer Checks performed by sensors and computer Cycle igniter to verify integrity Ecomponent pre-cycling C. Automated attaic checkout Historical data base Instruction more regine starts. Electrical resistance measurements to verify igniter integrity | Currently | Hardware conditioning has occurred Stearty arts hear head rids conditions arbitrate | | | | since static electrical check on its own may be misleading. Spark |
| Very ignite operation at power up Very ignite operation at power up Checks performed by sensors and computer Cycle igniter to verify integrity Cycle igniter to verify integrity Performed by sensors and computer Comment attacts and computer Cycle igniter to verify integrity Flucturated attacts area computer Sector attacts and computer Flucture operation from prior engine starts. Electrical resistance measurements to verify igniter integrity | | Creardy along any read the control active of Creardy made on transient to pump idle. Vieto 1 | | | | rate and intensity are critical issues because of propellant |
| B. Component pre-cycling Cycle igniter to verify integrity Performed by sensors and controller Performated static checkout Historical data base Instorical data base Electrical resistance measurements to verify igniter integrity | | vering ignition operation at power up Checks performed by sensors and computer | | | | accumulation. |
| Cycle igniter to verify integrity Performed by sensors and controller Automated static checkout Historical data base Igniter operation from prior engine starts. Electrical resistance measurements to verify igniter integrity | | B. Component pre-cycling | | | | |
| C. Automated static checkout Historical data base Electrical resistance measurements to verify igniter integrity | | Cycle igniter to verity integrity Performed by sensors and controller | | | | |
| Historical data base igniter operation from prior engine starts. Electrical resistance measurements to verify igniter integrity | | C. Automated static checkout | | | | |
| | | Historical data base Igniter operation from prior engine starts. Electrical resistance measurements to verify igniter integrity | | | | |

II. Leak Checks

| Check | Approach | Sensors | /hardware | Selection | Comments | |
|----------|--|--|-----------|-----------|--|--|
| 1. HPOTP | A. Prelim. power-up | Current: | Advanced: | U | Drain line pressure monitor is | |
| Lox see | Hardware conditioning has not completely occurred. Engine Start condition (just prior to Tank head idle) Propellant dropped to MOV. Temperature measured at lox seel drain cavity | Pressure transducer, temperature sensor, flowmeter, | | | probably all that is needed to show seel degradation. | |
| | Component Pre-cycling | pressurized inert gas supply | | | | |
| | Lock-up system at MOV and GOV. Preseurize with inert gas. Thermodynamic conditions measured at lox seal drain cavity System lock-up performed by controller Checks performed by sensors and computer | | | | | |
| | C. Automatic static checkout | | | | | |
| | Use historical data base Lox seal drain cavity temperature and pressure at prior engine Uses trend analysis | | | | | |
| 2. HPOTP | A. Prelim. power-up | Current: | Advanced: | U | Can also be checked just prior to | |
| seal | Hardware conditioning has occurred Steady state tank head idle conditions achieved Check made on transient to pump idle. Temperature measured at informadiate lox seal drain cavity Checks performed by sensors and computer | Pressure transducer, temperature sensor, pressurized inert gas supply | | | start for verification | |
| | B. Component Pre-cycling | | | | | |
| | Remotely activate seal purge system Measure intermediate lox seal supply and drain cavity pressure Checks performed by sensors and computer | | | | | |
| | C. Automatic static checkout | | | | | |
| | Use historical data base Intermediate Lox seal supply and drain cavity temperatures and pressures at prior engine opeation. Uses trend analysis | | | | | |

| Check | Approach | Sensors | /hardware | Selection | l Comments |
|---------------------------------|--|---------------------------------|-----------|-----------|--|
| 3. Main | A. Prelim. power-up | Current: | Advanced: | Ο | Ox. Tank valve is constantly leak |
| oxidizer valve ball Seals | Hardware conditioning is occurring. Check partormed when MOV is closed | iskin temperature eeneor | | | checked because Lox propellant is constantly against it. HPOP |
| | Measure leakage past MOV ball seal with skin temp sensors Check performed by sensors and computer | | | | Intermediate seal purge read. When propellant introduced into engine. So purge assumption is |
| | B. Component Pre-cycling | | | | justified. |
| | Assumes purge line added just downstream of Ox. inlet valve. Lock-up system at MOV and GOV. Pressurize with inert gas. Measure leakage past MOV ball seal with skin temp sensors System lock-up performed by controller Checks performed by sensors and computer | | | | |
| | C. Automatic static checkout | | | | |
| | Use historical data base Lealage past ball seel at prior starts as engine is chilling down. Check performed by sensors and computer. | | | | |
| 4. Main fue vetre hell | l A. Prelim. power-up | Current: | Advanced: | C | |
| 1808 1908 | Hardware conditioning has not completely occurred. Engine start condition (just prior to tank heed idle) Propellant dropped to MFV Measure leakage past MFV ball seel with skin temp sensors Check performed by sensors and computer | skin temperature sensors, | | | During stand-by or long term storage, propellants are stored in vehicle tanks. The tank pre-valve is always sell-checked since it will always tave a closing pressure or a soring closing force |
| | B. Component Pre-cycling | | | | applied. |
| | Check performed prior to engine start Assumes purge line added just downstream of Fuel inlet valve. Lock-up system at MFV Lock-up system at MFV Ressurize with inent gas. Measure leakage past MFV ball seal with skin temp sensors System lock-up performed by controller Checks performed by sensors and computer | | | | |
| | C. Automatic static checkout | | | | |
| | Use historical data base Leakage past ball seal at prior starts as engine is chilling down. Check performed by sensors and computer. | | | | |

| Check | Approach | Sensors | /hardware | Selection | - Common |
|--|---|---|-----------|-----------|---|
| 5. Puralise | A. Prelim. power-up | Current: | Advanced: | 0 | |
| rropenarn vaive primary shaft seels | Hardware conditioning has not completely occurred. Engine start condition (just prior to tank head idle) Propellant dropped to MFV | Pressure transducer, temp sensor | | | this is generally not a problem due to vacuum environment in space to provide venting - the need for this check needs to be |
| | Measure leakage of shart seals by monitoring temperature at dynamic seal port Check performed by sensors and computer | | | | |
| | B. Component Pre-cycling | | | | |
| | Assumes purge line added just downstream of Fuel inlet valve. Lock-up system at MFV Pressurize with inert gas. Measure leakage of shaft seals by monitoring temperature and pressure at obratine seal portioned by controller System lock-up performed by controller | | | | |
| · | Unecks performed by sensors and computer Automatic static obsciout | | | | |
| | Use historical data base Leakage past shaft seal at prior starts and shutdowna. Check performed Y sensors and computer. | | | | |
| 6. | A. Prelim. power-up | Current: | Advanced: | 0 | Svetom Inck-un with accounts |
| rneumauc control assembly internal seals | Hardware conditioning has occurred Steady state stark head idle conditions achieved Check made on transient to pump idle Verify nominal pneumatic system supply pressures during power up Checks performed by sensors and controller | LVDT , on/off position sensor, pressurized inert gas source. | | | decay will be a concerpt with pressure decay will satisfy the requirement in combination with past history data. Note that leakage itself is not the problem since the gas is inert. |
| | B. Component Pre-cycling | | | | |
| | Check performed prior to engine start Lock-up pressure in PCA (pneumatic control assy) May require marry pressure transducers and on/off valves Measure pneumatic system decay System lock-up performed by controller Checks performed by sensors and computer | | | | |
| | C. Automatic static checkout | | | | |
| | Use historical data base Monitor preumatic system operation Check performed by sensors and computer, Uses freed analysis, a plot increase in leakare rate | | | | |

| Check | Approach | Sensors | /hardware | Selection | Commente | |
|----------------------|---|--|-----------|-----------|---|--|
| 7. Heat exchencer | A. Prelim. power-up | Current: | Advanced: | 8 | The lock-up with pressure decay | |
| coil leak test | Approach not applicable in performing check. Recommended that check must be performed prior to power up because of dangerous conditions imposed. | Pressure ransducer, lemp sensor, lowmeter | | | may be the best approach. However, the leakage may be tho small to detect and still presents a denominan Lasters | |
| | B. Component Pre-cycling | | | | in the checkout isolation valve may also invalidate the results | |
| | Assumes purge line added just downstream of Ox. inlet valve. Lock-up system at MOV and GOV. Pressurize with inert pas. | | | | This check can be eliminated by utilizing a highly robust heat exchanger design | |
| | Monitor pressure decay System lock-up performed by controller Checks performed by sensors and computer May not depact small leaks. | | - | | | |
| | Possible checkourt isolation valve leateage | | | | | |
| | G. Automatic static checkout Use historical data base | <u> </u> | | | | |
| _ | Monitor pressure, temperature and flow conditions at heat exchanger inter and exits. Provides data base for Heat exchanger health assessment | | | | | |
| | Check performed by sensors and computer. Leak check (specifically small leaks) not accomplished using this method | | | | | |

