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An Experimental Study of the Aerodynamics of a NACA0012 Airfoil With a Simulated Glaze Ice Accretion — Volume II

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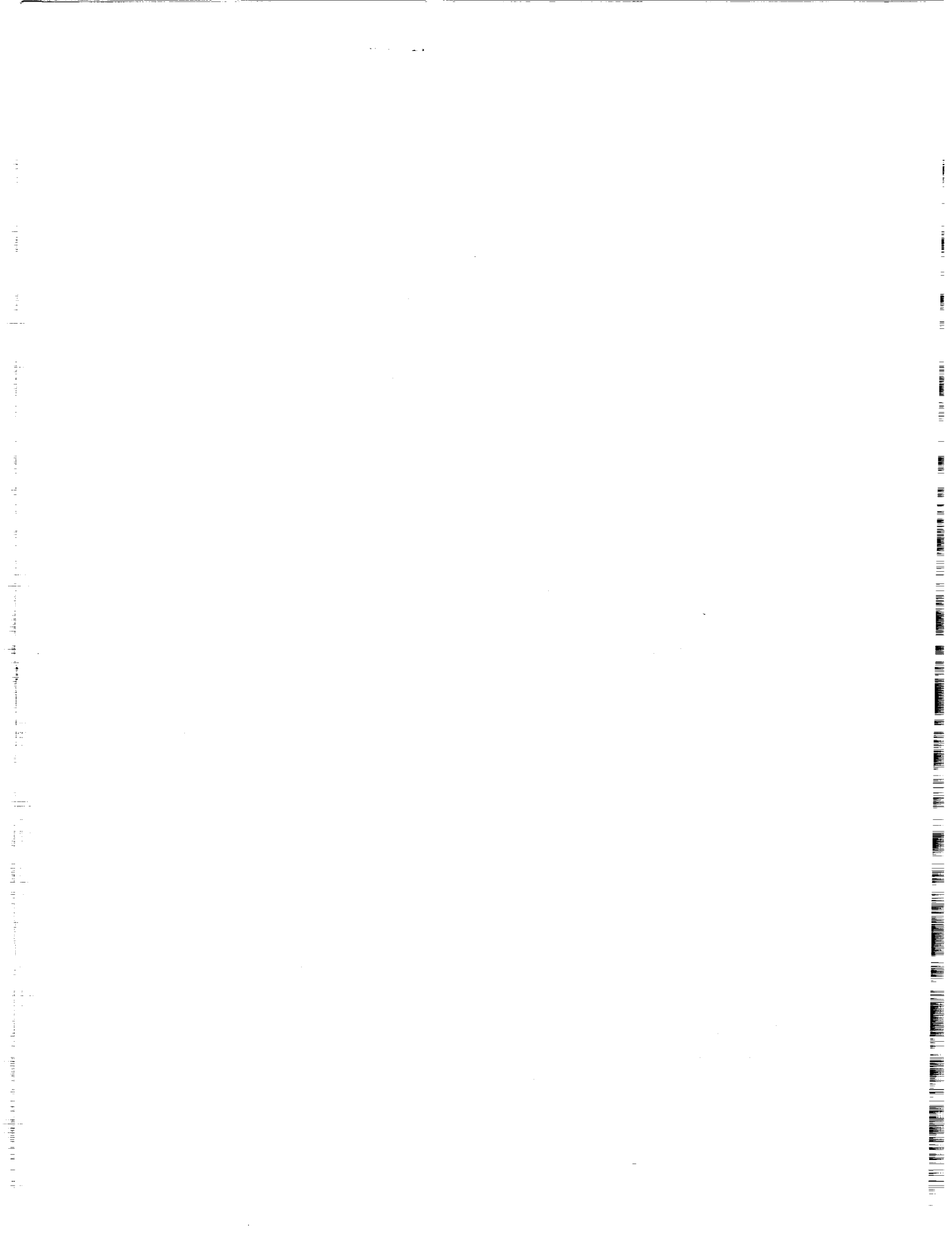


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**AN EXPERIMENTAL STUDY OF THE AERODYNAMICS OF A
NACA 0012 AIRFOIL WITH A SIMULATED GLAZE ICE ACCRETION
VOL. II**

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June, 1990

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ABSTRACT

This is the second volume of a report documenting the effect of a simulated ice accretion on the aerodynamic performance of a NACA 0012 airfoil. Both an experimentally measured and a computer generated ice shape are studied. The purpose of this report is to present the results of the measurements, not an analysis of the data. Surface pressure, integrated lift and pitching moment data are presented as well as drag from a wake survey. A split hot film probe was used to document the flow-field about the airfoil with simulated ice. Data in the separation bubbles, reattached boundary layer and wake are presented. Both tabulated and graphical data are presented in the paper. The data are also available on computer disk for easy access.

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1. The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that this is crucial for the company's financial health and for providing reliable information to stakeholders.

2. The second part of the document outlines the specific procedures for recording transactions. It details the steps from identifying a transaction to entering it into the accounting system, ensuring that all necessary details are captured.

3. The third part of the document addresses the role of the accounting department in monitoring and controlling the company's resources. It discusses how accurate records enable the company to identify areas of inefficiency and to take corrective action.

4. The fourth part of the document discusses the importance of regular audits and reviews. It explains how these processes help to ensure the accuracy and integrity of the company's financial records and to detect any potential errors or fraud.

5. The fifth part of the document concludes by summarizing the key points discussed and reiterating the company's commitment to maintaining high standards of financial reporting and transparency.

6. The sixth part of the document provides a detailed overview of the company's financial performance over the past year. It includes a comparison of actual results with budgeted figures and an analysis of the factors that have influenced the company's performance.

7. The seventh part of the document discusses the company's financial outlook for the coming year. It outlines the key financial goals and the strategies that will be implemented to achieve them, taking into account the current market conditions and the company's competitive position.

8. The eighth part of the document provides a detailed breakdown of the company's assets and liabilities. It includes a list of all major assets and liabilities, along with their respective values and a description of their nature and purpose.

9. The ninth part of the document discusses the company's capital structure and its financing strategy. It explains how the company has raised capital over the past year and how it plans to manage its debt and equity in the future.

10. The tenth part of the document concludes by summarizing the company's financial performance and outlook, and reiterating the company's commitment to transparency and accountability.

NOMENCLATURE

<u>Symbol</u>	<u>Description</u>
c	Airfoil chord length
C_d	Airfoil drag coefficient
C_l	Airfoil lift coefficient
C_m	Airfoil moment coefficient
C_p	Airfoil pressure coefficient
MACH	Mach number
R_e	Reynolds number
U_e	Boundary-layer edge velocity
U_∞	Tunnel velocity
x	Airfoil x coordinate, nondimensionalized by c
y	Airfoil y coordinate, or coordinate out from airfoil surface, nondimensionalized by c
α	Airfoil angle of attack
δ^*	Boundary-layer displacement thickness, nondimensionalized by c
θ	Boundary-layer momentum thickness, nondimensionalized by c

Subscripts

u Uncorrected data

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I. INTRODUCTION

This report is a continuation of NASA Contractor's Report 179571 (Ref. 1). Ref. 1 documented the effect of a simulated ice accretion on the aerodynamics of a NACA 0012 airfoil. Detailed surface pressure distributions, lift, drag and moment coefficient data were presented for the NACA 0012 airfoil, with and without simulated ice. Ref. 1 also presented some preliminary velocity profile measurements on an earlier NACA 0012 model.

The remaining NACA 0012 data are contained in this report. The effect of surface roughness on the simulated ice accretion is shown through surface pressures, C_l , C_d and C_m data. A split hot-film probe was used to measure the velocity profiles in the upper and lower surface separation bubbles, in the boundary layer downstream of reattachment, and in the airfoil wake. These data are reported here as well. An additional ice shape generated by the LEWICE code² was built and tested on this model. Surface pressure, lift, drag and moment data from this ice shape are presented.

All the measurements reported here were taken in the Ohio State University's 3 by 5 foot subsonic wind tunnel. This research was supported by NASA Lewis under grant NAG 3-28. The preparation of this report was completed at the University of Illinois and supported in part by grant NAG 3-1134, also from NASA Lewis.

II. EXPERIMENTAL PROCEDURES AND RESULTS

These data have been analyzed and the experimental procedures described in several other papers. Two of these AIAA papers^{3,4} are reproduced in Appendix C. The Masters theses by Spring⁵ and Khodadoust⁶ are also good references with regards to these data. These theses were too large to include in Appendix C, but are available as NASA Contractor's Reports. A complete description of the experimental procedures is also included in Ref. 1. Therefore, no detailed description of the experiment or data reduction will be included here.

All data in this report was taken on a NACA 0012 airfoil with or without a simulated ice accretion. Table 1 gives the coordinates for this model without ice and Table 2 with the simulated ice accretion. Note that the model used here is referred to as model No. 2 in Ref. 1. For the rough ice accretion tests, cloth-backed sandpaper was applied to the ice shape from $x/c = .085$ on the lower surface to $x/c = .015$ on the upper surface. Two roughness sizes were used: a 60-grit paper with a nominal roughness size of 0.012 inches, $k/c = 0.00057$, and a grit number of 36 where $k/c = 0.0011$.

The data in this report are organized as described below. In Section III Tables containing the run summaries are given. The run summaries act as an index for finding data in this report. For the runs where surface pressure measurements were taken; C_p , C_l , C_d and C_m are given for each run. With the subscript, e.g. C_{l_u} , represents the raw, measured value. Without the subscript, e.g. C_l , is the value corrected for tunnel wall effects⁷. Mach number and Reynolds number are also given for each run. A plot of the surface pressure coefficient versus X/C is given for each of these runs in Section IV. The plots are

in run number order. Note that right-side-up triangles represent upper-surface pressures and upside-down triangles are lower surface pressures. For many pressure runs, plots of the measured wake surveys are given. The pressure and wake plots are uncorrected with regards to wall interference.

Runs during which split-film velocity profiles were taken appear differently in Sections III and IV. The run summaries in Section III document each run by giving α , X/C , R_e and U_∞ . The boundary-layer parameters U_e , δ^*/C and θ/C are determined from the measurements and presented. For runs where reverse flow is measured Y_{stag}/C and Y_{sep}/C are also given. The calculation of these parameters is explained in Appendix C or the references. Plots of the measured velocity profiles are found in Section IV. Note that the coordinate y in these plots is measured out from the airfoil surface, perpendicular to the tunnel axis (or free-stream velocity direction). This was due to the orientation of the probe traversing mechanism. A zero value of y corresponds to the model surface, except for measurements in the wake where $y = 0$ always corresponds to the trailing edge.

Also contained in this report are Appendices A, B and C. Appendix C contains copies of references 3 and 4 as discussed earlier. Appendix A contains the pressure data on the NACA 0012 with the LEWICE shape. The format is the same as Sections III and IV, but the data were placed here to minimize confusion with the other ice shape. A 5 1/4 high density disk is available upon request and contains, in ASCII format, the run summaries and the numerical data contained in all the plots. Appendix B gives the format used for these data on the disk.

TABLE 1. COORDINATES FOR THE NACA 0012 MODEL

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
1	0.00000	0.00000	0.00000	0.00000
2	0.00309	0.00967	0.00309	-0.00967
3	0.00621	0.01356	0.00621	-0.01356
4	0.01380	0.01984	0.02230	-0.02481
5	0.02230	0.02481	0.04080	-0.03256
6	0.03140	0.02899	0.08000	-0.04307
7	0.04080	0.03256	0.12000	-0.04988
8	0.05000	0.03555	0.16000	-0.05442
9	0.06000	0.03838	0.20000	-0.05738
10	0.07000	0.04086	0.24000	-0.05913
11	0.08000	0.04307	0.28000	-0.05993
12	0.09000	0.04505	0.32000	-0.05993
13	0.10000	0.04683	0.36000	-0.05926
14	0.11000	0.04843	0.40000	-0.05803
15	0.12000	0.04988	0.44000	-0.05631
16	0.13000	0.05119	0.50000	-0.05294
17	0.14000	0.05238	0.56000	-0.04878
18	0.15000	0.05345	0.60000	-0.04563
19	0.16000	0.05442	0.65000	-0.04132
20	0.17000	0.05529	0.70000	-0.03664
21	0.18000	0.05607	0.75000	-0.03160
22	0.19000	0.05676	0.80000	-0.02623
23	0.20000	0.05738	0.85000	-0.02053
24	0.21000	0.05792	0.90000	-0.01448
25	0.22000	0.05839	0.95000	-0.00807
26	0.23000	0.05879	0.97500	-0.00471
27	0.24000	0.05913	1.00000	0.00000
28	0.25000	0.05941		
29	0.26000	0.05864		
30	0.27000	0.05981		
31	0.28000	0.05993		
32	0.29000	0.06000		
33	0.30000	0.06002		

TABLE 1. (Continued)

No.	X _{upper}	Y _{upper}
33	0.30000	0.06002
34	0.31000	0.05999
35	0.32000	0.05993
36	0.33000	0.05982
37	0.34000	0.05967
38	0.35000	0.05949
39	0.36000	0.05926
40	0.37000	0.05900
41	0.38000	0.05871
42	0.39000	0.05839
43	0.40000	0.05803
44	0.42000	0.05723
45	0.44000	0.05631
46	0.47000	0.05473
47	0.50000	0.05294
48	0.53000	0.05095
49	0.56000	0.04878
50	0.60000	0.04563
51	0.65000	0.04132
52	0.70000	0.03664
53	0.75000	0.03160
54	0.80000	0.02623
55	0.85000	0.02053
56	0.90000	0.01448
57	0.95000	0.00807
58	0.97500	0.00471
59	1.00000	0.00000

TABLE 2. COORDINATES FOR THE NACA 0012 MODEL
ICED CONFIGURATION

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
1	-0.02660	0.01690*	-0.02660	0.01690
2	-0.02450	0.02870*	-0.02220	0.00390
3	-0.02080	0.03060*	-0.01750	-0.00700
4	-0.01000	0.02880	-0.01070	-0.01840
5	-0.00010	0.02680	-0.00360	-0.02840
6	0.01000	0.02500	0.00590	-0.03930
7	0.02210	0.02670	0.01500	-0.04740
8	0.03110	0.03000	0.02580	-0.05330**
9	0.04070	0.03330	0.03000	-0.05300**
10	0.04910	0.03610	0.03970	-0.05030
11	0.05950	0.03900	0.04950	-0.04730
12	0.06940	0.04140	0.06000	-0.04410
13	0.07940	0.04350	0.06950	-0.04210
14	0.08910	0.04550	0.07930	-0.04360
15	0.09900	0.04720	0.10940	-0.04870
16	0.10970	0.04870	0.11930	-0.0500
17	0.11970	0.05000	0.12900	-0.05110
18	0.12969	0.05140	0.14000	-0.05200
19	0.14000	0.05240	0.16000	-0.05442
20	0.16000	0.05442	0.2000	-0.05738
21	0.17000	0.05500	0.24000	-0.05913
22	0.18000	0.05607	0.28000	-0.05993
23	0.19000	0.05676	0.32000	-0.05993
24	0.20000	0.05738	0.36000	-0.05926
25	0.21000	0.05792	0.40000	-0.05803
26	0.22000	0.05839	0.44000	-0.05631
27	0.23000	0.05879	0.50000	-0.05294
28	0.24000	0.05913	0.56000	-0.04878
29	0.25000	0.05941	0.60000	-0.04563
30	0.26000	0.05864	0.70000	-0.03664
31	0.28000	0.05993	0.75000	-0.03160
32	0.30000	0.06002	0.85000	-0.02053

TABLE 2. (Continued)

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
33	0.32000	0.05993	0.90000	-0.01448
34	0.34000	0.05967	0.95000	-0.00807
35	0.36000	0.05926	0.97500	-0.00471
36	0.38000	0.05871	1.00000	0.00000
37	0.40000	0.05800		
38	0.42000	0.05700		
39	0.44000	0.05631		
40	0.47000	0.05473		
41	0.50000	0.05294		
42	0.53000	0.05095		
43	0.56000	0.04878		
44	0.60000	0.04563		
45	0.70000	0.03664		
46	0.75000	0.03160		
47	0.80000	0.02623		
48	0.85000	0.02053		
49	0.90000	0.01448		
50	0.95000	0.00807		
51	0.97500	0.00471		
52	1.00000	0.00000		

* Note: Upper surface horn radius of curvature, $(r/c)_u = 0.00595$.

** Note: Lower surface horn radius of curvature, $(r/c)_l = 0.01042$.

SECTION III:
RUN SUMMARIES

NACA 0012 MODEL - GLAZE ICE CONFIGURATION

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1118	0.00	-0.01	-0.002	-0.001	0.0269	0.0262	-.0075	-.0074	0.125	1.51
1119	2.00	2.05	0.187	0.178	0.0291	0.0283	0.0023	0.0036	0.130	1.50
1120	4.00	4.12	0.386	0.366	0.0402	0.0390	0.0131	0.0156	0.126	1.50
1121	6.00	6.17	0.555	0.523	0.0701	0.0677	0.0136	0.0171	0.125	1.48
1122	8.00	8.10	0.589	0.551	0.1114	0.1066	-.0592	-.0529	0.121	1.46
1123	-2.00	-2.06	-0.186	-0.177	0.0342	0.0333	-.0109	-.0120	0.124	1.50
1124	-4.00	-4.11	-0.378	-0.359	--	--	-.0103	-.0128	0.126	1.50
1125	-6.00	-6.13	-0.540	-0.507	0.0936	0.0899	0.0197	0.0153	0.122	1.48
1126	-8.00	-8.10	-0.600	-0.559	0.1204	0.1150	0.0541	0.0479	0.121	1.47

NACA 0012 MODEL - GLAZE ICE CONFIGURATION, 60 GRIT ROUGHNESS

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1149	4.00	4.12	0.396	0.375	0.0455	0.0442	0.0135	0.0160	0.122	1.56
1150	0.00	-0.01	-0.012	-0.012	0.0300	0.0292	-.0103	-.0102	0.121	1.62
1151	6.00	6.15	0.563	0.529	0.0829	0.0798	-.0019	0.0021	0.121	1.58
1152	1.00	1.01	0.072	0.069	0.0298	0.0289	-.0054	-.0048	0.121	1.62
1153	2.00	2.05	0.174	0.165	0.0318	0.0309	-.0006	0.0007	0.122	1.62
1154	3.00	3.08	0.273	0.259	0.0354	0.0344	0.0048	0.0066	0.122	1.61
1155	4.00	4.12	0.392	0.371	0.0448	0.0435	0.0142	0.0167	0.122	1.62
1156	5.00	5.15	0.474	0.448	0.0587	0.0567	0.0519	0.0189	0.122	1.61
1157	6.00	6.15	0.582	0.545	0.0923	0.0887	-.0119	-.0074	0.122	1.59
1158	7.00	7.12	0.598	0.556	0.1281	0.1222	-.0390	-.0333	0.121	1.56
1159	8.00	8.09	0.554	0.516	--	--	-.0595	-.0534	0.119	1.57
1160	9.00	9.06	0.480	0.447	--	--	-.0625	-.0567	0.119	1.56
1161	0.00	-0.02	-0.037	-0.035	0.0306	0.0298	-.0083	-.0084	0.121	1.61
1162	-1.00	-1.06	-0.116	-0.110	0.0332	0.0323	-.0215	-.0218	0.121	1.60
1163	-2.00	-2.09	-0.238	-0.226	0.0377	0.0366	-.0188	-.0201	0.120	1.60
1164	-1.00	-1.05	-0.125	-0.118	0.0328	0.0319	-.0176	-.0182	0.121	1.62
1166	-3.00	-3.11	-0.334	-0.317	0.0436	0.0423	-.0186	-.0205	0.120	1.60
1167	-4.00	-4.14	-0.405	-0.383	0.0526	0.0509	-.0228	-.02522	0.120	1.60
1168	-5.00	-5.15	-0.497	-0.469	0.0668	0.0645	-.0122	-.0154	0.118	1.60
1169	-6.00	-6.12	-0.558	-0.523	0.0985	0.0945	0.0254	0.0207	0.118	1.59
1170	-7.00	-7.10	-0.533	-0.497	0.1193	0.1140	0.0435	0.0382	0.117	1.57
1171	-8.00	-8.06	-0.477	-0.442	0.1504	0.1428	0.0630	0.0570	0.117	1.56

NACA 0012 MODEL - GLAZE ICE CONFIGURATION, 36 GRIT ROUGHNESS

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1172	6.00	6.15	0.541	0.517	--	--	0.0042	0.0080	0.121	1.55
1173	0.00	-0.01	-0.017	-0.016	0.0298	0.0290	-0.0093	-0.0092	0.120	1.57
1174	1.00	1.01	0.073	0.070	0.0294	0.0286	-0.0052	-0.0045	0.121	1.58
1175	2.00	2.05	0.182	0.173	0.0316	0.0308	0.0012	0.0025	0.121	1.56
1176	3.00	3.09	0.306	0.291	0.0362	0.0352	0.0064	0.0084	0.122	1.56
1177	4.00	4.11	0.370	0.351	0.0432	0.0419	0.0111	0.0135	0.122	1.57
1178	5.00	5.15	0.481	0.454	0.0564	0.0546	0.0160	0.0190	0.122	1.58
1179	6.00	6.15	0.542	0.510	0.0794	0.0765	0.0033	0.0070	0.121	1.60
1180	7.00	7.13	0.589	0.551	0.1101	0.1054	-0.0280	-0.0229	0.120	1.57
1181	8.00	8.10	0.553	0.516	--	--	-0.0433	-0.0379	0.119	1.57
1182	9.00	9.05	0.477	0.446	--	--	-0.0697	-0.0639	0.118	1.54
1184	0.00	-0.01	0.006	0.006	0.0296	0.0288	-0.0071	-0.0069	0.121	1.59
1185	-1.00	-1.03	-0.087	-0.083	0.0322	0.0313	-0.0084	-0.0089	0.120	1.56
1186	-2.00	-2.07	-0.184	-0.174	--	--	-0.0175	-0.0185	0.122	1.61
1187	-2.00	-2.07	--	--	0.0392	0.0380	--	--	0.120	1.61
1188	-3.00	-3.11	-0.304	-0.288	0.0439	0.0426	-0.0232	-0.0248	0.119	1.61
1189	-4.00	-4.12	-0.389	-0.368	0.0525	0.0509	-0.0134	-0.0158	0.119	1.60
1190	-5.00	-5.14	-0.483	-0.455	0.0745	0.0718	-0.0066	-0.0098	0.119	1.60
1191	-6.00	-6.12	-0.528	-0.495	0.1010	0.0969	0.0231	0.0186	0.118	1.59
1192	-7.00	-7.08	-0.525	-0.489	0.1280	0.1221	0.0556	0.0498	0.118	1.55
1193	-8.00	-8.06	-0.470	-0.437	0.1411	0.1342	0.0639	0.0580	0.117	1.57

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α_u (deg)	X/C	R_e $\times 10^{-6}$	U_∞	U_e (ft/s)	δ^*/C	θ/C $\times 10^3$	Y_{stag}/C	Y_{sep}/C
UPPER SURFACE									
1218	0.00	-0.02	1.51	132.9	166.3	0.00256	0.08368	0.001206	0.001294
1219	0.00	0.00	1.54	134.7	170.8	0.01379	2.06816	0.009277	0.013129
1220	0.00	0.02	1.52	133.4	174.4	0.01938	3.59458	0.011610	0.018316
1221	0.00	0.04	1.51	132.5	170.7	0.01329	3.07344	0.006240	0.011052
1222	0.00	0.06	1.51	132.5	159.9	0.00849	2.29566	0.001769	0.003223
1223	0.00	0.08	1.52	132.2	151.0	0.00501	2.60386	--	--
1224	0.00	0.10	1.51	131.6	151.0	0.00388	2.42981	--	--
1225	0.00	0.12	1.50	130.7	151.0	0.00302	1.93082	--	--
1226	0.00	0.30	1.51	130.8	153.1	0.00260	1.75967	--	--
1227	0.00	0.60	1.52	131.7	143.4	0.00377	2.63889	--	--
LOWER SURFACE									
1228	0.00	0.03	1.58	133.9	165.1	0.00274	0.20916	0.002090	0.002163
1229	0.00	0.04	1.58	133.6	169.9	0.01038	1.17907	0.007456	0.009837
1230	0.00	0.06	1.58	133.8	176.3	0.02194	2.69767	0.015746	0.020972
1231	0.00	0.08	1.54	133.2	182.5	0.02581	3.87665	0.016286	0.024223
1232	0.00	0.10	1.53	132.2	184.4	0.02421	4.89539	0.012915	0.021599
1233	0.00	0.12	1.52	132.2	180.3	0.02174	4.94855	0.010273	0.018256
1234	0.00	0.14	1.51	132.8	179.1	0.01932	4.46379	0.008019	0.014209
1235	0.00	0.16	1.50	132.6	170.0	0.01587	3.93228	0.004049	0.006794
1236	0.00	0.20	1.50	132.1	159.5	0.01114	4.93231	--	--
1237	0.00	0.32	1.51	132.5	153.9	0.00635	4.41128	--	--
1238	0.00	0.60	1.51	132.6	142.9	0.00585	4.36459	--	--
LOWER SURFACE									
1240	2.00	0.03	1.58	133.3	149.9	0.00277	0.19498	0.001936	0.002248
1241	2.00	0.04	1.57	132.7	153.7	0.00869	1.01987	0.006457	0.008171
1242	2.00	0.06	1.57	132.8	159.1	0.01933	2.67214	0.012980	0.018183
1243	2.00	0.08	1.56	131.7	159.7	0.02223	3.95914	0.012943	0.020362
1244	2.00	0.10	1.56	131.9	157.0	0.01904	4.15164	0.009676	0.016275
1245	2.00	0.12	1.54	130.8	153.4	0.01550	3.59228	0.006314	0.011235
1246	2.00	0.14	1.55	130.9	145.6	0.01298	3.33829	0.002634	0.004886
1247	2.00	0.16	1.54	130.6	139.5	0.00952	4.00359	--	--
1248	2.00	0.20	1.52	129.8	141.3	0.00634	3.90459	--	--
1249	2.00	0.32	1.52	129.8	142.9	0.00413	2.98002	--	--
1250	2.00	0.60	1.52	129.6	138.7	0.00469	3.47950	--	--

¹ Each data point represents the average of 2,000 samples at 2 KHz with a 1KHz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α_u (deg)	X/C	R_e $\times 10^{-6}$	U_∞	U_e (ft/s)	δ^*/C	θ/C $\times 10^3$	Y_{stag}/C	Y_{sep}/C
LOWER SURFACE									
1251	4.00	0.03	1.49	127.1	140.4	0.00322	0.28970	0.002246	0.002420
1252	4.00	0.04	1.50	127.7	144.5	0.00790	1.04821	0.005119	0.007175
1253	4.00	0.06	1.49	127.3	148.7	0.01784	2.55881	0.011402	0.016488
1254	4.00	0.08	1.50	127.7	150.1	0.01876	3.48887	0.009945	0.016482
1255	4.00	0.10	1.50	127.8	145.9	0.01531	3.64209	0.006255	0.011989
1256	4.00	0.12	1.50	128.0	137.3	0.01163	2.93611	0.002925	0.005636
1257	4.00	0.14	1.49	127.6	133.5	0.00906	3.66426	--	--
1258	4.00	0.16	1.49	127.8	131.9	0.00657	3.61518	--	--
1259	4.00	0.20	1.50	128.3	133.2	0.00447	2.96064	--	--
1260	4.00	0.32	1.51	128.8	137.9	0.00325	2.32106	--	--
1261	4.00	0.60	1.52	129.3	135.6	0.00377	2.74562	--	--
LOWER SURFACE									
1263	4.00	0.04	1.54	131.1	143.1	0.00703	1.02225	0.003531	0.005215
1264	4.00	0.06	1.55	131.7	147.7	0.01578	2.26427	0.009532	0.014213
1265	4.00	0.08	1.54	131.0	148.0	0.01985	3.66746	0.010630	0.017507
1266	4.00	0.10	1.54	130.9	143.3	0.01607	3.61896	0.006585	0.012288
1267	4.00	0.12	1.53	130.5	137.8	0.01302	3.24311	0.003728	0.006543
1268	4.00	0.14	1.54	130.9	133.8	0.01052	3.82705	--	--
1269	4.00	0.16	1.53	130.7	132.0	0.00773	4.04689	--	--
1270	4.00	0.20	1.54	131.0	132.4	0.00519	3.38527	--	--
1271	4.00	0.32	1.53	131.0	135.9	0.00361	2.58847	--	--
1272	4.00	0.60	1.54	131.1	134.6	0.00391	2.85567	--	--
UPPER SURFACE									
1276	4.00	0.02	1.56	132.3	191.7	0.03078	3.87014	0.022805	0.029965
1277	4.00	0.04	1.56	132.8	191.7	0.03146	5.29906	0.021205	0.030443
1278	4.00	0.06	1.56	132.1	191.9	0.02927	5.96122	0.017012	0.027360
1279	4.00	0.08	1.56	132.3	190.4	0.02739	6.15397	0.014398	0.024604
1280	4.00	0.10	1.56	132.3	184.6	0.02467	5.49842	0.011652	0.019969
1281	4.00	0.12	1.55	131.3	179.7	0.02243	5.08189	0.008697	0.015248
1282	4.00	0.14	1.56	132.1	173.6	0.01996	5.17859	0.003021	0.005853
1283	4.00	0.16	1.55	131.7	170.1	0.01718	6.06629	--	--
1284	4.00	0.18	1.55	132.0	166.3	0.01533	6.70712	--	--
1285	4.00	0.20	1.55	131.6	164.1	0.01415	6.93622	--	--
1286	4.00	0.30	1.55	131.8	156.8	0.01103	7.10135	--	--
1287	4.00	0.60	1.53	130.4	145.1	0.01363	9.75852	--	--

¹ Each data point represents the average of 2,000 samples at 2Khz with a 1Khz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α_u (deg)	X/C	R_e $\times 10^{-6}$	U_∞	U_e (ft/s)	δ^*/C	θ/C $\times 10^3$	Y_{stag}/C	Y_{sep}/C
UPPER SURFACE									
1288	4.00	-0.02	1.51	129.7	146.1	0.00443	1.17114	0.002467	0.003133
1289	4.00	0.00	1.52	129.8	173.2	0.02067	2.43574	0.015509	0.019987
1290	4.00	0.02	1.52	130.4	184.5	0.03148	4.08657	0.022612	0.030640
1291	4.00	0.04	1.52	130.0	190.8	0.02962	4.84494	0.018890	0.028245
1292	4.00	0.06	1.52	130.0	194.2	0.02896	5.69942	0.016327	0.026883
1293	4.00	0.08	1.52	130.2	195.1	0.02658	5.77973	0.013564	0.023495
1294	4.00	0.10	1.52	130.3	191.9	0.02469	5.51482	0.011552	0.020470
1295	4.00	0.12	1.53	131.1	185.7	0.02242	5.00107	0.008816	0.016217
1296	4.00	0.14	1.53	130.8	179.5	0.02016	4.81829	0.005341	0.009662
1297	4.00	0.16	1.54	131.2	173.0	0.01743	5.38042	--	--
1298	4.00	0.18	1.54	131.2	166.5	0.01545	6.07596	--	--
1299	4.00	0.20	1.54	131.0	163.1	0.01404	6.48157	--	--
1300	4.00	0.30	1.55	131.5	156.1	0.01040	6.78434	--	--
1301	4.00	0.60	1.53	130.3	144.2	0.01352	9.85275	--	--
UPPER SURFACE									
1302	2.00	-0.02	1.54	130.5	138.7	0.00325	0.61470	0.002111	0.002150
1303	2.00	0.00	1.54	131.2	165.2	0.01823	2.57040	0.013138	0.017587
1304	2.00	0.02	1.54	131.2	177.9	0.02532	3.95163	0.017222	0.024493
1305	2.00	0.04	1.53	130.8	179.5	0.02191	4.48966	0.012344	0.020434
1306	2.00	0.06	1.54	131.3	176.5	0.01763	4.04237	0.008360	0.015040
1307	2.00	0.08	1.54	131.4	168.3	0.01321	3.10815	0.004641	0.008096
1308	2.00	0.10	1.54	131.1	160.9	0.01016	3.47808	--	--
1309	2.00	0.12	1.54	131.2	156.8	0.00806	3.91730	--	--
1310	2.00	0.14	1.53	130.8	154.1	0.00637	3.67451	--	--
1311	2.00	0.16	1.54	130.9	154.1	0.00527	3.29312	--	--
1312	2.00	0.30	1.55	131.9	153.8	0.00457	3.27906	--	--
1313	2.00	0.60	1.54	131.8	143.4	0.00631	4.70146	--	--

¹ Each data point represents the average of 2,000 samples at 2Khz with a 1Khz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α_{11} (deg)	X/C	R_e $\times 10^{-6}$	U_{∞}	U_e (ft/s)	δ^*/C	θ/C $\times 10^3$	Y_{stag}/C	Y_{sep}/C
UPPER SURFACE									
1344	6.00	-0.02	1.53	130.2	129.3	0.00552	1.06619	0.003710	0.004770
1346	6.00	0.02	1.53	129.8	167.3	0.03805	4.53448	0.028434	0.037064
1347	6.00	0.00	1.53	130.3	155.1	0.02531	2.94743	0.019326	0.024635
1348	6.00	0.04	1.53	130.1	171.7	0.03948	5.47956	0.027536	0.038037
1349	6.00	0.06	1.52	129.0	174.9	0.04108	6.49270	0.026288	0.039096
1350	6.00	0.08	1.52	129.0	179.5	0.04222	7.29865	0.025410	0.039702
1351	6.00	0.10	1.51	128.3	180.3	0.04390	8.03802	0.025263	0.040887
1352	6.00	0.12	1.51	128.0	182.7	0.04541	8.59370	0.025835	0.041558
1353	6.00	0.14	1.50	127.4	184.2	0.04620	9.11629	0.023625	0.041200
1354	6.00	0.16	1.48	126.1	183.3	0.04706	9.61884	0.023138	0.041395
1355	6.00	0.18	1.49	126.5	181.9	0.04821	9.88036	0.024241	0.041712
1356	6.00	0.20	1.49	126.3	180.7	0.04969	10.23559	0.023714	0.041902
1357	6.00	0.22	1.47	124.9	179.6	0.05007	10.14880	0.022834	0.040868
1358	6.00	0.24	1.46	124.1	176.1	0.05009	10.48751	0.020869	0.038888
1359	6.00	0.26	1.47	124.8	173.8	0.04966	10.33775	0.019498	0.036108
1360	6.00	0.28	1.46	124.3	172.2	0.04948	10.36652	0.018550	0.032963
1361	6.00	0.30	1.47	124.3	168.3	0.04942	10.80872	0.015084	0.029309
1362	6.00	0.34	1.46	124.0	163.7	0.04752	11.56415	0.006308	0.015349
1363	6.00	0.38	1.46	123.3	155.7	0.04856	15.38423	--	--
1364	6.00	0.42	1.46	123.4	154.5	0.04852	15.08397	--	--
1365	6.00	0.47	1.46	123.7	151.4	0.04865	17.42703	--	--
1366	6.00	0.53	1.45	123.0	145.0	0.04900	19.35245	--	--
1367	6.00	0.60	1.46	123.2	140.6	0.05055	21.83168	--	--

¹ Each data point represents the average of 2,000 samples at 2 Khz with a 10 Khz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α (deg)	X/C	R_e $\times 10^{-6}$	U_∞ (ft/s)	U_e (ft/s)	δ^*/C	θ/C
WAKE							
1850	0.00	1.80	1.57	138.4	135.7	0.01766	14.82117
1852	2.00	1.80	1.57	138.7	136.6	0.01930	16.24803
1856	4.00	1.80	1.61	138.6	128.4	0.02605	21.60597
1858	6.00	1.80	1.59	136.9	127.6	0.04478	36.59986
1859	-4.00	1.80	1.61	138.2	127.6	0.03064	25.74941
1860	-4.00	1.60	1.62	139.3	126.8	0.03235	26.47818
1862	0.00	1.60	1.62	139.5	129.0	0.01860	15.41965
1863	2.00	1.60	1.62	139.3	128.8	0.01883	15.56903
1864	4.00	1.60	1.62	139.6	129.2	0.02679	21.92687
1865	6.00	1.60	1.60	138.0	129.2	0.04913	38.81922
1866	6.00	1.40	1.60	137.6	129.5	0.05351	40.39152
1867	4.00	1.40	1.62	139.2	129.1	0.02857	22.81225
1868	2.00	1.40	1.63	139.9	127.8	0.01942	15.73106
1869	0.00	1.40	1.62	139.5	127.6	0.01858	15.04000
1870	-4.00	1.40	1.62	139.0	128.0	0.00061	0.01775
1872	0.00	1.20	1.62	139.5	126.0	0.02084	16.16307
1873	2.00	1.20	1.62	139.7	126.3	0.02176	17.05751
1874	4.00	1.20	1.62	139.2	126.9	0.03085	23.57301
1876	6.00	1.20	1.60	137.8	128.3	0.05827	40.11375
UPPER SURFACE							
1879	2.00	1.00	1.62	139.5	127.1	0.03332	22.36647
1880	4.00	1.00	1.62	139.2	128.7	0.04187	28.15812
1881	6.00	1.00	1.60	138.0	132.1	0.07399	42.70959
WAKE							
1885	6.00	1.20	1.55	138.3	143.0	0.06079	42.16321
1886	6.00	1.40	1.54	137.8	143.3	0.05282	39.78783
1887	6.00	1.60	1.60	138.0	130.0	0.04946	39.10095
1888	6.00	1.80	1.60	138.1	130.5	0.04718	38.47595

¹ Each data point represents the average of 2,000 samples at 2 Khz with a 1 Khz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES¹

RUN	α (deg)	X/C	R_e $\times 10^{-6}$	U_∞ (ft/s)	U_e (ft/s)	δ^*/C	θ/C
UPPER SURFACE							
1892	0.00	0.60	1.63	140.5	146.5	0.00415	2.88285
1893	2.00	0.60	1.63	140.3	150.2	0.00691	5.11234
1894	4.00	0.60	1.62	139.8	149.3	0.01338	9.70465
1895	6.00	0.60	1.61	138.9	150.3	0.03779	20.83421
1897	-4.00	0.60	1.68	139.3	127.6	0.00222	1.35198
1899	-4.00	0.80	1.67	142.1	137.5	0.00301	1.92959
1900	0.00	0.80	1.68	143.1	138.7	0.00523	3.66435
1901	2.00	0.80	1.67	142.3	139.9	0.00899	6.57726
1902	4.00	0.80	1.69	142.1	136.6	0.01634	11.82204
1903	6.00	0.80	1.68	141.1	137.4	0.04488	26.15406
1904	6.00	0.90	1.67	140.9	135.1	0.05363	30.77714
1905	4.00	0.90	1.68	141.7	134.0	0.02379	16.58441
1906	2.00	0.90	1.70	142.7	133.0	0.01236	9.06991
1907	0.00	0.90	1.69	141.8	131.5	0.00710	5.07290
1908	-4.00	0.90	1.70	143.1	131.7	0.00366	2.44436
1909	-4.00	1.00	1.70	142.8	128.2	0.00531	3.42559
1910	0.00	1.00	1.70	143.3	127.7	0.01021	6.78563
1911	2.00	1.00	1.70	143.4	129.2	0.01650	11.08343
1912	4.00	1.00	1.69	142.0	132.6	0.03153	20.27576
1913	6.00	1.00	1.68	141.3	133.7	0.06266	33.91847

¹ Each data point represents the average of 2,000 samples at 2 Khz with a 1 Khz low-pass filter.

NACA 0012 MODEL NO. 2 - GLAZE ICE CONFIGURATION
 SPLIT FILM VELOCITY PROFILES

RUN	α_u (deg)	X/C	Re $\times 10^{-6}$	U_∞ (ft/s)	U_e (ft/s)	δ^*/C	θ/C $\times 10^3$	Y-stag/C	Y-sep/C
1915 ¹	10.00	0.04	1.60	136.2	143.9	0.04301	5.61951	0.031715	0.041692
1916 ¹	8.00	0.04	1.61	137.0	149.4	0.03819	5.54065	0.027111	0.036917
1917 ¹	4.00	0.04	1.66	141.1	152.6	0.03111	5.63747	0.020469	0.030256
1925 ¹	4.00	0.20	1.66	141.1	153.8	0.01028	5.29112	--	--
1926 ¹	10.00	0.20	1.59	135.6	153.6	0.08171	16.99286	0.048324	0.075894
1927 ¹	10.00	0.50	1.59	135.3	152.1	0.15801	37.35664	0.086952	0.014530
1928 ²	0.00	0.00	1.58	140.5	157.3	0.01498	2.42523	0.009900	0.014389
1929 ²	2.00	0.00	1.58	140.1	167.6	0.01900	2.84426	0.013405	0.018421
1930 ²	4.00	0.00	1.57	139.9	167.8	0.02160	2.85243	0.015521	0.020875
1931 ¹	4.00	0.00	1.58	140.5	168.2	0.02140	2.85181	0.015495	0.020761
1932 ¹	4.00	0.04	1.58	140.4	169.7	0.03048	5.48212	0.019727	0.029523
1933 ²	4.00	0.04	1.61	139.8	157.7	0.03034	5.50181	0.019266	0.093628
1934 ²	6.00	0.04	1.61	139.5	157.5	0.03824	5.97609	0.026889	0.037162
1935 ¹	6.00	0.04	1.61	139.3	157.4	0.03792	5.83559	0.025946	0.036672
1936 ¹	8.00	0.04	1.58	136.9	148.5	0.04254	5.92125	0.030666	0.040896
1937 ²	8.00	0.04	1.56	135.4	149.7	0.04242	5.81611	0.030615	0.040379
1938 ²	10.00	0.04	1.56	135.1	134.9	0.04315	6.07493	0.031773	0.041806
1939 ¹	10.00	0.04	1.55	134.3	135.6	0.04270	5.88866	0.031190	0.041149
1940 ²	2.00	0.04	1.62	140.0	158.1	0.02038	4.65249	0.011004	0.018897
1941 ²	0.00	0.04	1.63	140.9	152.3	0.01232	2.82245	0.004958	0.009337
1942 ²	4.00	0.08	1.62	140.2	158.4	0.02501	5.90061	0.012873	0.022778
1944 ¹	4.00	0.08	1.55	138.9	170.7	0.02568	6.32683	0.013113	0.023166
1946 ¹	4.00	0.12	1.55	138.6	171.0	0.02081	4.64299	0.008902	0.015849
1947 ²	4.00	0.12	1.55	139.1	171.0	0.01958	4.55180	0.007755	0.014023
1948 ²	4.00	0.16	1.56	139.6	171.0	0.01539	5.00079	--	--
1949 ¹	4.00	0.16	1.55	138.5	171.0	0.01500	5.11705	--	--
1950 ¹	4.00	0.20	1.55	138.5	170.7	0.01223	6.16270	--	--
1951 ²	4.00	0.20	1.56	140.1	170.8	0.01223	6.10086	--	--
1952 ²	10.00	0.20	1.49	133.7	164.9	0.08371	17.95642	0.048933	0.079398
1953 ¹	10.00	0.20	1.49	133.4	164.1	0.08275	18.25781	0.048211	0.078107
1954 ¹	10.00	0.50	1.50	134.1	169.0	0.15810	36.94591	0.084156	0.144860
1955 ²	10.00	0.50	1.49	133.8	168.2	0.15927	36.00207	0.088328	0.147131

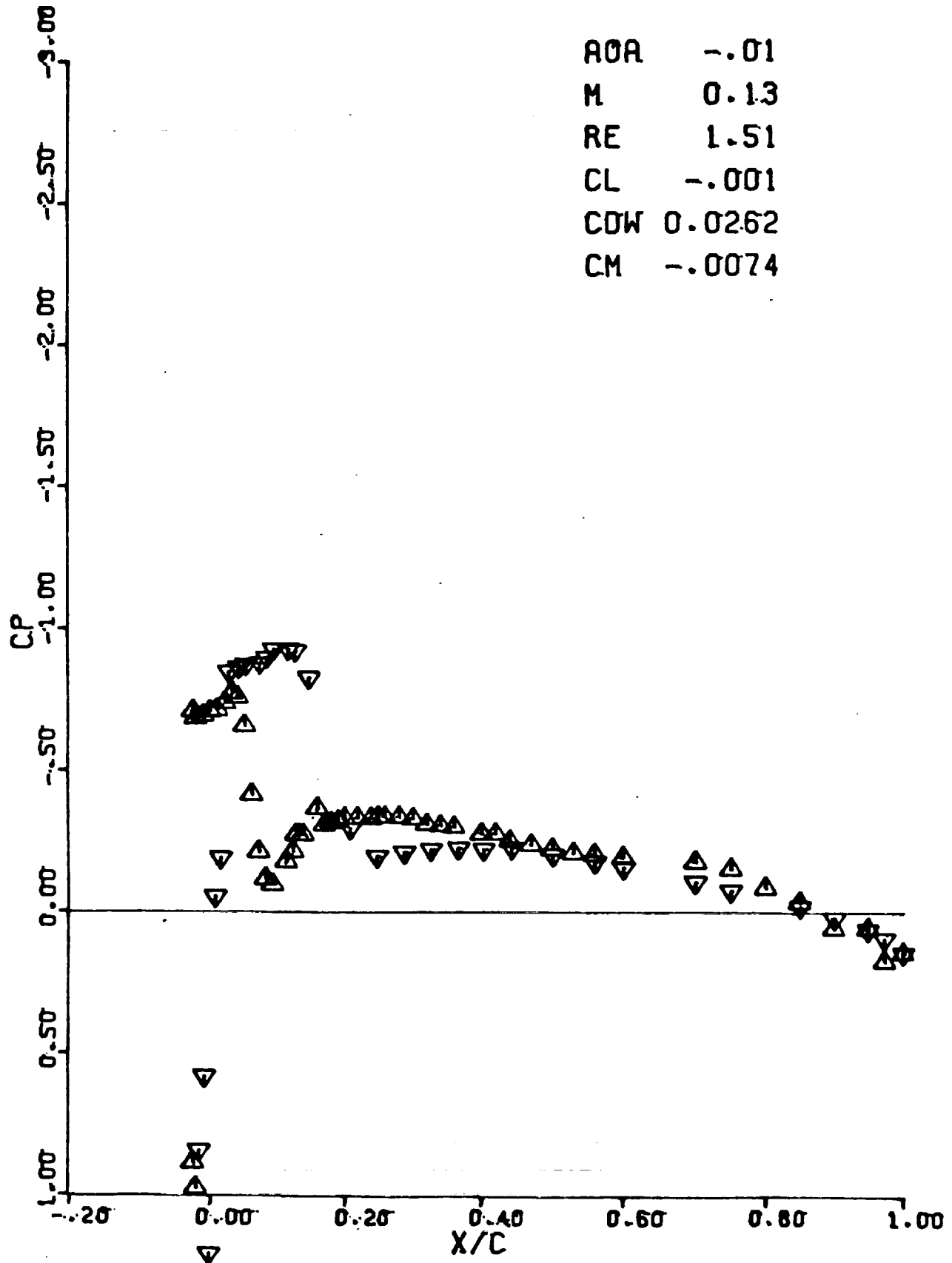
¹ Each data point represents the average of 10,000 samples at 2 Khz with a 1 Khz low-pass filter.

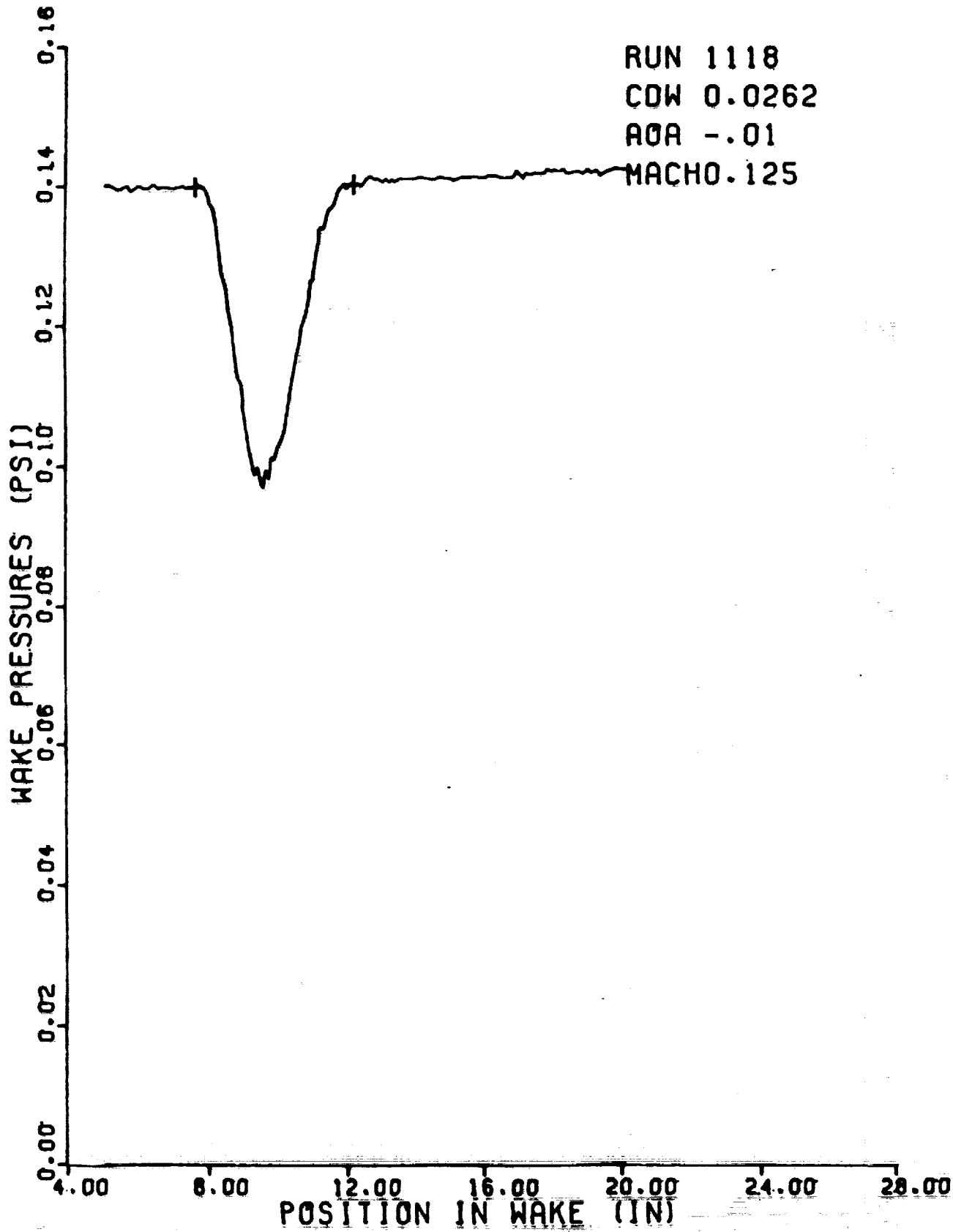
² Each data point represents the average of 10,000 samples at 10 Khz with a 5Khz low-pass filter.

SECTION IV: DATA PLOTS

RUN 1.1.18

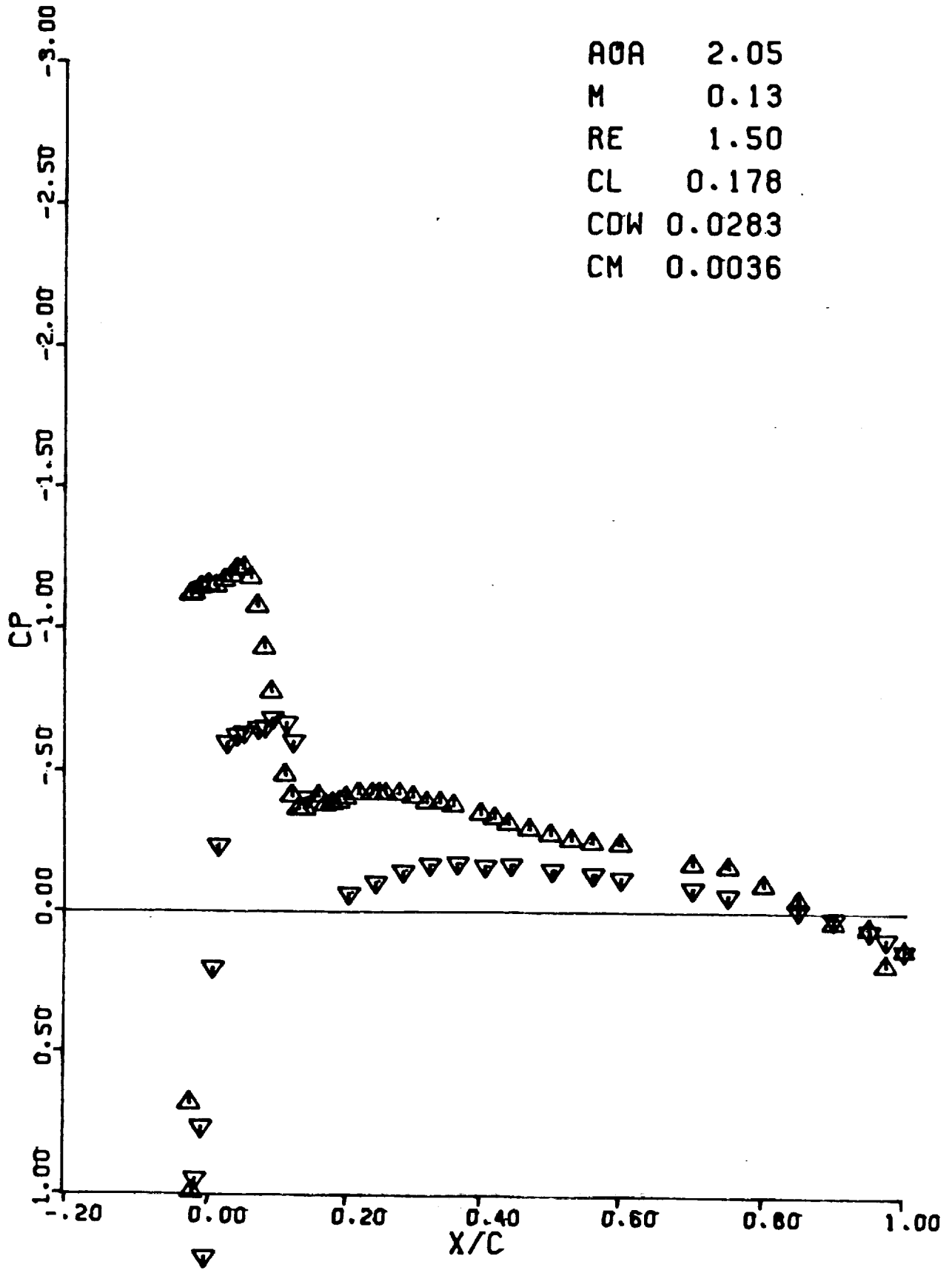
AOA -.01
M 0.13
RE 1.51
CL -.001
CDW 0.0262
CM -.0074

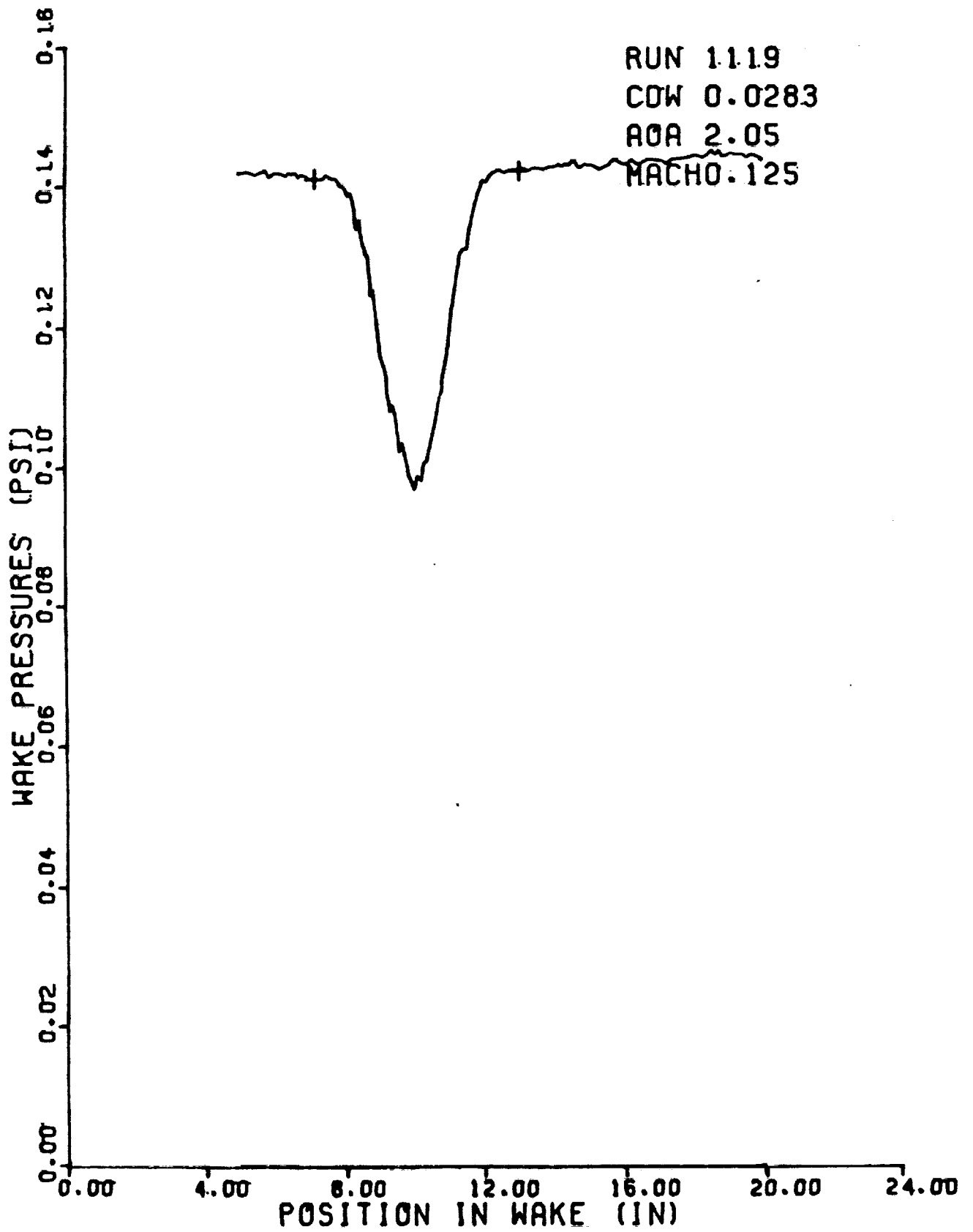




RUN 1119

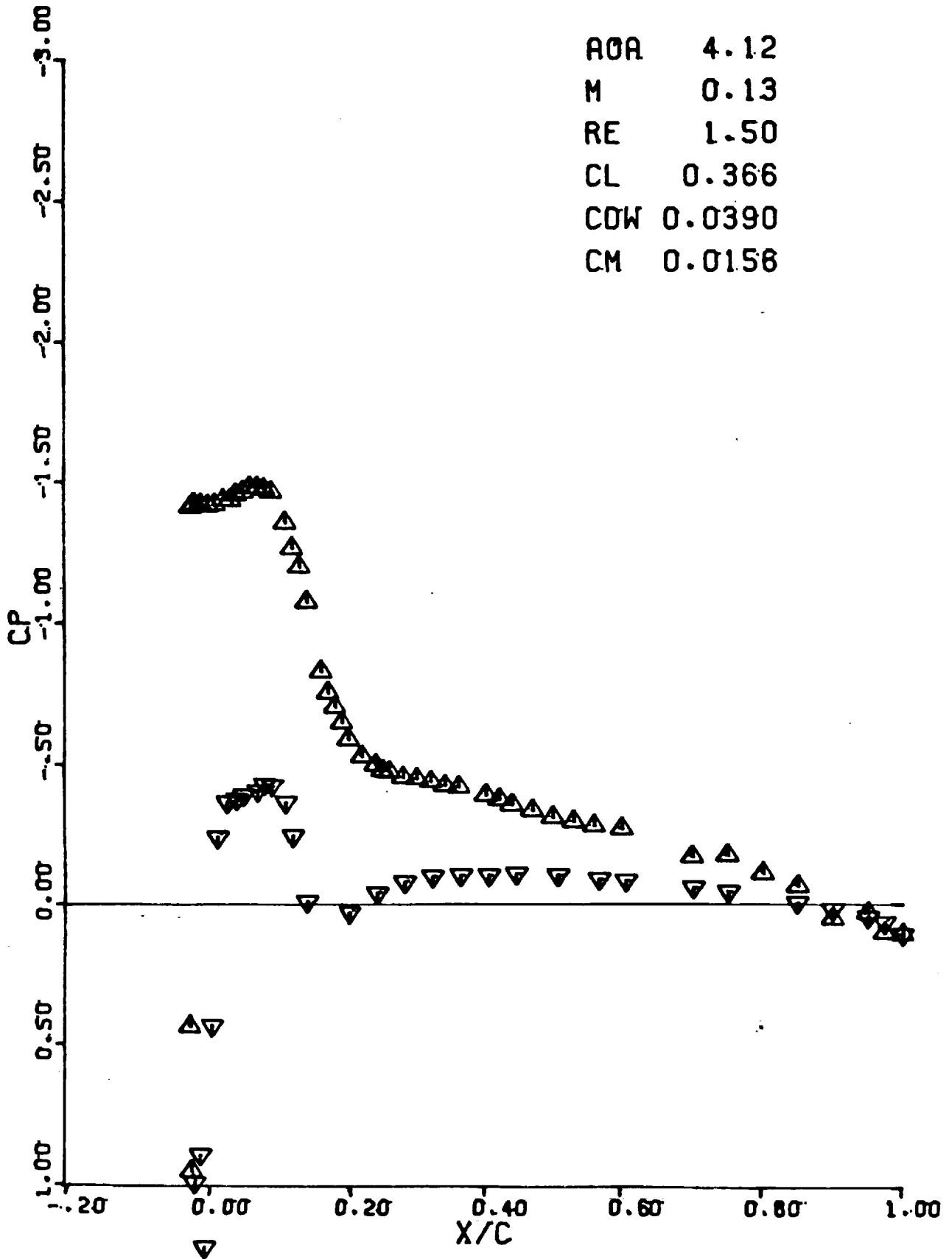
AOA 2.05
M 0.13
RE 1.50
CL 0.178
CDW 0.0283
CM 0.0036

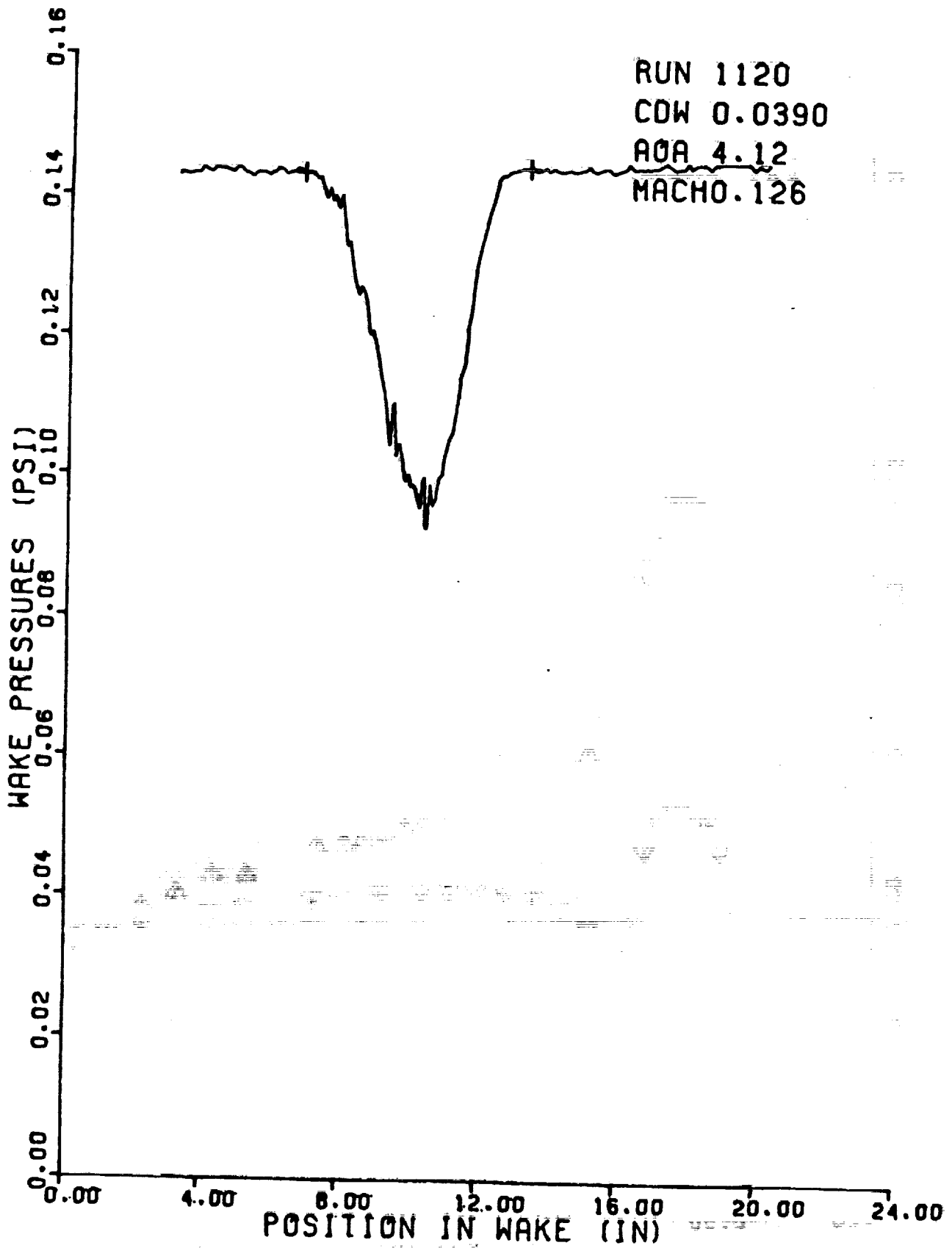




RUN 1120

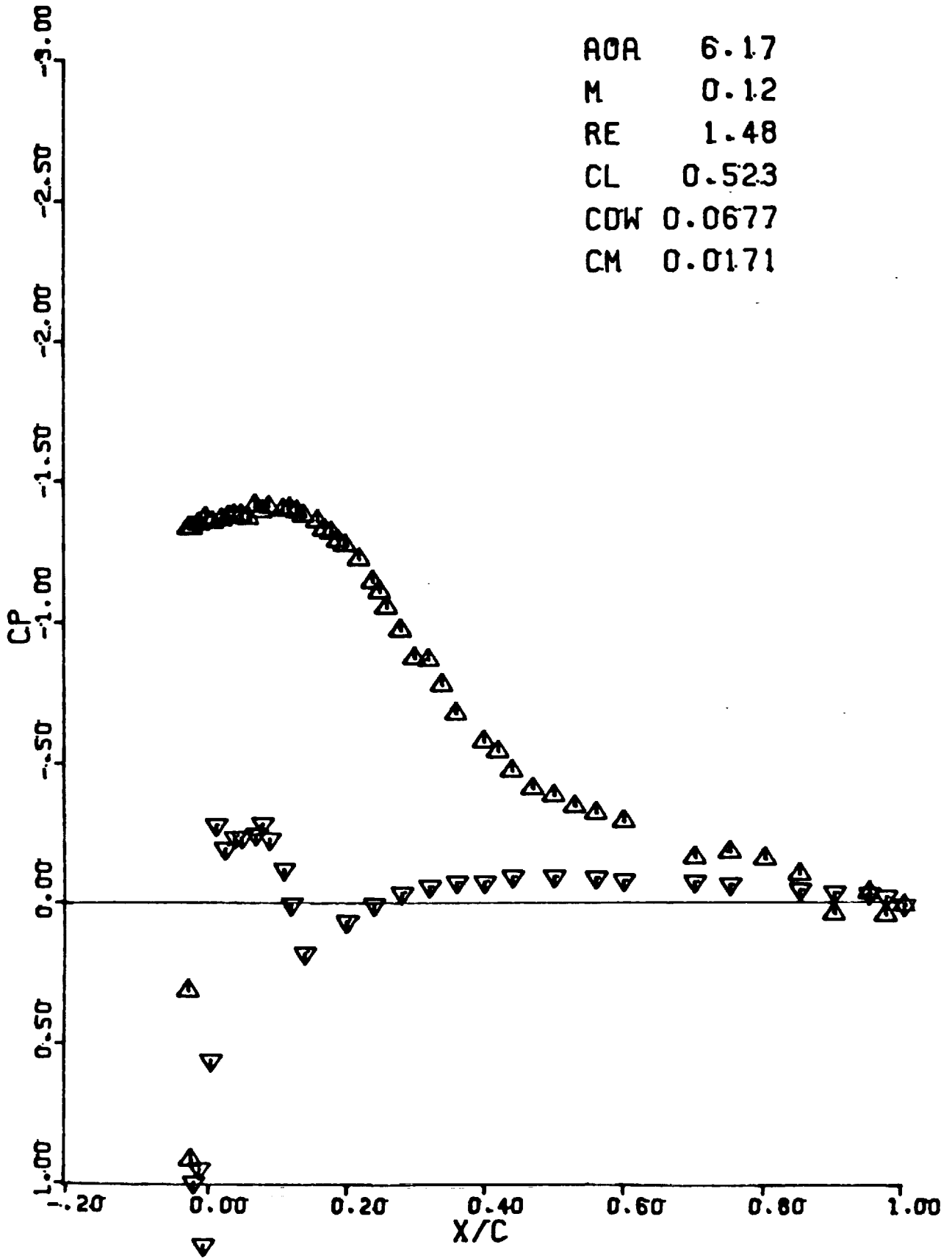
AOA 4.12
M 0.13
RE 1.50
CL 0.366
CDW 0.0390
CM 0.0158

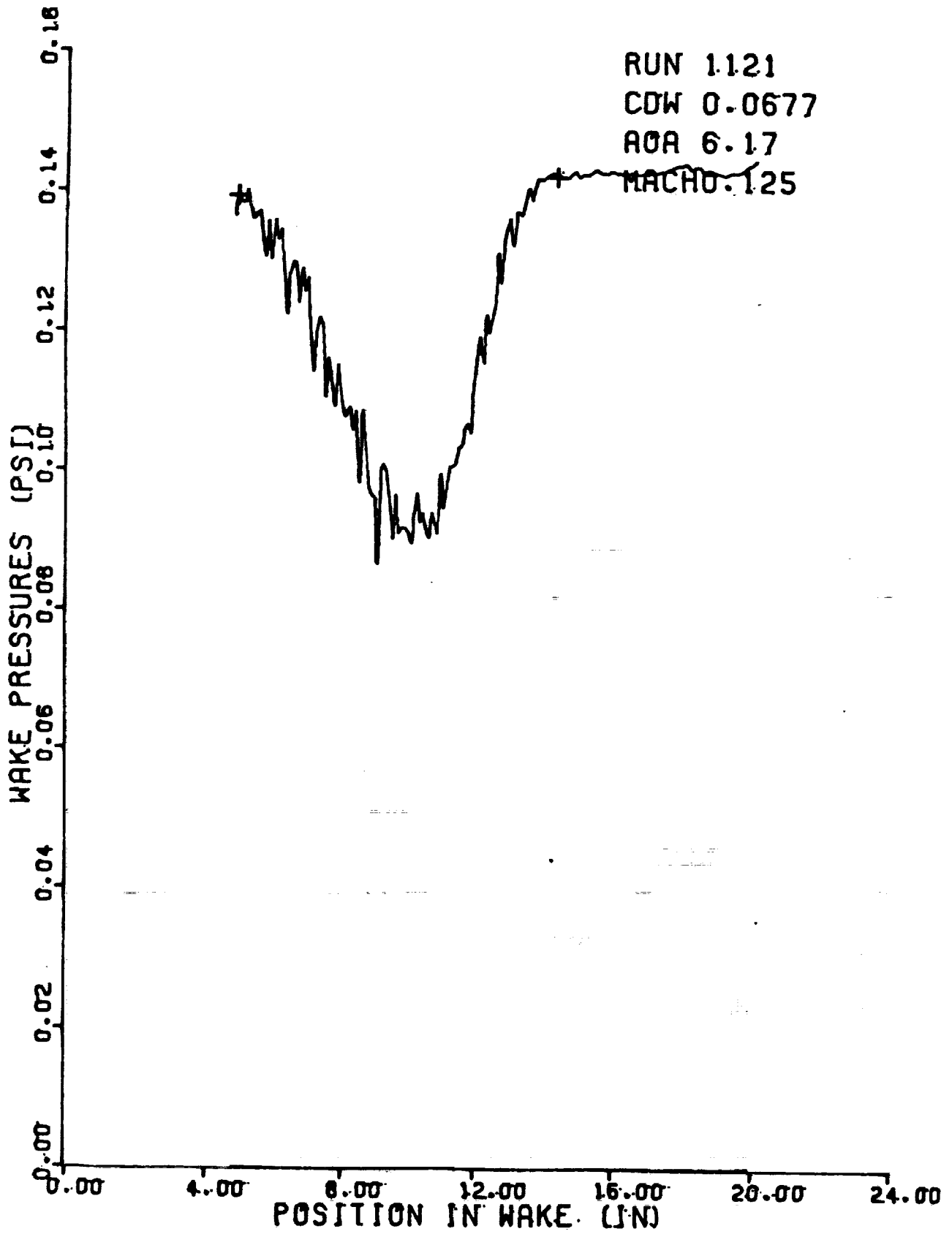




RUN 1121

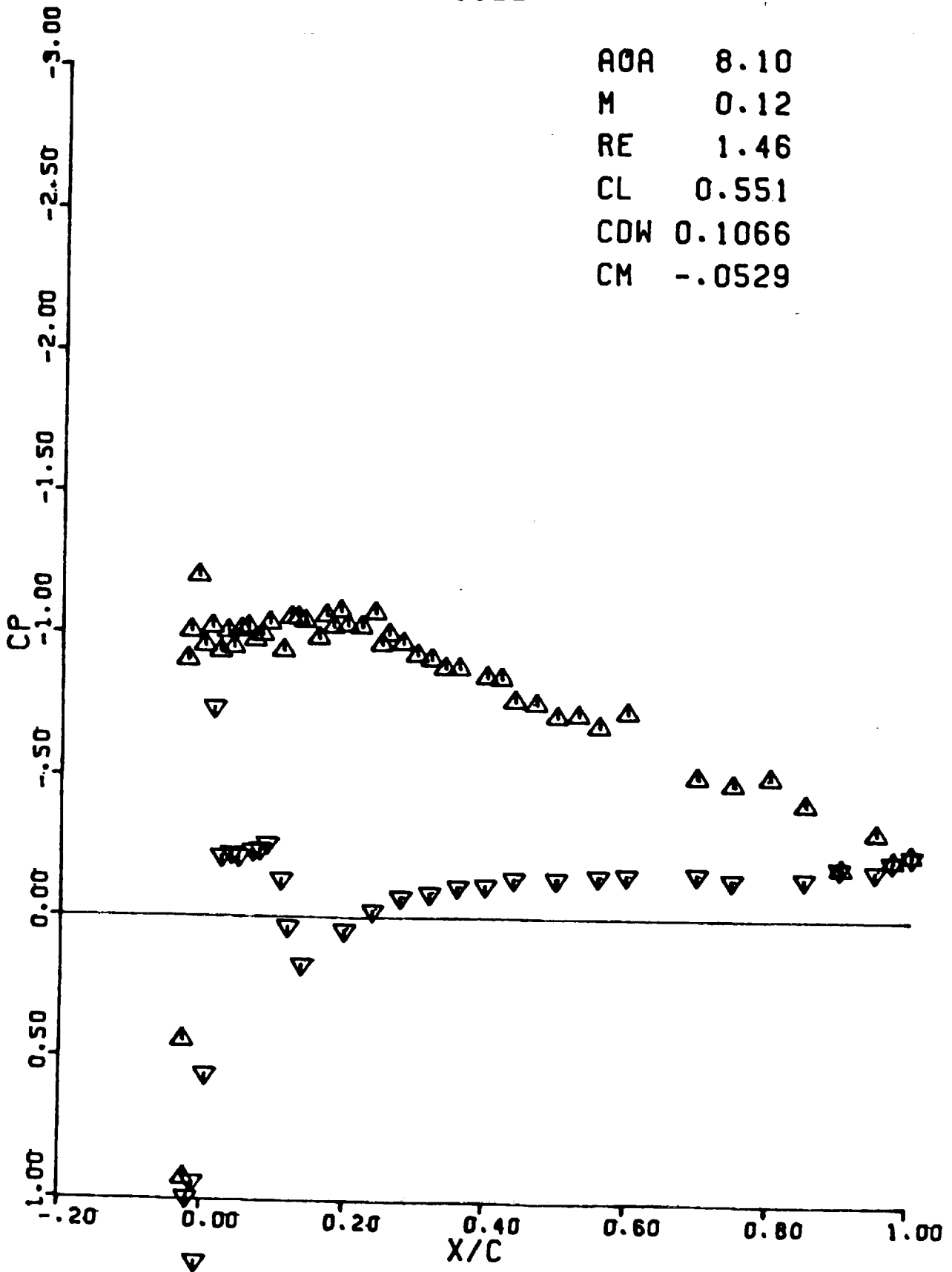
AOA 6.17
M 0.12
RE 1.48
CL 0.523
CDW 0.0677
CM 0.0171

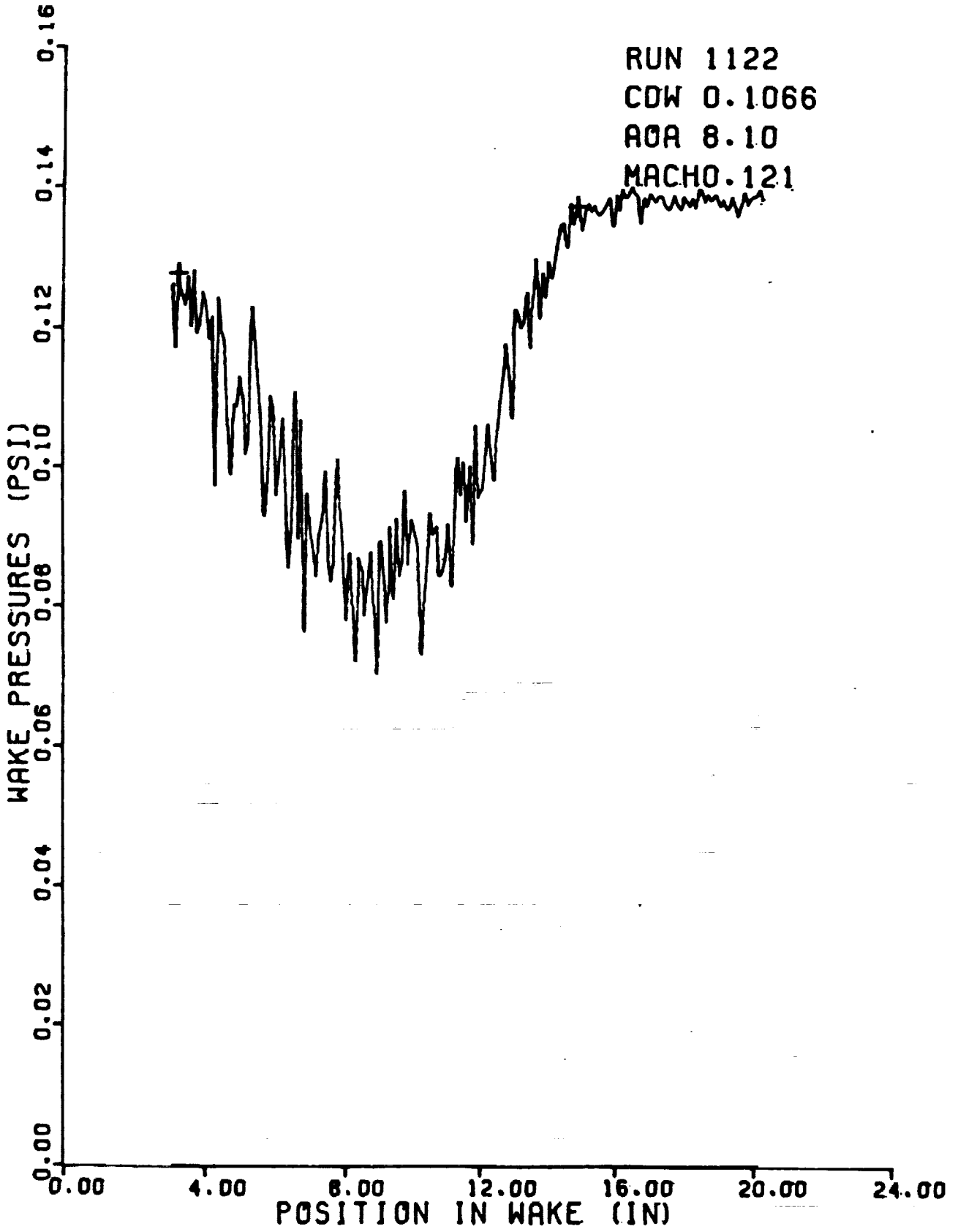




RUN 1122

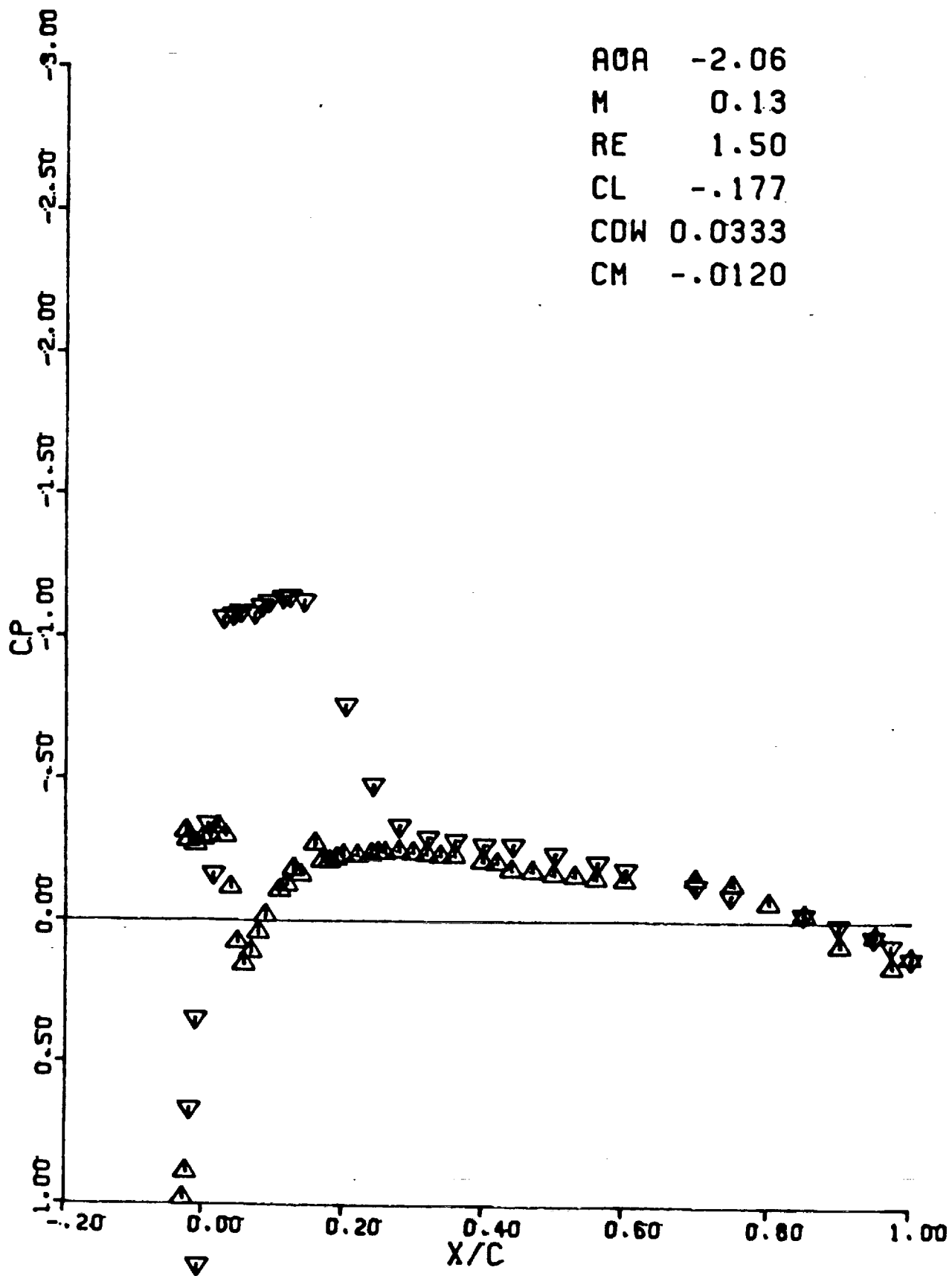
AOA 8.10
M 0.12
RE 1.46
CL 0.551
CDW 0.1066
CM -.0529

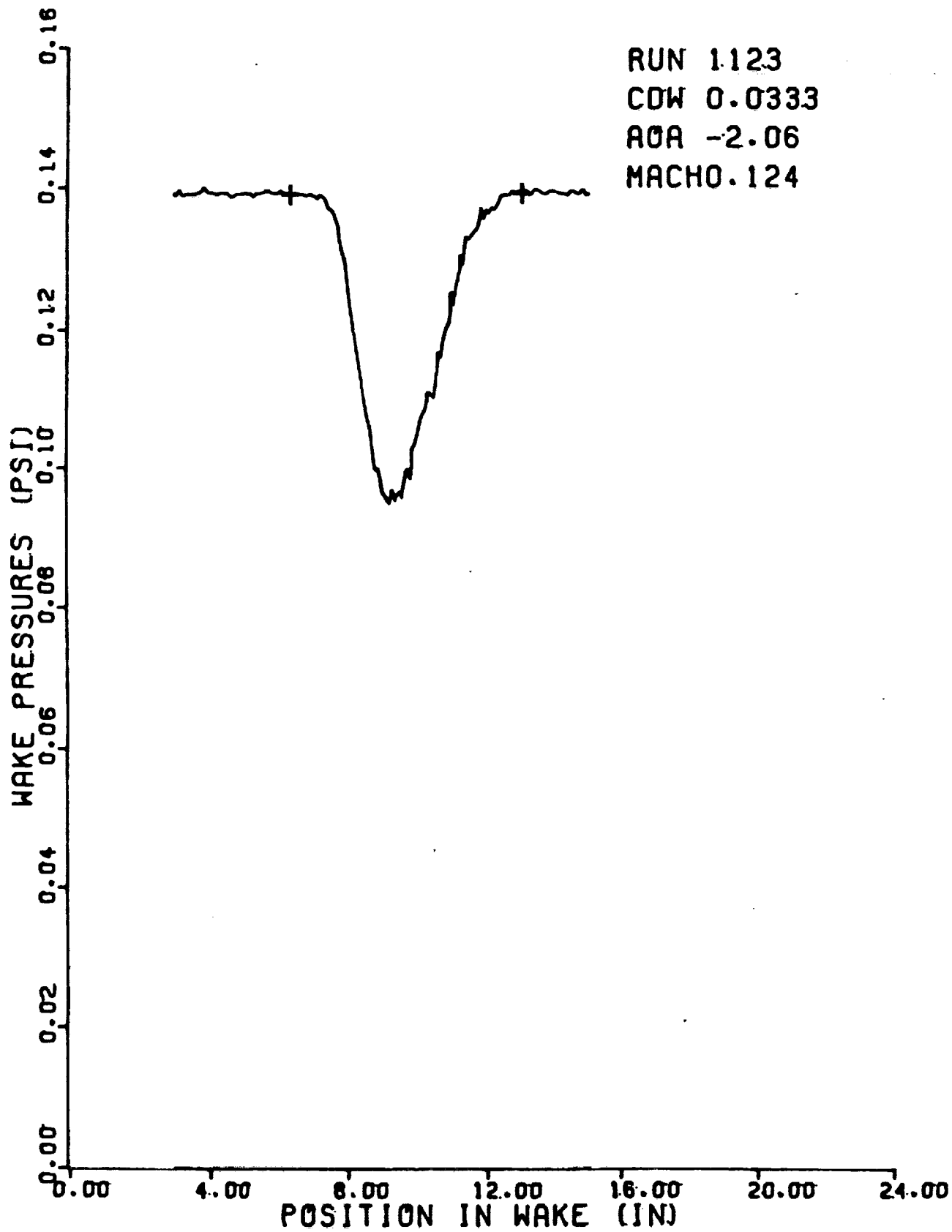




RUN 1123

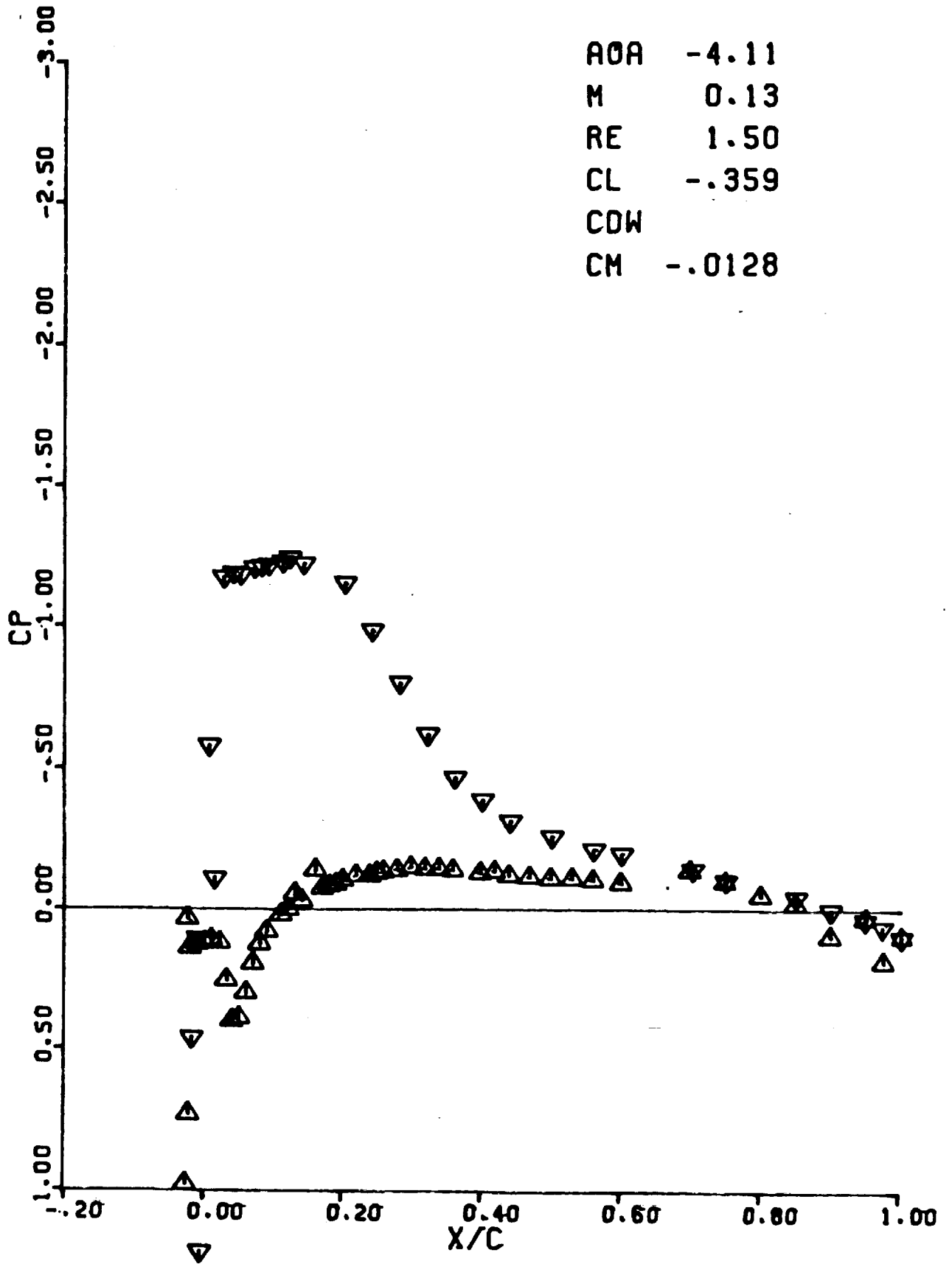
AOA -2.06
M 0.13
RE 1.50
CL -.177
CDW 0.0333
CM -.0120





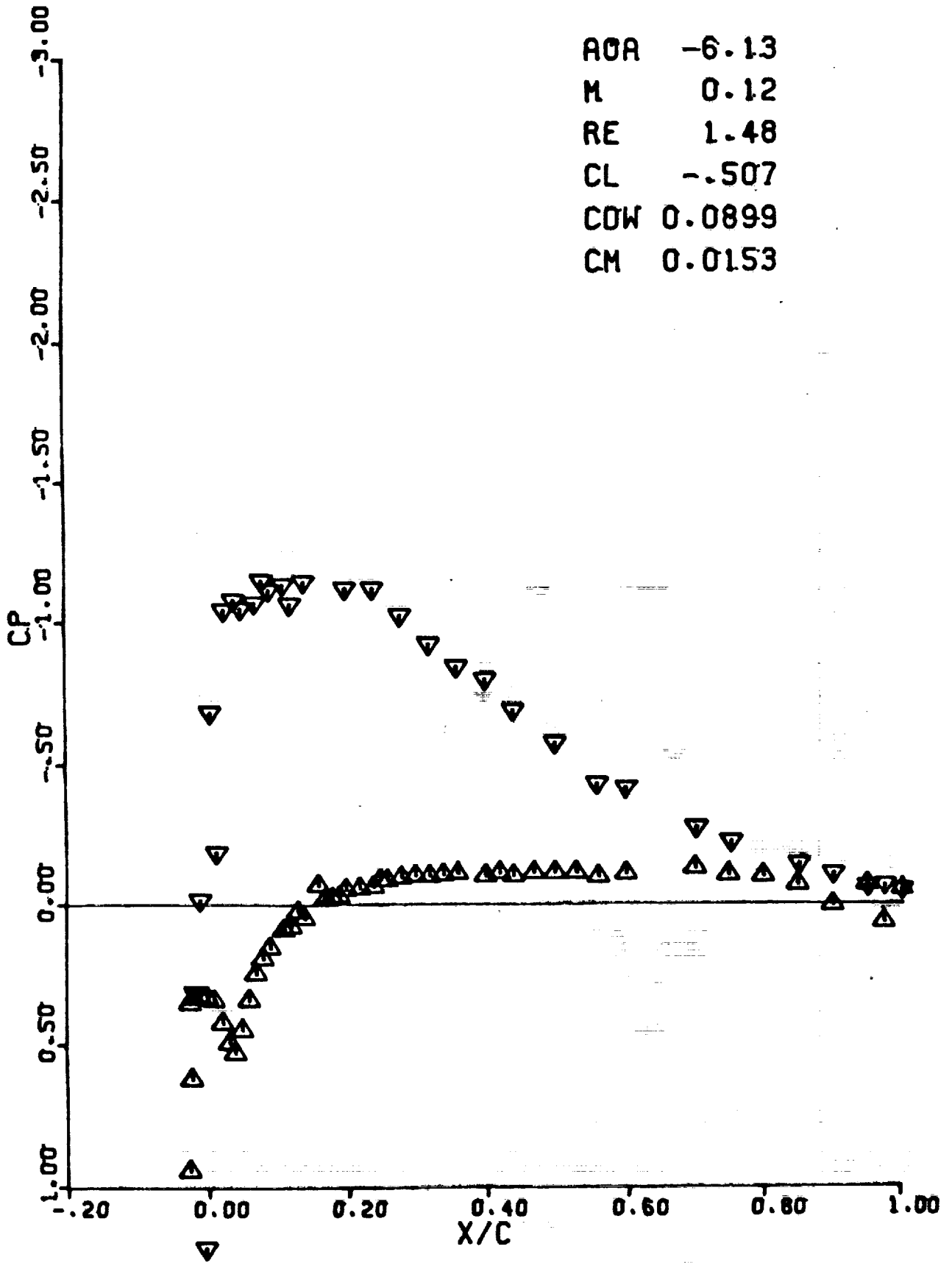
RUN 1124

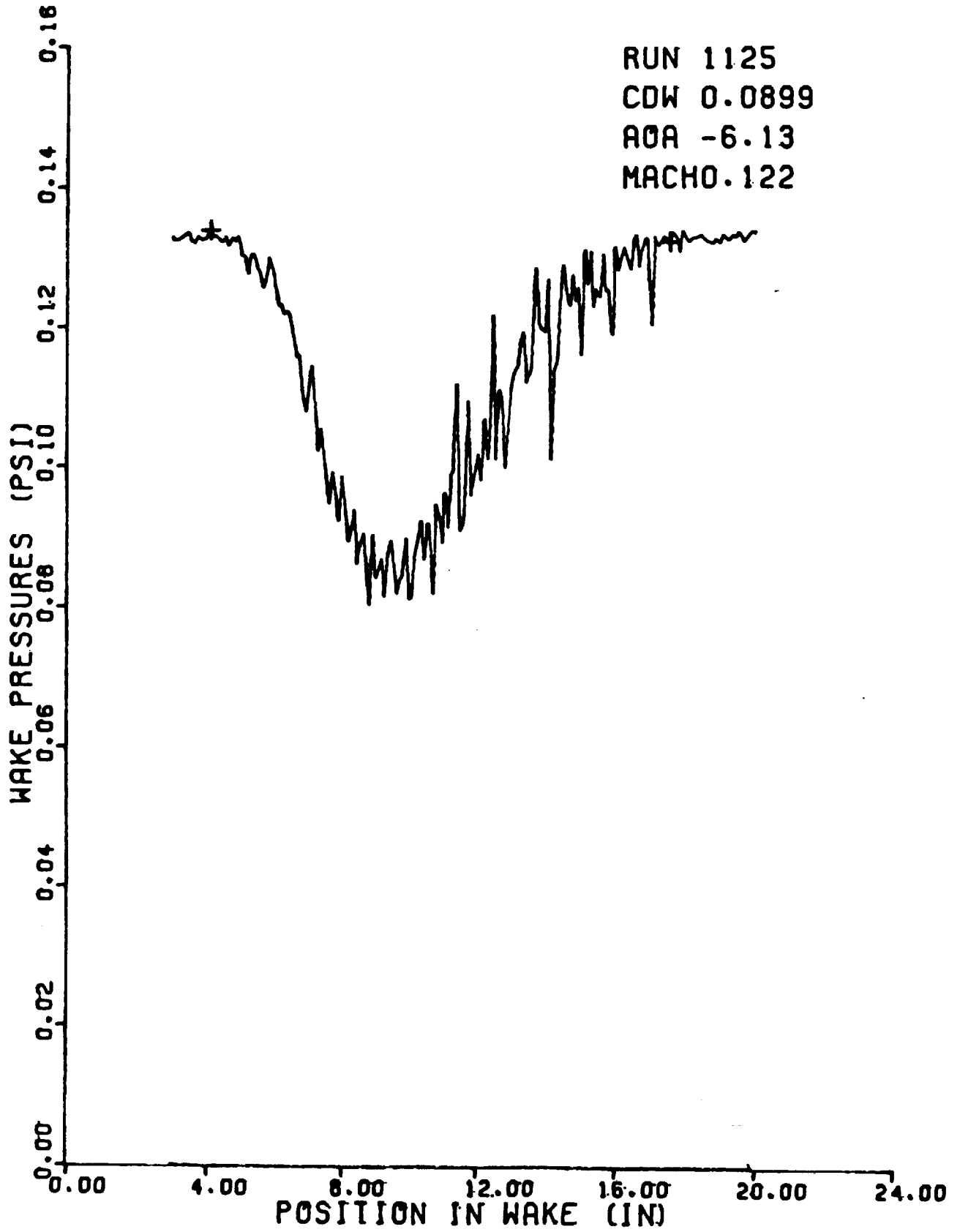
AOA -4.11
M 0.13
RE 1.50
CL -.359
CDW
CM -.0128



RUN 1.125

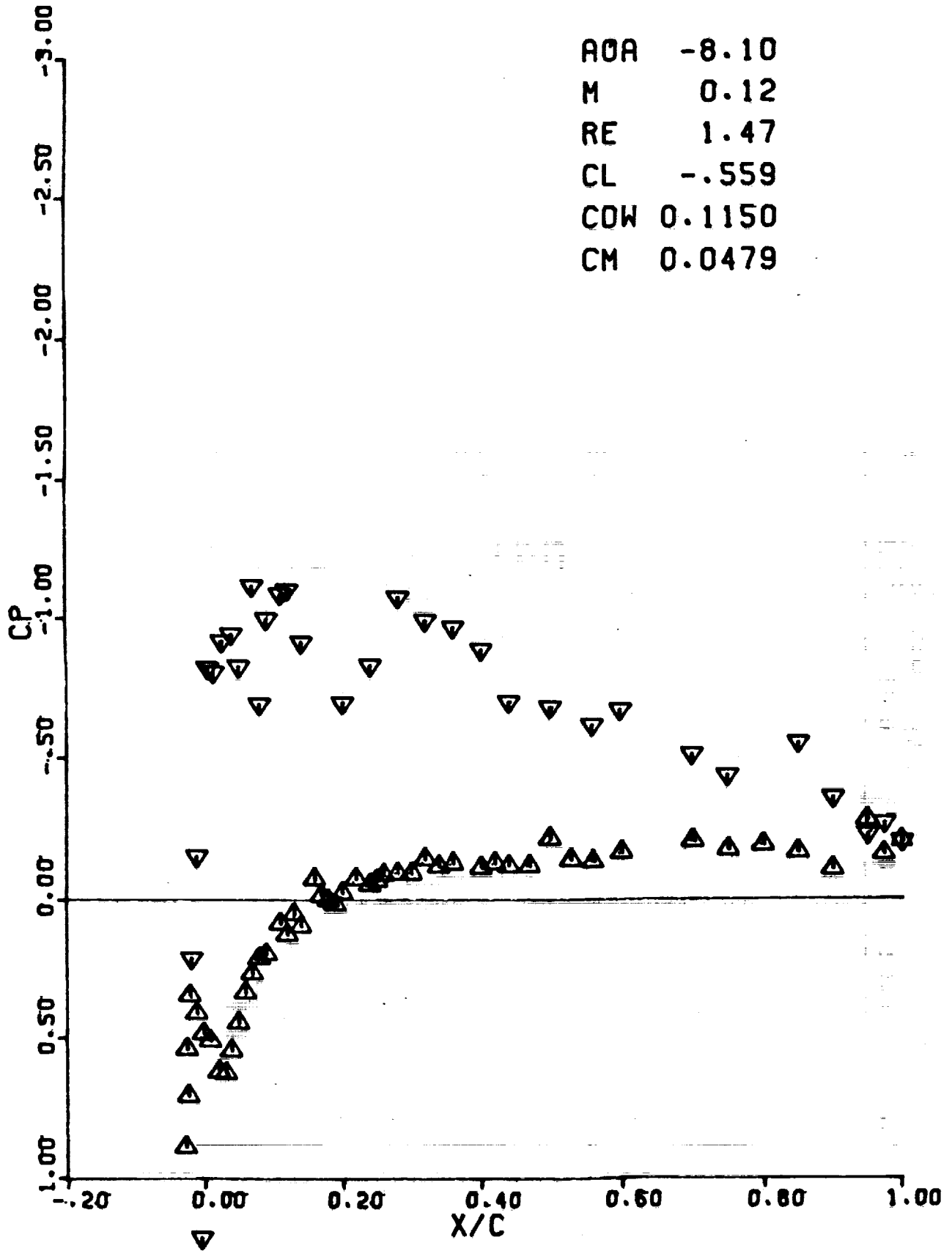
AOA -6.13
M 0.12
RE 1.48
CL -.507
COW 0.0899
CM 0.0153