| Current: Advanced: | Pressure must be performed prior to power up because of temp sensors, posed. | pressurzeo inent gas source. | l just downstream of Ox. inlet valve. 3OV and lox tank check valve. 3.1.25 times max operating pressure. | by controller ors and computer ted valve in tank pressurization line upstream of | | performing check operating condition to perform proof test termoerstrute and flow conditions at heat | and exits. es for Heat exchanger health assessment ins and computer. |
|---------------------|--|---|--|---|---|--|---|
| A. Prellm. power-up | Approach not applicable in Becommended that check i dangerous conditions inp | B. Component Pre-cycling Check performed prior to er | Assumes purge line added Cock-up aystam at MOV, G Presurize with inert gas to Monitor pressure docav | System lock-up performed Checks performed by sens Requires electrically actual tark check valve | May not detect small leaks C. Automatic static checkout | Approach not applicable in Need 1.25 times maximum Use historical Data base Monibr Pressue | exchanger iniet a exchanger iniet a • Exhibited anomalis • Provides data bas • Check performed by sensol • Provid sat not restructed |

| Check | Approach | Sensors | /hardware | Selection | Comments |
|----------------------|---|-----------------------------|---------------------------|-----------|--|
| 9. Thrust chember | A. Prelim. power-up | Current: | Advanced: | c | Use trend analysis (C): design |
| assembly | Hardware conditioning has occurred | Pressure transducer, | Optical leak detection | | hardware for slow consistant degradation (if any) Best to |
| outer walls | Steady state tank head rule conditions achieved Check made on transient to pump idle. | Temp sensor, flowmeters, | system | | eliminate this check and stick with a robust design. |
| | External leakage directable Internal leaks (into T/C core) present no problem | pressurized inert gas | | | |
| | Leakage also indicated by performance degradation (Pc vs. flow) Checks performed by sensors and computer | source | | | |
| | B. Component Pre-cycling | | | | |
| | Approach not applicable in performing check System cannot be isolated and pressurized | | | | |
| | Throat plug placed using robotic arm seems impractible but is an option Adds complexity and weight | | | | |
| | C. Automatic static checkout | | | | |
| | • Use historical data base - Evamel Indusor data from sociona ancoration | | | | |
| | Thrust thamber cosing jacket life prediction model Used Them derivatives the prediction model Used Them derivatives | | | | |
| 10. | A. Prelim. power-up | Current: | Advanced: | J | Optical leak detection may be the |
| tion and | Hardware conditioning has occurred | transducer. | opucal Heak detection | | Dest approach (C). Note that SSMF checks only dishirhed |
| propellant | · Steedy state tank head idle conditions achieved | pressurized | system | | joints. With this groundrule, this |
| system ininte | Check made on transient to pump idle. External lastance discrete descented. | inert gas | | | check might possibly be |
| ettinof | Checks performed by sensors and computer | supphy. | | | eliminated. |
| | B. Component Pre-cycling | | | | Detection may be easier by designing system with a minimal |
| | the day and the second | | | | number of joints. Also, this check |
| | Approach not approache in periorming check. System cannot be isolated and pressuricated Thinca thic nation ration rations are are invariable but is an ordion | | | | welded joints. The system can be welded joints. The system can be |
| | Adds complexity and weight | | | | turbopump interfaces. |
| | C. Automatic static checkout | | | | |
| | Use historical data base External leakace data from previous enoine operation | | | | |

III. Inspections

| Check | Approach | Sensors | /hardware | Selection | Comments |
|----------------------|--|--------------------------|---|-----------|--|
| 1. Exterior | A. Preliminary power-up | Current: | Advanced: | 0 | The practicality of the visual |
| damage/ security | Approach not applicable in performing check Required data consists of visual data only to assess condition of the engine exterior | | Remote Automated visual inspection | | inspection system needs to be assessed. Without this system , this check should be eliminated while in free space |
| | B. Component pre-cycling | | system | | |
| | Approach not applicable in performing check Required data consists of visual data only to assess condition of the engine exterior | | | | |
| | C. Automatic static checkout Use of historical data base Comparison of a series of superimposed images each covering a particular view or angle Remote real time viewing | | | | |
| 2. Thrust Chamber | A. Preliminary power-up | Current: | Advanced: | J | Delta-P trend analysis is a simple |
| Assembly | Hardware conditioning has occurred Socrational rate and rate occurred | Transducer, | Automated | | accurate approach. |
| evidence | Check made on transient to pump idle. | skin temp sensor, | visual inspection | | All indicated methods detect |
| Dessage | Measure pressure drop across cooling jacket. Check performed by sensors and computer | pressurized inert gas | system | | individual passage blockage would be difficult and require |
| | B. Component pre-cycling | source | | | many sensors or multiple thermal imaging cameras. |
| | Requires inert gas flow through hot gas system Messure pressure drop across cooling jacket Check performed by sensors and computer Requires large volume of inert gas | | | | |
| | C. Automatic static checkout | | | | |
| | Use of historical data base Cooling jacket pressure drop profiles at prior engine operation Check performed by sensors and computer Hot spot darmage may be seen using remote visual techniques | | | | |

III. Inspections (contd)

| Check | Approach | Sensors | /hardware | Selection | Comments Comments |
|---|---|---|------------------------------------|-----------|---|
| 2. mm-r.p. Wheele Diades for cracks,fa- tigue and demnage | A. Preliminary power-up Hardware conditioning has occurred Steady state tank head idle conditions achieved Steady state tank head idle conditions achieved Steady state tank head idle conditions achieved Steady state tank head idle conditions and RPM and compare to expected RPM those conditions Measure housing vibration Check performed by sensors and computer This approach does not detect fatigue or damage on non-rubbing surfaces B. Component pre-cycling Inert gas spin will not provide realistic conditions to assess turbine weekblades for wheer and damage Approach not applicable in performing check C. Automatic atatic checkout Use of historical data base Conditions (vibration and thermodynamic) monitored during prior engine operation Check performed by sensors and computer Check performed by sensors and computer Check performed by sensors and computer Check performation | Current: Pressure transducer, serect speed sensor, flowmeter acelerometer acelerometer | Ad vanced: Optical pyrometer | υ | The easiest approach would be to go with a high factor of safety/ robust design and look for signs of performance degradation. |
| 4. LPFTP turbine whee/ blades for cracks, fatigue, and damage | See Inspection #3 | | | | |
| 5. HPOTP Turbine whee/ blades for cracks, fatigue,and damage | See Inspection #3 | | | | |
| 6. LPOTP turbine whee/ blades for cracks, fatigue,and damage | See Inspection #3 | | | | |

III. Inspections (contd)

| Check | Approach | Sensors | /hardware | Salaction | tremmo |
|---|--|---|--|-----------|---|
| 7.HPOTP Bearings for Demage | A. Praliminary power-up Hardware conditioning has occurred Steady state tank head idle conditions achieved Check made on transient to pump idle. Steady state tank head idle conditions achieved Check made on transient to pump idle. Measure bearing vitrational spectrum at turbine spin-up Check parformed by sansors and computer Check parformed by sansors and computer Component pre-cycling Performed pre-cycling Decorporant pre-cycling Performed prior to engine start Heat gas to spin turbine Instrig as spin system required Increased weight and complexity C. Automatic static data base Component pre-cycling Increased weight and complexity C. Automatic static data base C. Automatic static data base Torque measurements along shut-down bareient Check performed by ware detection Check performed by ware detection Check performed by ware detection Use of historical data base | Current: strain gauges,acceler ometer, | Ad van ced: fiberoptic define spectrometer, isotope wear detector, ferromegretic torque meter | υ | This inspection may also be required for the fuel turbopump if the requirement is based on more than the possibility of LOX/H2 mixing. If Hydrostatic bearings are an option, possible requirements for preflight checks on hydrostatic bearings needs to be investigated. |
| 8. TC Assembly injector ioniter and lox post burning. burning. mination. | A. Preliminary power-up A. Preliminary power-up Hardware conditioning has occurred Steardware conditioning has occurred Steardware burne analyzed for contamination Check performed by sensors and computer printe cycled during functional check Technique does not provide all data required for inspection Approach not applicable in performing check B. Component pre-cycling B. Component pre-cycling Component pre-cycling<!--</td--><td>Current: Pressure transducer, temperature flowmeter</td><td>Ad vanced: Plume spectrometer, automote visual inspection.</td><td>U</td><td>Visual inspection seems impractical due to the inaccessibility of the injector and vc interior to a fixed remote visual system. Performance parameters can monitored for degradation. Possible design improvements to components may eliminate check.</td> | Current: Pressure transducer, temperature flowmeter | Ad vanced: Plume spectrometer, automote visual inspection. | U | Visual inspection seems impractical due to the inaccessibility of the injector and vc interior to a fixed remote visual system. Performance parameters can monitored for degradation. Possible design improvements to components may eliminate check. |

III. Inspections (contd)

| Check | Approach | l Sensors | /hardware | Selection | l Commente |
|---|---|--|--|-----------|--|
| Gimbal bearing and TVC and TVC and TVC point for evidence of bearing seizure and fatigue. | A. Preliminary power-up Hardware conditioning has occurred Steady state tank head idle conditions achieved Steady state tank head idle conditions achieved Steady state tank head idle conditions achieved Check made on transient to pump idle. Measure excessive vibration at TVC attach points and gimbal bearing Check performed by sensors and computer Technique does not provide all data required for inspection B. Component pre-cycling Gimaballing of the angine over the preacribed range will indicate gimbal bearing and TVC attach point damage (see functional direct 14). Check performed by sensors and computer Use of historical data base | Current: allignment sensor, acceler ometers | Ad van ced: Ramois automated visual inspection | đ | Check the gimbal pattern by cycling the nozzle. Torque required to gimbal may be masured using electro-magnetic actuators. Because this involves tasting the functioning of the gimballing mechanism, it will be changed to a functional check. |
| 10. Heat exchanger for cracke, of wear, demage | Vibration of gimbal bearing and TVC attach points at previous engine operation Vibration of gimbal bearing and TVC attach points at previous engine operation Torque required for gimballing during prior engine operation Varity correct positioning of nozzle Verity correct positioning of nozzle Checks performed by sensors and computer Torque attalysis applicable A. Preliminary power-up Hardware conditioning has occurred Steady state tank head life conditions achieved Checks partomed by the conditions achieved Checks partomed by the conditions achieved Check made on transient to pump idla. View surface remotely for presence of hot spots Hardware conditioning has occurred Steady state tank head life conditions achieved Check partomed prior be engine attracted to the spots Hardware the made on the pump idla. Component pre-cycling Check partomed prior be engine start Component pre-cycling Check performed by for presence of hot spots Hardware attraction is to measure exiternal leakage from heat exchanger to indicate tailing Component pre-cycling Check performed prior be engine start Consolicitable in performing check C. Automatic effection High resolution High resolution views of surface High resolution Checks performed visually sensitive surface costing for hot spot detection | Current: Pressure transducer, fowmstansor, fowmatant gas source | Advanced: remote sutomated visual inspection | υ | Performance data can be used to assess heat exchanger health. A robust design rationale can eliminate this check |

IV. Servicing Tasks

| Check | Approach | Sensors | /hardware | Selection | Comments |
|--|---|---|-----------|-----------|---|
| 1. Combus- tion zone drying Pc sensors and igniter valves valves | A. Preliminary power-up This servicing task is done at engine shudown Approach not applicable in performing servicing task B. Component pre-cycling Shutdown purge lox from injector Shutdown purge lox from injector Appy a quick drying blast to remove any water from MCC Accum environment in space is helpful C. Automatic etails checkout Approach not applicable in performing servicing task | Current: Presurized inert gas Bource | Advanced: | | See J-2 space restart data |
| 2. HPOTP LovTurbin e drive gas intermediat start purge start purge | A. Preliminary power-up hardware conditioning has accurred Steady state bank head ide conditions achieved Eurge done as part of normal pre-start procedure Prover up in itself is not a means for performing this task approach not applicable B. Component pre-cycling Servicing performed as part of normal pre-start procedure Approach not applicable in performing servicing task | Current: nert gas source | Advanced: | ۵ | Purge required - See groundrules and assumptions - preumatic system |

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Appendix 3

Issues and Benefits of Preflight Methods

Page 82 Part A - Issues and Benefits of Preflight Methods - General Approach Descriptions

| Preflight Checkout | Approach | | Issues and Benefits | | Comments |
|-----------------------|---------------------------------------|--|--|---|----------|
| | | Space Basing | Vehicle/Infrastructure | Engine system | |
| | Preliminary Power-up | Issues: Deployment of vehicle may result, particularly if prelfight checks occur while vehicle is in orbit. Determination/resolution of problems too late to avoid missing launch window. Additional checkout hardware will have to be designed to withstand the space environment for long durations. Benefits: Minimum maintenance requirement. | Issues: Use of propeliants required to perform checkouts. Additional propeliant may be required to recover the vehicle if deployed unintentionally. Short fire-up period required - possibly several seconds. Benefits: No requirement for sophisticated condition monitoring sensors and historical data base. | Start transient conditions are severe. May cause damage to system. Minor damage detectable by other means may otherwise propogate. May reduce the life of some components due to additional hot firing. Benefits: Actual hot-fire conditions for realistic assessment of engines readiness to fire. Preliminary power-up approach is part of routine engine start procedure prior to mission. Therefore, this approach can be used redundantly no matter which preflight checkout approach is selected. | |
| | Automated Component Pre-cycling | Additional checkout hardware will have to be designed to withstand the space environment for long durations. Greatest maintenance requirements. Benefite: Degradation during space storage evaluated. | Allowable vehicle payload impacted by the weight and volume of mechanical and electrical hardware required for emulating dynamic conditions. This includes a large supply of pressurized inert gas. Benefite: To Be Determined | Additional hardware may reduce the reliability of the engine and possibly result in additional failure modes. Benefite: Inert conditions for checkouts. Assessment based on actual cycling of components. | |
| | Automated Static Checkout | Issues: Condition monitoring sensors will have to be designed to withstand the space environment for long durations. Degradation of components during downtime just prior to preflight check must be considered in historical database. Additional checkout hardware will have to be designed to withstand the space environment for long durations. Benefite: Minimum space maintenance. | Issues: • Requires extensive data mass storage capabilities which may impact the allowable vehicle payload due to weight and volume. • Requires the most sophisticated integrated control and health monitoring system of all approaches suggested. Benefits: • Remaining life prediction based on accurate analytical methods and life prediction models. • Possibly more rapid checkout sequence since performed statically. | Many sensors will be required for an accurate assessment of engine readiness to fire. Many condition monitoring sensors are necessarily intrusive. Sensors will require a high degree of acuracy and reliability for complete condition assessments. Benefite: Component life not impacted by checkout approach since no components are cycled. | |

Part B - Issues and Benefits of Preflight Methods - Functional Checks

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|---------------------------------|------------------------------|--|--|----------|
| 1. Valve actuator Check | a. Prelim. power-up | Benefite: • See references | General Approaches • Preliminary Power up | |
| | | | Sensors/Hardware • Resolver Position sensor • Eddy current position sensor | |
| | | | Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | • Requires power consumption for actuation. | General Approaches • Automated component precycling | |
| | | Benefite: • Approach can demonstrate full range of actuator operation | Sensors/Hardware • Resolver Position sensor • Eddy current position sensor | |
| | | | Alternate Design Recommendations • r/a | |
| | c. Automated static | Loss not adequately assess degradation during idle period. cannot address full range of actuator operation Benefita: | General Approaches • Automated static check Sensors/Hardware • Resolver Position sensor • Eddw current position sensor | |
| | | Requires minimal power consumption | Alternate Design Recommendations | |
| 2. Sensor check/calibration. | a. Prelim. power-up | High risk aproach to sensor check and calibration. Low level power-up may not provide sufficiently stable operation to allow sensor calibration. | General Approaches • Preliminary Power up Sensors/Hardware • n/a | |
| | | provides complete end-to-end sensor system checkout Provides mechanical input required to check dynamic sensors. | Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Check of dynamic sensors (speed, torque, acceleration, valve postion,etc.) requires additional complexity of actuation systems and power consumption. | General Approaches • Automated component pre-cycling Sensors/Hardware •n/a | |
| | | Benefits: • Provides complete end-to-end sensor checkout | Atternate Design Recommendations • r/a | |
| | c. Automated static | Issues: • Only checks sensor elements for continuity, does not identify all sensing element problems. | General Approaches • Automated Static check | |
| | | Benefits: | Sensore/Hardware +n/a | |
| | | Provides sufficient level of confidence for the operational requirements of most systems | Alternate Design Recommendations • r/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|---------------------------------------|------------------------------|---|--|----------|
| 3. Pneumatic Component checkout | a. Prelim. power-up | Benefite: • Provides most complete checkout of system | General Approaches • Preliminary Power up Sensors/Hardware • Pressure Transducer Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Functional checkout requires power consumption for valve actuation. Benefits: provides excellent functional checkout of pneumatic valves and actuators. | General Approaches • Automated Component precycling Sensors/Hardware • Pressure transducer Alternate Deelgn Recommendations • n/a | |
| | c. Automated static | Issues: • Only provides partial system checkout Benefits: • Minimum power consumption required | General Approaches • Automated static check Sensors/Hardware • Pressure transducer Alternate Dealgn Recommendations • r/a | |
| 4. Operational sequence test | a. Prelim. power-up | Benefite: • Provides most complete checkout of system | General Approaches • Preliminary Power up Sensors/Hardware • Resolver Position sensor • Eddy current position sensor • Pressure transducer Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | Requires power consumption for valve actuation Benefits: Provides most complete checkout with minimal risk to engine or vehicle | General Approaches • Automated component precycling Sensors/Hardware • Resolver Position sensor • Eddy current position sensor • Pressure transducer Alternate Design Recommendations • n/a | |
| | c. Automated static | Issues: • Does not provide complete checkout of system Benefite: • Requires minimal power consumption | General Approaches • Automated static check Sensors/Hardware • Resolver Position sensor • Eddy current position sensor • Pressure transducer Alternate Design Recommendations • r/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|---|---|--|---|----------|
| 5. Control systems redundancy check | a. Prelim. power-up | Issues: • High risk to engine to investigate system redundancy during engine operation Benefits: • See references | General Approaches • Preliminary Power up Sensors/Hardware • n/a Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | Not Applicable | | |
| | c. Automated static | Allows verification of electrical systems only Benefits: Provides high level of confidence in system with minimal risk | General Approaches • Automated static check Sensore/Hardware • n/a Alternate Design Recommendations • n/a | |
| 6. Controller memory verification | a. Prelim. power-up | Not Applicable | | |
| | b. Automated pre- cycling | Not applicable | | |
| | c. Automated static | Issues: • Past history data not required Benefits: • Simple electrical check providing high level of confidence for safe operation | General Approaches - Automated static checkout Sensors/Hardware - r/a Alternate Design Recommendations - r/a | |

Page 86 Part B - Issues and Benefits of Preflight Methods - Functional Checks (contd.)