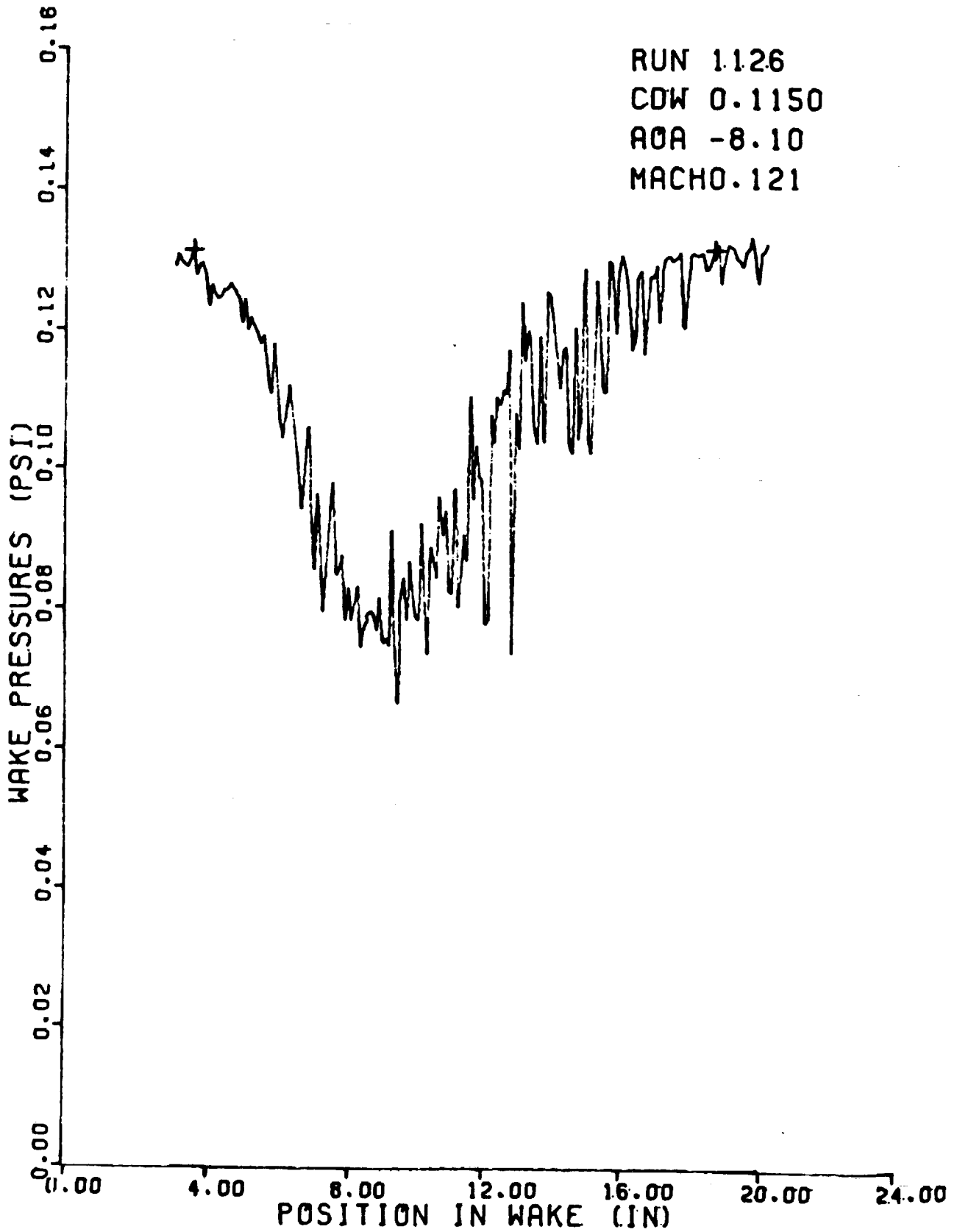


RUN 1126

AOA -8.10
M 0.12
RE 1.47
CL -.559
COW 0.1150
CM 0.0479

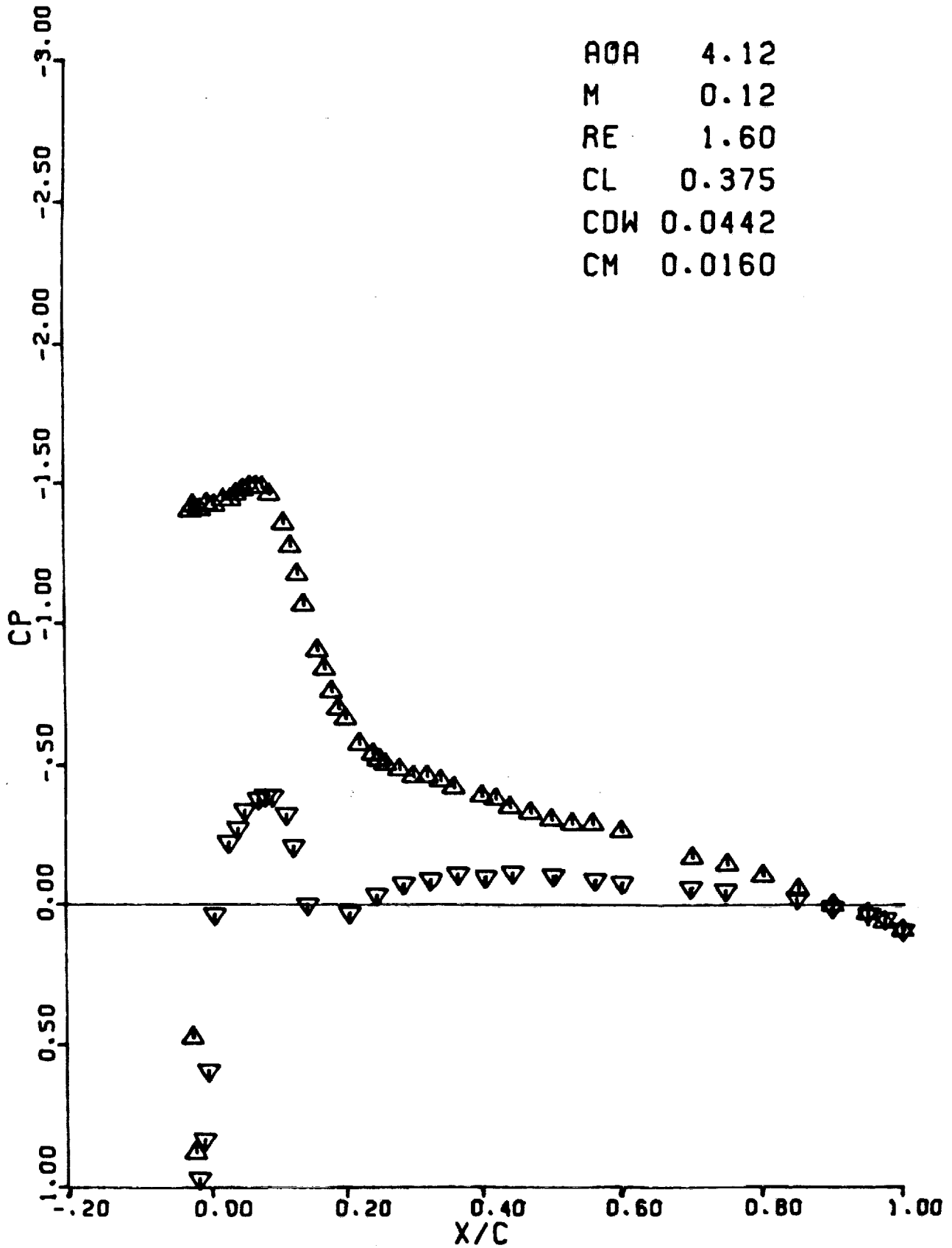


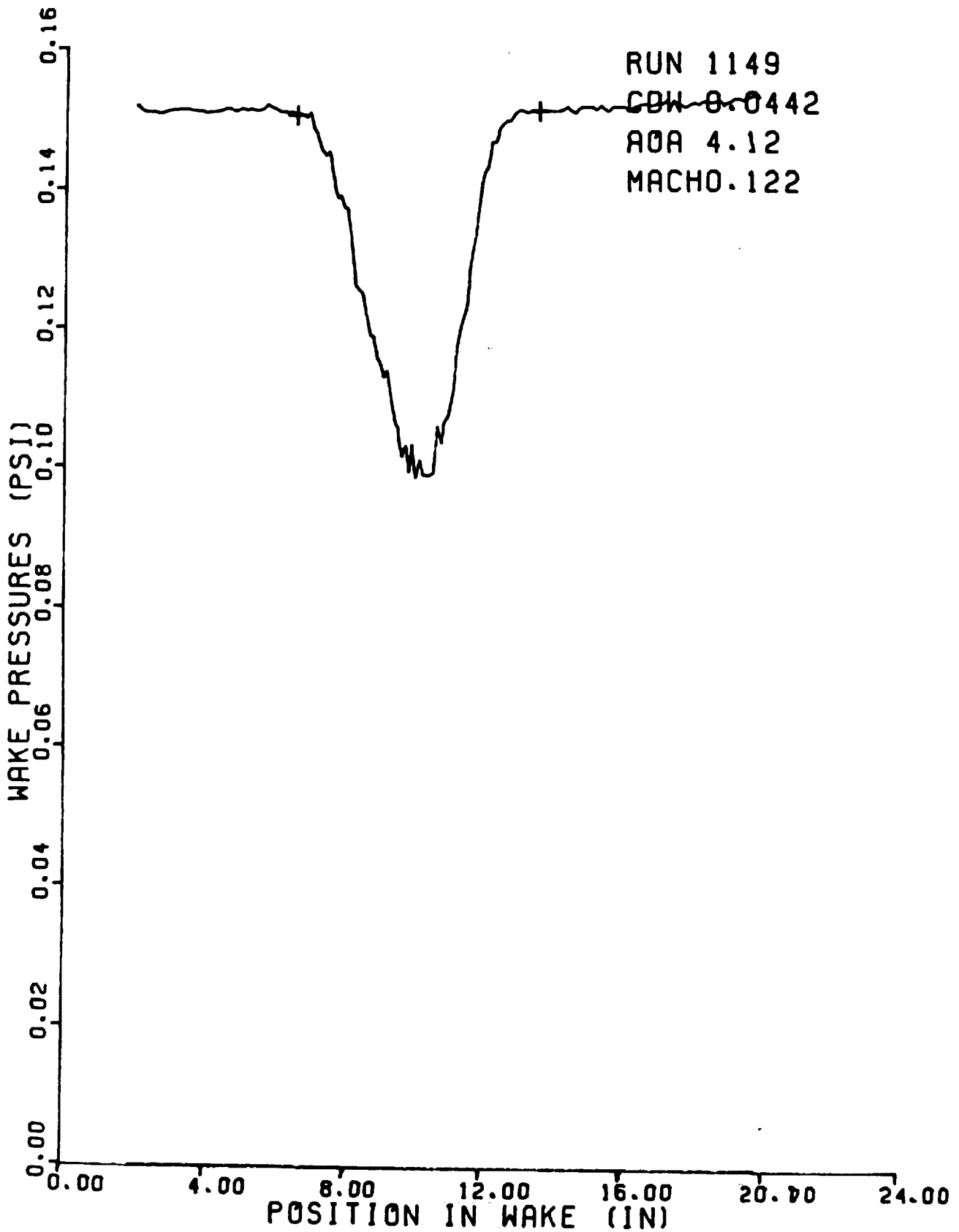
RUN 1.126
CDW 0.1150
AOA -8.10
MACHO.121



RUN 1149

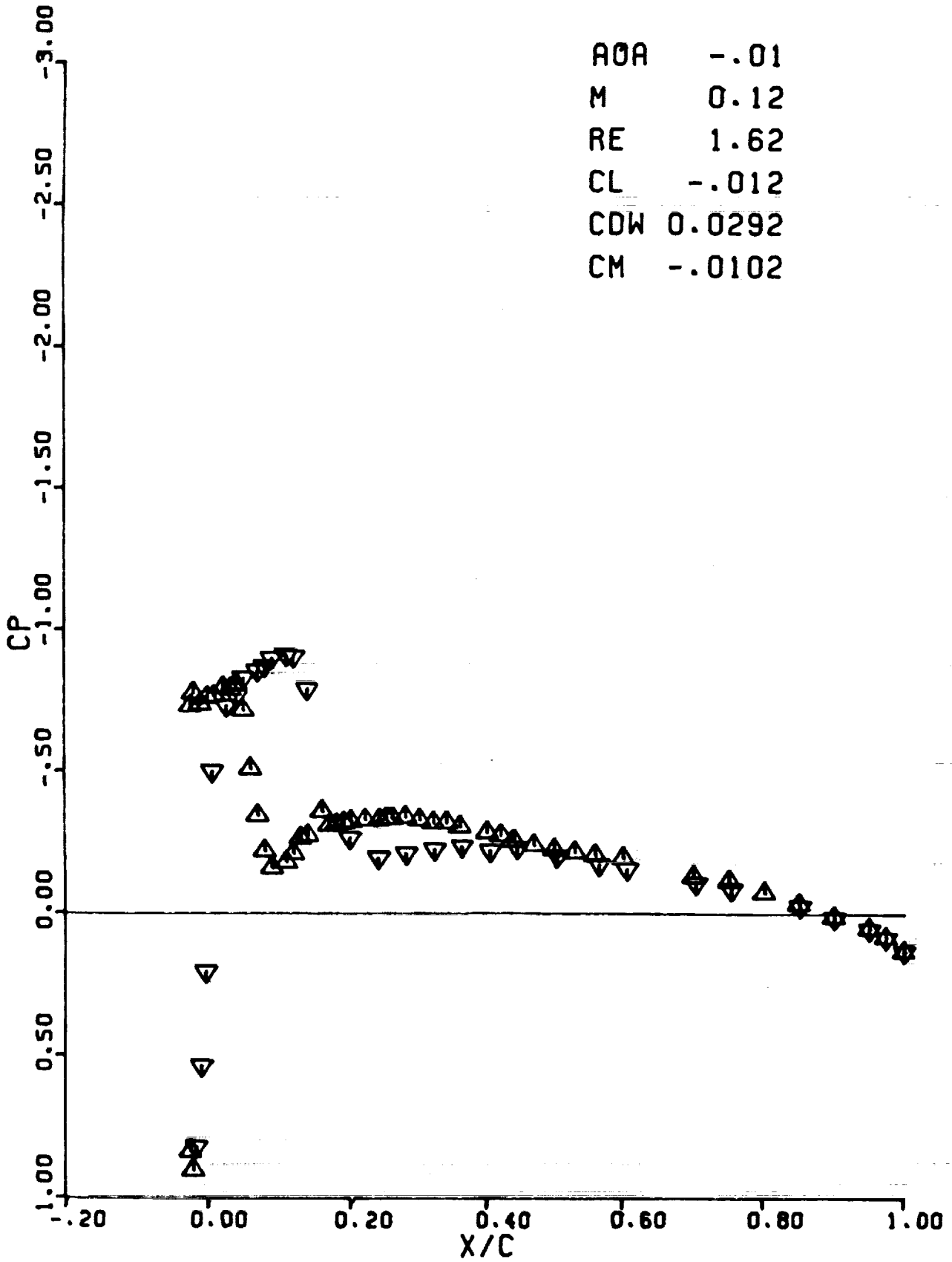
AOA 4.12
M 0.12
RE 1.60
CL 0.375
CDW 0.0442
CM 0.0160

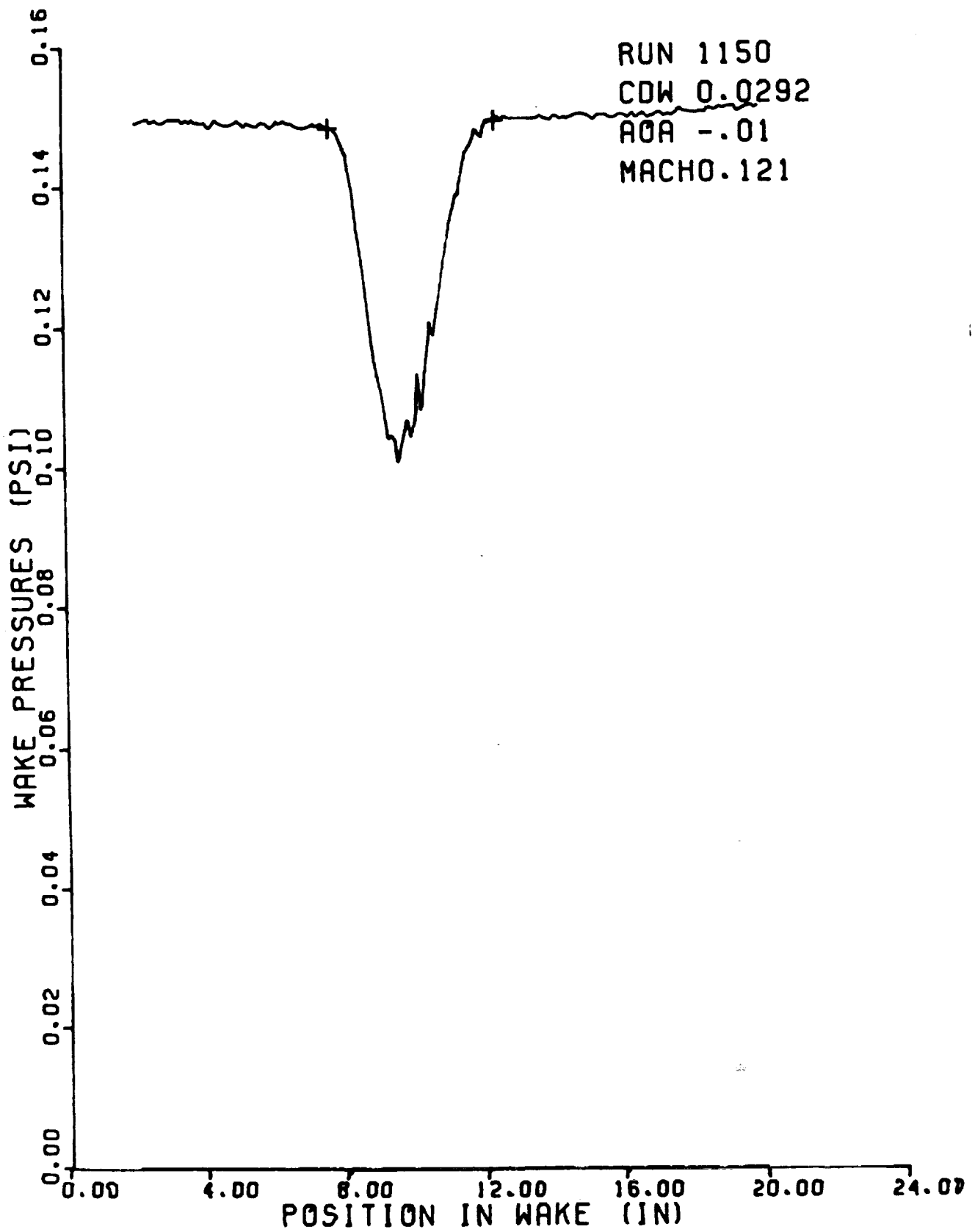




RUN 1150

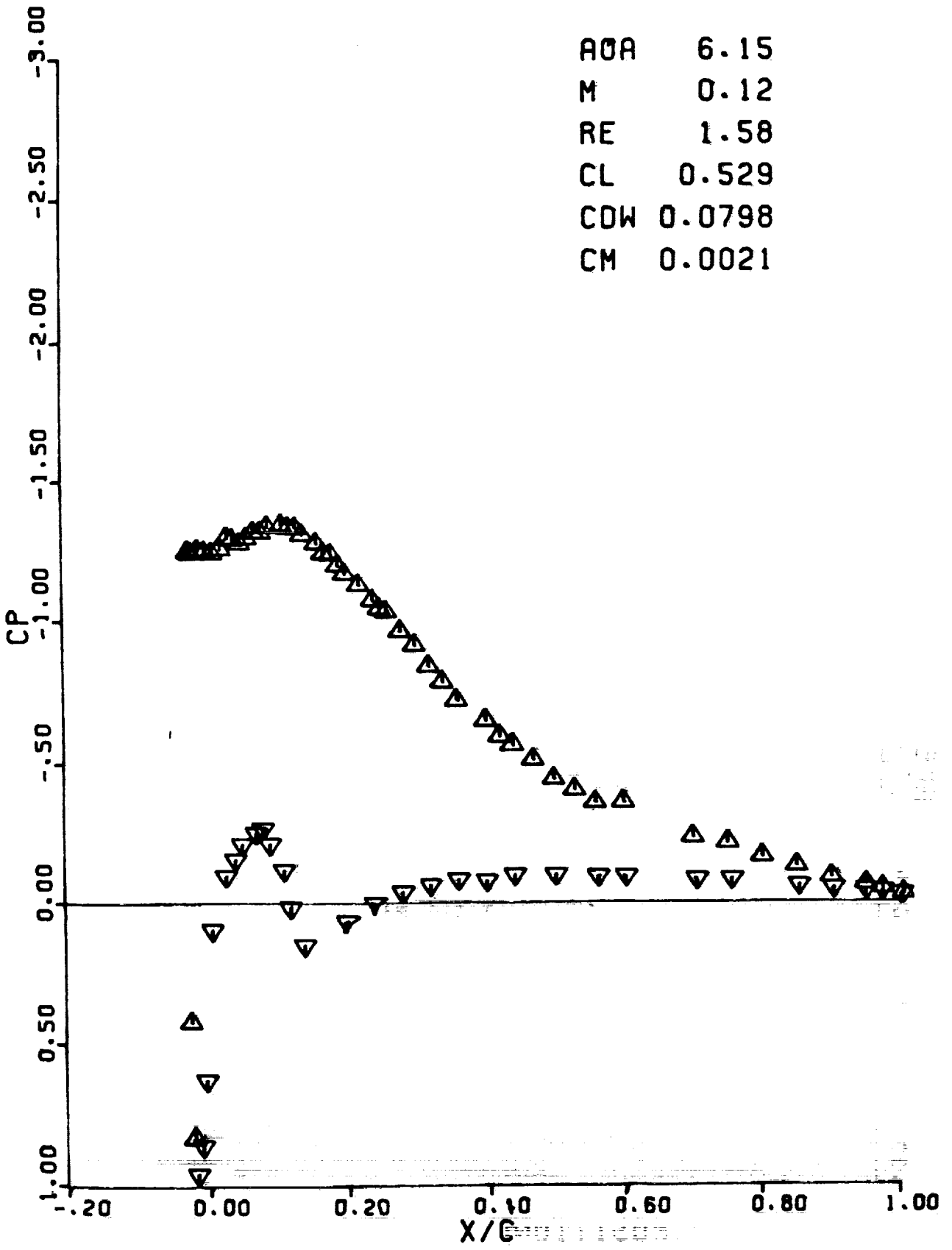
AOA -.01
M 0.12
RE 1.62
CL -.012
CDW 0.0292
CM -.0102

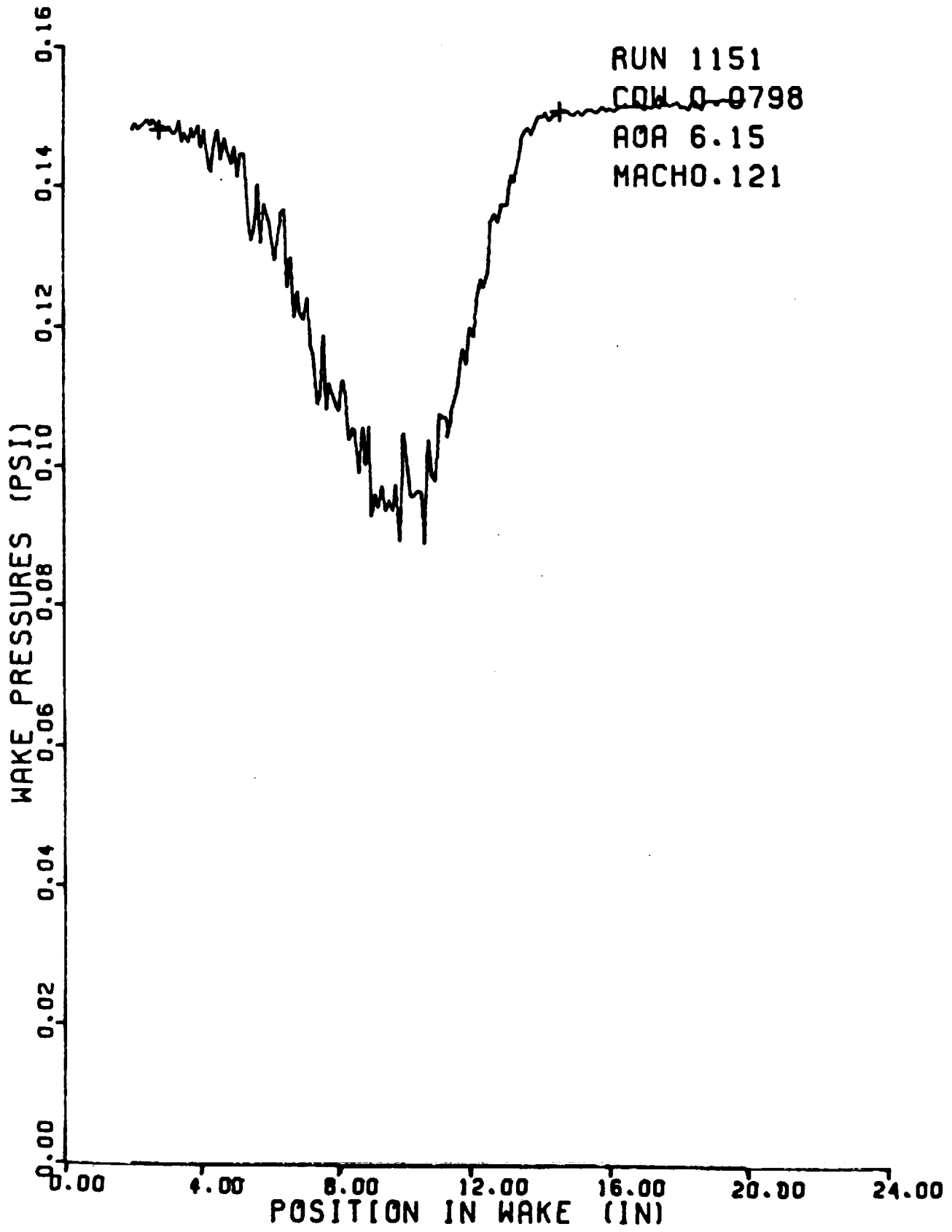




RUN 1151

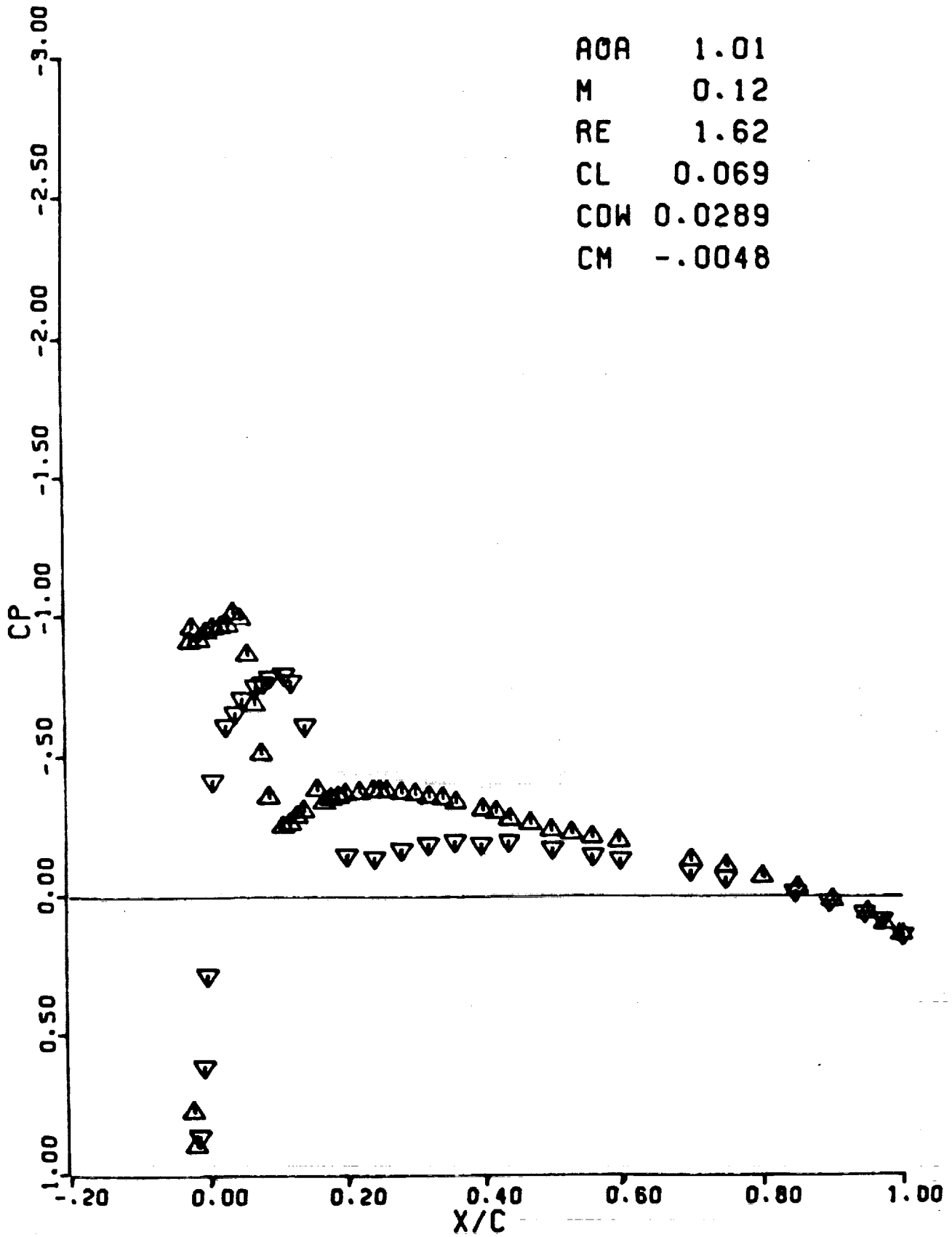
AOA 6.15
M 0.12
RE 1.58
CL 0.529
CDW 0.0798
CM 0.0021

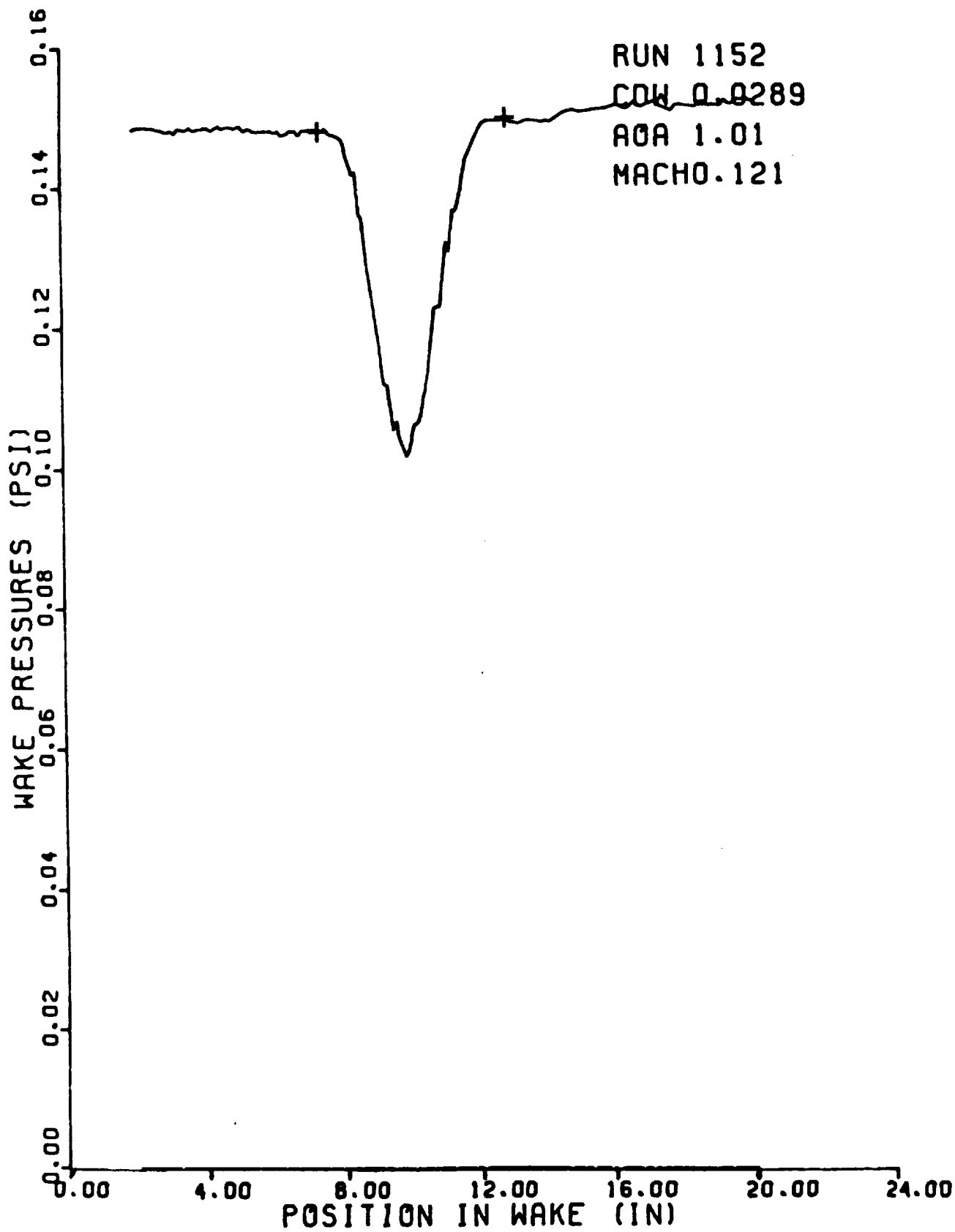




RUN 1152

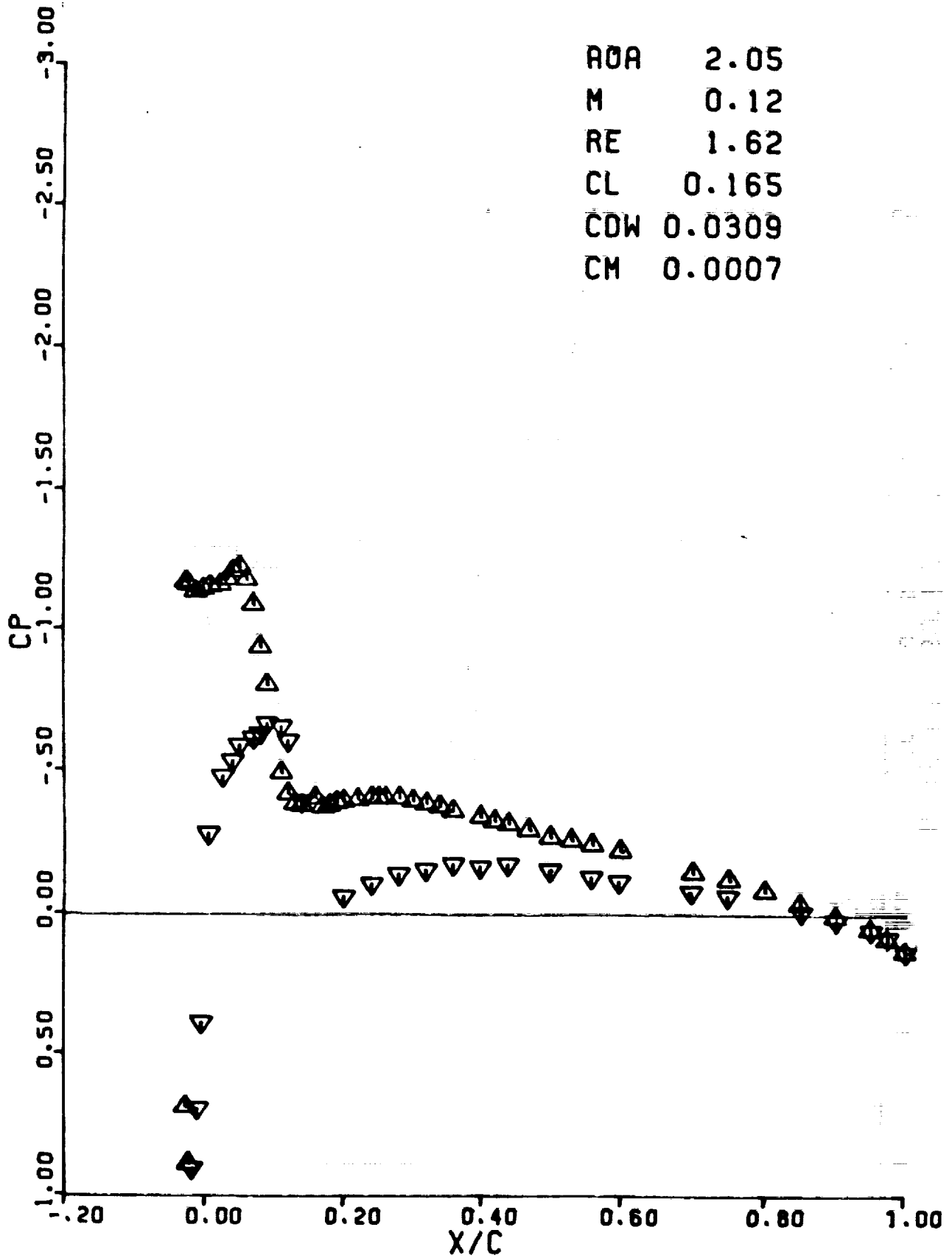
AOA 1.01
M 0.12
RE 1.62
CL 0.069
CDW 0.0289
CM -.0048

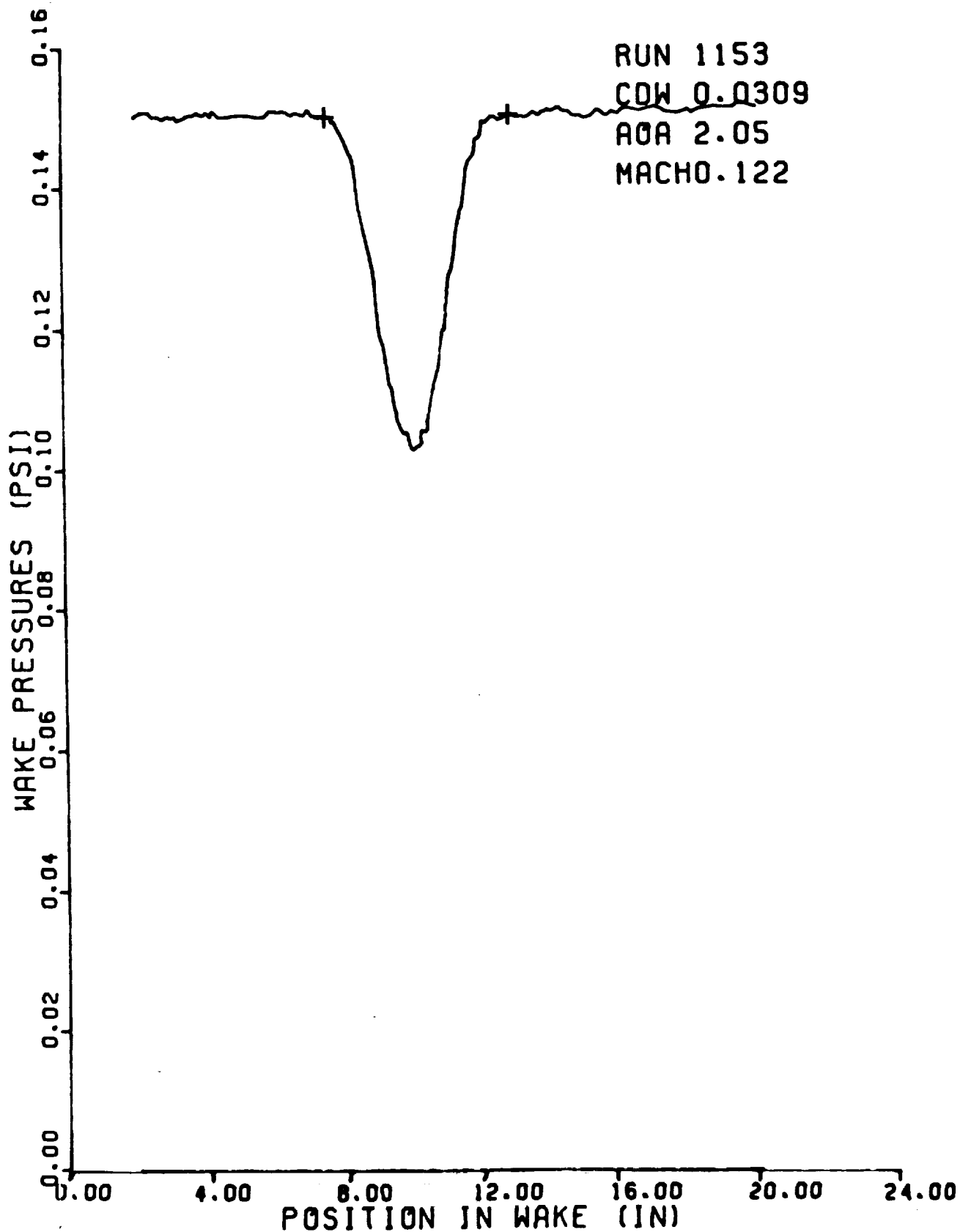




RUN 1153

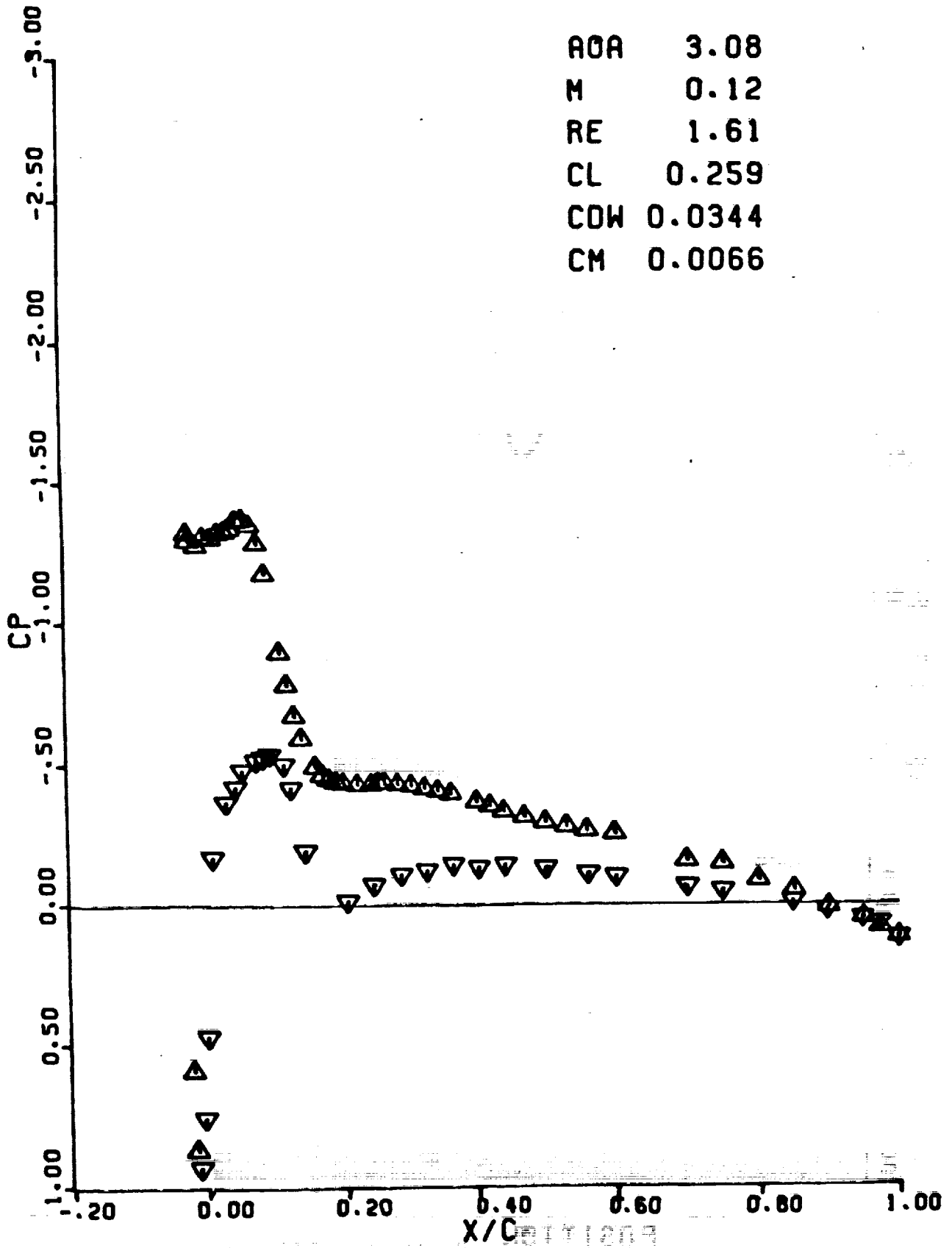
AOA 2.05
M 0.12
RE 1.62
CL 0.165
CDW 0.0309
CM 0.0007

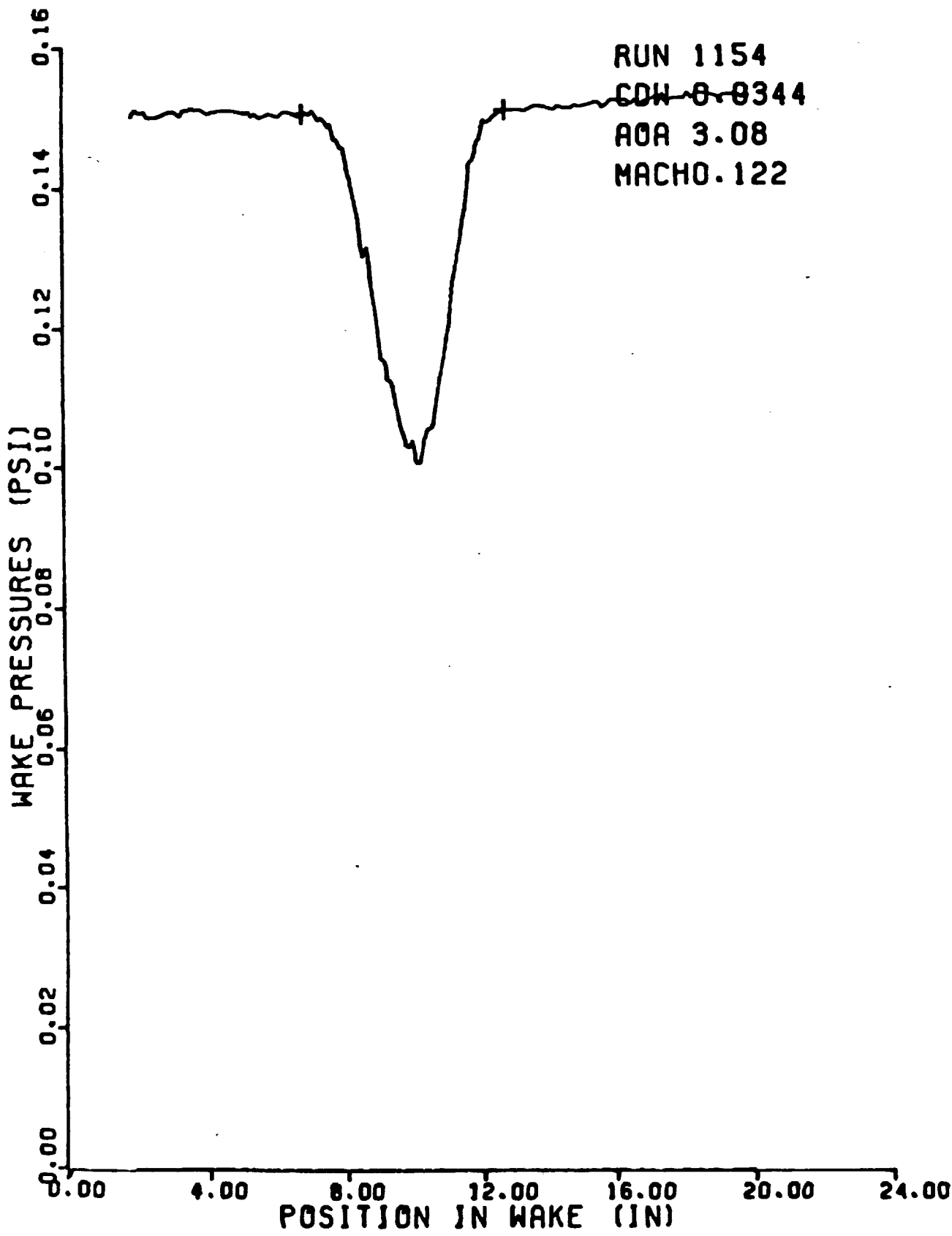




RUN 1.154.

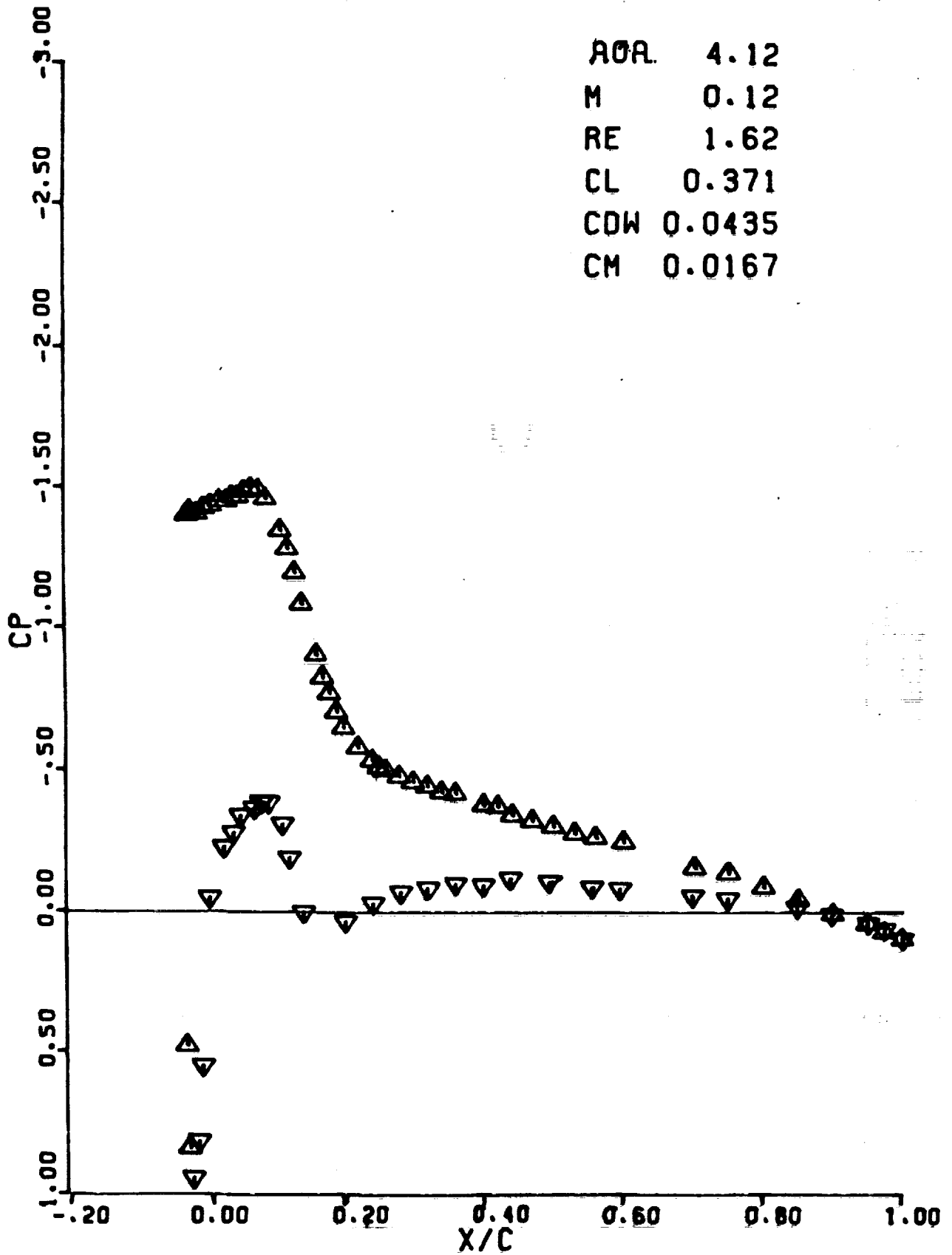
AOA 3.08
M 0.12
RE 1.61
CL 0.259
CDW 0.0344
CM 0.0066

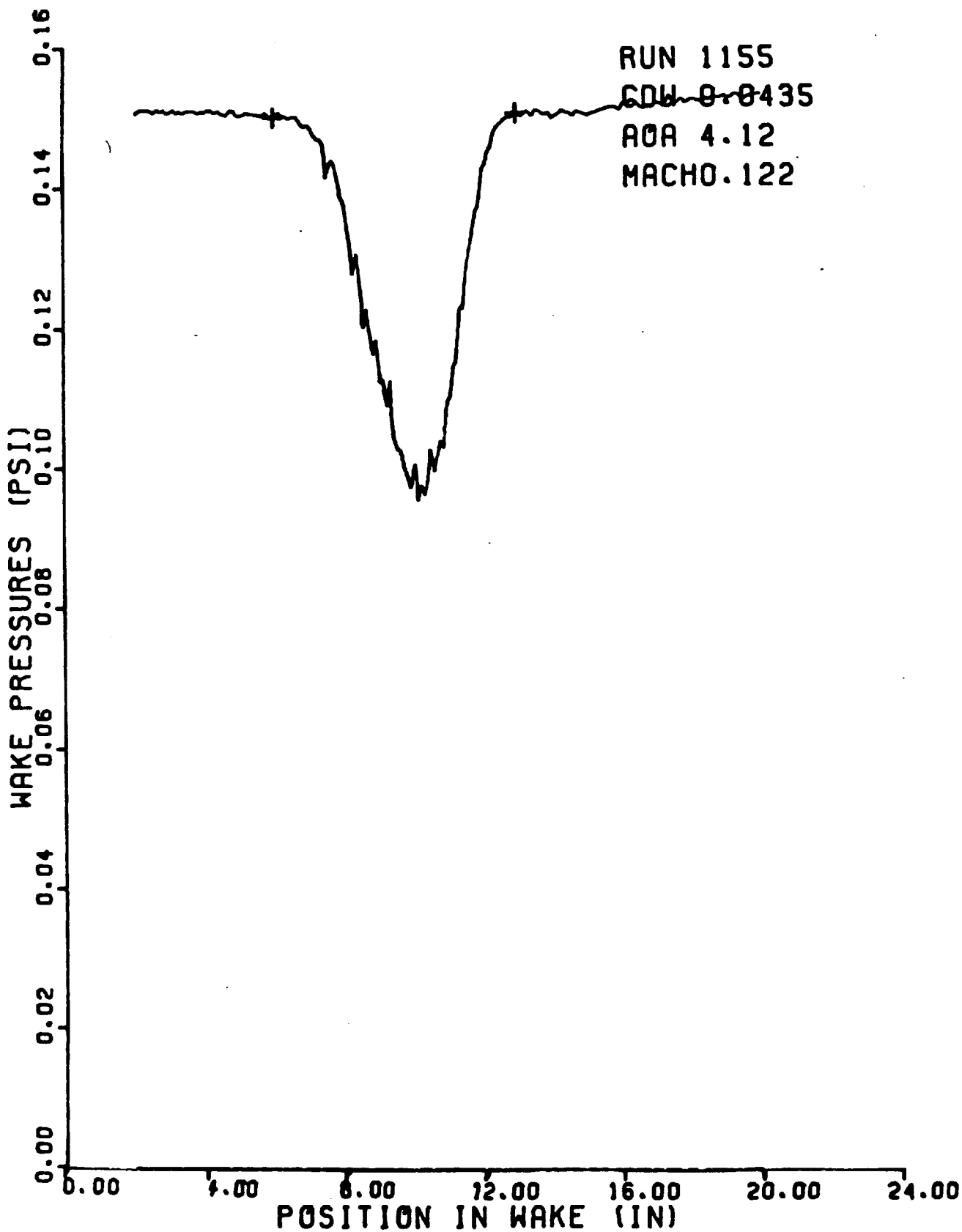




RUN 1155

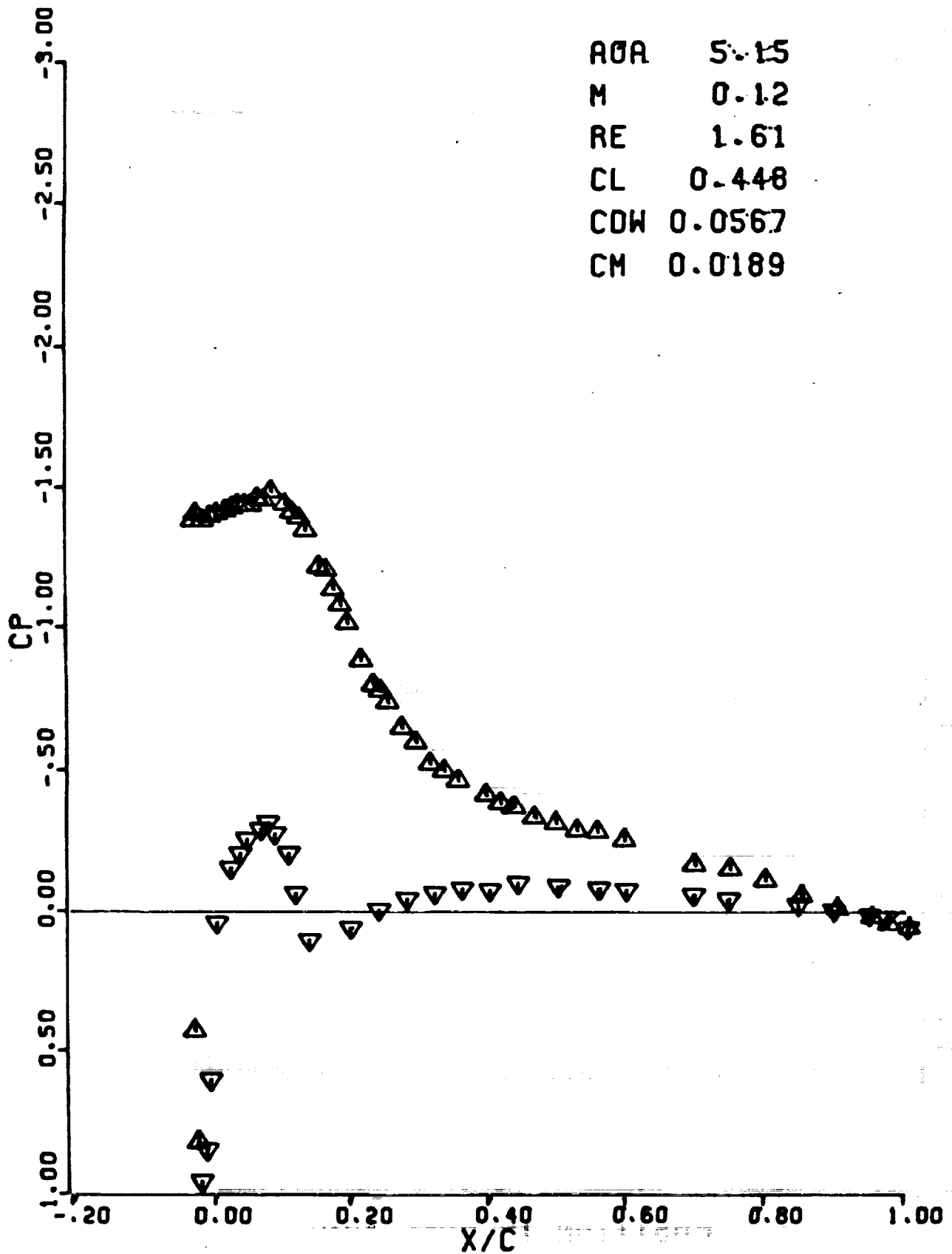
AOA. 4.12
M 0.12
RE 1.62
CL 0.371
CDW 0.0435
CM 0.0167

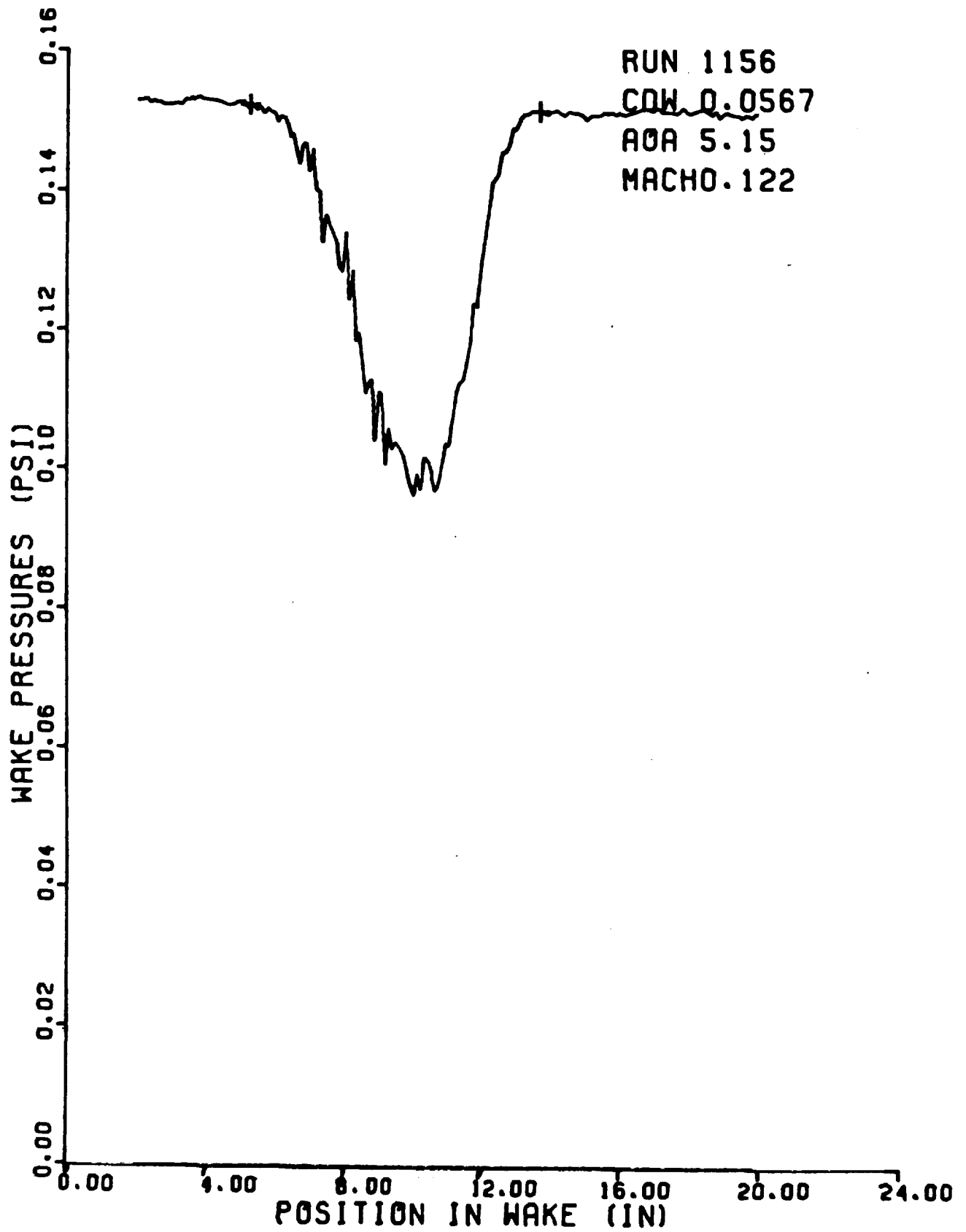




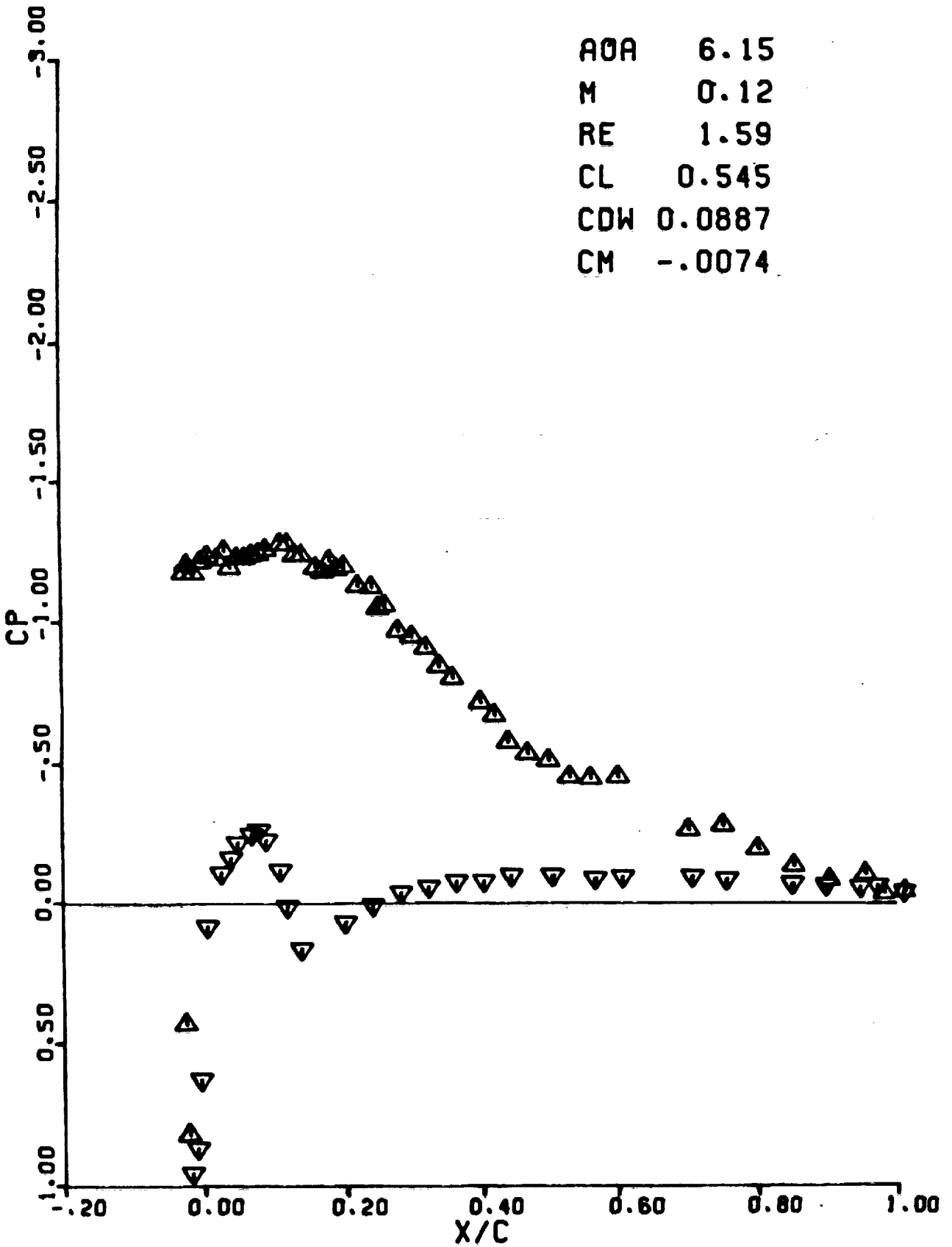
RUN 1156

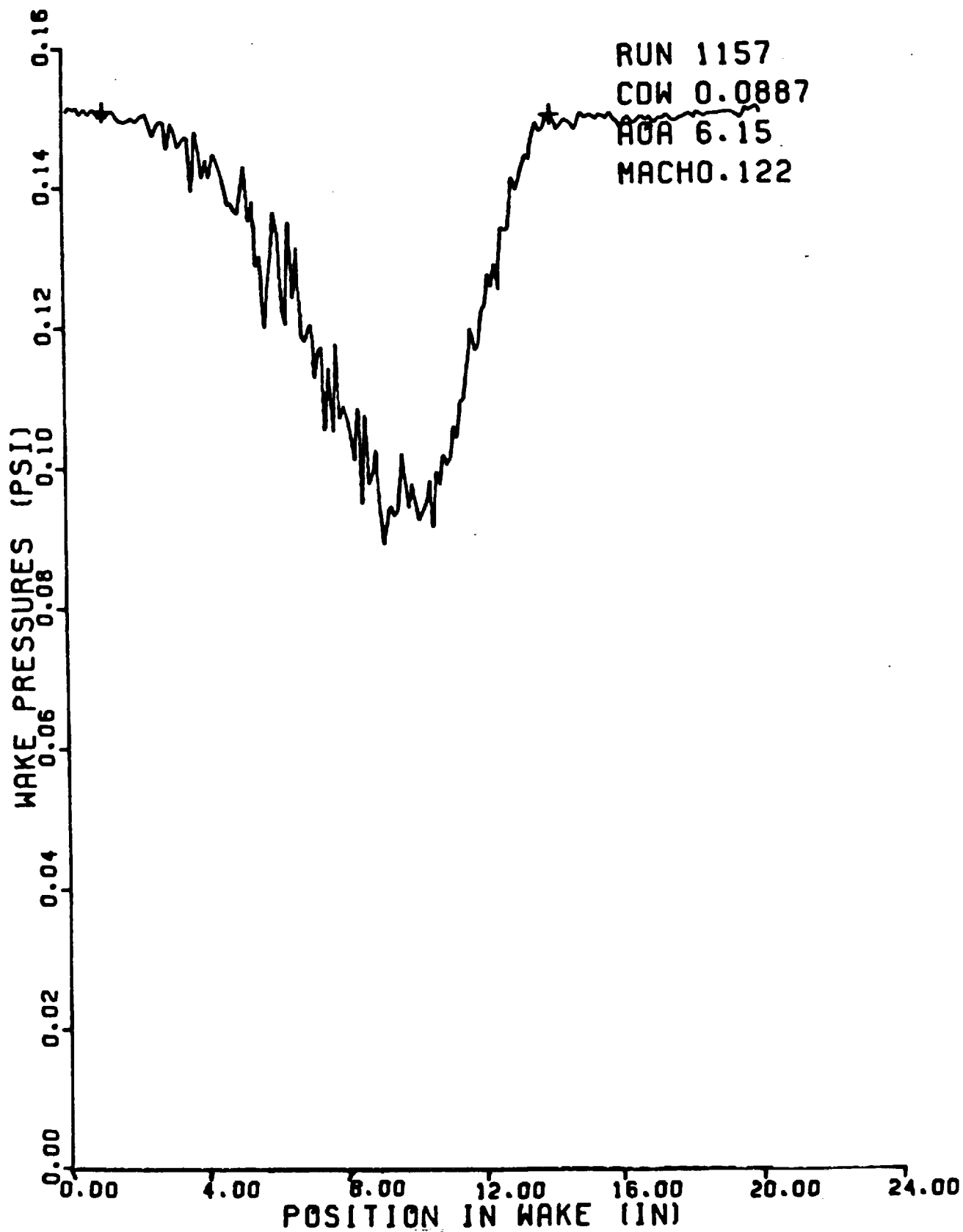
AOA 5.15
M 0.12
RE 1.61
CL 0.448
CDW 0.0567
CM 0.0189





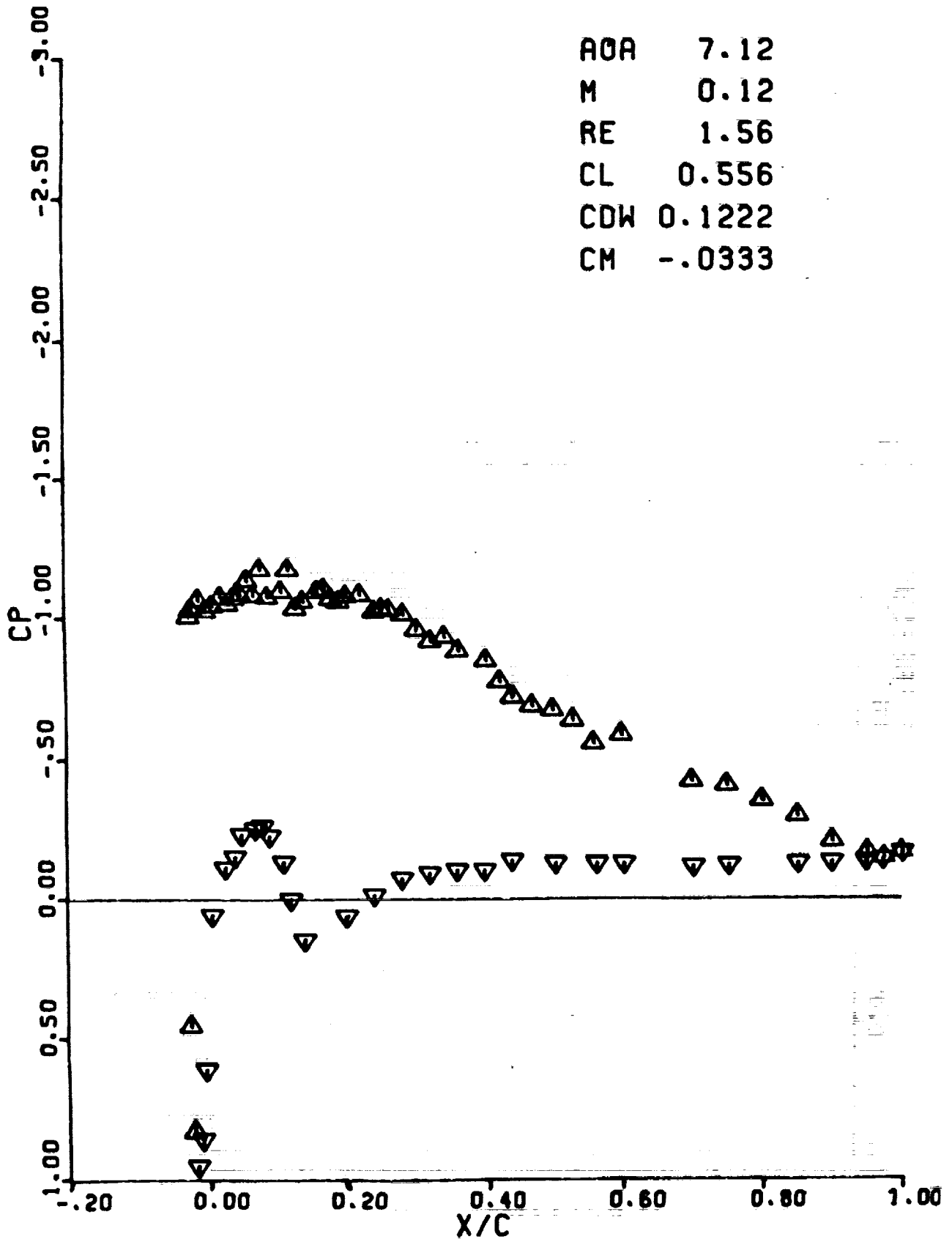
RUN 1157

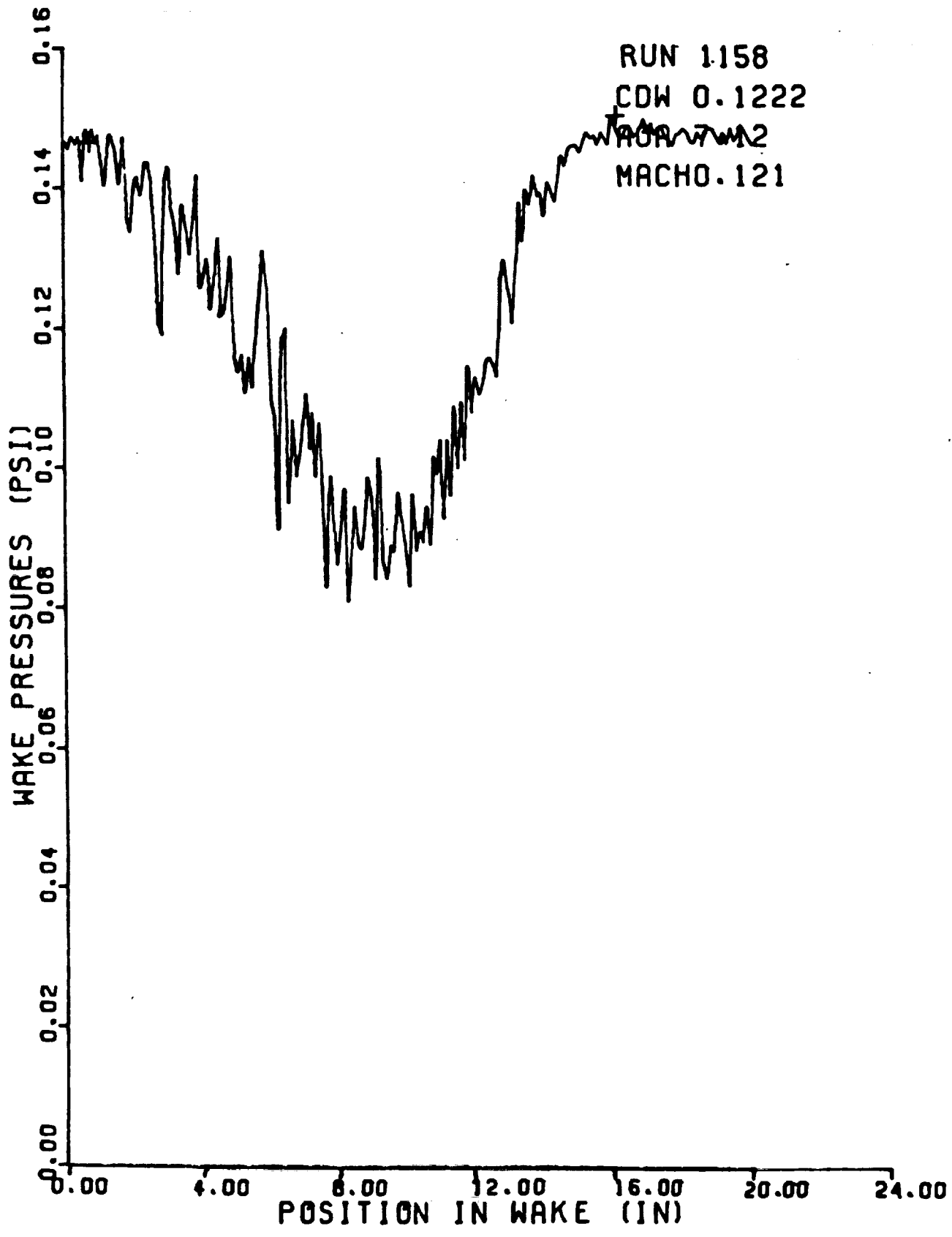




RUN 1158

AOA 7.12
M 0.12
RE 1.56
CL 0.556
CDW 0.1222
CM -.0333

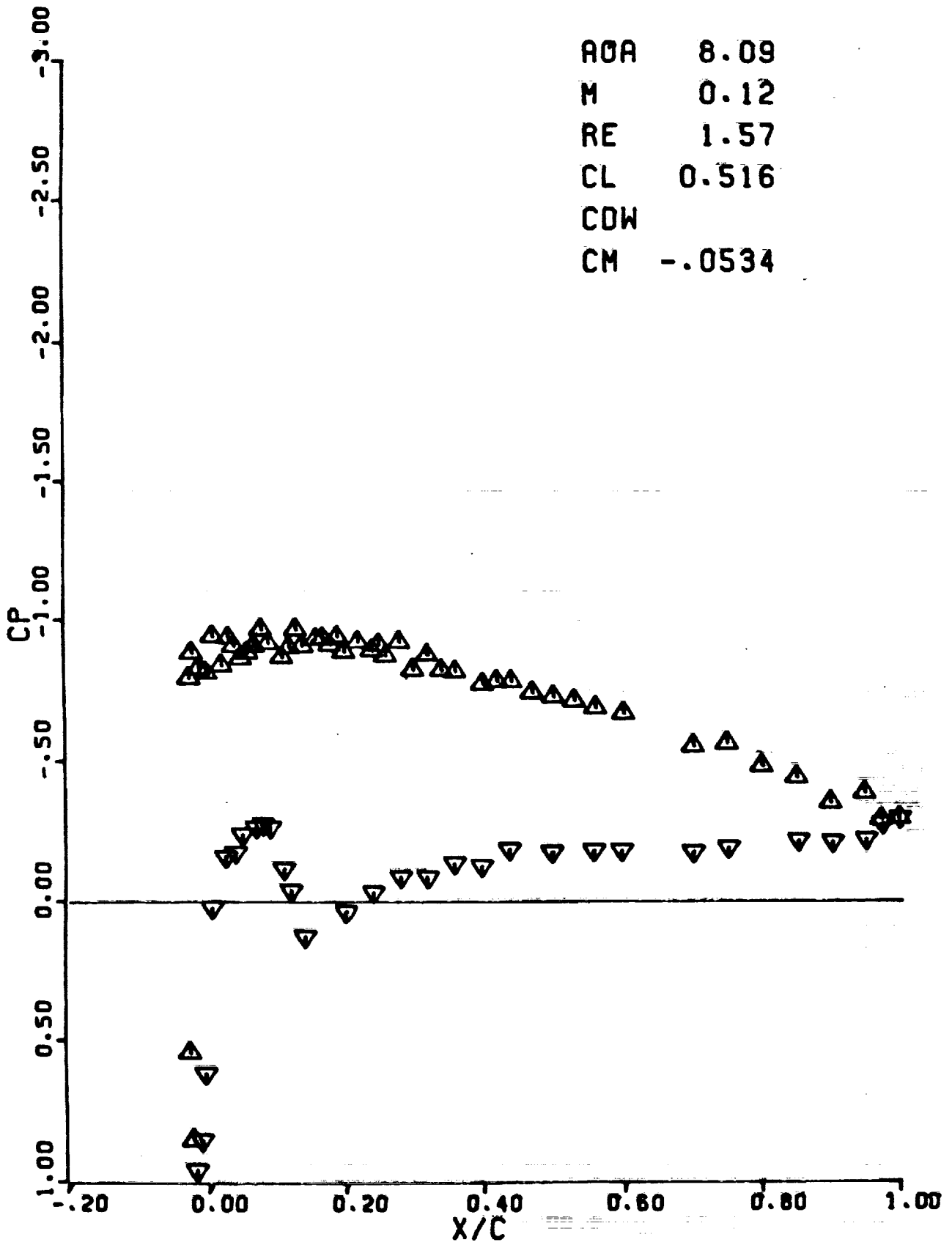




RUN 1158
CDW 0.1222
AOR 7.12
MACHO.121

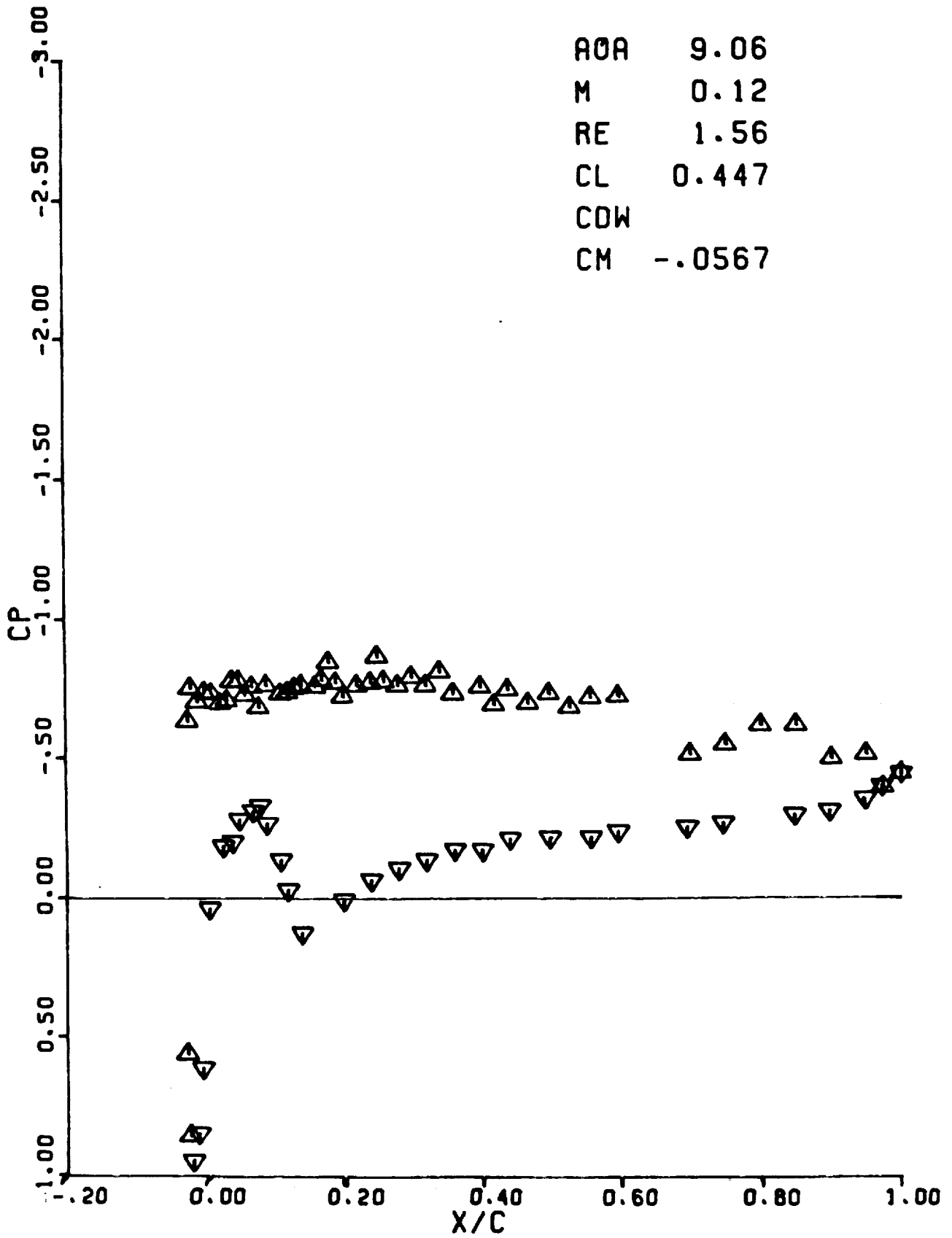
RUN 1159

AOA 8.09
M 0.12
RE 1.57
CL 0.516
CDW
CM -.0534



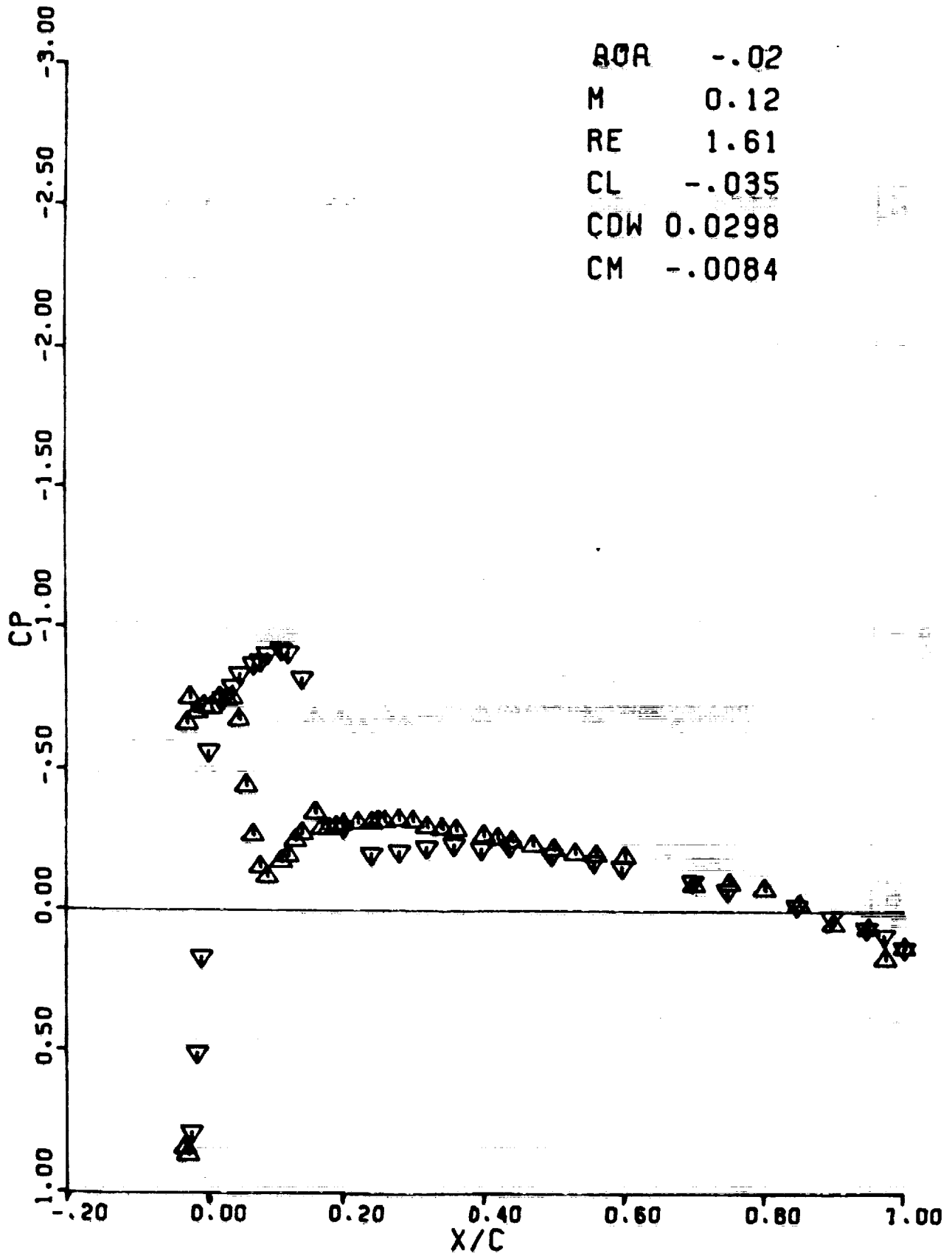
RUN 1-160

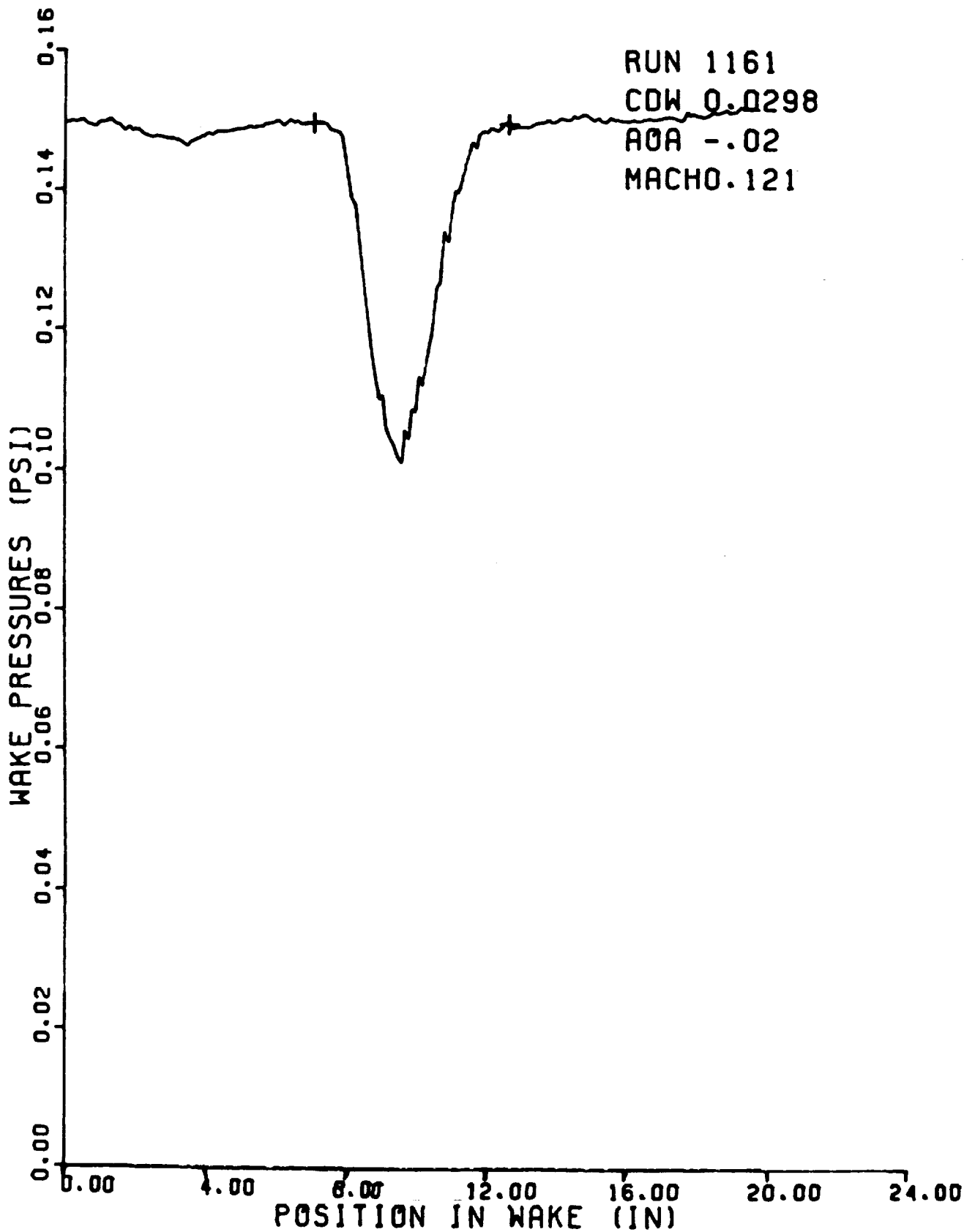
AOA 9.06
M 0.12
RE 1.56
CL 0.447
CDW
CM -.0567



RUN 1161

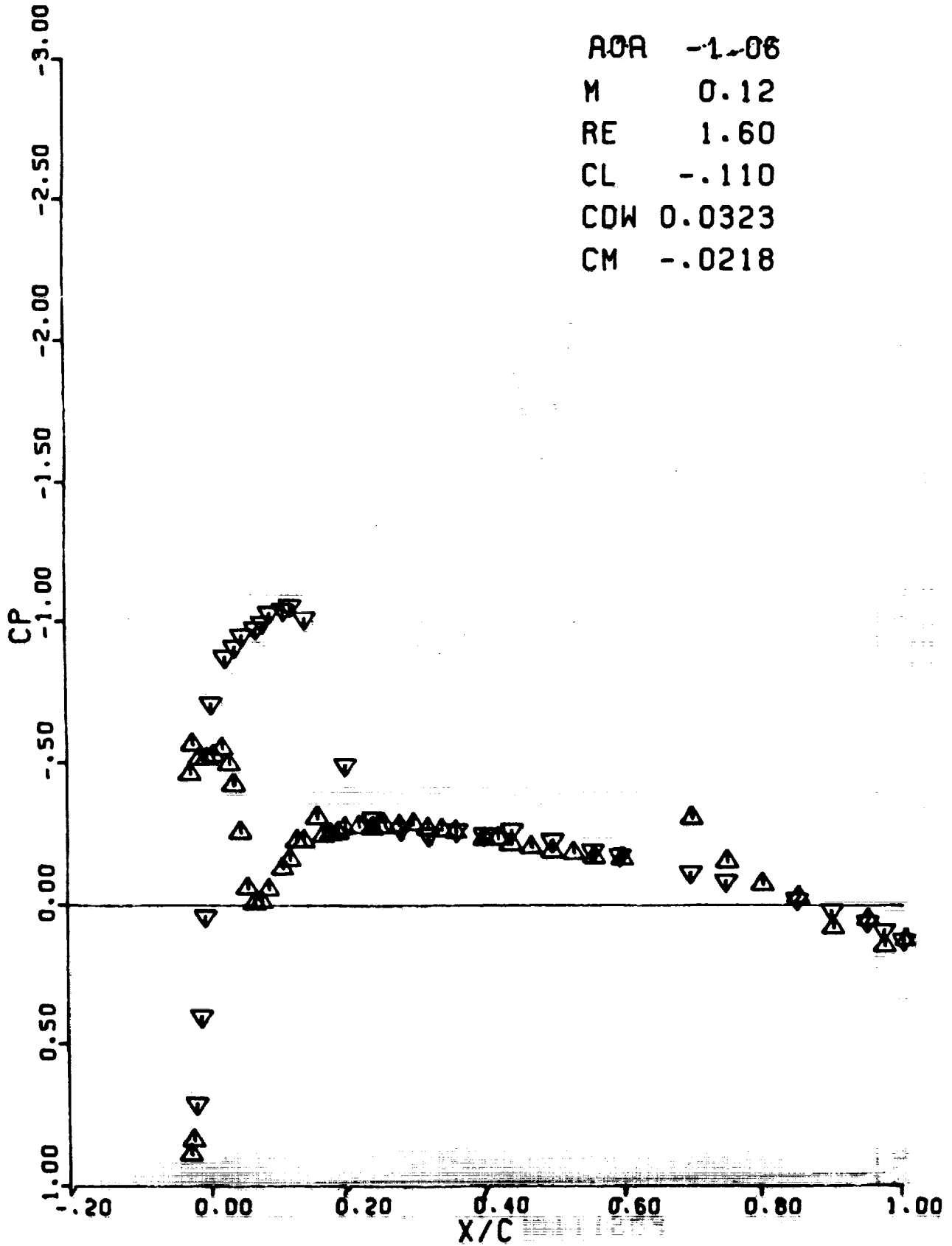
AOA -.02
M 0.12
RE 1.61
CL -.035
CDW 0.0298
CM -.0084

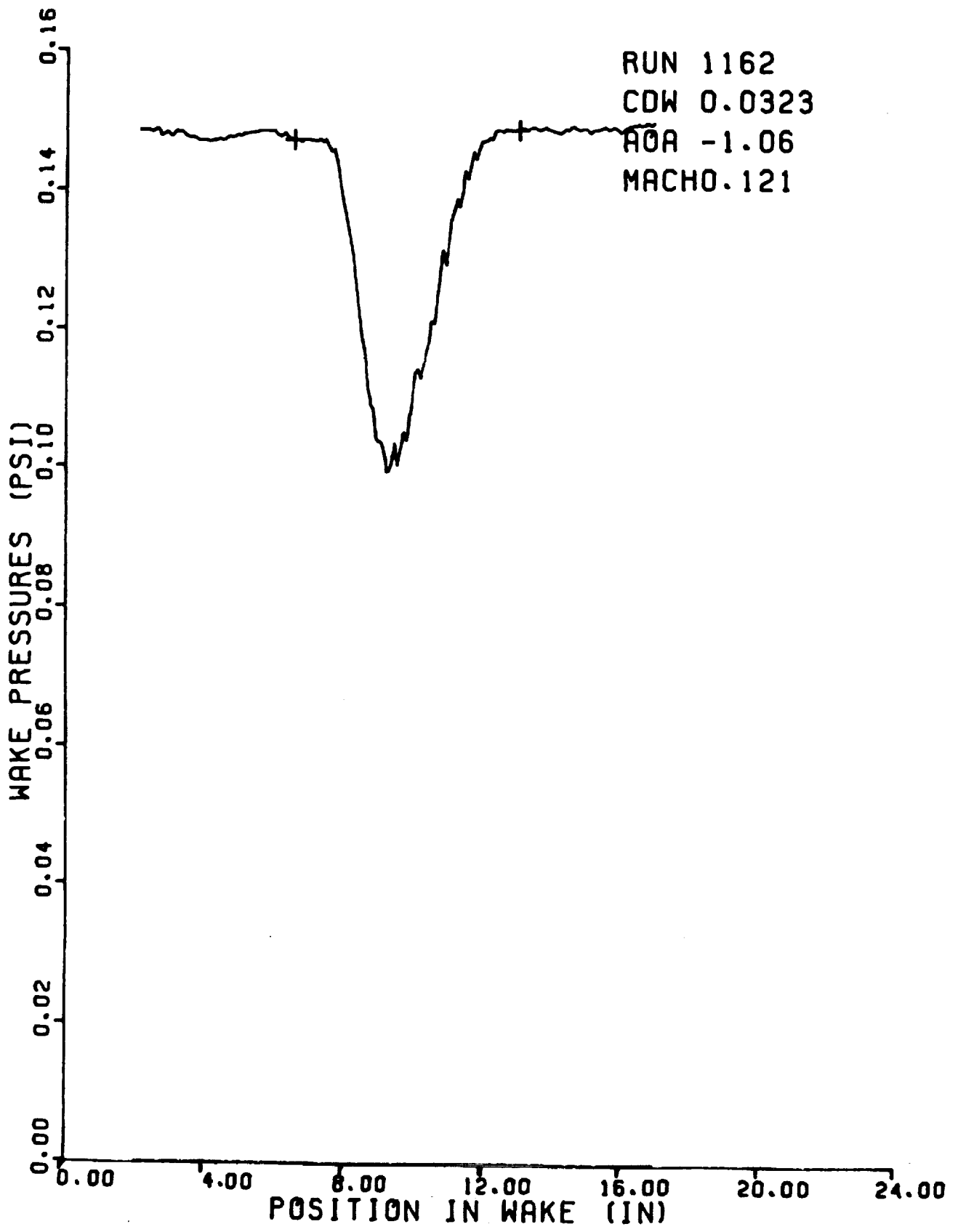




RUN 1162.

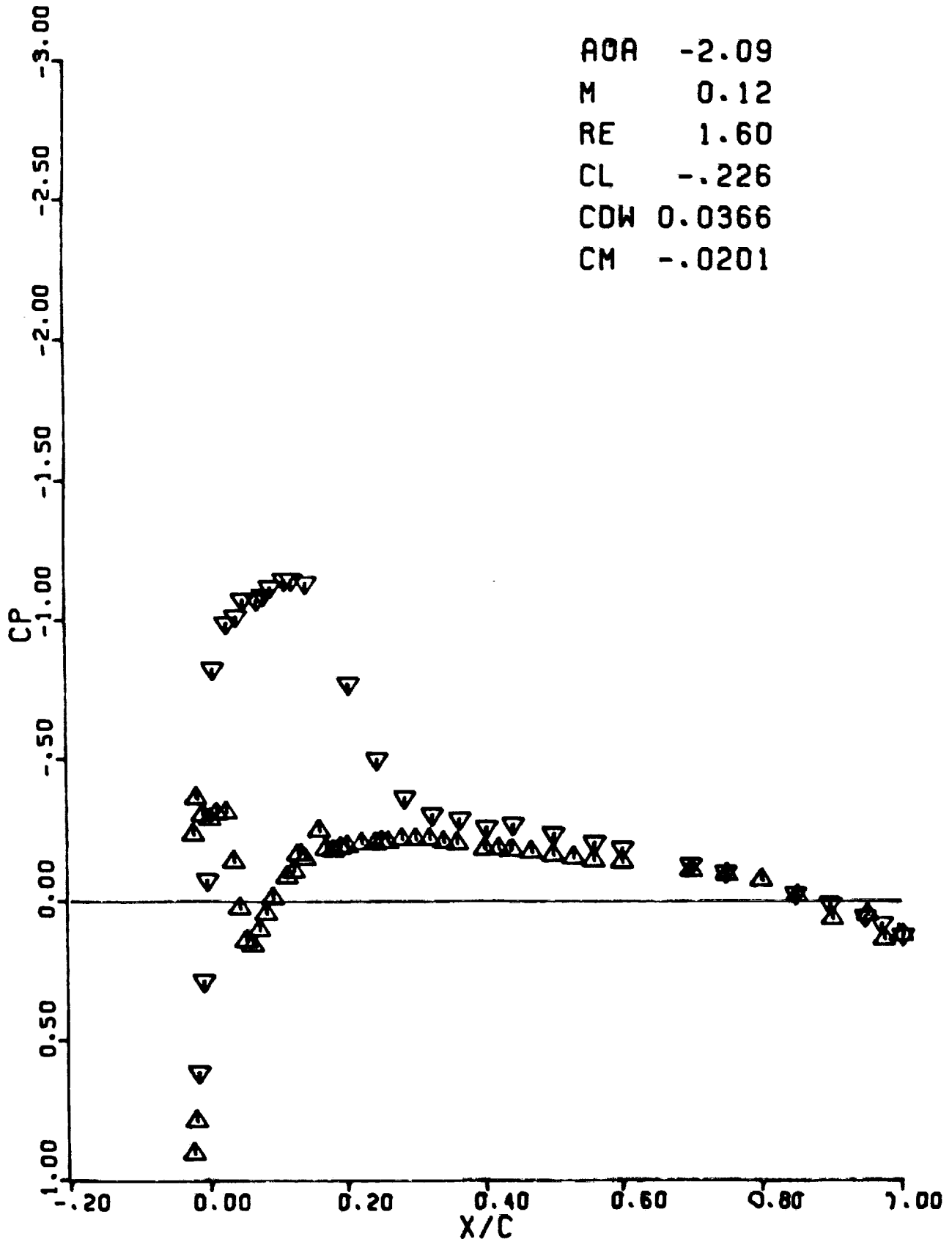
AOR -1.06
M 0.12
RE 1.60
CL -.110
CDW 0.0323
CM -.0218

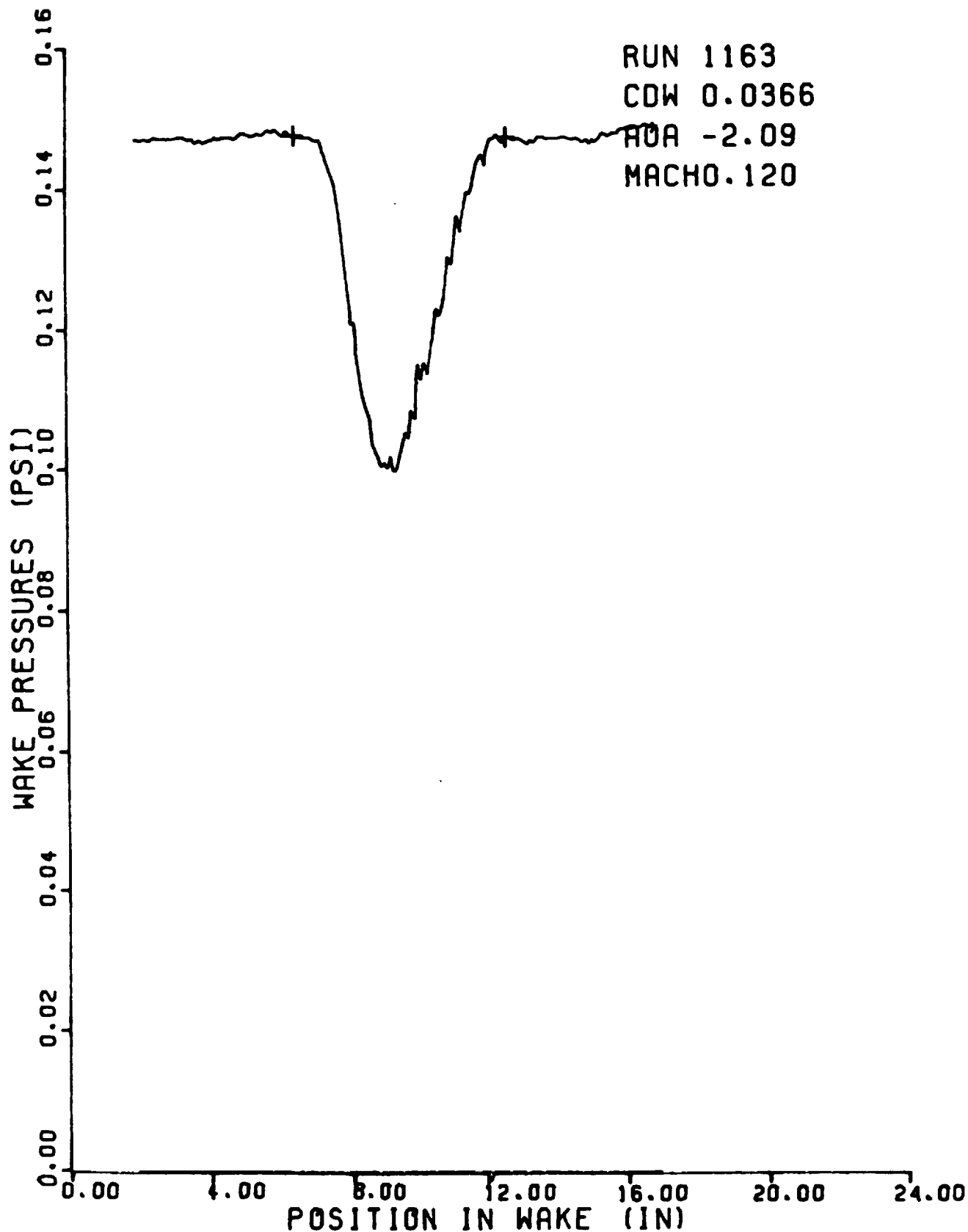




RUN 1163

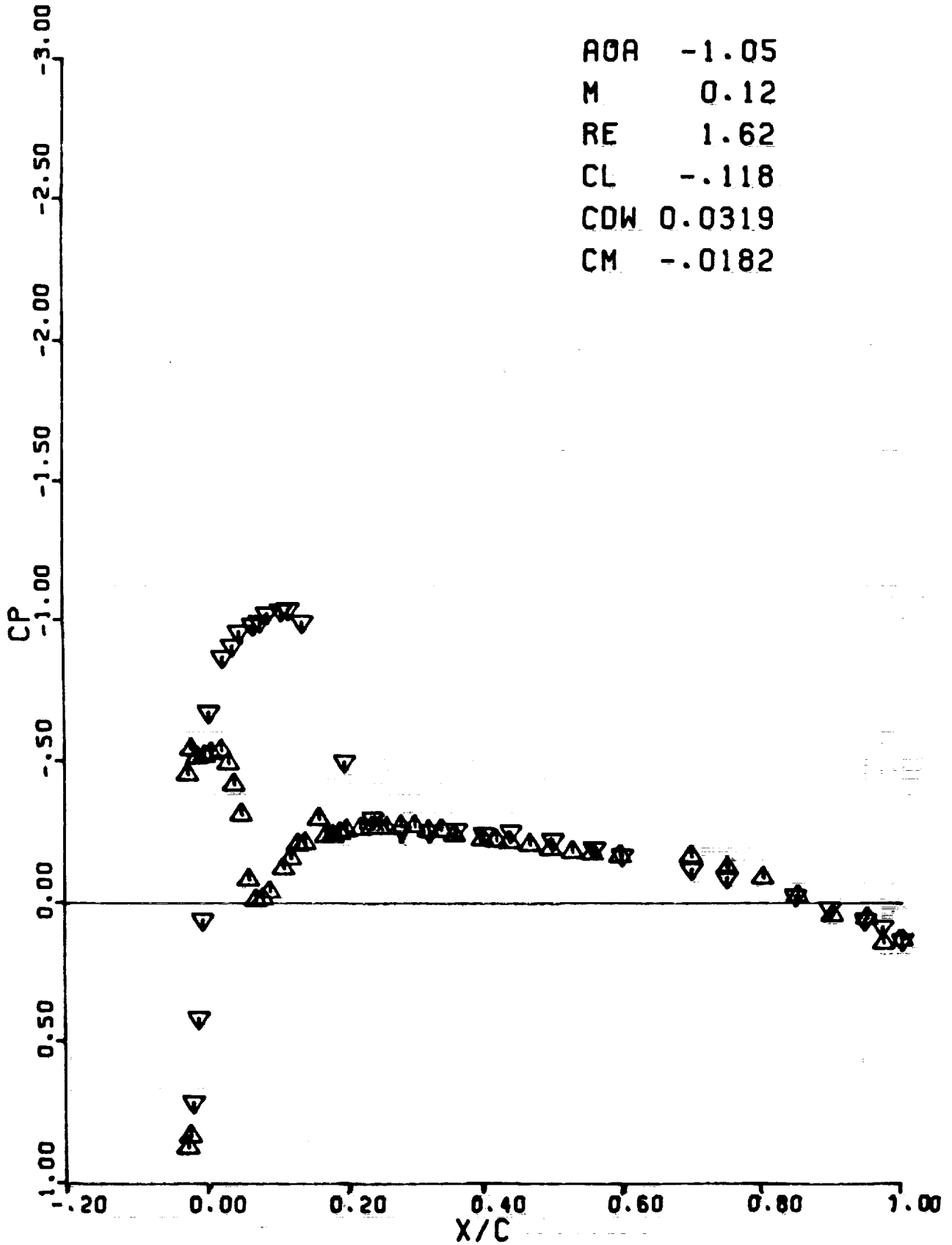
AOA -2.09
M 0.12
RE 1.60
CL -.226
CDW 0.0366
CM -.0201

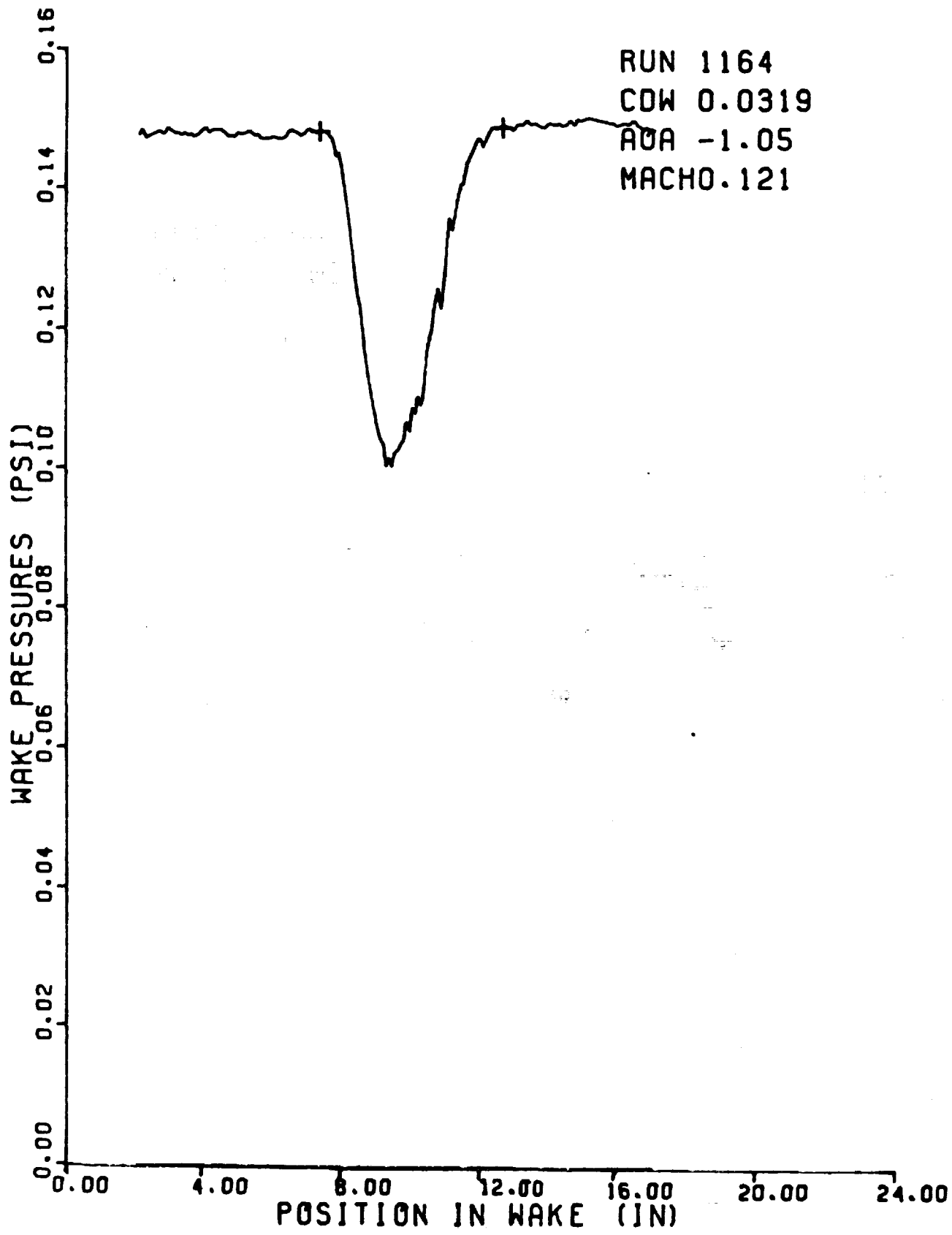




RUN 1164

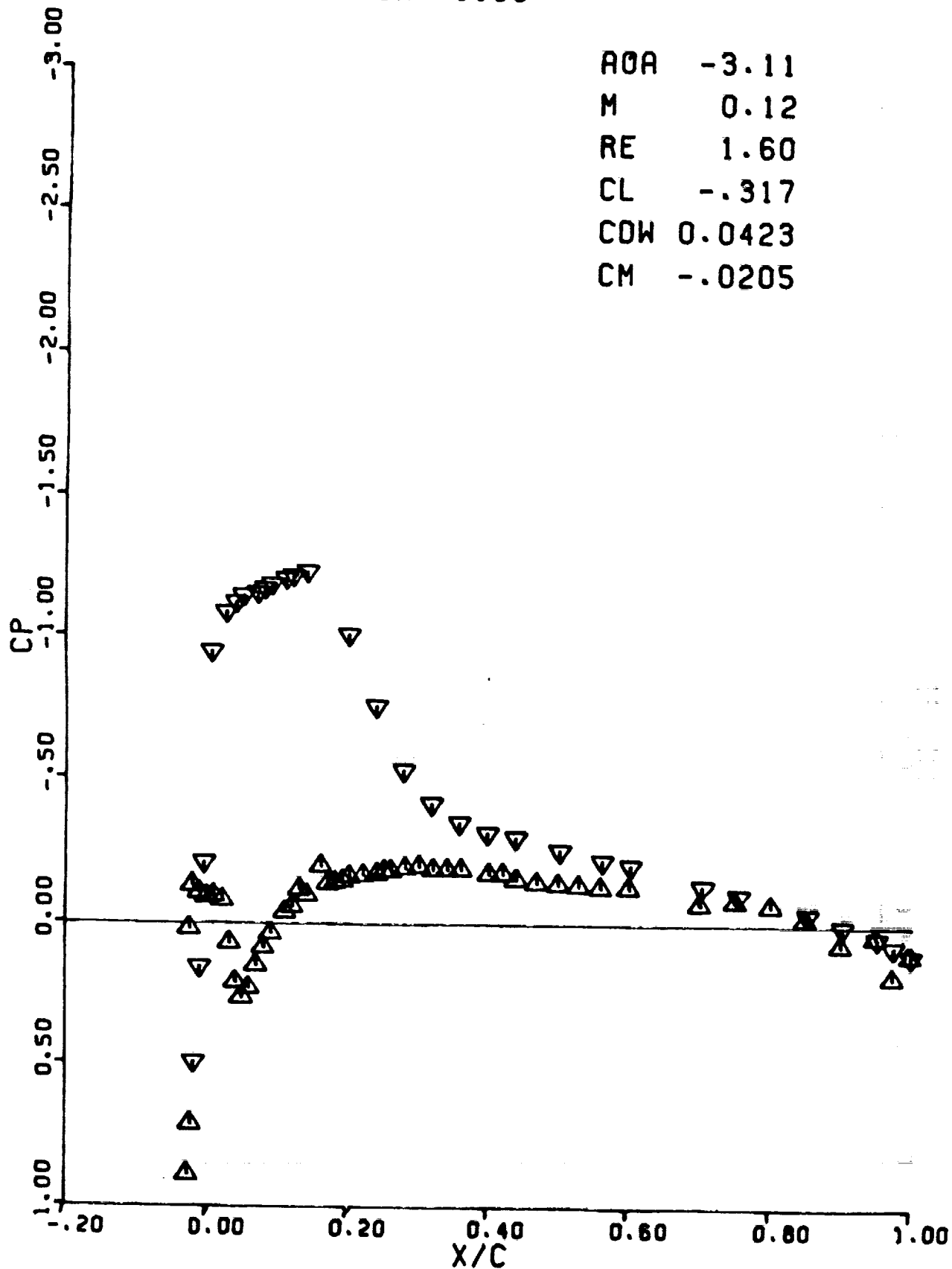
AOA -1.05
M 0.12
RE 1.62
CL -.118
CDW 0.0319
CM -.0182

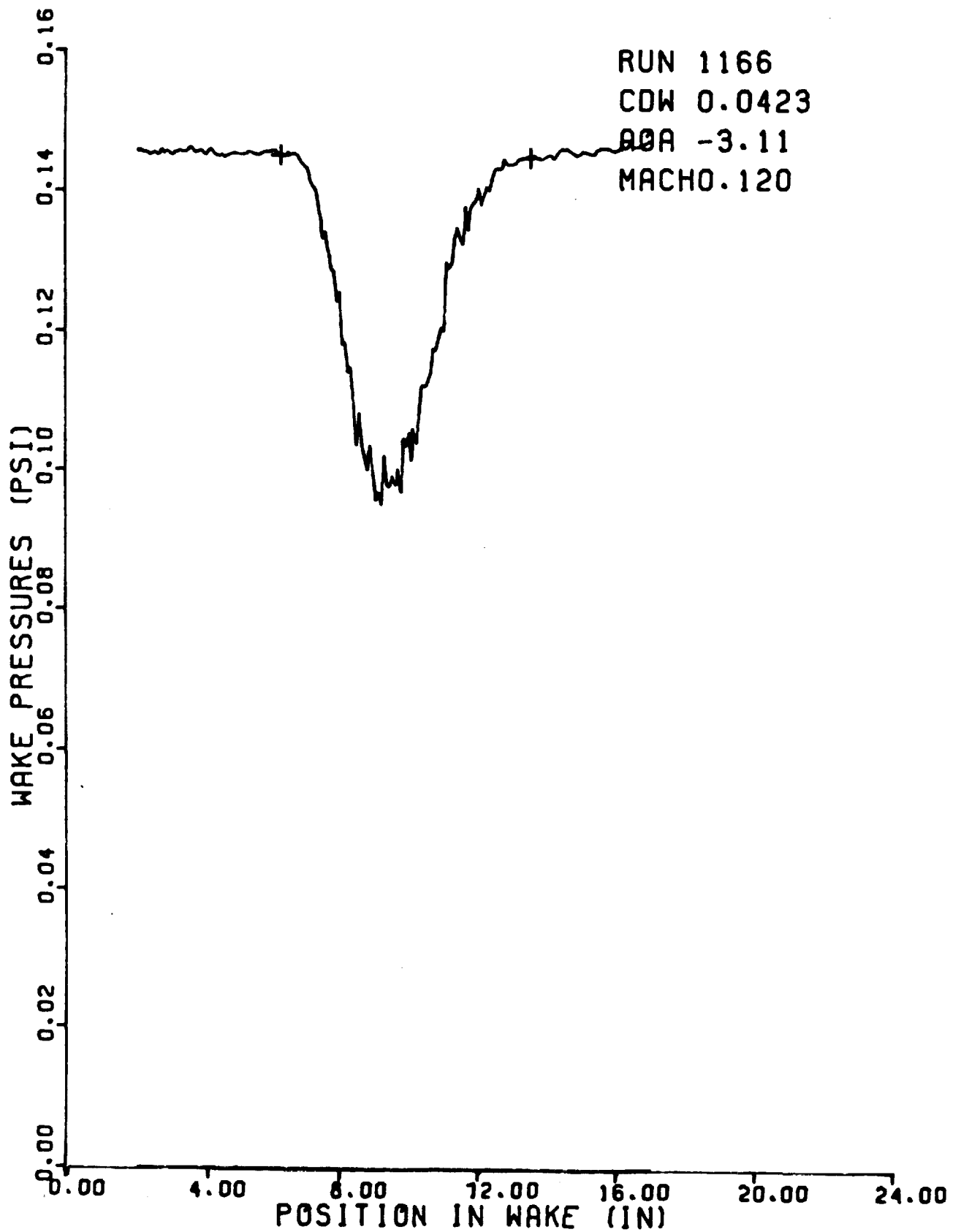




RUN 1166

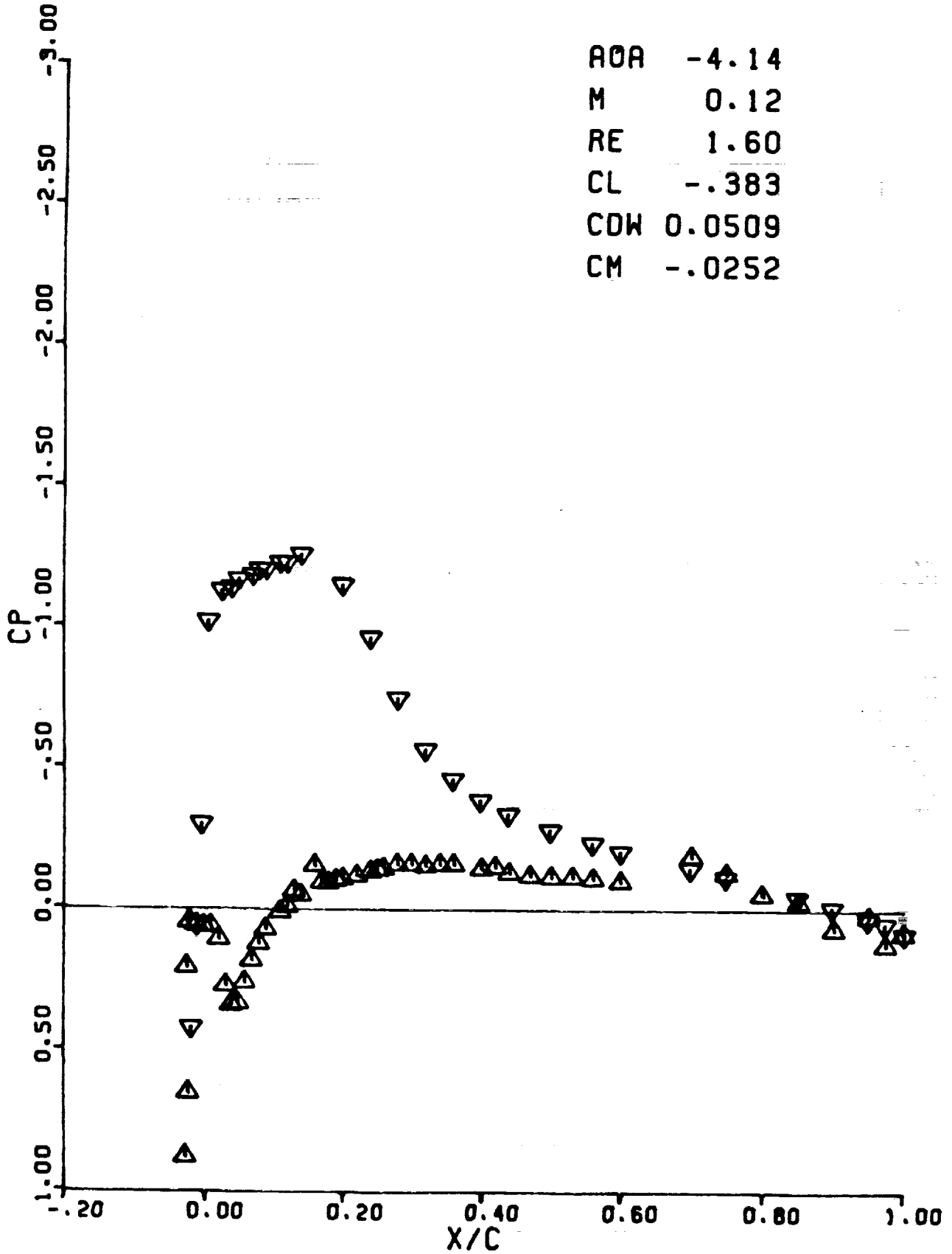
AOA -3.11
M 0.12
RE 1.60
CL -.317
CDW 0.0423
CM -.0205

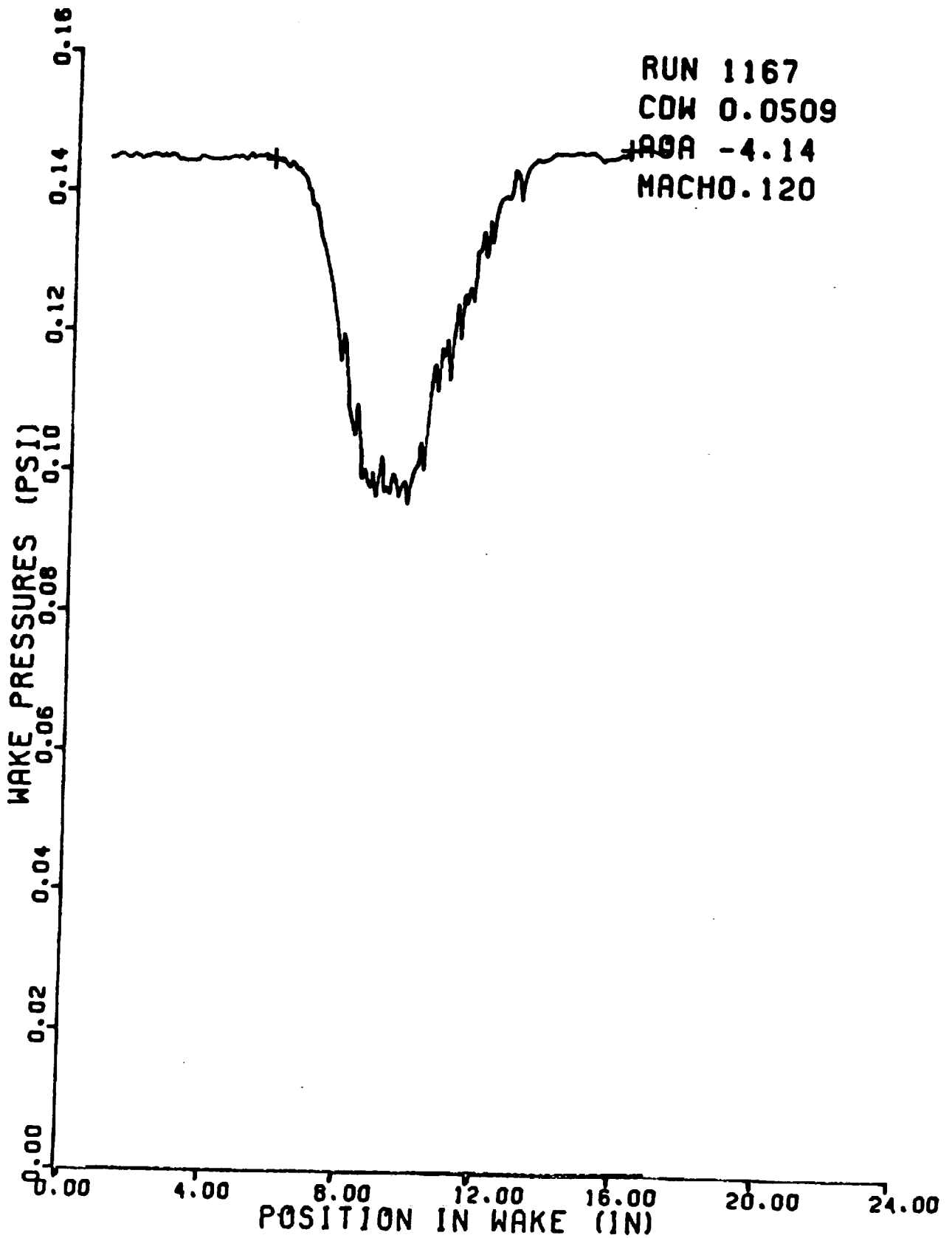




RUN 1167

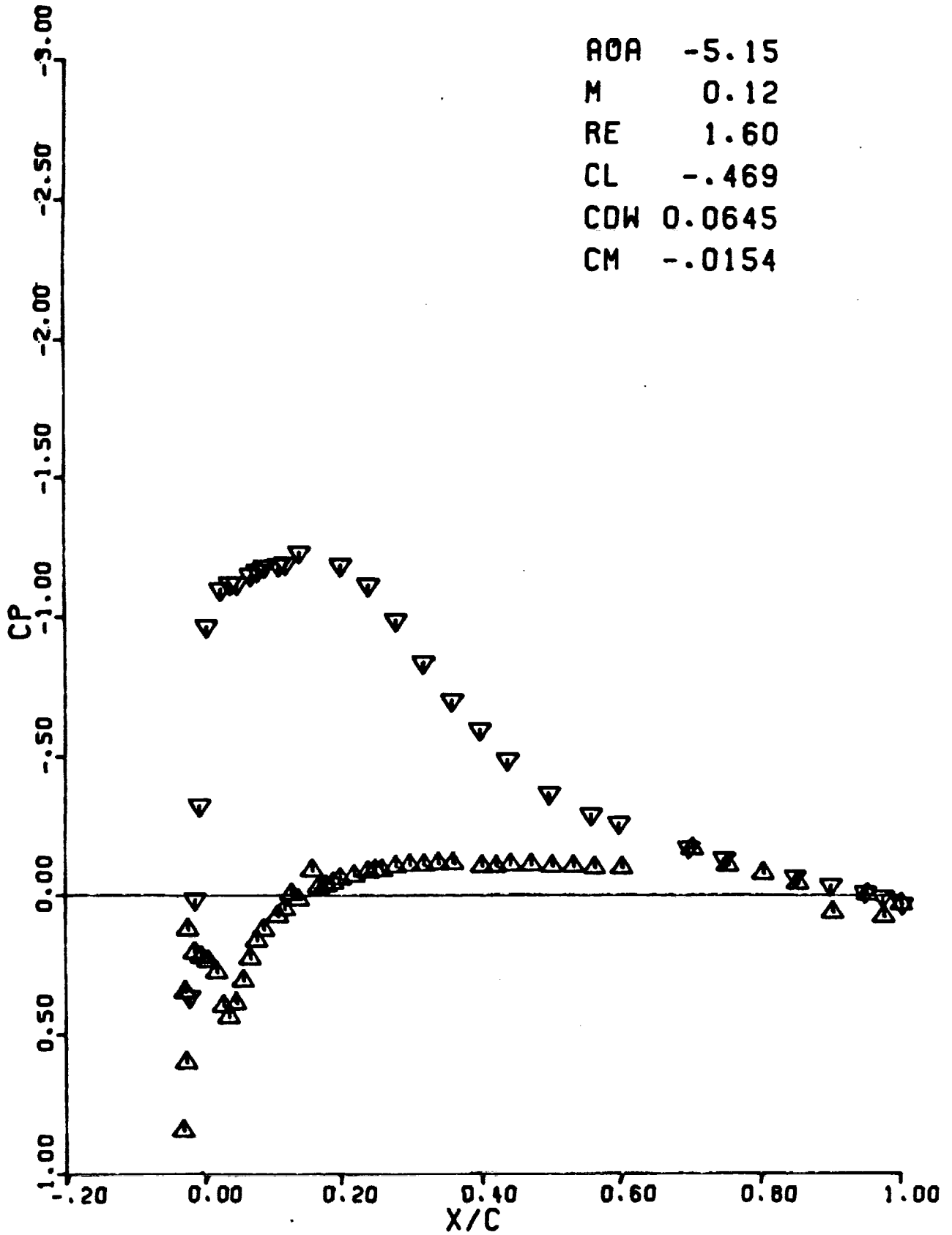
AOA -4.14
M 0.12
RE 1.60
CL -.383
CDW 0.0509
CM -.0252

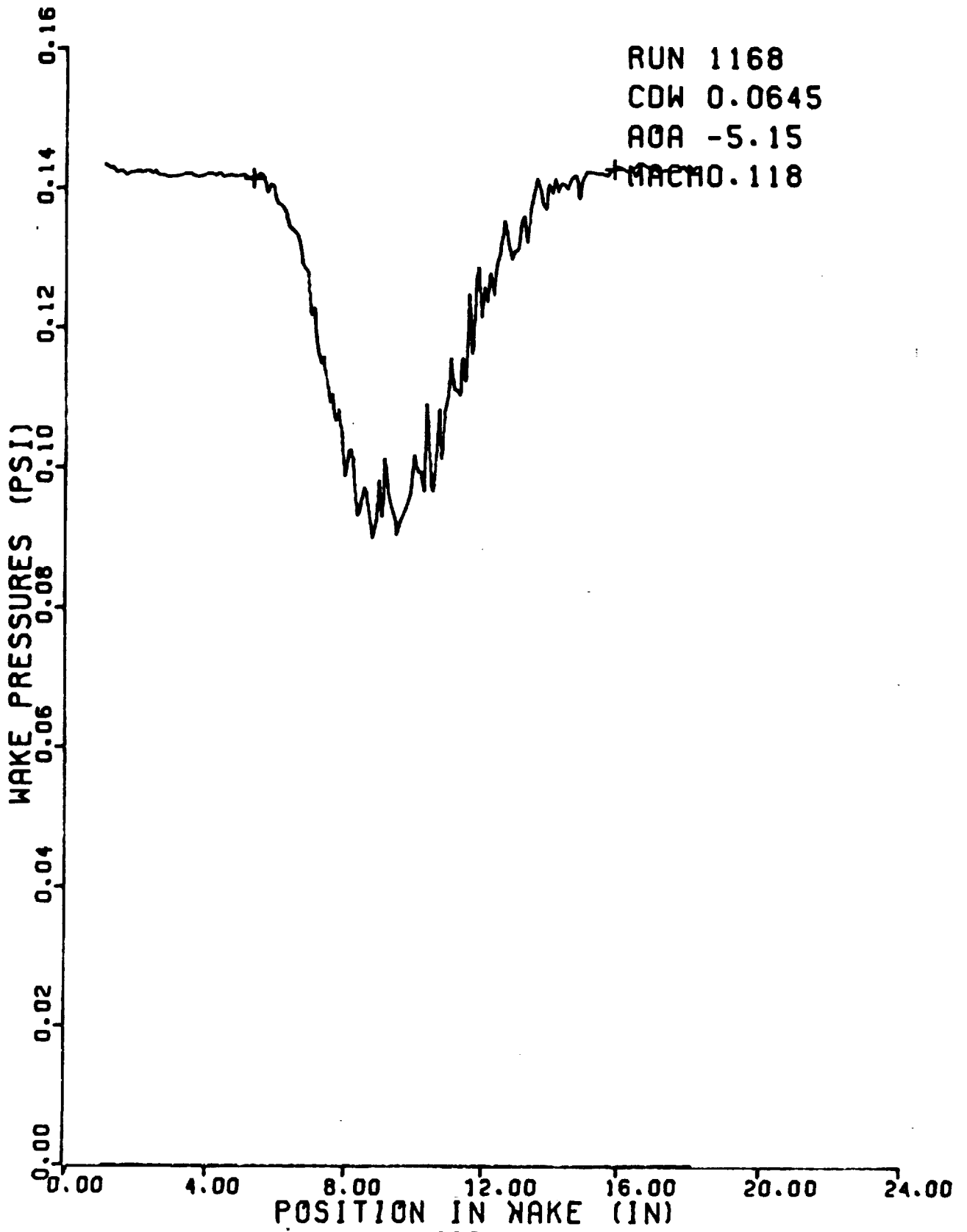




RUN 1168

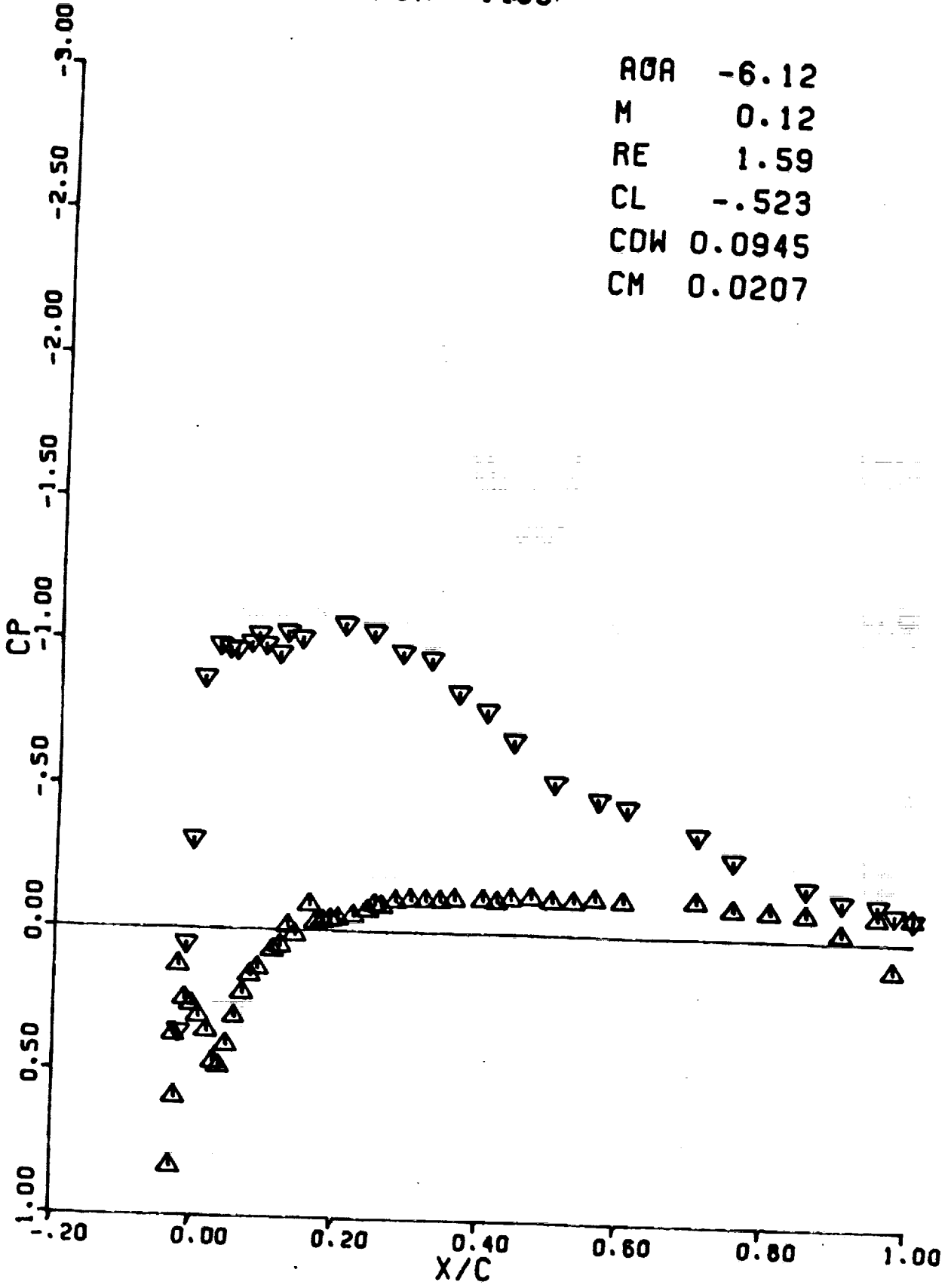
AOA -5.15
M 0.12
RE 1.60
CL -.469
CDW 0.0645
CM -.0154

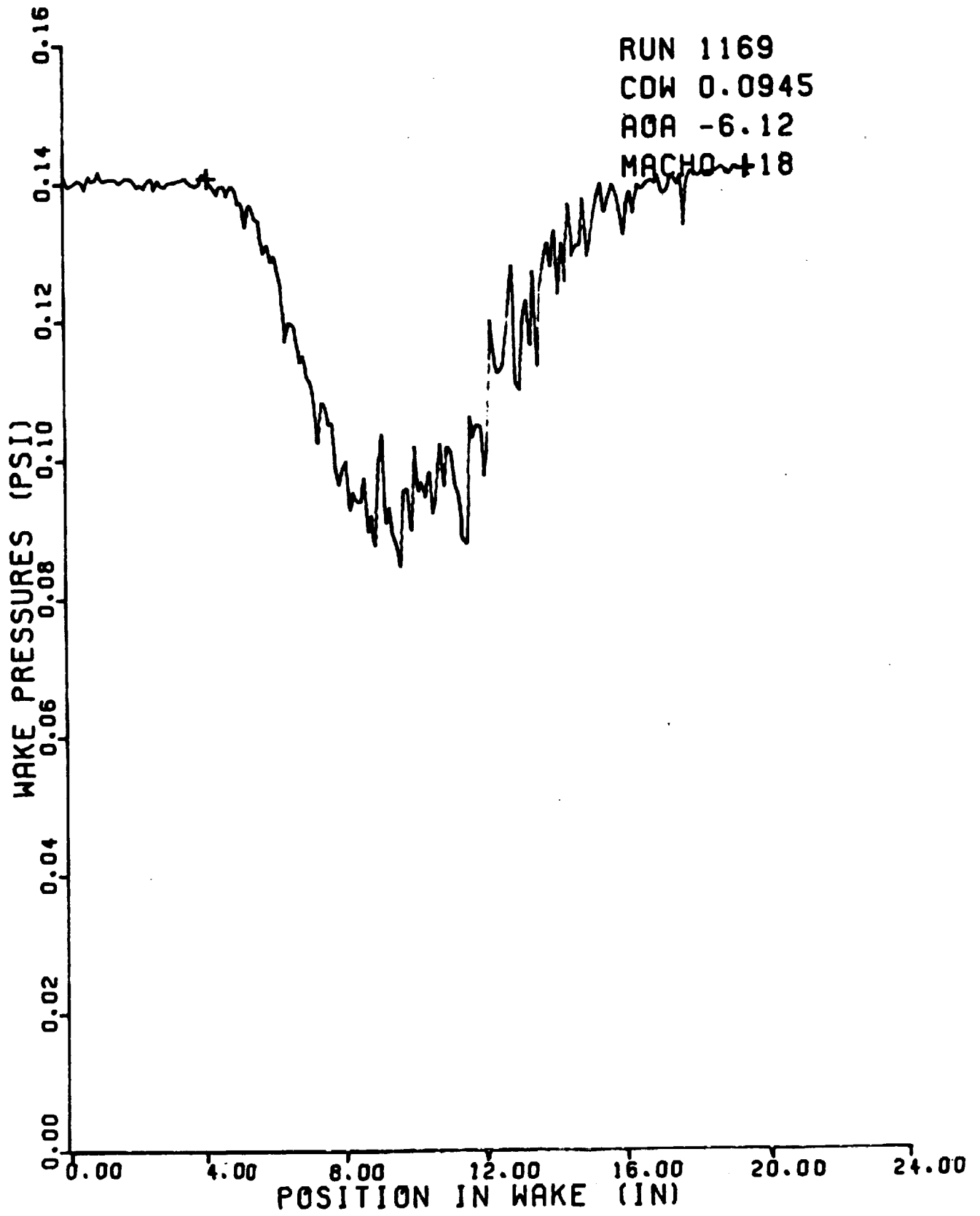




RUN 1.169

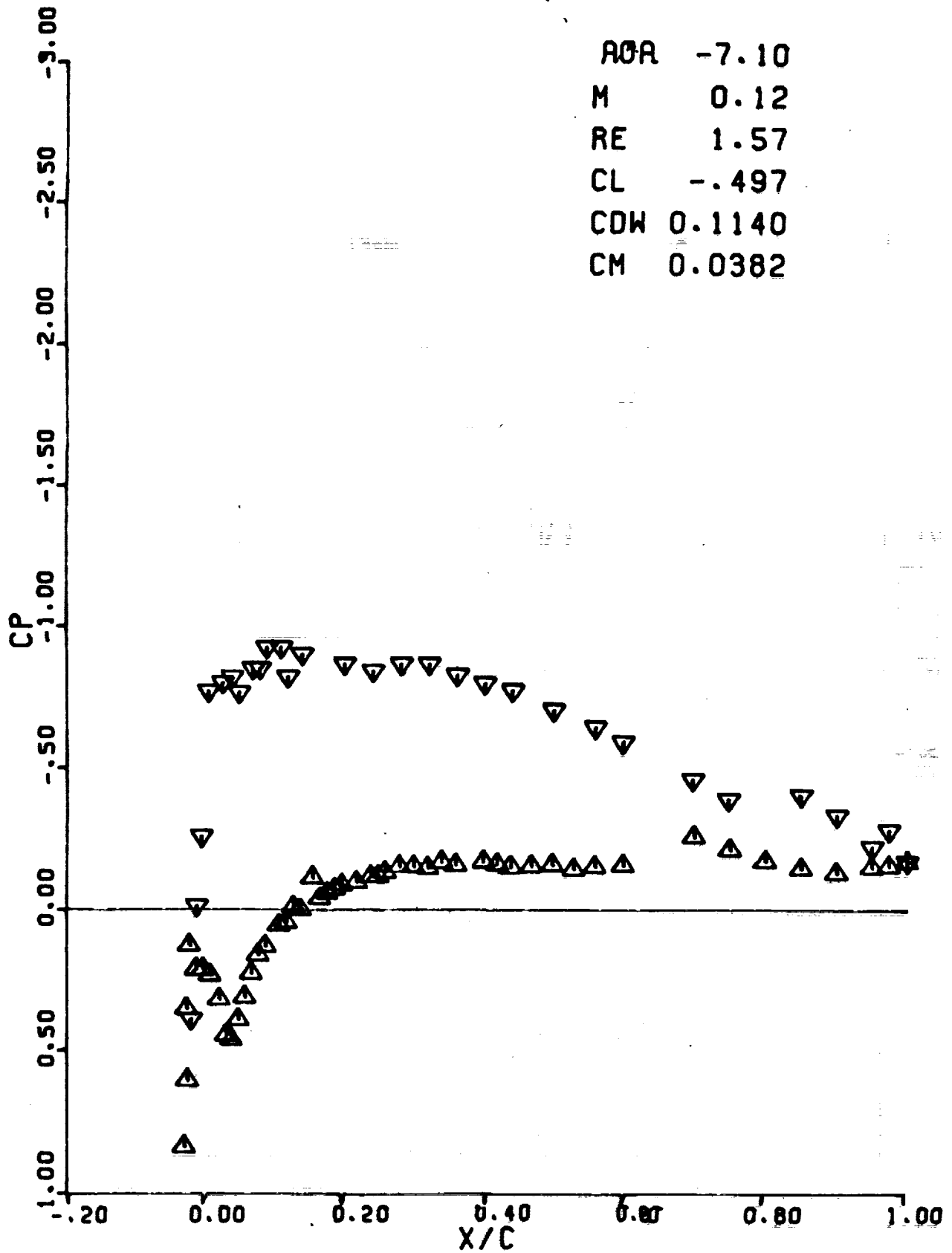
ROA -6.12
M 0.12
RE 1.59
CL -.523
CDW 0.0945
CM 0.0207

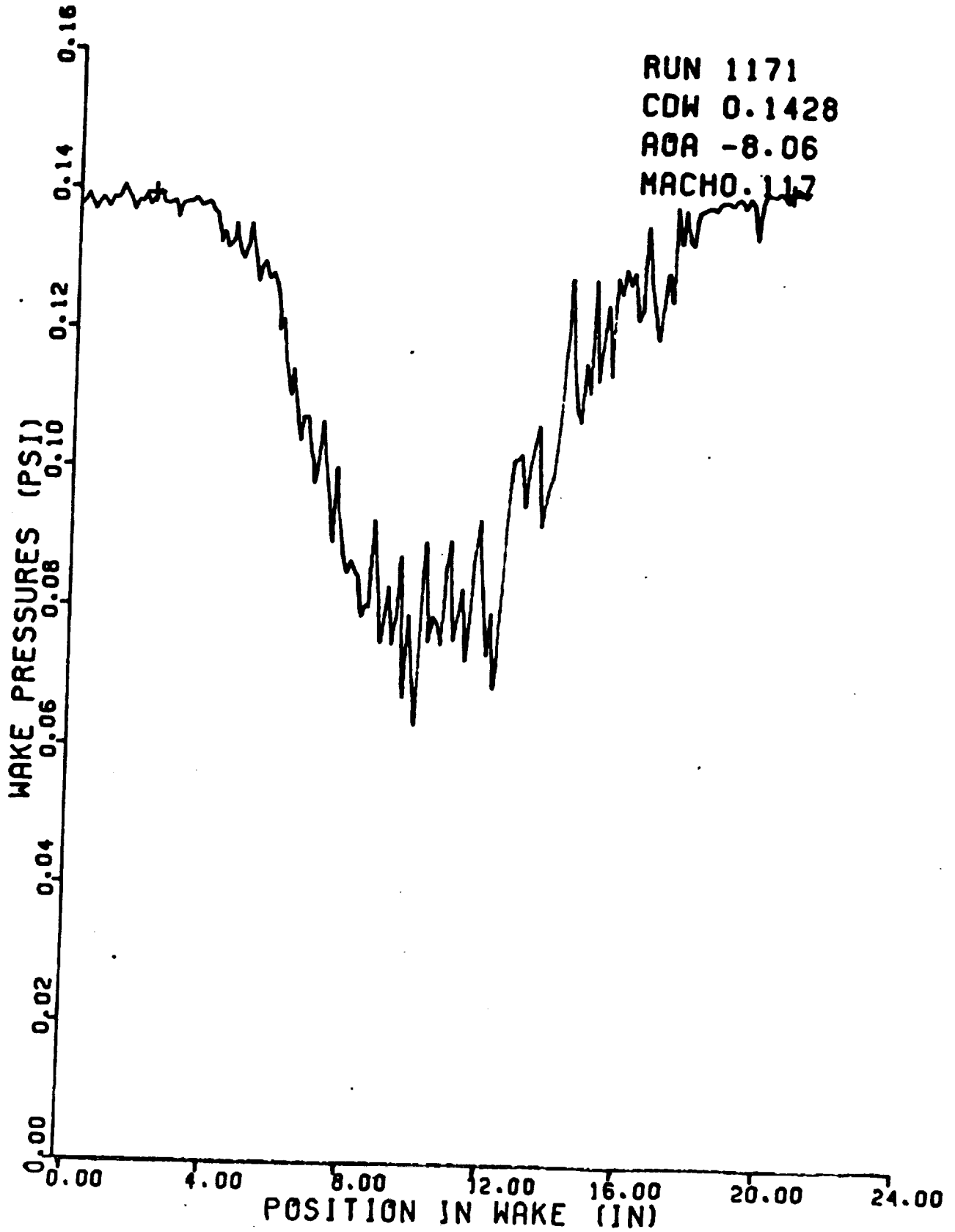




RUN 1170

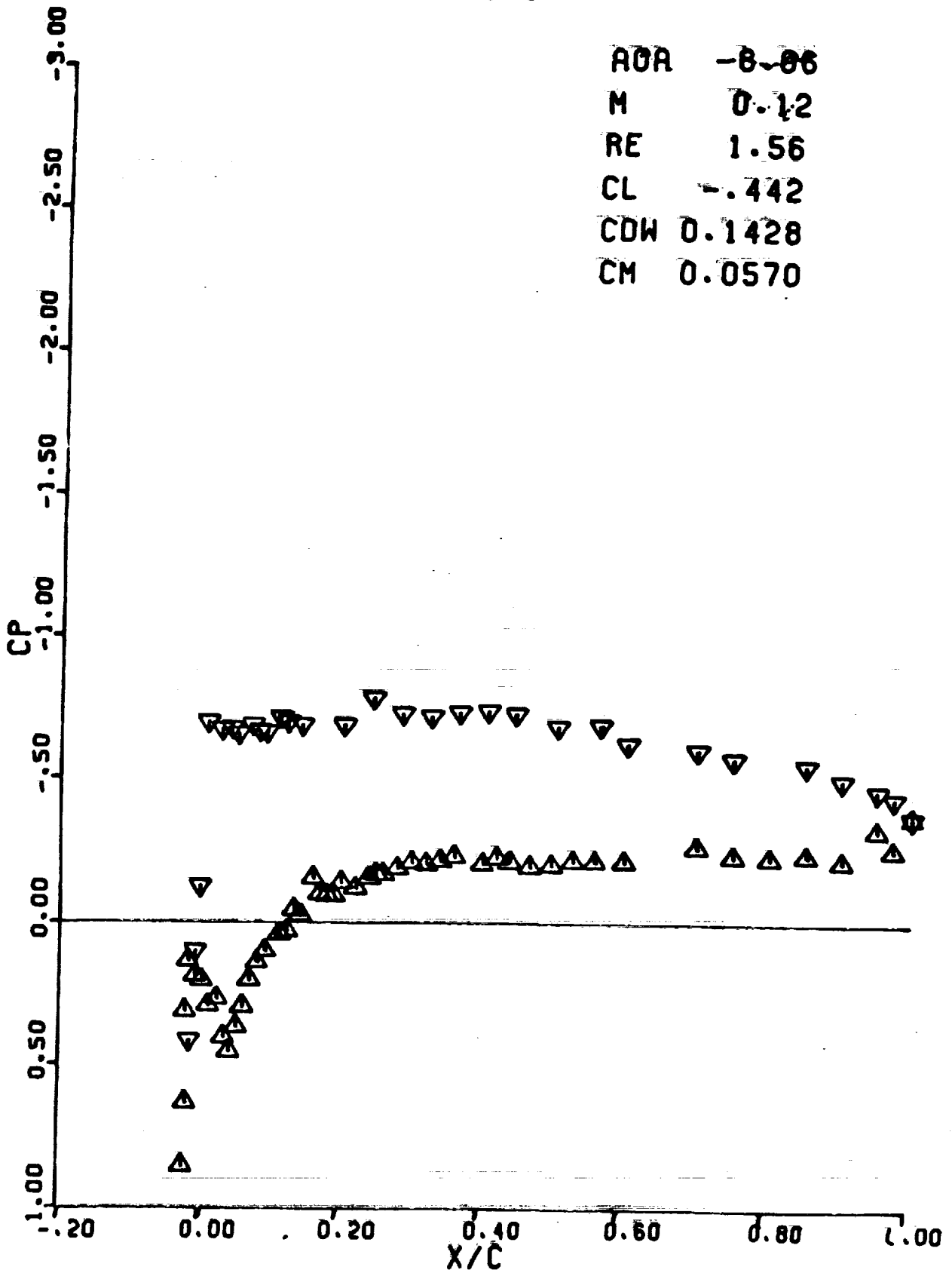
AOA -7.10
M 0.12
RE 1.57
CL -.497
CDW 0.1140
CM 0.0382





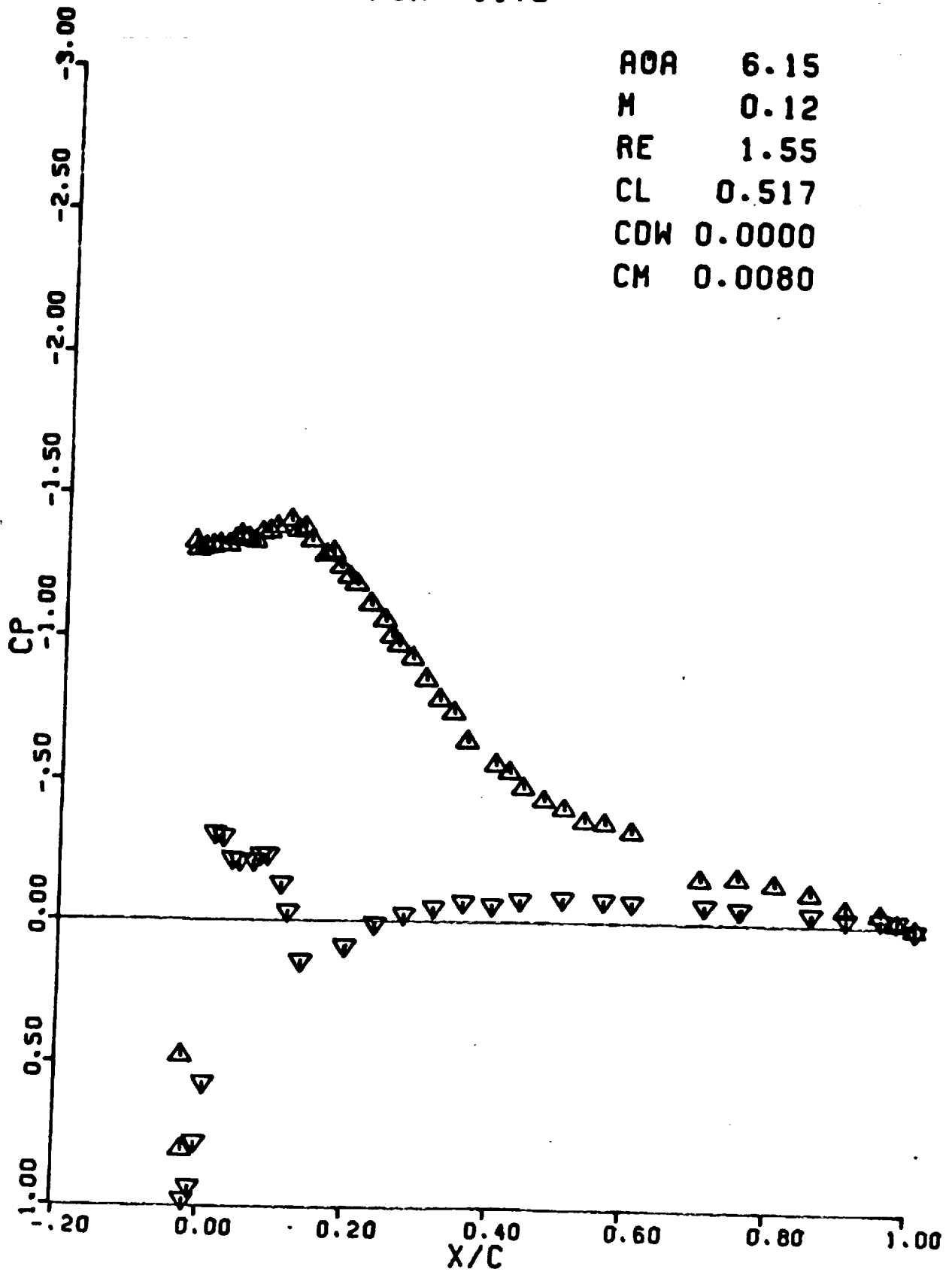
RUN 1171

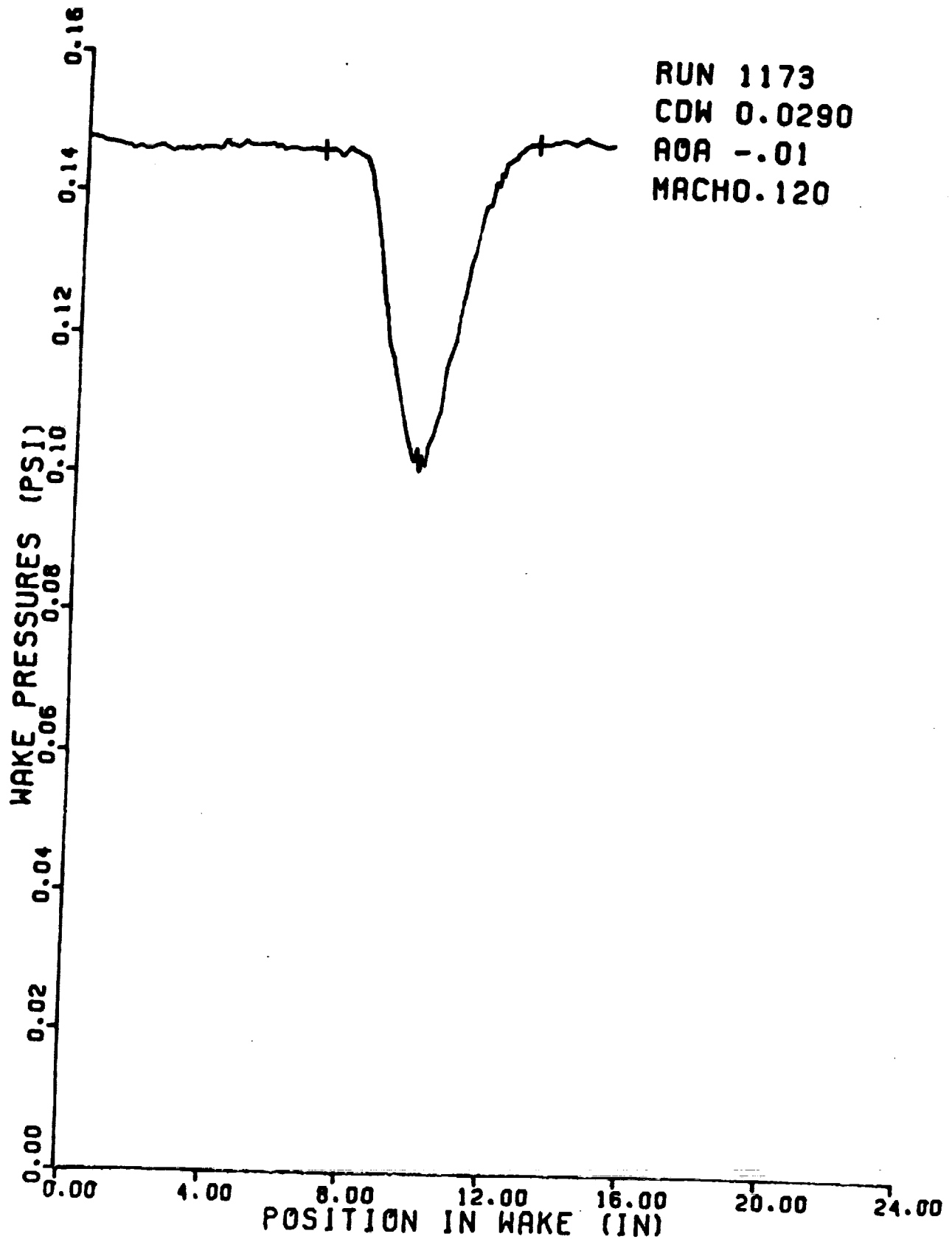
AOA -8.06
M 0.12
RE 1.56
CL -.442
CDW 0.1428
CM 0.0570



RUN 1172

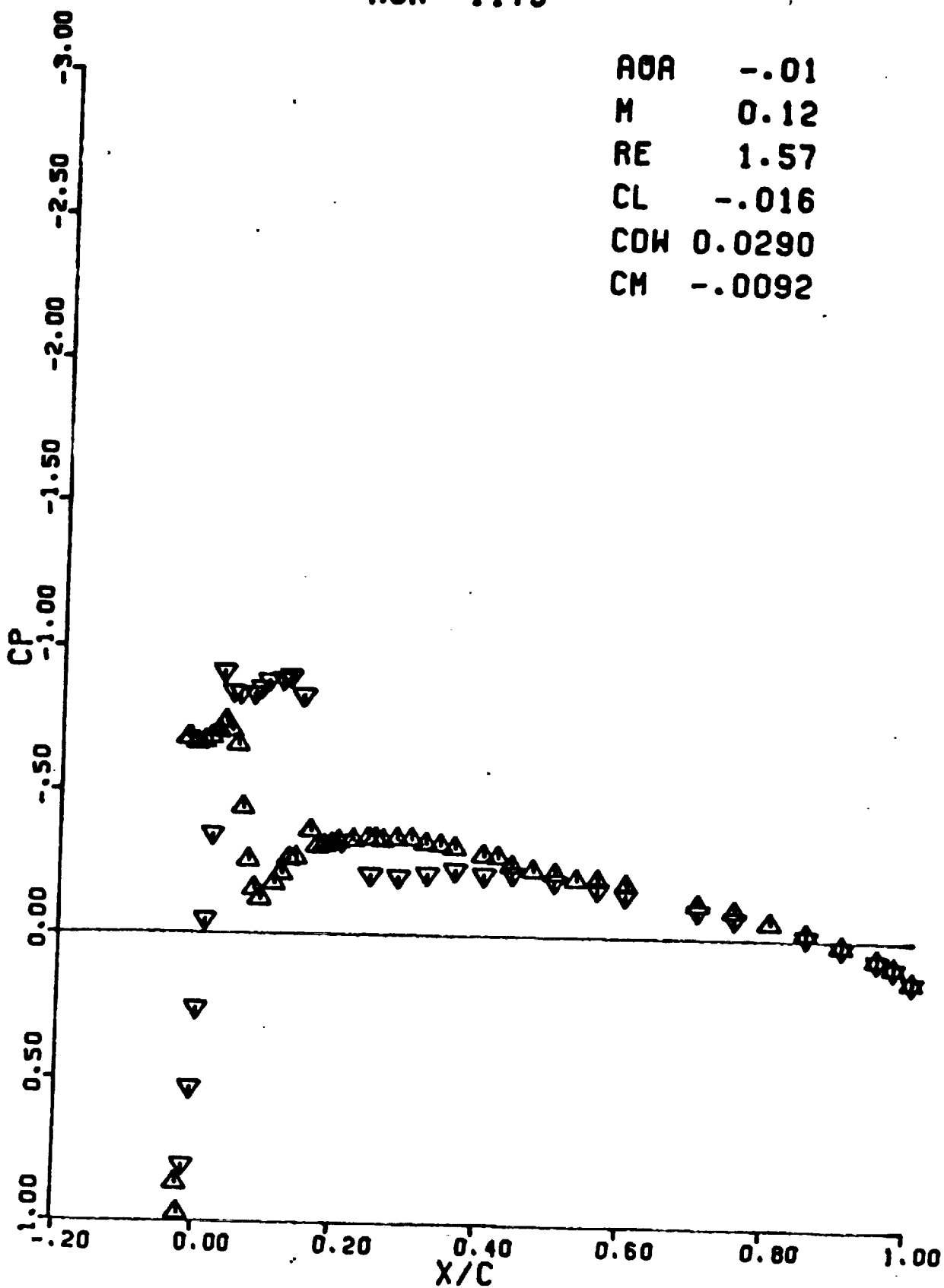
AOA 6.15
M 0.12
RE 1.55
CL 0.517
CDW 0.0000
CM 0.0080





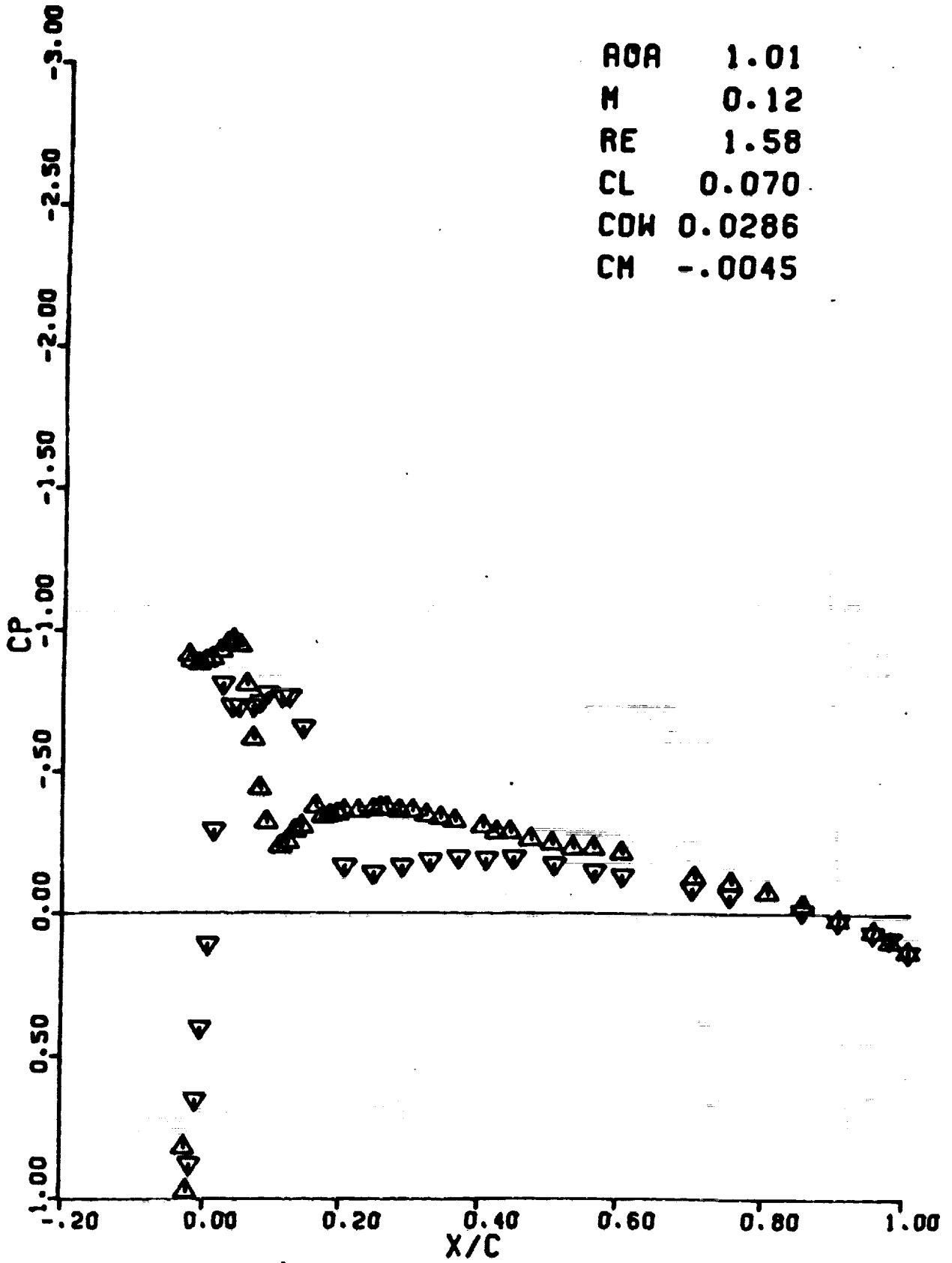
RUN 1173

AOA -.01
M 0.12
RE 1.57
CL -.016
CDW 0.0290
CM -.0092



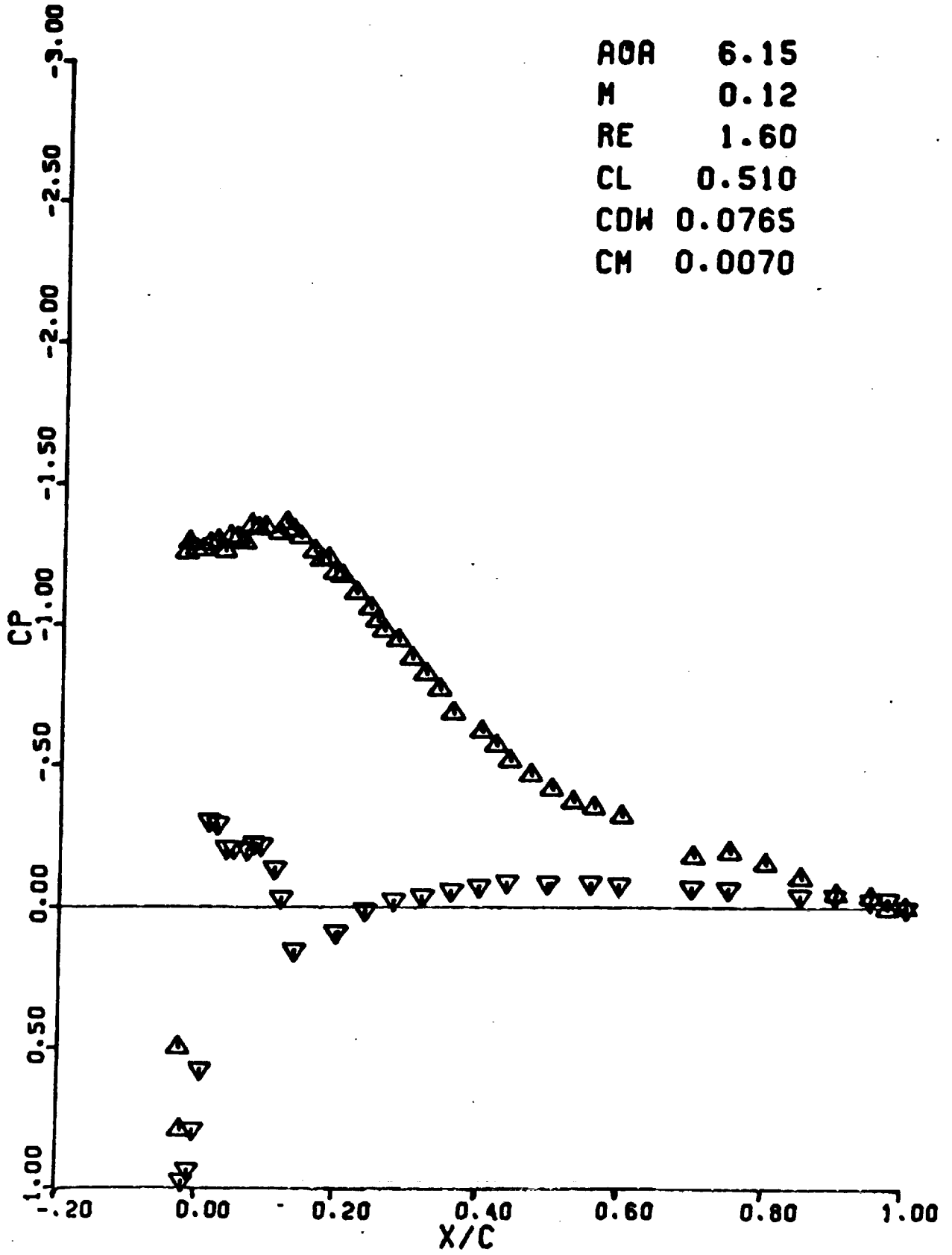
RUN 1174

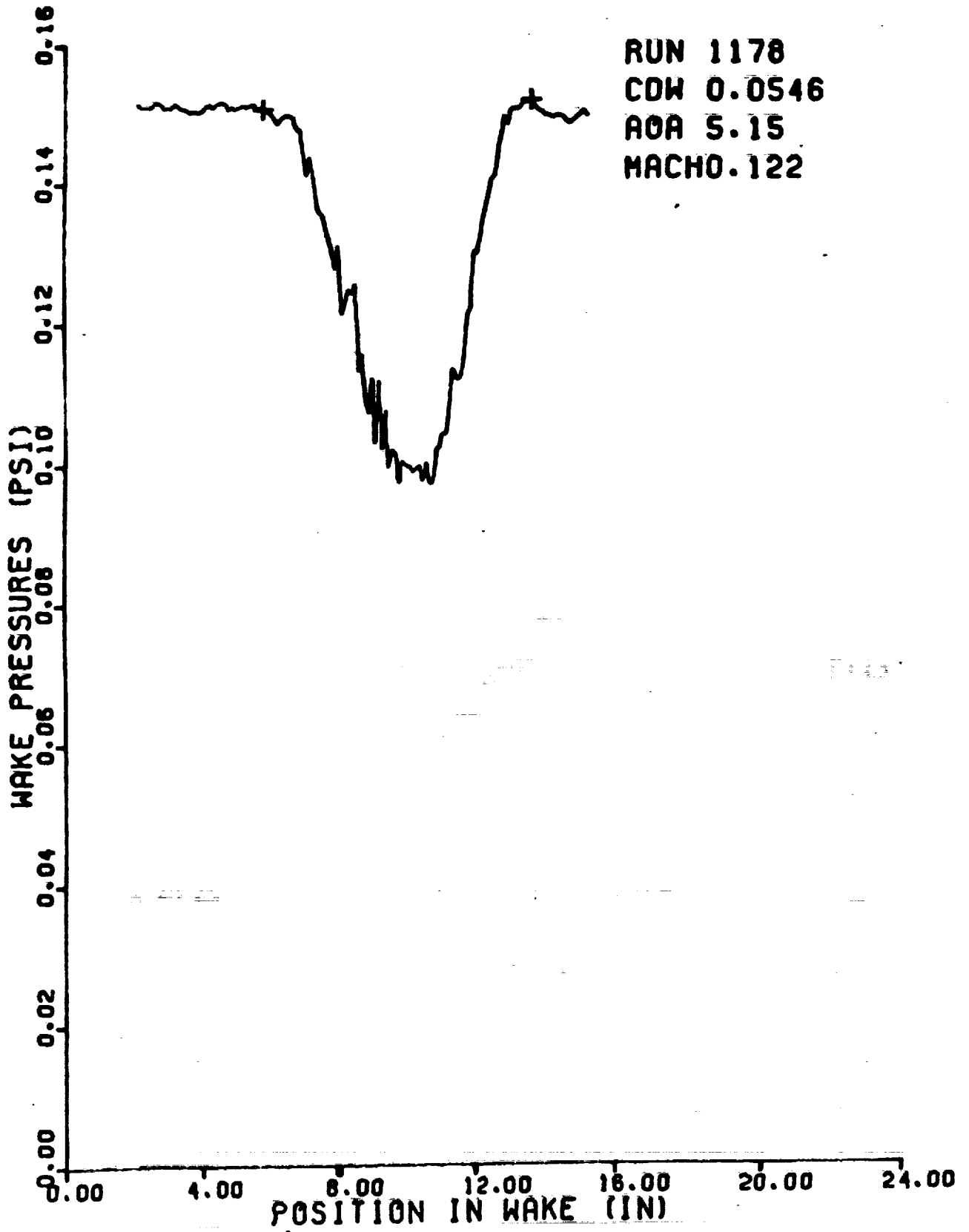
AOA 1.01
M 0.12
RE 1.58
CL 0.070
CDW 0.0286
CM -.0045



RUN 1179

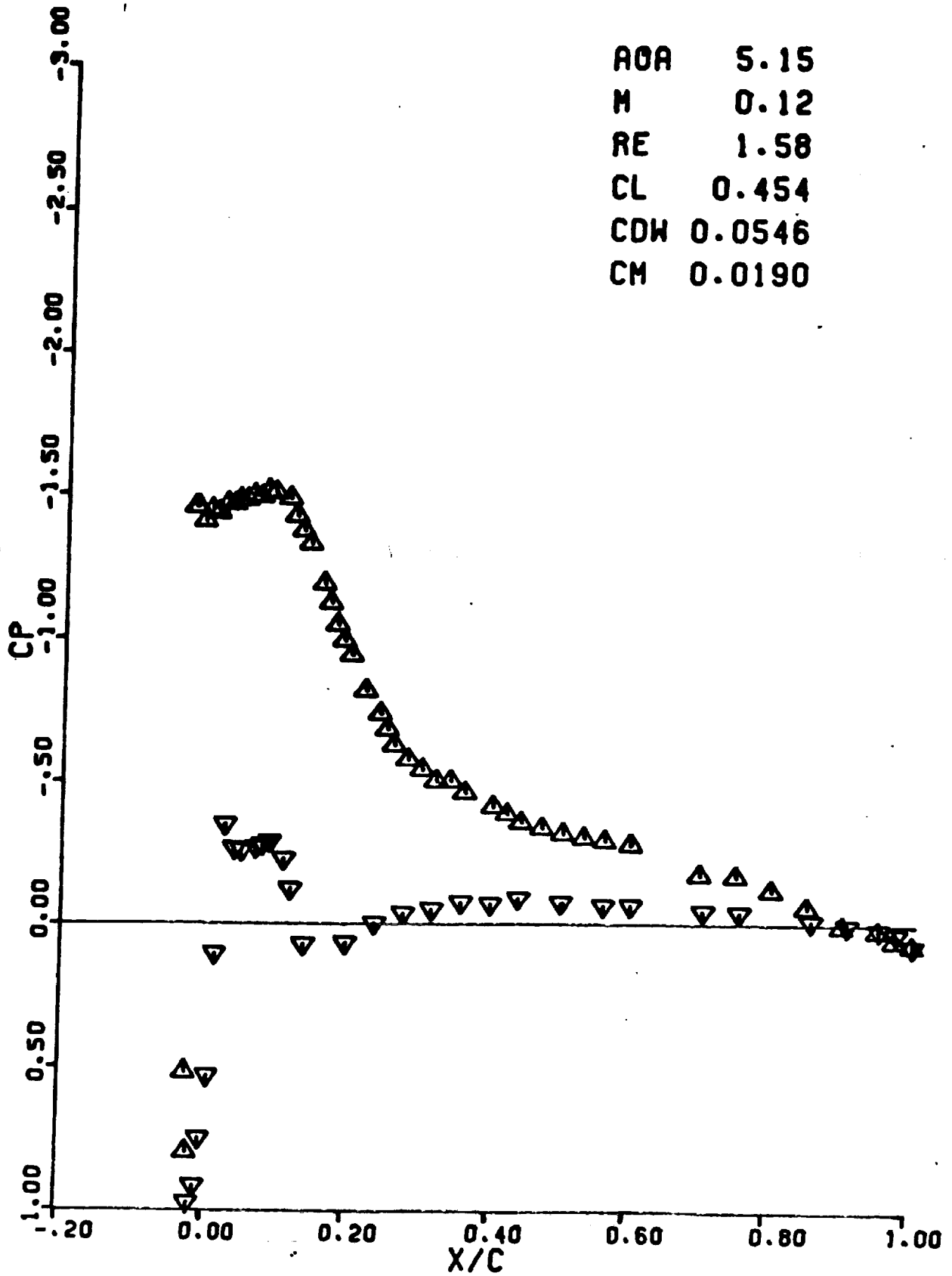
AOA 6.15
M 0.12
RE 1.60
CL 0.510
CDW 0.0765
CM 0.0070

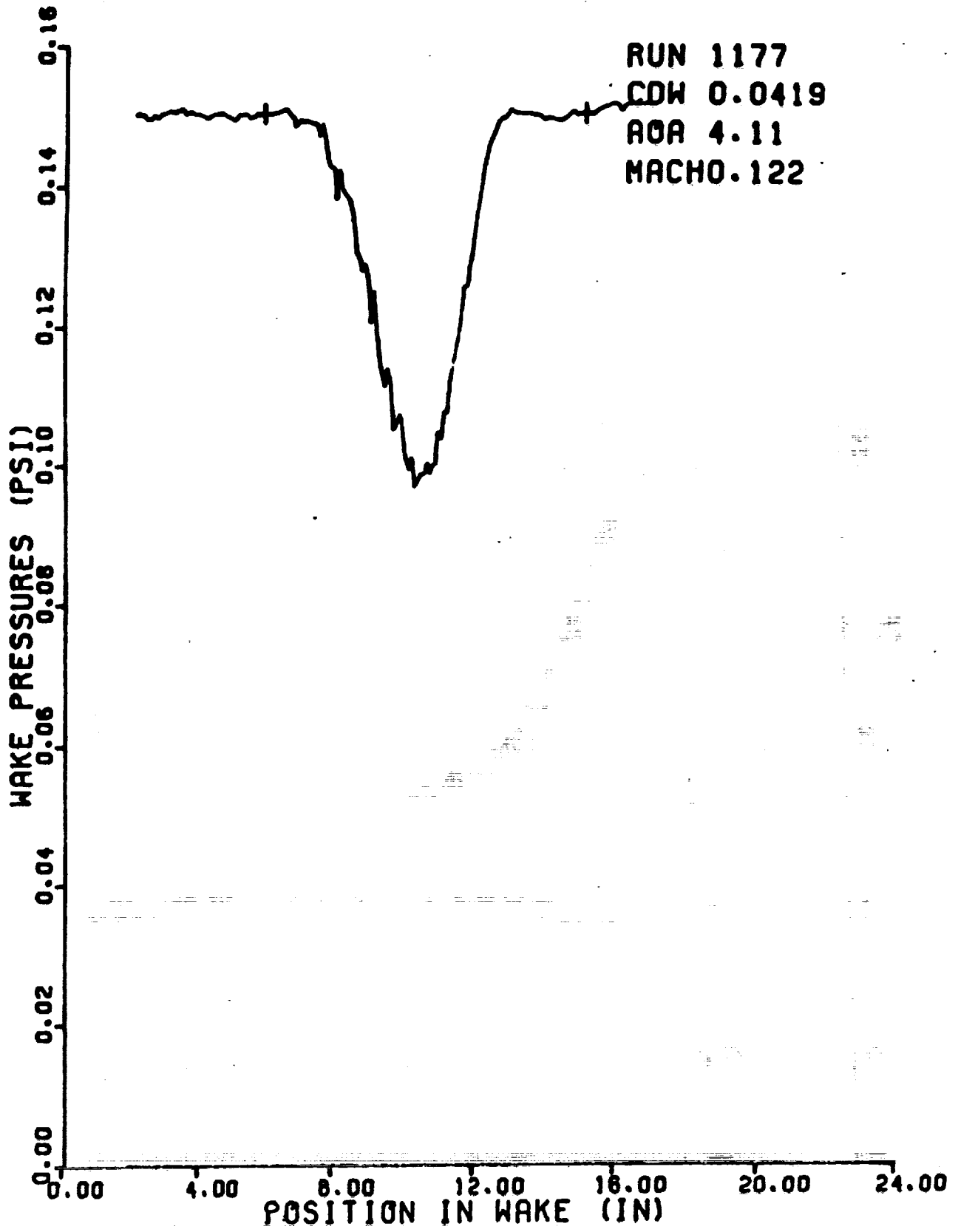




RUN 1178

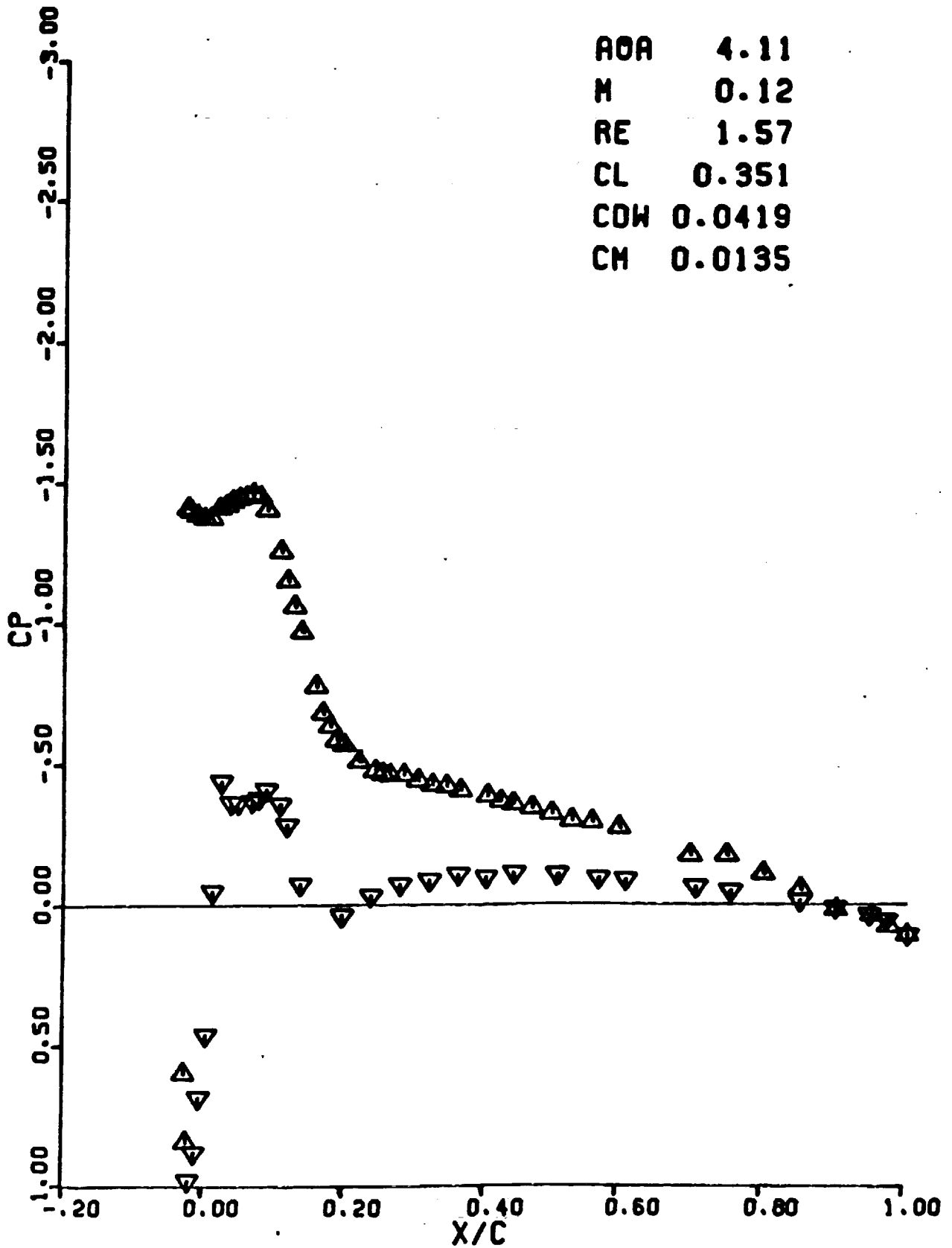
AOA 5.15
M 0.12
RE 1.58
CL 0.454
CDW 0.0546
CM 0.0190