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS REFERENCES | COMMENTS |
|---|------------------------------|--|---|---|
| 7. Controller pressurization verification | a. Prelim. power-up | Issues: • Power-up not required - Simple static check may be performed without firing engine. Benefits: • see references | General Approaches • Preliminary power up Sensors/Hardware • Pressure transducer Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Not Applicable | n/a | |
| | c. Automated static | Issues: • Past history data may not be applicable here. Simple static check may be all that is required. Benefits: • Simple pressure check is adequate. | General Approaches • Automated static checkout Sensors/Hardware • Pressure transducer Alternate Design Recommendations • rva | |
| 8. HPOTP torque check 9. HPFTP torque check 10. LPOTP Torque check 11. LPFTP torque check. | a. Prelim. power-up | Breakaway torque can't be measured at spin-up or power down. Benefite: could provide excellent condition evaluation with proper instrumentation. | General Approaches • Preliminary power -up Sensors/Hardware • Ferromagnetic torquemeter Alternate Design Recommendations • Hydrostatic bearings | Modification to the turbopump torque checks would be required to accommodate the use of hydrostatic bearings. This applies to all approaches. |
| | b. Automated pre- cycling | Issues: • Highly sensitive torquemeter required for measurement of small breakaway torque. • Remote spin system would likely be heavy, complex, and require significant power consumption. Benefits: • Safest method for providing dynamic evaluation of pump systems. | General Approaches • Automated component precycling Sensors/Hardware • Ferromagnetic torquemeter Alternate Design Recommendations • Hydrostatic bearings | |
| | c. Automated static | Issues: • Not a complete system checkout • Requires extensive statistical data base to justify the use of this approach Benefite: • Provides lightest, simplest checkout with little power consumption | General Approaches • Automated static checkout Sensors/Hardware • Ferromagnetic torquemeter Alternate Design Recommendations • Hydrostatc bearings | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|--|------------------------------|---|--|---|
| 12. axial shaft travel check | a. Prelim. power-up | Issues: • If significant wear present the T/P could be further damaged during power-up Benefits: • Component integrity verified in dynamic hot-fire environment. | General Approaches: • Preliminary power-up. Sensors/Hardware: • Fiberoptic deflectometer. • Isotopic wear detector. Alternate Design Recommendations: • Hydrostatic bearings. | |
| | b. Automated pre- cycling | Issues: • Extra weight and complexity of mechanical actuation system. Benefits: • Assesses bearing integrity without T/P rotation which could result in damage if bearings are worn. | General Approaches: • Automated component precycling. Sensors/Hardware • Mechanical actuation system. • Displacement sensor. Alternate Design Recommendations: • Hydrostatic bearings | |
| | c. Automated static | Issues: • Axial translation during next start transient may not be predictable from previous firing steady state bearing vibration spectrum. • Requires extensive statistical data base. Benefits: • No additional hardware for displacement. | General Approaches: • Automated static checkout. Sensors/Hardware: • Fiberoptic deflectometer. • Isotopic wear detector. Alternate Design Recommendations | |
| 13. extendible nozzle travei check | a. Prelim. power-up | Lissues: Check may not require power-up - simple position check during gimballing sequence may be all that is necessary. Risk and propellant consumption does not justify added fidelity to nozzle travel check Benefits: Vibration magnitude at extendible nozzle attach point may give an accurate assessment of travel. Provides closest simulation of actual operating conditions. | Hydrostatic bearings. General Approaches Preliminary power -up Sensors/Hardware Accelerometer Eddy current position sensor Alternate Design Recommendations rva | Since gimballing and nozzle extension / retraction will occur for checkout purposes, the actuating and control mechanisms for these processes should be highly robust. |
| | b. Automated pre- cycling | Issues: • Requires robust gimballing mechanism and nozzle actuator mechnism since full range gimballing required for checkout purposes. • requires power consumption for actuation. Benefits: • provides greatest confidence for safe operation for any low risk checkout method. | General Approaches • Automated Component precycling Sensors/Hardware • Accelerometer • Eddy current position sensor Alternate Design Recommendations • n/a | |
| | c. Automated static | Issues : • Does not adequately assess degradation during idle period. Benefite: • low power consumption | General Approaches • Automated static checkout Sensors/Hardware • Accelerometer • Eddy current position sensor Alternate Design Recommendations • r/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS | COMMENTS |
|----------------------------------|------------------------------|---|--|----------|
| 14. Igniter Operational check | a. Prelim. power-up | Issues: • Special preliminary power up verification provides no advantage over verification during operational start-up. Benefits: • see references | General Approaches • Preliminary power -up Sensors/Hardware • r/a Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Issues: • Igniter must be highly reliable and robust to accomodate many checkout cycles, • spark check requires power consumption Benefite: • Allows verification of proper system operation prior to introduction of propellants | General Approaches - Automated component precycling Sensors/Hardware - r/a Alternate Design Recommendations - r/a | |
| | c. Automated static | Issues: • Continuity and past history may not provide complete assessment. Cycling should be included. Benefite: • see references | General Approaches • Automated static checkout. Sensors/Hardware • n/a Alternate Design Recommendations • n/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS REFERENCES | COMMENTS |
|-------------------------------|------------------------------|--|---|----------|
| 1. HPOTP primary Lox seal | a. Prelim. power-up | Issues: • Offers no advantage over monitoring redline pressure during operation Benefits: • see references | General Approaches • Preliminary power -up Sensors/Hardware • Temperature sensor Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | Issues: • increases helium consumption required for normal seal operation. Benefits: • verifies system operation prior to introduction of propellants | General Approaches • Automated component precycling Sensors/Hardware • Pressure transducer • Turbine flowmeter Atternate Design Recommendations • r/a | |
| | c. Automated static | Issues: • Does not adequately assess degradation during idle period. Benefits: • see references | General Approaches • Automated static check Sensors/Hardware • Temperature sensor Alternate Design Recommendations • r/a | |
| 2. HPOTP intermediate seal | a. Prelim. power-up | Issues: • Past history data provides no advantage over monitoring redline pressure during operation. Benefits: • see references | General Approaches • Preliminary power -up Sensors/Hardware • Temperature sensor Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Issues: • Increases helium consumption required for normal seal operation. Benefits: • Verifies system operation prior to introduction of propellants | General Approaches • Automated component precycling Sensors/Hardware • Pressure transducer • Turbine flowmeter Alternate Design Recommendations • n/a | |
| | c. Automated static | Does not adequately assess degradation during idle period. Benefits: see references | General Approaches • Automated static checkout Sensors/Hardware • Temperature sensor Alternate Design Recommendations • r/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|-------------------|------------------------------|---|---|----------|
| 3. MOV Ball seals | a. Prelim, power-up | Seal integrity cannot be thoroughly evaluated | General Approaches • Preliminary power -up | |
| | | during short power-up. Benefits: | Sensors/Hardware | |
| | | • see references | Alternate Design Recommendations | |
| | h Automated pre- | | | |
| | cycling | Inert gas may not give large enough temp difference to be detected by skin temp sensors - | General Approaches • Automated component precycling | |
| | | cryogenic may be preferable. • Requirement for extra propellant if cryogenics are used. | Sensors/Hardware • Temperature sensor | |
| | | Difficult to detect small leakage rates due to mild test conditions. | Alternate Design Recommendations • n/a | |
| | | Benefits: | | |
| | Automated | Simple to perform pressure lock-up and monitor system pressure decay | | |
| | static | Past history data does not adequately assess degradation during idle period | General Approaches • Automated static check | |
| | | Benefits: | Sensors/Hardware • Temperature sensor | |
| | | • see references | Alternate Design Recommendations • r/a | |
| 4. MFV Bail seals | a. Prelim. power-up | Issues: | | |
| | | seal integrity cannot be thoroughly evaluated during preliminary power-up. | General Approaches • Preliminary power -up | |
| | | Benefits: | Sensors/Hardware • Temperature sensor | |
| | | • see references | Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | Issues: | General Approaches | |
| | | Assumes purge line added downstream of fuel inlet valve. | Automated component precycling | |
| | | Inert gas may not give large enough temp difference to be detected by skin temp sensors - cryopenics may be preferable. | Sensors/Hardware • Temperature sensor | |
| | | requirement for extra propellants if cryogenics are used. Difficult to detect small leakage rates | Alternate Design Recommendations • n/a | |
| | | Benefits: | | |
| | | Simple to perform pressure lock-up and monitor system pressure decay. | | |
| | c. Automated | lesues: | | |
| | JULIC | Past history does not adequately assess degradation during idle period. | • Automated static checkout | |
| | | Benefits: | Sensors/Hardware • Temperature sensor | |
| | | • see references | Alternate Design Recommendations • n/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS REFERENCES | COMMENTS |
|---|------------------------------|---|--|----------|
| 5. Propellant valve primary shaft seals | a. Prelim. power-up | Issues: • offers no advantage over assessment during actual operation Benefits: • see references | General Approaches • Preliminary power -up Sensors/Hardware • Temperature sensor Alternate Design Recommendations • n/a | |
| | b. Automated pre- cycling | I se u es : • Assumes purge line added downstream of fuel inlet valve. • may not be able to detect excessive (hazardous) leakage without full power level conditions (flow , pressure, and temperature). • inert gas may not give large enough temp difference to be detected by skin temp sensors - cryogenics may be preferable. • requirement for extra propellants if cryogencs are used. Benefite: • low risk identification of major leaks. | General Approaches • Automated component precycling Sensors/Hardware • Temperature sensor Alternate Design Recommendations • r/a | |
| | c. Automated static | Issues: • Past history data does not adequately assess degradation during idle period. Benefits: • see references | General Approaches • Automated static check Sensors/Hardware • Temperature sensor Alternate Design Recommendations • n/a | |
| 6. Pneumatic control assembly internal seals. | a. Prelim, power-up | Issues: • Short firing period may not provide enough time to detect leakage. • offers no advantage over assessment during actual operation Benefits: • see references | General Approaches • Preliminary power -up Sensors/Hardware • Pressure transducer Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Numerous pressure transducers and checkout valves required to thoroughly check system. may not be able to detect low level leakage Benefite: Longer measurement period may allow small leaks to be accurately detected. low risk identification of major leaks. | General Approaches • Automated component precycling Sensors/Hardware • Pressure transducer Alternate Design Recommendations • r/a | |
| | c. Automated static | Issues: • Past history data does not adequately assess seal degradation during idle period. Benefits: • see references | General Approaches • Automated static checkout Seneors/Hardware • Pressure transducer Alternate Design Recommendations • n/a | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS REFERENCES | COMMENTS |
|-------------------------------------|------------------------------|--|--|----------|
| 7. Heat exchanger coil leak test | a. prelim-power up | Not applicable | | |
| | b. automated pre- cycling | Issues: • Complexity, weight, and large quantity of inert gas required. • Cannot discern between internal vs external leaks. • May not detect small leaks which could increase during hot-fire conditions. Benefits: • Inert environment provides safe test conditions. • Can detect leaks generated during thermal transient at least engine shuldown (auto static data may not). | General Approaches: • Automated component precycling. Sensors/Hardware • Pressurized inert gas source. • Pressure transducer. Alternate Design Recommended: • Seamless robust heat exchanger design. | |
| 8 Heat exchanger | c. Automated static | Issues Historical data base may not be capable of predicting sudden catastrophic failures which are not preceded by shifts on operating parameters. Small leaks may not be detected in this manner. Benefits: Not aronicable | General Approaches • Automated static checkout Sensors/Hardware • Existing thermocouples and pressure transducers. | |
| coil proof test | | | | |
| | b. automated pre- cycling | See previous checkout 7. | | |
| | c. Automated static | Not applicable | | |

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|---|------------------------------|---|--|---|
| 9. T/C Assembly outer walls | a. Prelim. power-up | Issues: Short firing period may not provide enough time to detect leakage. Performance degradation may not indicate localized leakage - could be a result of many other factors. Benefits: Provides reasonable simulation of operating | General Approaches • Preliminary power-up Sensors/Hardware • Optical leak detector • Pressure transducer • Temperature sensor • Turbine flowmeter Alternate Design Recommendations | |
| | b. Automated pre- cycling | thermal environment. Issues: Throat plug required. System to place and secure throat plug would likely be highly complex and heavy. Benefits: No benefits to this particular approach since pressurizing the hot gas system is not feasible. | rva General Approaches · Automated component precycling Sensore/Hardware · Optical leak detector (for alternate approach) Alternate Design Recommendations · r/a | This check could be performed by injecting IR absorbing gas into liner to visually detect external leakage. |
| | c. Automated static | Promising . Increase in a potential reak detection approach seems promising . Issues : Requires development of sensitive optical hardware and physical degredation identification techniques . Benefits: Leakage from prior operation may be all that is necessary. does not required additional commodoties or impose risky operation. | General Approaches • Automated static checkout Sensors/Hardware • Optical leak detector Alternate Design Recommendations • n/a | Design should reflect use of hardware with predicatable degradation characteristics which could augment leak detection techniques. |
| 10 . Combustion and propellant system joints. | a. Prelim. power-up | Issues: • Short firing period may not provide enough time to detect leakage. Benefits: • Provides reasonable simulation of operating thermal environment. | General Approaches • Preliminary Power-up Sensors/Hardware • Optical leak detector Alternate Design Recommendations • Welded combustion and propellant system joints. | |
| | b. Automated pre- cycling | Insures: Throat plug required. System to place and secure throat plug would likely be highly complex and heavy. Benefite: No benefits to this particular approach since pressurizing the hot gas system is not feasible. However, an optical leak detection approach seems promising. | General Approaches • Automated component pre-cycling Sensors/Hardware • Optical leak detector (for alternate approach) Alternate Design Recommendations • Welded combustion and propellant system joints. | |
| | c. Automated static | Issues: • Requires development of sensitive optical hardware. Benefits: • Leakage from prior operation may be all that is necessary. • does not required additional commodoties or impose risky operation. | General Approaches • Automated static check Sensors/Hardware • Optical leak detector Alternate Design Recommendations • Welded combustion and propellant system joints. | |

Part B - Issues and Benefits of Preflight Methods - Inspections

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|--|------------------------------|---|---|--|
| 1. Exterior of components for damage/security | a. Prelim. power-up | not applicable | | |
| | b. Automated pre- cycling | not applicable | ······ | |
| | c. Automated static | Issues: • Accessibility may be a problem for some interior components • requires engine design with optical access Benefits: • see references | General Approaches • Automated static checkout Sensors/Hardware • Remote high resolution visual Alternate Design Recommendations • r/a | Prefer to eliminate requirement by robust design in combination with statistical analysis techniques to predict component life. |
| 2. Thrust chamber assembly for evidence of coolant passage blockage. | a. Prelim. power-up | Issues: • Short fire-up may not be effective. Accurate assessment may require an interval of steady state operation. • no advantages over monitoring during actual operation Benefits: • see references | General Approaches • Preliminary power-up Sensors/Hardware • Pressure transducer Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Issues: • Very high inert gas pressures may be required to perform check. Implies a massive inert gas tank. • high gas consumption required to identify blockages Benefite: • low risk method of identification | General Approaches • Automated component precycling Sensors/Hardware • Pressure transducer Alternate Design Recommendations • n/a | |
| | c. Automated static | Past history data does not predict sudden, large scale blockage scenarios (i.e. pump seal fragmentation, etc.) Benefite: In-flight monitoring augmented by trend analysis would be a simple and accurate approach. slow blockage accumulation easily predictable and can be tracked through operation history. | General Approaches • Automated static checkout Sensors/Hardware • Pressure transducer Alternate Design Recommendations • n/a | |

Part B - Issues and Benefits of Preflight Methods - Inspections (contd.)

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS REFERENCES | COMMENTS |
|---|------------------------------|--|--|--|
| HPFTP turbane whee/blades for creacks, fatigue, and damage. HPOTP LPFTP LPFTP LPOTP | a. Prelim. power-up | Issues: Short fire-up may not be effective. Accurate assessment may require an interval of steady state operation. puts engine and vehicle at risk if problem exists Benefits: Optical pyrometer is effective for assessing turbine health and may be a more mature technology than exo-electron fatigue det. most effective method of identifying damage. | General Approaches • Preliminary Power-up Sensors/Hardware • Ferromegnetic torquemeter • Optical pyrometer • Plume spectrometer Alternate Design Recommendations • rva | |
| | b. Automated pre- cycling | not applicable | | |
| | c. Automated static | Issues: • can only track slow degradation • Down time degradation may be an issue. Not considered by past history data. Benefits: • Past history performance data in combination with trend analysis should provide accurate assessment. • robust design and statistical analysis can sufficiently mitigate the risk of any failure other than slow degradation. • Optical pyrometer is effective for assessing turbine health and may be a mature technology than exo-electron fatigue det. | General Approaches • Automated static checkout Sensors/Hardware • Ferromagnetic torquemeter • Optical pyrometer • Plume spectrometer Alternate Design Recommendations • n/a | A more robust design should be considered to permit predictable slow degradation which lends itself to a life prediction model. |
| 7. HPOTP bearings for damage | a. Prelim. power-up | Issues: • Risk engine hardware during power-up if bearings damaged • short power-up not adequate to assess bearing operation Benefits: • see references | General Approaches • Preliminary Power-up Sensors/Hardware • Fiberoptic deflectometer Alternate Design Recommendations • Hydrostatic bearings | Check will also include HPFTP bearings. Hydrostatic bearings and their subsystems in both pumps would require inspection and functional checks. |
| | b. Automated pre- cycling | Issues: Pre-spin hardware greatly adds weight and complexity to pump. Benefite: low risk approach to determine bearing condition May use same electrical drive hardware as torque checks. | General Approaches • Automated component precycling Sensors/Hardware • Fiberoptic deflectometer Atternate Design Recommendations • Hydrostatic bearings | Since hydrostatic bearings result in minimal wear, this check although complex, would be required less frequently if this alternate design feature was adopted. |
| | c. Automated static | Issues: does not address sudden bearing degradation Benefits: probably acceptable since most bearing degradation is a slow function of "in operation" time Zero gravity environment may prevent wear during downtimes and engine start. Downtime degradation may not be an issue in space. | General Approaches • Automated static checkout Sensors/Hardware • Fiberoptic deflectometer Alternate Design Recommendations • Hydrostatic bearings | |