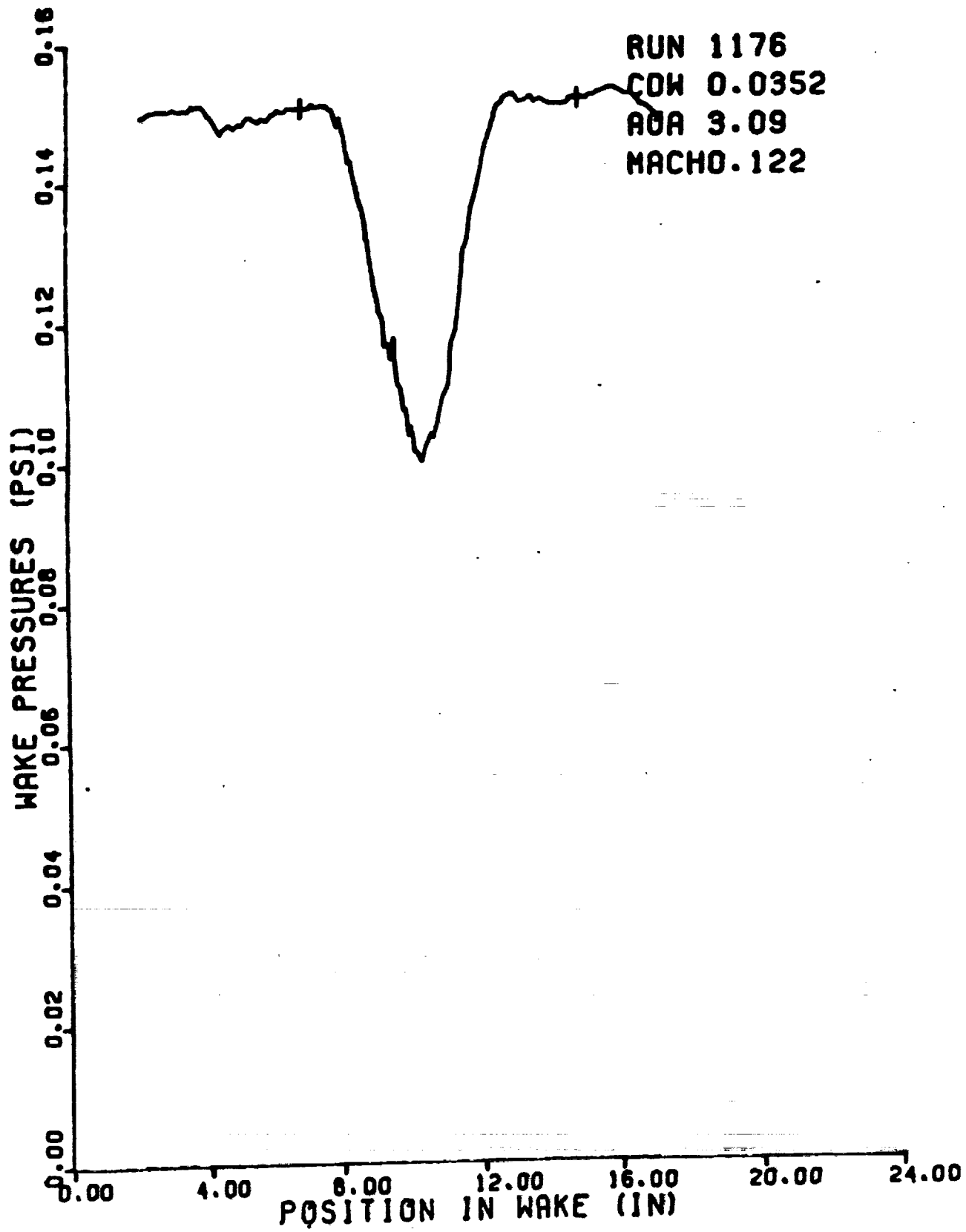


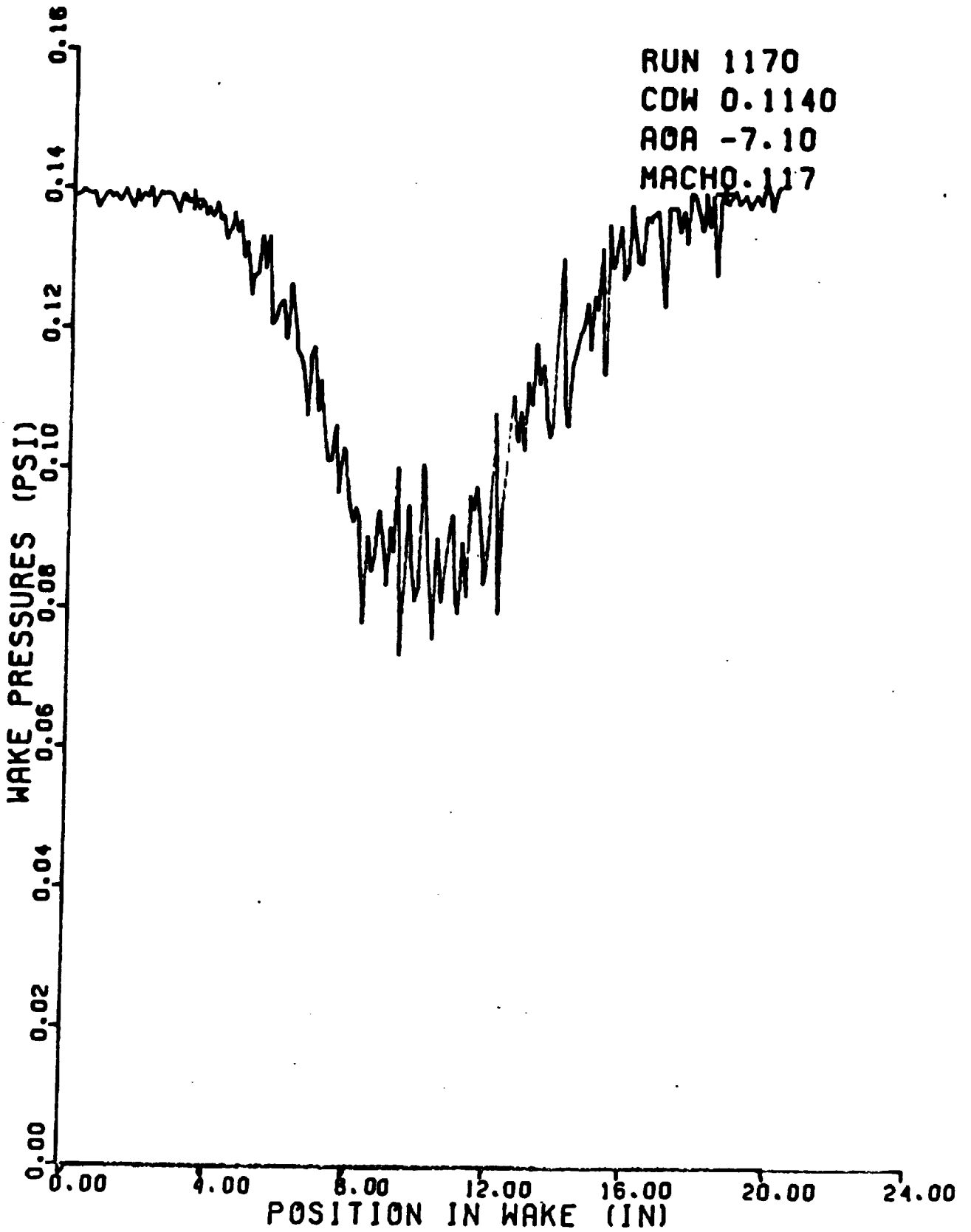


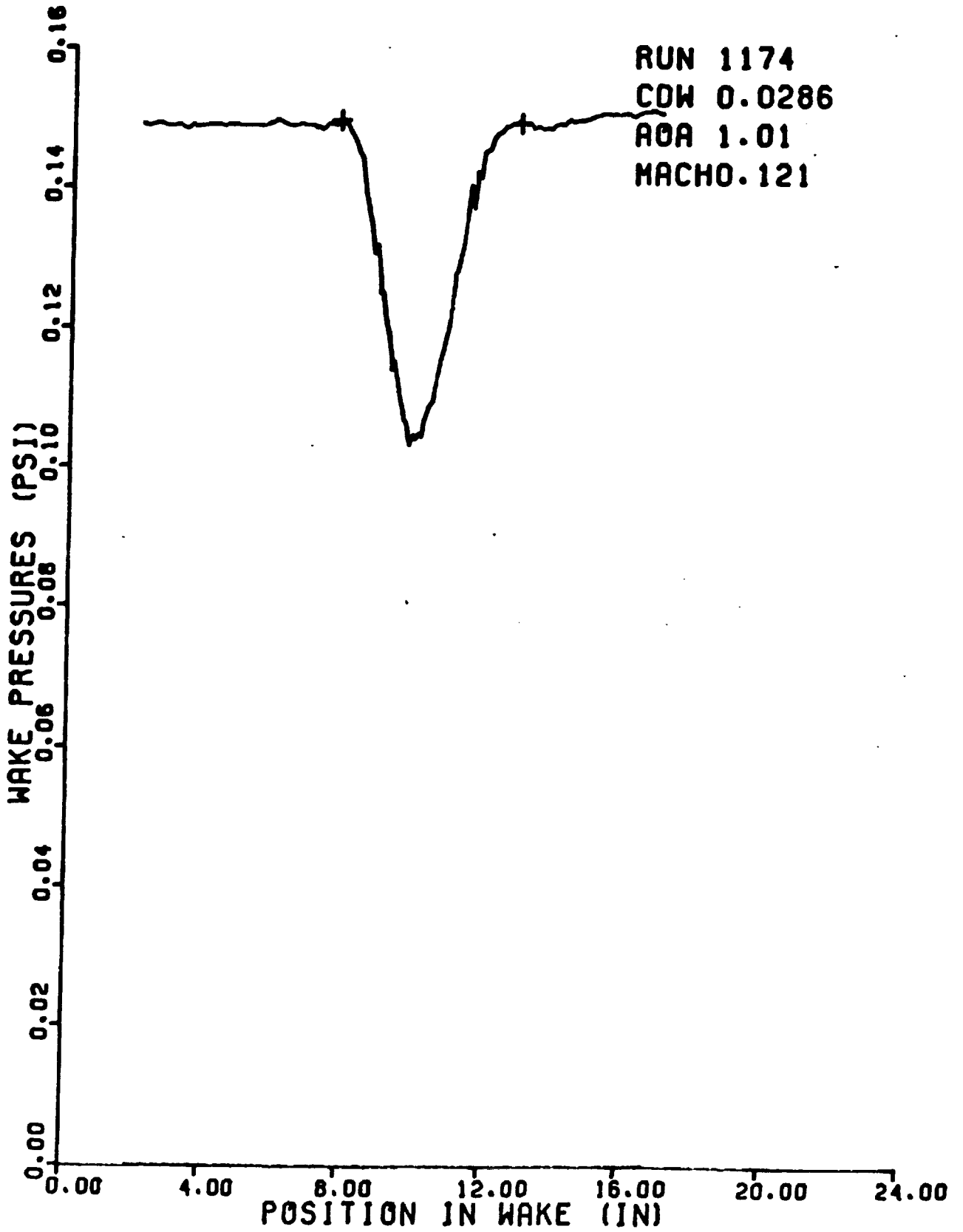
RUN 1177

AOA 4.11
M 0.12
RE 1.57
CL 0.351
CDW 0.0419
CM 0.0135



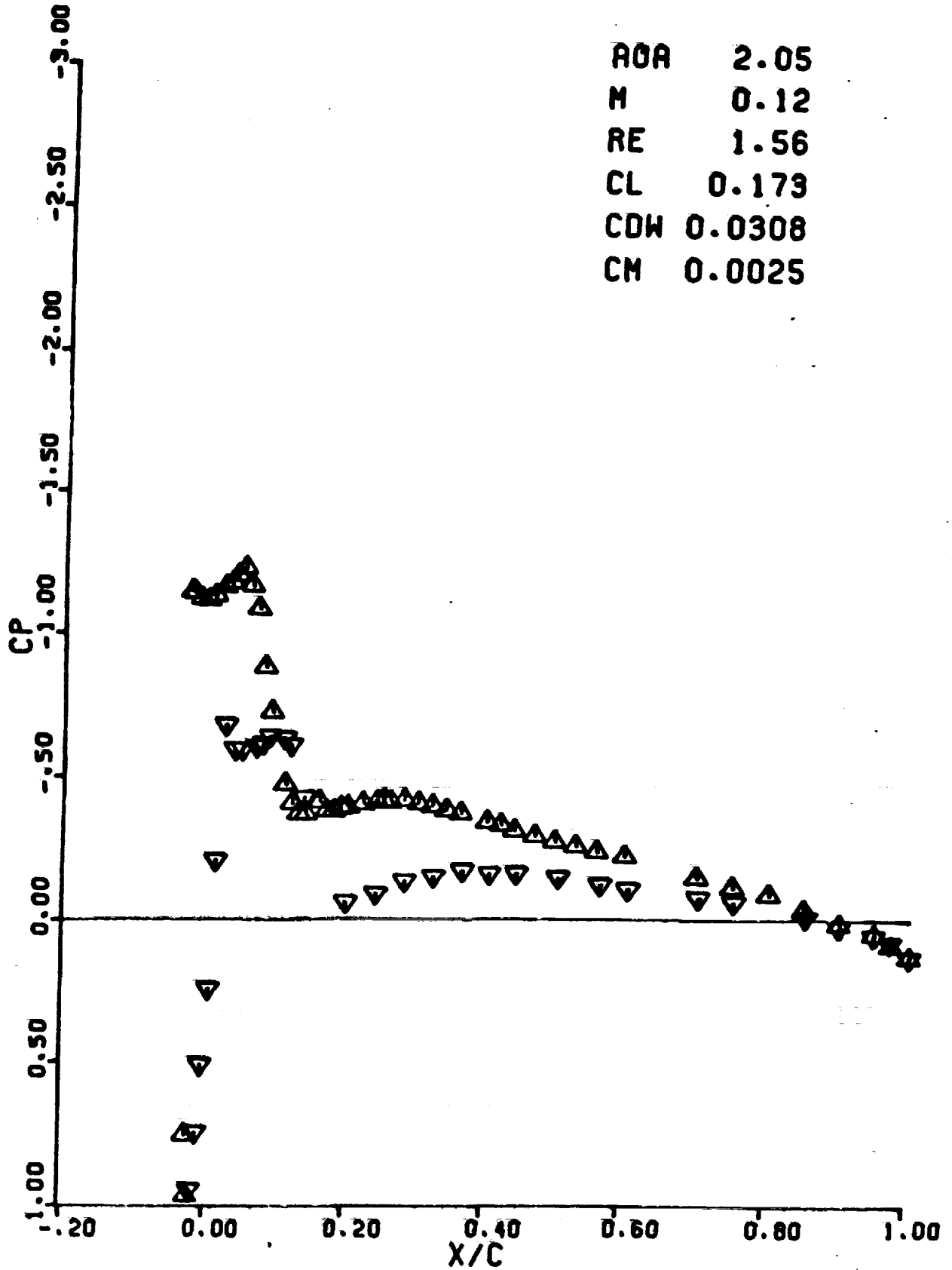


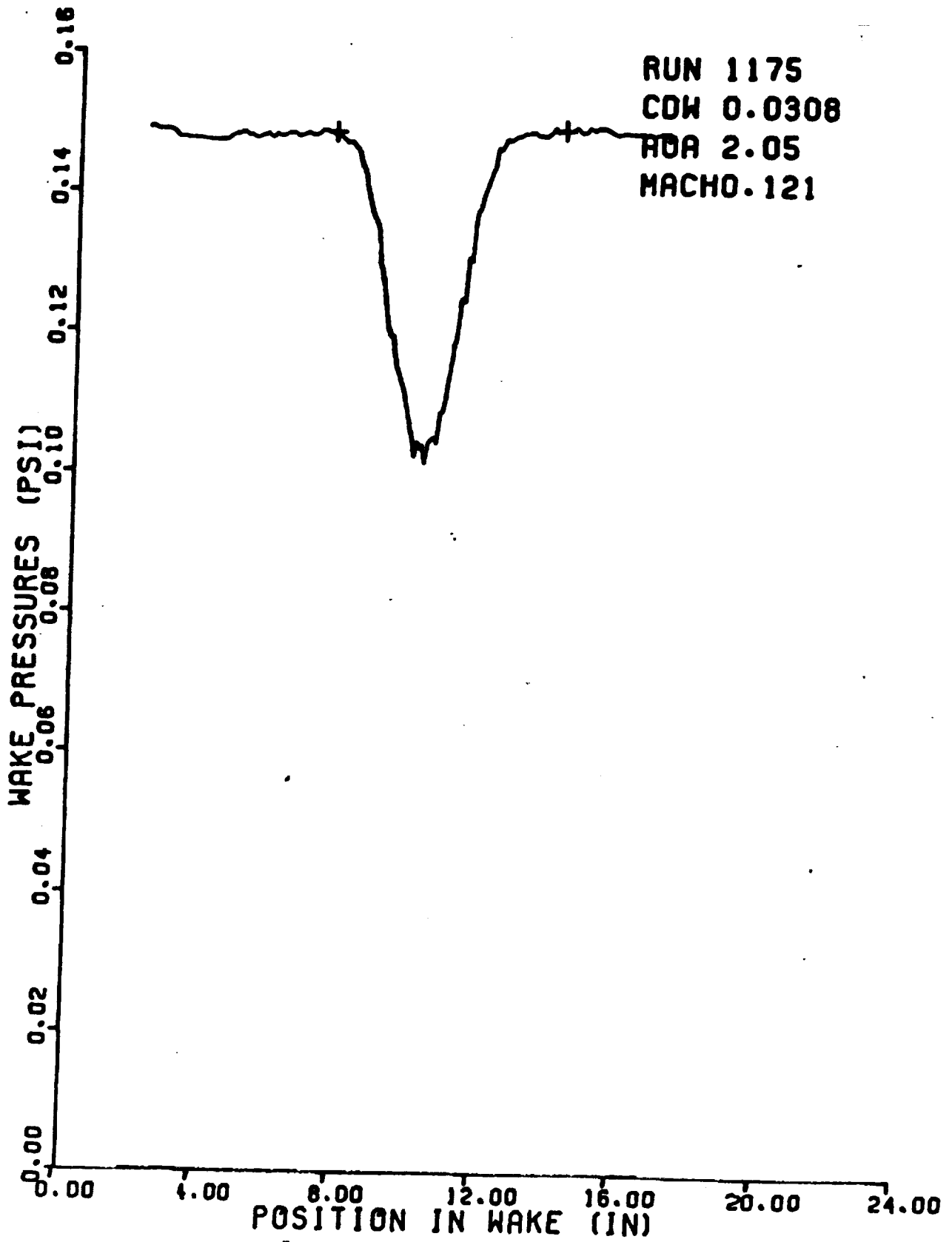




RUN 1175

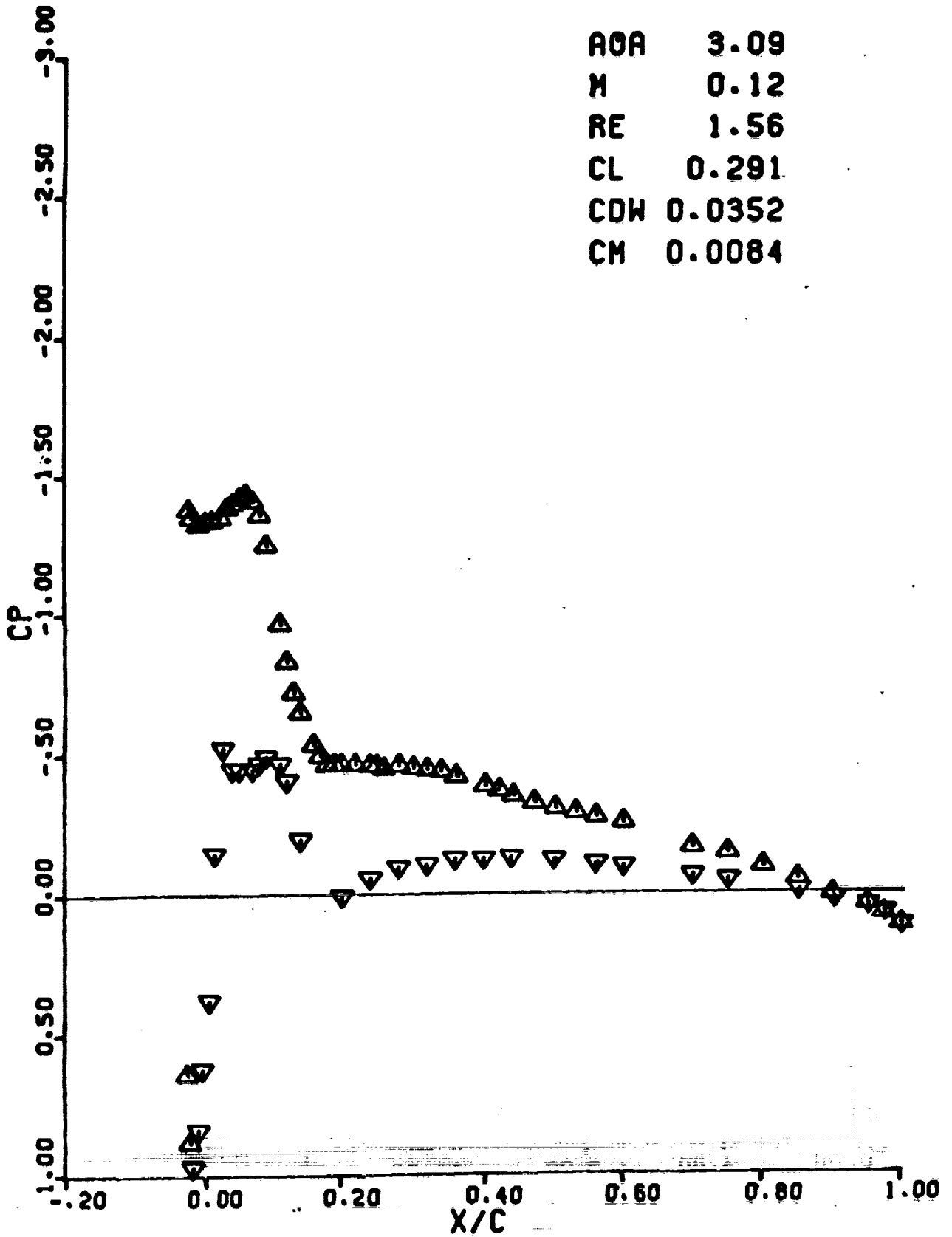
AOA 2.05
M 0.12
RE 1.56
CL 0.173
CDW 0.0308
CM 0.0025

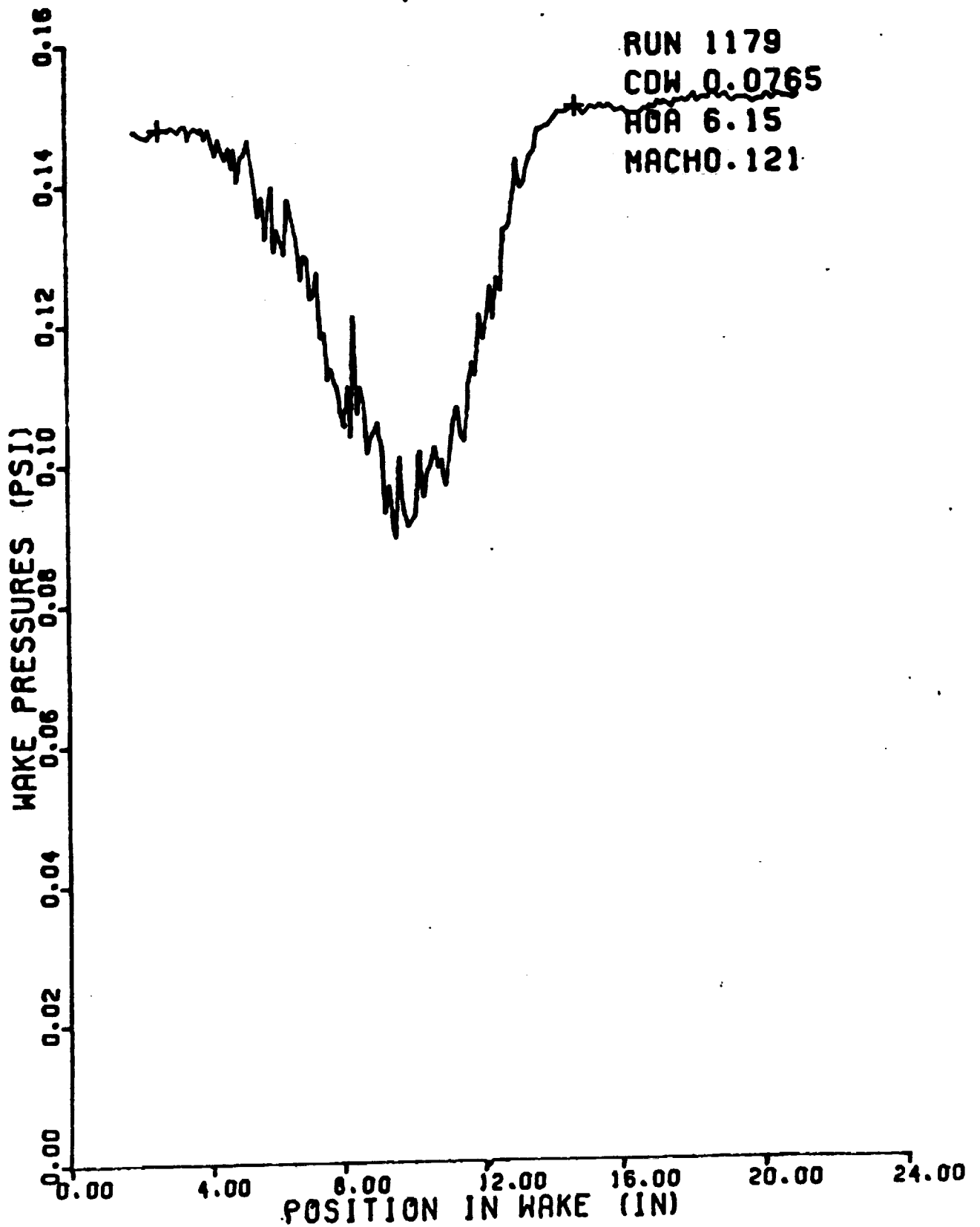


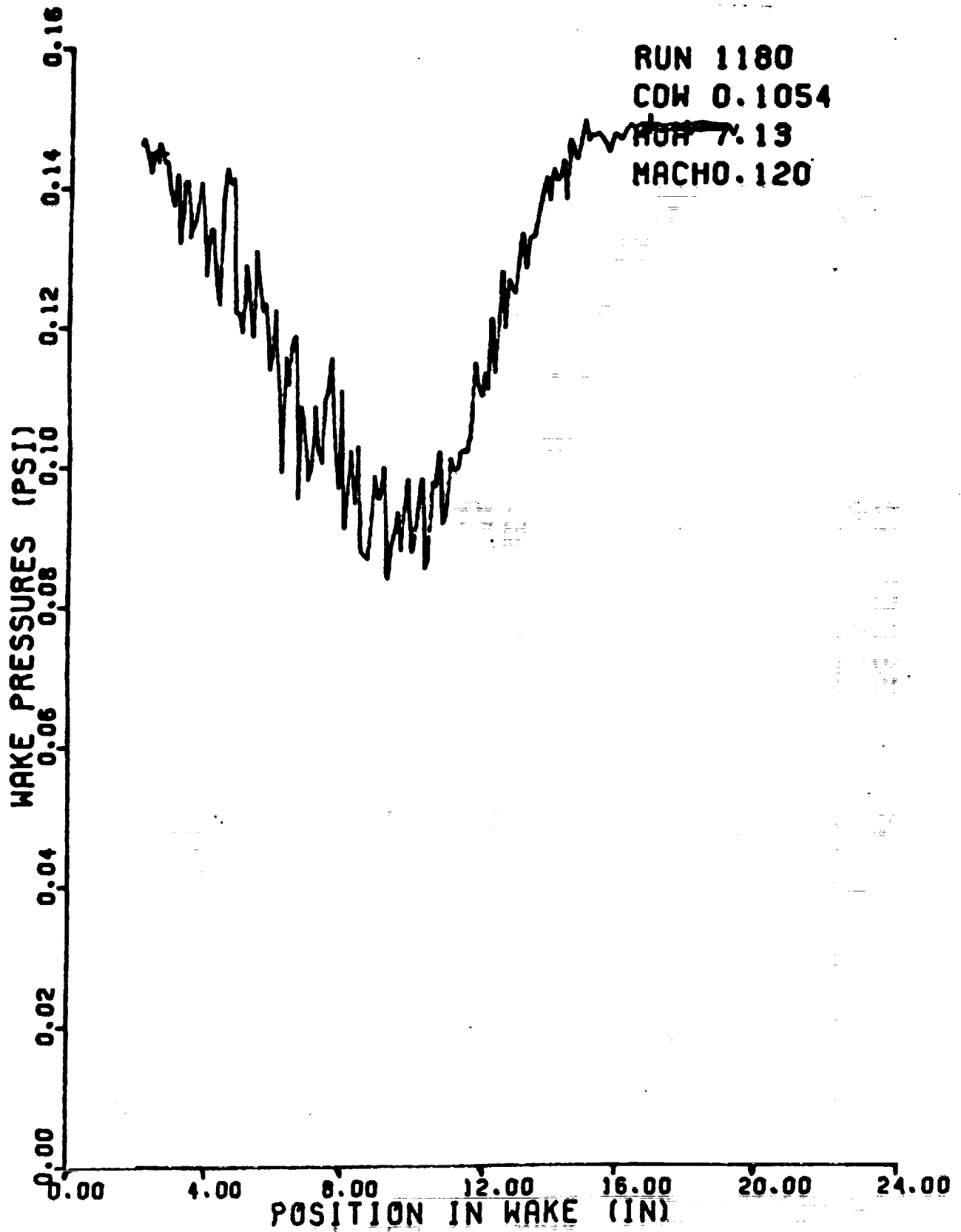


RUN 1176

AOA 3.09
M 0.12
RE 1.56
CL 0.291
CDW 0.0352
CM 0.0084

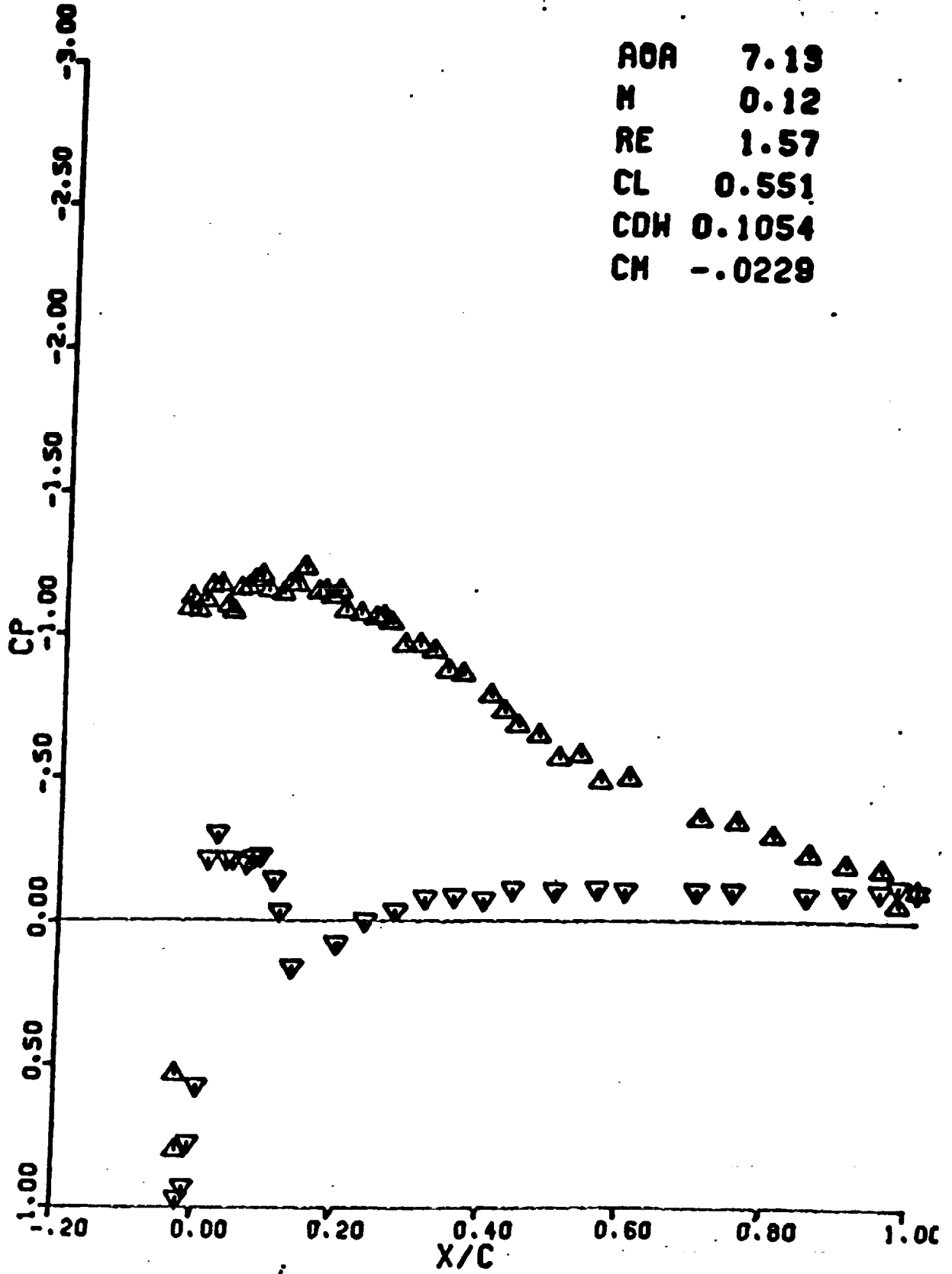






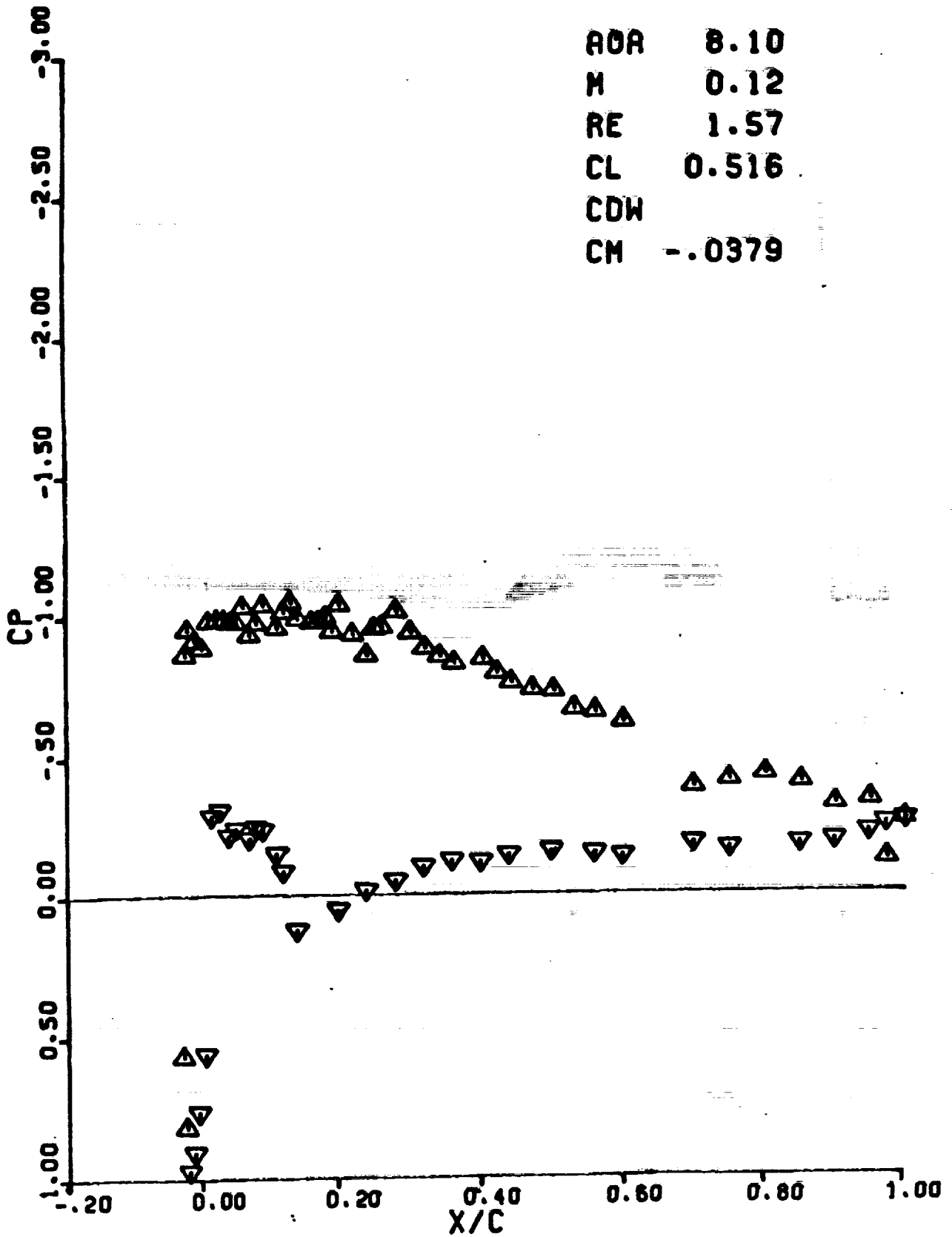
RUN 1180

AOA 7.19
M 0.12
RE 1.57
CL 0.551
CDW 0.1054
CM -0.0229



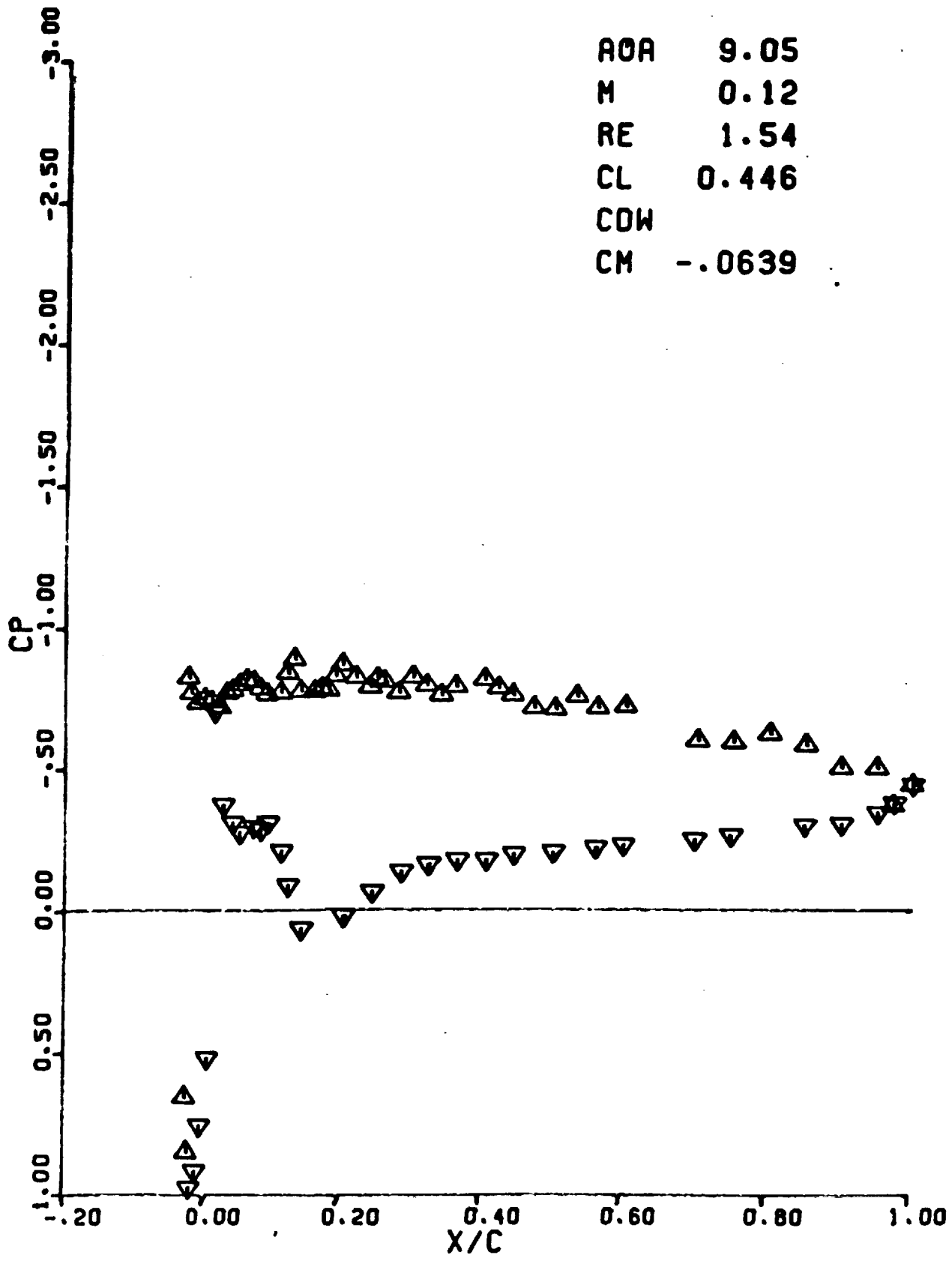
RUN 1181

AOA 8.10
M 0.12
RE 1.57
CL 0.516
CDW
CM -.0379



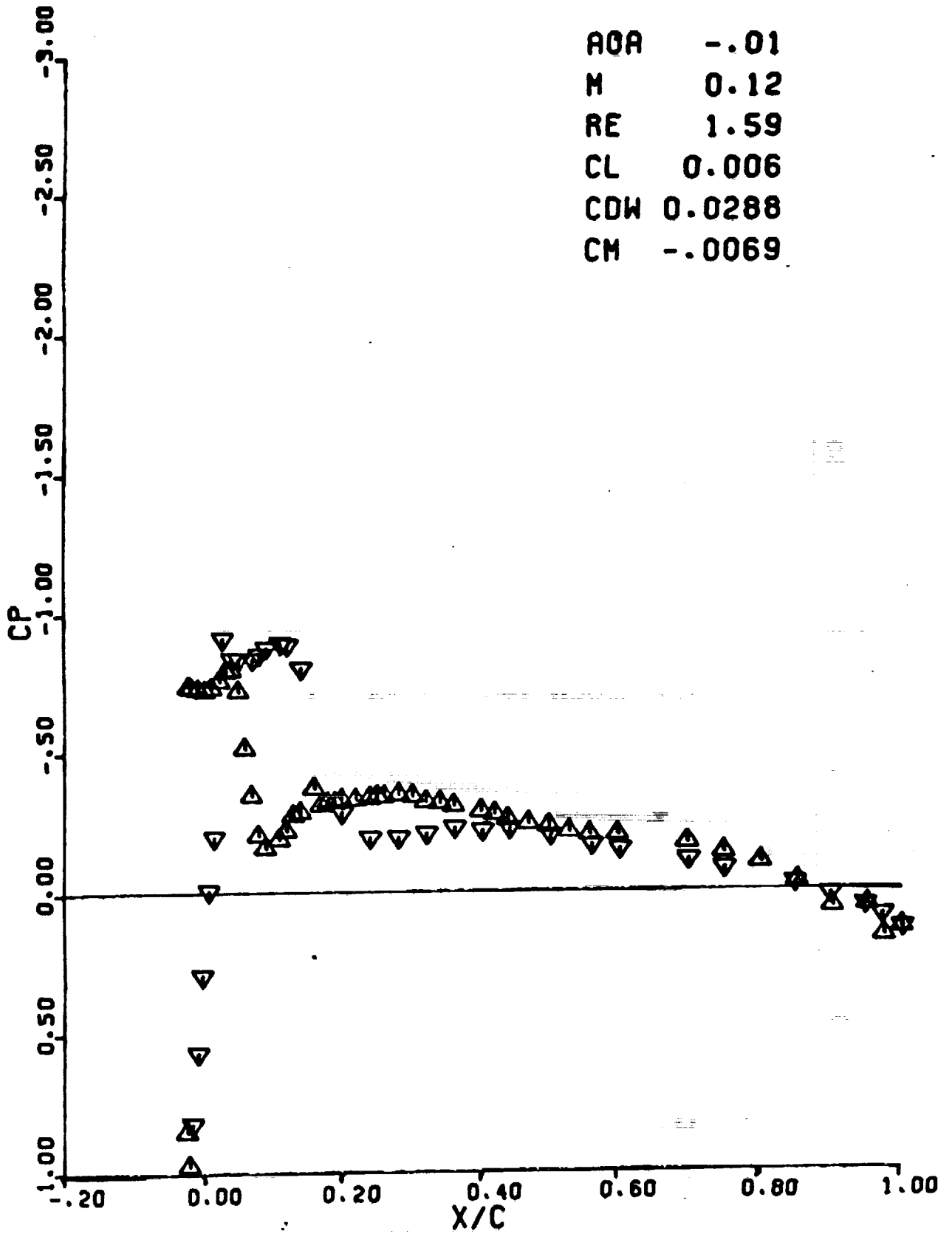
RUN 1182

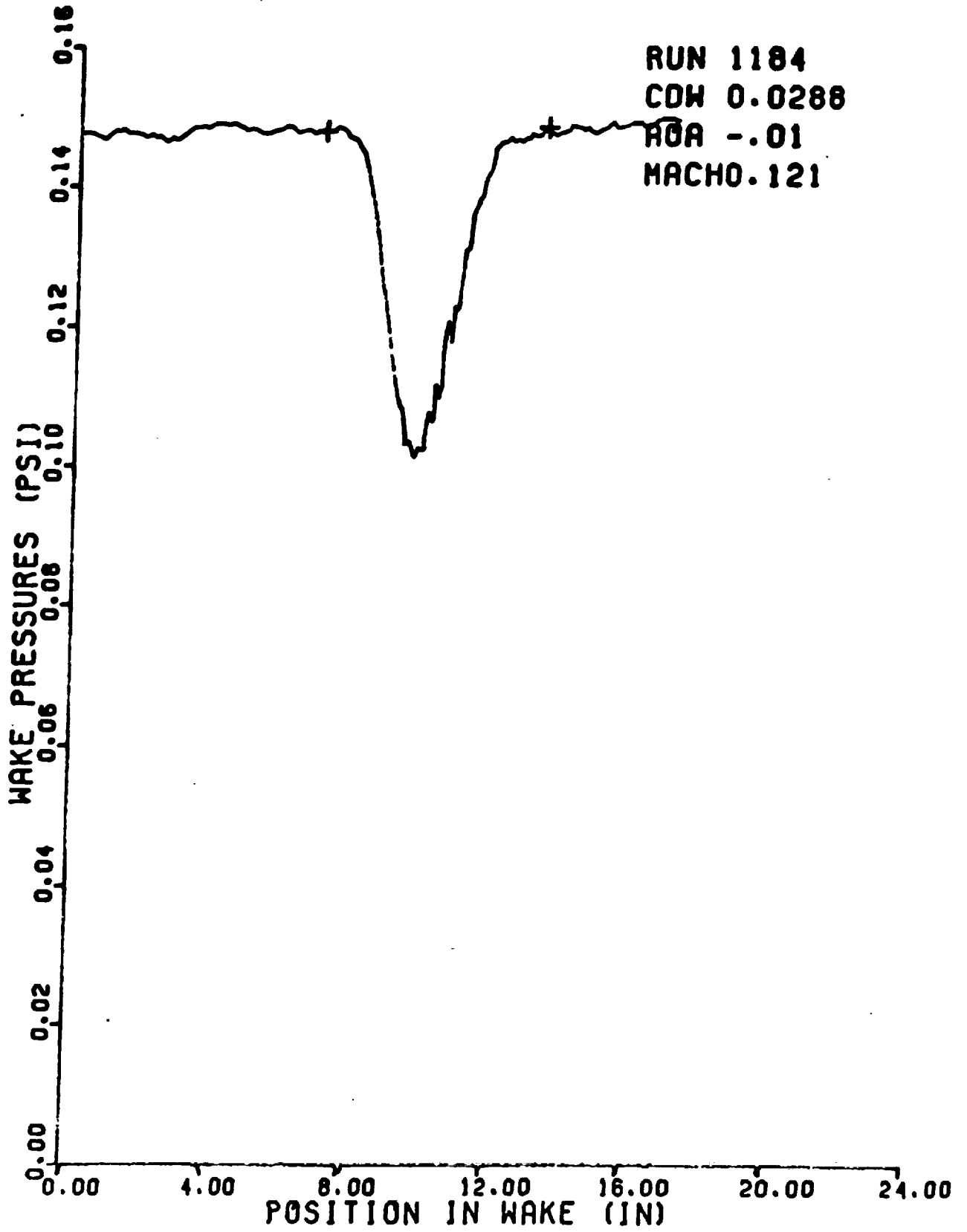
AOA 9.05
M 0.12
RE 1.54
CL 0.446
CDW
CM -.0639



RUN 1184

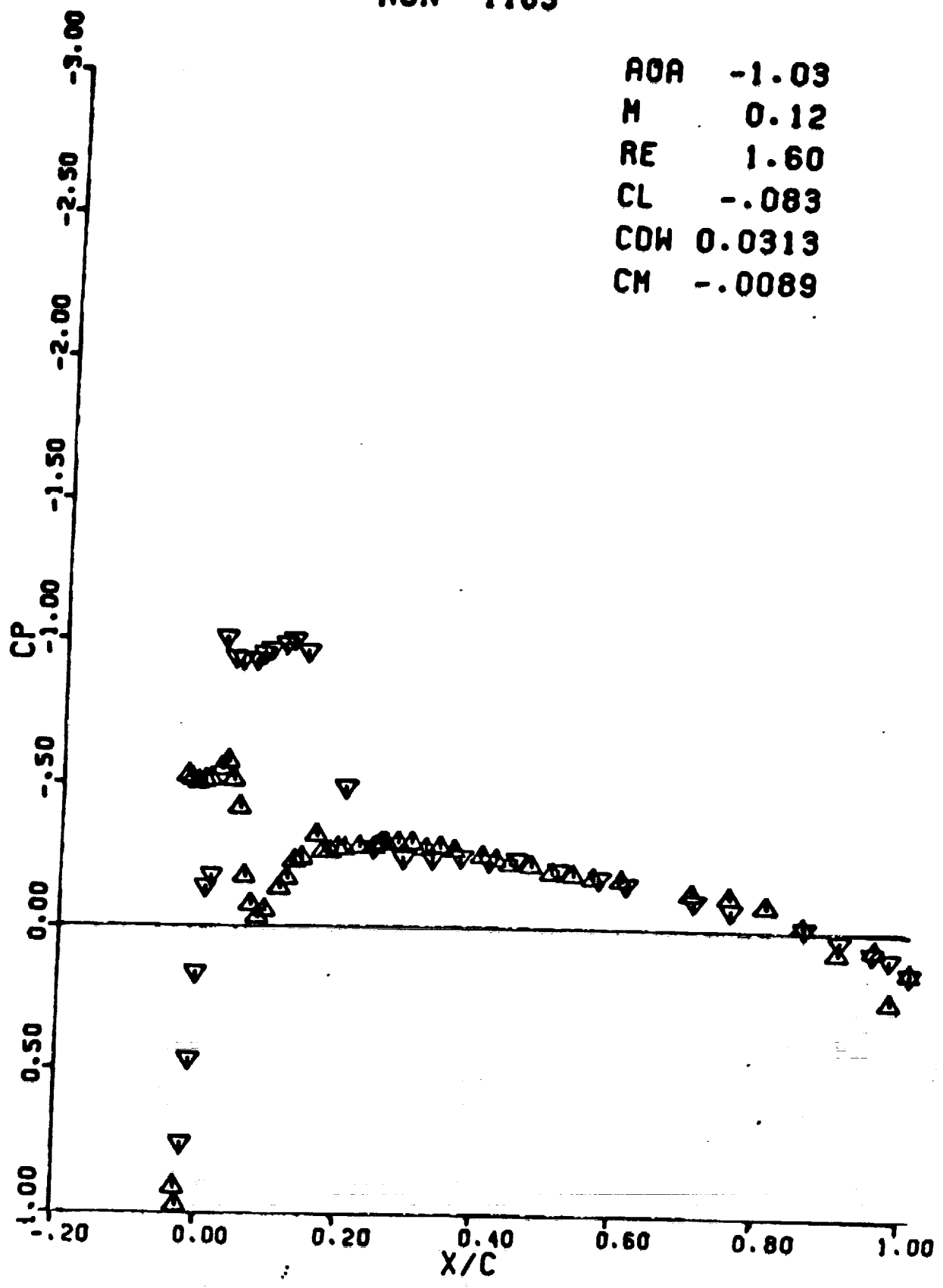
AOA -.01
M 0.12
RE 1.59
CL 0.006
CDW 0.0288
CM -.0069

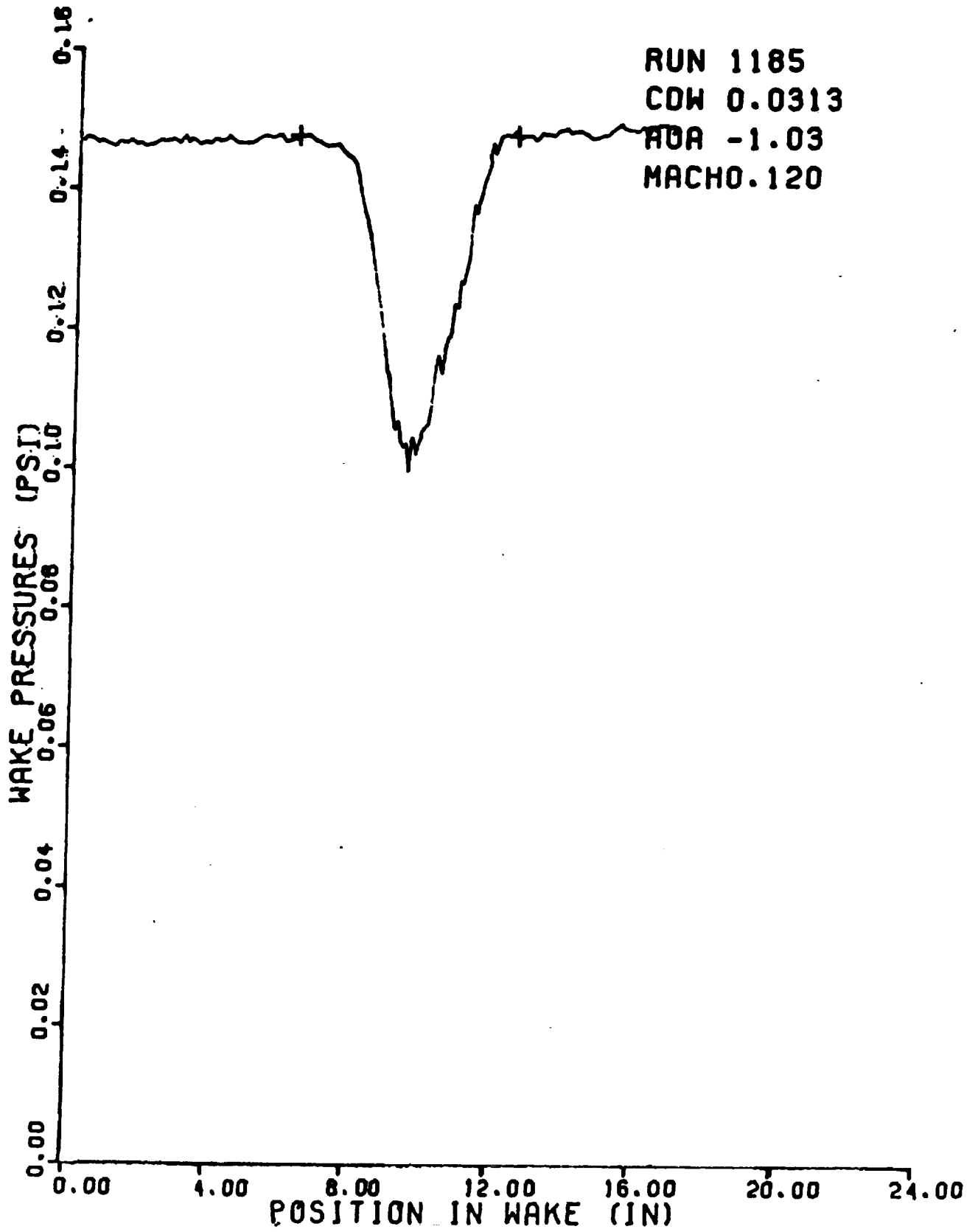




RUN 1185

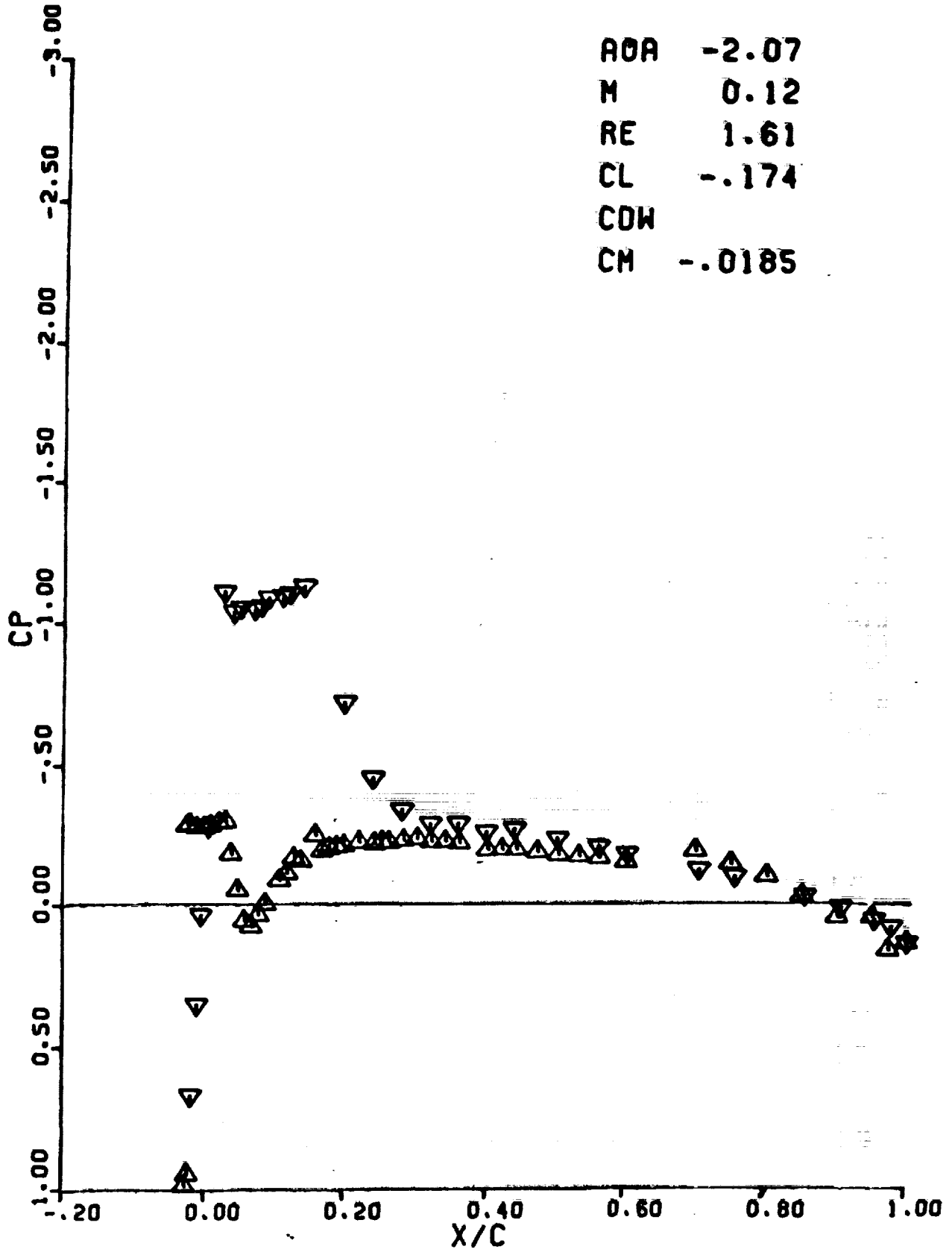
AOA -1.03
M 0.12
RE 1.60
CL -.083
CDW 0.0313
CM -.0089





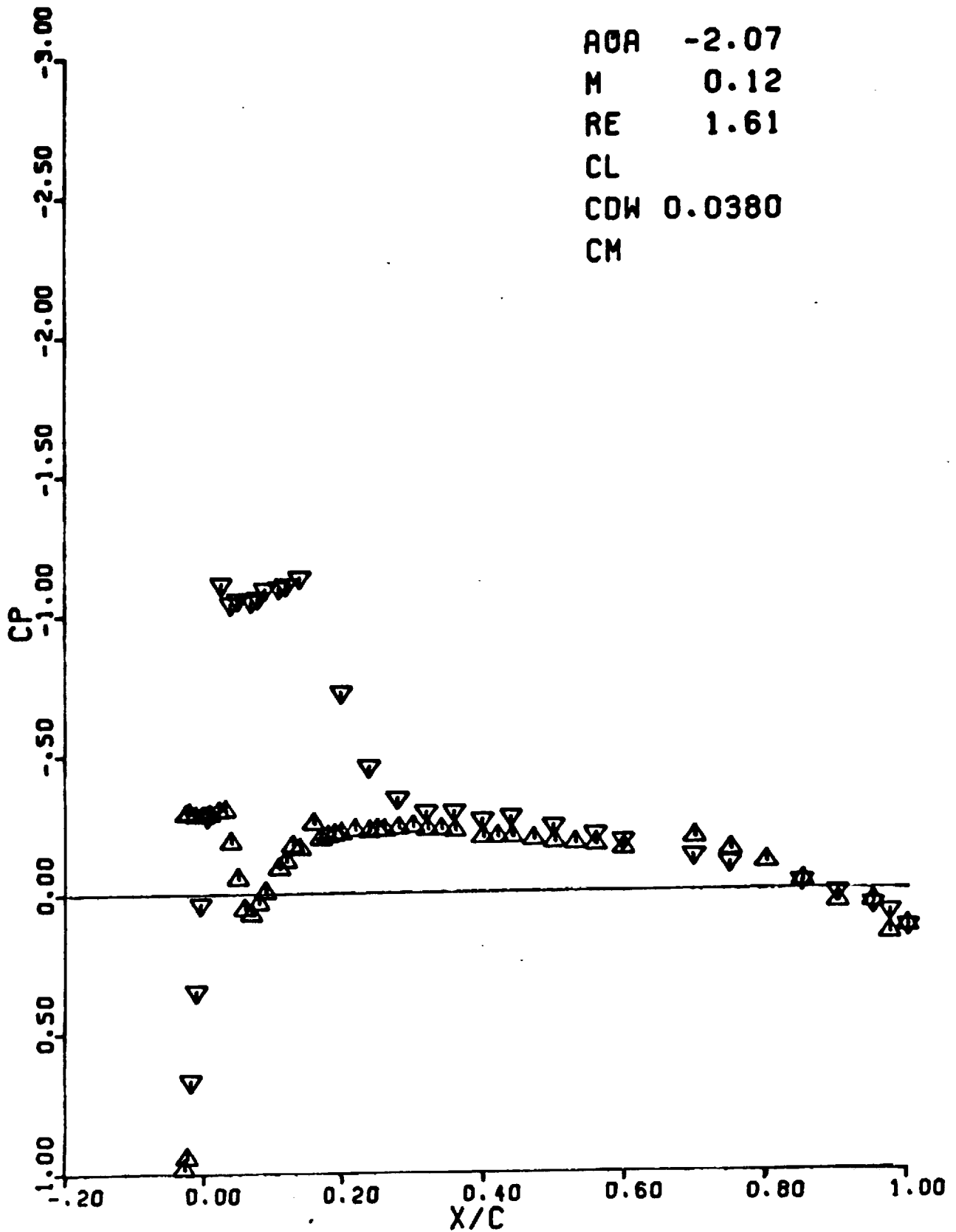
RUN 1186

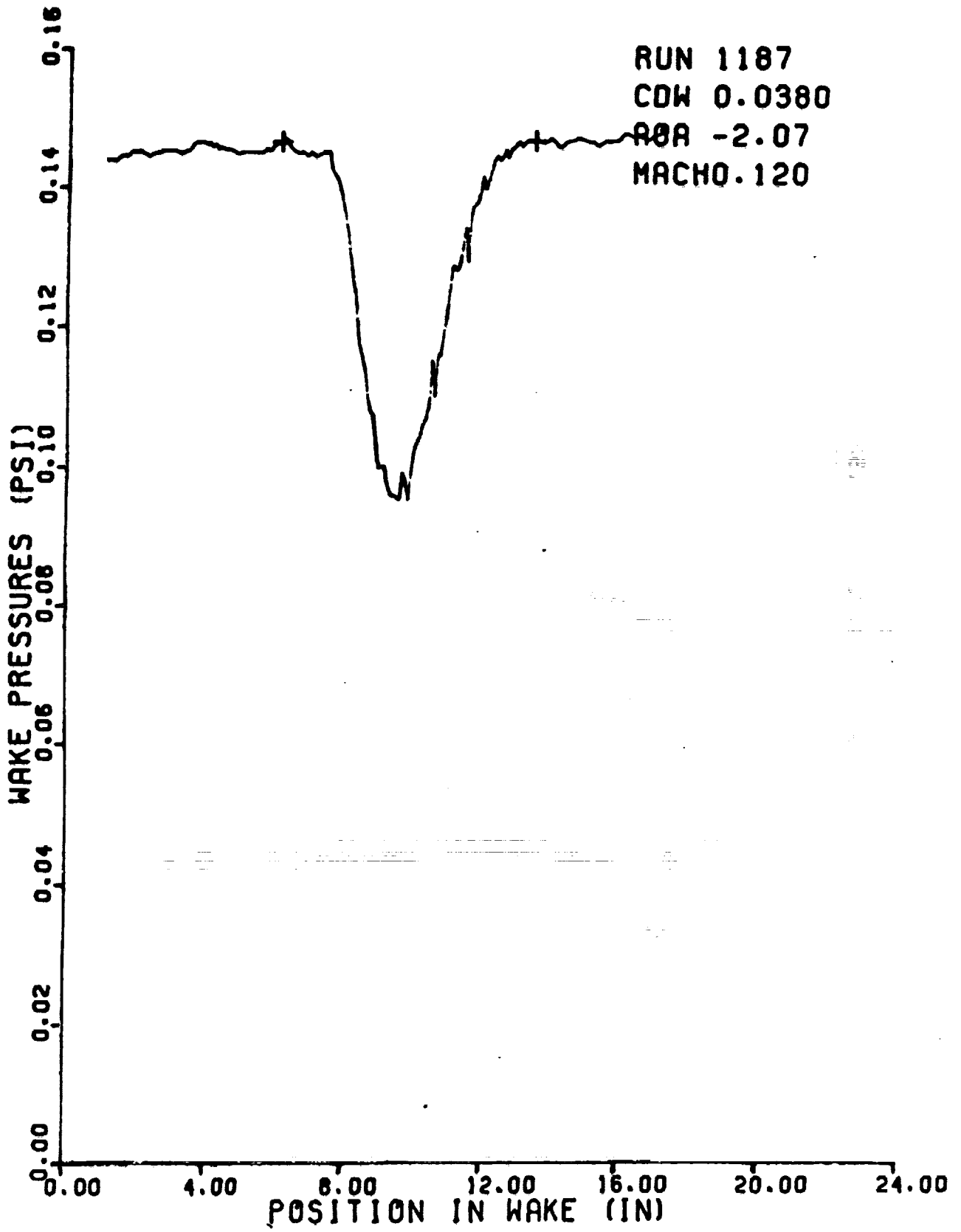
AOA -2.07
M 0.12
RE 1.61
CL -.174
CDW
CM -.0185



RUN 1187

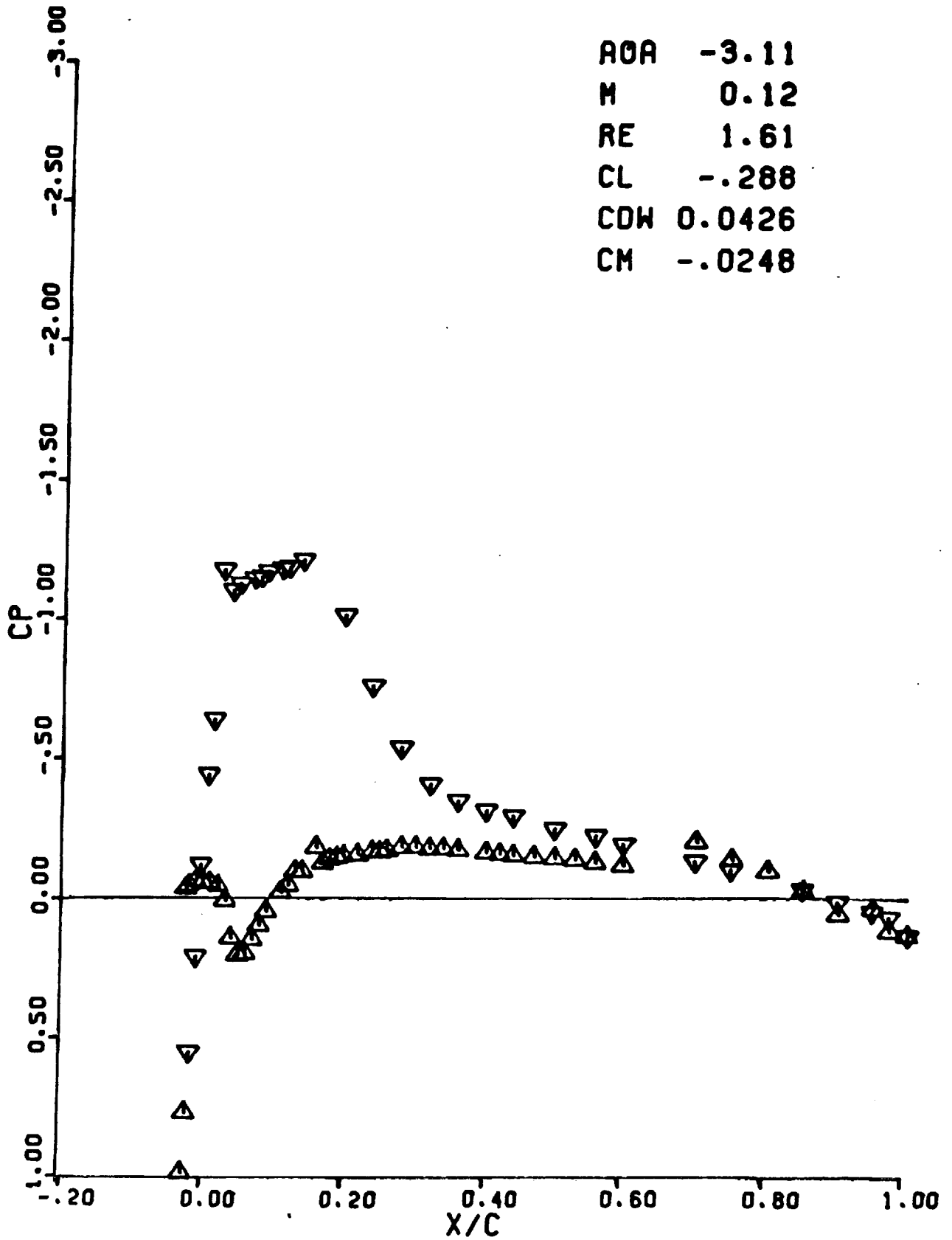
AOA -2.07
M 0.12
RE 1.61
CL
CDW 0.0380
CM

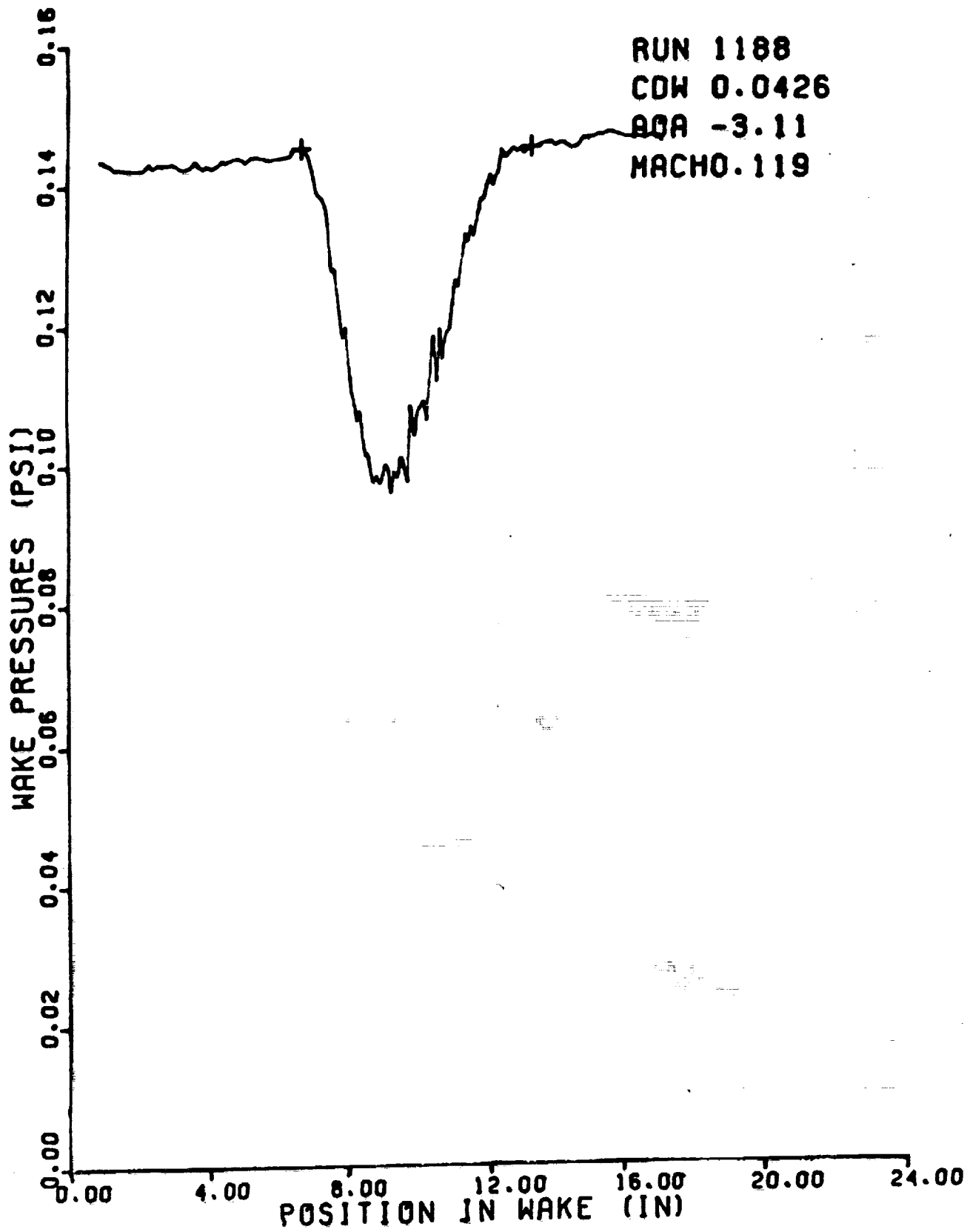


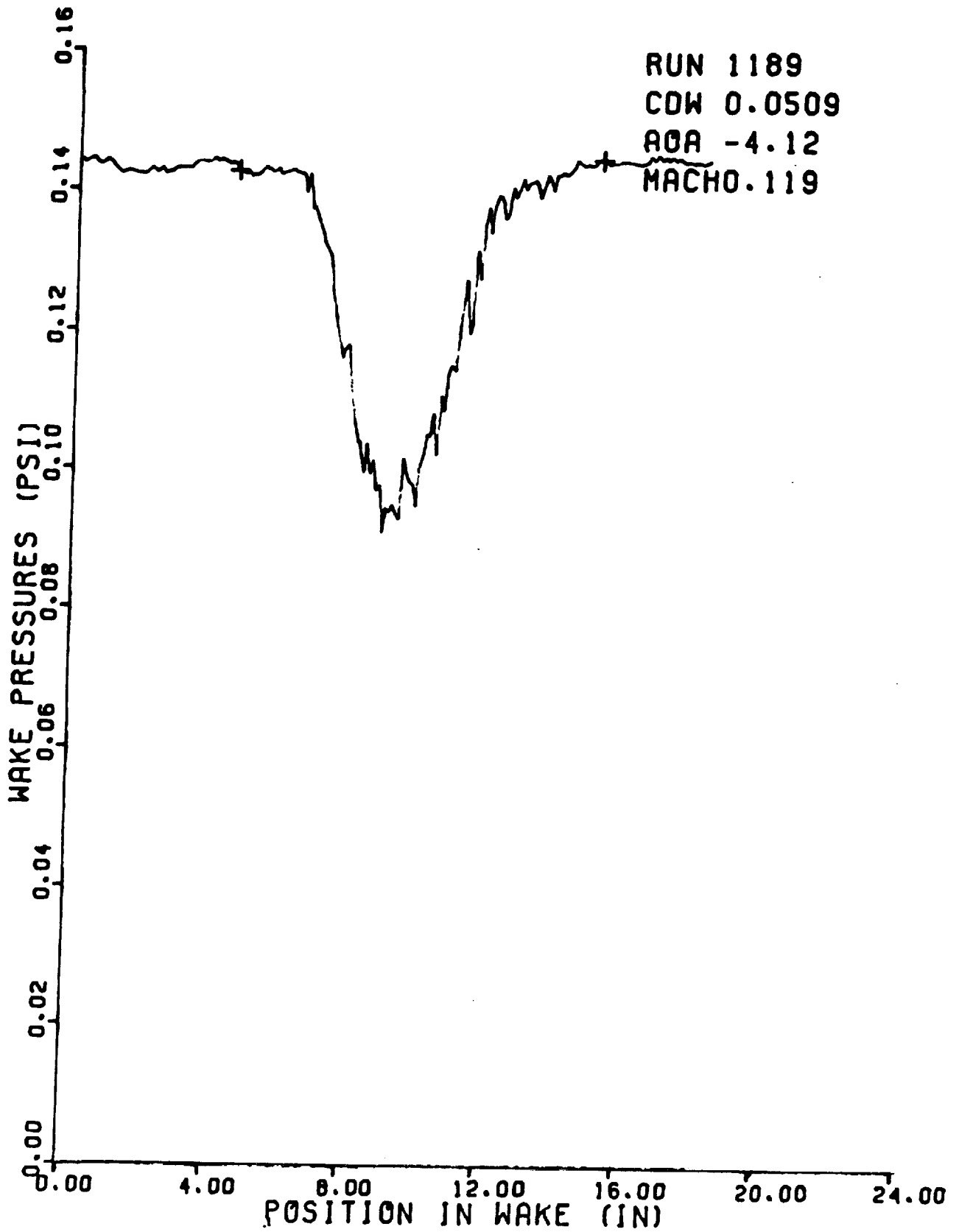


RUN 1188

AOA -3.11
M 0.12
RE 1.61
CL -.288
CDW 0.0426
CM -.0248

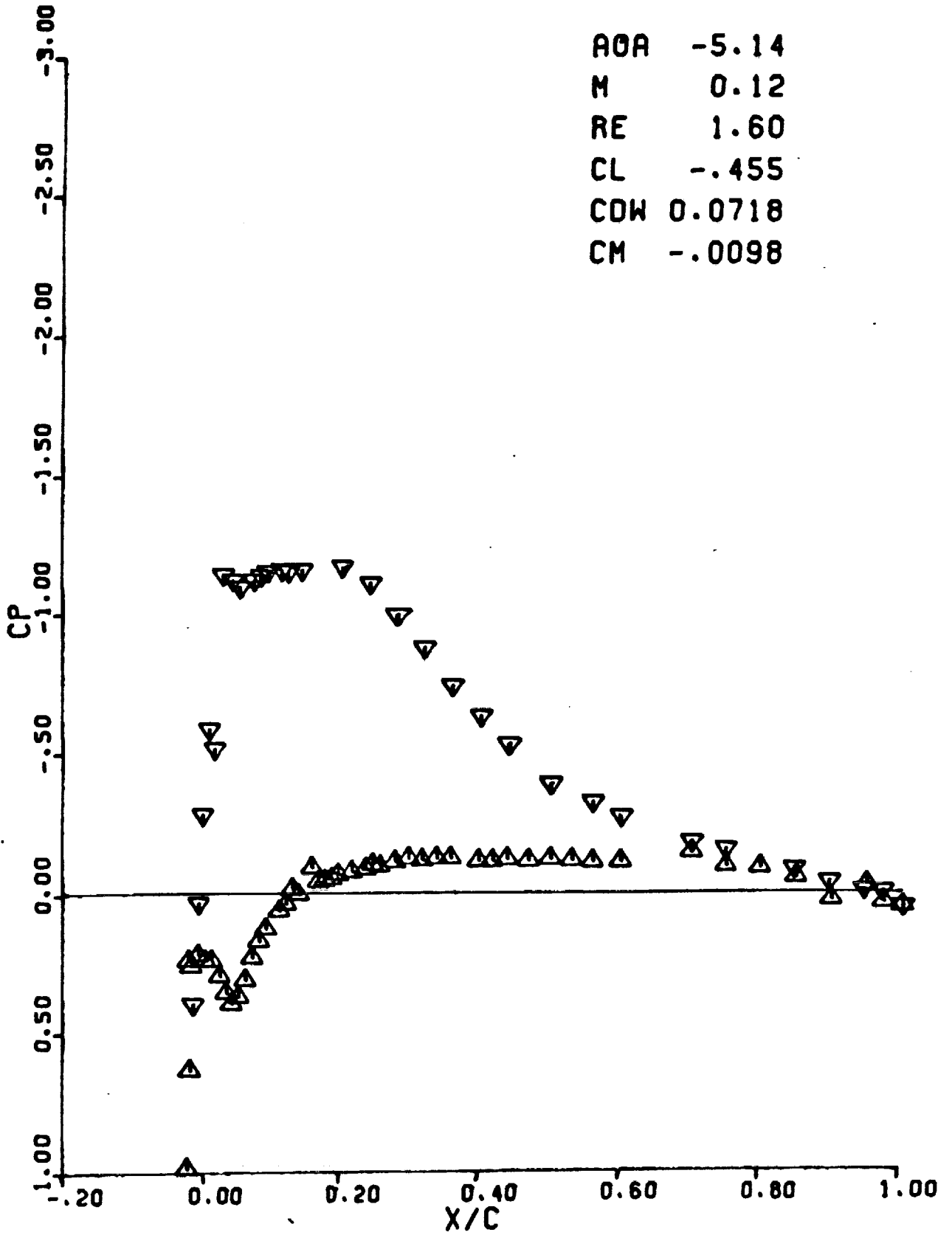


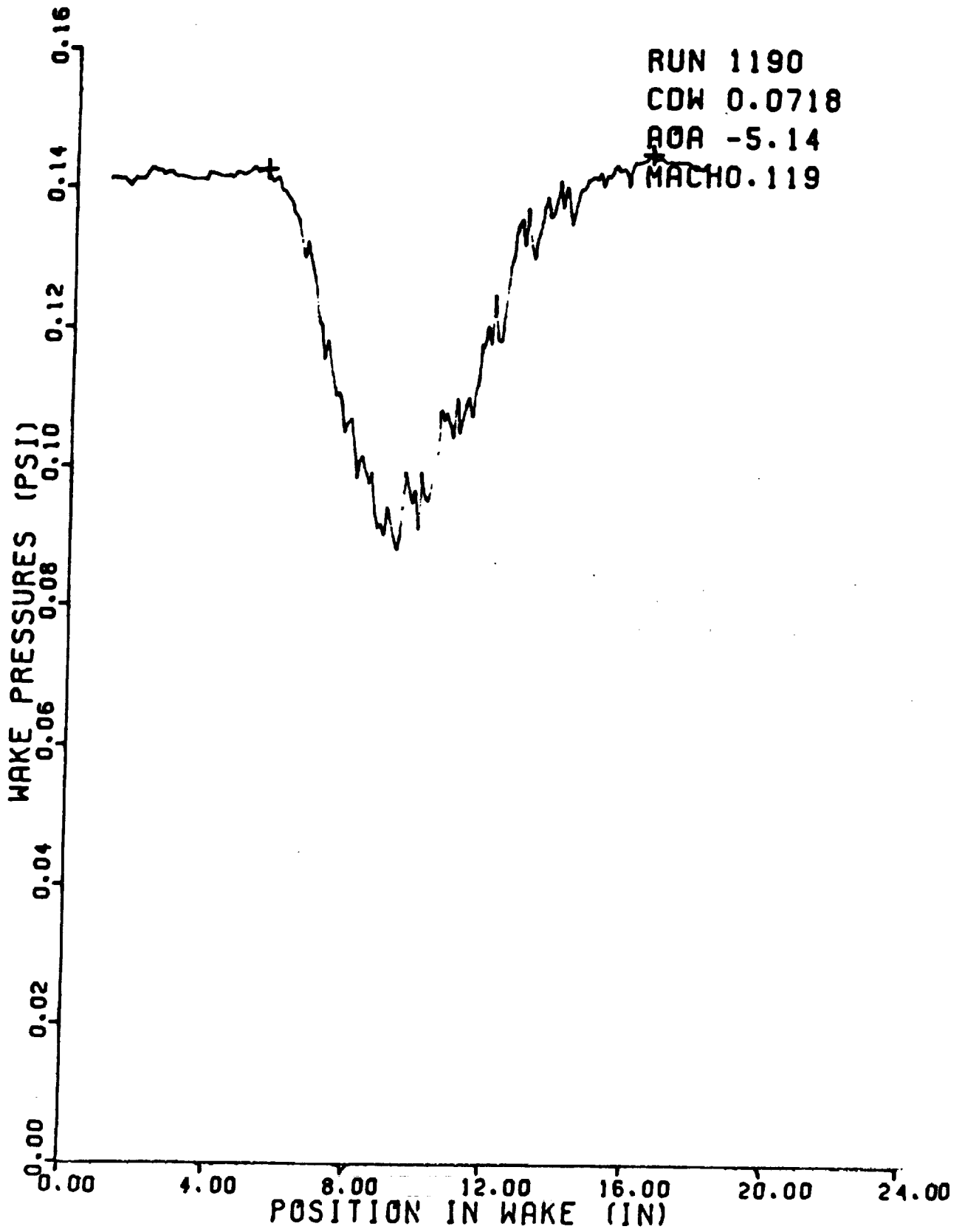




RUN 1190

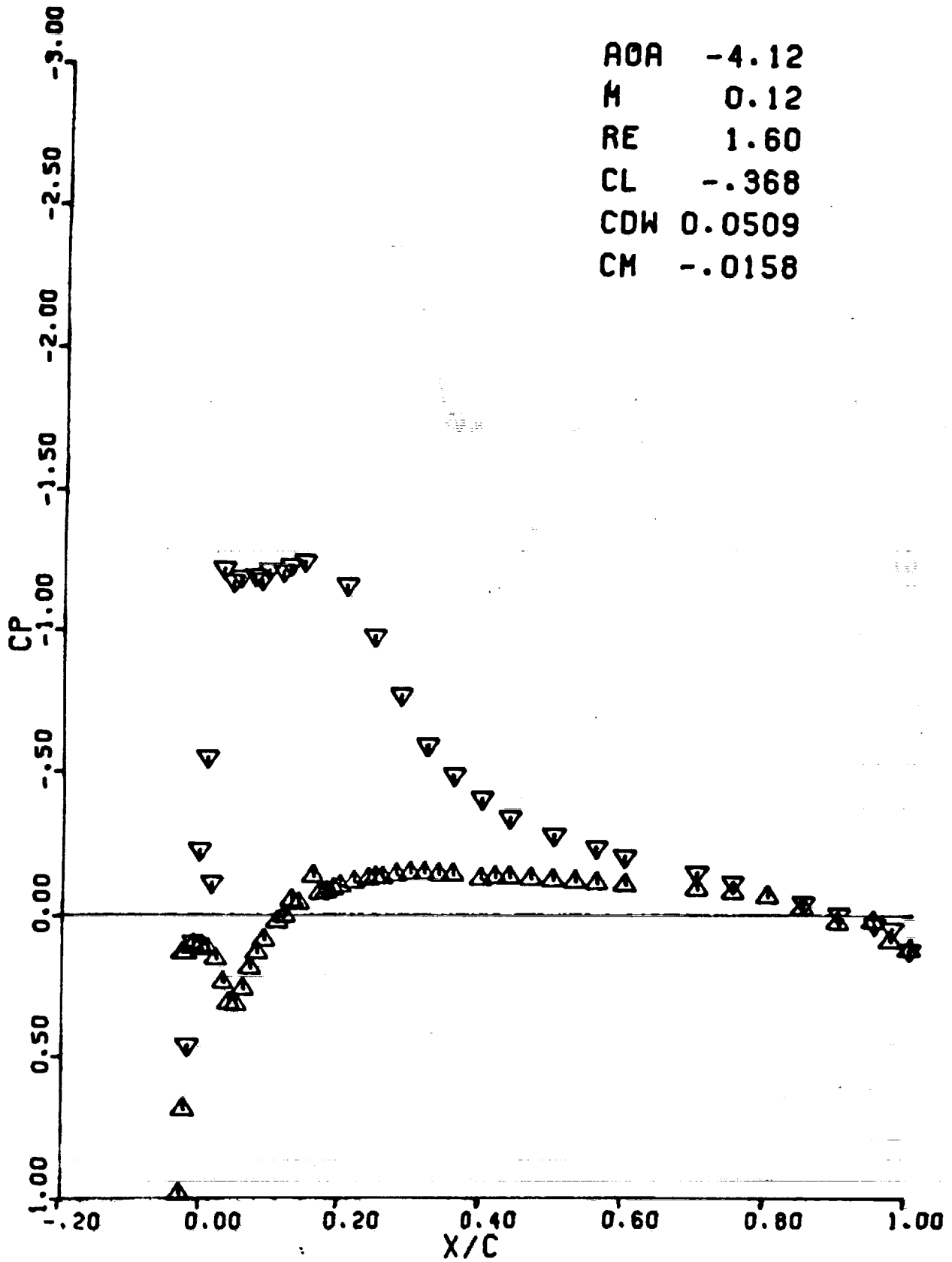
AOA -5.14
M 0.12
RE 1.60
CL -.455
CDW 0.0718
CM -.0098





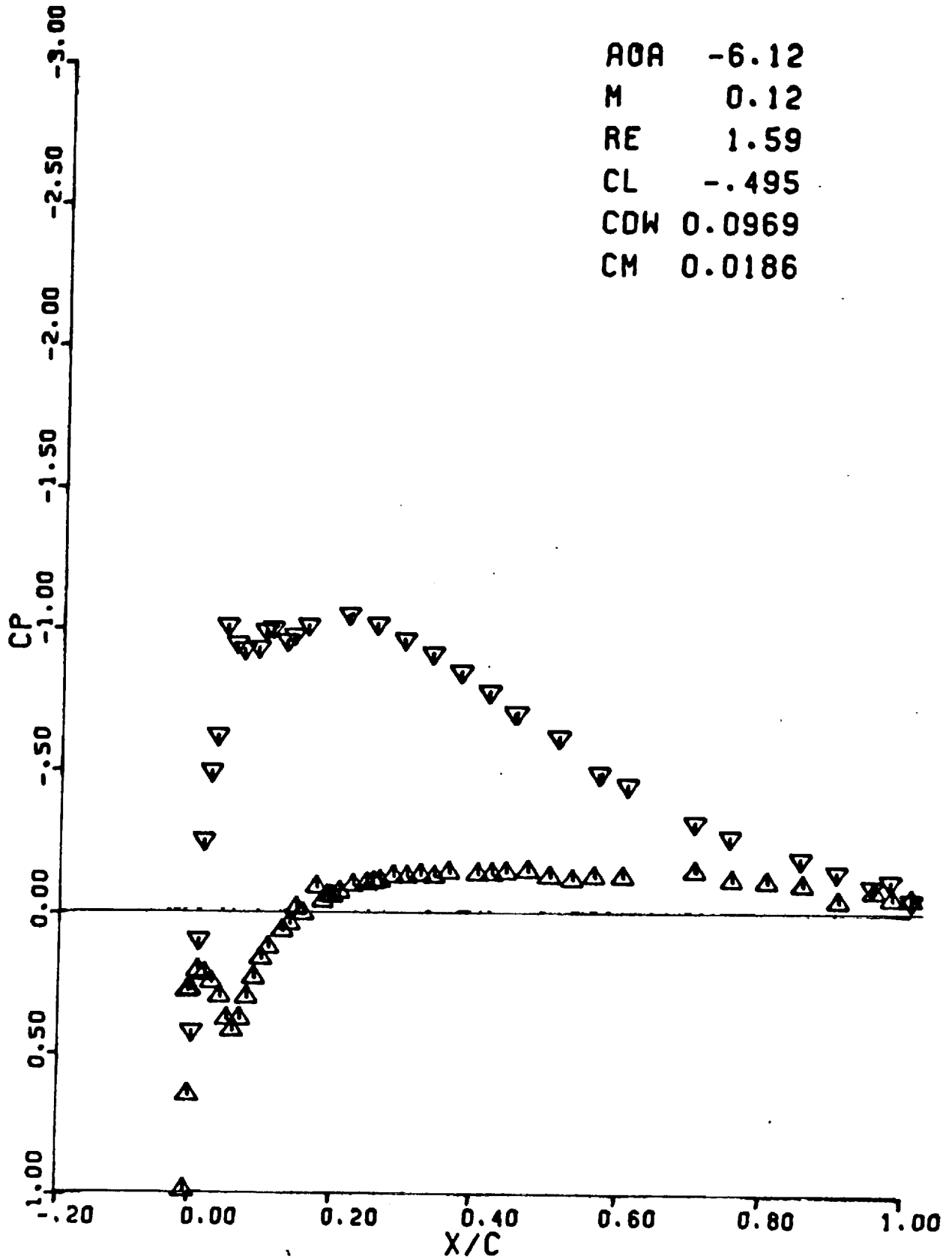
RUN 1189

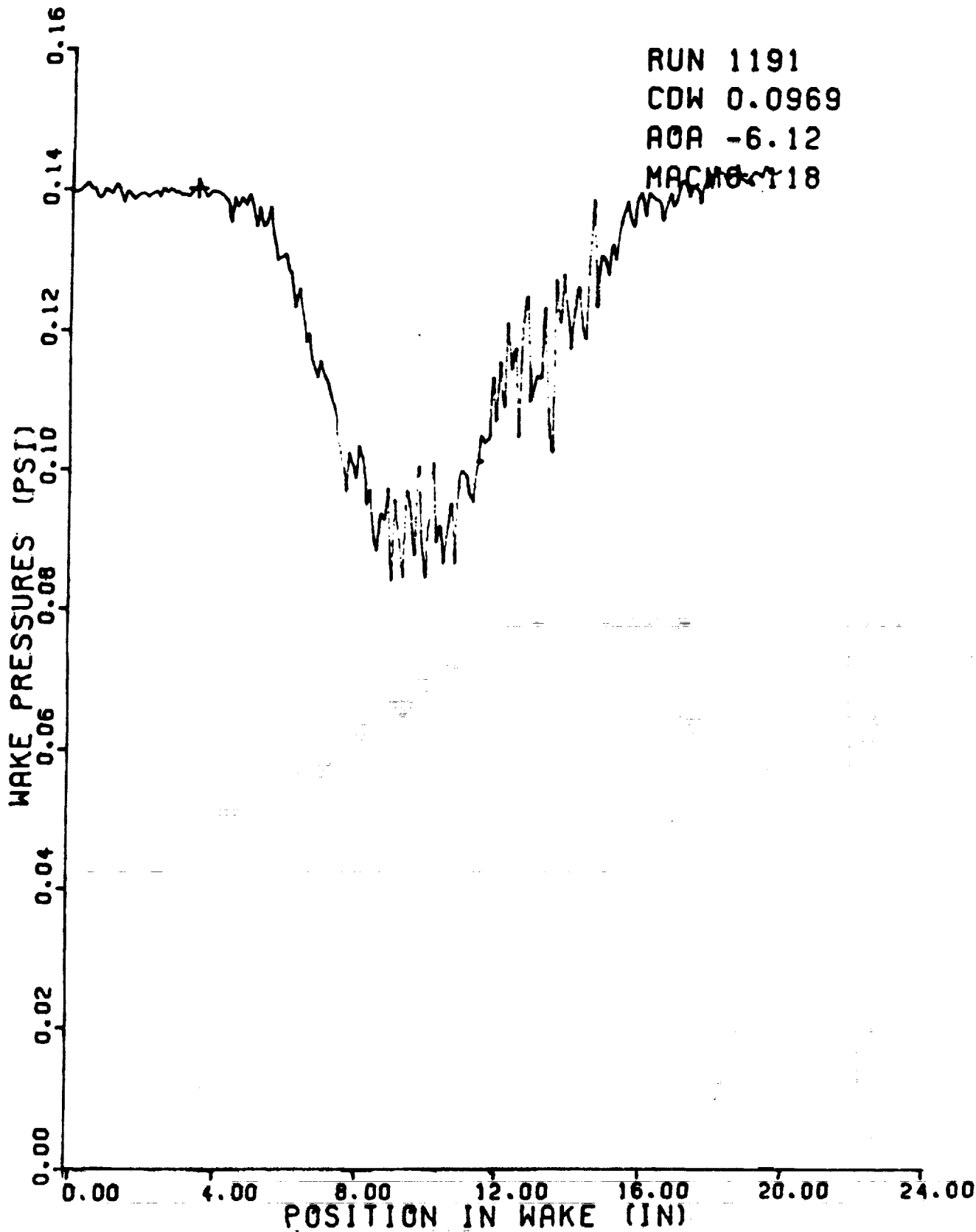
AOA -4.12
M 0.12
RE 1.60
CL -.368
CDW 0.0509
CM -.0158



RUN 1191

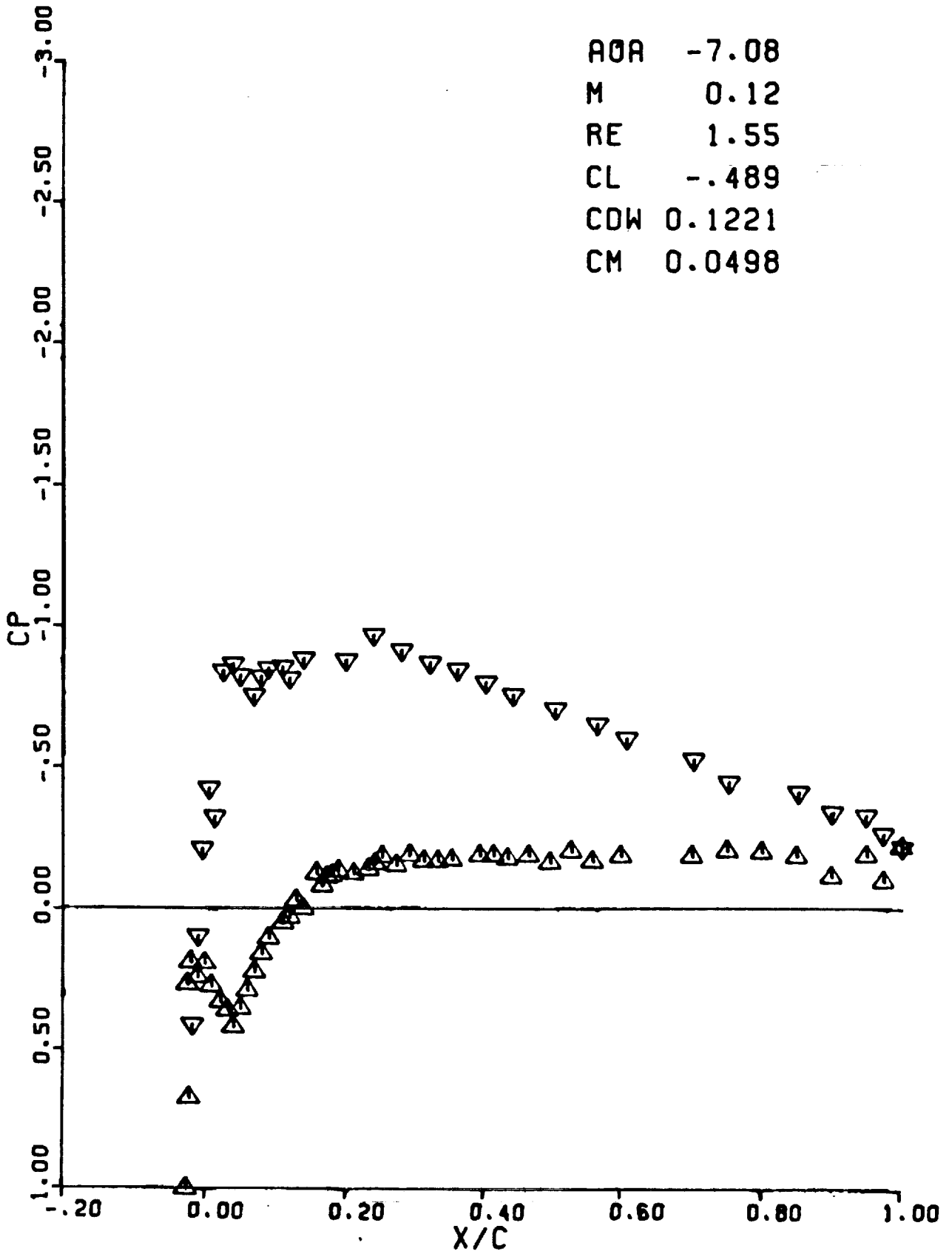
AOA -6.12
M 0.12
RE 1.59
CL -.495
CDW 0.0969
CM 0.0186

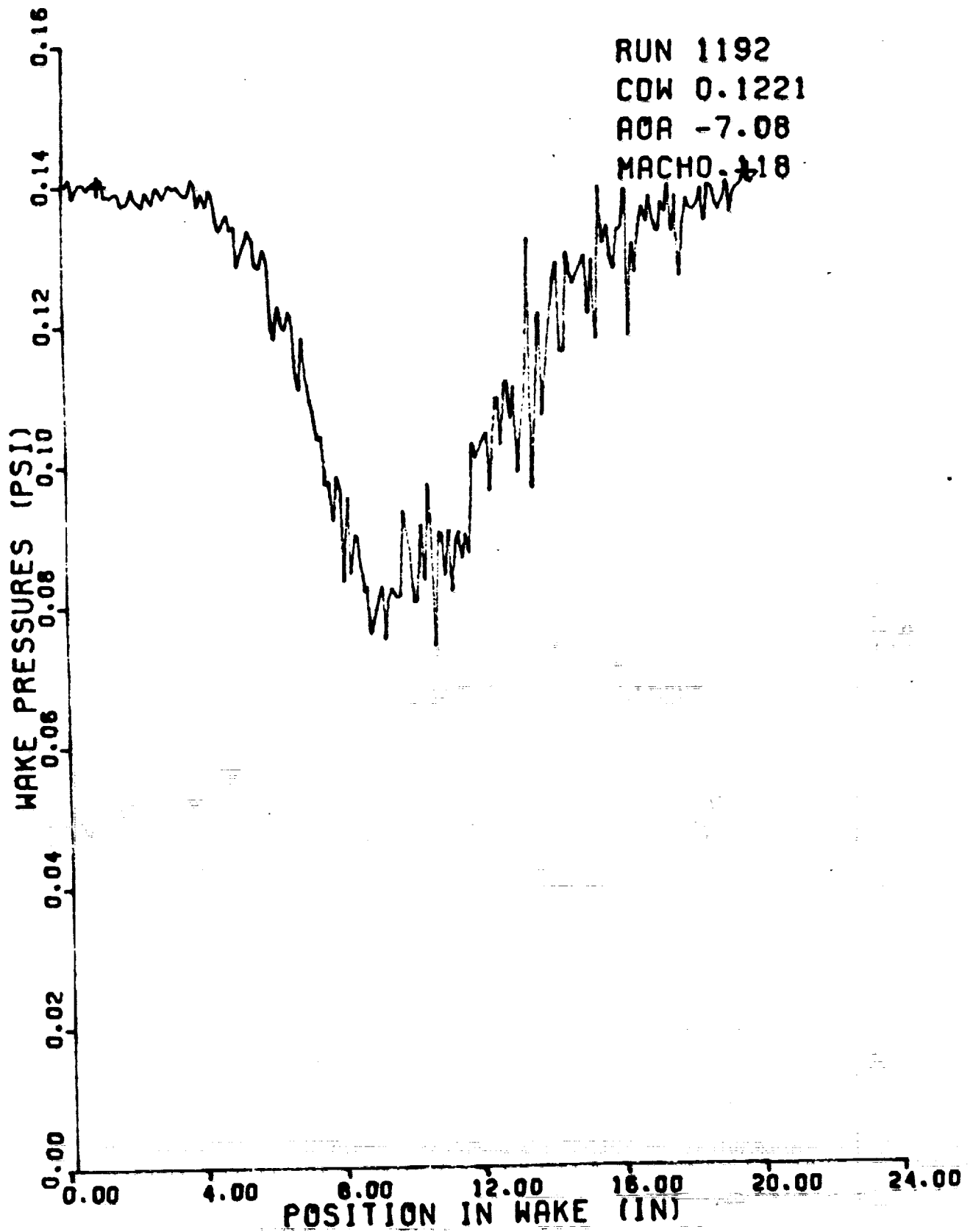




RUN 1192

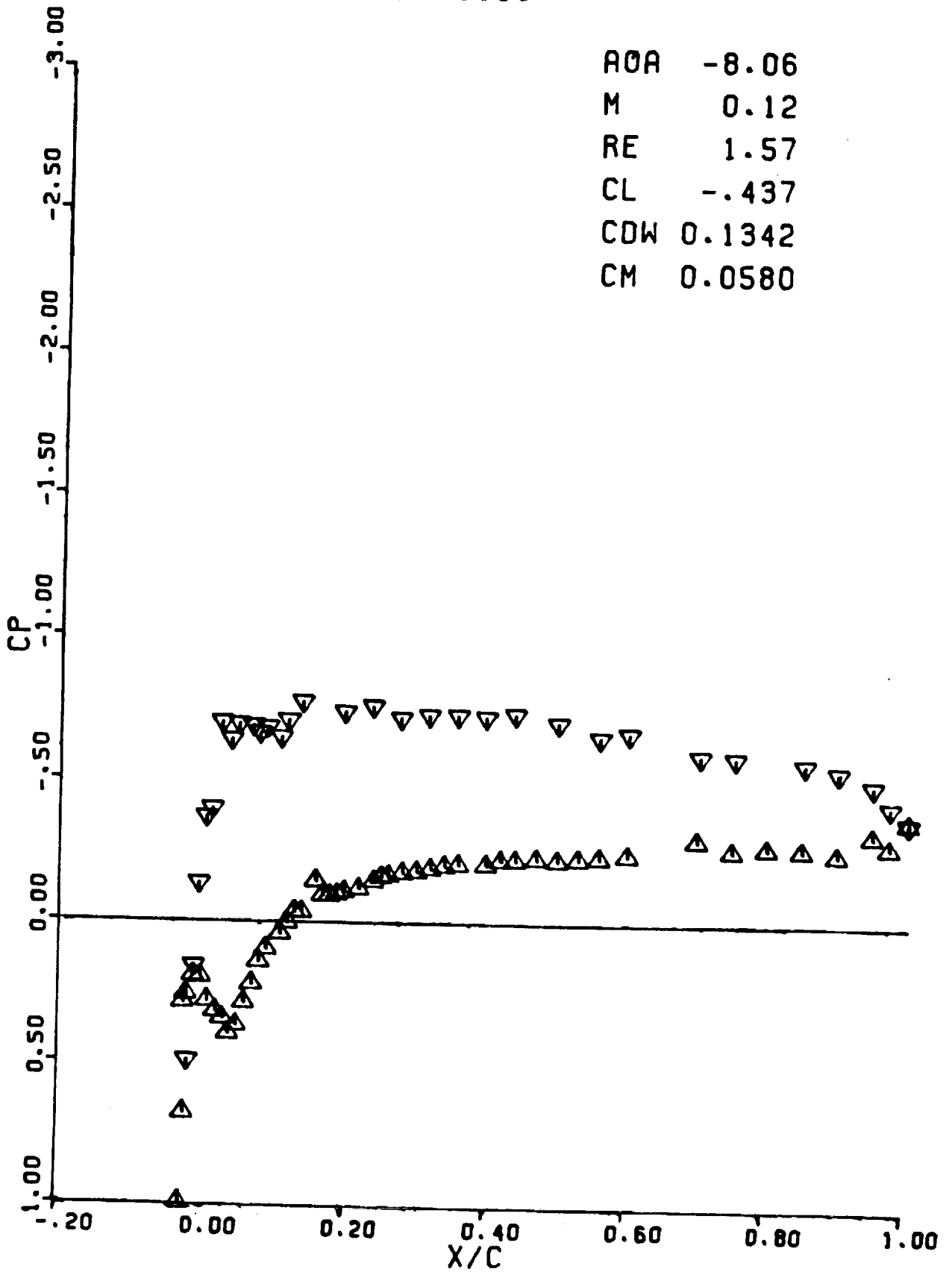
AOA -7.08
M 0.12
RE 1.55
CL -.489
CDW 0.1221
CM 0.0498