Part B - Issues and Benefits of Preflight Methods - Inspections (contd.)

| CHECKOUT | HECKOUT APPROACH ISSUES AND BENEFITS | | APPLICABLE ISSUES AND BENEFITS COMMENT References | | |
|---|--------------------------------------|--|--|---|--|
| T/C assembly injector face plate, igniter, and lox post tips for erosion, burning, and contamination. | a. Prelim. power-up | Issues: • Analysis of exhaust plume may not give complete assessment. • risks further hardware damage and produces harsh operating environment for monitoring devices. Benefite: • see references | General Approaches • Preliminary power-up Sensors/Hardware • Plume spectrometer Alternate Design Recommendations • r/a | Robust design should be implemented to reduce need for detailed inspection. | |
| | b. Automated pre- cycling | Not applicable | | | |
| | c. Automated static | I esues: • Injector elements may be inaccessible using current automated visual techniques. Techniques may require enhancements (intrusive fiber optic devices) for inspection purposes. • cannot address sudden failure occuring at end of subsequent operation. Benefite: • trend analysis will identify virtially all failures by monitoring typical slow degradation of the injector | General Approaches • Automated static checkout Sensors/Hardware • Plume spectrometer • remote high resolution visual • Pressure transducer • Turbine flowmeter • Turbine flowmeter • Temperature sensor Alternate Design Recommendations • n/a | | |
| 9. Gimbal bearing and TVC attach points for evidence of bearing seizure and fatigue. | a. Prelim. power-up | Issues: • Not a complete check since assessment relies on vibration data alone. • power-up does not significantly alter the operation the gimbal and TVC system. Benefite: • see references | General Approaches • Preliminary power up Sensors/Hardware • Accelerometer Alternate Design Recommendations • r/a | This can be combined with the functional check for ext. nozzle travel which involves gimballing and actuation. The nature of this check makes it a functional check. | |
| | b. Automated pre- cycling | Issues: Requires robust gimballing mechanism since full- range gimballing required for checkout purposes. requires power consumption for actuation Benefite: Gimballing will provides real-time source for required data. Vibration data combined with verification of gimballing function provides complete assessment of gimbal system. | General Approaches • Automated component precycling Sensors/Hardware • Accelerometer • Eddy current position sensor Alternate Design Recommendations • r/a | Robust gimbal bearing and TVC attach points recommended to delete check. Design for uprated thrust to absorb large thrust loads. | |
| | c. Automated static | lesues: • does not address idle time degradation of TVC system • Visuals may be a problem due to inaccessibility. • Vibration data plus position data aquired from past history database may not provide enough information for accurate assessment. Benefite: • little power consumption | General Approaches • Automated static check Sensors/Hardware • Accelerometer • Eddy current position sensor • Remote high resolution visual Atternate Design Recommendations • n/a | | |

Part B - Issues and Benefits of Preflight Methods - Inspections (contd.)

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS References | COMMENTS |
|--|------------------------------|---|--|---|
| 10. Heat exchanger for cracks, evidence of wear, and damage. | a. Prelim. power-up | Issues: • power-up forces visual inspection sensors to operate in harsh environment unnecessarily • Potential accessibility problems with visual. • Requires development of physical degradation identification techniques and sensitive optical hardware. Benefite: • see references | General Approaches • Preliminary power up Sensors/Hardware • remote high resolution visual Alternate Design Recommendations • r/a | Another possible approach is monitoring inlet and exit conditions - this may result in failure during power up. This may be an option with automated static check. |
| | b. Automated pre- cycling | Not applicable | | |
| | c. Automated static | Issues: •Potential accessibility problems with visual. • must design unit for visual accessibility • Requires development of physical degradation identification techniques and sensitive optical hardware. Benefits: • Past history data assessment is safest approach | General Approaches • Automated static check Sensore/Hardware • remote high resolution visual Alternate Design Recommendations • n/a | |

Part B - Issues and Benefits of Preflight Methods - Servicing Tasks

| CHECKOUT | APPROACH | ISSUES AND BENEFITS | APPLICABLE ISSUES AND BENEFITS | COMMENTS |
|--|------------------------------|--|--|---|
| 1. Combustion zone drying | a. Prelim power-up | issues: • no advantage over operational redline Benefits: • see references | General Approaches • Proliminary power up Sensors/Hardware • r/a Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Issues: • Assumes purge system is available Benefits: • Simple task performed during normal shutdown purge sequence. • requires no change in routine system operation to perform servicing. • Vacuum environment simplifies task due to rapid dissapation. | General Approaches • Automated component precycling Sensors/Hardware • n/a Alternate Design Recommendations • n/a | With a purge system, this task is simple and routine. Without a purge system, self drying of sensors is a possible approach. |
| | c. Automated static | Not applicable | | ** * |
| 2 HPOTP LOx turbine drive gas seal pre-start purge. | a. Prelim power-up | Issues: • no advantage over operational redline Benefits: • see references | General Approaches • Preliminary power up Sensors/Hardware • r/a Alternate Design Recommendations • r/a | |
| | b. Automated pre- cycling | Issues: • assumes purge system is available Benefits: • Part of normal pre-start procedure • requires no change in routine system operation to perform servicing. | General Approaches • Automated component precycling Sensors/Hardware • n/a Alternate Design Recommendations • n/a | With a purge system, this task is simple and routine. Without a purge system, non-purge seals would be required. These would effectively eliminate this task. |
| | c. Automated static | Not applicable | | |

Part C - Issues and Benefits of Preflight Methods - ICHM Sensors and Hardware

| Sensor Measurement /Advanced Hardware | | Issues and Benefits | | Comments |
|--|---|--|---|--|
| Chine D | Space Basing | Vehicle/Infrastructure | Engine system | |
| Static Pressure | Issues: Solar radiation effects unknown | Required features dictate size (weight) ie, number of channels, | • Sensor is intrusive - Access must be made through fluid | |
| | * Calibration can be verified at | installation needs, etc. | media. Benefits: | |
| | operation • Vacuum can verify absolute pressure. | Sensor is self contained - no additional support hardware required. No external power supply required. | Calibration can be verifed without engine operation. Vacuum can verify absolute pressure. | |
| Static Temperature | Issues: | Issues: | issues: | |
| | Solar radiation effects unknown May be subject to long term drift (certain technologies). | Required features dictate size (weight) ie, number of channels, structural requirements, installation needs, etc. | • Sensor is intrusive Benefite: | |
| | Benefite: * Continuity can be confirmed | Benefita: | Continuity can be confirmed without engine operation. | |
| | without engine operation | Sensor is self contained - no additional support hardware required. No external power supply | | |
| Flow | Issues: | lesues: | lesues: | |
| | Solar radiation effects on lubricant unknown. | • Turbine flowmeters tend to be heavy (16 - 20 oz.) | Flowmeter requires major component teardown is repair is necessary. | |
| | Benefits: | Benefits: | Benefits: | |
| | | Flowmeter is integral with duct - no servicing required. Pickups are passive - no external power required. | Integral to engine component. | |
| Speed | Issues: | Issues: | lesues: | ······································ |
| | - To Be Determined | To Be Determined. | Intrusive design is mature - non- intrusive design is not. | |
| | Benefits: | Benefite: | Benefita: | |
| | | • Pick-ups are passive - No external power supply required. | Can be non-intrusive. | |
| Displacement | lesues: | issues: | issues: | |
| | To Be Determined | Sensors require their own unique signal processor. | • mature design for engine non- existent. | |
| | To Be Determined. | Benefite: | Benefits: | |
| | | Sensor are non-contacting. | To Be Determined | |
| Position (on/off) | Issues: | lseues: | Issues: | |
| | To Be Determined | Limited experience on liquid rocket programs. | To Be Determined | |
| | Benefits: | Benefits: | Benefits: | |
| | No moving parts. Static displacement can always be measured. | Sensors are lightweight and occupy a small volume. | Sensor can be used in any fluid including lox. | |
| Acceleration | lesues: | lesues: | leeves: | |
| | • To Be Determined. Benefits: | Piezoelectric transducer output subject to "spiking" at cryogenic temperatures. | • To Be Determined. Benefite: | |
| | Piezoelectric crystals maintain stability over time. No external power required. | verified statically - requires mechanical input. | Simple non-intrusive installation. | |
| | | Sensors are lightweight | | |

Part C - Issues and Benefits of Preflight Methods - ICHM Sensors and Hardware (contd.)

| Sensor Measurement | | issues and Benefits | | Comments |
|-------------------------------|--|--|---|----------|
| | Space Basing | Vehicle/Infrastructure | Engine system | |
| Deflectometer | lasues: | lseues: | lasues: | |
| | Limited thermaliy to 250 F (709 R) | To Be Determined. | Engine version not mature. Probe is intrusive. | |
| | Benefits: | Benefits: | Benefits: | |
| | Fliberoptics unaffected by long term storage. Immune to EMI/RFI. | • Fiberopuc assembly is lightweight. | To Be Determined. | |
| Exo-electron fatigue detector | lesues: | lssues: | lasues: | |
| | May require routine optical re- allignment. Light source has limited life. | System is currently at prototype stage. Sensor probe needs to be ruggedized. | Repeatability has not been demonstrated on engine materials. | |
| | Benefits: | Benefits: | Benefits: | |
| | Best results have been achieved in vacuum environment. Can be automated. | Can be made lightweight. High sensitivity with low power consumption. | Non-destructive measurement. Limited engine disassembly. | |
| Isotope wear detector | lasues: | Issues: | leeues: | |
| | Historical data base required. Need long-lived reference activity for anchoring data. Time dependent crystal/detector degradation. Compensation required for | Requires power for multi-channel analyzer and detector. Detector requires LN ₂ cooling. Benefits: | Electronics are suceptable to shock, vibration, and thermal effects. Type and amount of activation is material dependent. Shielding of activation by | |
| | backround radiation via backround subtraction. | Simple data analysis, Possible real-time implementation | intervening materials. Benefita: | |
| | Benefits: | | • Non-intrusive. | |
| | Monitors mass loss from exterior. | | | |
| lorquemeter | lesues: | lasues: | lssues; | |
| | Long term stability not demonstrated. | May require specialized signal processor. | Pickup sensor is intrusive. | |
| | Benefits: | Benefits: | • Pump shaft requires magnetoresistive deposits | |
| | Eliminate human intervention for torque and runout measurement. Not affected by vacuum environment. | Torque and speed measurements aquired from a single sensor. Torque and speed can be corellated with vehicle parameters. | Benefits: • Increase efficiency and reliability of engine system. • Measureing speed, torque, and shaft displacement eliminates redundant sensors resulting in reduced system weight and complexity. | |
| Automated Visual Inspection | leaues: | lasues: | issues: | |
| | Computer/video system required to be radiation hardened. Requires knowledge based system for independent decisions. | Computer and optics susceptability to vibration, shock and thermal effects. Power required for computer, carnera, and carnera robotics. | Criteria needs to be established for determining component condition. View of component required - either direct access or inspection port | |
| | Benefite: | Benefits: | Resolution of video system. | |
| | Eliminate human intervention for inspection procedures. | Can be used for vehicle inspections also. | Benefits: | |
| | | | Decreases cost and increases speed, reliability, and repeatability of between flight inspections. | |
| Optical Leak Detection | lsaues: | Issues: | leeues: | |
| | Has not been tested in vacuum environment. May require routine optical reallignment. Light source has limited life. | Optics need to be ruggedized. System requires gas purge. Currently requires cryogenic (LN ₂) cooling for detector. | • Tracer gas compatability not demonstrated on engine materials. Benefite: | |
| | Benefits: | Benefite: | Highly sensitive to pinpoint | |
| | Can be automated. Eliminate human intervention for leak detection procedures. | Jan be made lightweight. Low power consumption. | Remotely automated operation. Limited or no engine disassembly required. | |

Page 101 Part C - Issues and Benefits of Preflight Methods - ICHM Sensors and Hardware (contd.)

| Sensor Measurement /Advanced Hardware | Issues and Benefits | | | Comments |
|--|--|--|--|----------|
| | Space Basing | Vehicle/Infrastructure | Engine system | |
| Plume Spectroscopy | Issues: | lesues: | Issues: | |
| | Calibration required prior to engine start. Potential interference from backround solar radiation. Benefits: Demonstrated long term component stability . | Optics need to be ruggedized. Benefite: Low power consumption. | Spectrometer must be isolated from engine. Uses fiberoptic probe to transmit data to spectrometer. Benefite: Modular components for repair simplicity. Verification of nominal combustion. Thrust level determination. Realtime evaluation of hardware erosion and anomalous combustion. Identification and quantification of eroding materials. Engine readline/cutoff capability. | |

Part D - Issues and Benefits of Preflight Methods - Alternate Design Recommendations

| Design Recommendation | Effected Preflight | | Issues and Benefits | |
|--|--|--|---|---|
| | nequirement(s) | Space Basing | Vehicle/ Infrastructure | Engine System |
| Component: <u>Heat</u> Exchanger | Leak checks:The following requirements may be deleted | Issues: | issues: | lesues: |
| Motivation for selecting an alternate: To delete the requirements for the heat exchanger leak test and proof test. Based on the current design, small leaks would be very difficult to detect. A robust design will greatly reduce the probability of this leakage over the life of the engine. Current Design Description: Cylindrically contoured section, flat thin multi- brazed panels. This design reflects minimum weight and convenient packaging. Suggested Alternate Design Description: Highly robust flexible line in shell. This design reflects a minimal number of welds and effectively eliminates coil leakage. Other alternate Design Concepts: 1. Similar to current design with minimal changes to the basic geometry. Materials would be selected for high fatigue life. Design would reflect use of intermediate channels containing inert fluid would be located between the Lox and the hydrogen for minimum risk. | using the proposed robust design rationale. 1. Heat exchanger coil leak test. 2. Heat exchanger coil proof test. Inspections:The following inspection may be required less frequently, however the requirement cannot be deleted. 1. Heat exchanger inspection for cracks, evidence of wear, and damage. | Heat exchanger may be subject to debris damage because of large surface area. The actual surface area exposed will depend on the location of the heat exchanger in the powerhead. Damage caused by debris may propogate with repeated engine firings. Thermal cycling caused by solar radiation may increase probability of failure - the alternate design should allow for this. Radiation effects on brazed joints - Long duration space exposure may degrade material and reduce strength. A solution might be diffusion bonding or some protective coating. Benefits: A robust design will eliminate the leak check requirements and make the heat exchanger less vulnerable to damage from debris. Robust design should not be adversely affected by the space environment. Small volume leakage of gasses into space will dissipate rapidly thus reducing the overall risk of space combustable mixtures. | Payload may possibly be impacted because of the increased heat exchanger weight. A mature operational data base is required to reduce the need for an external inspection of the heat exchanger. Benefits: Overall simpler diagnostics since the leak check requirements can be deleted. | Robust design may result in different engine performance characteristics due to different system delta-P and heat transfer characteristics. Higher weight and volume may impact the component arrangement on the engine powerhead. Benefits: Robust design improves overall engine reliability, maintainability, and safety. No special checkout valves required. |
| Component: <u>Combustion</u> | Leak checks:The following | lesues: | Benefits: | lasues: |
| Component: <u>Combustion</u> and propellant system joints. Motivation for selecting an alternate: To delete the requirement for leak checking the combustion and propellant system joints. Current Design Description: Flanged and bolted joints located throughout the engine system Suggested Alternate Design Description:Welded combustion and propellant system with the exception of the vehicle interface flanges and possibly the extendible / retractable nozzle attach point. The welds would reflect a very high factor of safety. Other alternate Design Concepts: 1. Welded nozzle extension which would allow the nozzle to extend from a retracted position using a bellows-convolute nozzle design. This eliminates leakage from the extendible nozzle attach point. | Leak checks: The following leak check requirement would not be deleted, however it would be simplified using the proposed design rationale. This is because only the extendible nozzle attach point seal would need to be checked for seal integrity. 1. Combustion and propellant system joints for leakage. | Issues: Radiation effects on welds may cause degradation. No other problems are anticipated. Special tools for space maintainability would need to be developed if space maintainability was a consideration. Benefite: Small volume leakage of gasses into space will disapate rapidly. Overall simpler diagnostics since the leak checking requirement has been simplified. Space maintainance is potentially simpler with welds than boltad flanges because of fewer parts. This assumes the development of special tools. | Benefite: • Heavier payload permitted since welds are lighter in weight than flanges. • Cost and reliability benefits since welded joints are simple, rugged, and have fewer parts. | Issues: Engine removal for maintenance is currently assumed. A very high factor of safety is required to assure quality welds which can withstand many cycles under extreme conditions. Drop-through of weld into system may cause downstream contamination. There are design solutions to mitigate this, possibly at the cost of weight. Benefits: Reduction in the number of leakage paths. Eliminates concern for damage to flanges, seals, and a large number of bolts. Tighter and lighter packaging is possible because of elimination of bulky flanges and bolts. |