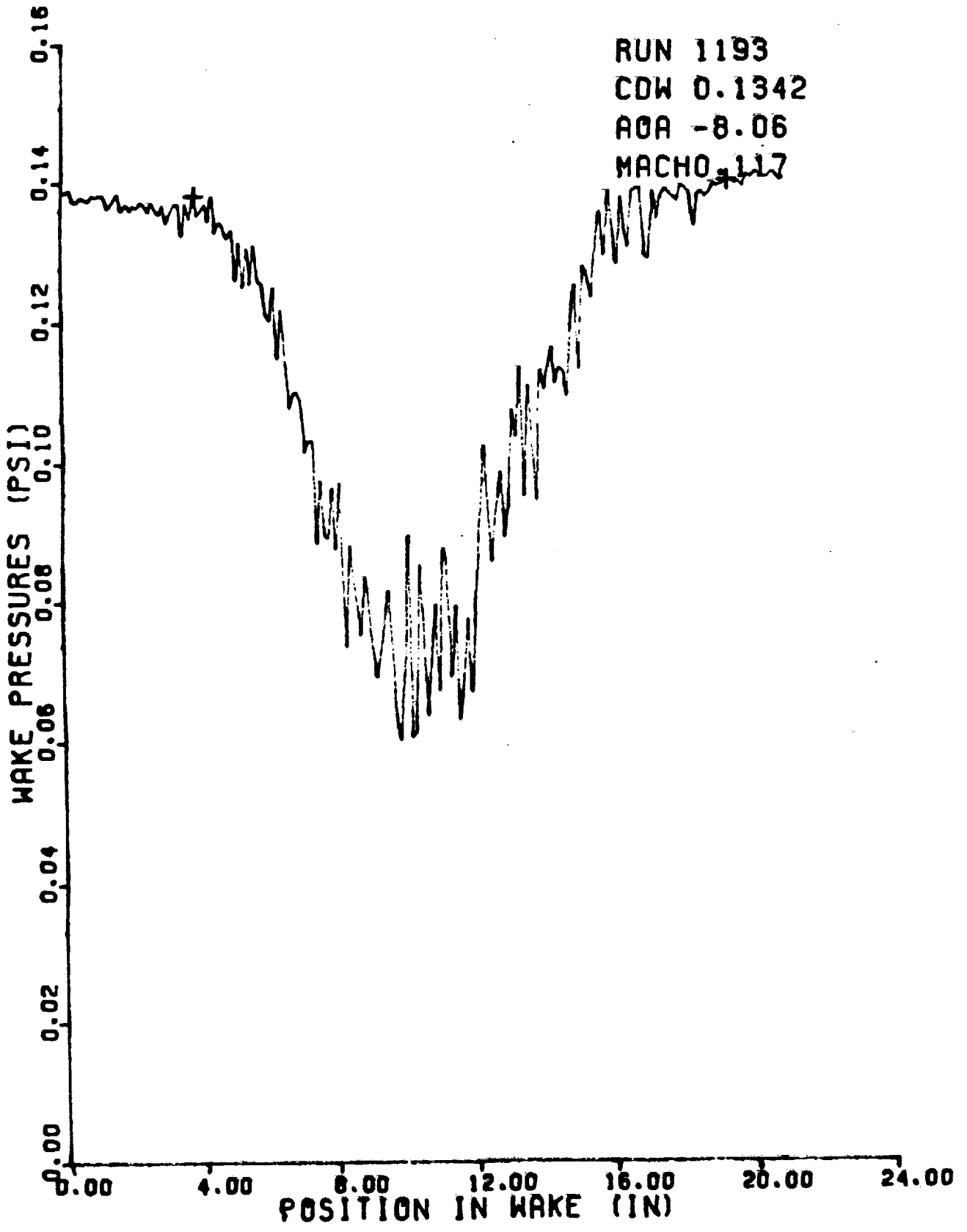




RUN 1193

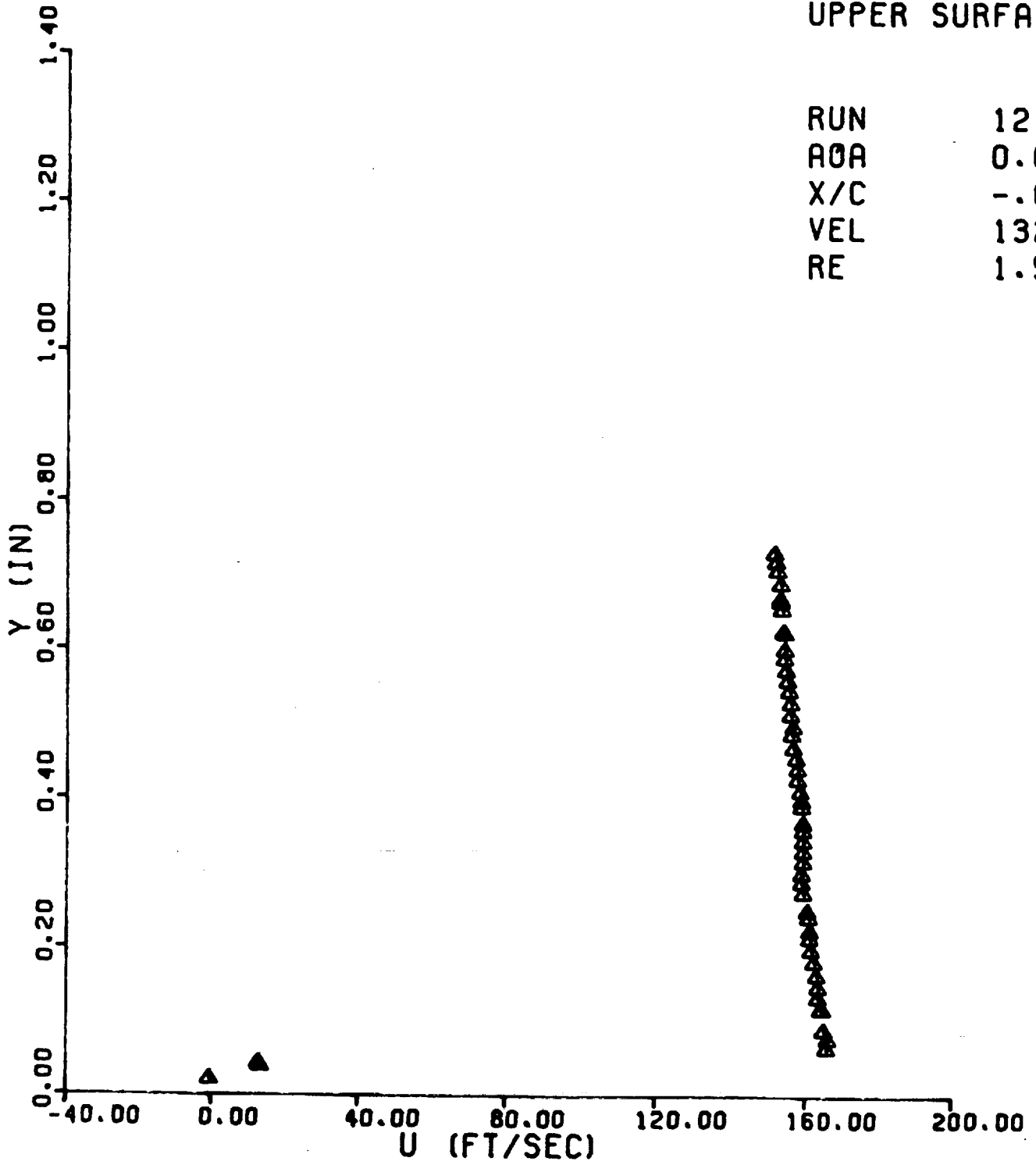
AOA -8.06
M 0.12
RE 1.57
CL -.437
CDW 0.1342
CM 0.0580





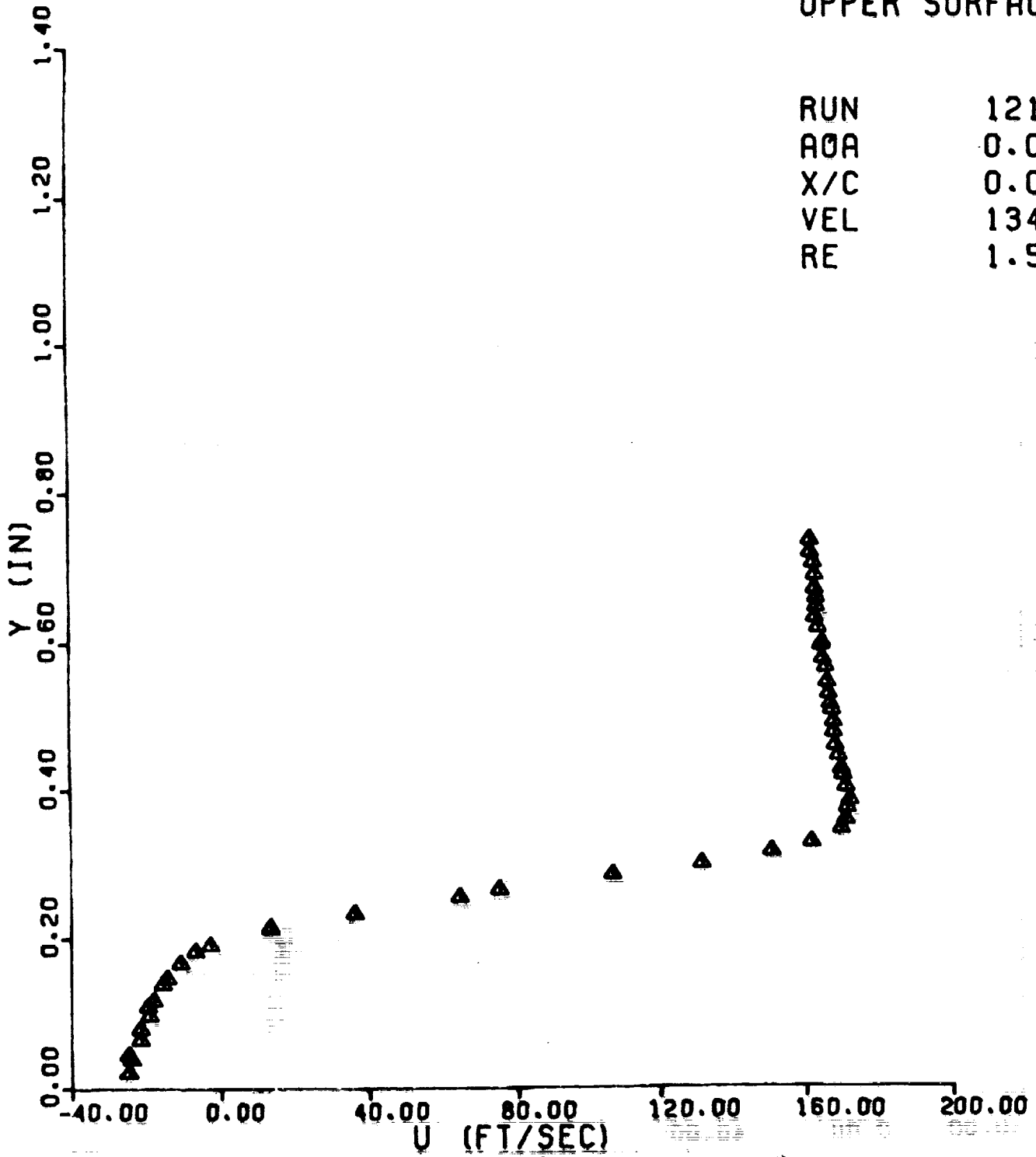
NACA 0012
UPPER SURFACE

RUN 1218
AOA 0.000
X/C -.0200
VEL 132.9
RE 1.51



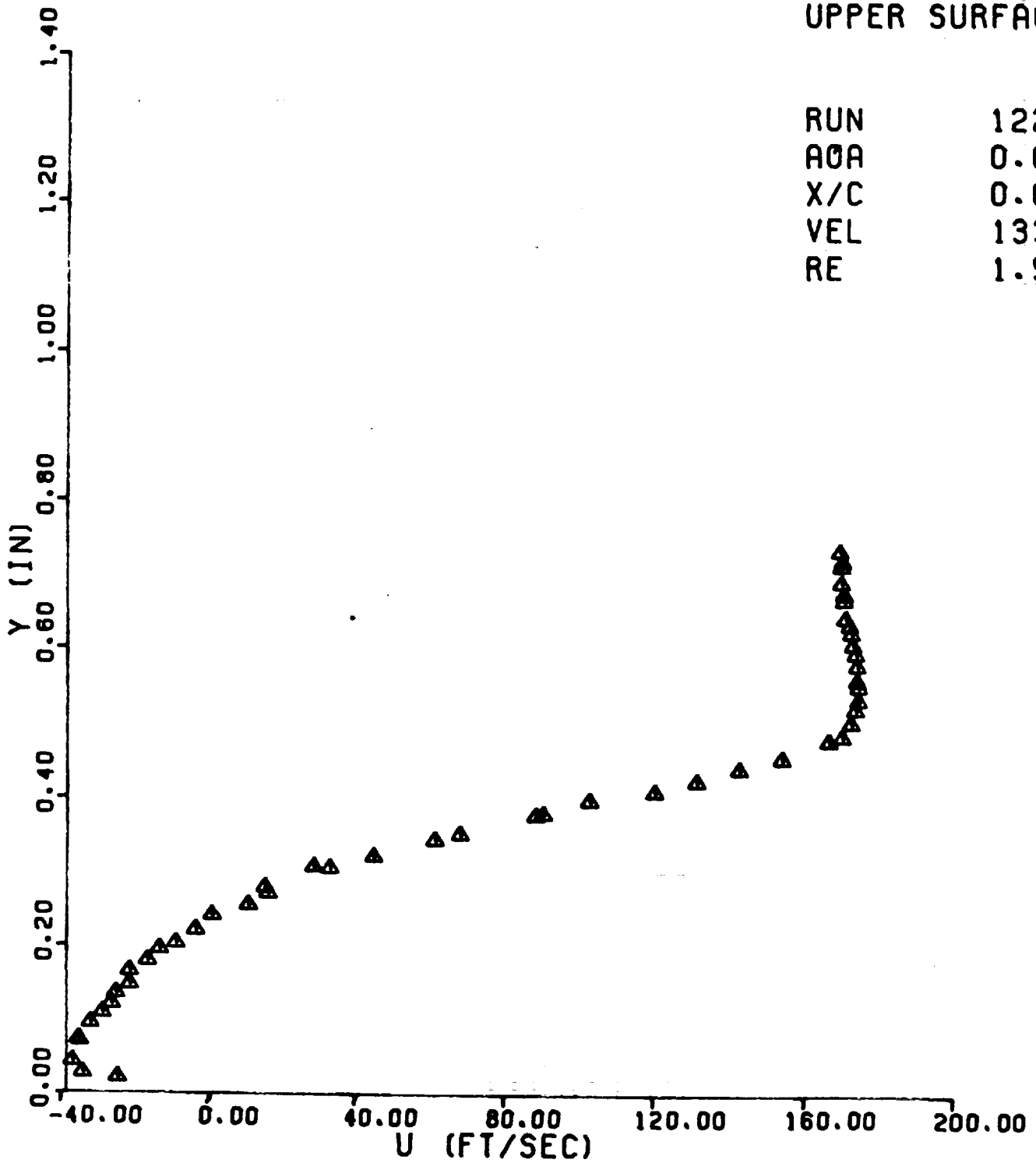
NACA 0012
UPPER SURFACE

RUN 1219
AOA 0.000
X/C 0.0000
VEL 134.7
RE 1.54



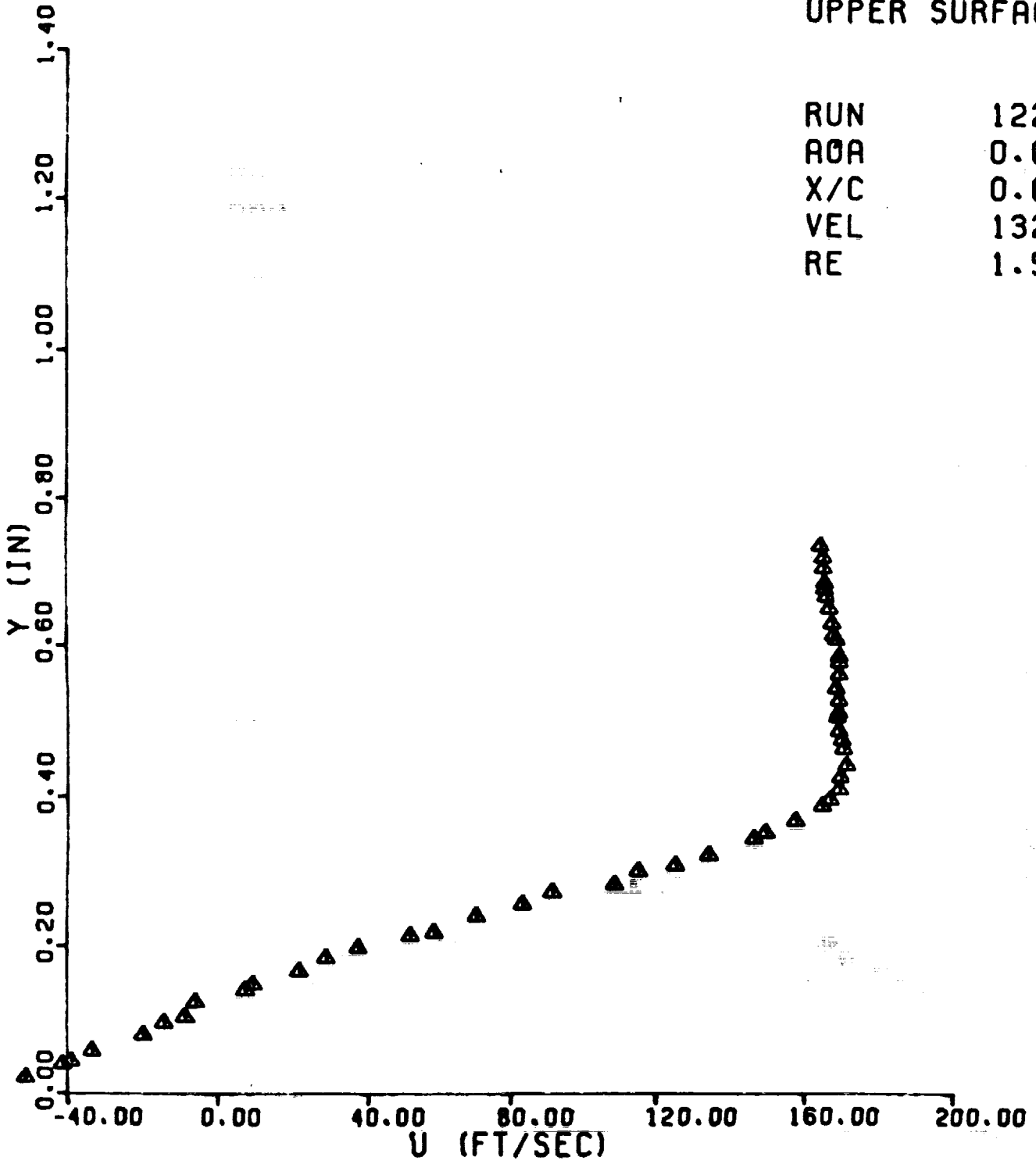
NACA 0012
UPPER SURFACE

RUN 1220
AOA 0.000
X/C 0.0200
VEL 133.4
RE 1.52



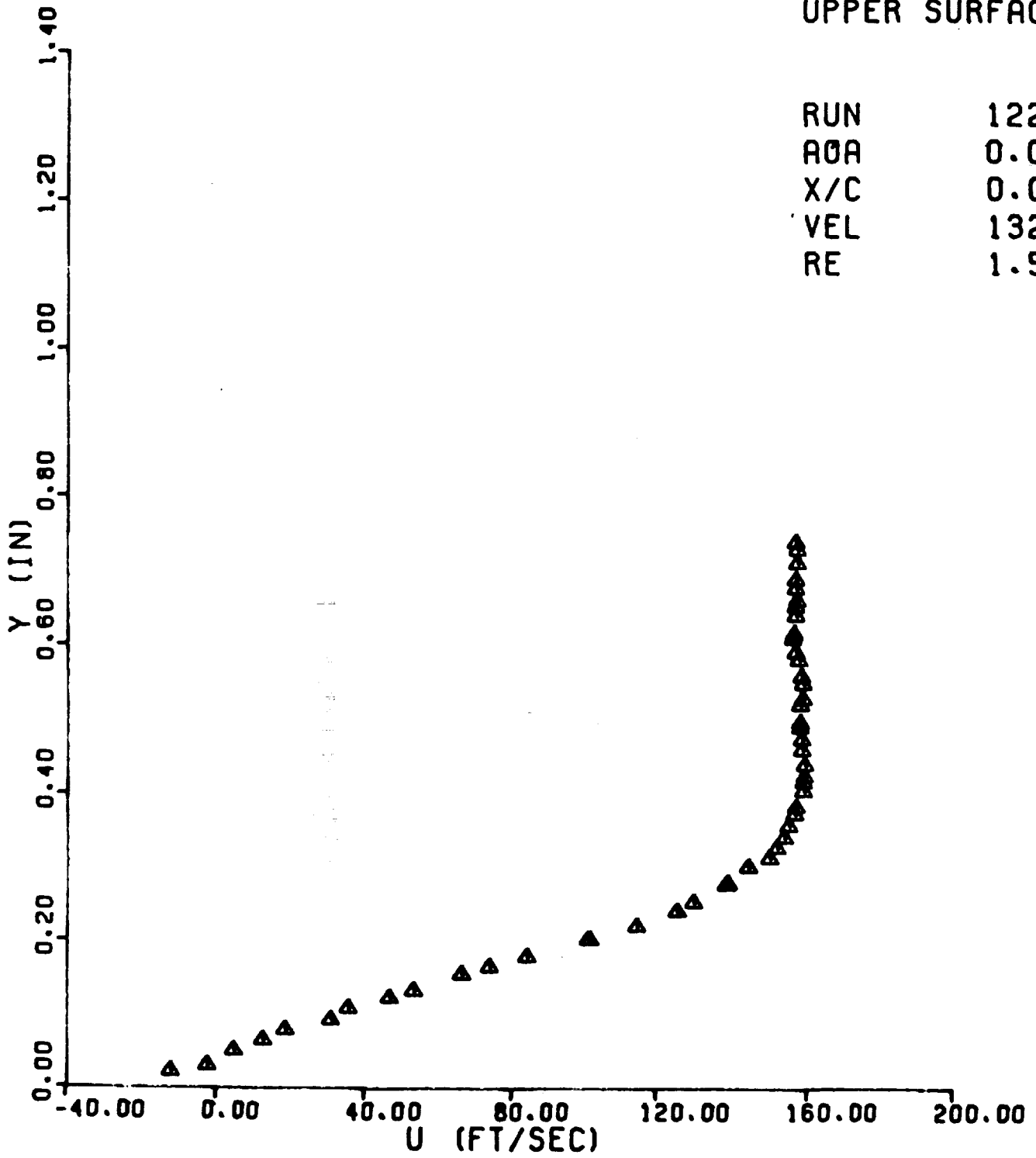
NACA 0012
UPPER SURFACE

RUN 1221
AOA 0.000
X/C 0.0400
VEL 132.5
RE 1.51



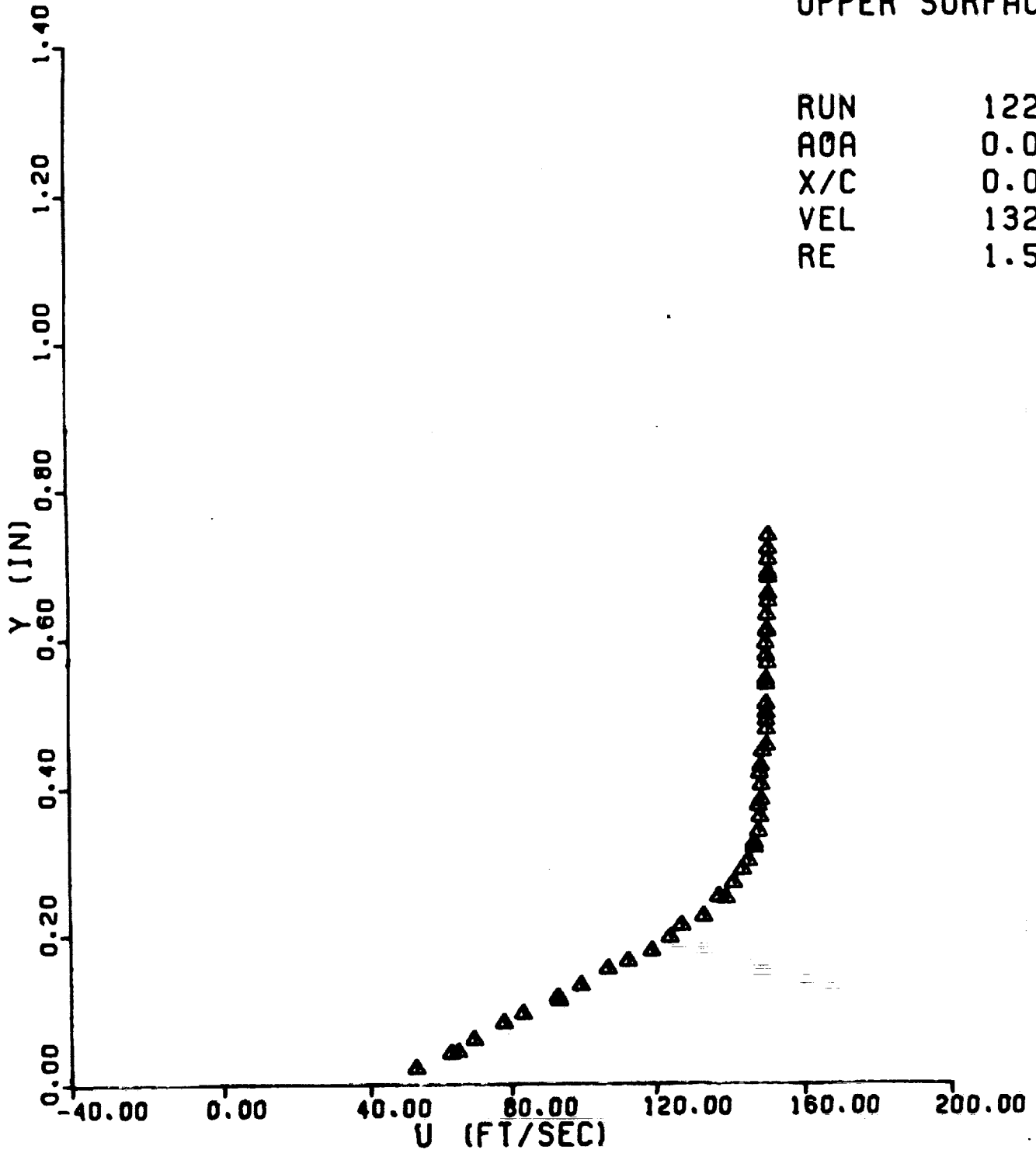
NACA 0012
UPPER SURFACE

RUN	1222
AOA	0.000
X/C	0.0600
VEL	132.5
RE	1.51



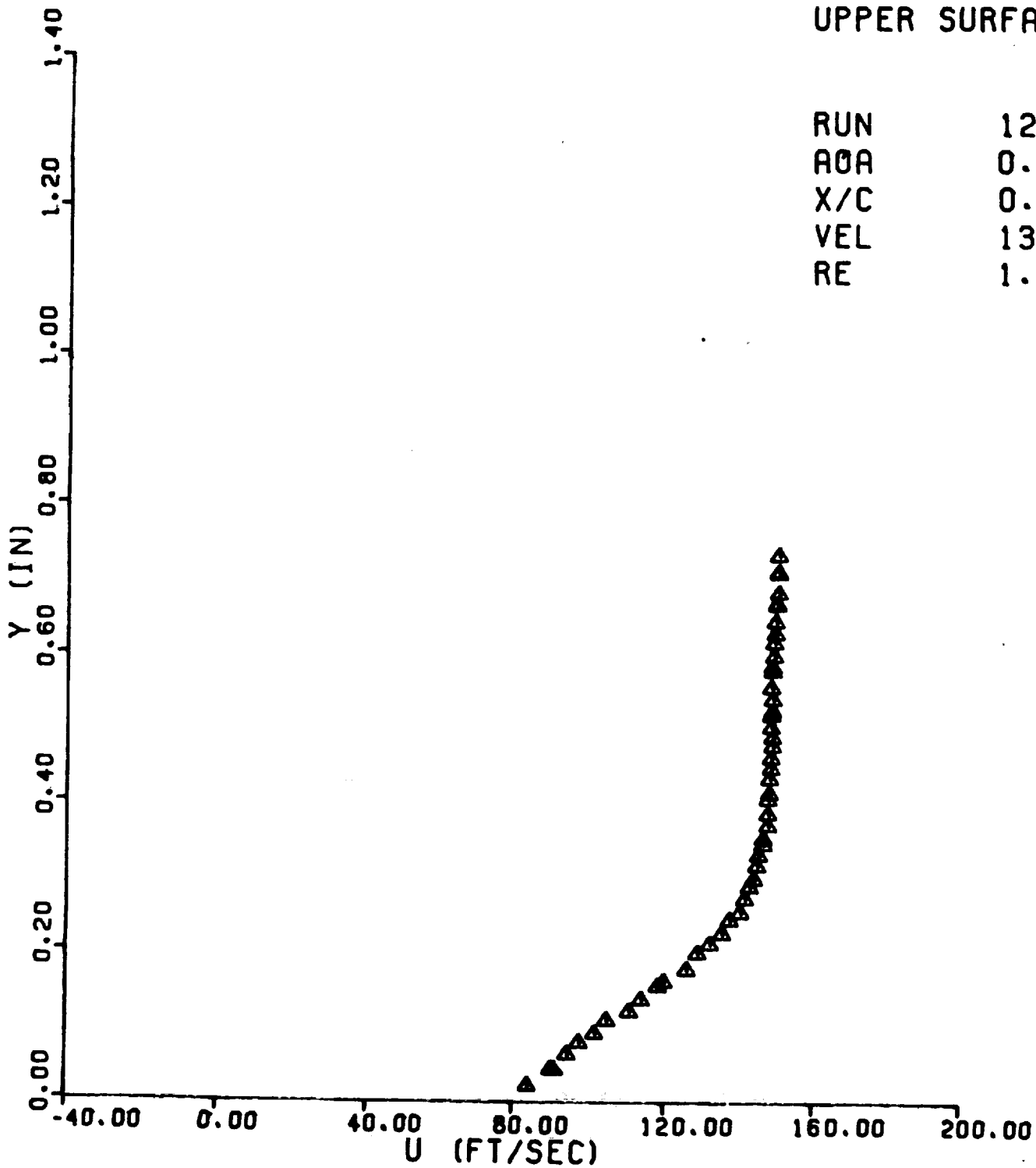
NACA 0012
UPPER SURFACE

RUN	1223
AOA	0.000
X/C	0.0800
VEL	132.2
RE	1.52



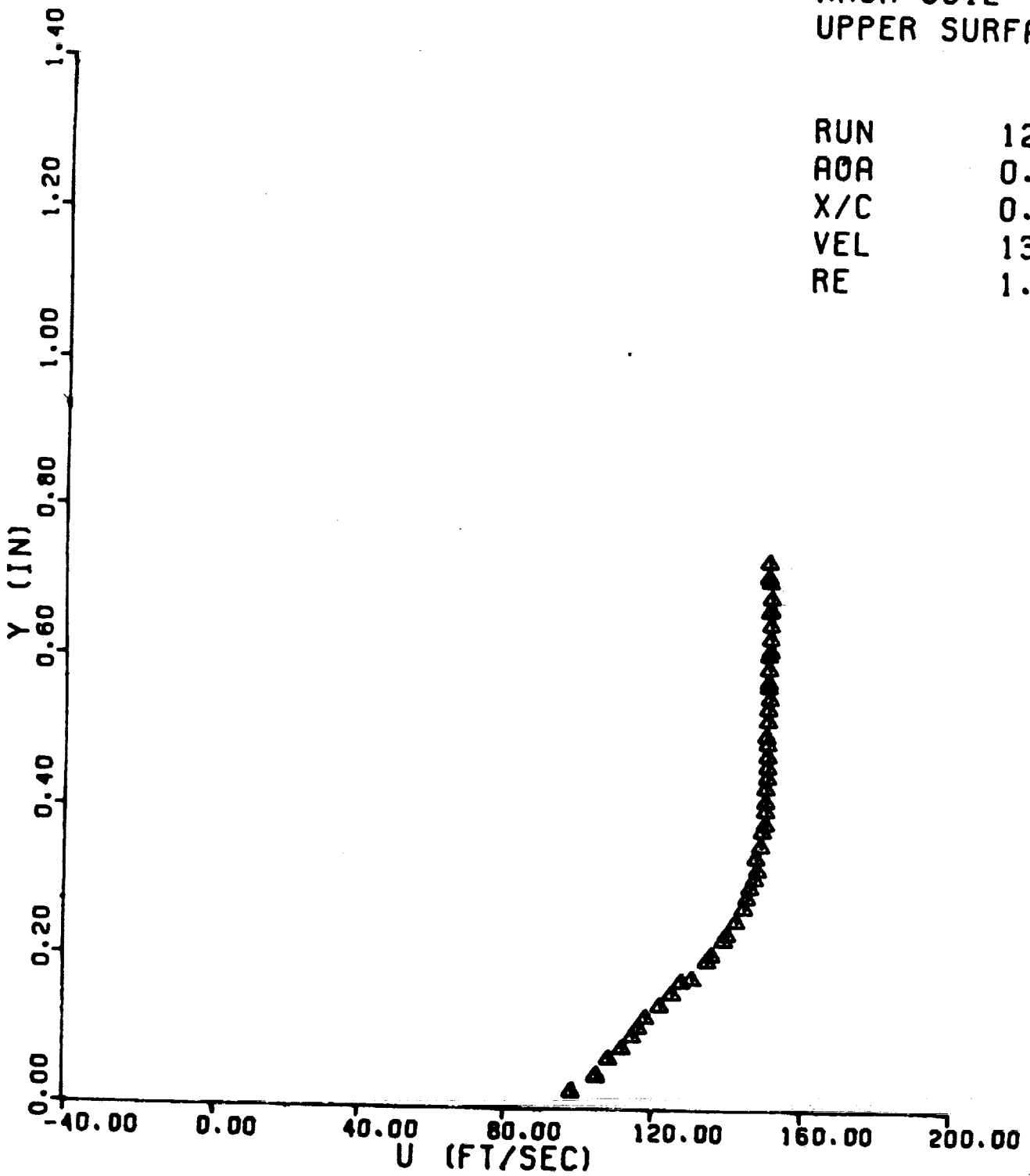
NACA 0012
UPPER SURFACE

RUN 1224
AOA 0.000
X/C 0.1000
VEL 131.6
RE 1.51



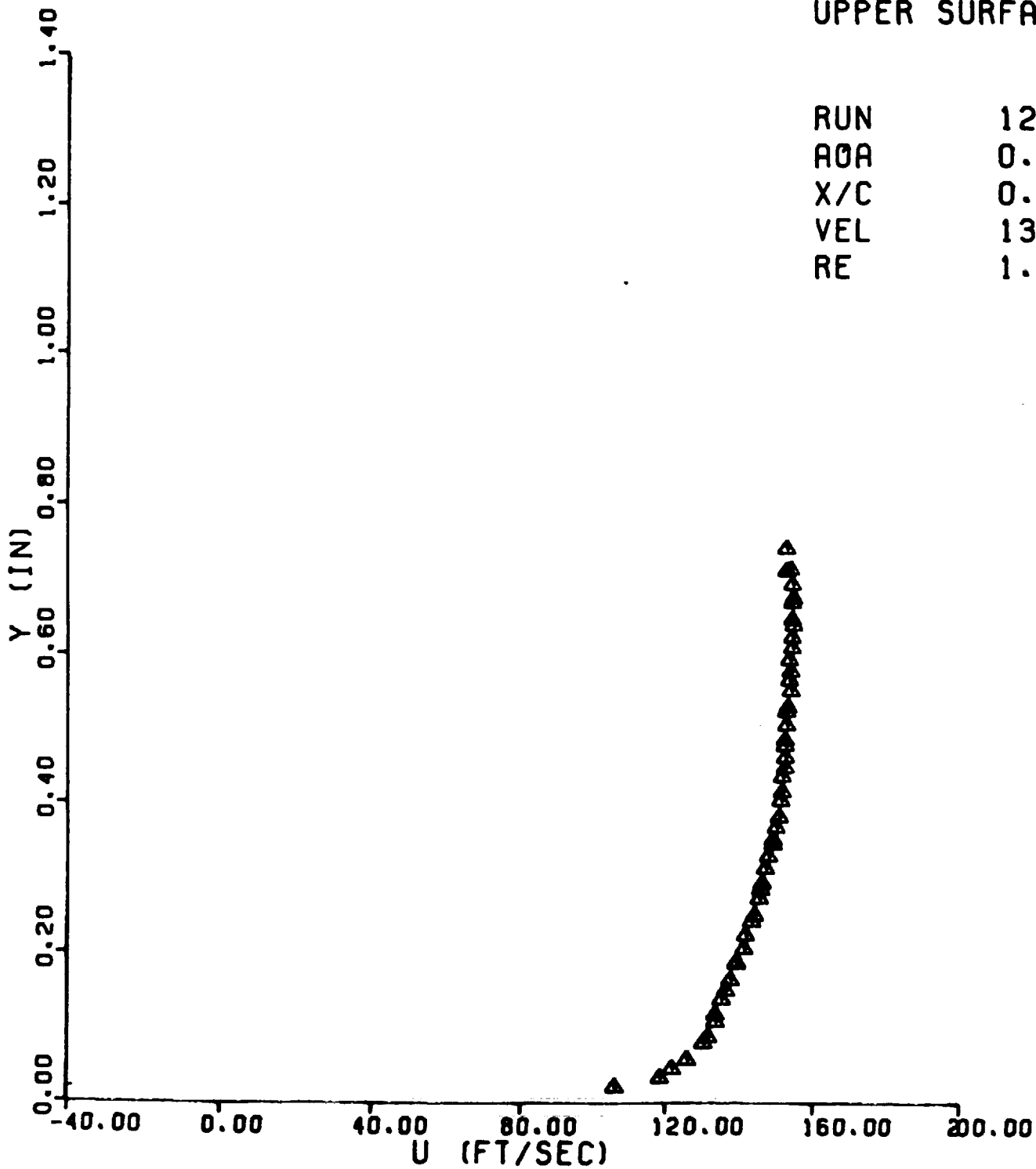
NACA 0012
UPPER SURFACE

RUN	1225
AOA	0.000
X/C	0.1200
VEL	130.7
RE	1.50



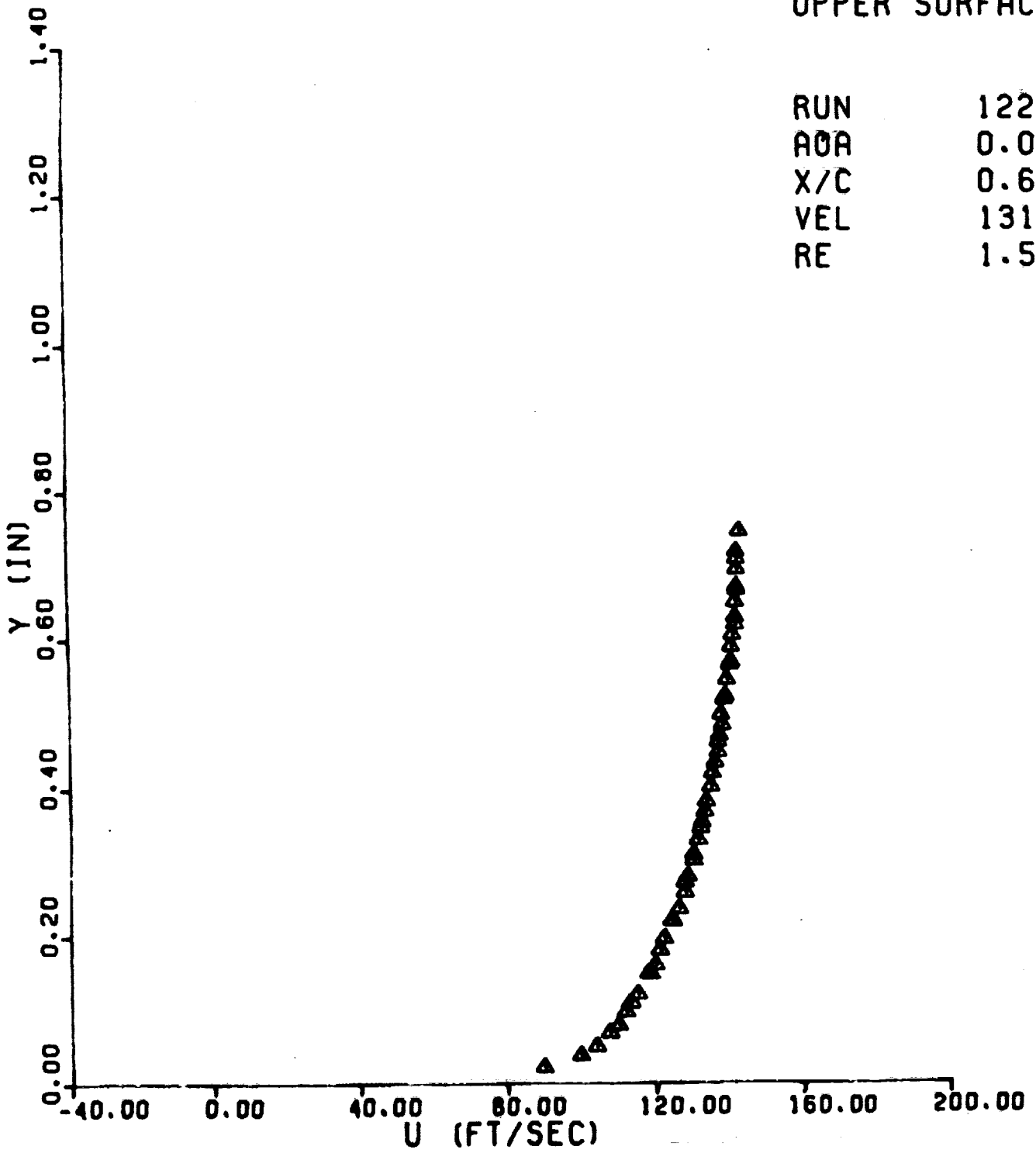
NACA 0012
UPPER SURFACE

RUN 1226
AOA 0.000
X/C 0.3000
VEL 130.8
RE 1.51



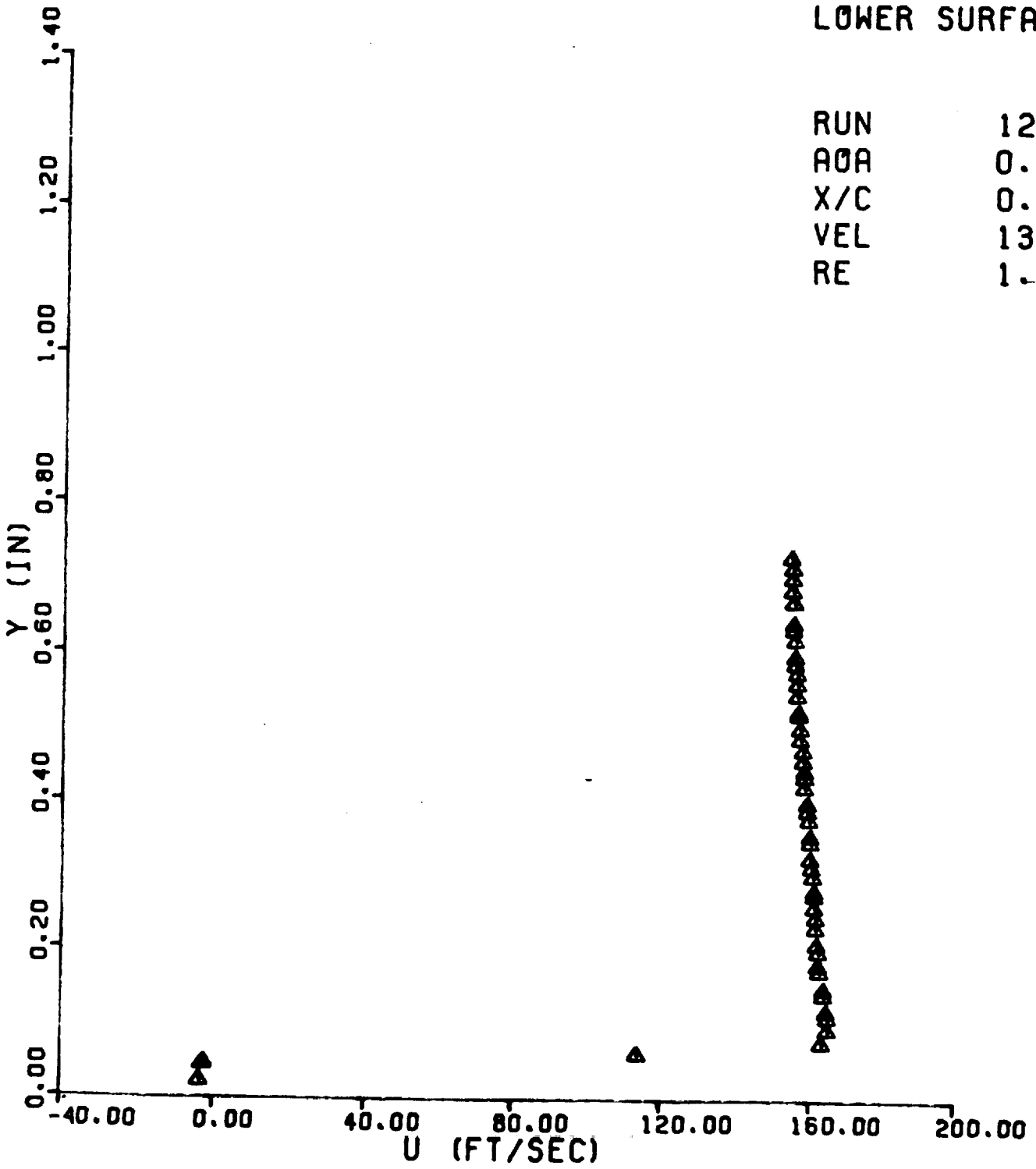
NACA 0012
UPPER SURFACE

RUN 1227
AOA 0.000
X/C 0.6000
VEL 131.7
RE 1.52



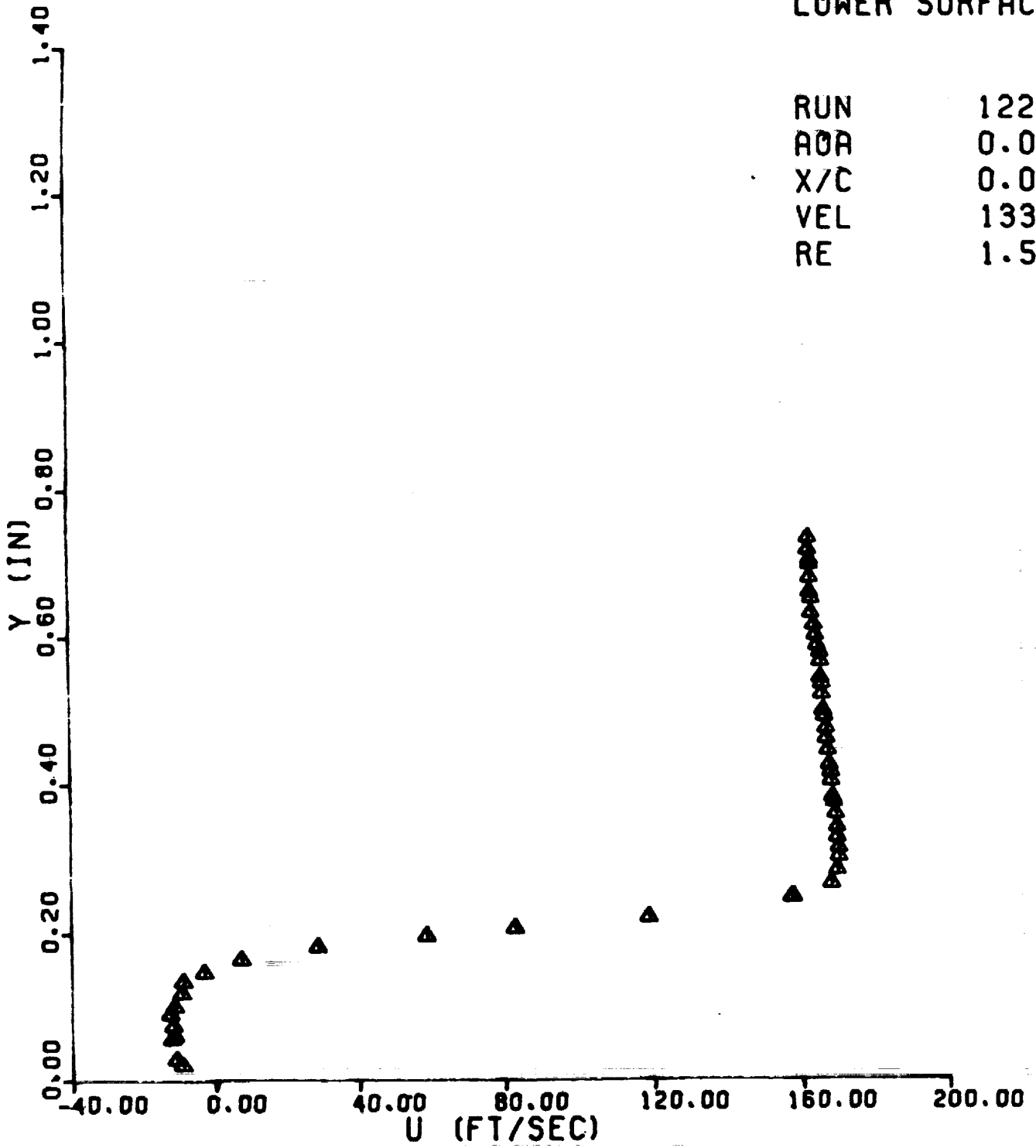
NACA 0012
LOWER SURFACE

RUN	1228
AOA	0.000
X/C	0.0300
VEL	133.9
RE	1.58



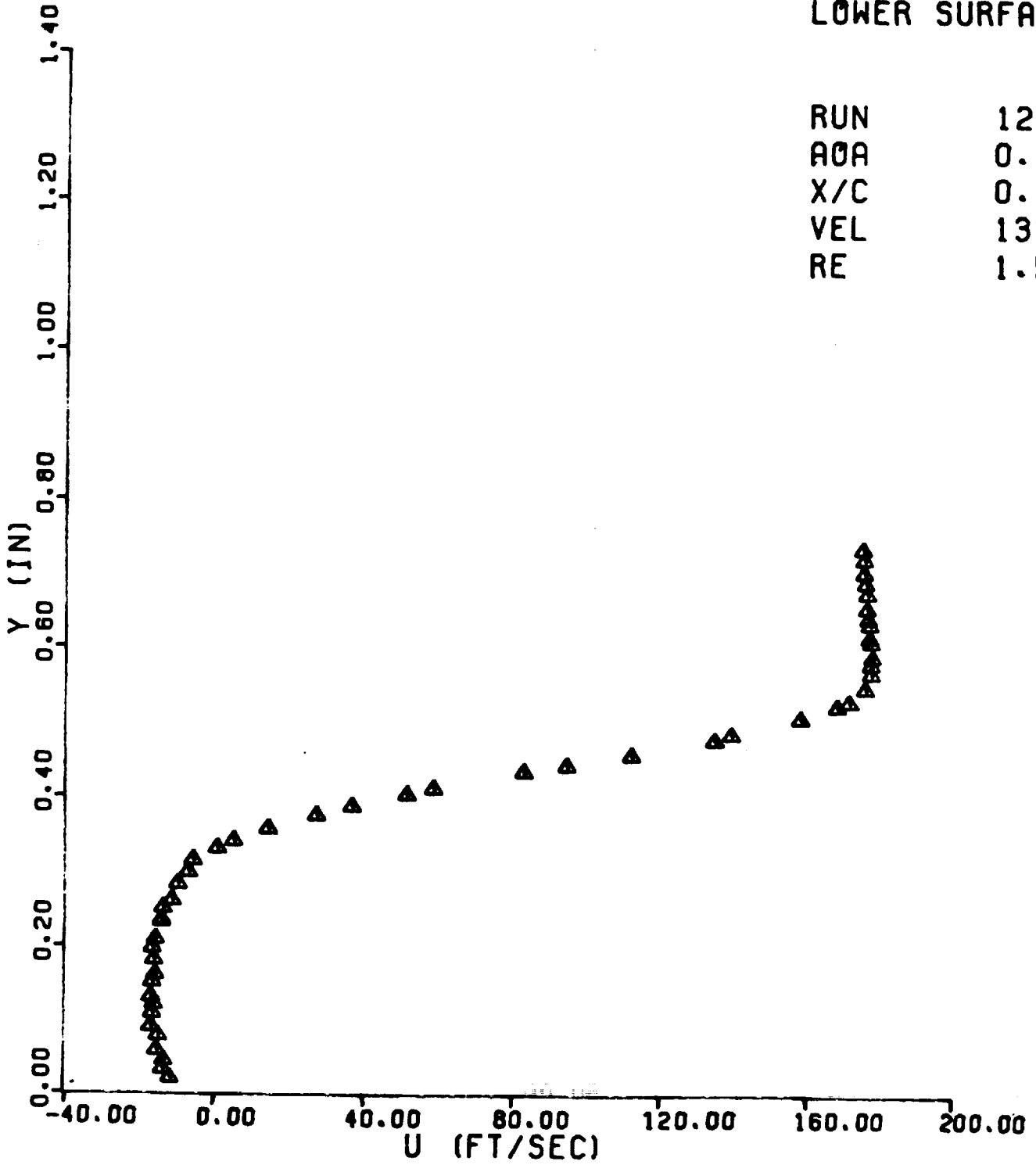
NACA 0012
LOWER SURFACE

RUN 1229
AOA 0.000
X/C 0.0400
VEL 133.6
RE 1.58



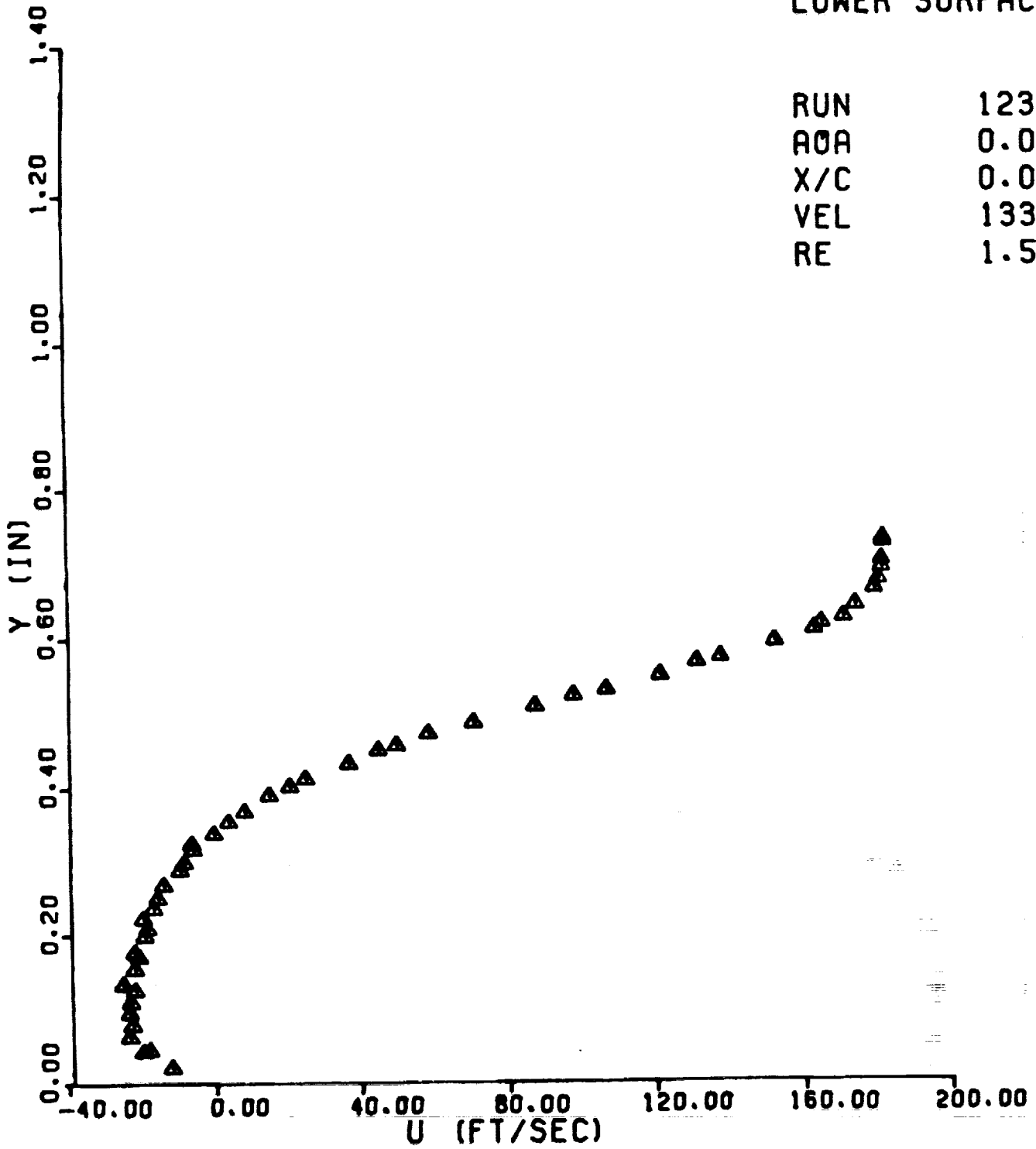
NACA 0012
LOWER SURFACE

RUN	1230
AOA	0.000
X/C	0.0600
VEL	133.8
RE	1.58



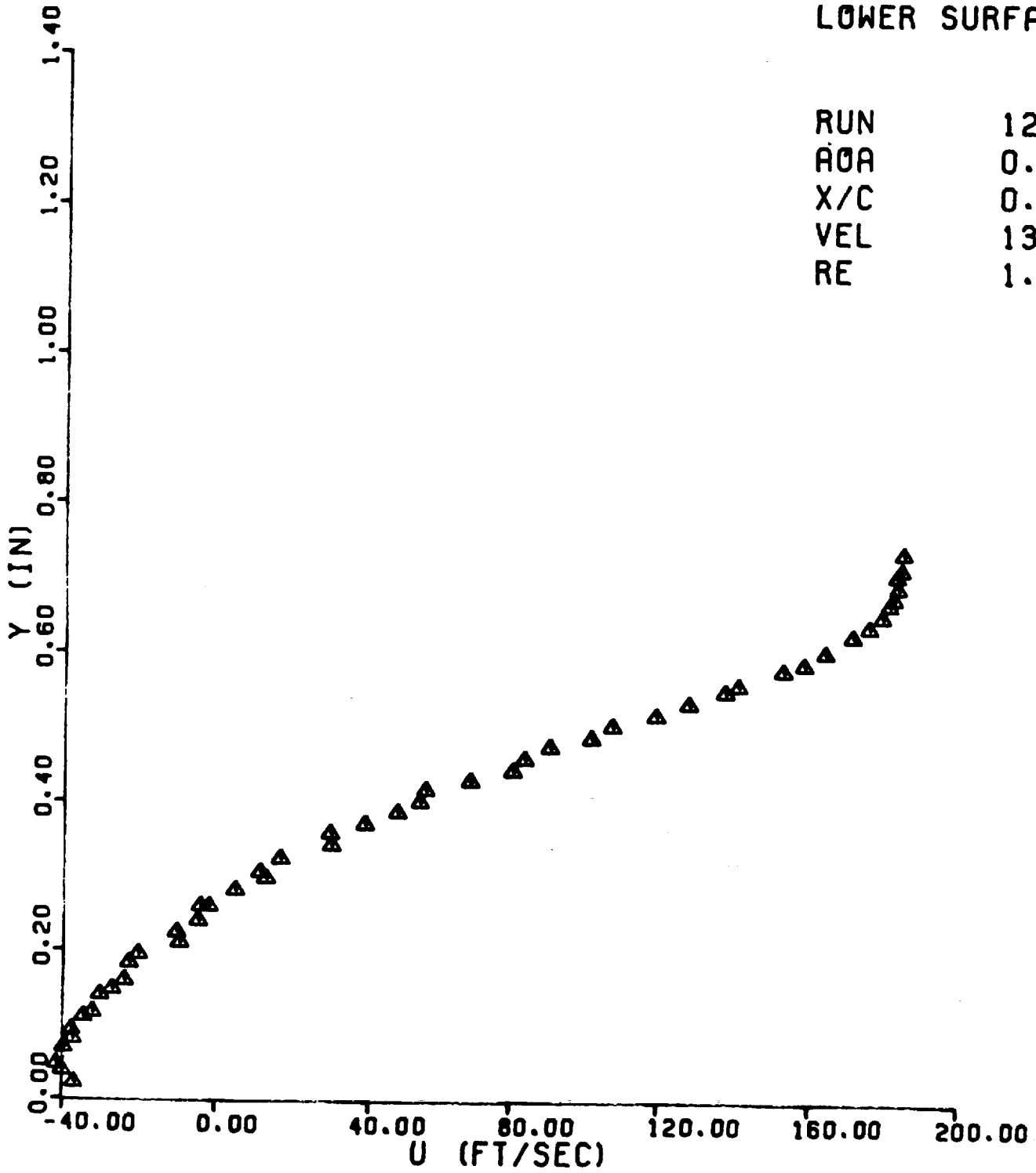
NACA 0012
LOWER SURFACE

RUN	1231
AOA	0.000
X/C	0.0800
VEL	133.2
RE	1.54



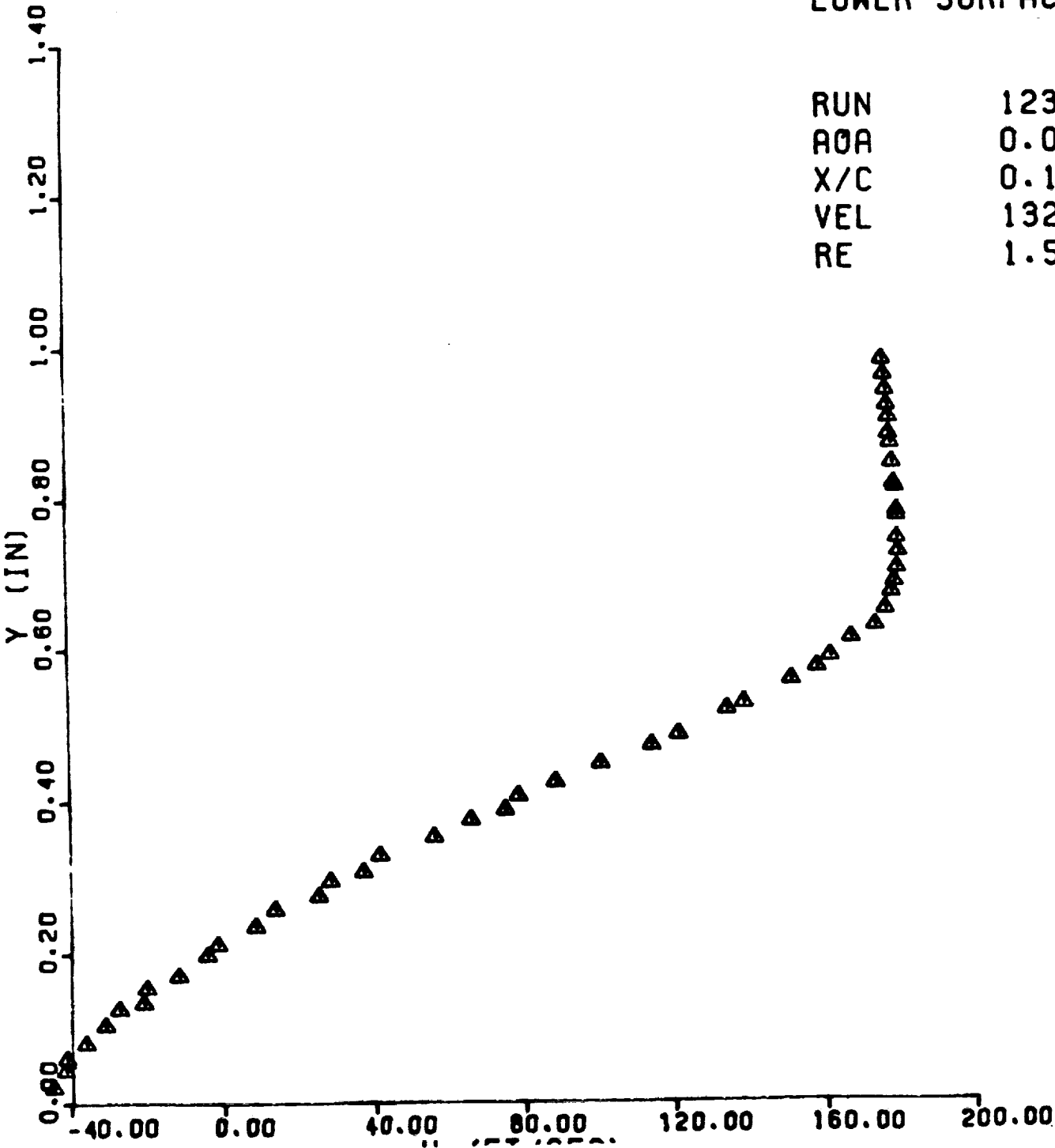
NACA 0012
LOWER SURFACE

RUN	1232
AOA	0.000
X/C	0.1000
VEL	132.2
RE	1.53



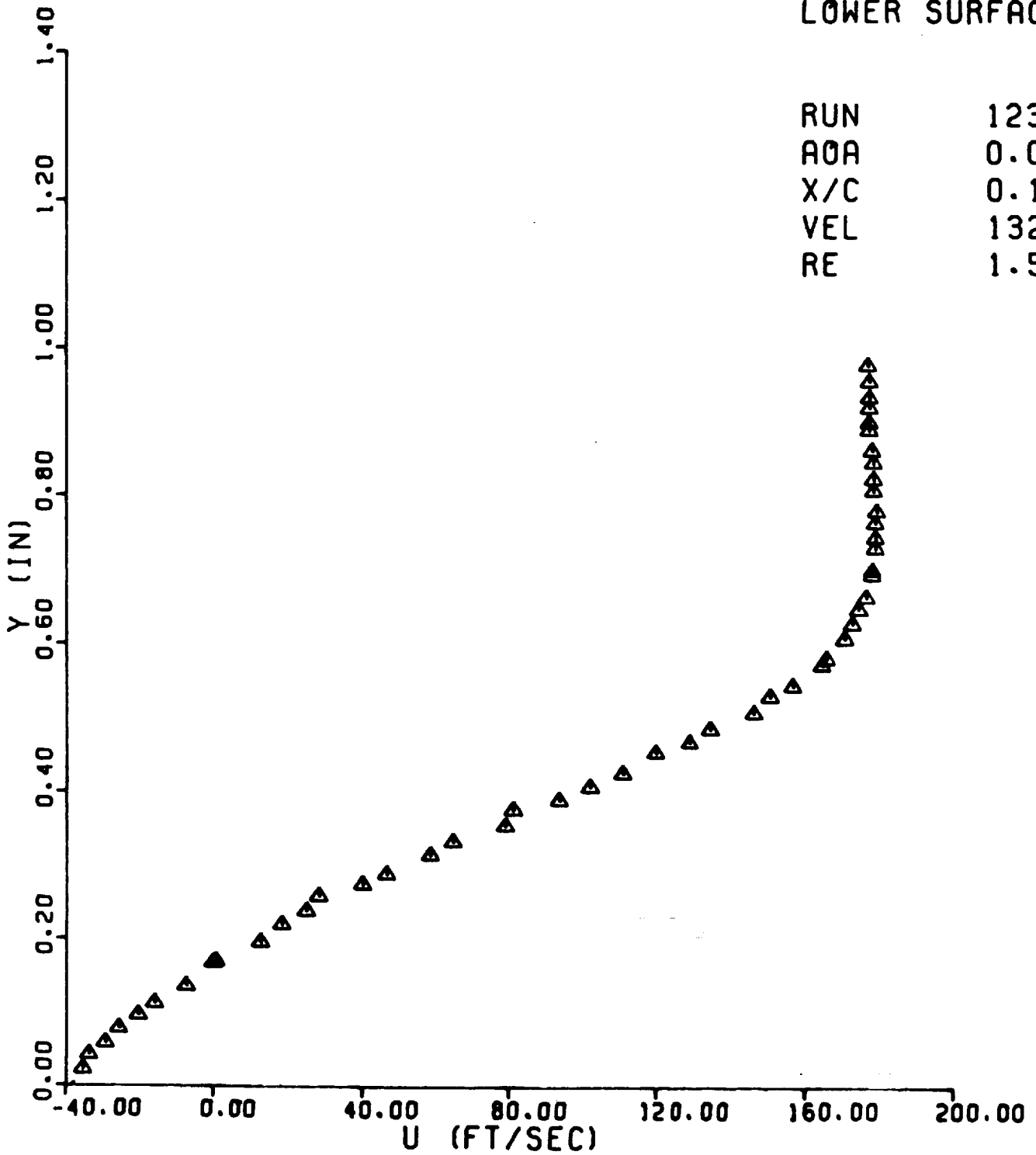
NACA 0012
LOWER SURFACE

RUN	1233
AOA	0.000
X/C	0.1200
VEL	132.2
RE	1.52



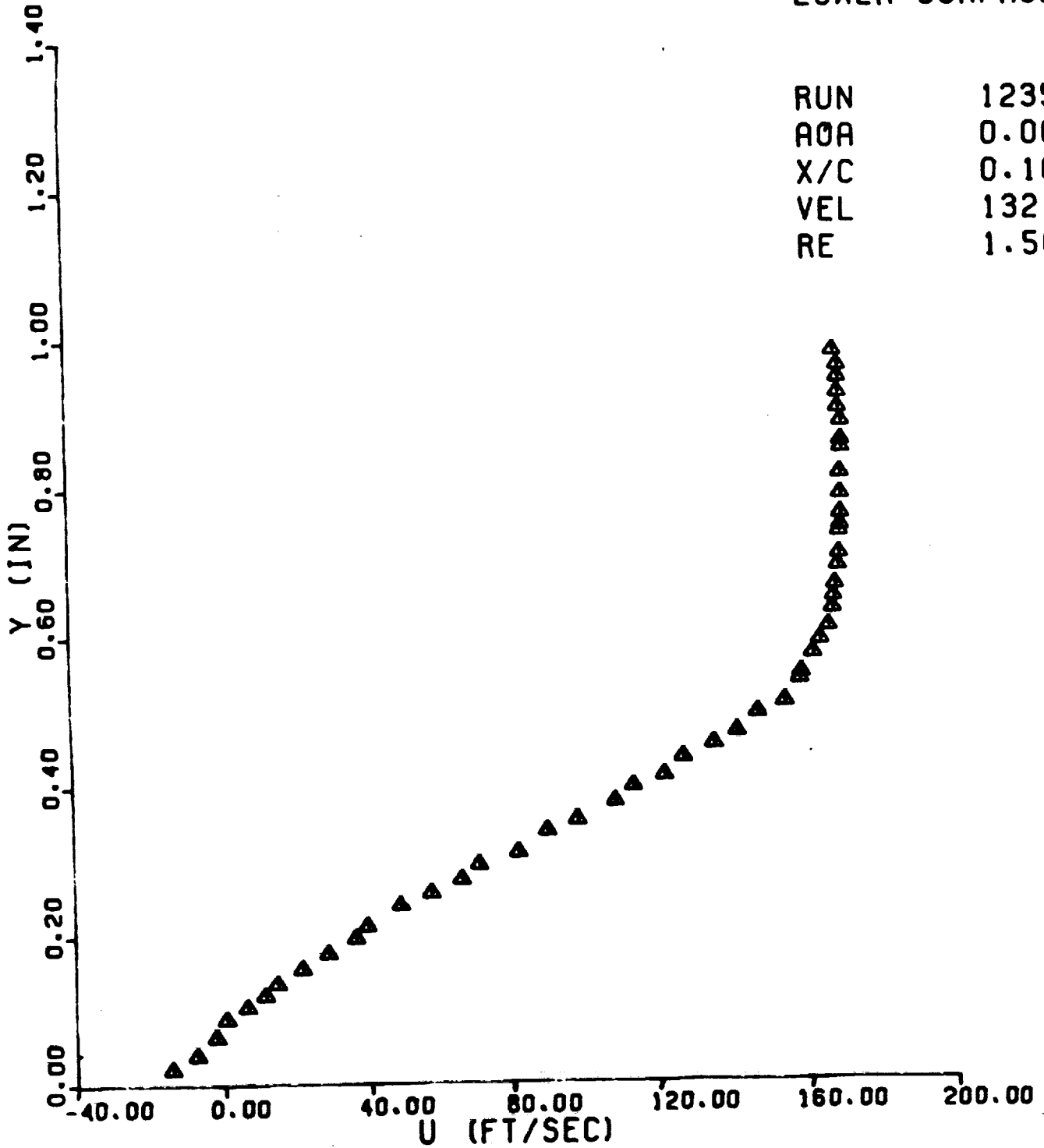
NACA 0012
LOWER SURFACE

RUN	1234
AOA	0.000
X/C	0.1400
VEL	132.8
RE	1.51



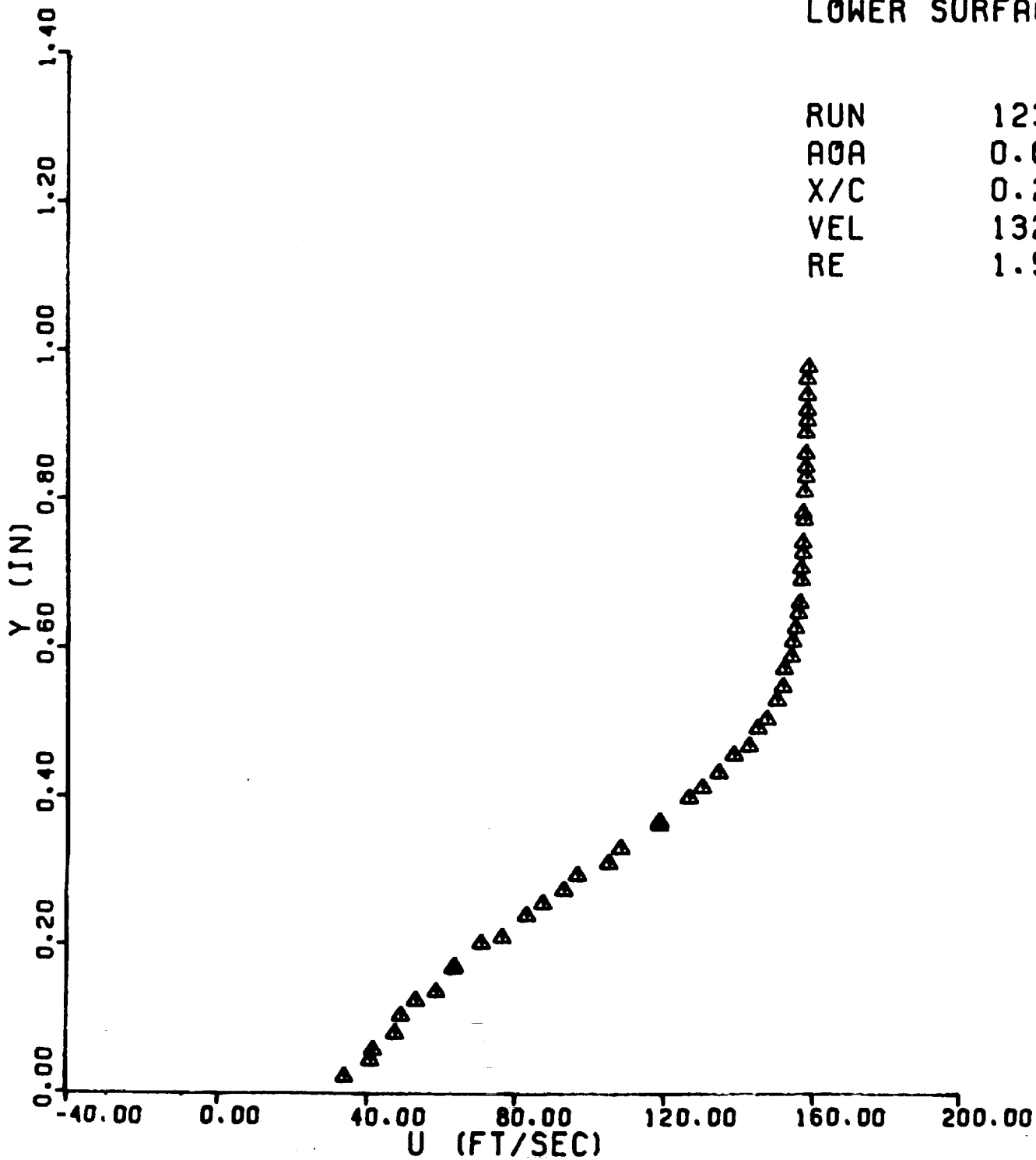
NACA 0012
LOWER SURFACE

RUN	1235
AOA	0.000
X/C	0.1600
VEL	132.6
RE	1.50



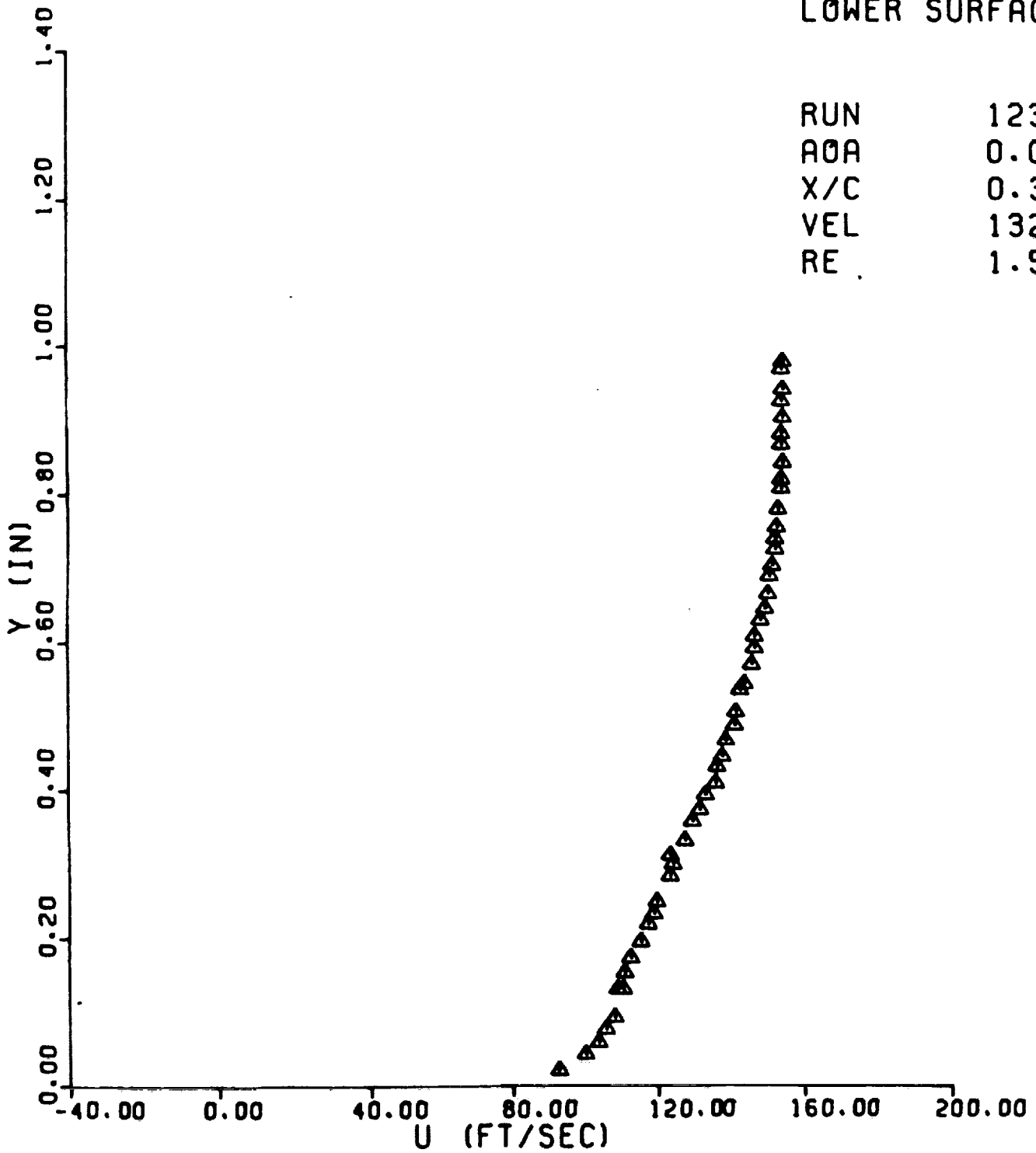
NACA 0012
LOWER SURFACE

RUN	1236
AOA	0.000
X/C	0.2000
VEL	132.1
RE	1.50



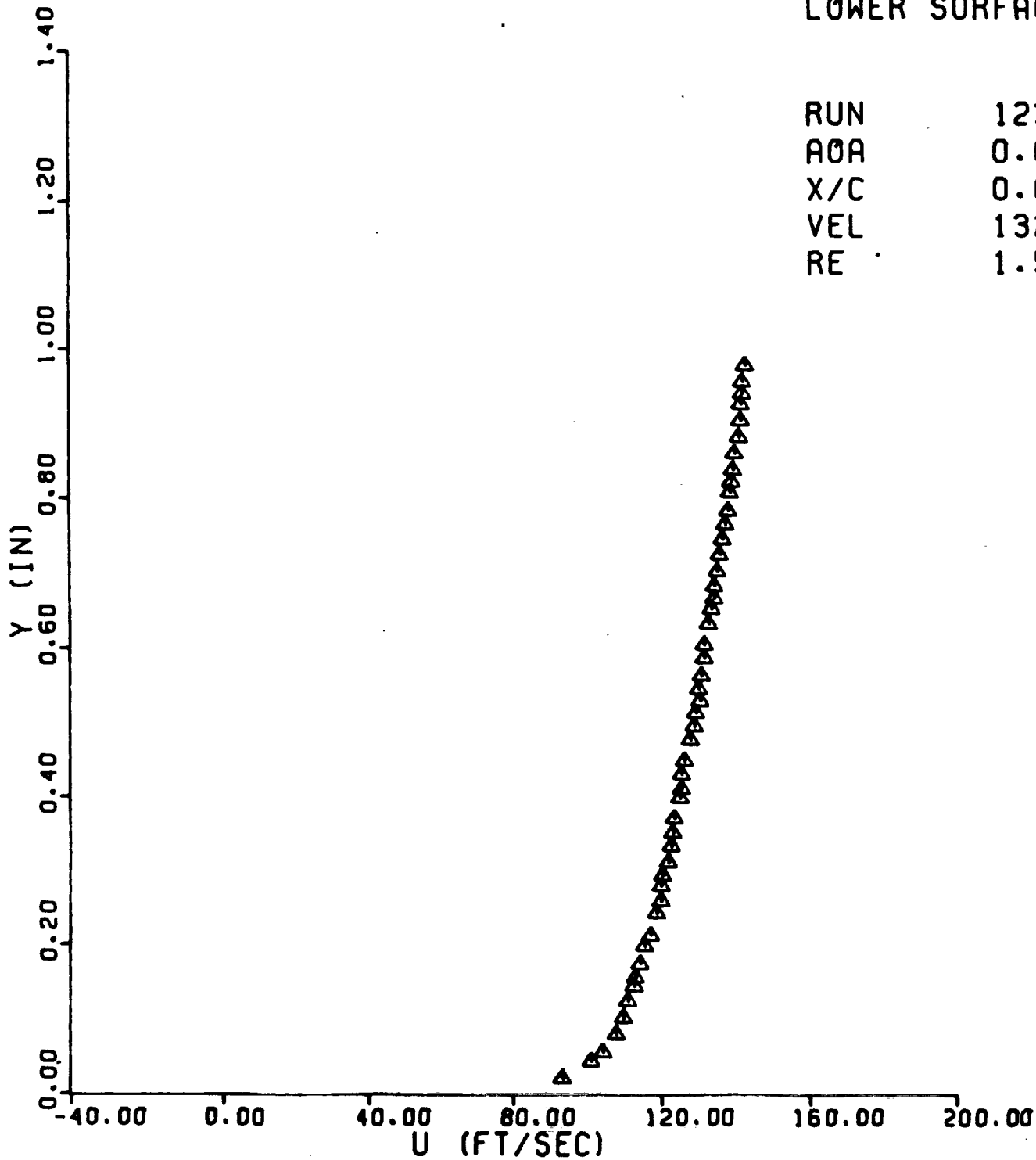
NACA 0012
LOWER SURFACE

RUN	1237
AOA	0.000
X/C	0.3200
VEL	132.5
RE	1.51



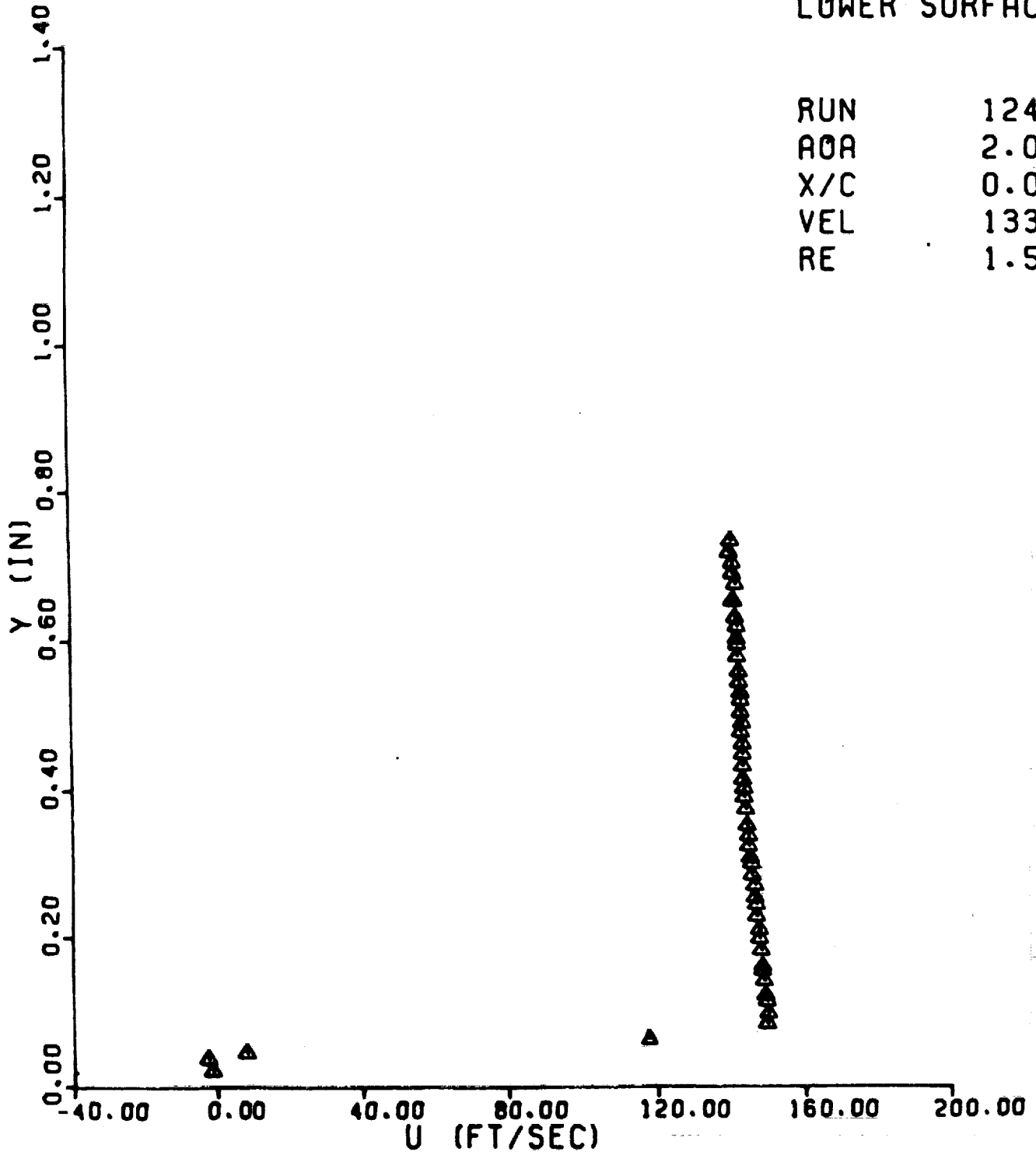
NACA 0012
LOWER SURFACE

RUN	1238
AOA	0.000
X/C	0.6000
VEL	132.6
RE	1.51



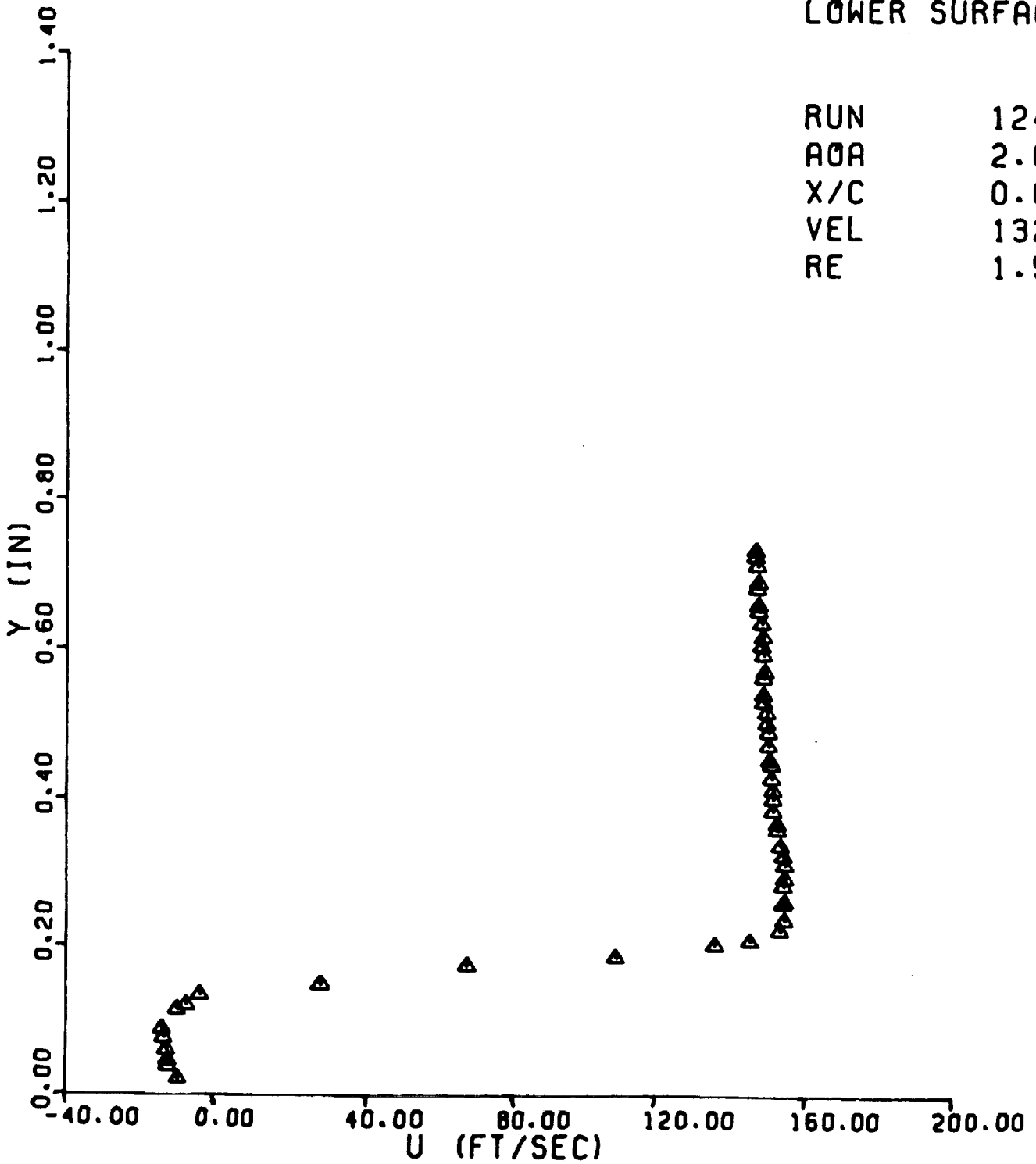
NACA 0012
LOWER SURFACE

RUN 1240
AOA 2.000
X/C 0.0300
VEL 133.3
RE 1.58



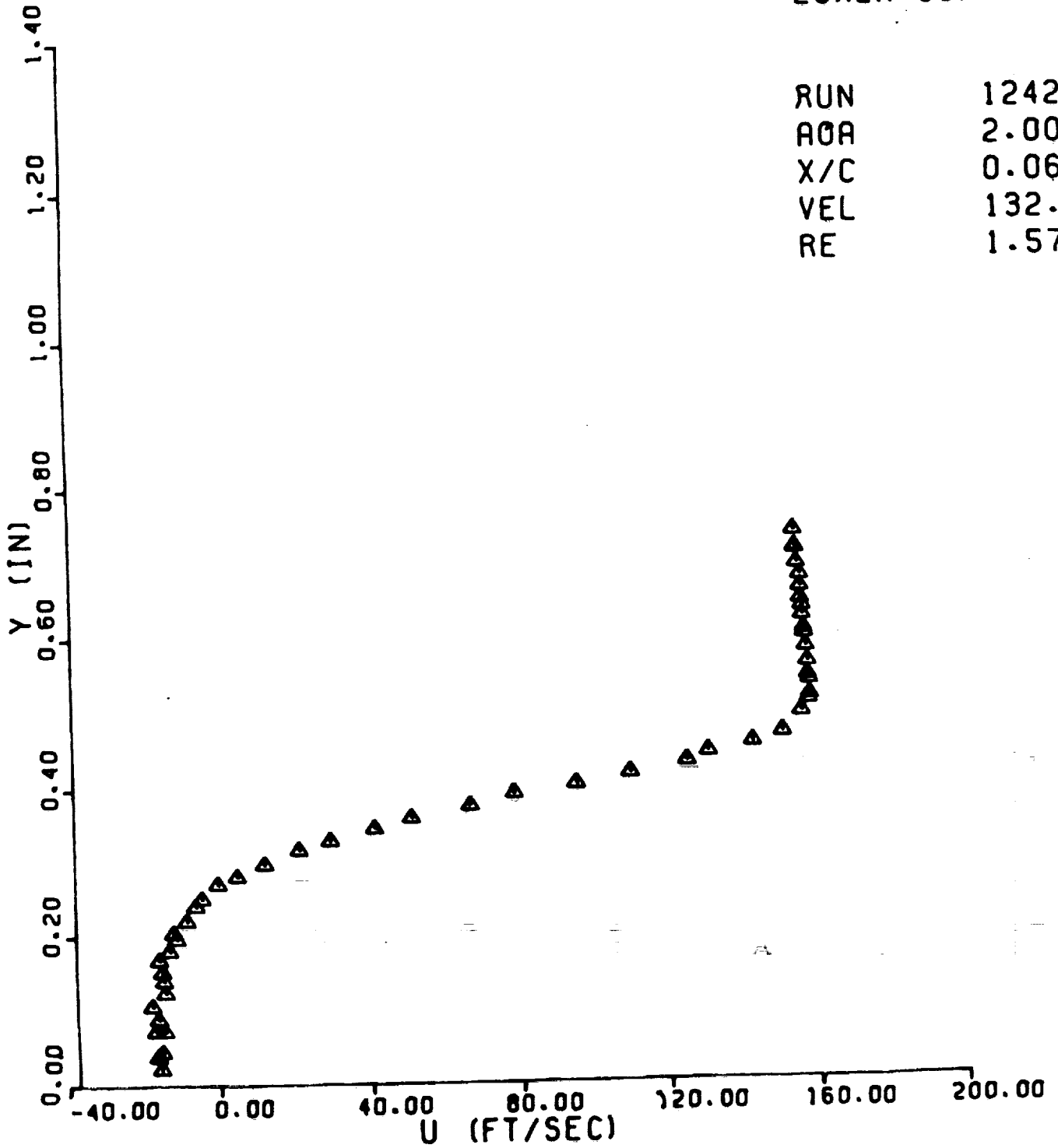
NACA 0012
LOWER SURFACE

RUN 1241
AOA 2.000
X/C 0.0400
VEL 132.7
RE 1.57



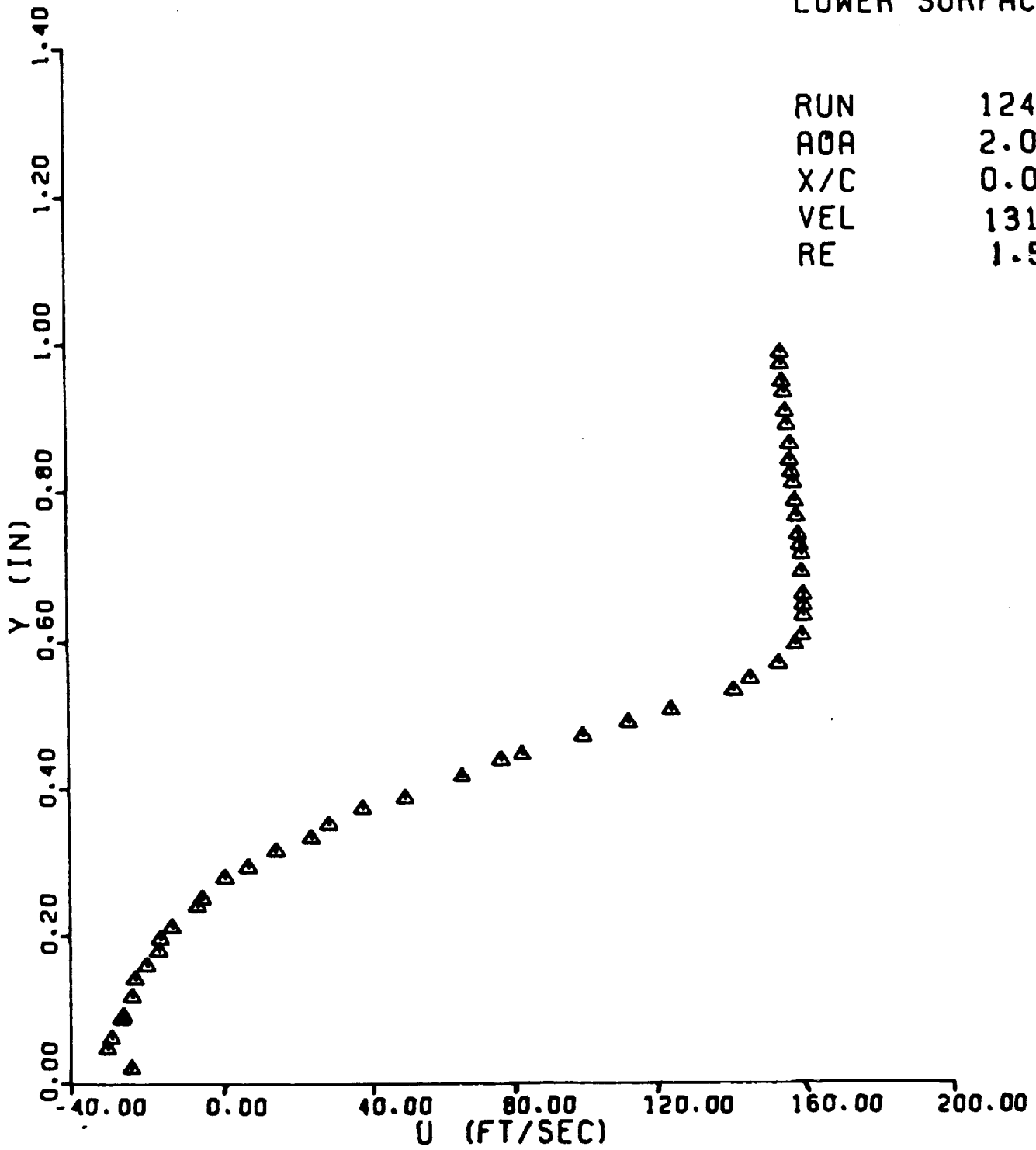
NACA 0012
LOWER SURFACE

RUN	1242
AOA	2.000
X/C	0.0600
VEL	132.8
RE	1.57



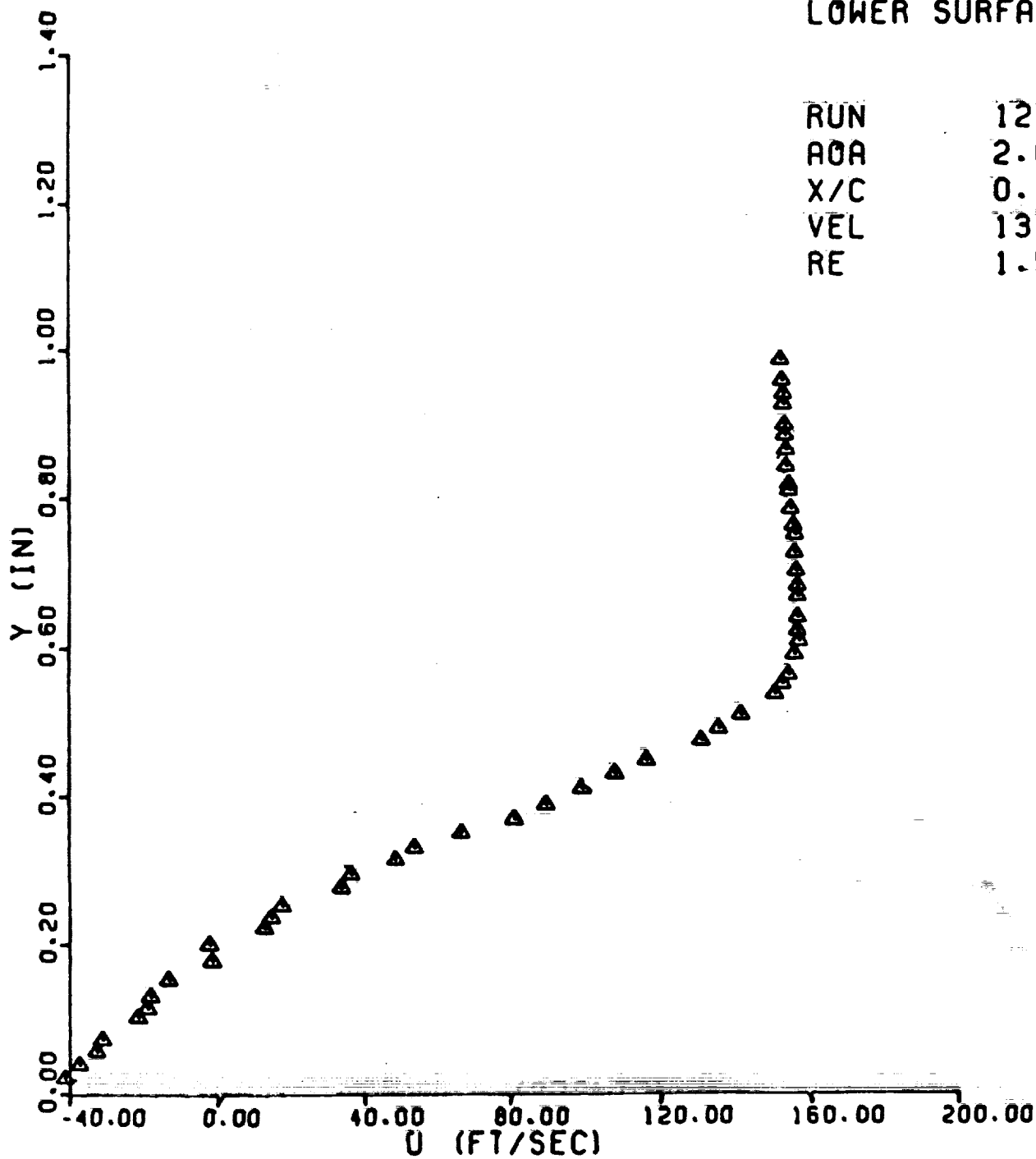
NACA 0012
LOWER SURFACE

RUN 1243
AOA 2.000
X/C 0.0800
VEL 131.70
RE 1.56



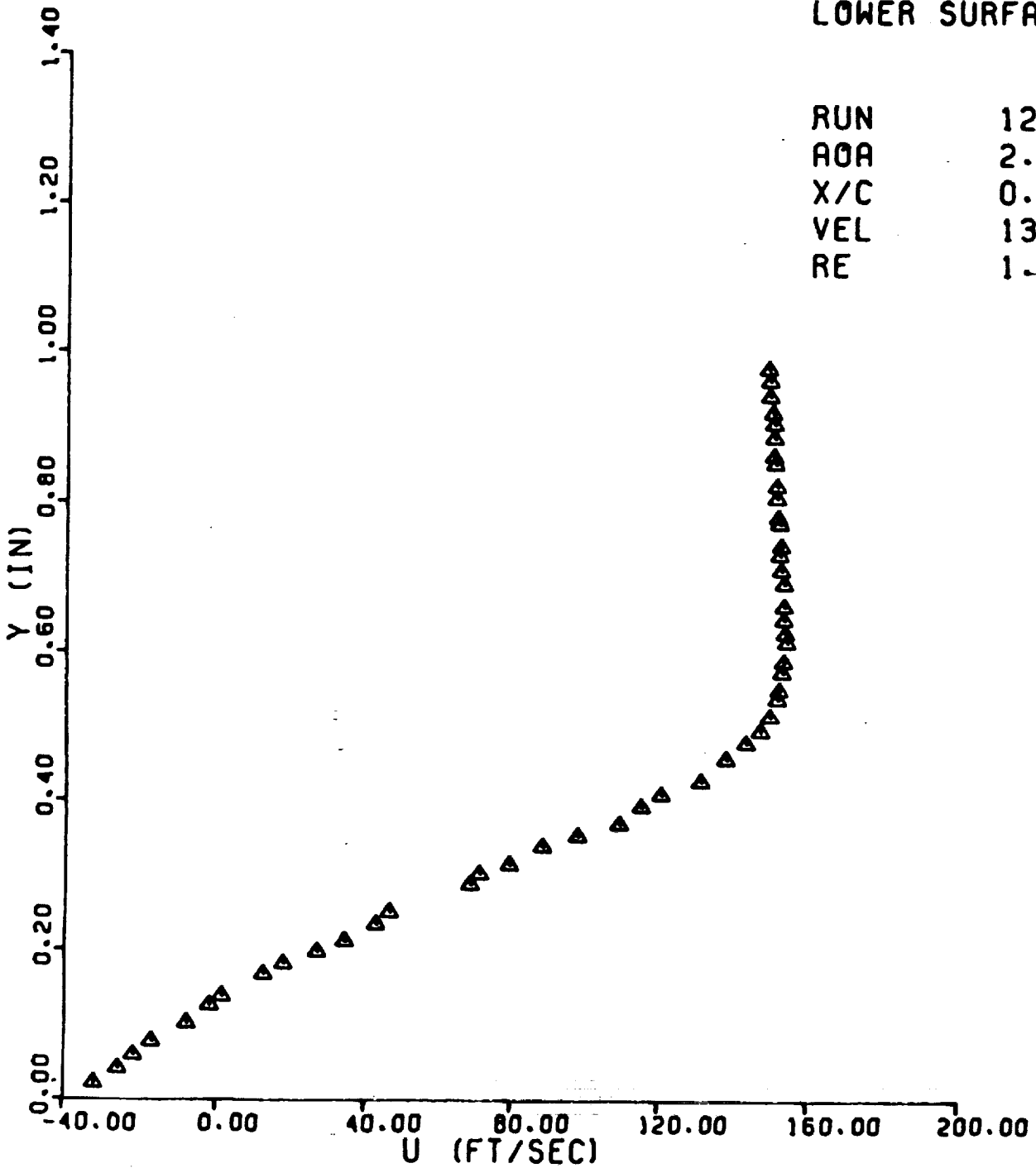
NACA 0012
LOWER SURFACE

RUN	1244
AOA	2.000
X/C	0.1000
VEL	131.9
RE	1.56



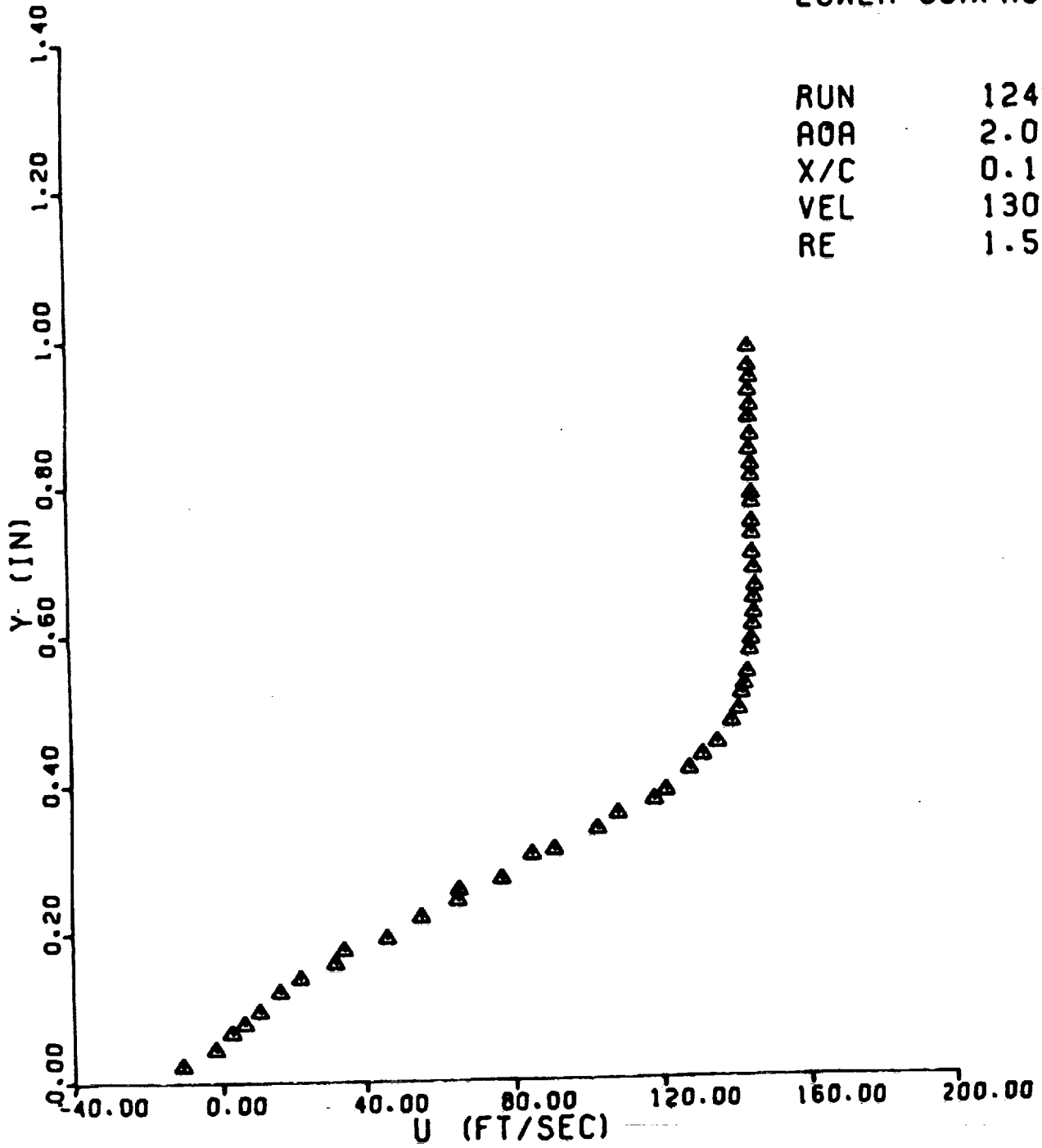
NACA 0012
LOWER SURFACE

RUN 1245
AOA 2.000
X/C 0.1200
VEL 130.8
RE 1.54



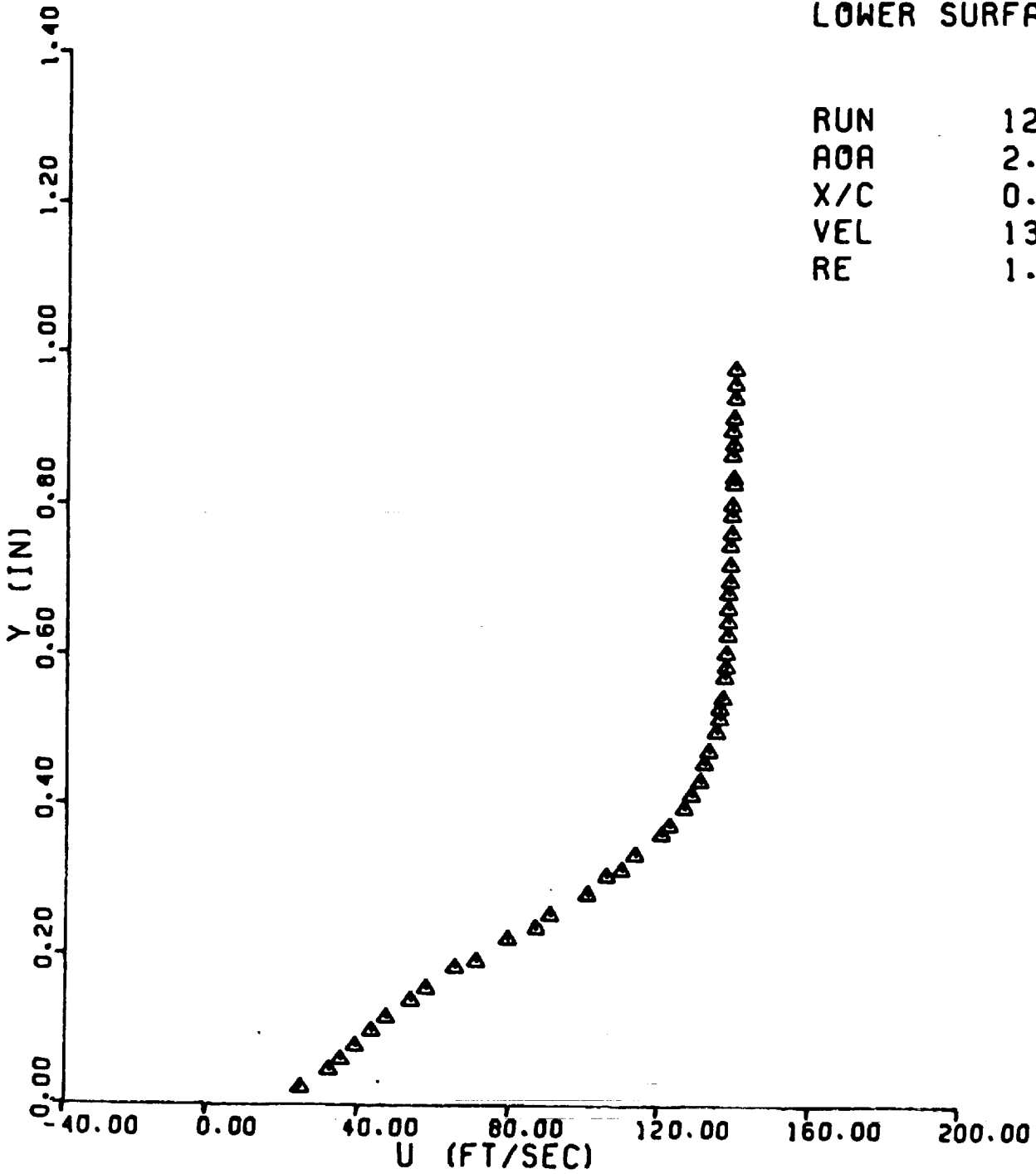
NACA 0012
LOWER SURFACE

RUN	1246
AOA	2.000
X/C	0.1400
VEL	130.9
RE	1.55



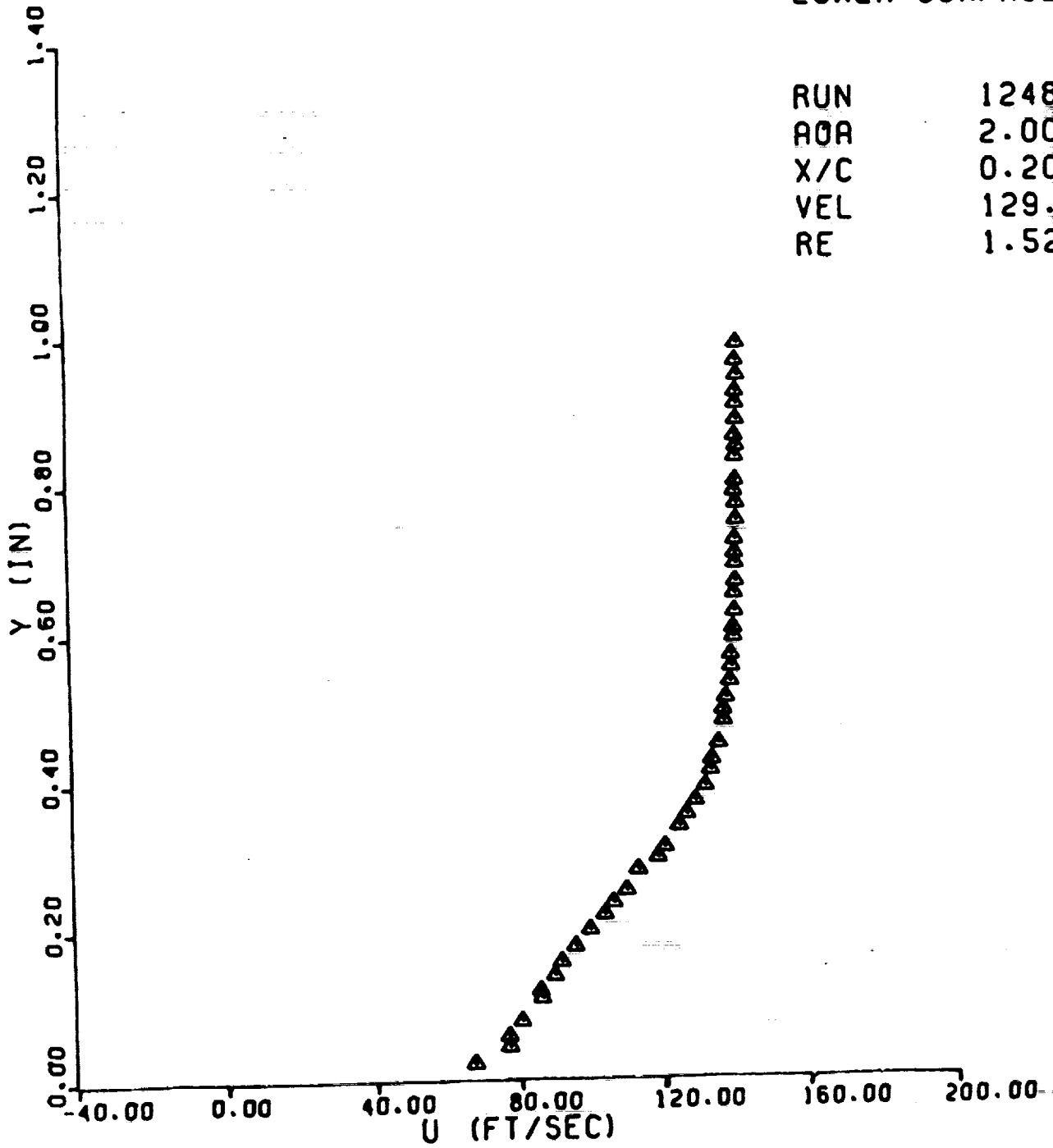
NACA 0012
LOWER SURFACE

RUN	1247
AOA	2.000
X/C	0.1600
VEL	130.6
RE	1.54



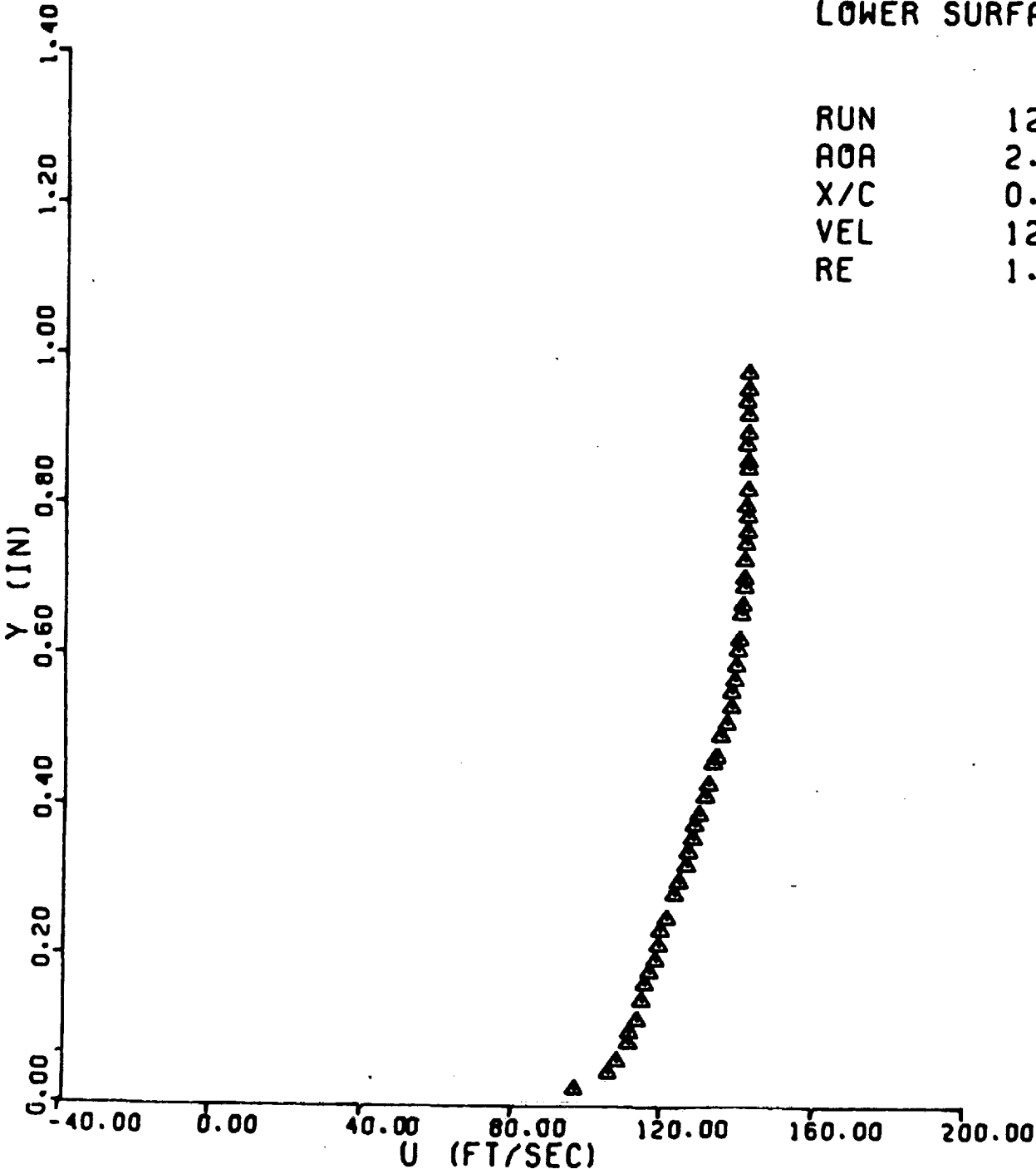
NACA 0012
LOWER SURFACE

RUN 1248
AOA 2.000
X/C 0.2000
VEL 129.8
RE 1.52



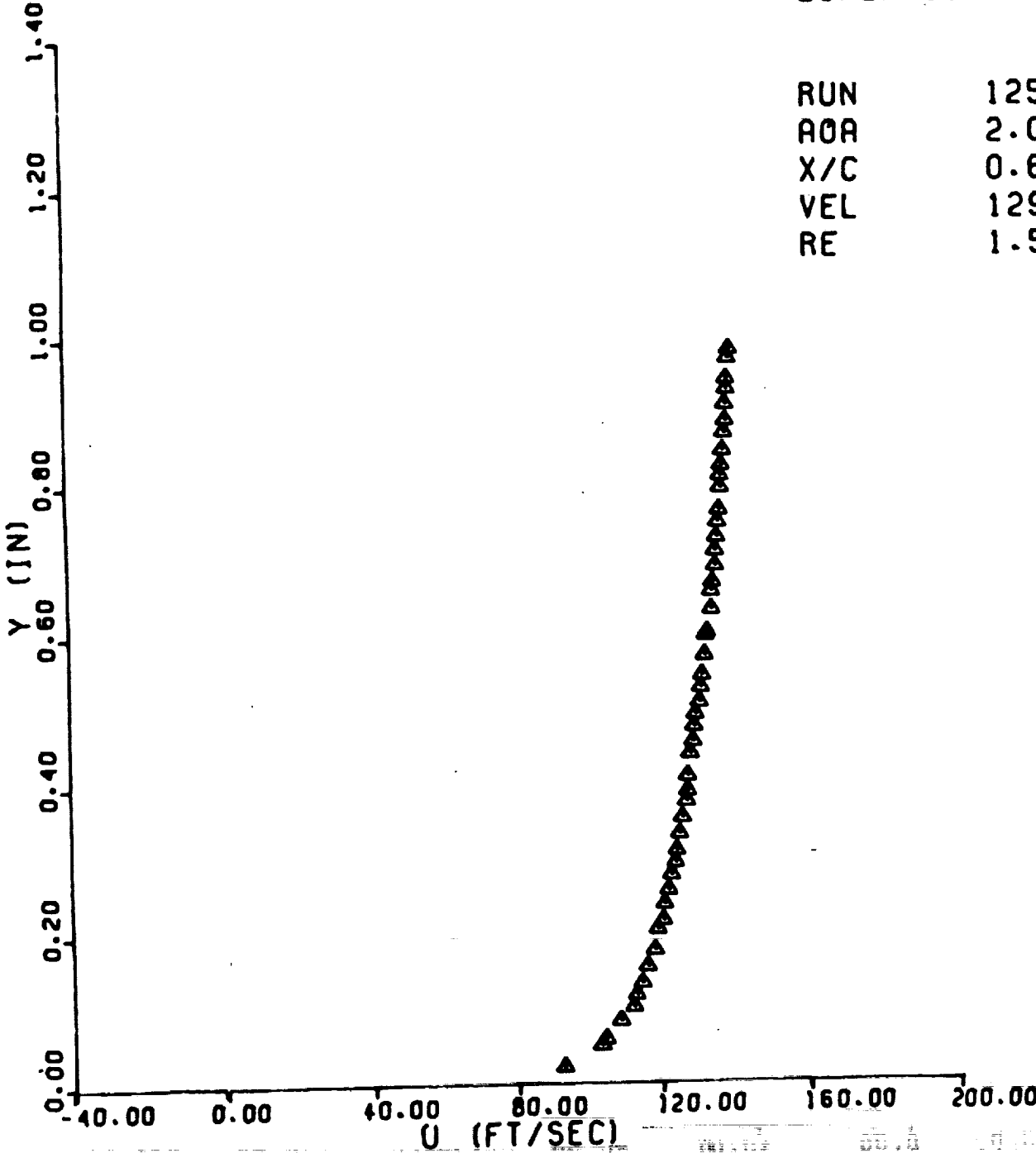
NACA 0012
LOWER SURFACE

RUN 1249
AOA 2.000
X/C 0.3200
VEL 129.8
RE 1.52



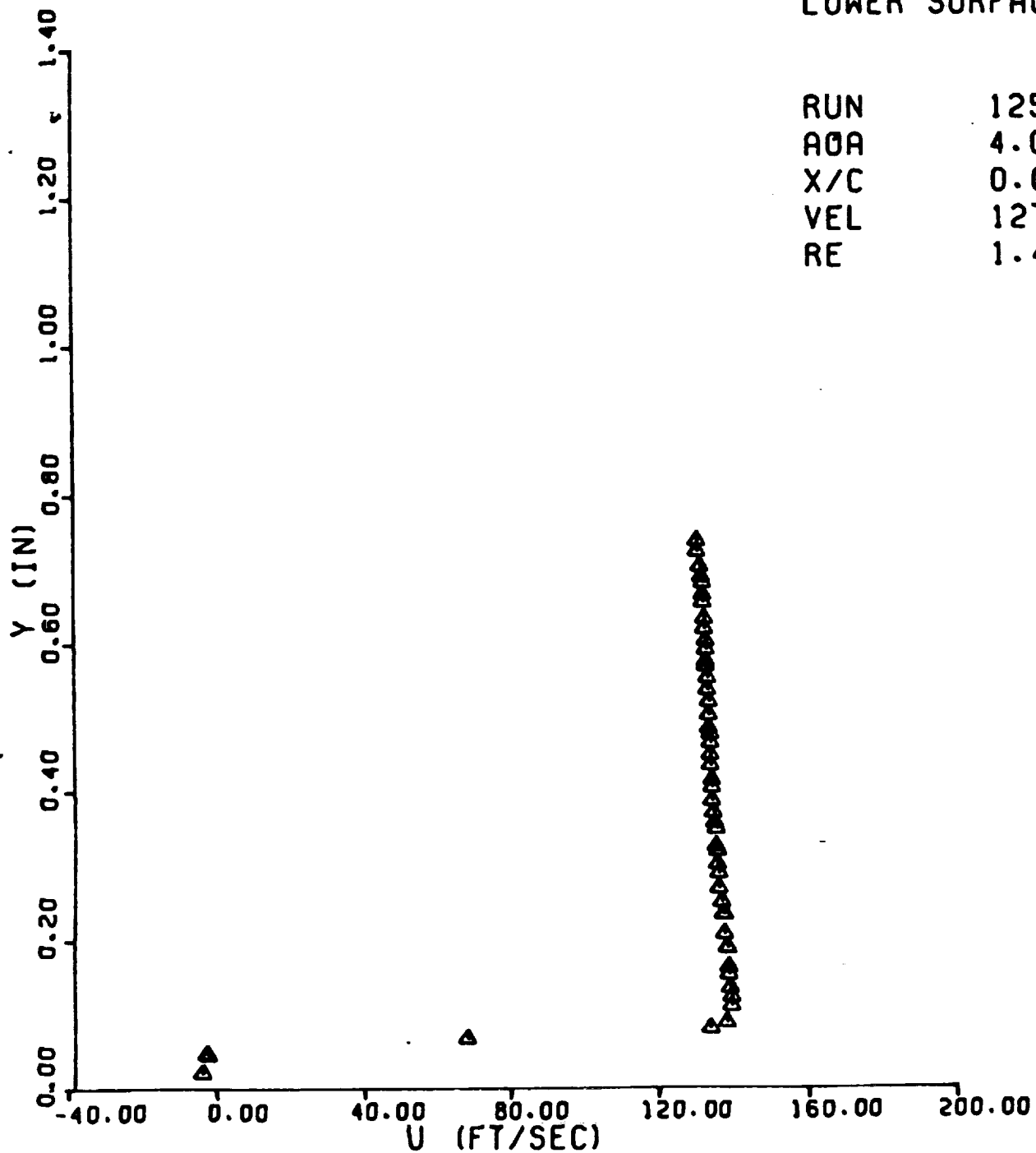
NACA 0012
LOWER SURFACE

RUN 1250
AOA 2.000
X/C 0.6000
VEL 129.6
RE 1.52



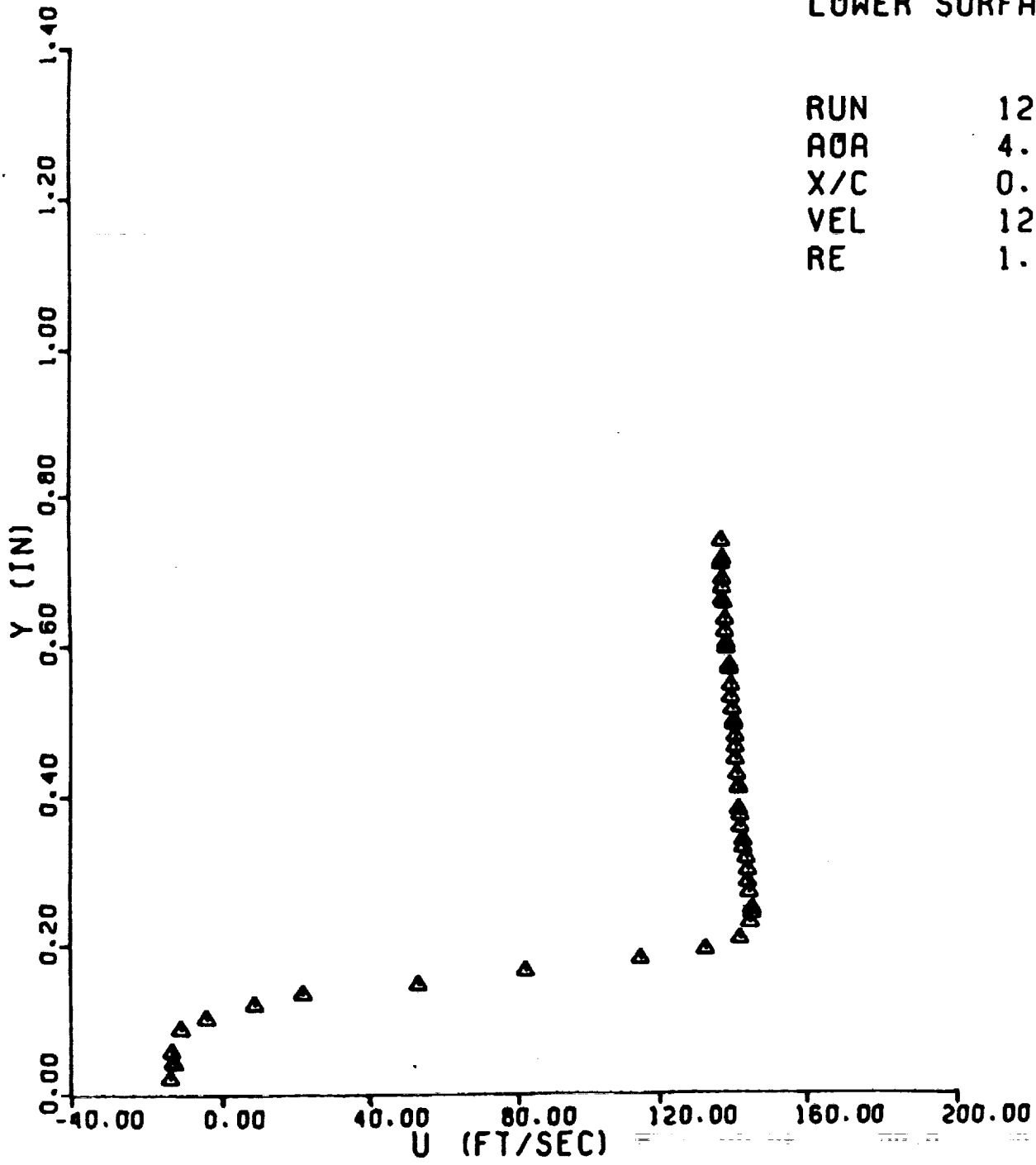
NACA 0012
LOWER SURFACE

RUN 1251
AOA 4.000
X/C 0.0300
VEL 127.1
RE 1.49



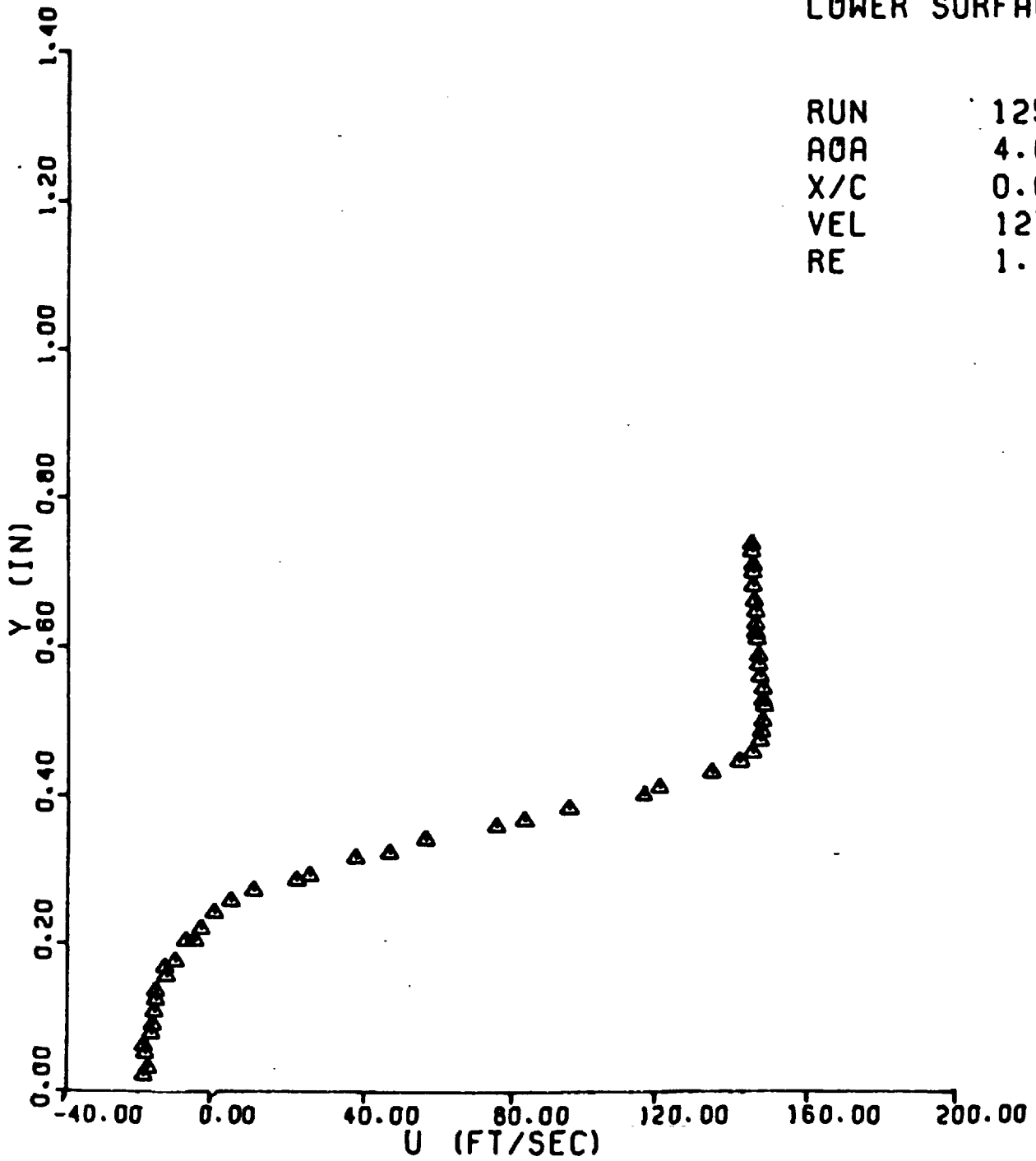
NACA 0012
LOWER SURFACE

RUN 1252
AOA 4.000
X/C 0.0400
VEL 127.7
RE 1.50



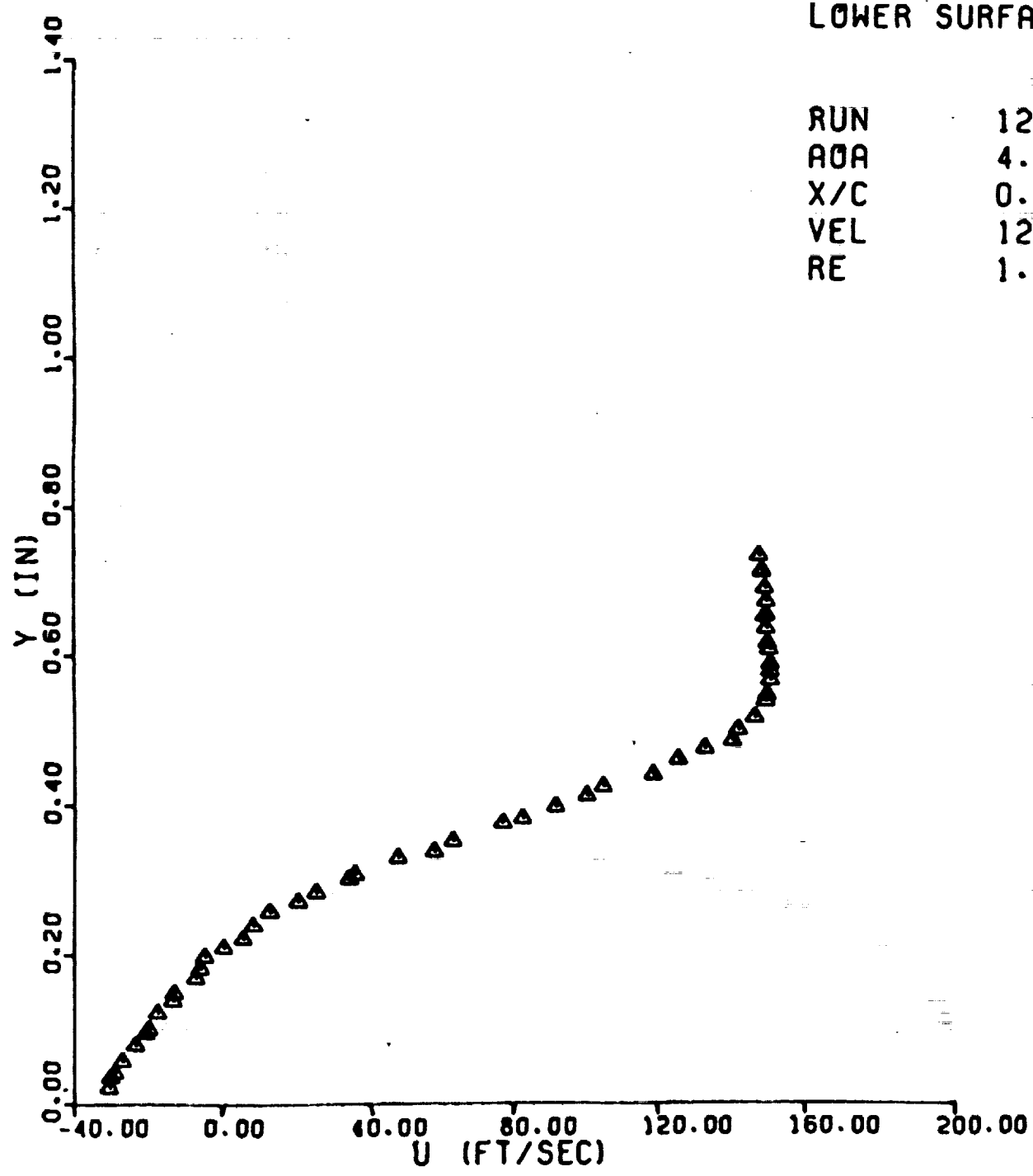
NACA 0012
LOWER SURFACE

RUN 1253
AOA 4.000
X/C 0.0600
VEL 127.3
RE 1.49



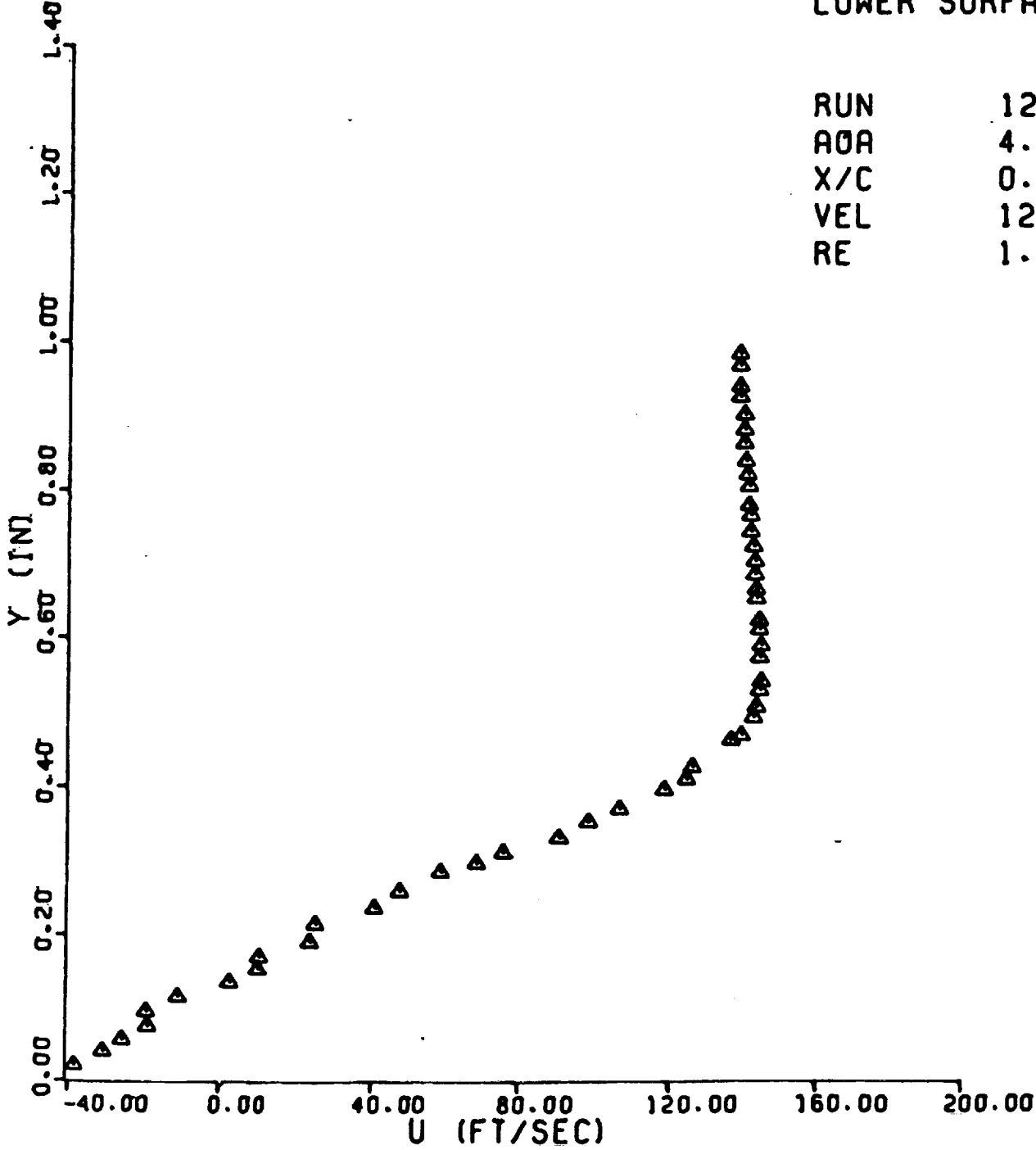
NACA 0012
LOWER SURFACE

RUN	1254
AOA	4.000
X/C	0.0800
VEL	127.7
RE	1.50



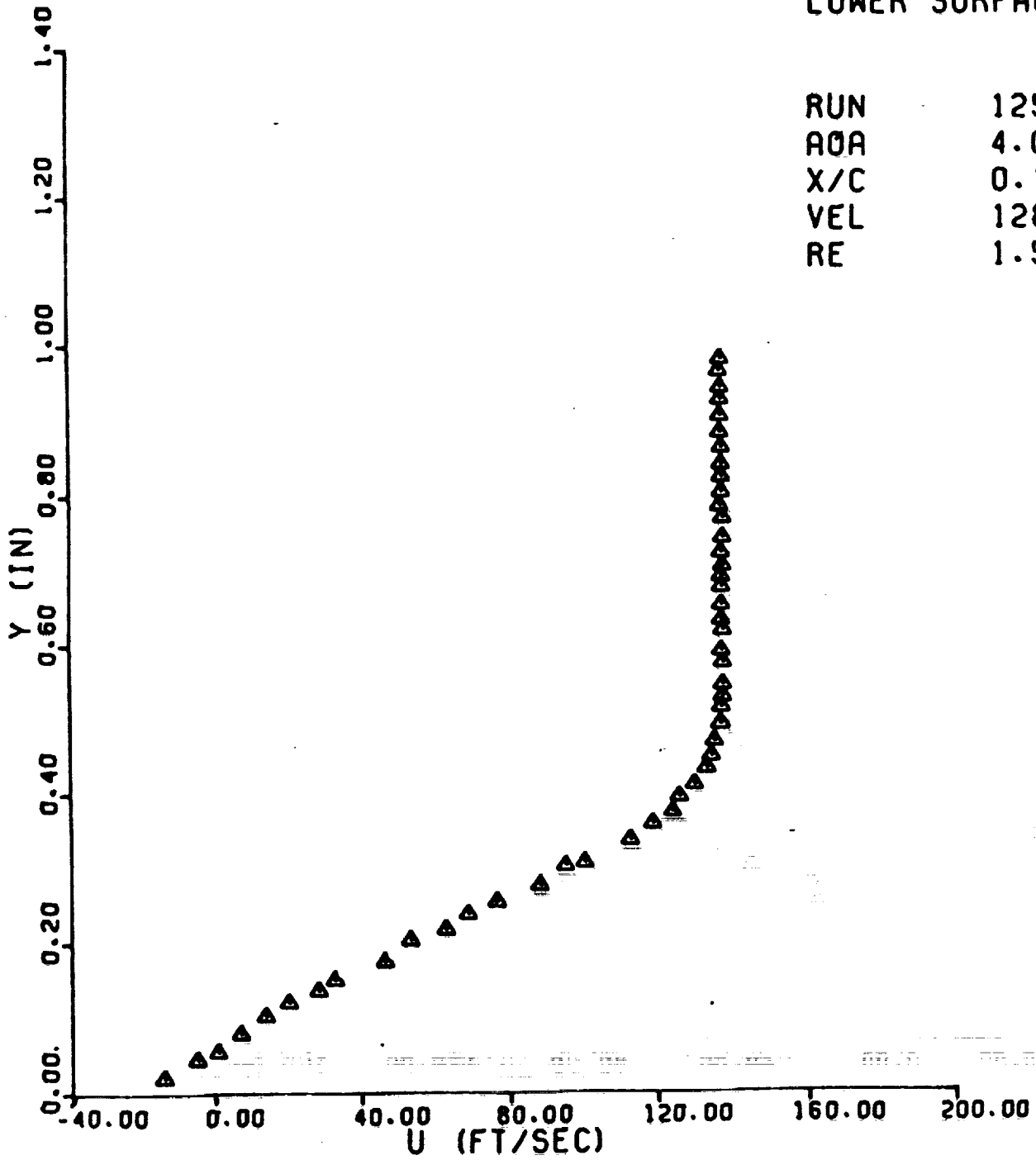
NACA 0012
LOWER SURFACE

RUN 1255
AOA 4.000
X/C 0.1000
VEL 127.8
RE 1.50



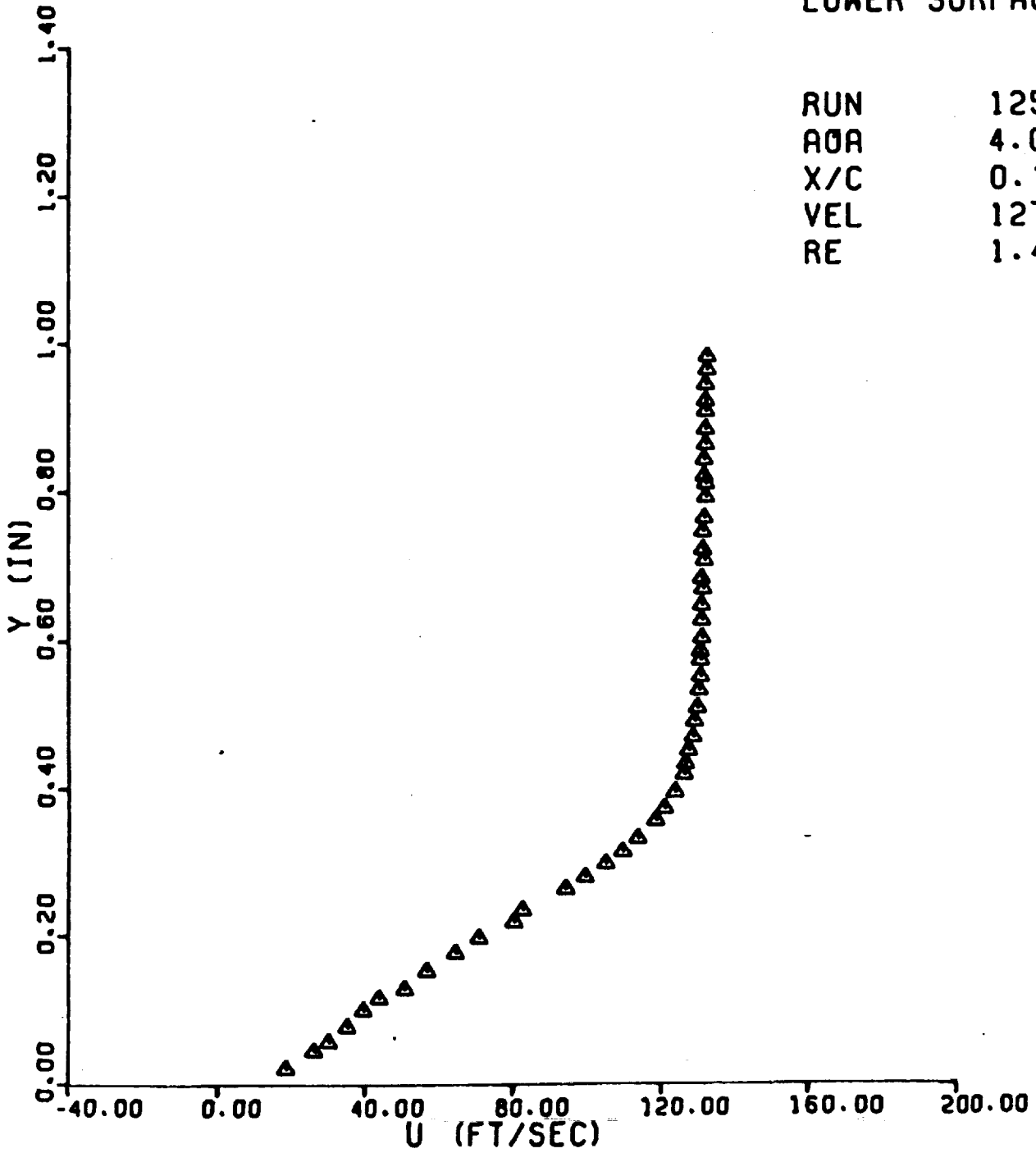
NACA 0012
LOWER SURFACE

RUN 1256
AOA 4.000
X/C 0.1200
VEL 128.0
RE 1.50



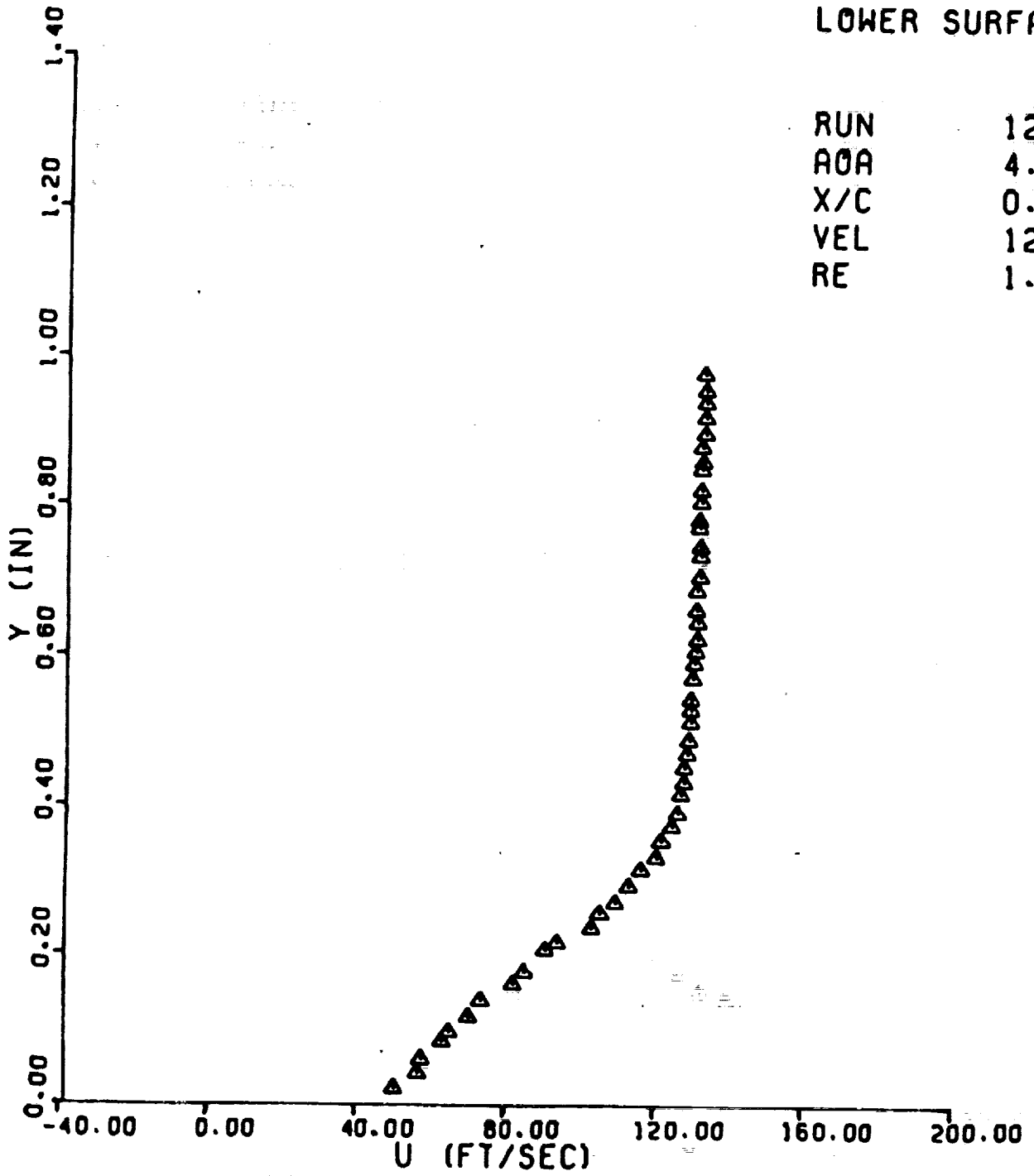
NACA 0012
LOWER SURFACE

RUN	1257
AOA	4.000
X/C	0.1400
VEL	127.6
RE	1.49



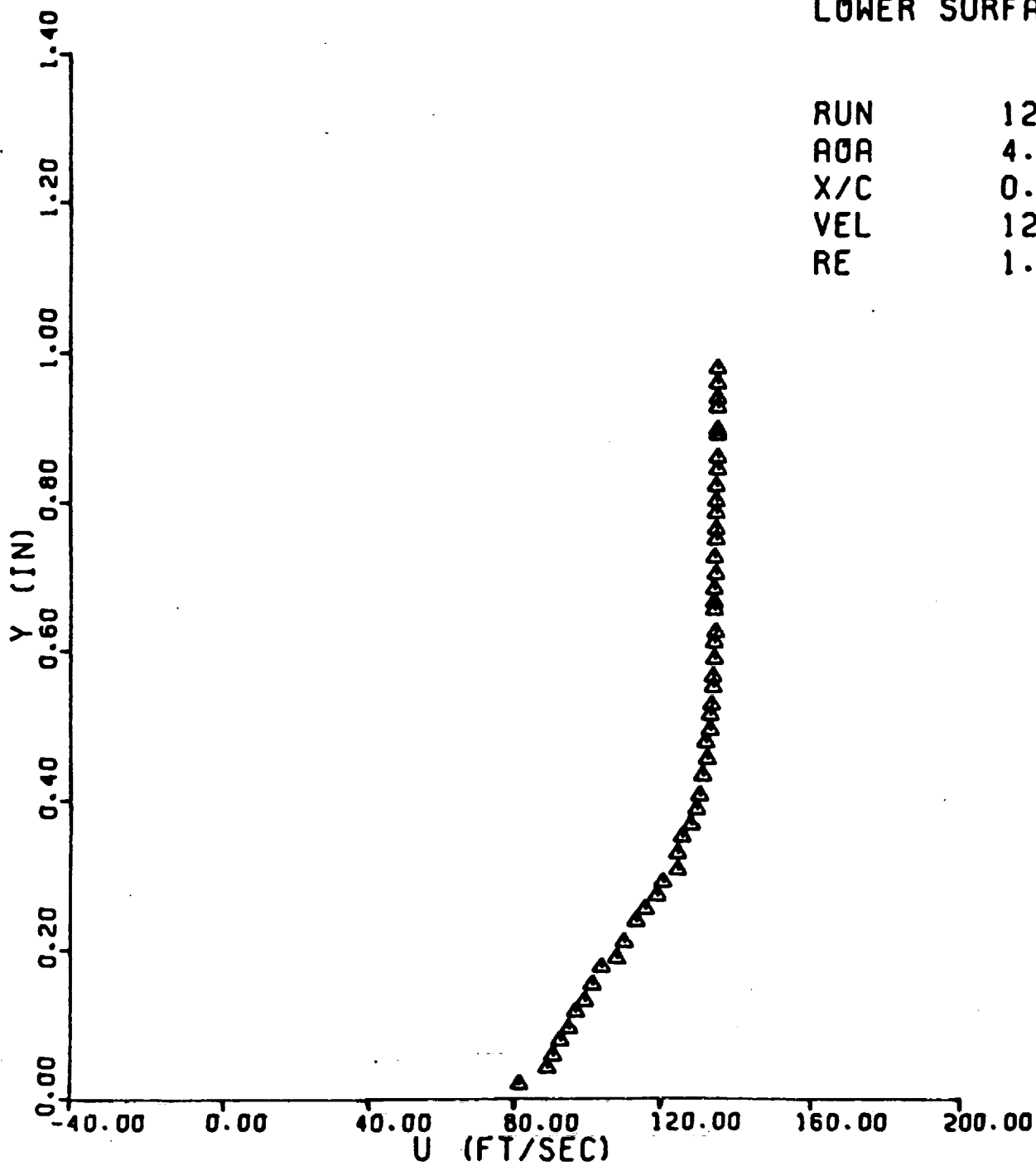
NACA 0012
LOWER SURFACE

RUN	1258
AOA	4.000
X/C	0.1600
VEL	127.8
RE	1.49



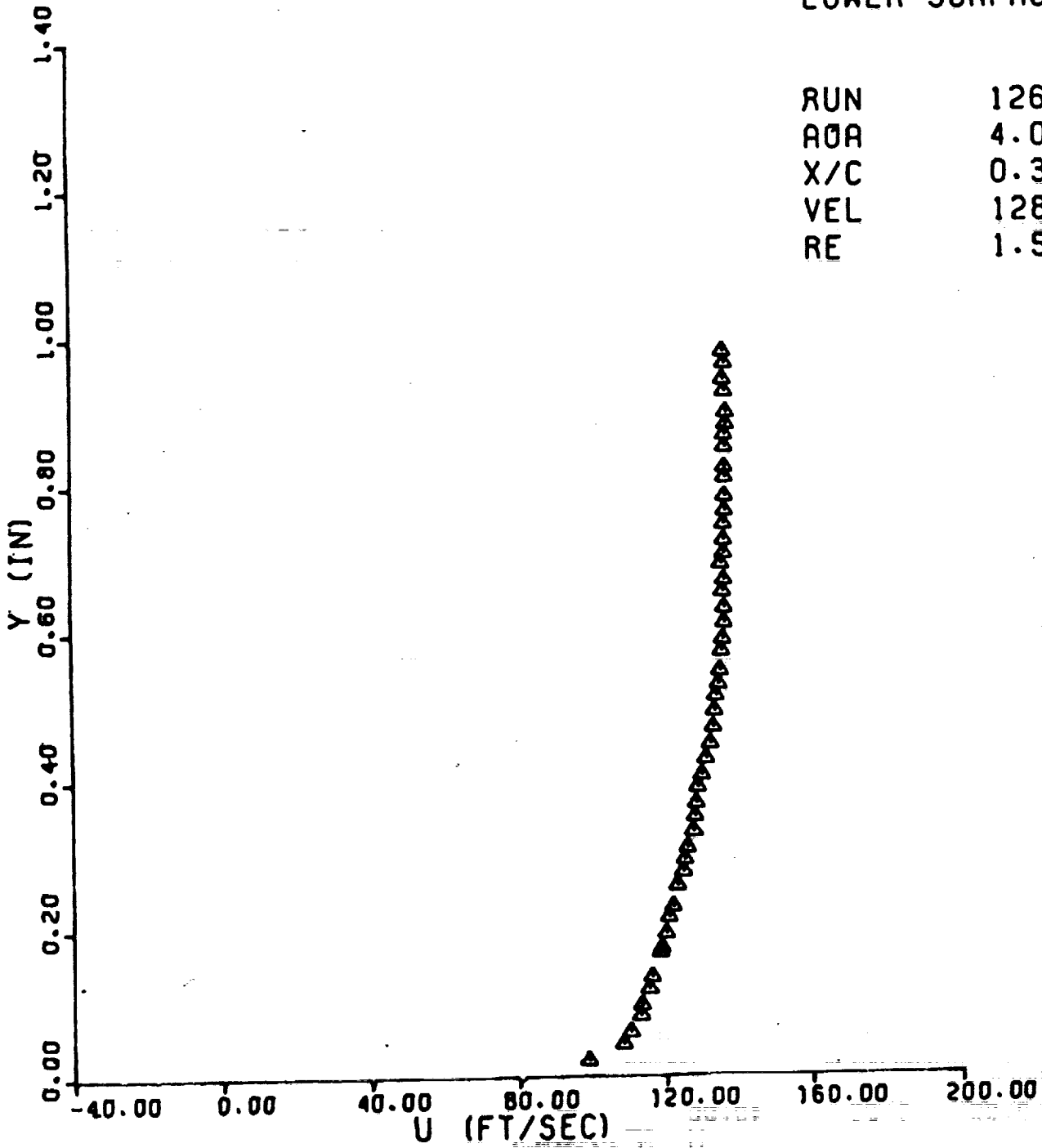
NACA 0012
LOWER SURFACE

RUN	1259
AOA	4.000
X/C	0.2000
VEL	128.3
RE	1.50



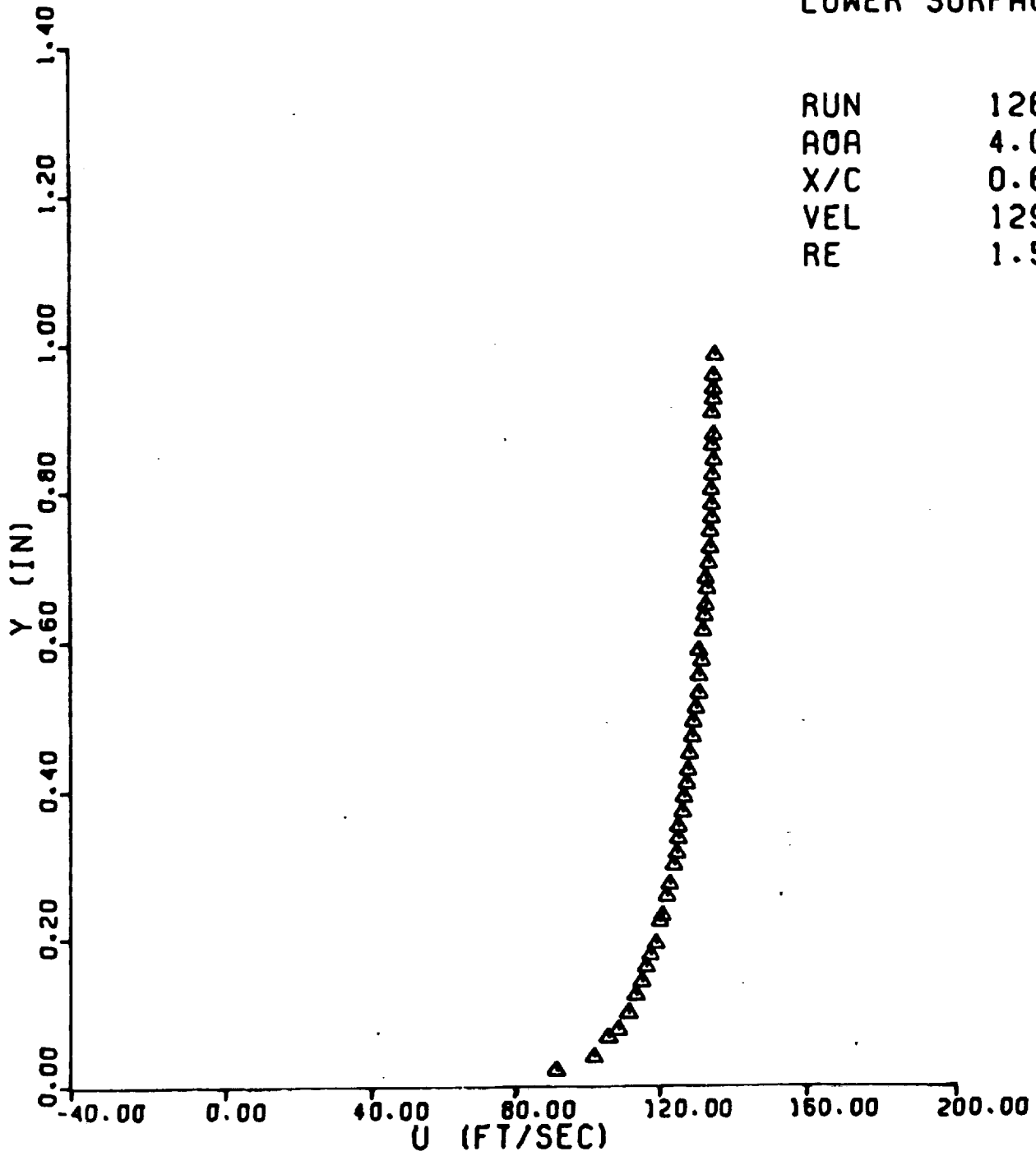
NACA 0012
LOWER SURFACE

RUN	1260
AOA	4.000
X/C	0.3200
VEL	128.8
RE	1.51



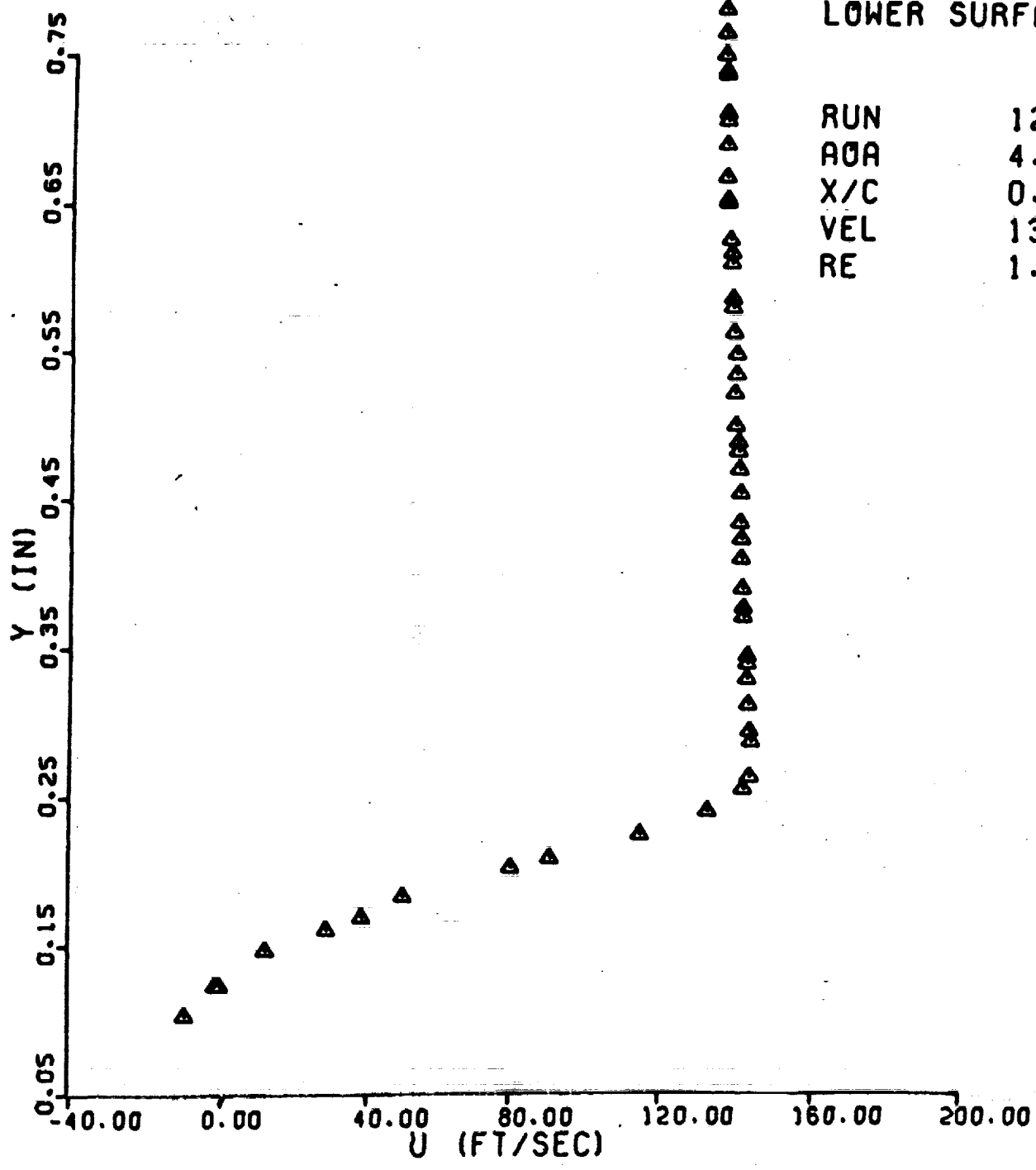
NACA 0012
LOWER SURFACE

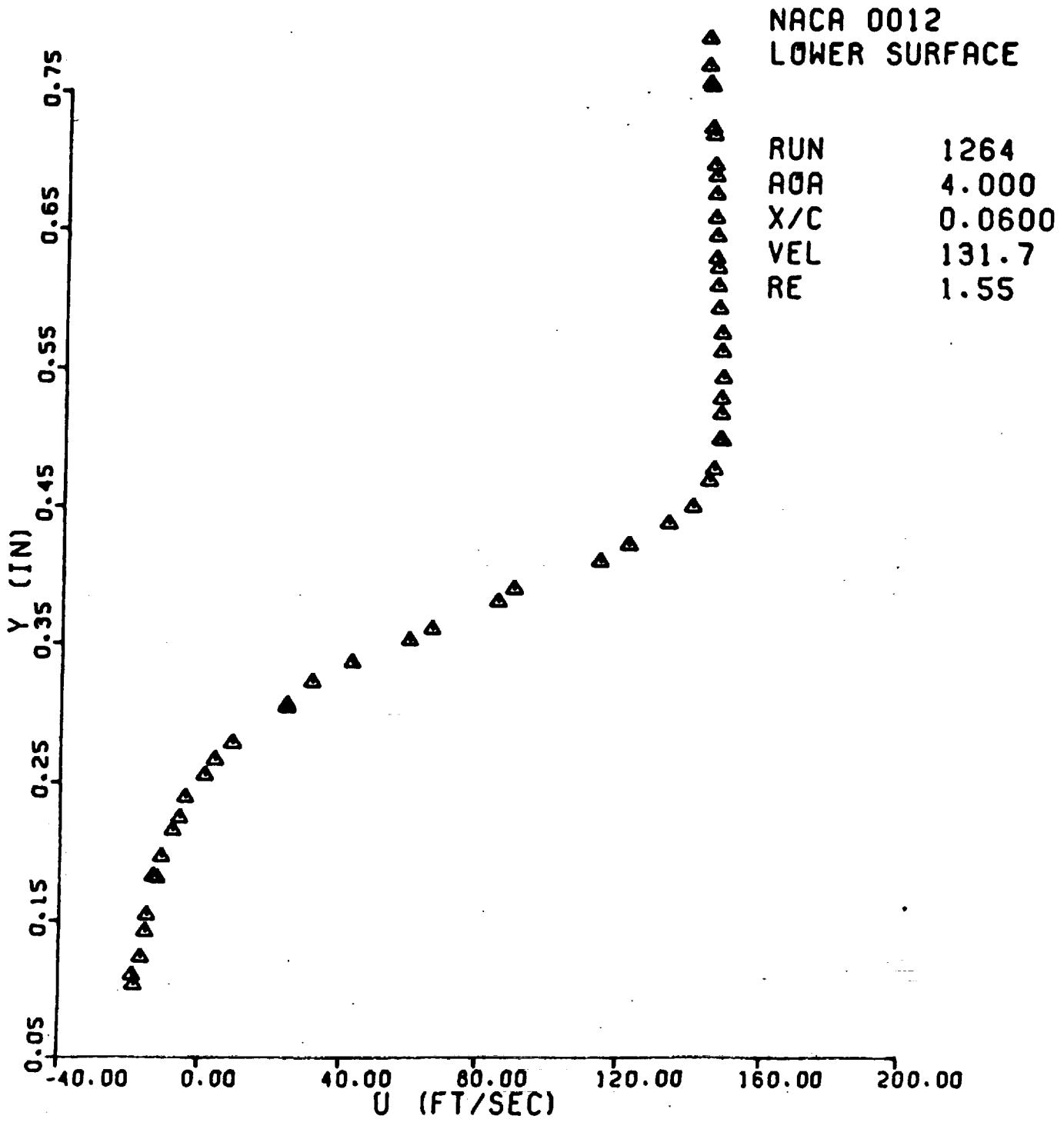
RUN	1261
AOA	4.000
X/C	0.6000
VEL	129.3
RE	1.52



NACA 0012
LOWER SURFACE

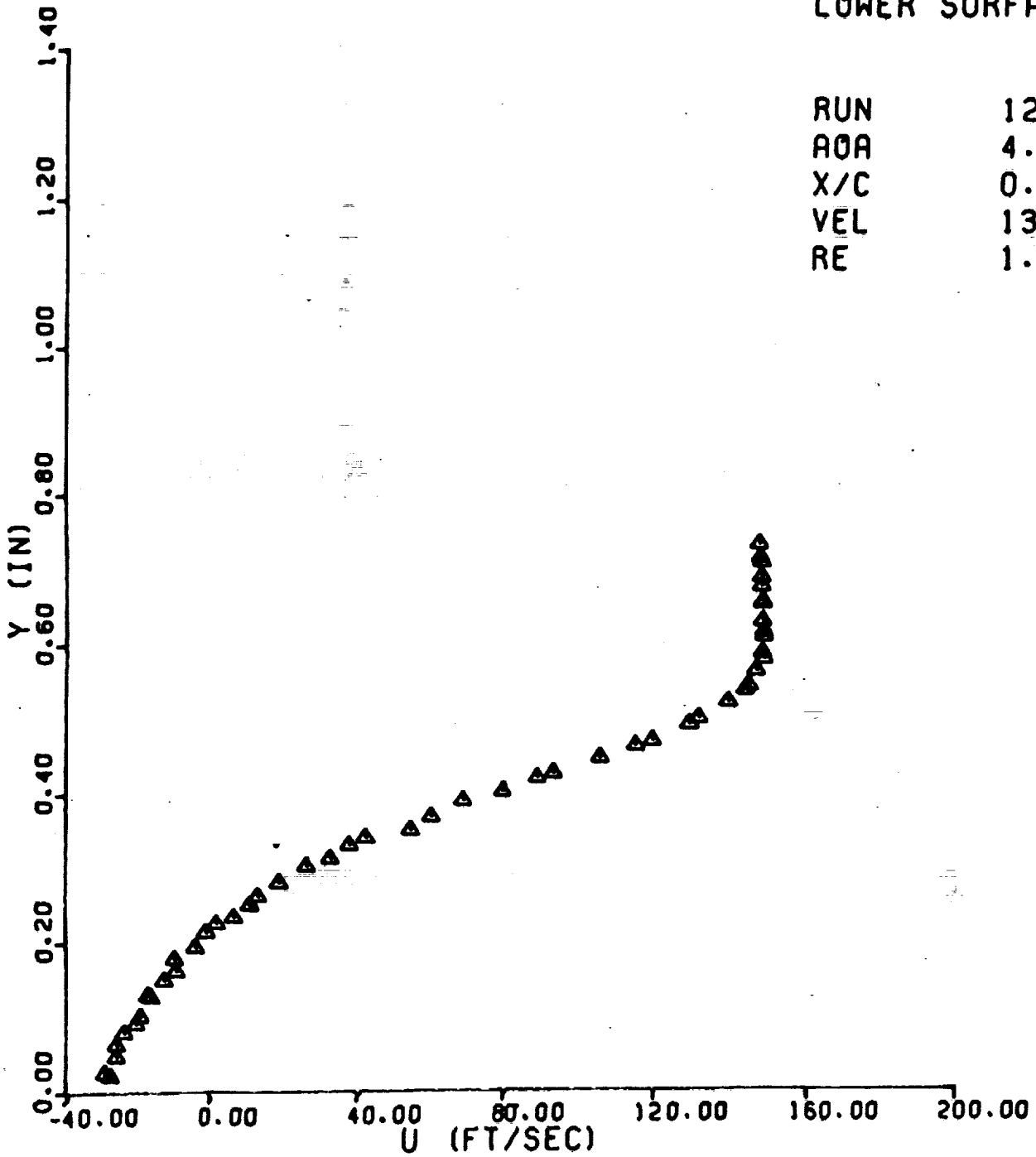
RUN 1263
AOA 4.000
X/C 0.0400
VEL 131.1
RE 1.54