Part D - Issues and Benefits of Preflight Methods - Alternate Design Recommendations (contd.)

| Design Recommendation | Effected Preflight Requirement(s) | Space Basing | issues and Benefits Vehicle/ Infrastructure | Engine System |
|---|--|--|--|--|
| Component: <u>Turbonump</u> <u>Bearings</u> Motivation for selecting an alternate: To delete the requirement for the axial shaft travel check, and the bearing damage inspection for the fuel and lox turbopumps. Current Design Description: Ball bearings on both the pump and turbine ends of both the pump and turbine ends of both the fuel and oxidizer pumps. One alternative design included a series hybrid bearing which consists of a ball bearing and a hydrostatic bearing on the outside diameter of the ball bearing. Suggested Alternate Design Description: Exclusive use of hydrostatic bearings on the high presure turbopumps. Other alternate Design Concepts: 1. Hybrid bearing concept where the hydrostatic bearings are augmented with a ball bearing. | Functional Checks :The following checkouts are not eliminated but would need to be modified. For example, a torque check with an unpressurized hydrostatic bearing will always reveal rubbing at the bearing. For the torque check to be meaningful, the bearing should either be pre-pressurized or be augmented with some kind of axial centering support or ball bearing : 1. HPFTP torque check. 2. HPOTP torque check. 3. LPFTP torque check. 4. LPOTP torque check. 4. LPOTP torque check. 5. LPFTP torque check. 6. LPOTP torque check. 7. The following checkout can be deleted since it would not be meaningful with the use of hydrostatic bearings: 1. Axial shaft travel check. 6. Inspections:The following requirements cannot be eliminated but would need to be modified to accommodate hydrostatic bearings is wear. 1. HPOTP bearings for damage (wear). 7. HPFTP bearings for damage (wear). | Issues: Materials and coatings selected for hydrostatic bearing components may be affected by solar radiation, however these effects are likely to be minimal. The lengthy downtime in space could effect the hydrostatic bearings depending on the configuration. Benefite: Shaft could be held in the centered position with relative ease due to lack of gravity. A centered shaft would virtually eliminate wear of the bearing during start-up, shutdown, and transport. Adequate hydrostatic support forces to overcome hydraulic side forces during start/shutdown must be assured. | Issues: • External hardware including lines, fluid tank, several valves, and some electronics hardware for feedback and control are required for hydrostatic bearing pressurization. Pressurization is required as a means of eliminating bearing wear during transients. • Payload will be impacted by the additional weight of a filtration system required for the hydrostatic bearing fluid. • Line interfaces to the vehicle will be required if the hydrostatic bearings are fed from from an extenal source. Benefits: • Vehicle vibration and noise levels may be reduced as a result of the increase in bearing damping. | Lesues: Contamination could result from hydrostatic bearing wear therefore some form of filtration may be required. Added filters could increase the system pressure drop. Hydrostatic bearing flows are typically parasitic and do lead to a slight reduction in pump efficiency. Benefite: Significant gain in bearing life can be achieved by using hydrostatic bearings. The actual life will depend on the duty cycle. Many starts and stops will limit the life, however, no wear occurs during sustained operation. |

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Appendix 4

Required Sensors for Preflight Engine Checkout Methods

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| CHECKOUT TASK | METHOD | | | | $\left \right\rangle$ | \square | | | \$ | | \square |
| 1.X FUNCTIONAL CHECKS | A. PRELIMINARY POWER-UP | | | J | | 605 | CSN35 | N. S. S. | 65 6 | | |
| 2.X LEAK CHECKS | B. AUTOMATED COMPONENT PRE-CYCLING | νų. | 40 | Contraction of the second seco | 4300 | ASS. | X SHUMO | NOL N | \$0/23 0/23 | C | |
| 3.X INSPECTIONS | C. AUTOMATED STATIC CHECKOUT | 10 × 10 × | Stop 1 | | 1500 | Y SAVIO | AND AND | 423 | ANO STO | 130 34 190 H | |
| 4.X SERVICING TASKS | *SENSORS EITHER NOT REQUIRED OR NOT APPI ICARLE | 137300 × 1000 | SSJ4 THE STATE | 24) VS | 7373 10 | N 64 83 | 300100 | 123/200 | S JAND | 2000 | |
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| 1.1 VALVE ACTUATOR CHECK | A | | е Г | ~ | | | | | | - | |
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| 1.2 SENSOR CHECKOUT/ | A* | | | | | | | - | | 1 | |
| CALIBRATION | * 8 | | | | | | | - | | T | |
| | * U | | | | | - | | | | | |
| 1.3 PNEUMATIC COMPONENT | A | | | | | - | | | | 1 | |
| CHECKOUT | B | | - | | | | | | | 1 | |
| | U | | - | | | | | \vdash | | - V = ALREADY | |
| 1.4 OPERATIONAL SEQUENCE | A | | 7 | ~ | | | | - | | | |
| TEST (FLIGHT READINESS | В | | 77 | ~ | | - | | | | PREVIOUS | |
| | c | | 7 7 | ~ | | | | | | TASK E.6 | |
| 1.5 CONTROL SYSTEM | * A | | | | | | | | | 1 | |
| REDUNDANCY VERIFICATION | • 8 | | | | | | | | | T | |
| | t U | | | | | | | | | 1 | |
| 1.6 CONTROLLER MEMORY | A* | | | | | | | | | 1 | |
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| Ndda | enaix 4. Hequired | Sensors for Preflight Engine Checkout Methods (continued) |
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| CHECKOUT TASK | METHOD | |
| 1.X FUNCTIONAL CHECKS | A. PRELIMINARY POWER-UP | READINESS LEVEL) |
| 2.X LEAK CHECKS | B. AUTOMATED COMPONENT PRE-CYCLING | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 |
| 3.X INSPECTIONS | C. AUTOMATED STATIC CHECKOUT | Solution of the set of |
| 4.X SERVICING TASKS | *SENSORS EITHER NOT REQUIRED OR NOT APPLICABLE | 2 12 12 12 12 12 12 12 12 12 12 12 12 12 |
| 1.7 CONTROLLER | A | NUMBER OF SENSORS NEEDED |
| PRESSURIZATION | . 60 | |
| VEHILICATION | v | |
| 1.8 HPOTP TORQUE CHECK | A | |
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| | U | |
| 1.9 HPFTP TORQUE CHECK | A | |
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| 1.10 LPOTP TORQUE CHECK | A | |
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| 1.11 LPFTP TORQUE CHECK | A | |
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| 1.12 TURBOPUMP AXIAL | A | |
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| PRELIMINARY WER-UP | ŘEAC | SINES | S LEVE | | | | A A A | to shi | N.S. | | 4 | | No. 43 | |
| AUTOMATED MPONENT E-CYCLING | | VOSN. | | SA SA | | A SS A | NOLIS | Not Contraction | | | 5 43 6 43 | 67723 (2) (2) (2) (2) (2) (2) (2) (2) (2) (2) | \mathbf{X} | |
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|--|--|---|---|--|-----------------------|--|
| CHECKOUT TASK | METHOD | (TECHNOLOGY | | S | | |
| 1.X FUNCTIONAL CHECKS | A. Preliminary Power-up | READINESS LEVEL) | Ser les | | | (3, 2, 3, 5) (3, 2, 1) (3, 2, 1)) (3, 2, 1) (3, 2, 1)) (3, 2, 1))) (3, 2, 1)))(3, 2, 1)))(3, 2, 1)))(3, 2, 1)))(3, 2, 1))(3, 2, 1)))(3, 2, 1))(|
| 2.X LEAK CHECKS | B. AUTOMATED COMPONENT PRE-CYCLING | 202 20 20 20 20 20 20 20 20 20 20 20 20 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | | ELES CLONELLE |
| 3.X INSPECTIONS | C. AUTOMATED STATIC CHECKOUT | | SI AND | 30 + 23 | 0413 340 | 24 45 C |
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| HPFTP TURBINE | A | | | - | $\left \right $ | |
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| METHOD | A. PRELIMINARY POWER-UP | B. AUTOMATED COMPONENT PRE-CYCLING | C. AUTOMATED STATIC CHECKOUT | SENSORS EITHER ' | | A | æ | U | A | B | ပ | A | B | v | A | B | v | A* | * | *0 | * A | B * | *: |
| CHECKOUT TASK | 1.X FUNCTIONAL CHECKS | 2.X LEAK CHECKS | 3.X INSPECTIONS | 4.X SERVICING TASKS | | 3.7 HPOTP BEARINGS FOR | | | 3.8 T/C ASSY., INJ., IGNITER, AND | LUX POST TIPS FOR EROSION, T | | 3.9 GIMBAL BEARINGS AND | | | 3.10 HEAT EXCHANGER FOR | | | 4.1 COMBUSTION ZONE | DRYING | | 1.2 HPOTP LOX/TURBINE | DRIVE GAS INTERMEDIATE | |

Appendix 4. Required Sensors for Preflight Engine Checkout Methods (continued)

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