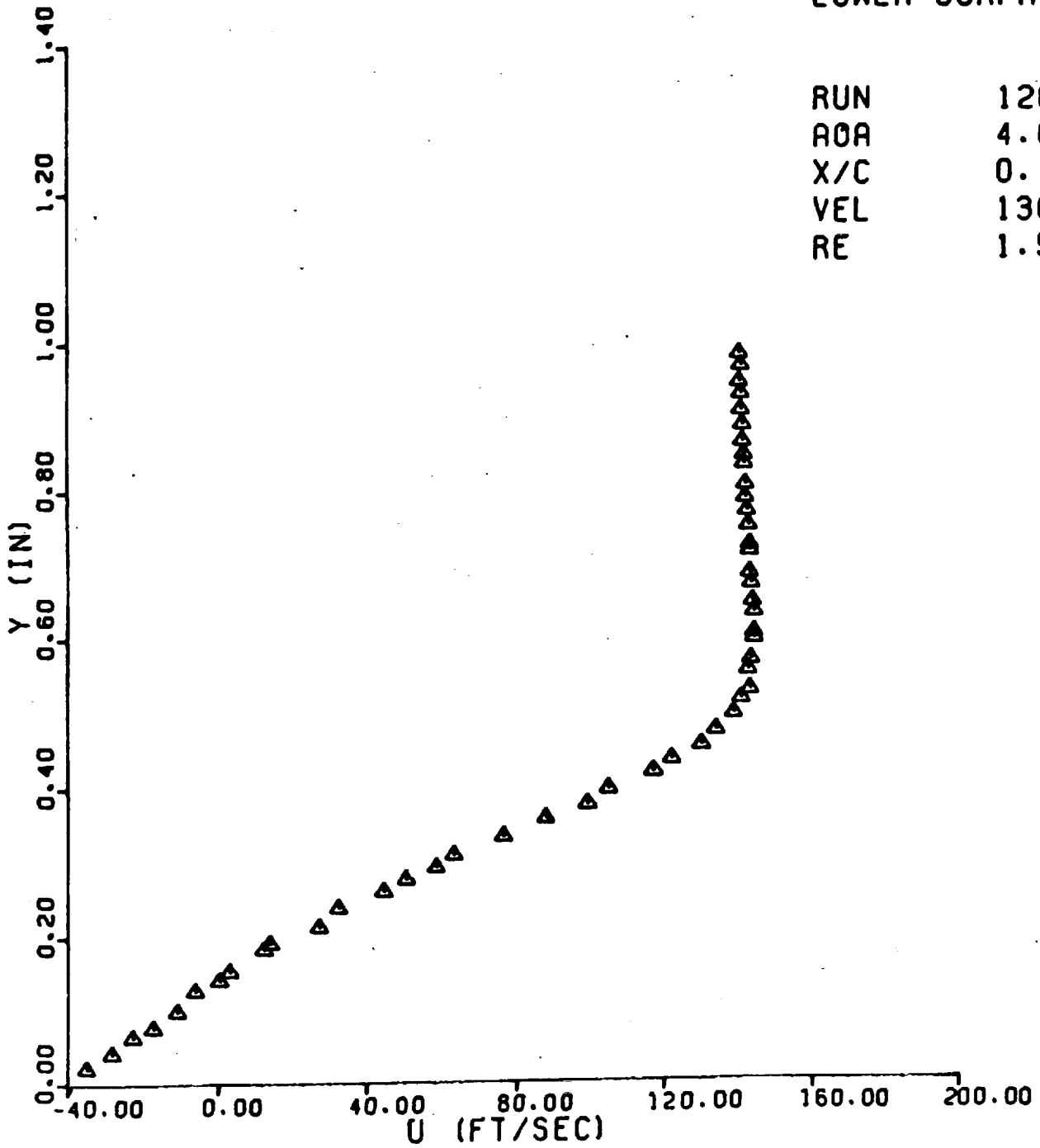
NACA 0012
LOWER SURFACE

RUN	1265
AOA	4.000
X/C	0.0800
VEL	131.0
RE	1.54



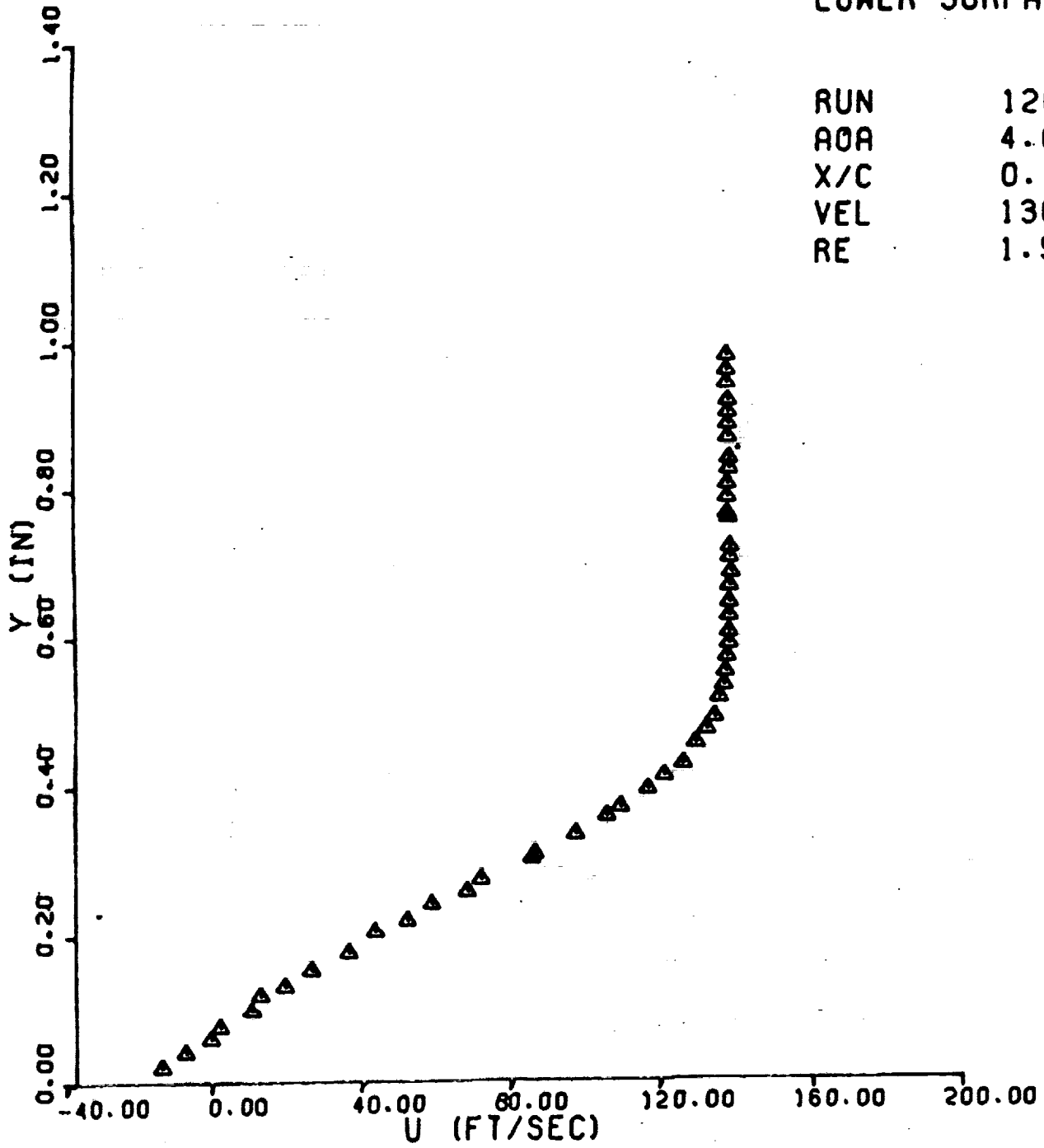
NACA 0012
LOWER SURFACE

RUN	1266
AOA	4.000
X/C	0.1000
VEL	130.9
RE	1.54



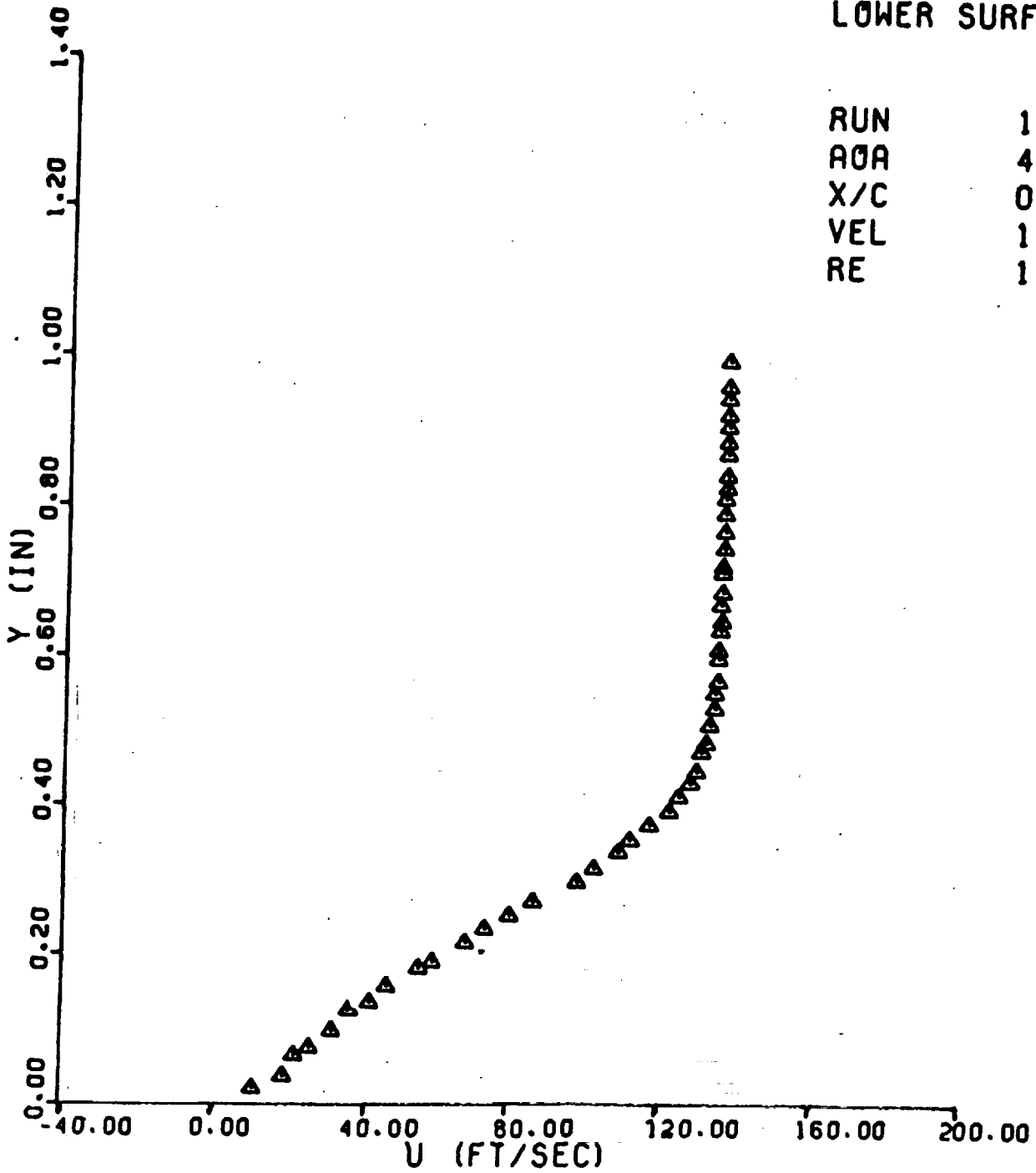
NACA 0012
LOWER SURFACE

RUN 1267
AOA 4.000
X/C 0.1200
VEL 130.5
RE 1.53



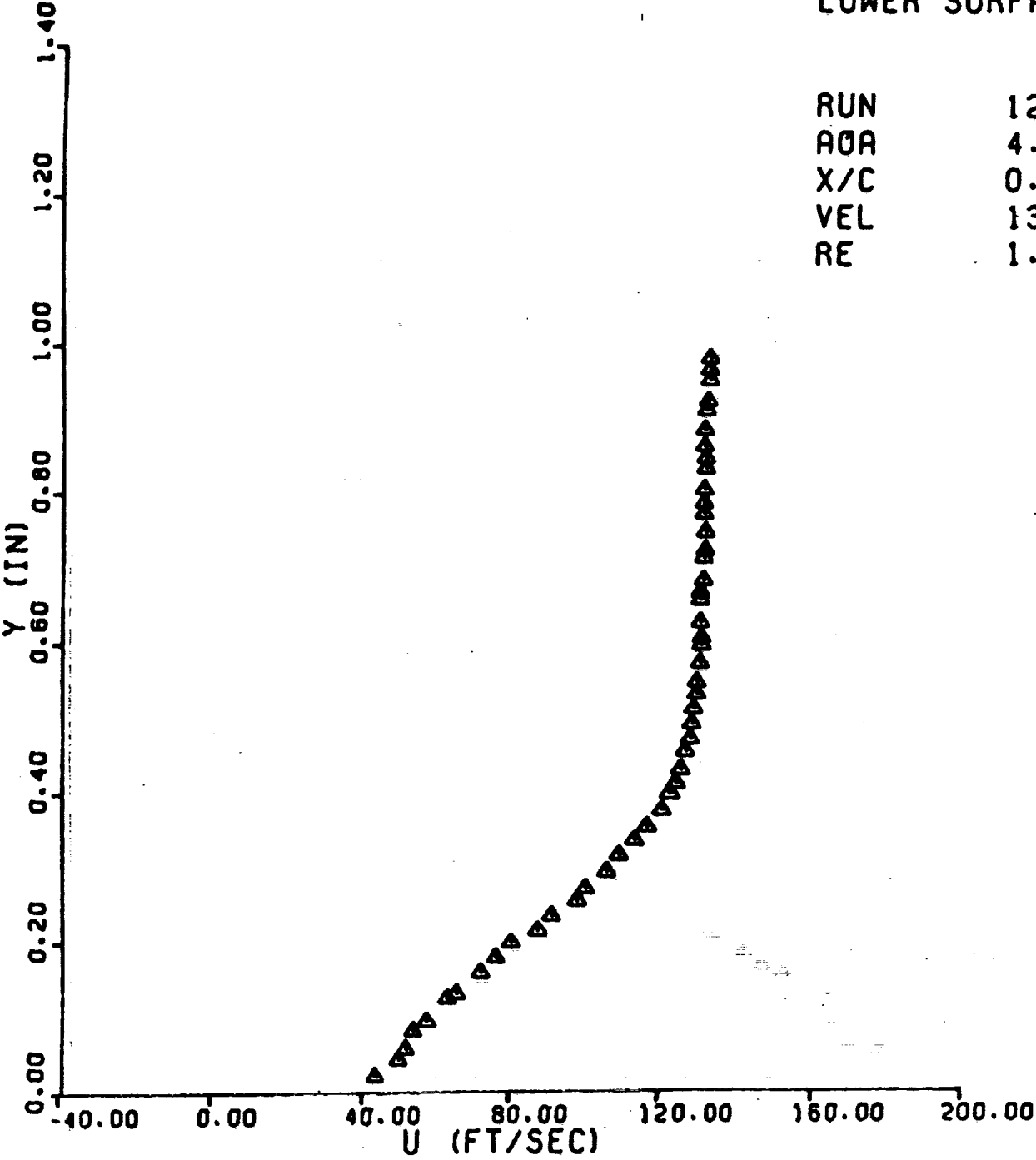
NACA 0012
LOWER SURFACE

RUN 1268
AOA 4.000
X/C 0.1400
VEL 130.9
RE 1.54



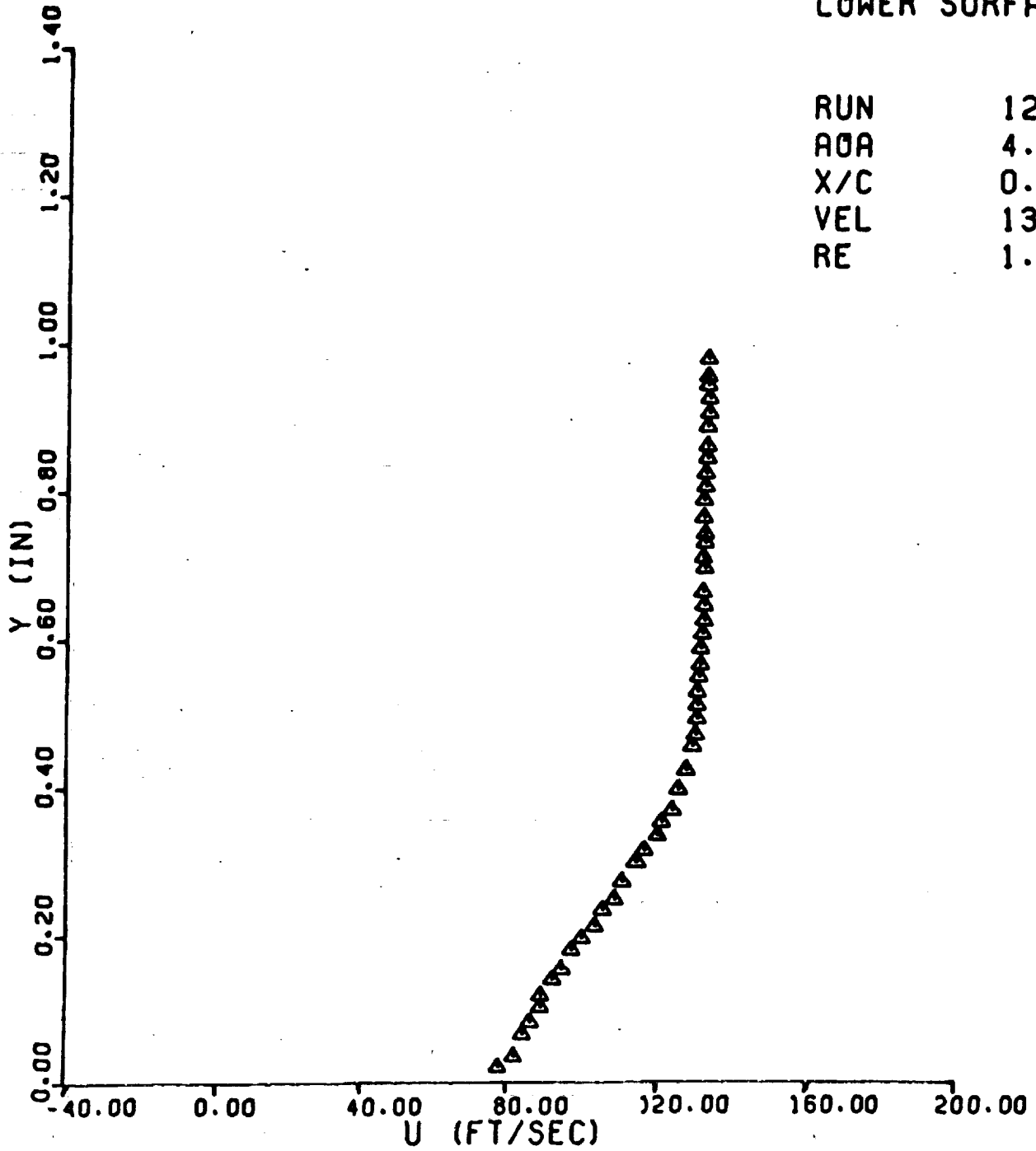
NACA 0012
LOWER SURFACE

RUN 1269
AOA 4.000
X/C 0.1600
VEL 130.7
RE 1.53



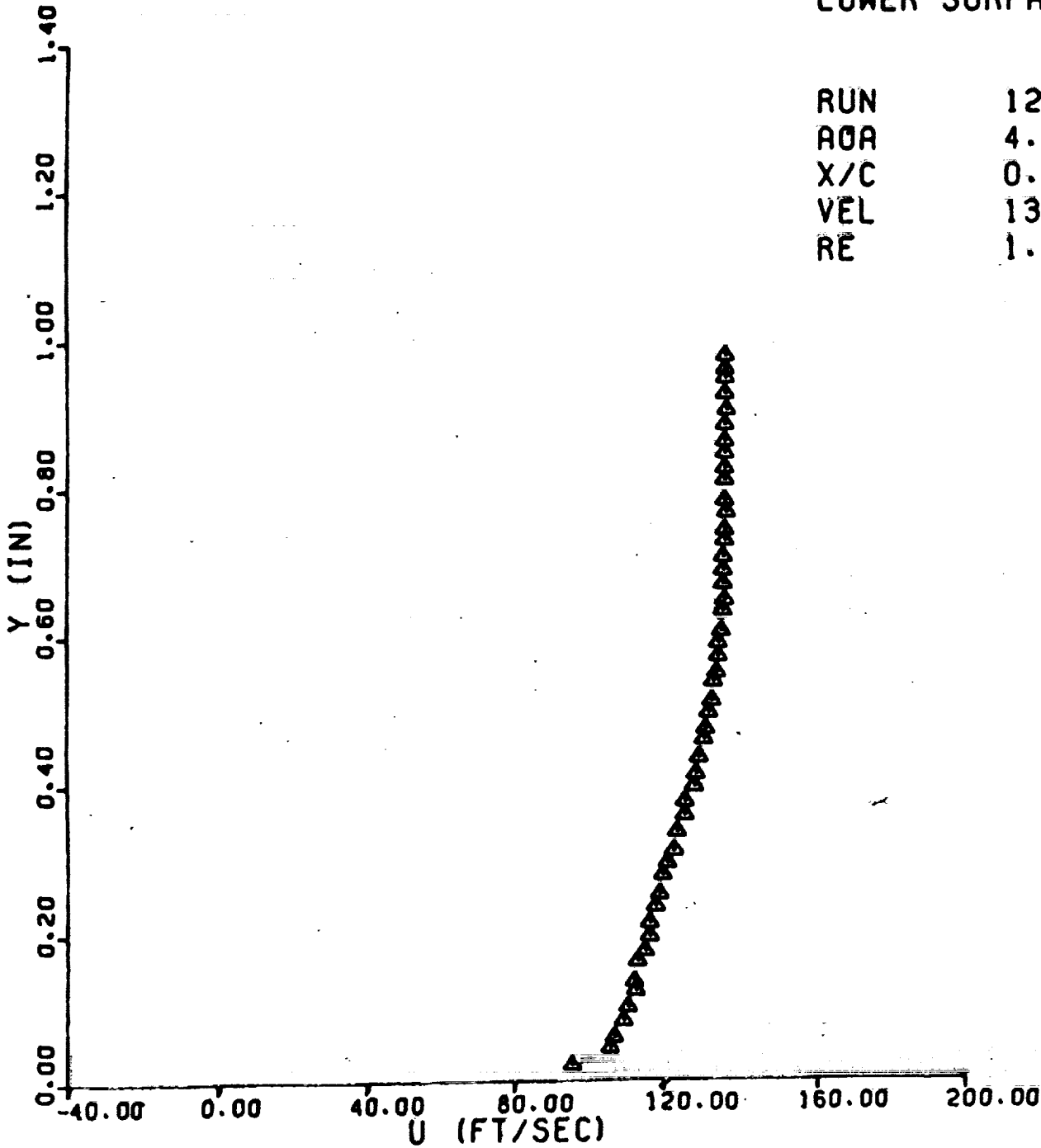
NACA 0012
LOWER SURFACE

RUN 1270
AOA 4.000
X/C 0.2000
VEL 131.0
RE 1.54



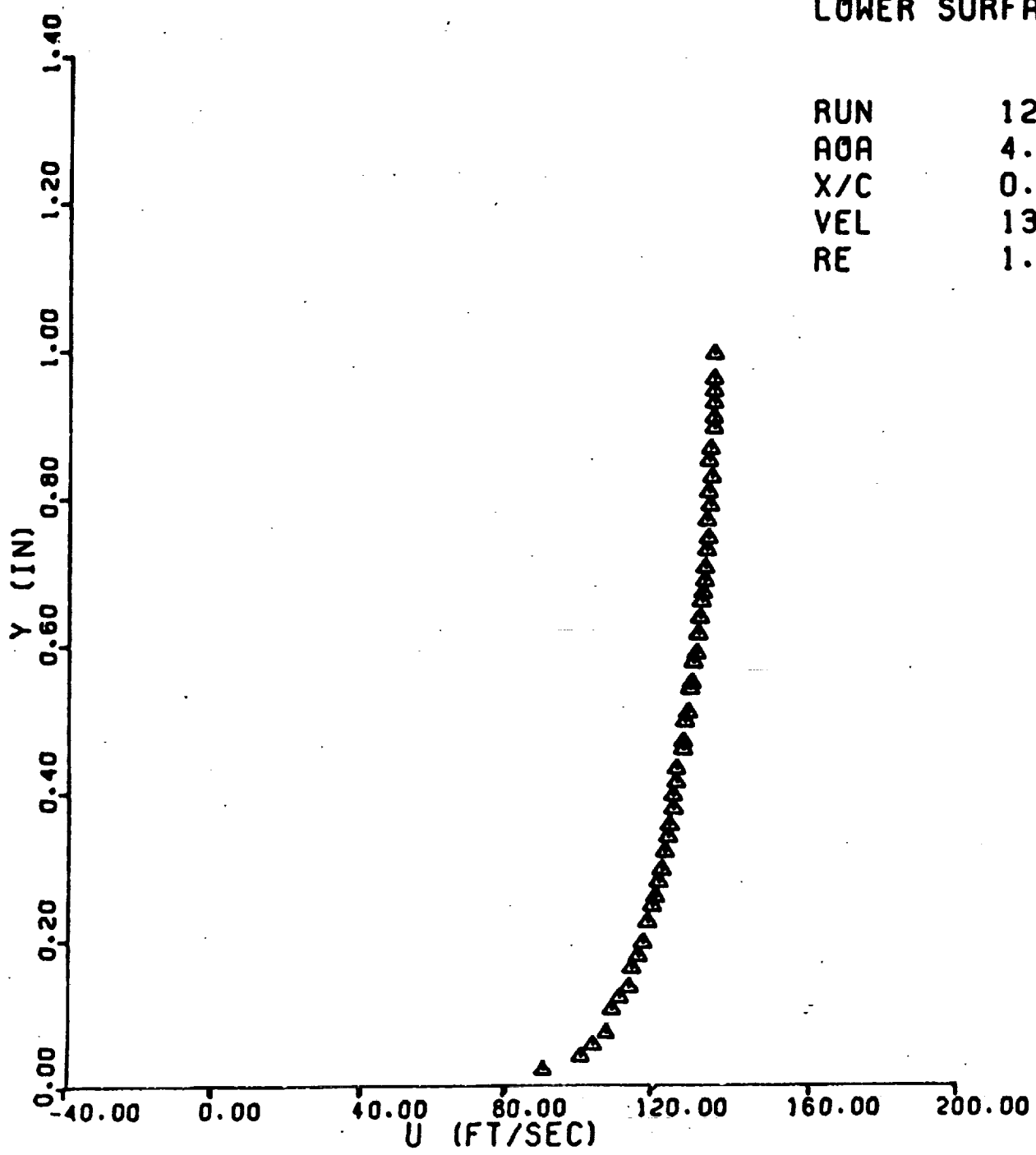
NACA 0012
LOWER SURFACE

RUN 1271
AOA 4.000
X/C 0.3200
VEL 130.6
RE 1.53



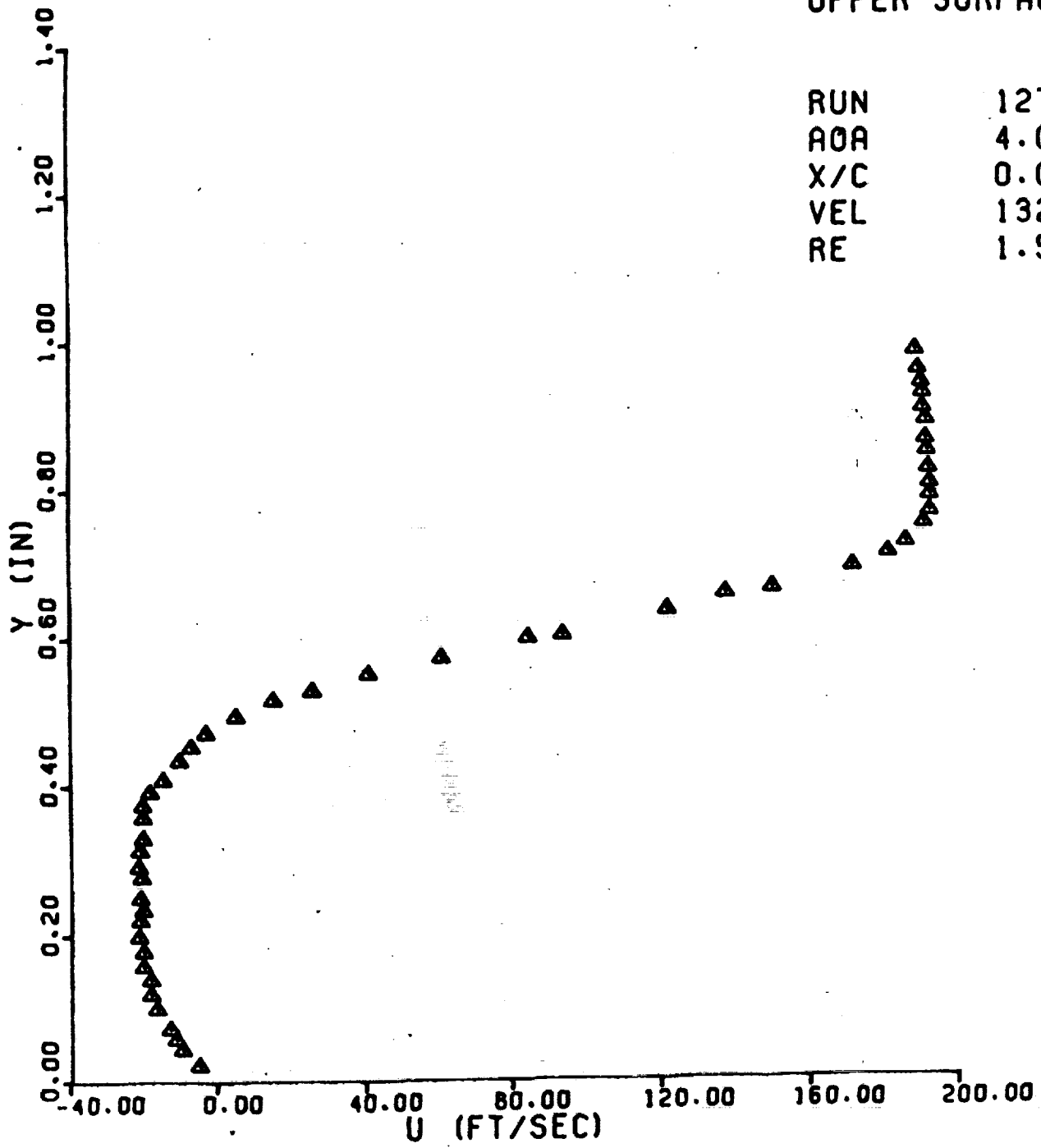
NACA 0012
LOWER SURFACE

RUN 1272
AOA 4.000
X/C 0.6000
VEL 131.1
RE 1.54



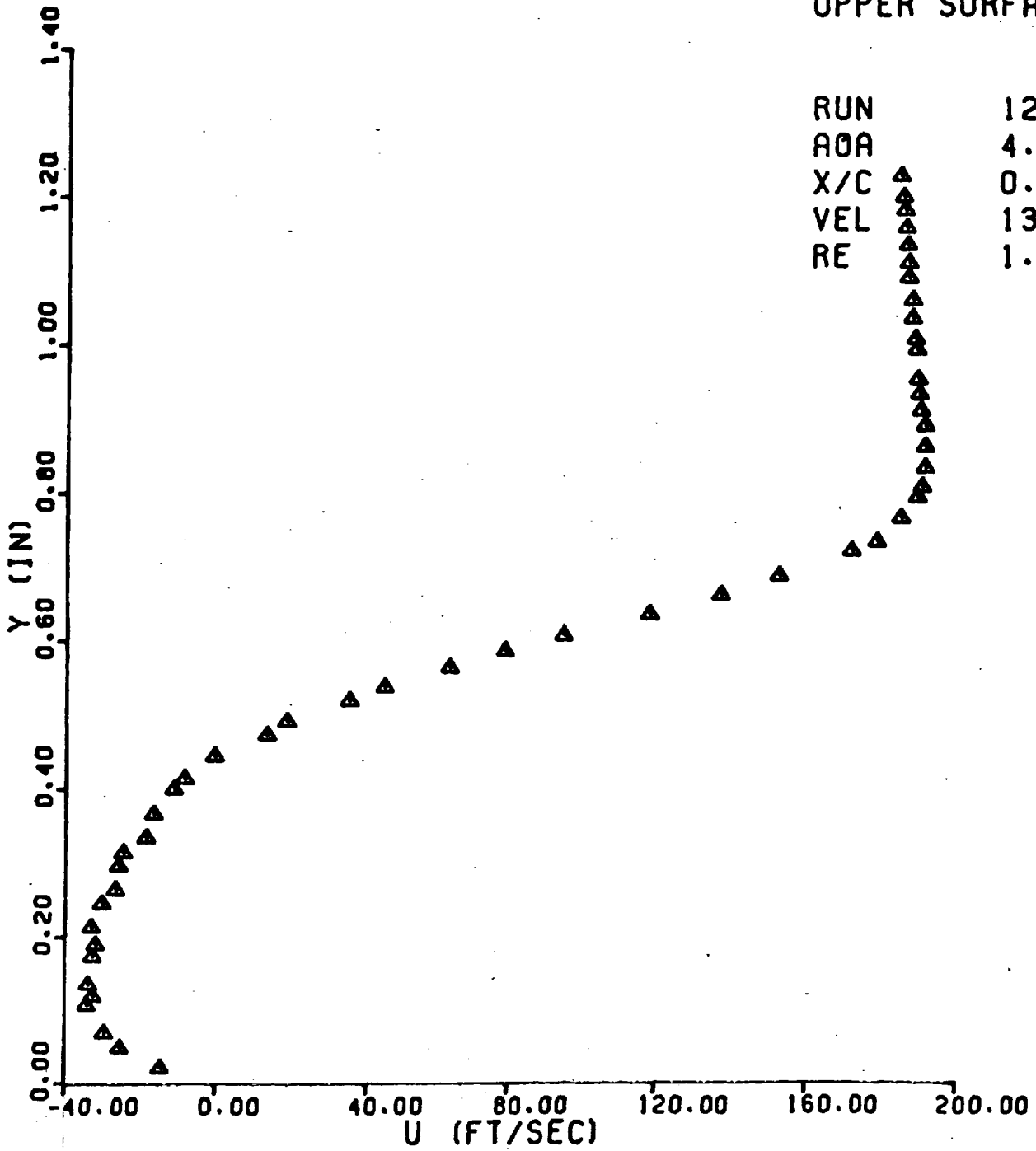
NACA 0012
UPPER SURFACE

RUN	1276
AOA	4.000
X/C	0.0200
VEL	132.3
RE	1.56



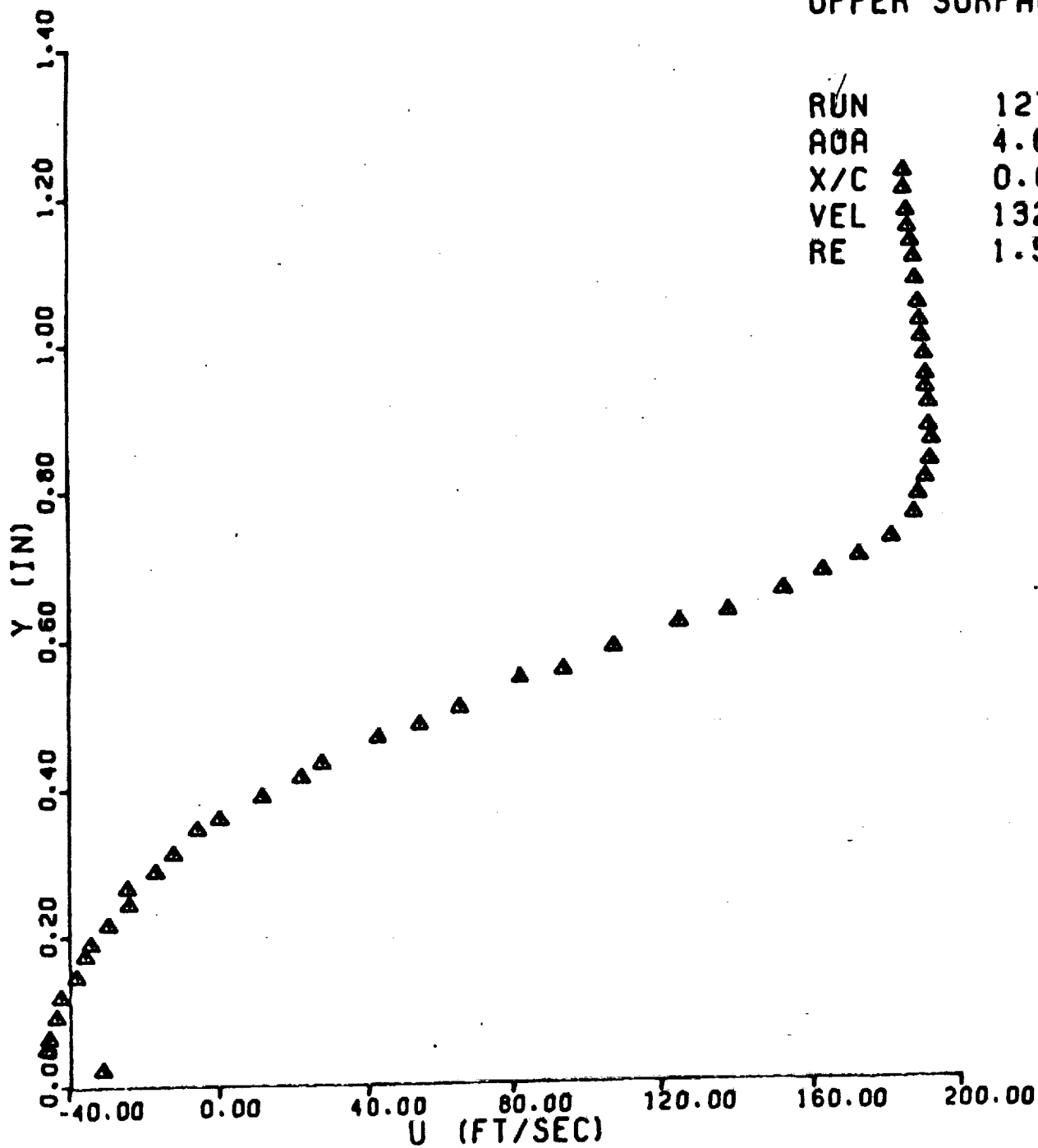
NACA 0012
UPPER SURFACE

RUN 1277
AOA 4.000
X/C 0.0400
VEL 132.8
RE 1.56

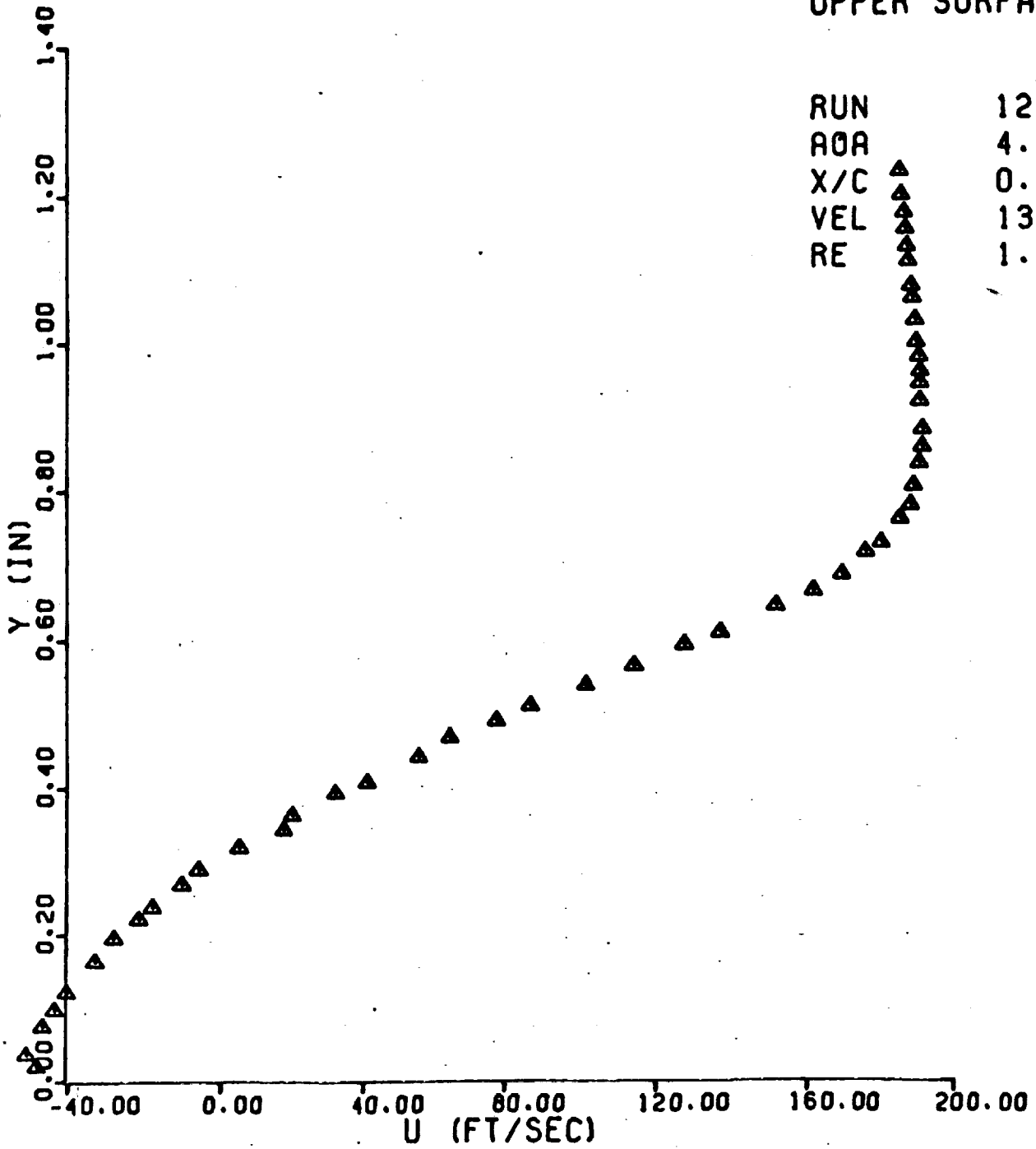


NACA 0012
UPPER SURFACE

RUN 1278
AOA 4.000
X/C Δ 0.0600
VEL 132.1
RE 1.56



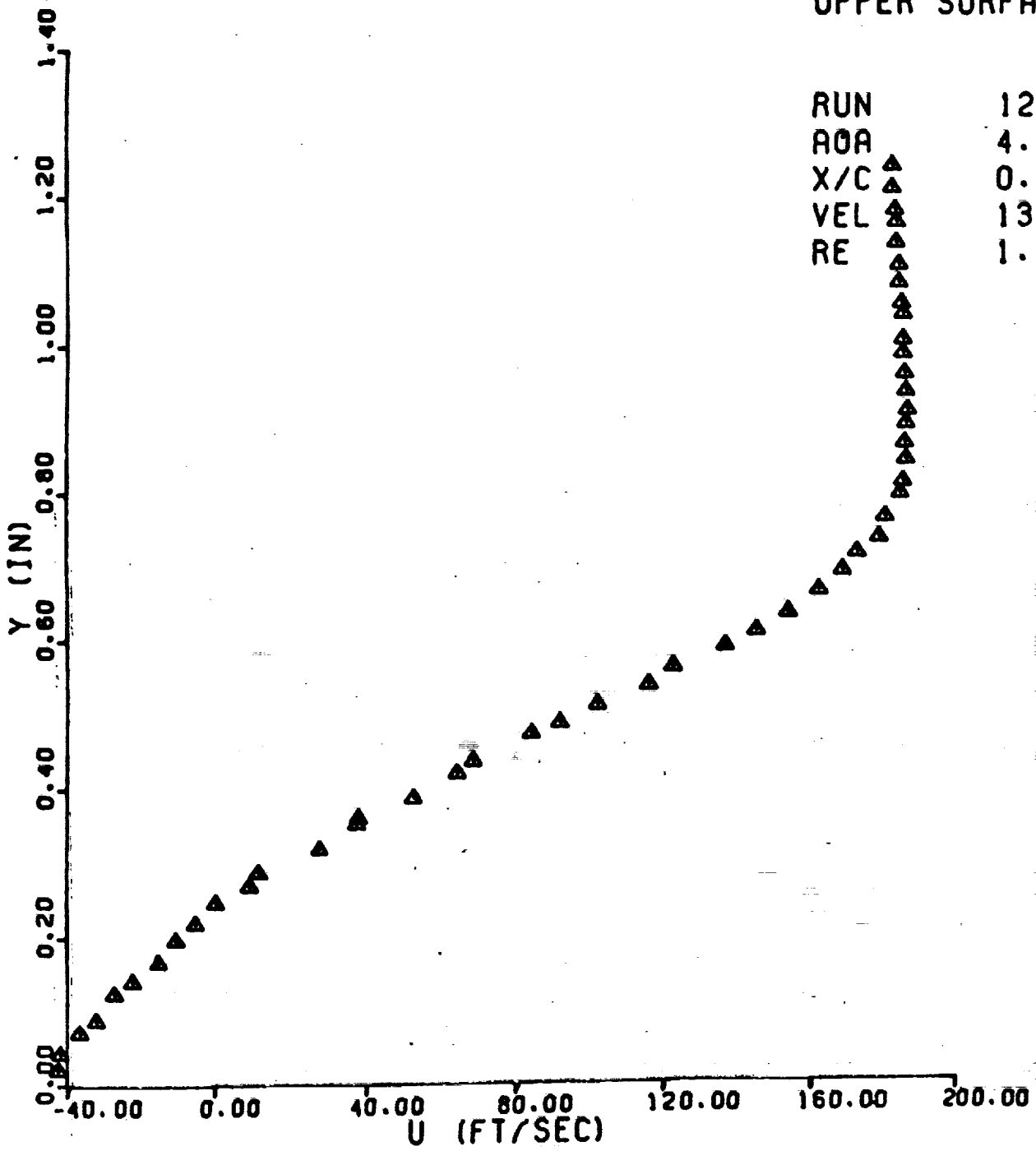
NACA 0012
UPPER SURFACE



RUN 1279
AOA 4.000
X/C 0.0800
VEL 132.3
RE 1.56

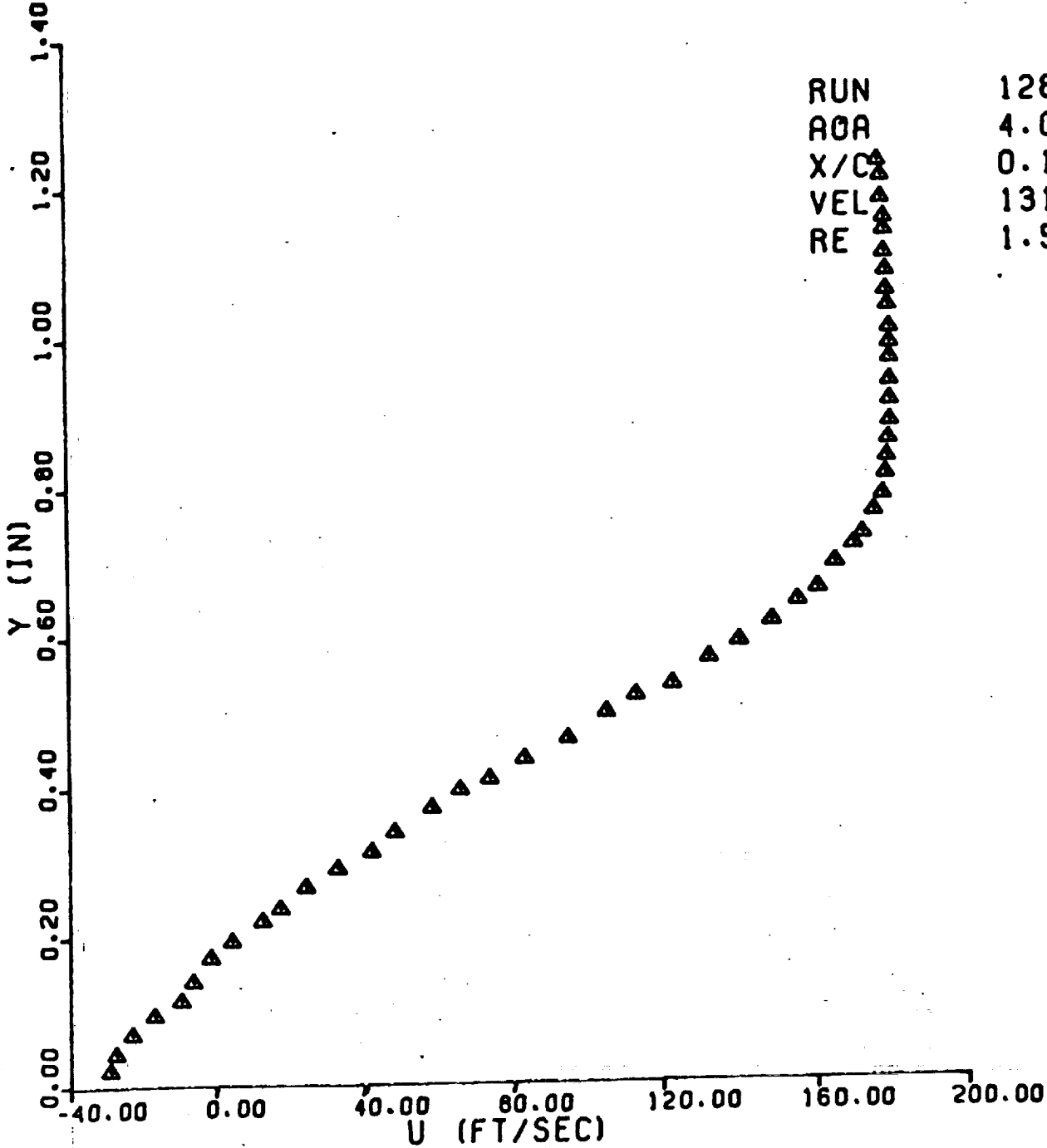
NACA 0012
UPPER SURFACE

RUN	1280
AOA	4.000
X/C	0.1000
VEL	132.3
RE	1.56

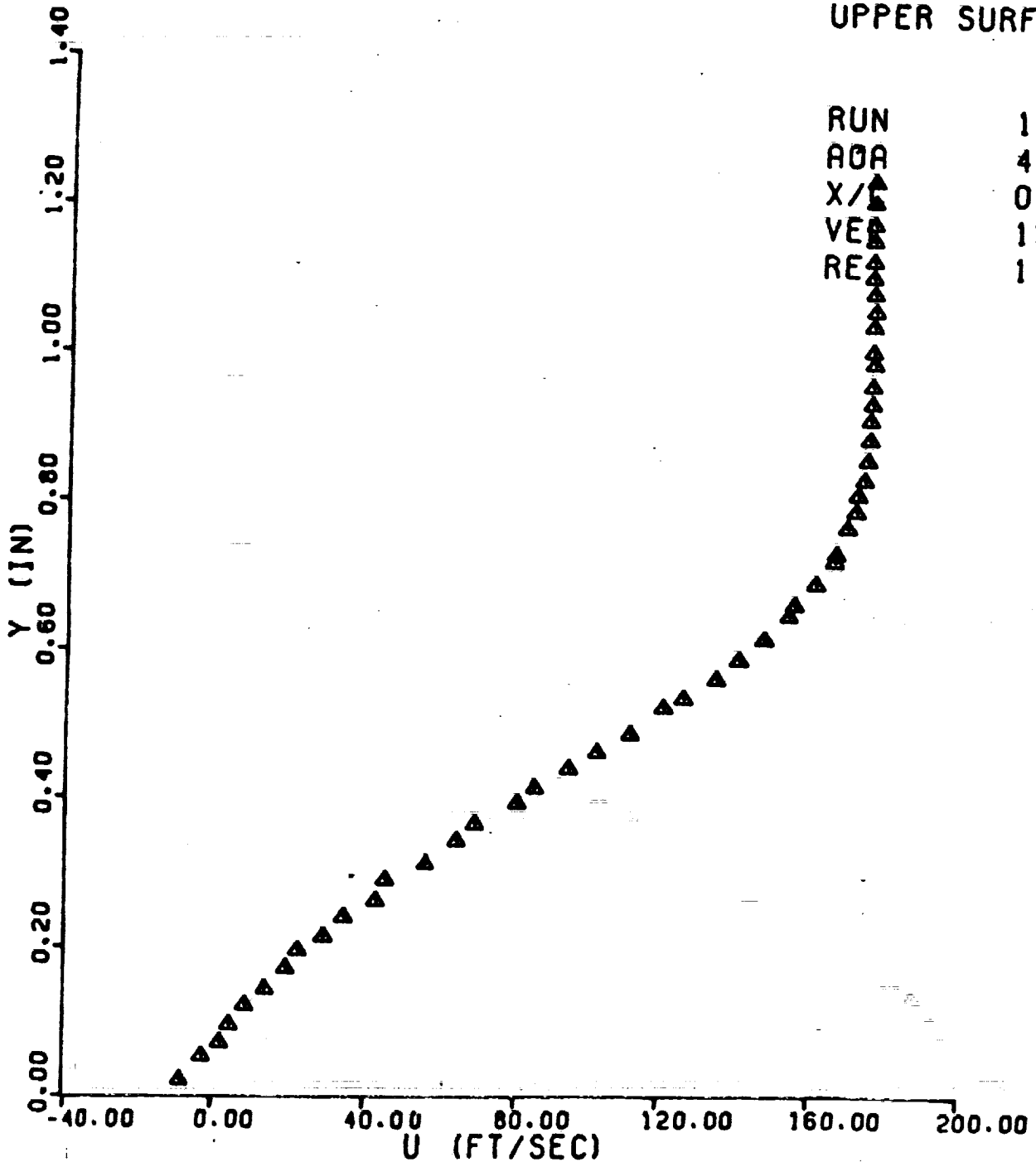


NACA 0012
UPPER SURFACE

RUN	1281
AOA	4.000
X/C	0.1200
VEL	131.3
RE	1.55

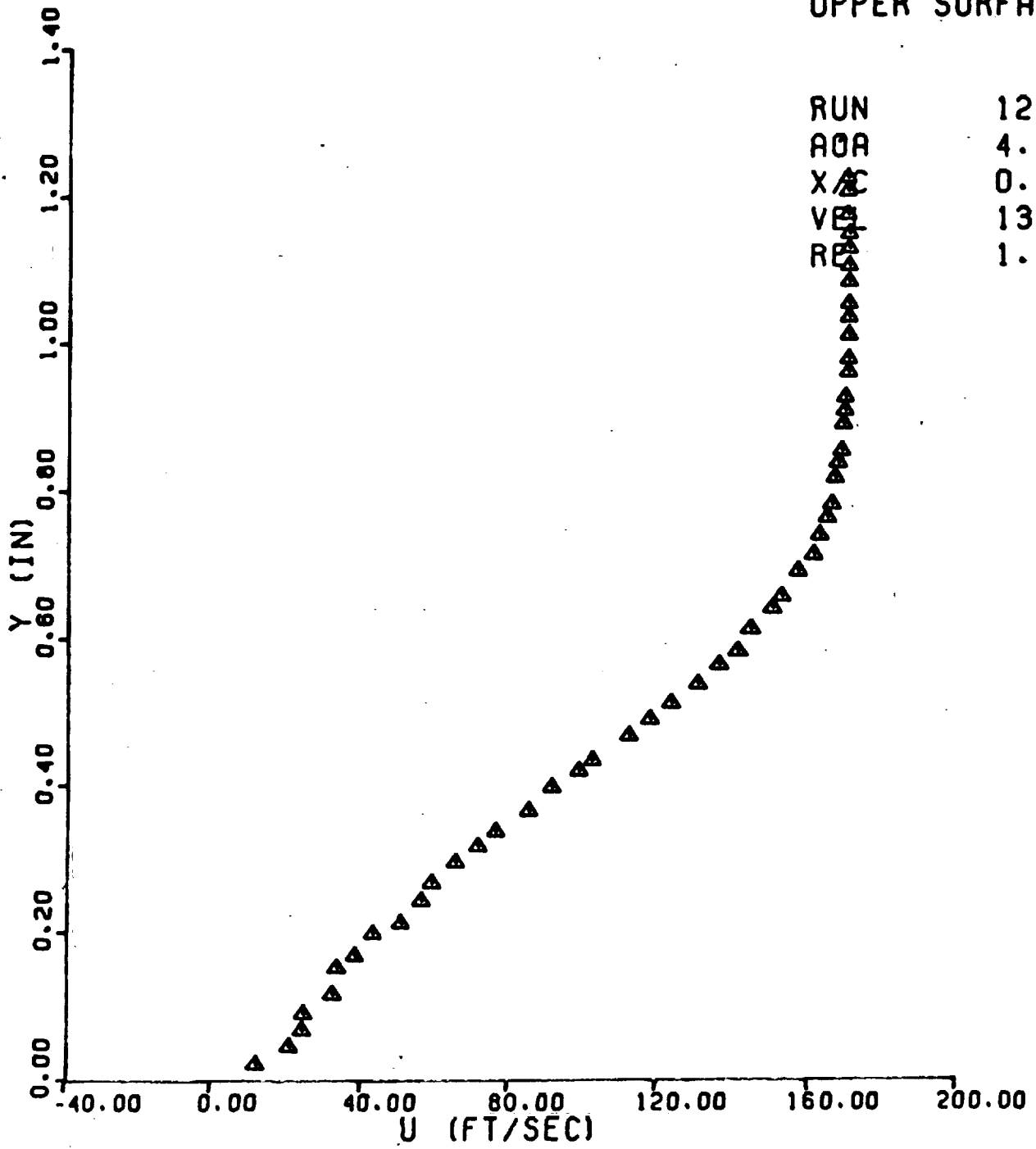


NACA 0012
UPPER SURFACE



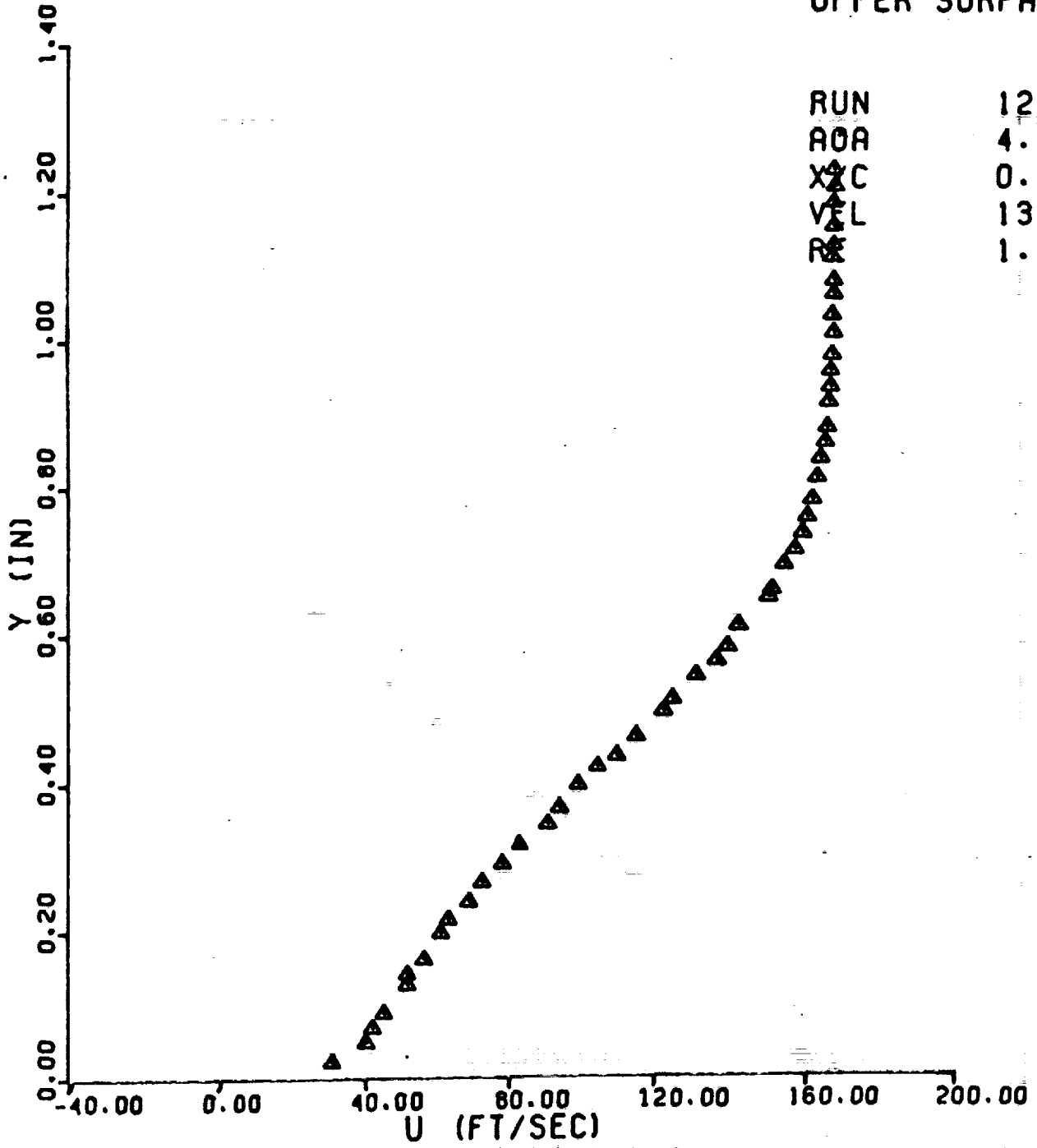
RUN	1282
AOA	4.000
X/	0.1400
VE	132.1
RE	1.56

NACA 0012
UPPER SURFACE



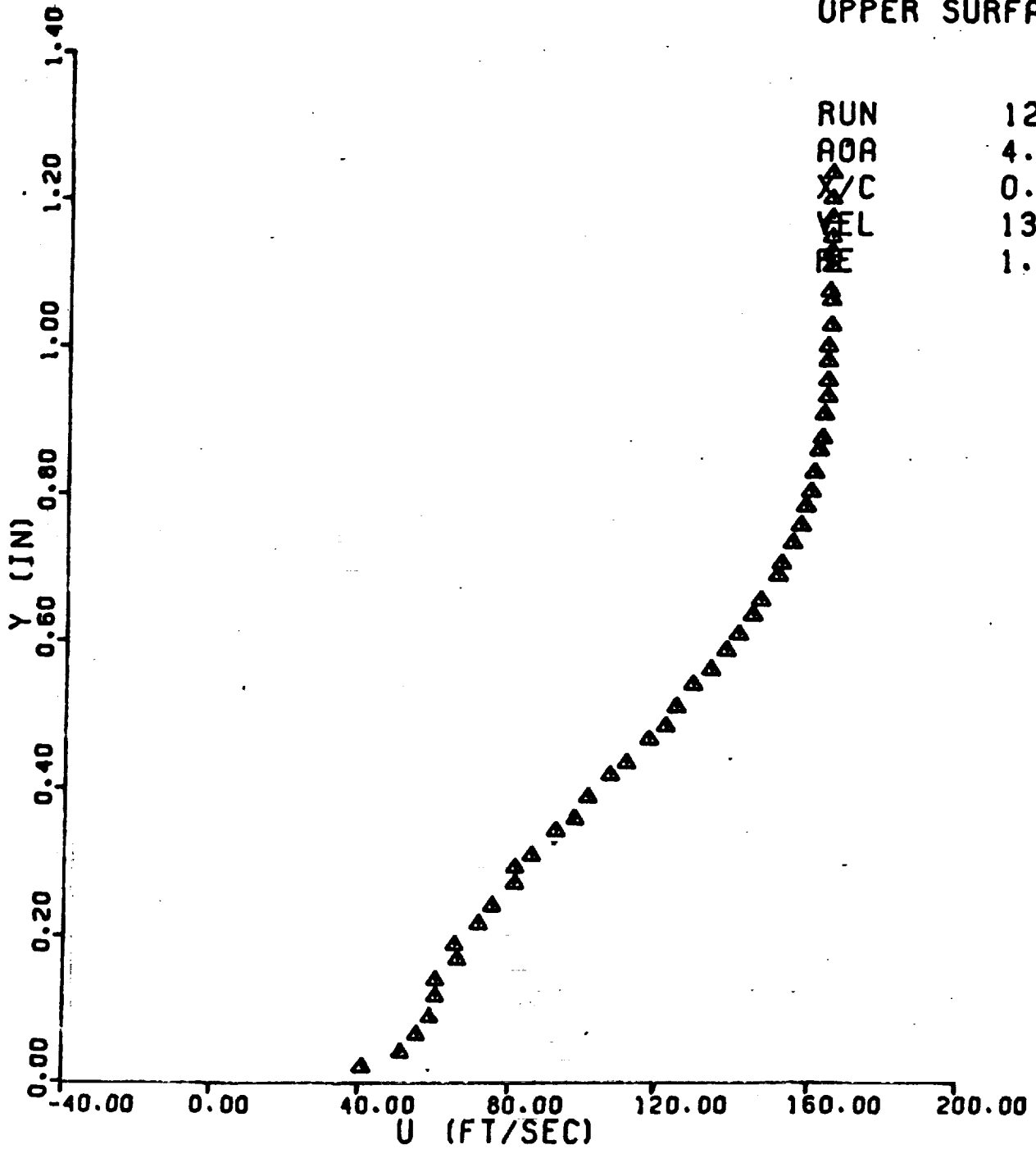
RUN	1283
AOA	4.000
X/C	0.1600
VE	131.7
RE	1.55

NACA 0012
UPPER SURFACE



RUN	1284
AOA	4.000
X/C	0.1800
VEL	132.0
RE	1.55

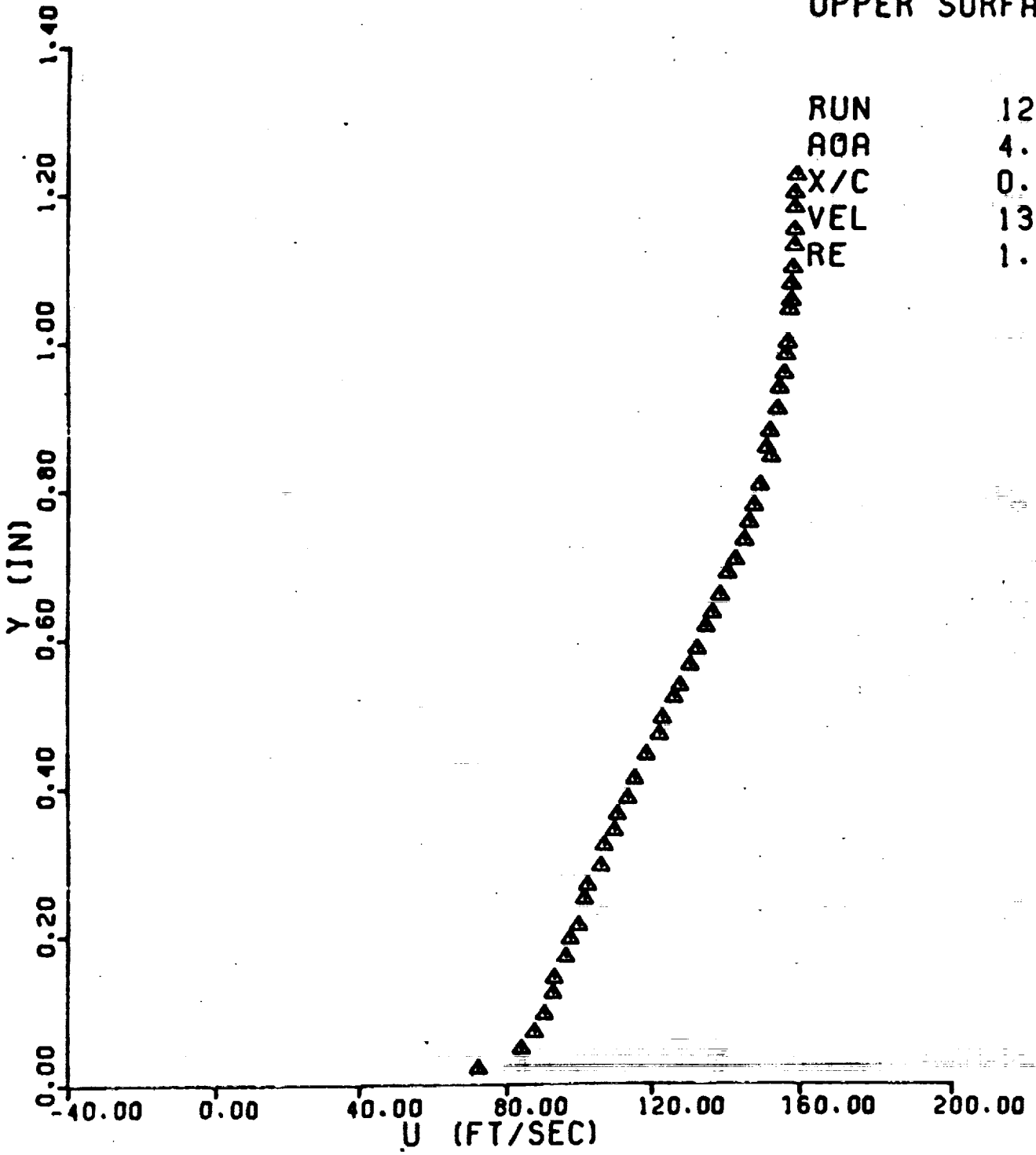
NACA 0012
UPPER SURFACE



RUN 1285
AOA 4.000
X/C 0.2000
VEL 131.6
RE 1.55

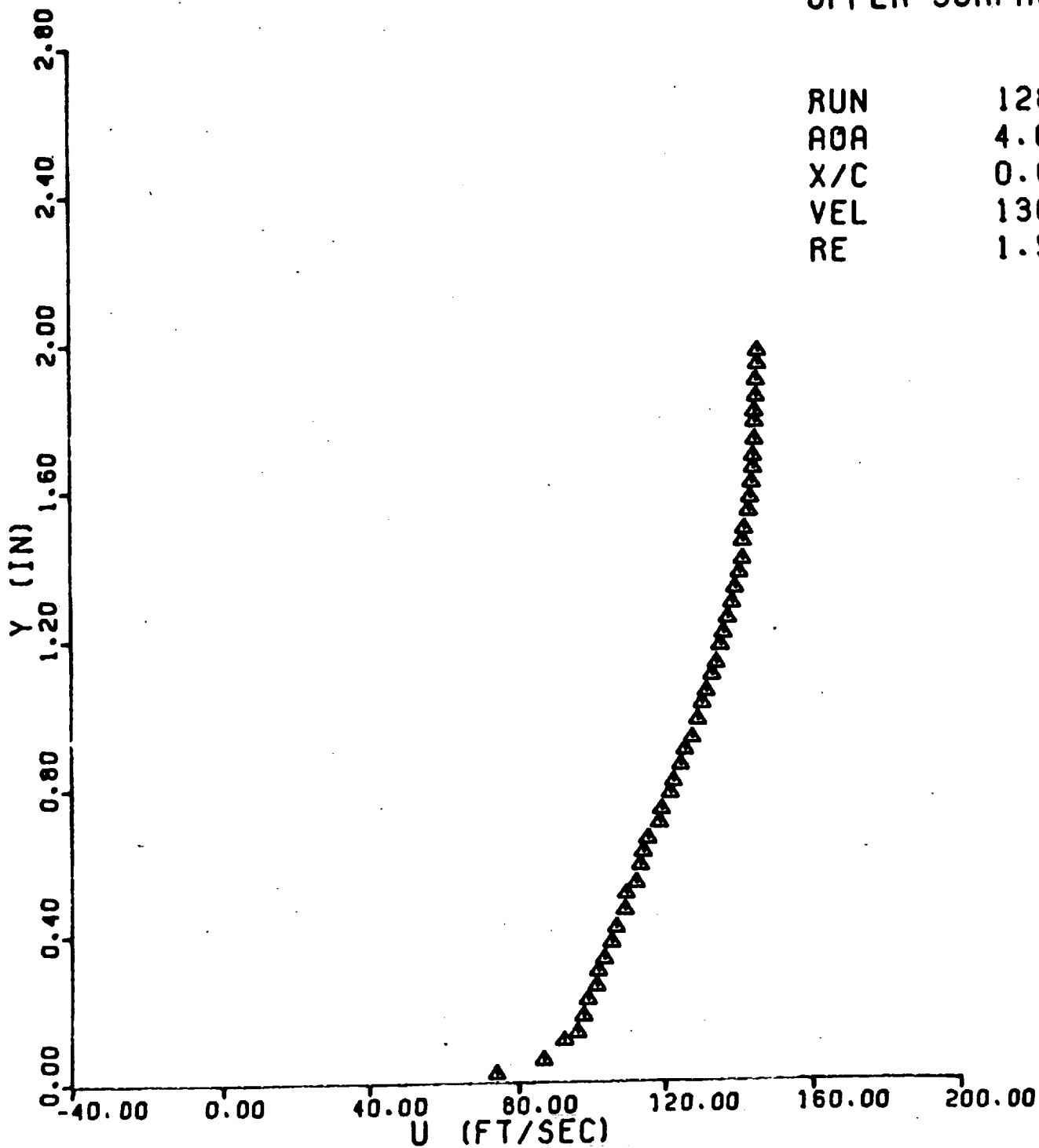
NACA 0012
UPPER SURFACE

RUN 1286
AOA 4.000
X/C 0.3000
VEL 131.8
RE 1.55



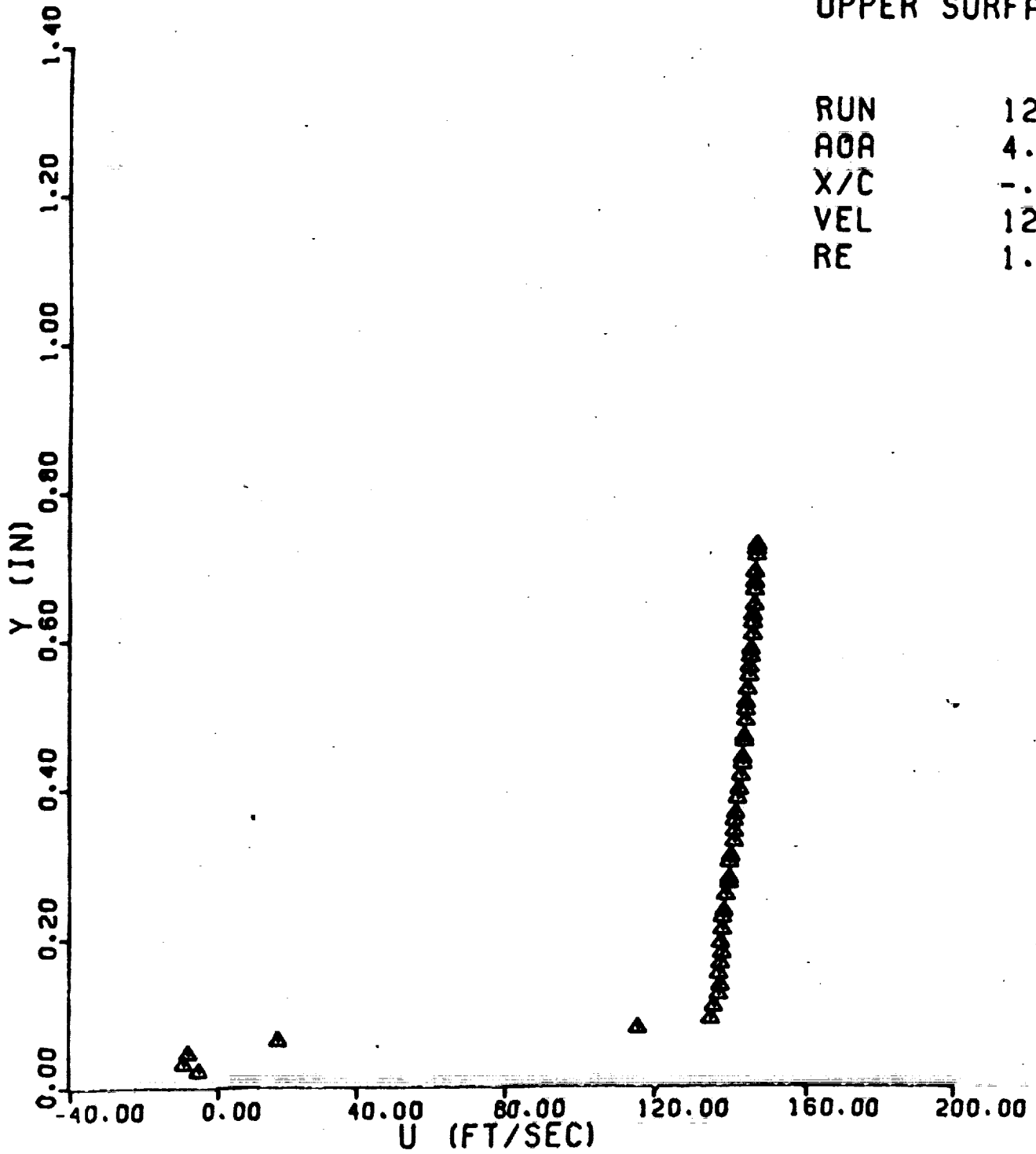
NACA 0012
UPPER SURFACE

RUN 1287
AOA 4.000
X/C 0.6000
VEL 130.4
RE 1.53



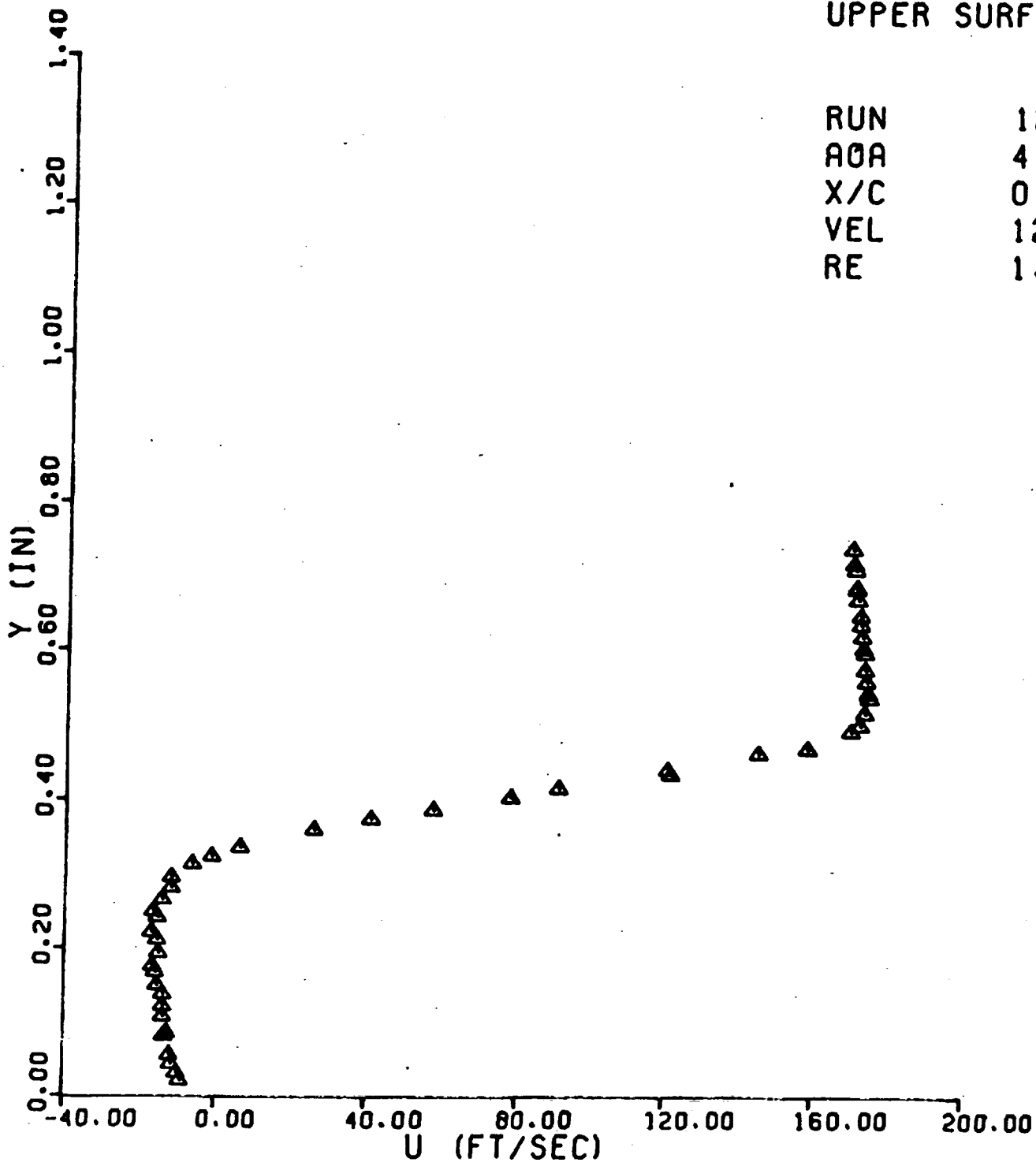
NACA 0012
UPPER SURFACE

RUN 1288
AOA 4.000
X/C -.0200
VEL 129.7
RE 1.51



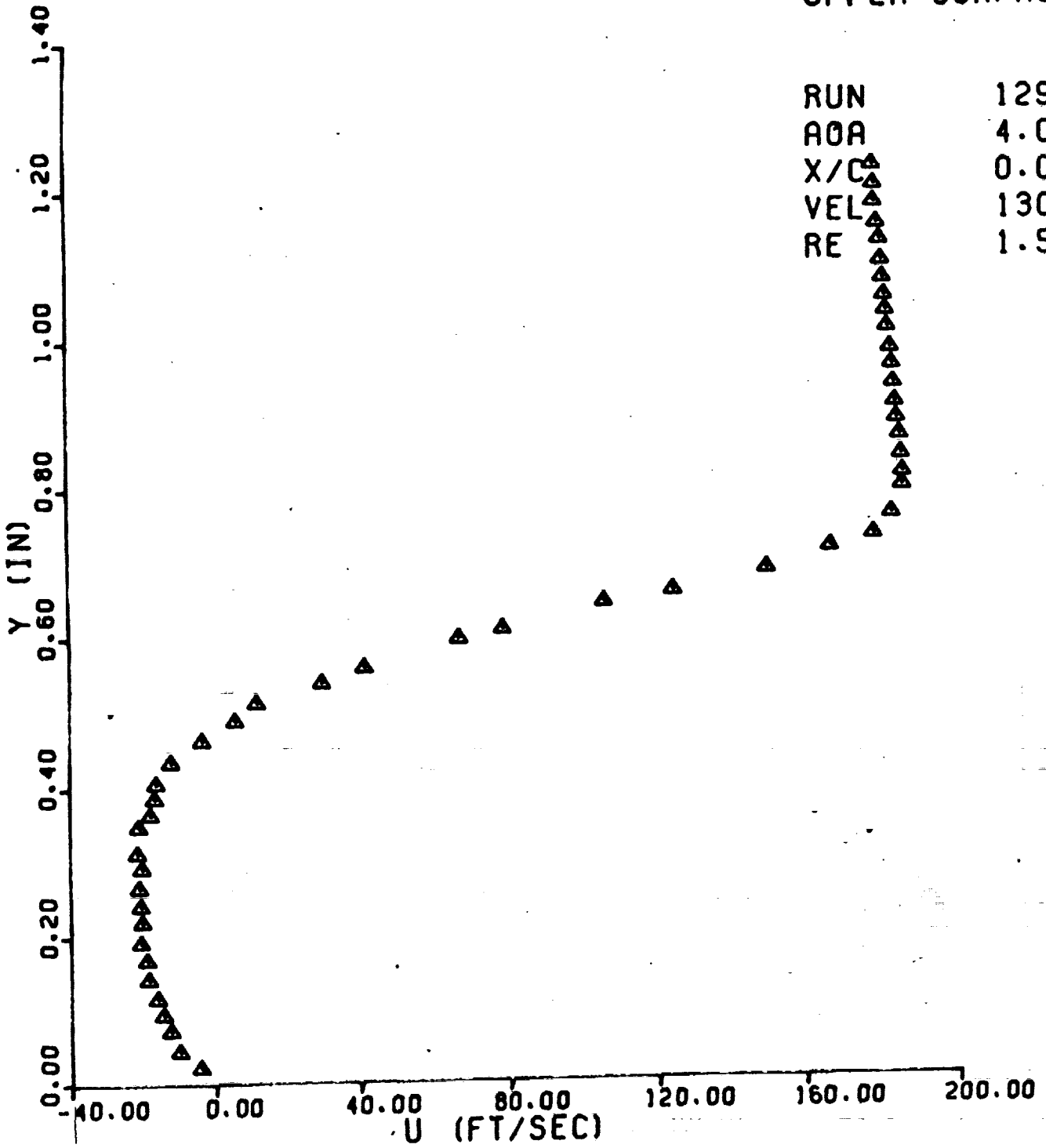
NACA 0012
UPPER SURFACE

RUN 1289
AOA 4.000
X/C 0.0000
VEL 129.8
RE 1.52

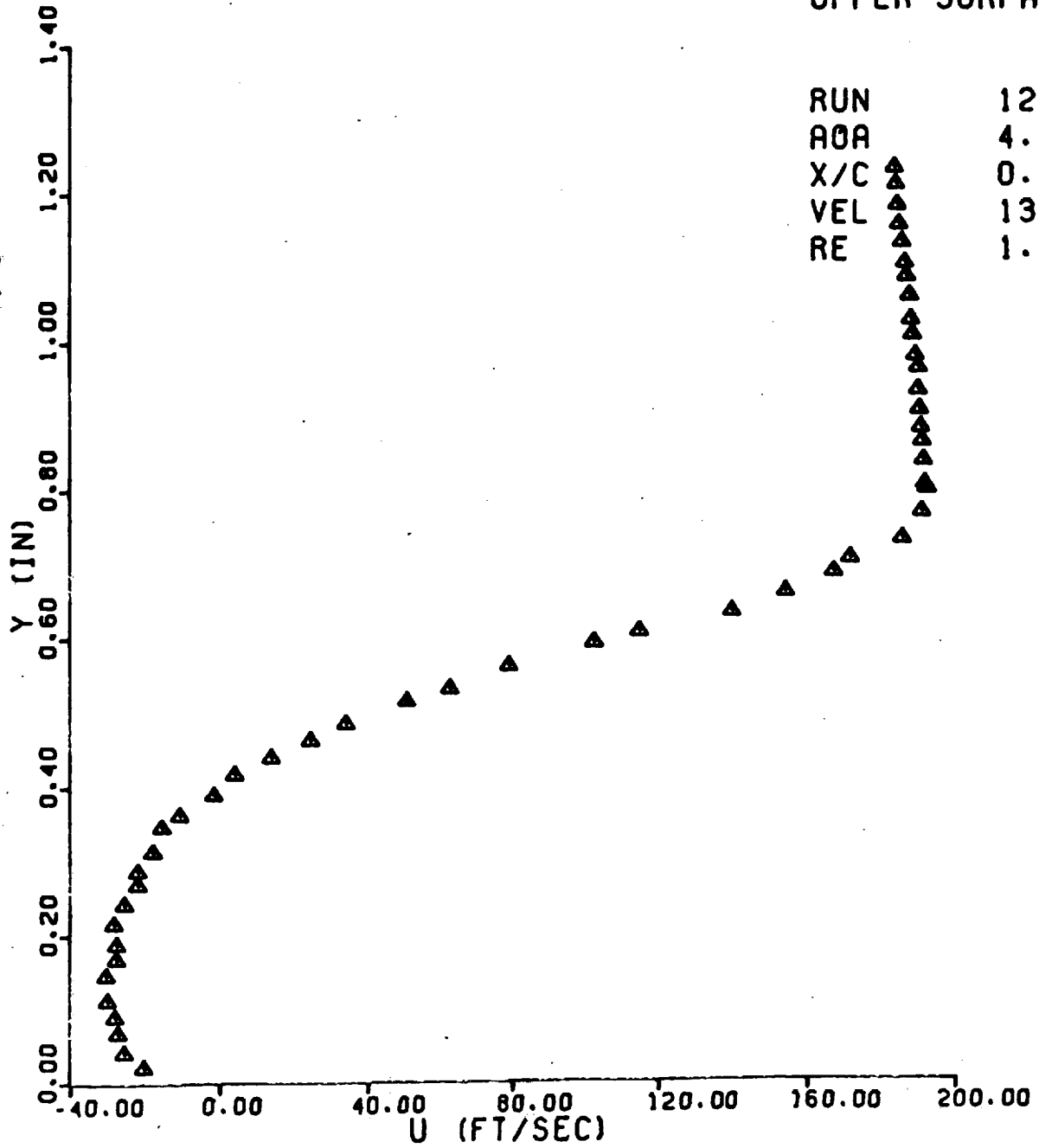


NACA 0012
UPPER SURFACE

RUN 1290
AOA 4.000
X/C 0.0200
VEL 130.4
RE 1.52

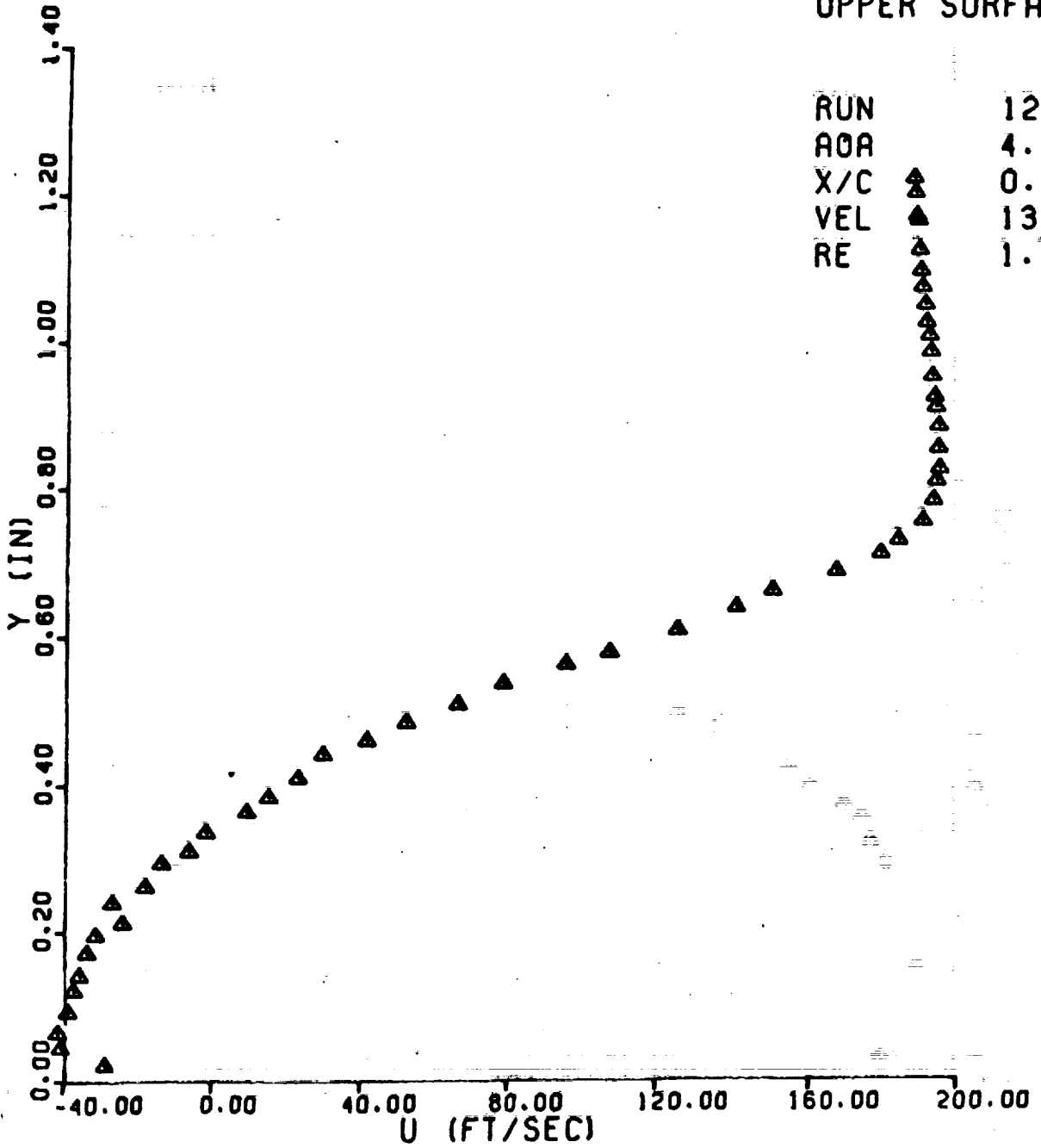


NACA 0012
UPPER SURFACE



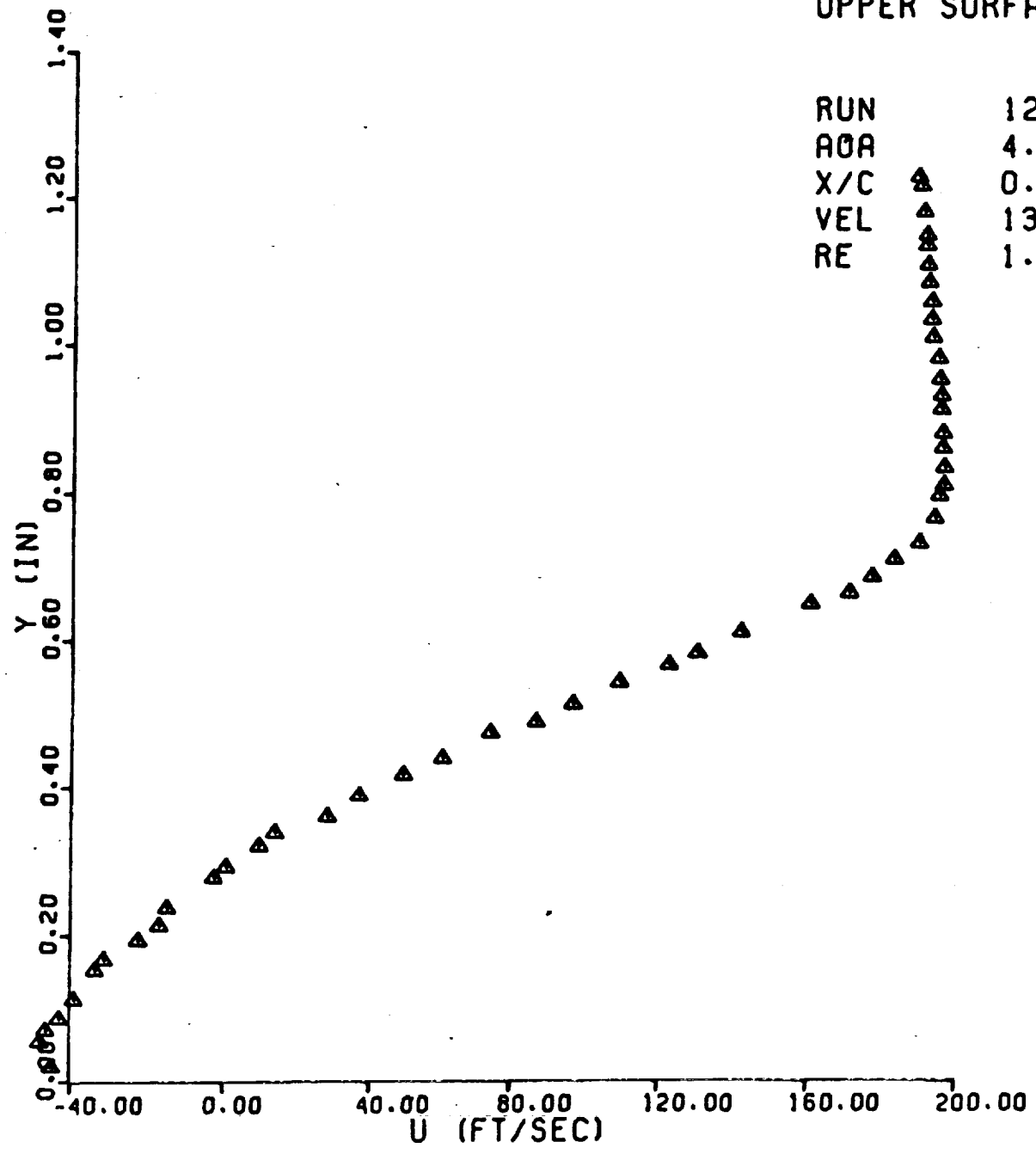
NACA 0012
UPPER SURFACE

RUN	1292
AOA	4.000
X/C	0.0600
VEL	130.0
RE	1.52



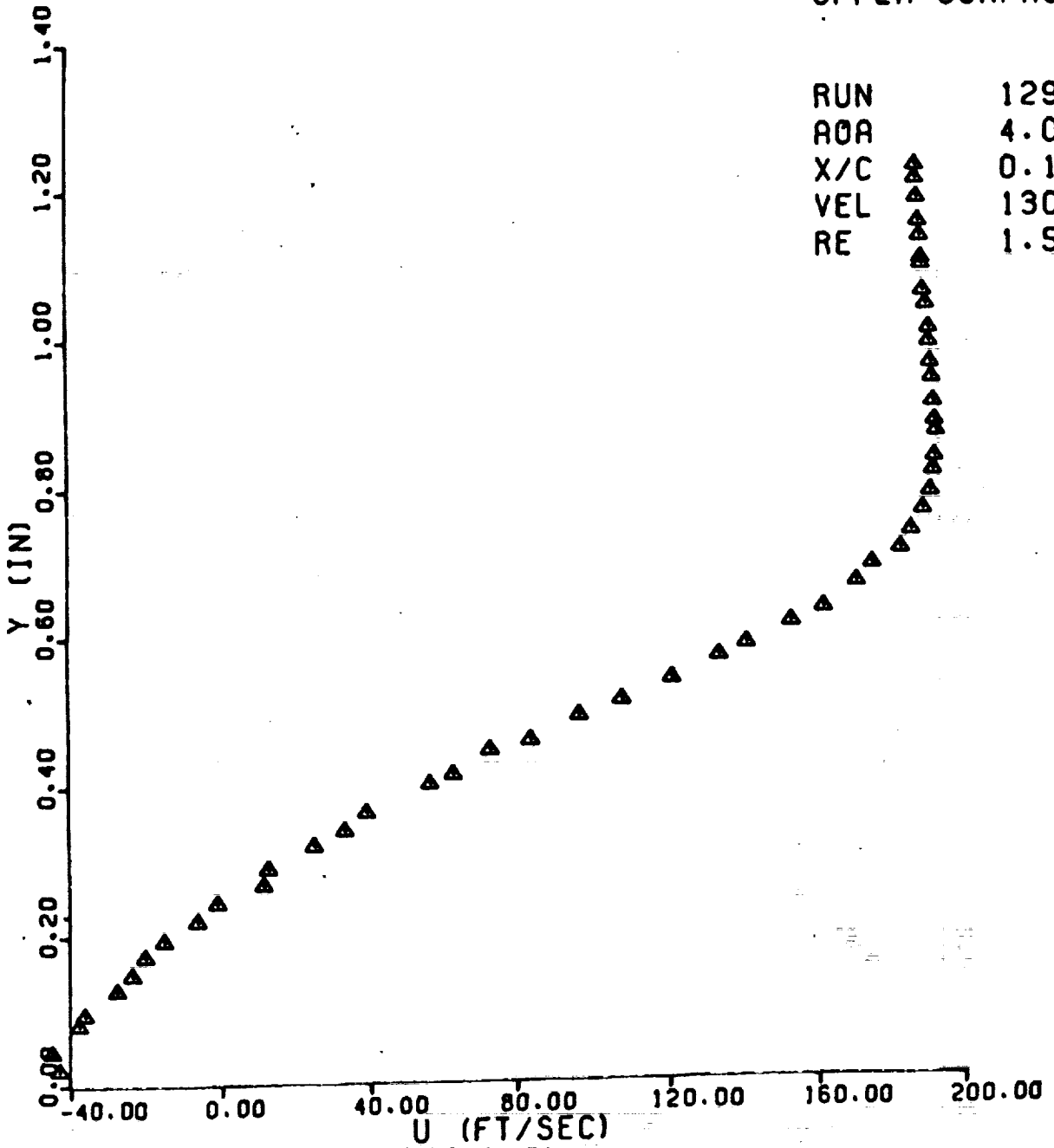
NACA 0012
UPPER SURFACE

RUN 1293
AOA 4.000
X/C Δ 0.0800
VEL 130.2
RE 1.52

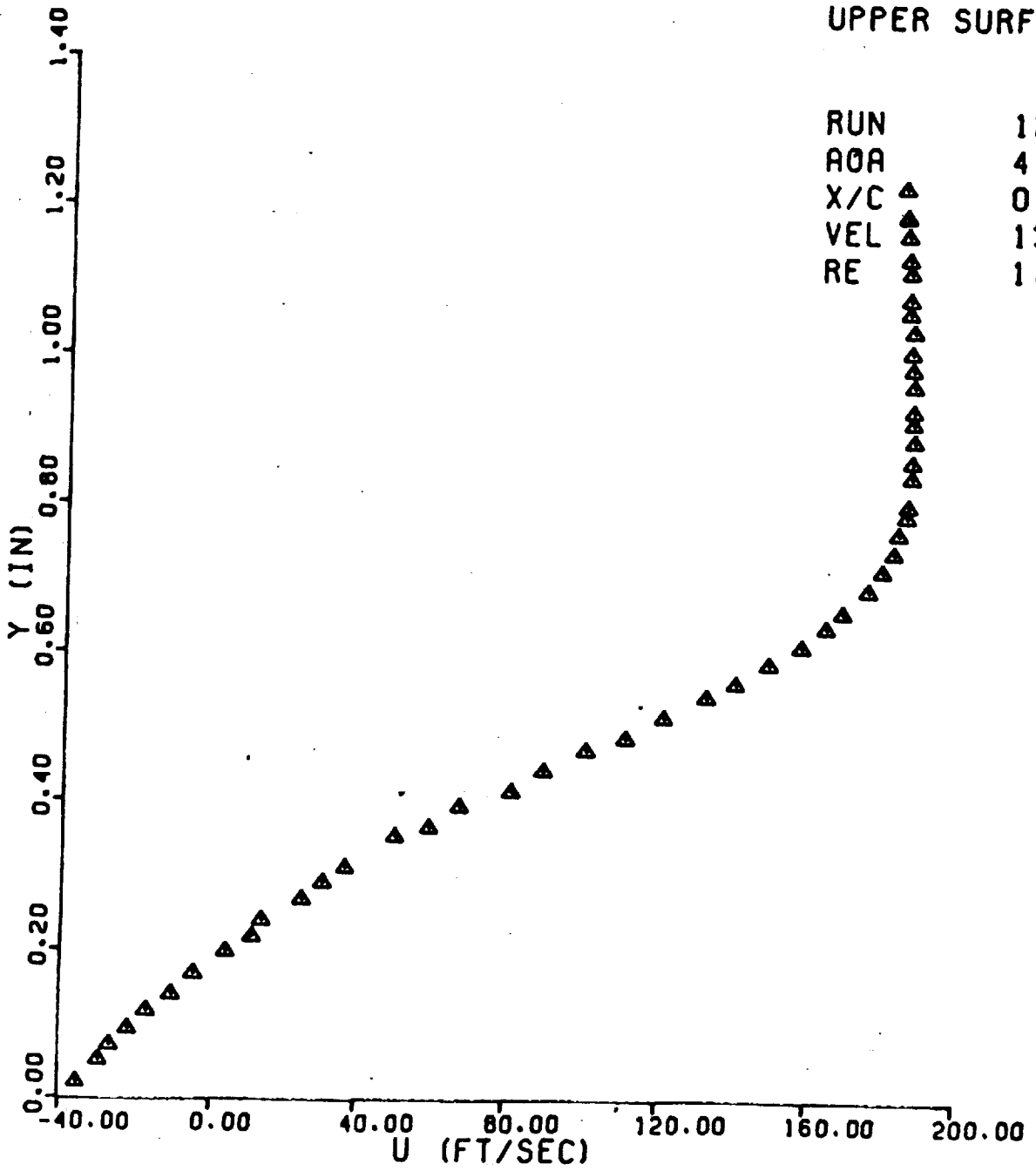


NACA 0012
UPPER SURFACE

RUN	1294
AOA	4.000
X/C	0.1000
VEL	130.3
RE	1.52

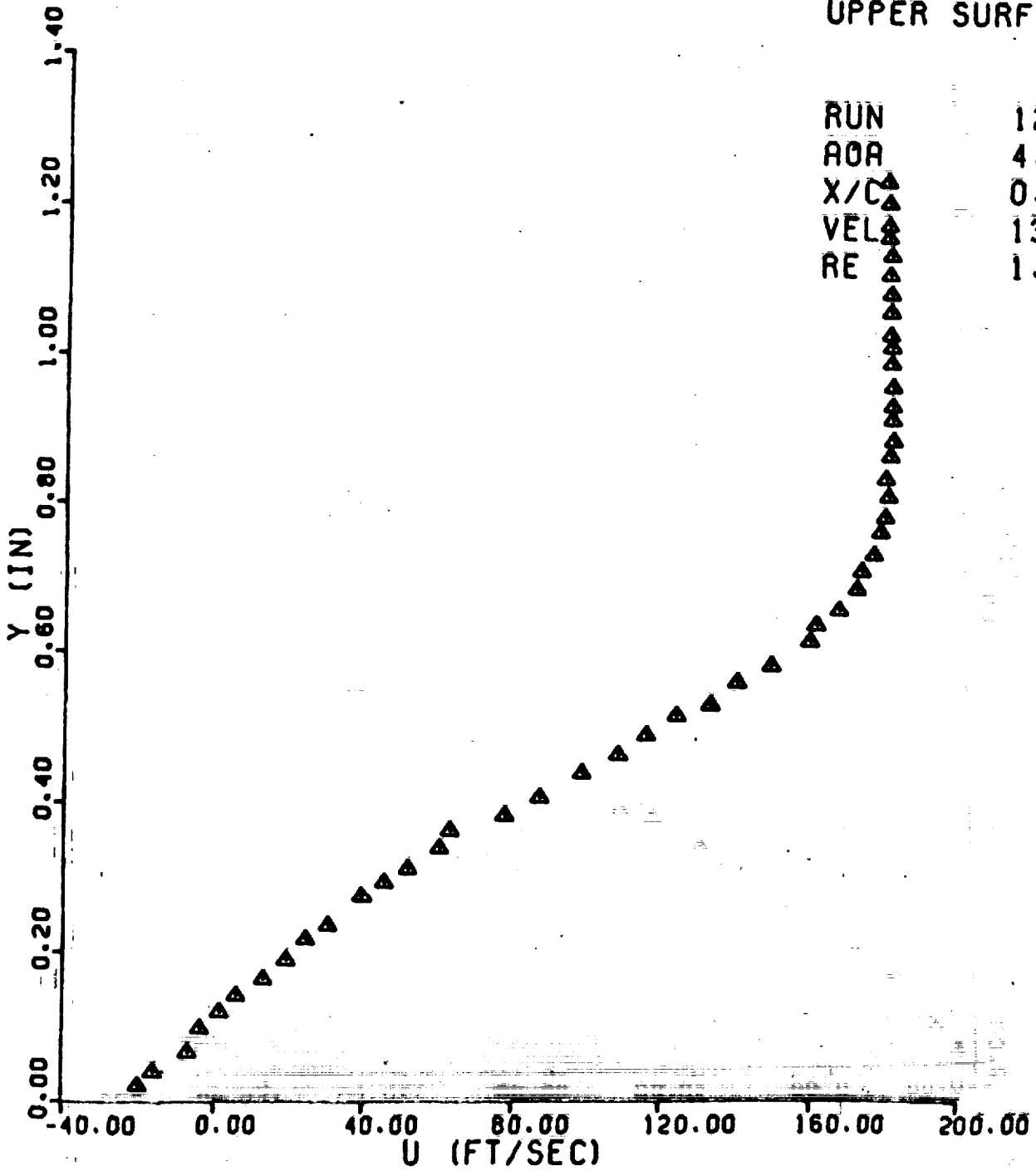


NACA 0012
UPPER SURFACE



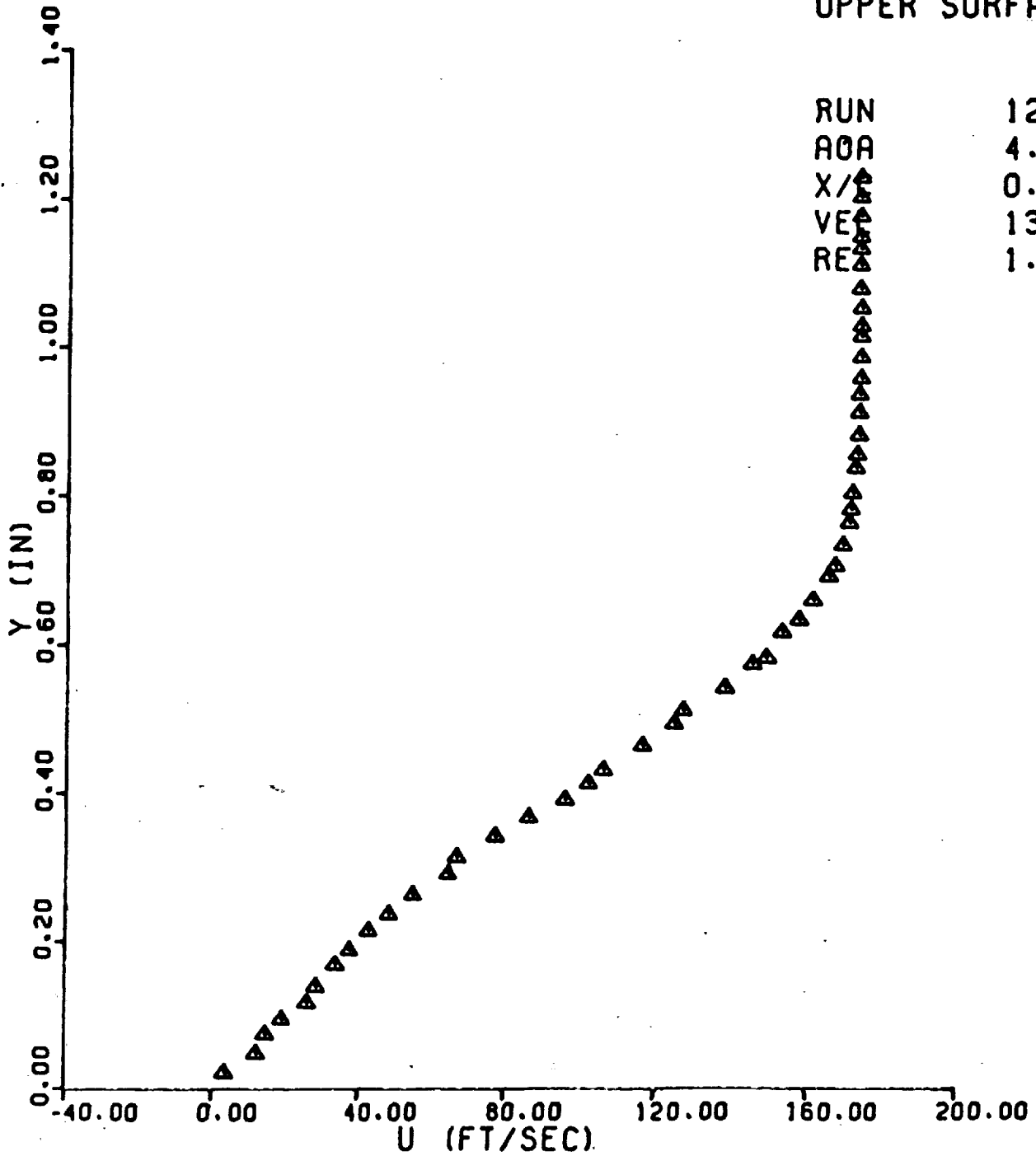
RUN	1295
AOA	4.000
X/C	0.1200
VEL	131.1
RE	1.53

NACA 0012
UPPER SURFACE



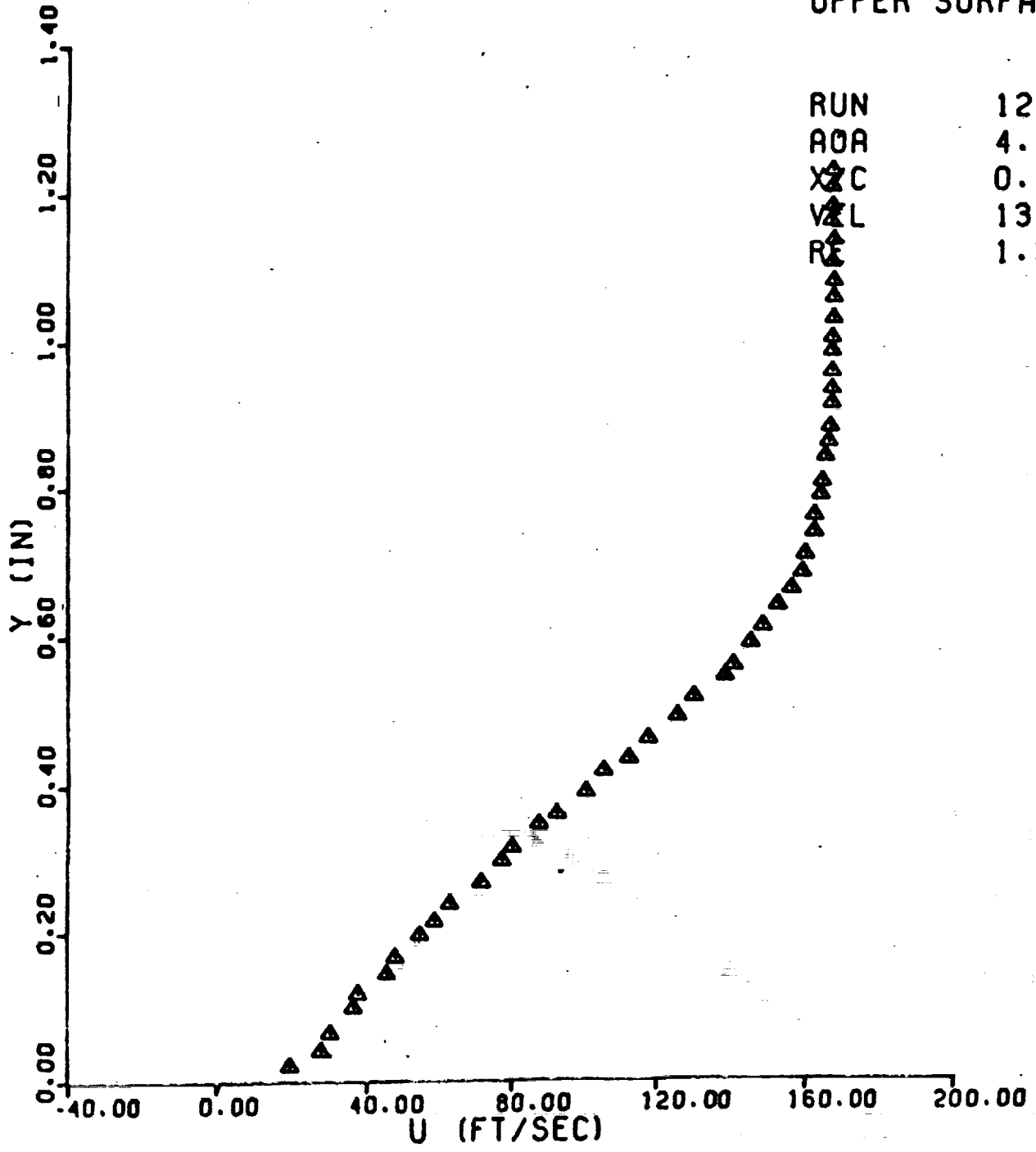
RUN 1296
AOA 4.000
X/C 0.1400
VEL 130.8
RE 1.53

NACA 0012
UPPER SURFACE



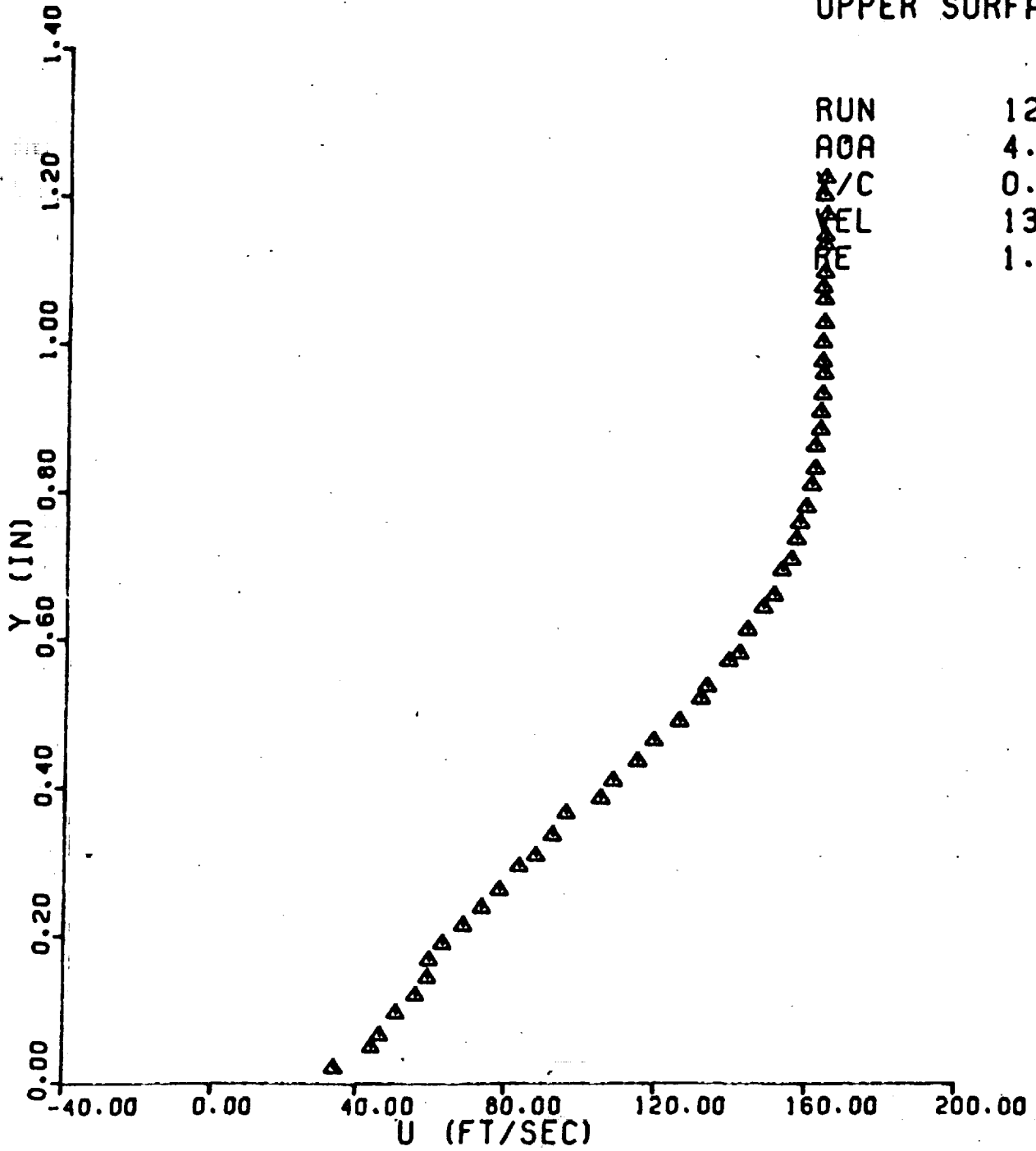
RUN 1297
AOA 4.000
X/△ 0.1600
VE△ 131.2
RE△ 1.54

NACA 0012
UPPER SURFACE



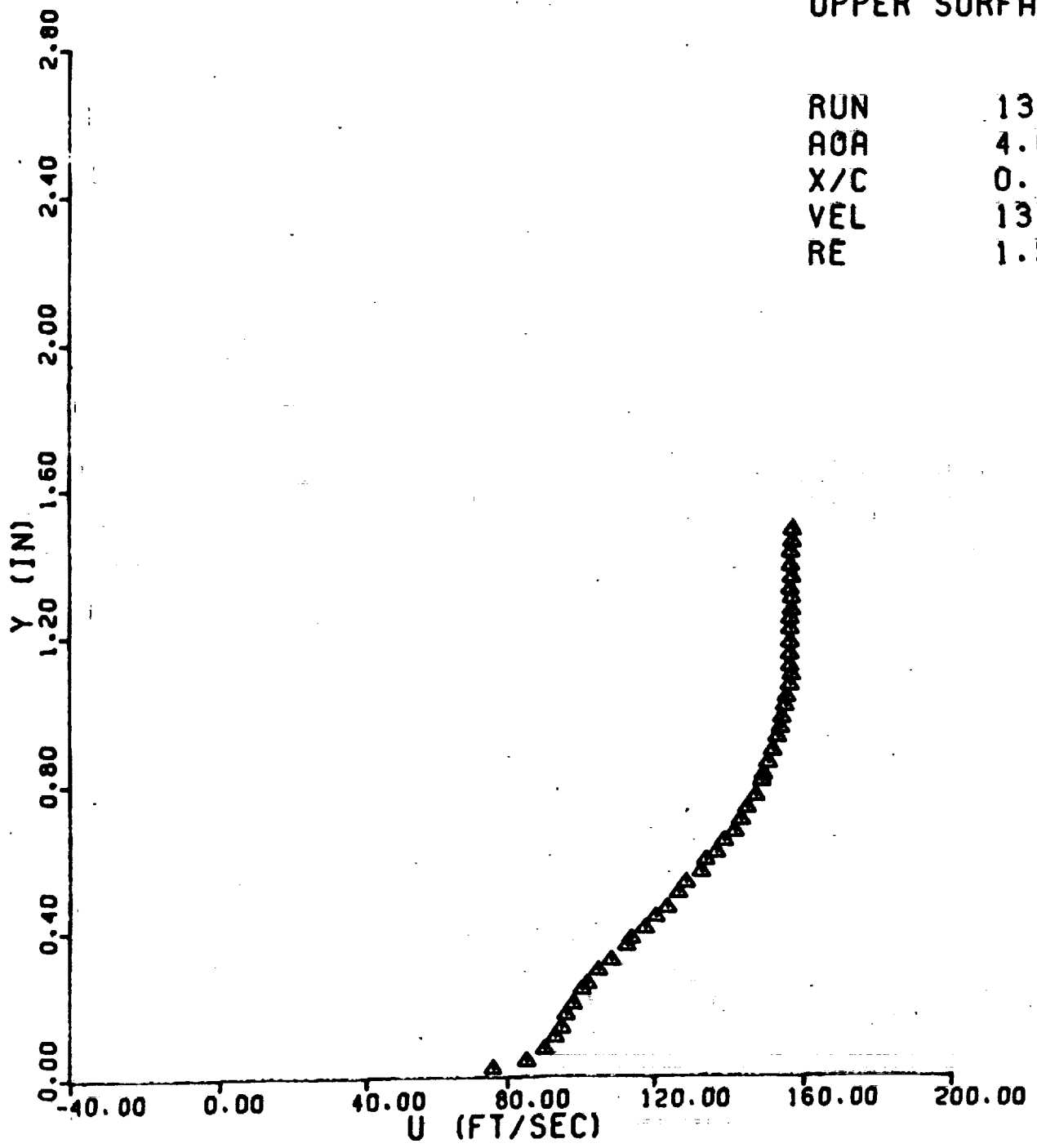
RUN 1298
AOA 4.000
XZC 0.1800
VZL 131.2
RC 1.54

NACA 0012
UPPER SURFACE



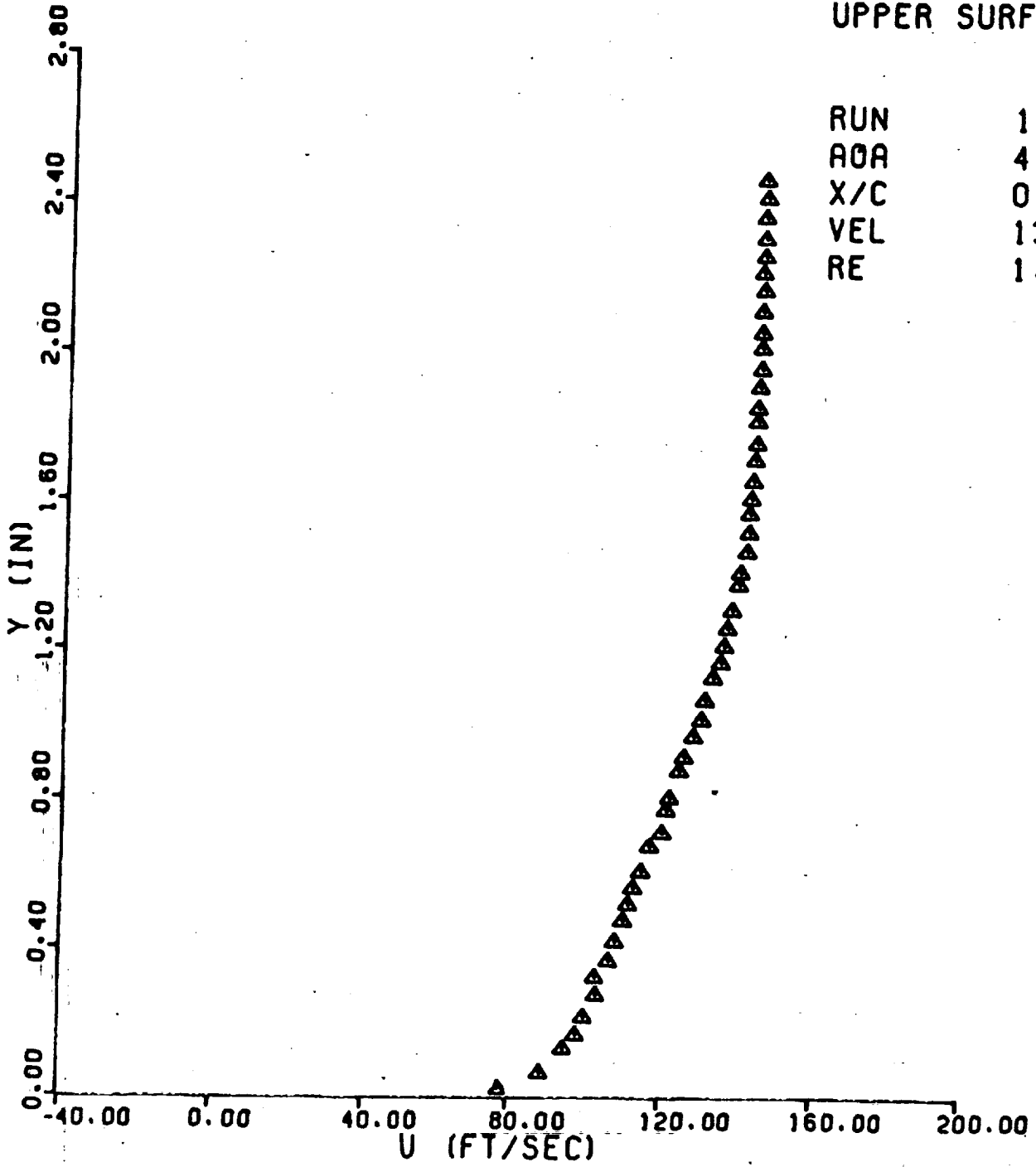
NACA 0012
UPPER SURFACE

RUN	1300
AOA	4.000
X/C	0.3000
VEL	131.5
RE	1.55



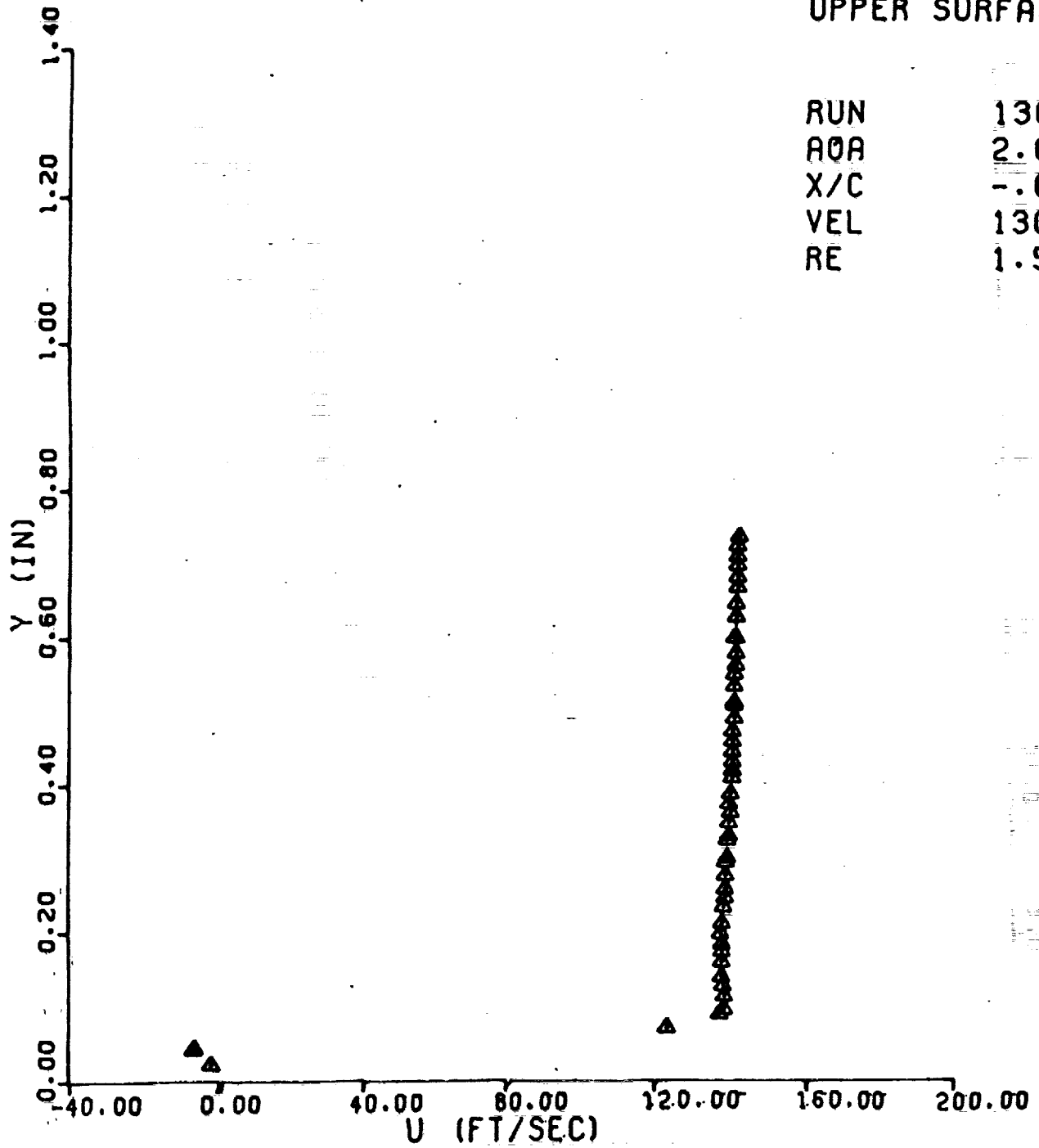
NACA 0012
UPPER SURFACE

RUN 1301
AOA 4.000
X/C 0.6000
VEL 130.3
RE 1.53



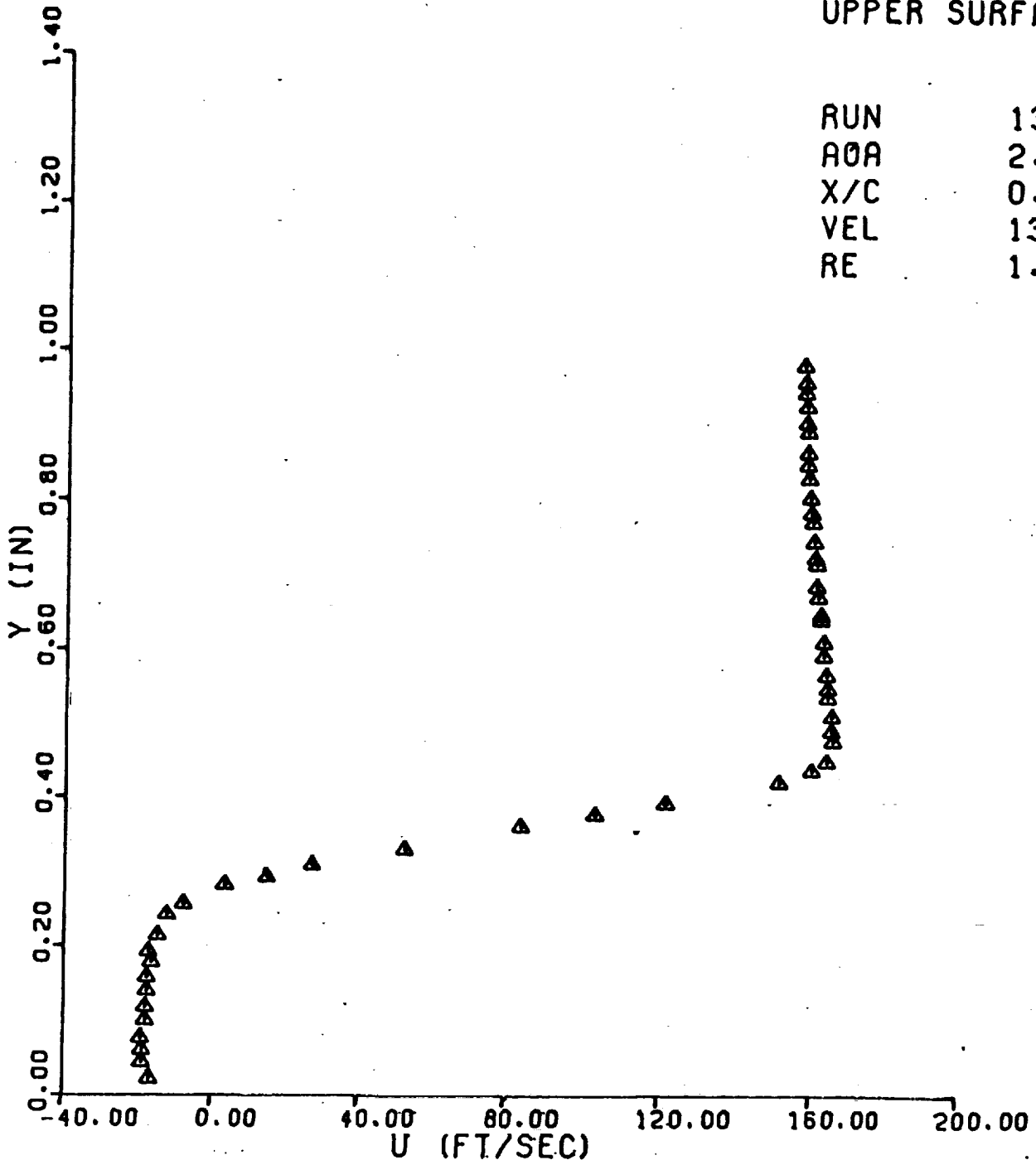
NACA 0012
UPPER SURFACE

RUN	1302
AOA	2.000
X/C	-.0200
VEL	130.5
RE	1.54



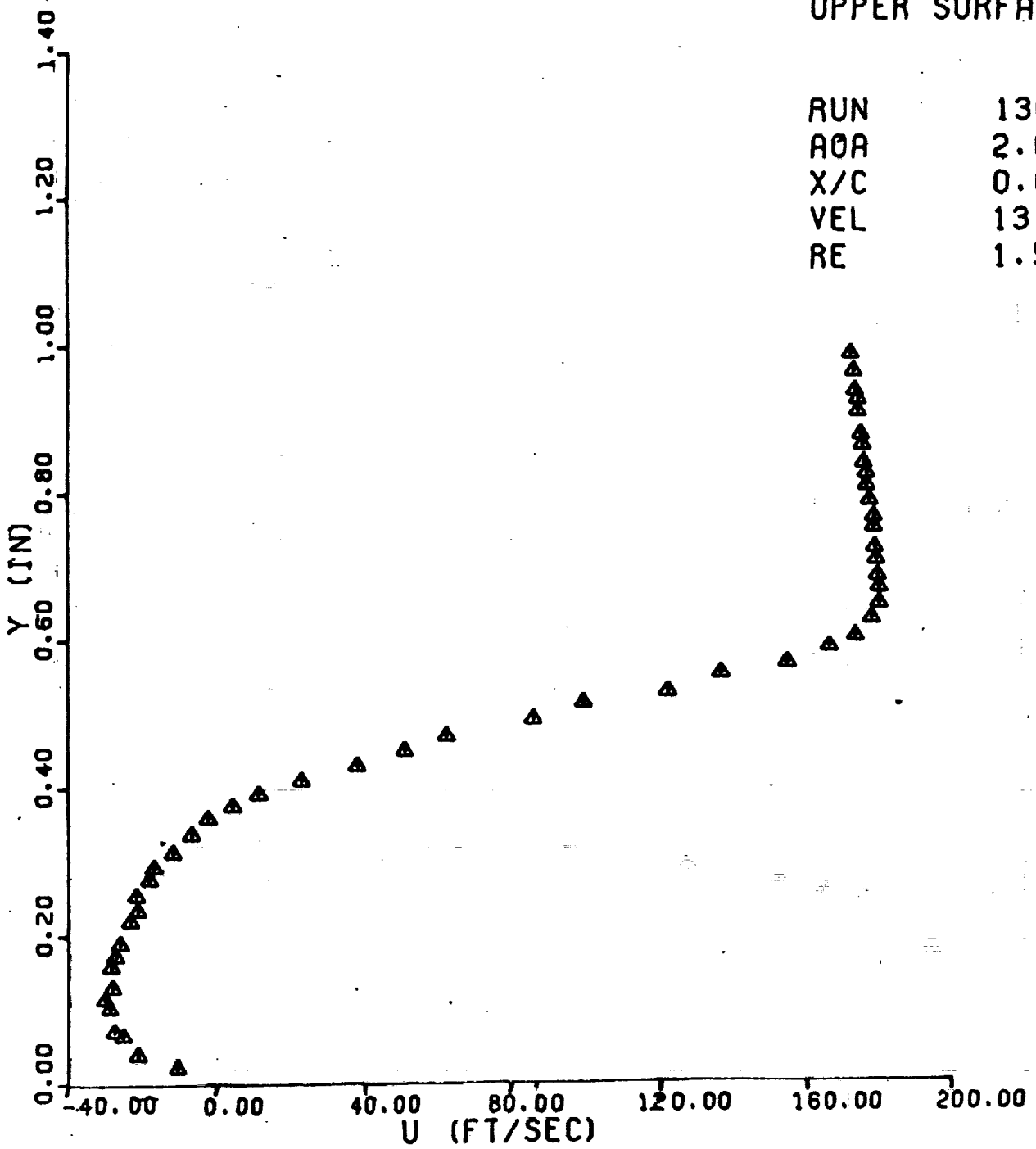
NACA 0012
UPPER SURFACE

RUN 1303
AOA 2.000
X/C 0.0000
VEL 131.2
RE 1.54



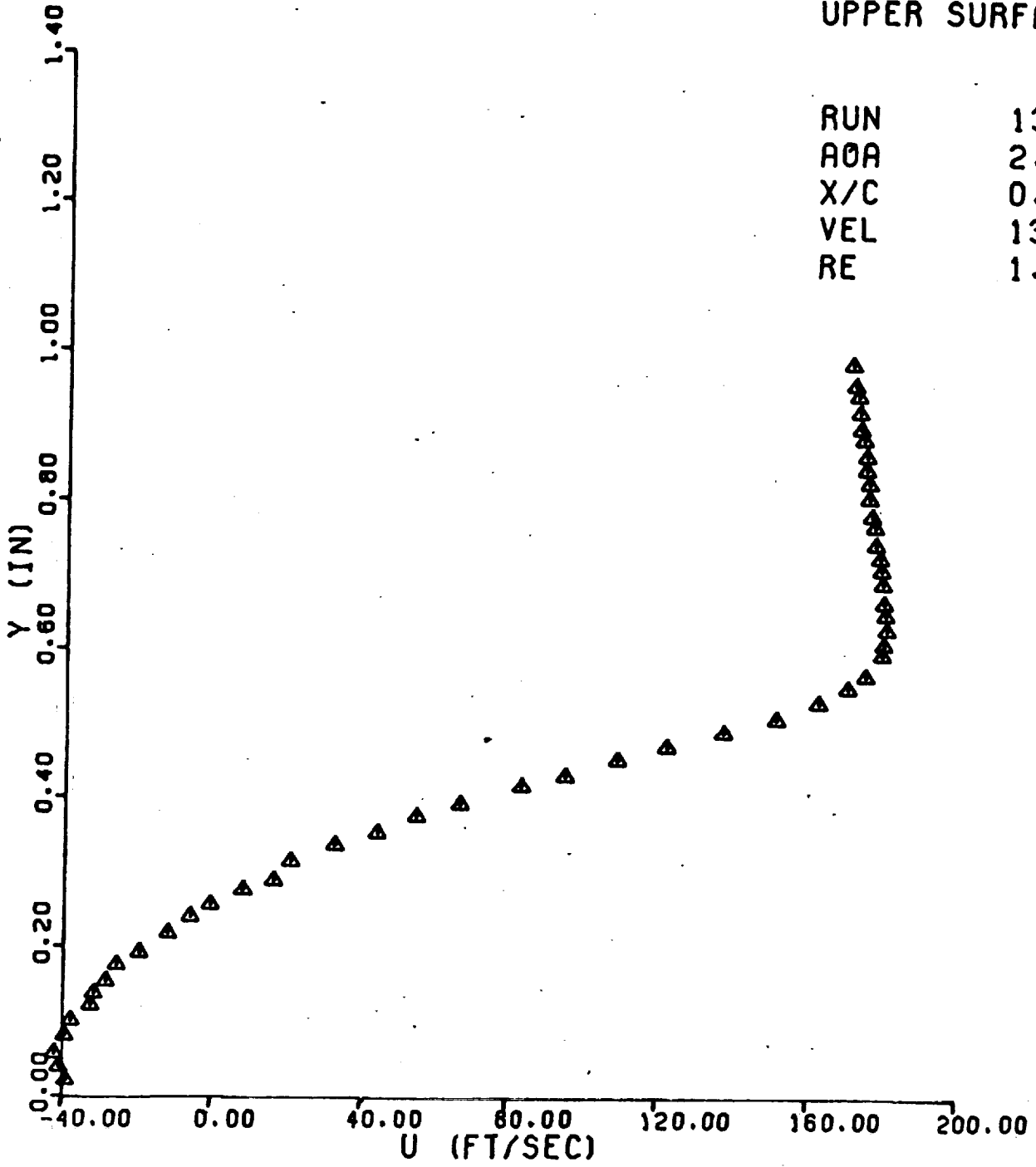
NACA 0012
UPPER SURFACE

RUN	1304
AOA	2.000
X/C	0.0200
VEL	131.2
RE	1.54



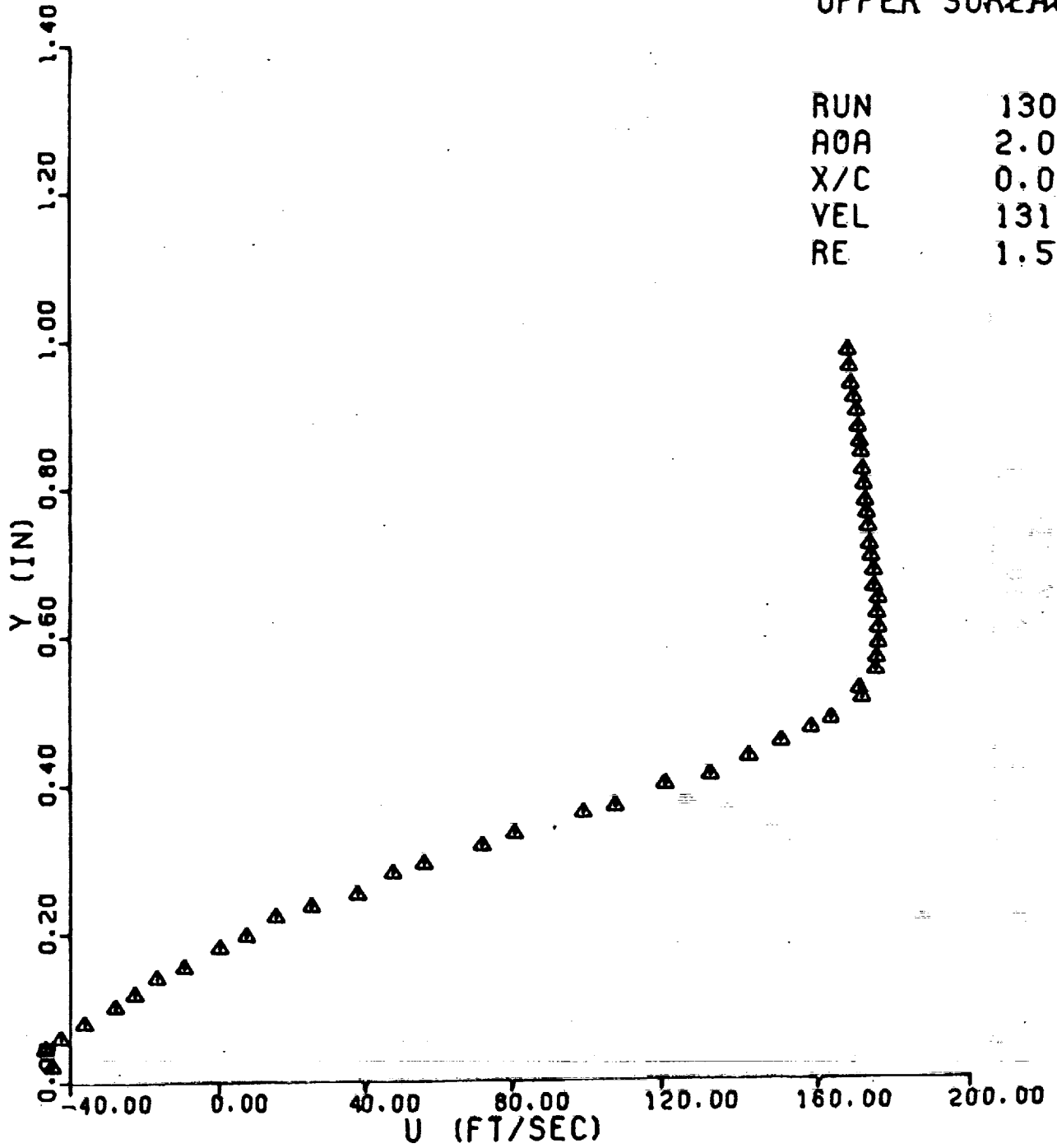
NACA 0012
UPPER SURFACE

RUN	1305
AOA	2.000
X/C	0.0400
VEL	130.8
RE	1.53



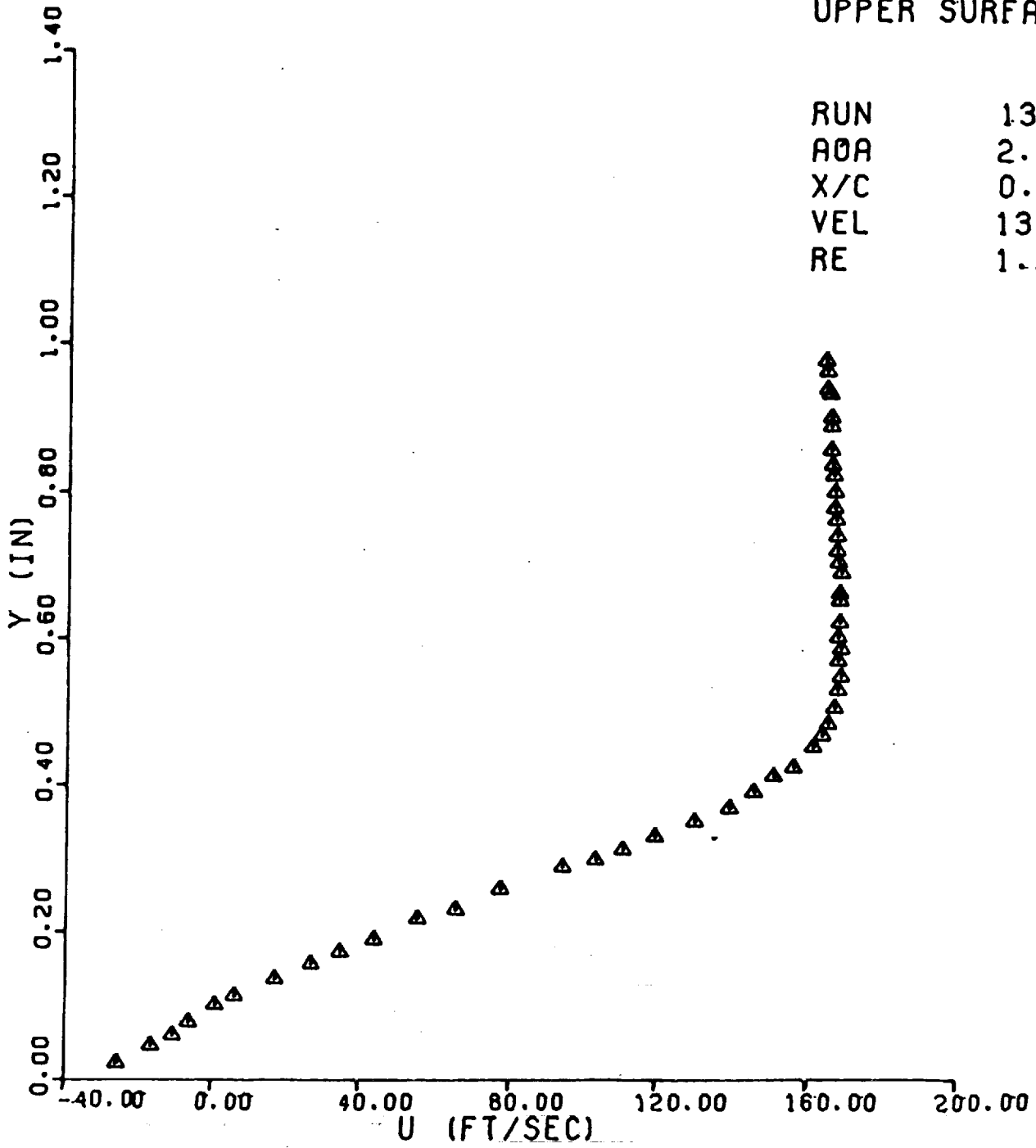
NACA 0012
UPPER SURFACE

RUN 1306
AOA 2.000
X/C 0.0600
VEL 131.3
RE 1.54

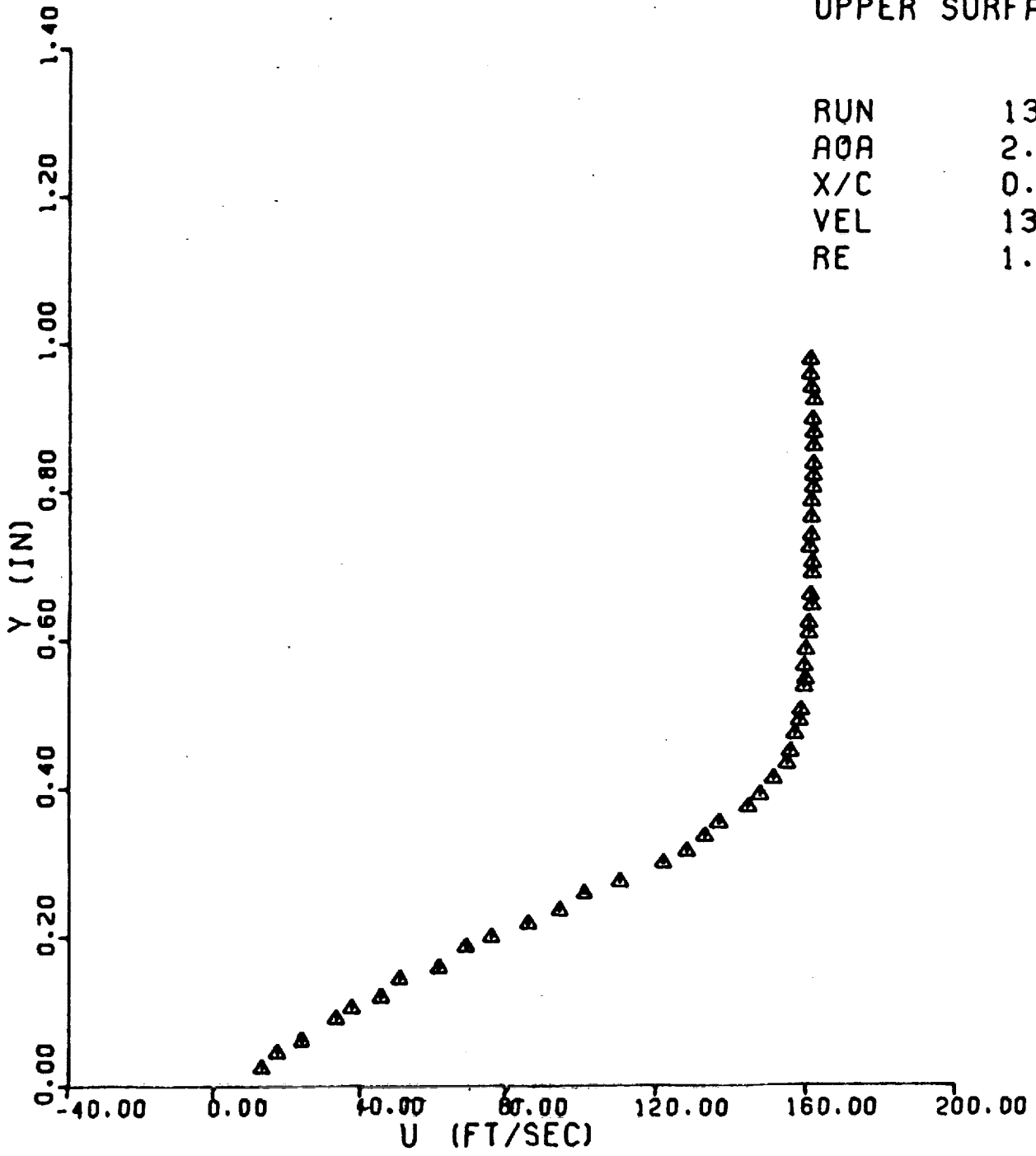


NACA 0012
UPPER SURFACE

RUN	1307
AOA	2.000
X/C	0.0800
VEL	131.4
RE	1.54



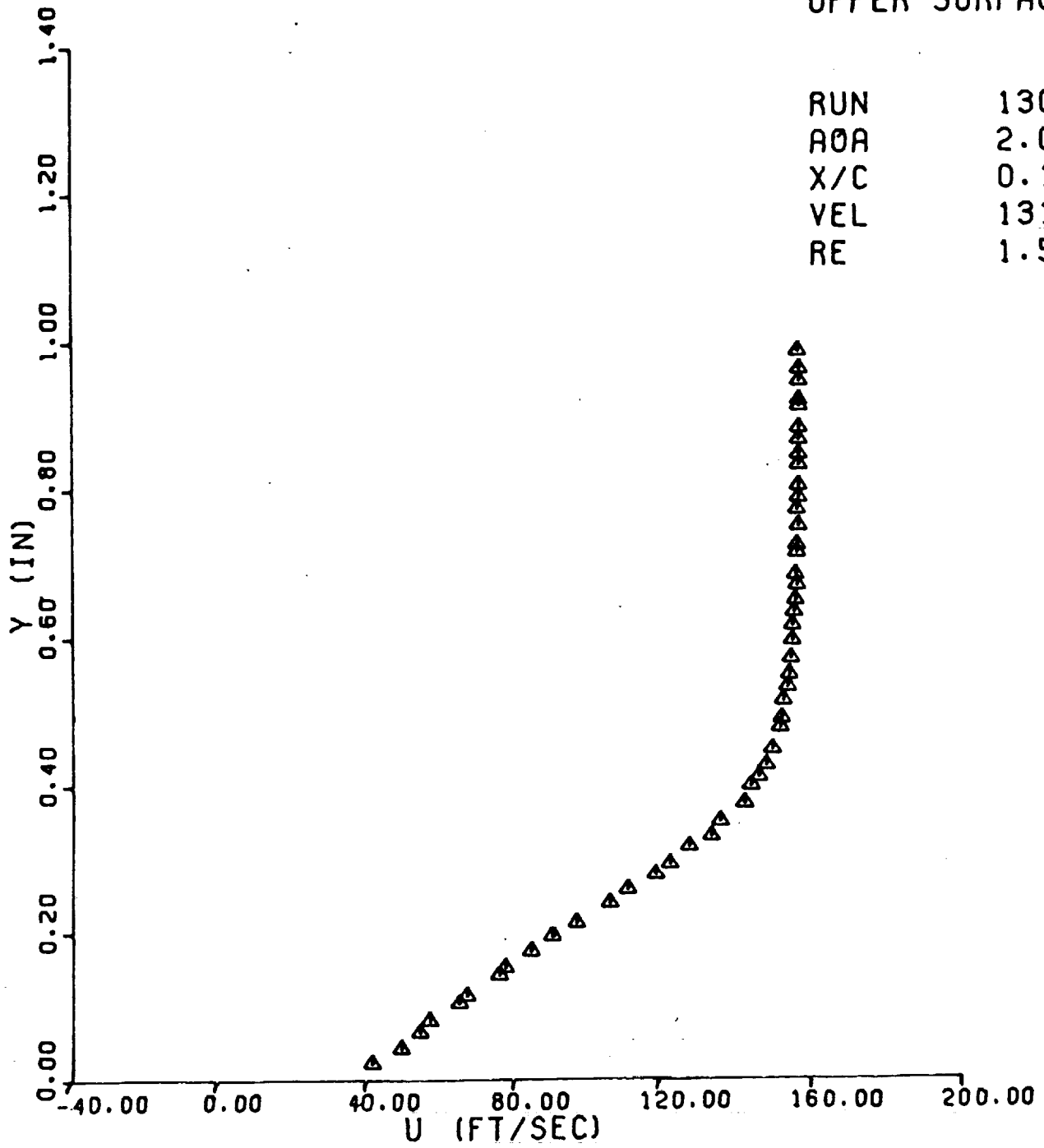
NACA 0012
UPPER SURFACE



RUN	1308
AOA	2.000
X/C	0.1000
VEL	131.1
RE	1.54

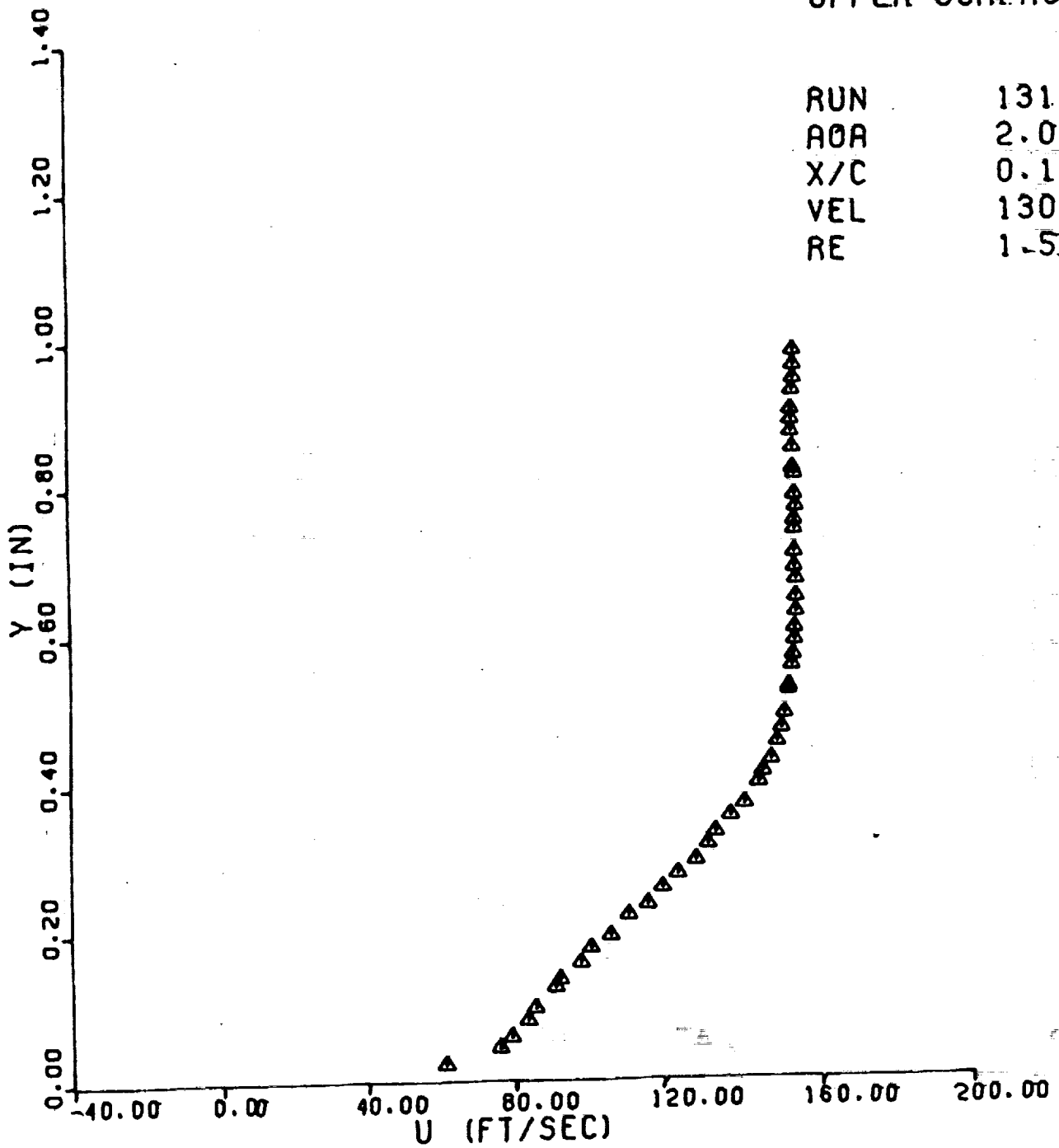
NACA 0012
UPPER SURFACE

RUN	1309
AOA	2.000
X/C	0.1200
VEL	131.2
RE	1.54



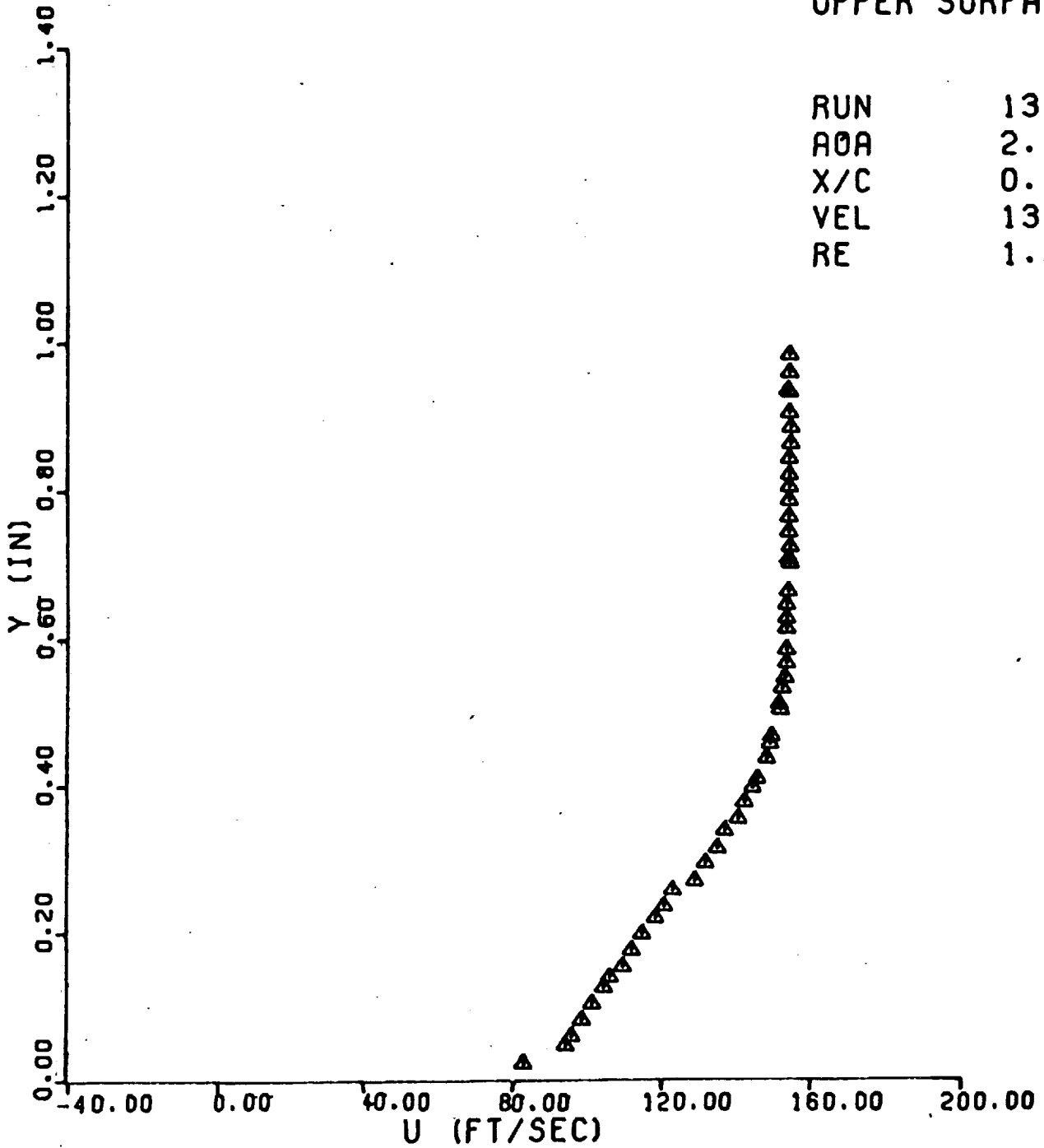
NACA 0012
UPPER SURFACE

RUN	1310
AOA	2.000
X/C	0.1400
VEL	130.8
RE	1.53



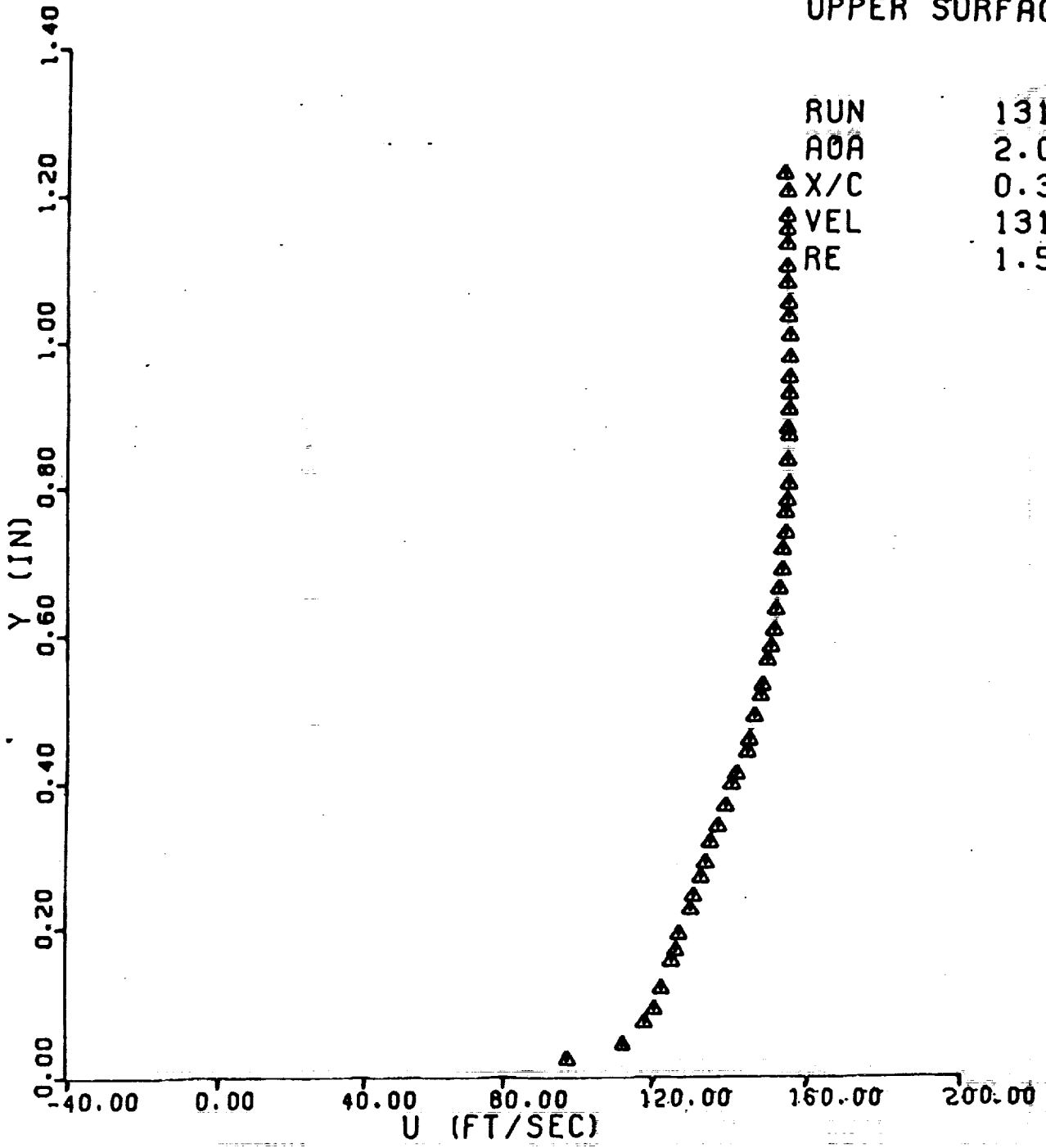
NACA 0012
UPPER SURFACE

RUN	1311
AOA	2.000
X/C	0.1600
VEL	130.9
RE	1.54



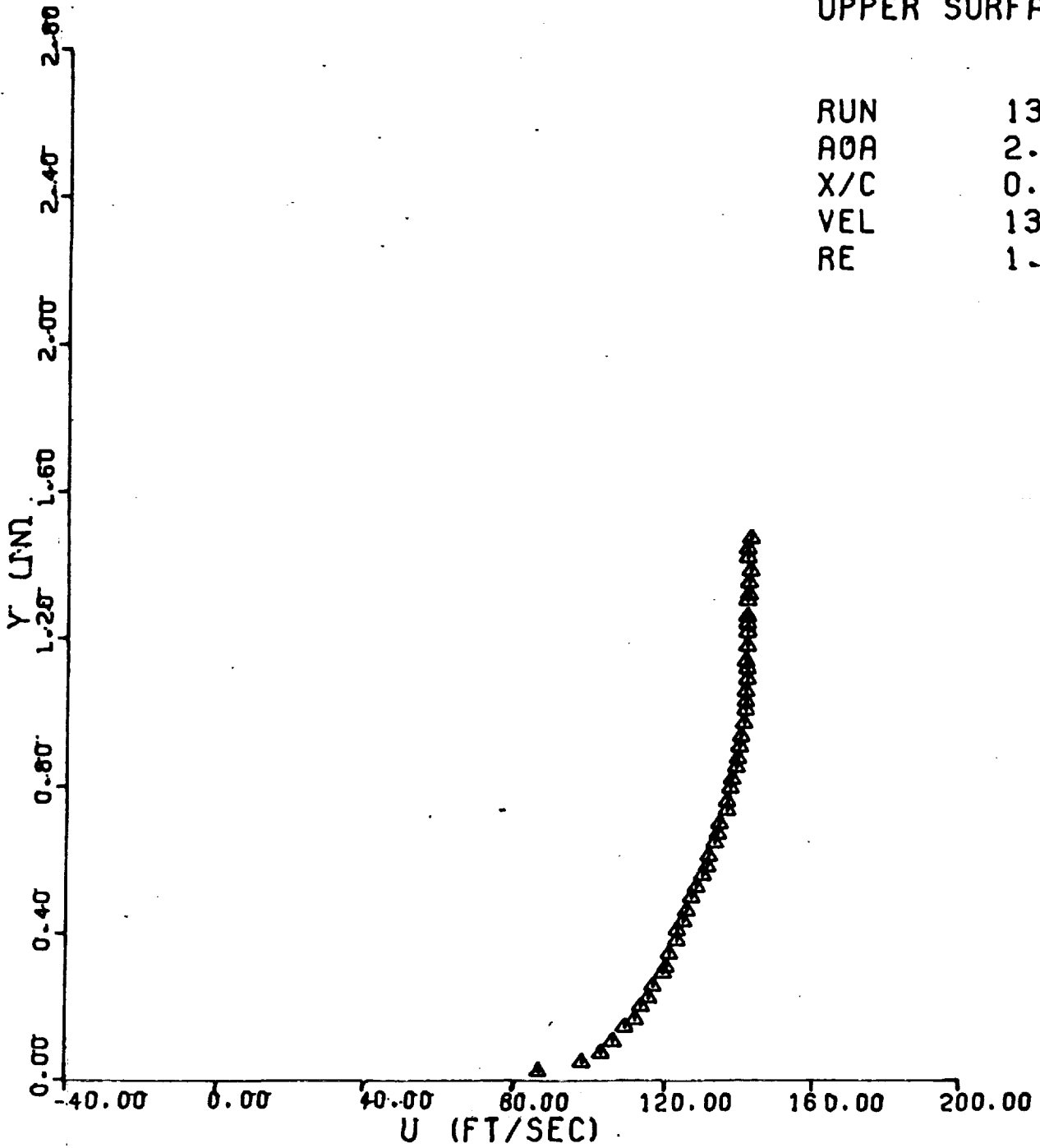
NACA 0012
UPPER SURFACE

RUN	1312
AOA	2.000
X/C	0.3000
VEL	131.9
RE	1.55



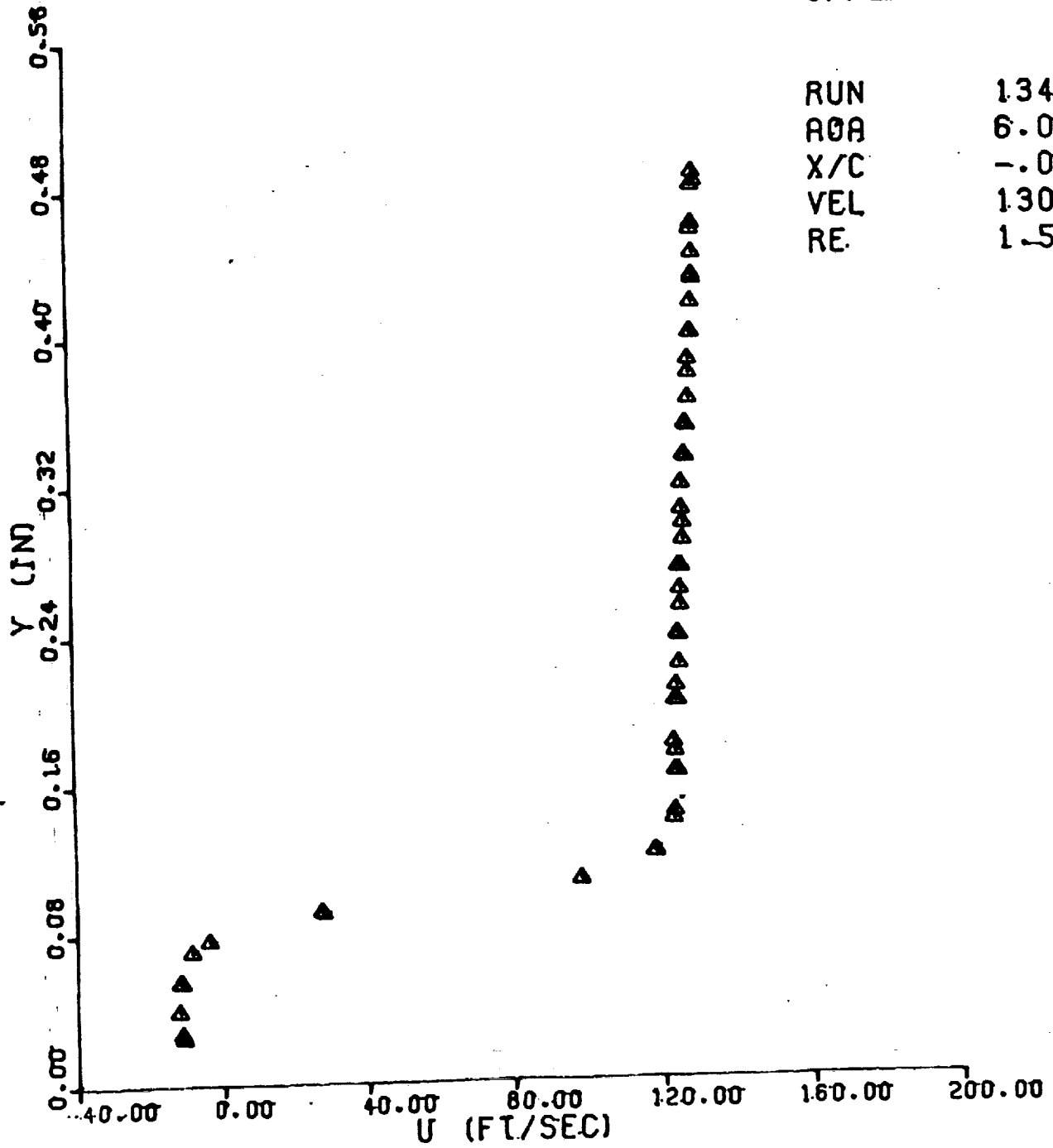
NACA 0012
UPPER SURFACE

RUN	1313
AOA	2.000
X/C	0.6000
VEL	131.8
RE	1.54



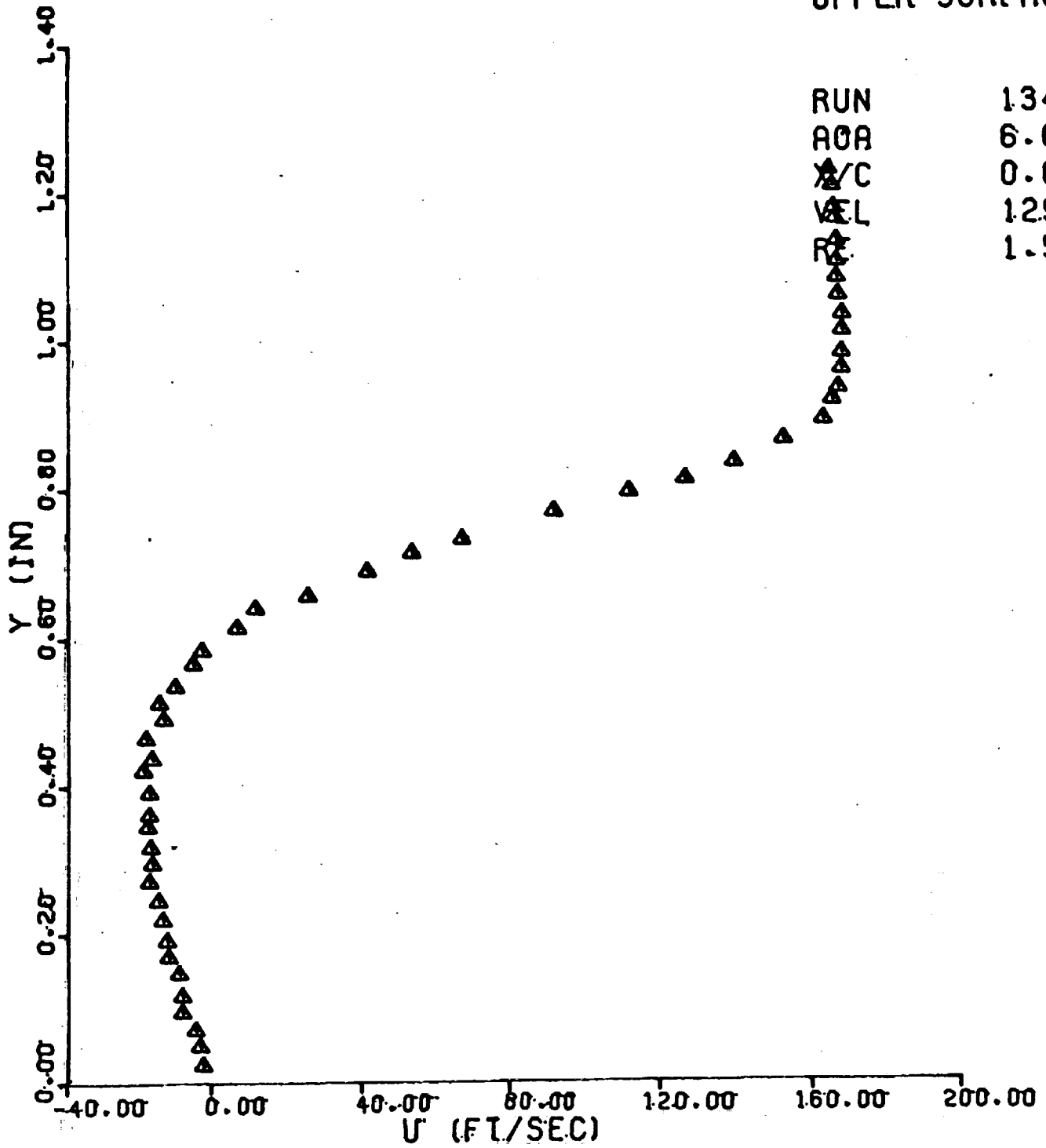
NACA 0012
UPPER SURFACE

RUN	1344
AOA	6.000
X/C	-.0200
VEL	130.2
RE	1.53



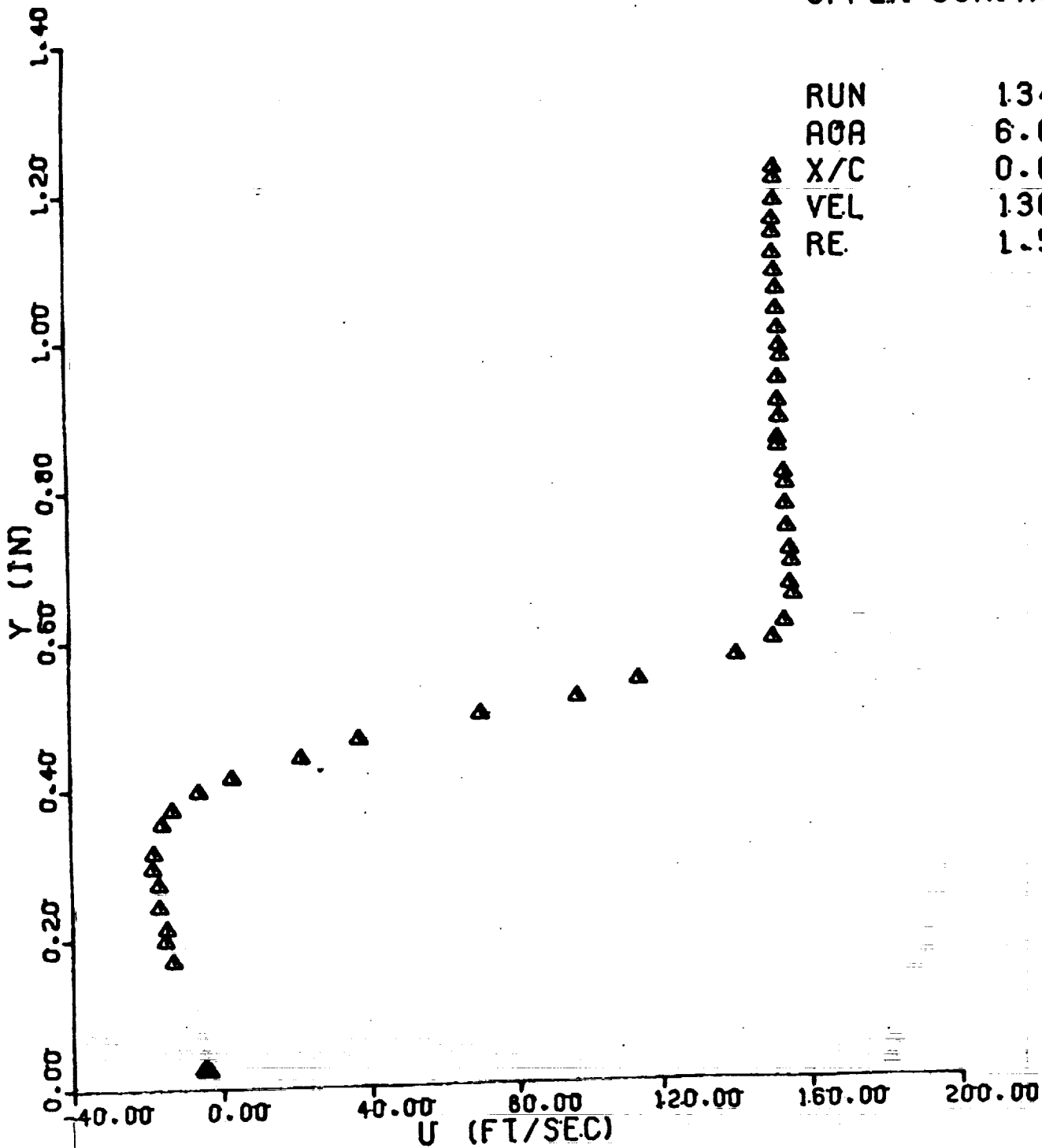
NACA 0012
UPPER SURFACE

RUN	1346
AOA	6.000
X/C	0.0200
VEL	129.8
RE	1.53



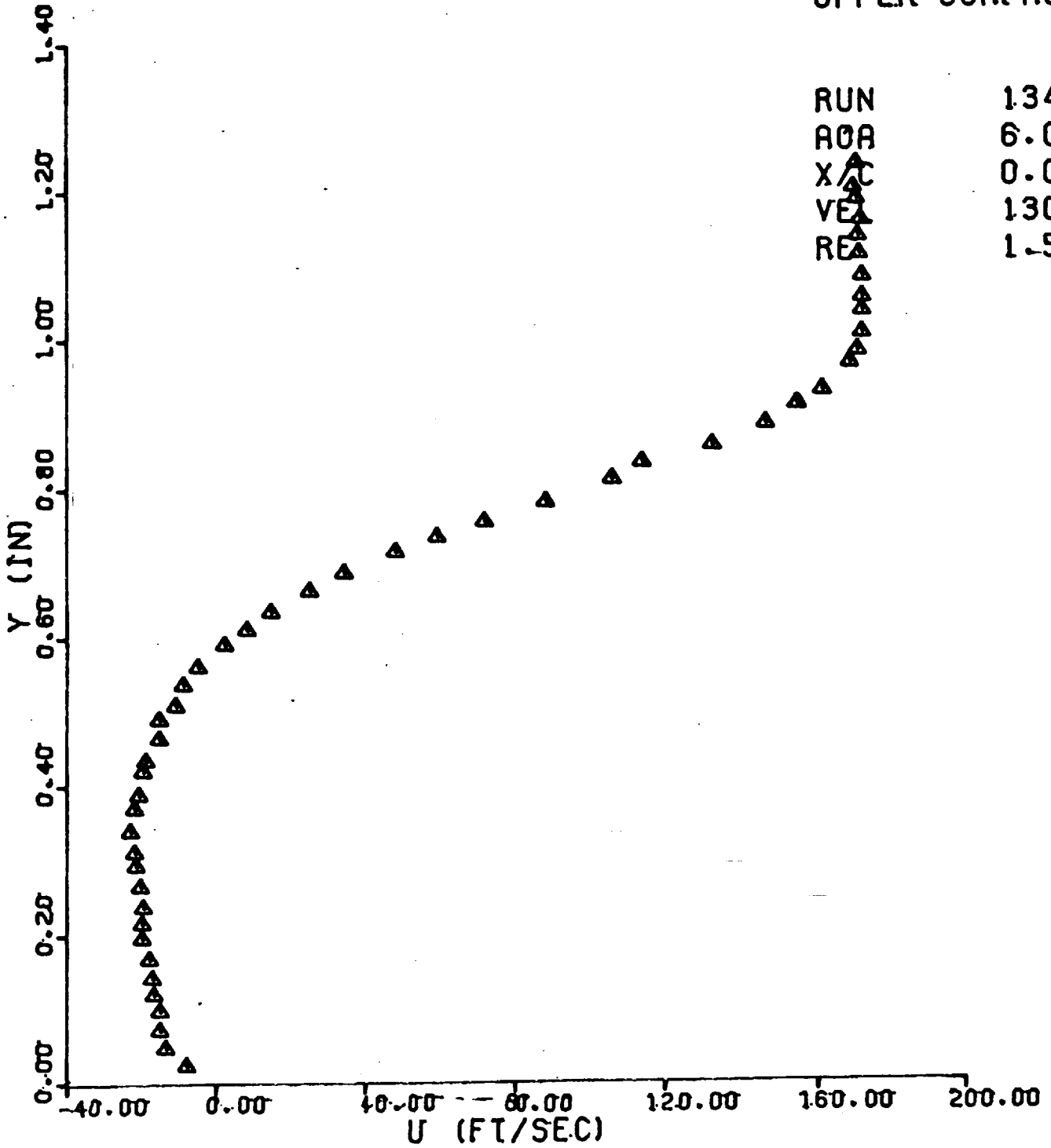
NACA 0012
UPPER SURFACE

RUN	1347
AOA	6.000
X/C	0.0000
VEL	130.3
RE	1.53



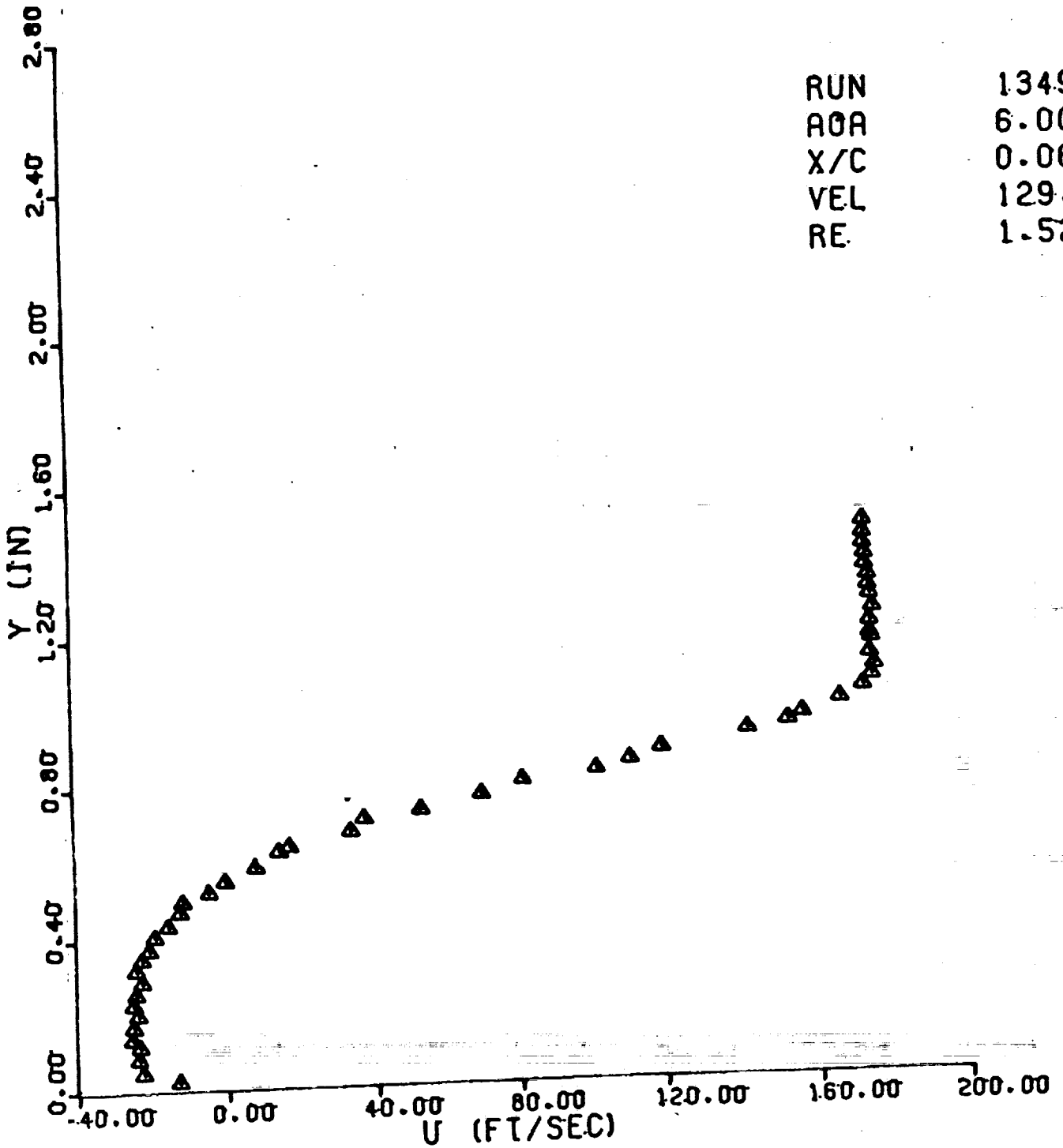
NACA 0012
UPPER SURFACE

RUN	1348
AOA	6.000
X/C	0.0400
VE	130.1
RE	1.53



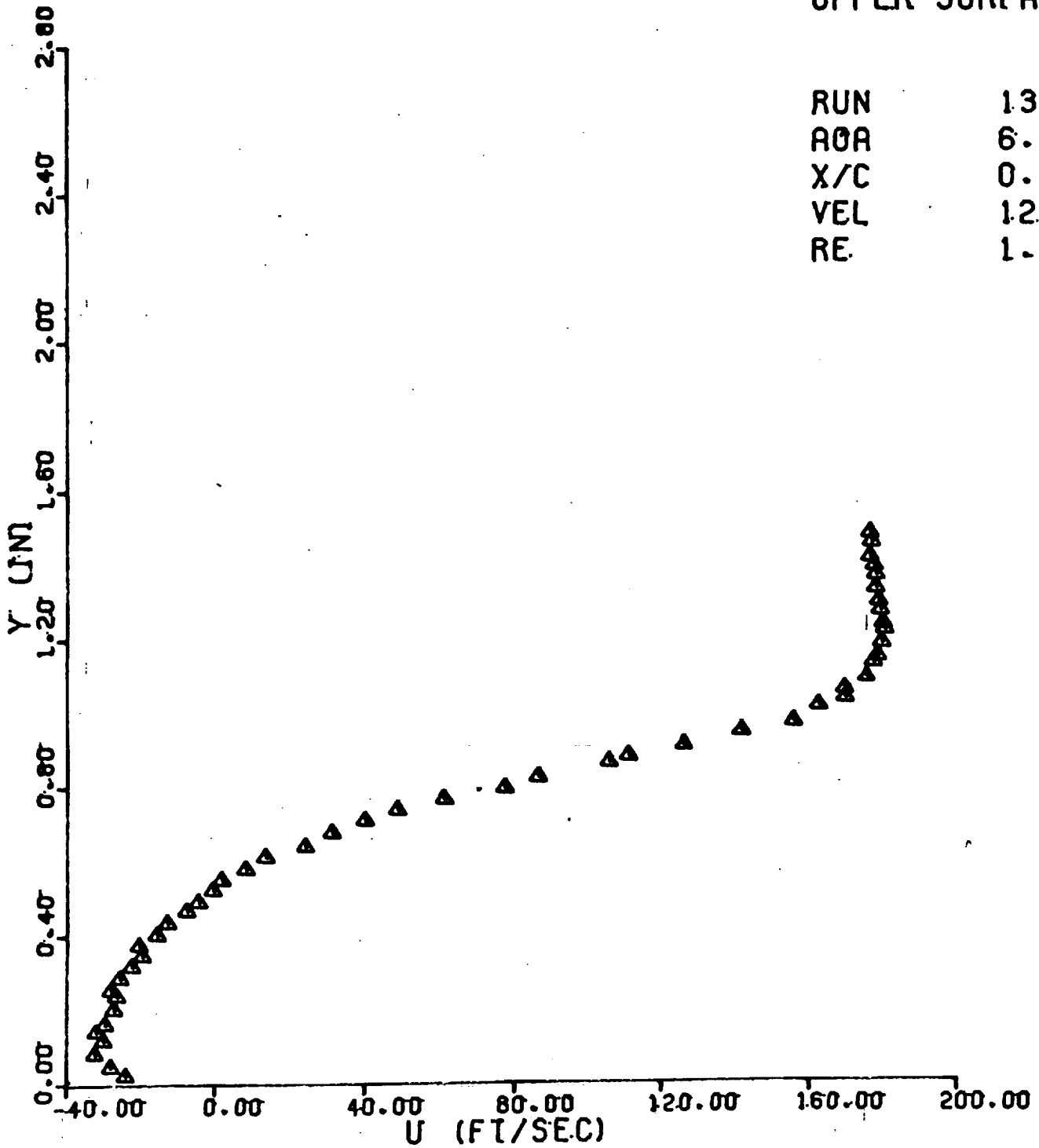
NACA 0012
UPPER SURFACE

RUN	1349
AOA	6.000
X/C	0.0600
VEL	129.0
RE	1.52



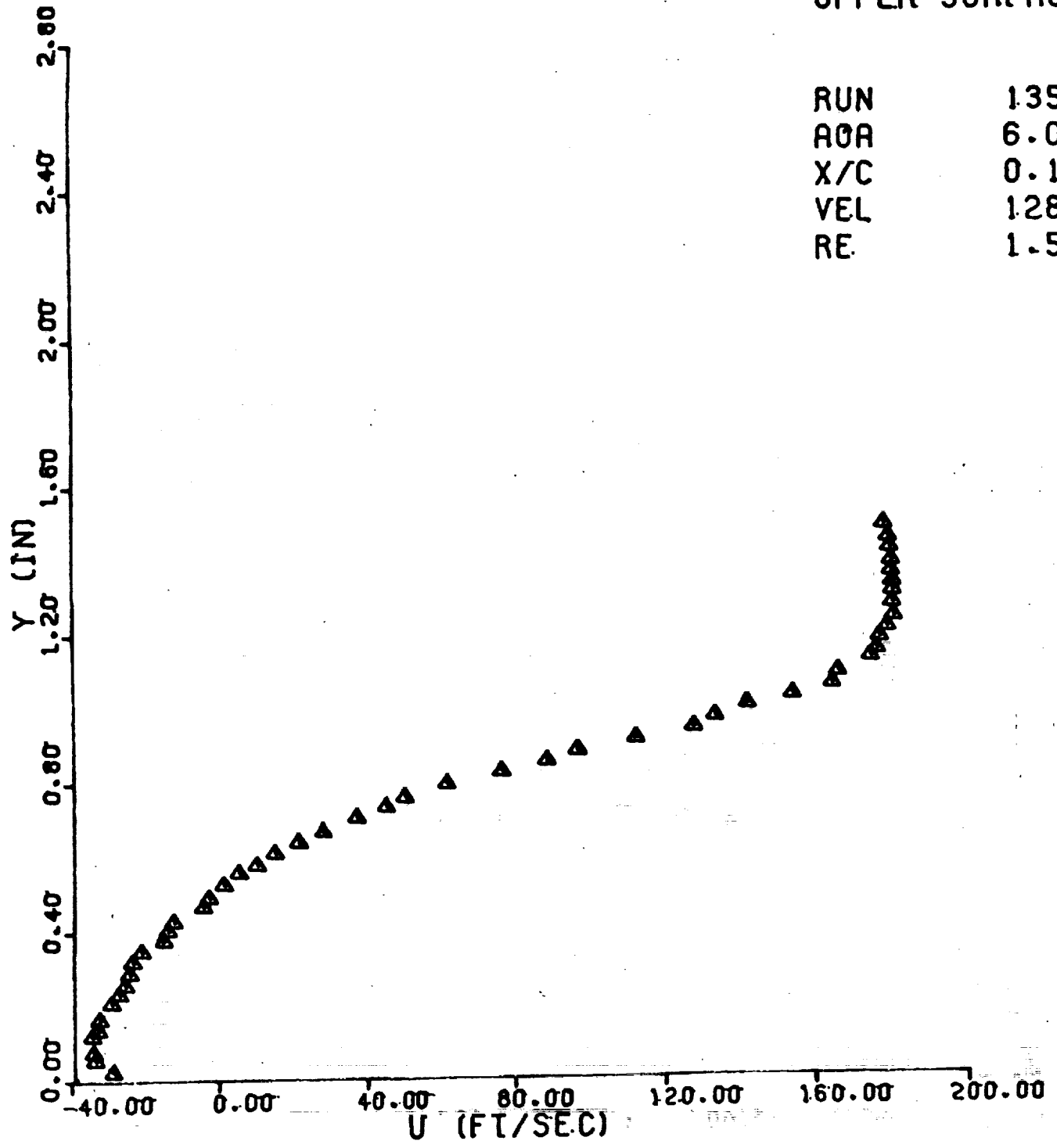
NACA 0012
UPPER SURFACE

RUN	1350
AOA	6.000
X/C	0.0800
VEL	129.0
RE	1.52



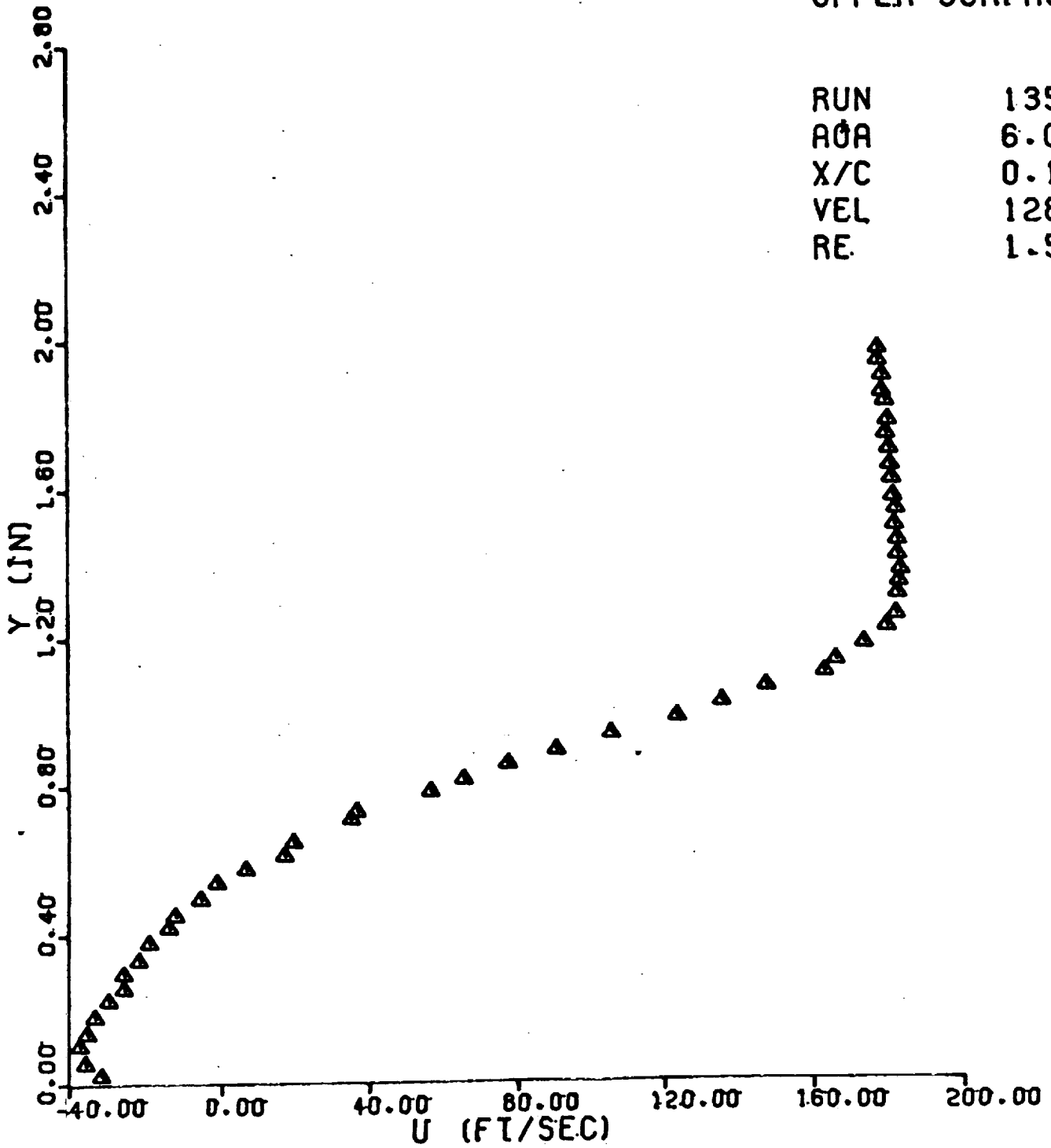
NACA 0012
UPPER SURFACE

RUN	1351
AOA	6.000
X/C	0.1000
VEL	128.3
RE	1.51



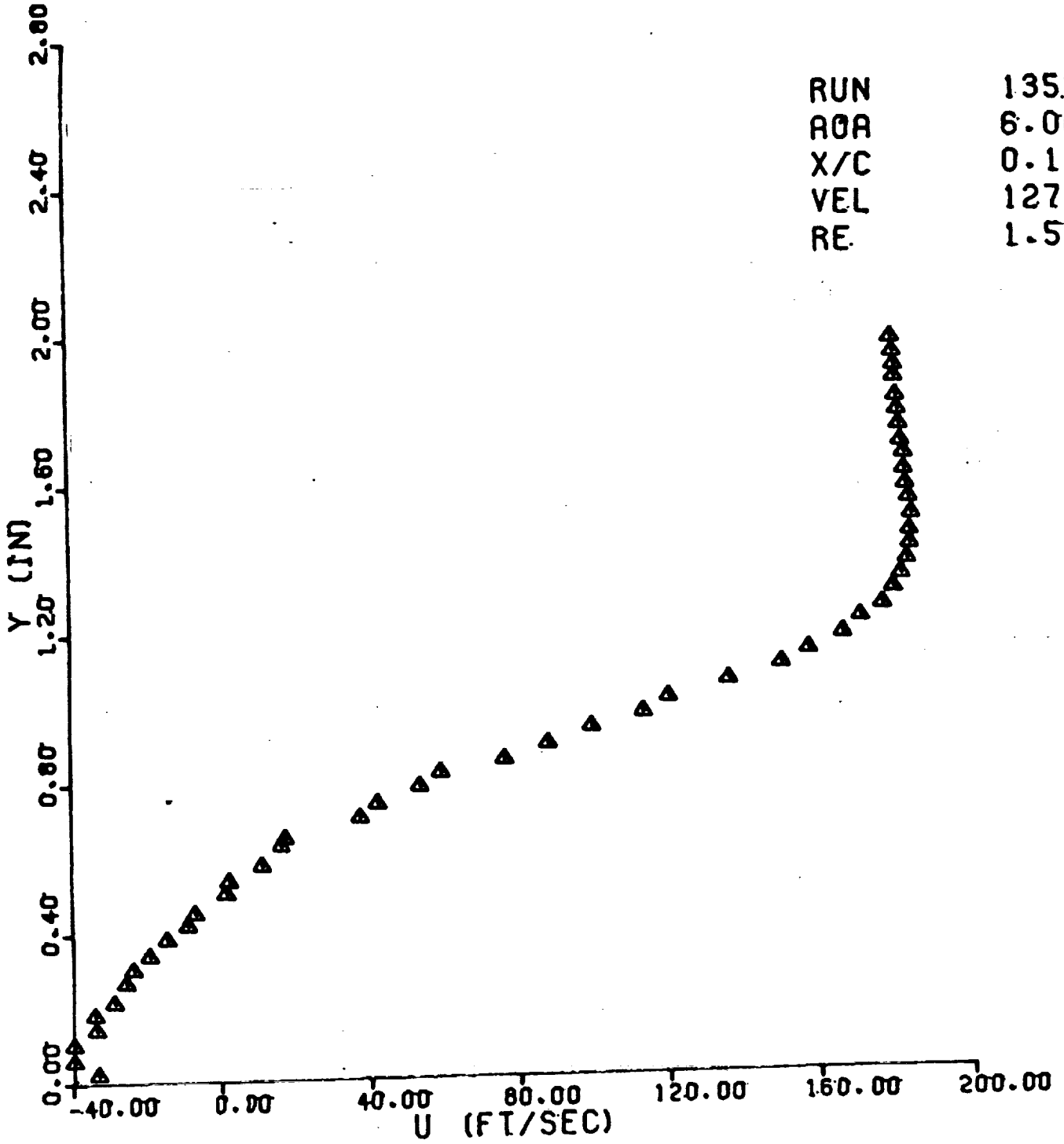
NACA 0012
UPPER SURFACE

RUN	1352
AOA	6.000
X/C	0.1200
VEL	128.0
RE.	1.51



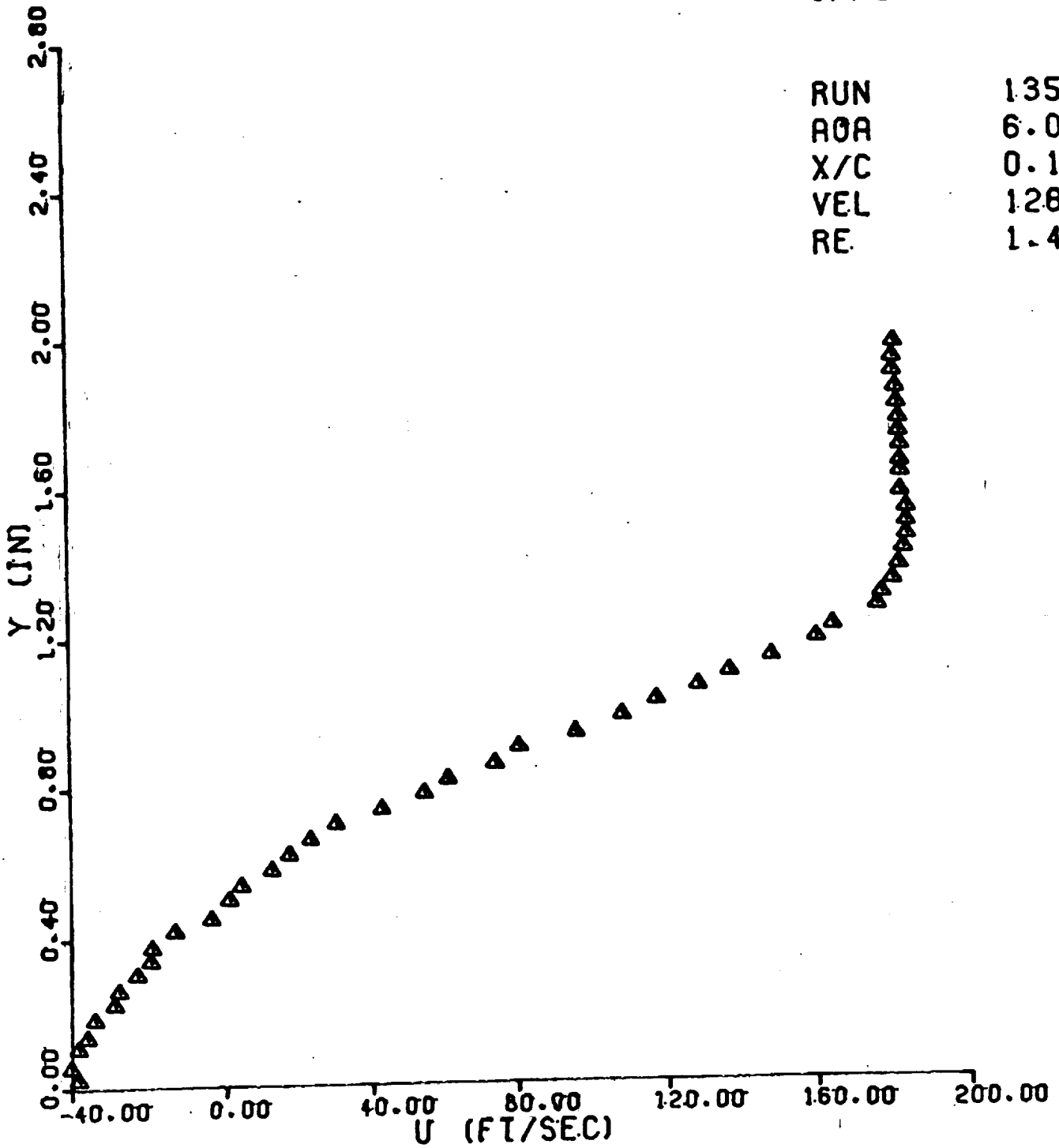
NACA 0012
UPPER SURFACE

RUN	1353
AOA	6.000
X/C	0.1400
VEL	127.4
RE	1.50



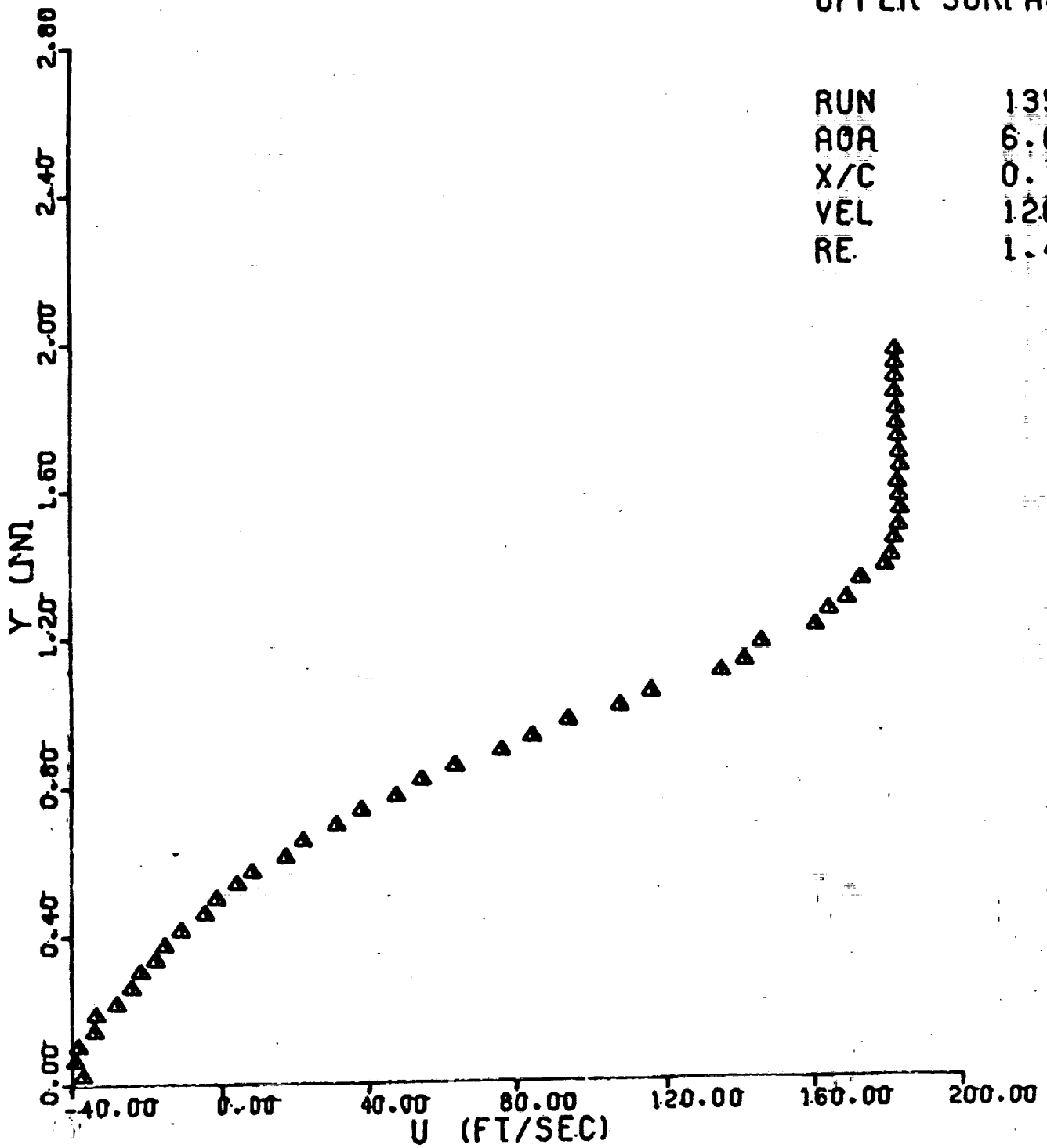
NACA 0012
UPPER SURFACE

RUN	1354
AOA	6.000
X/C	0.1600
VEL	128.1
RE	1.48

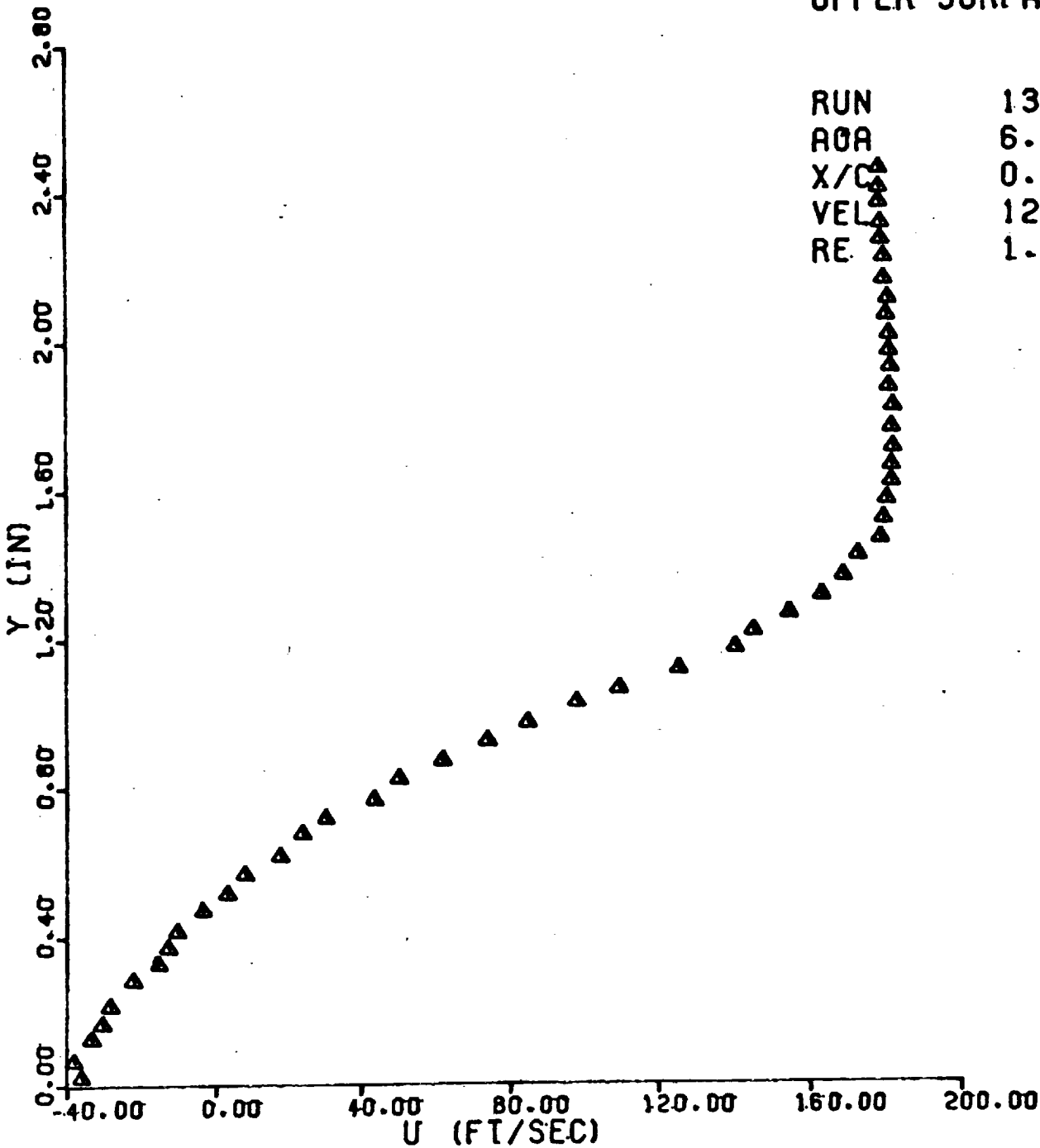


NACA 0012
UPPER SURFACE

RUN 1355
AOA 6.000
X/C 0.1800
VEL 126.5
RE 1.49

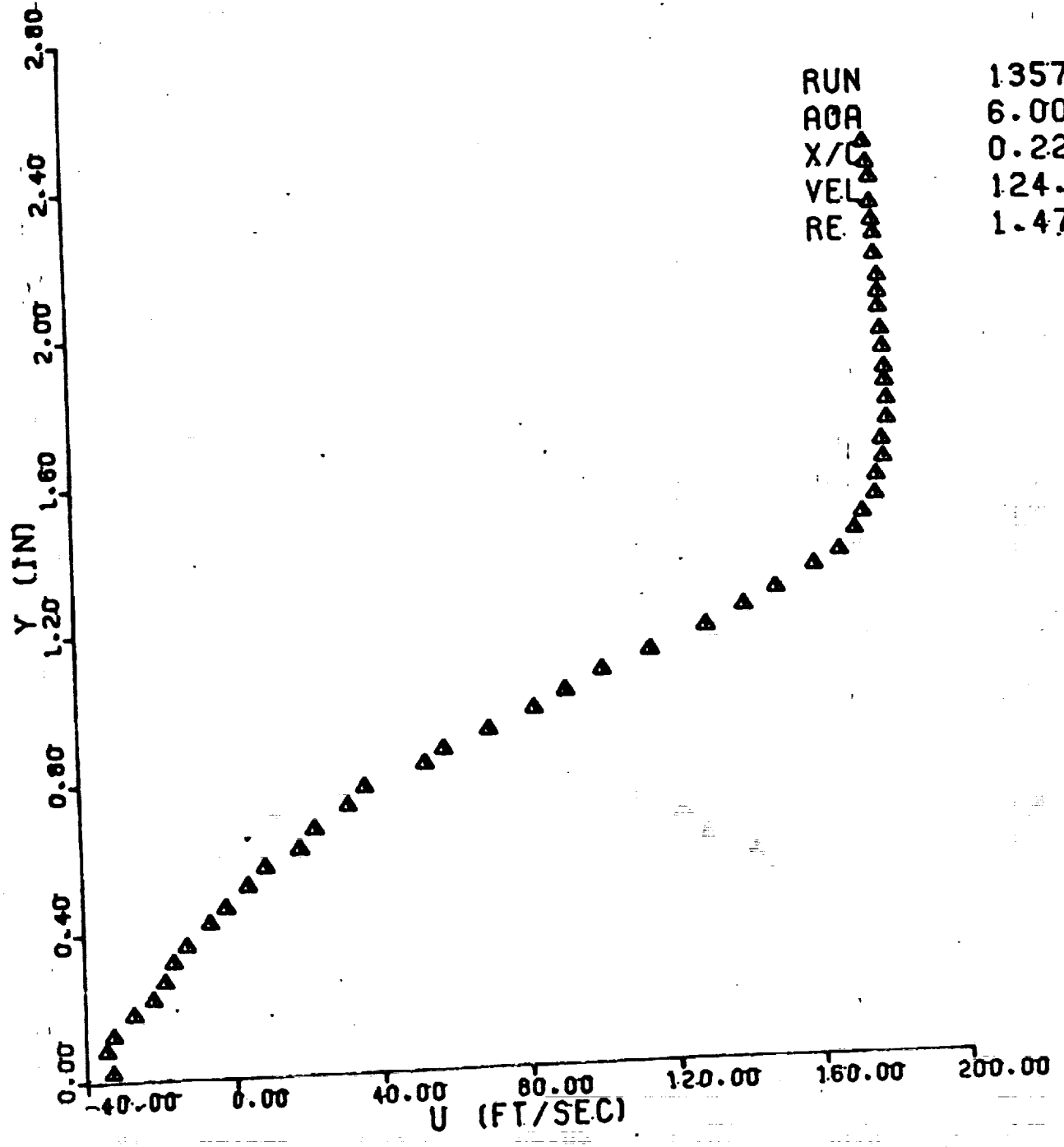


NACA 0012
UPPER SURFACE



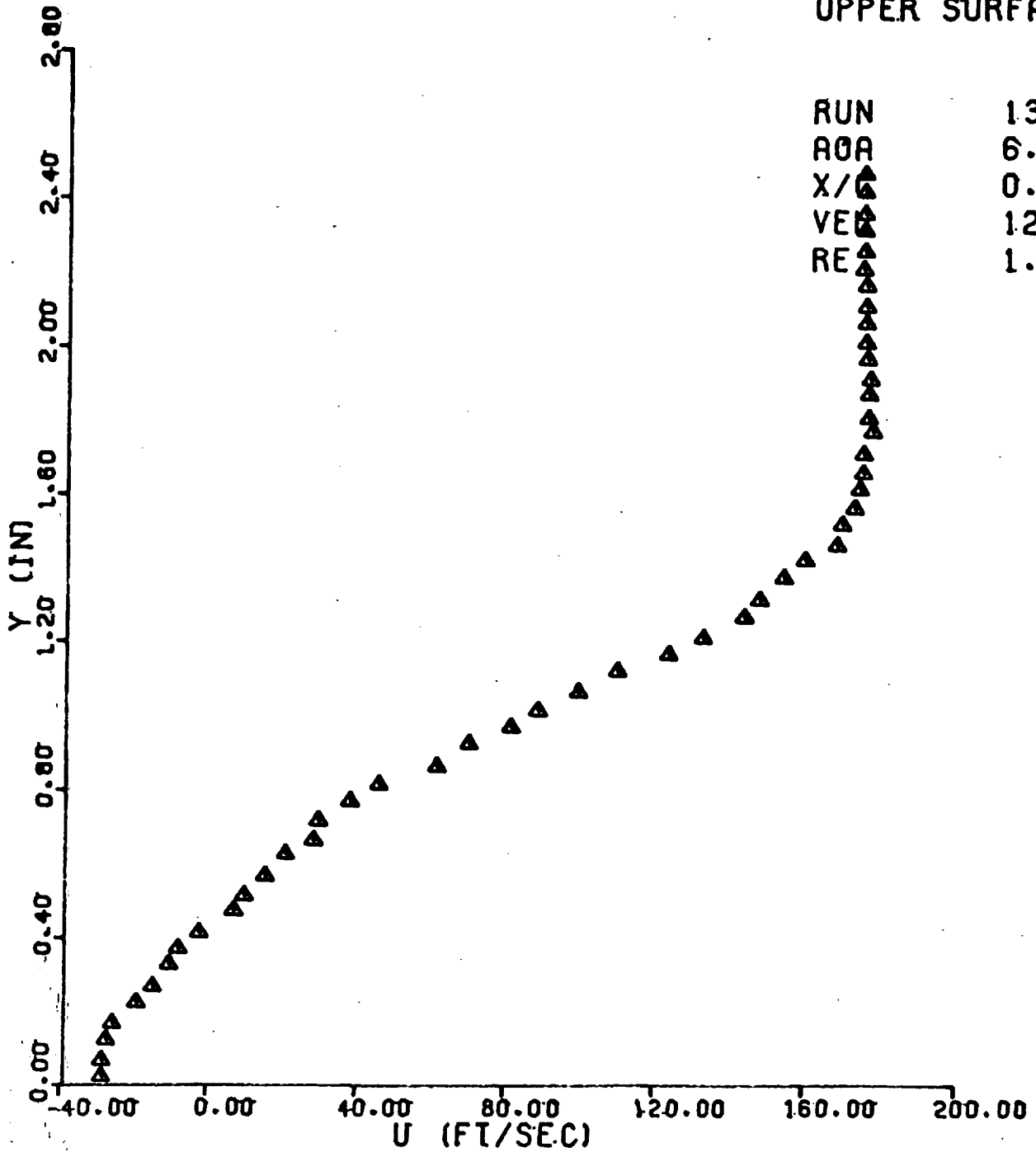
RUN 1356
AOA 6.000
X/C 0.2000
VEL 126.3
RE. 1.49

NACA 0012
UPPER SURFACE



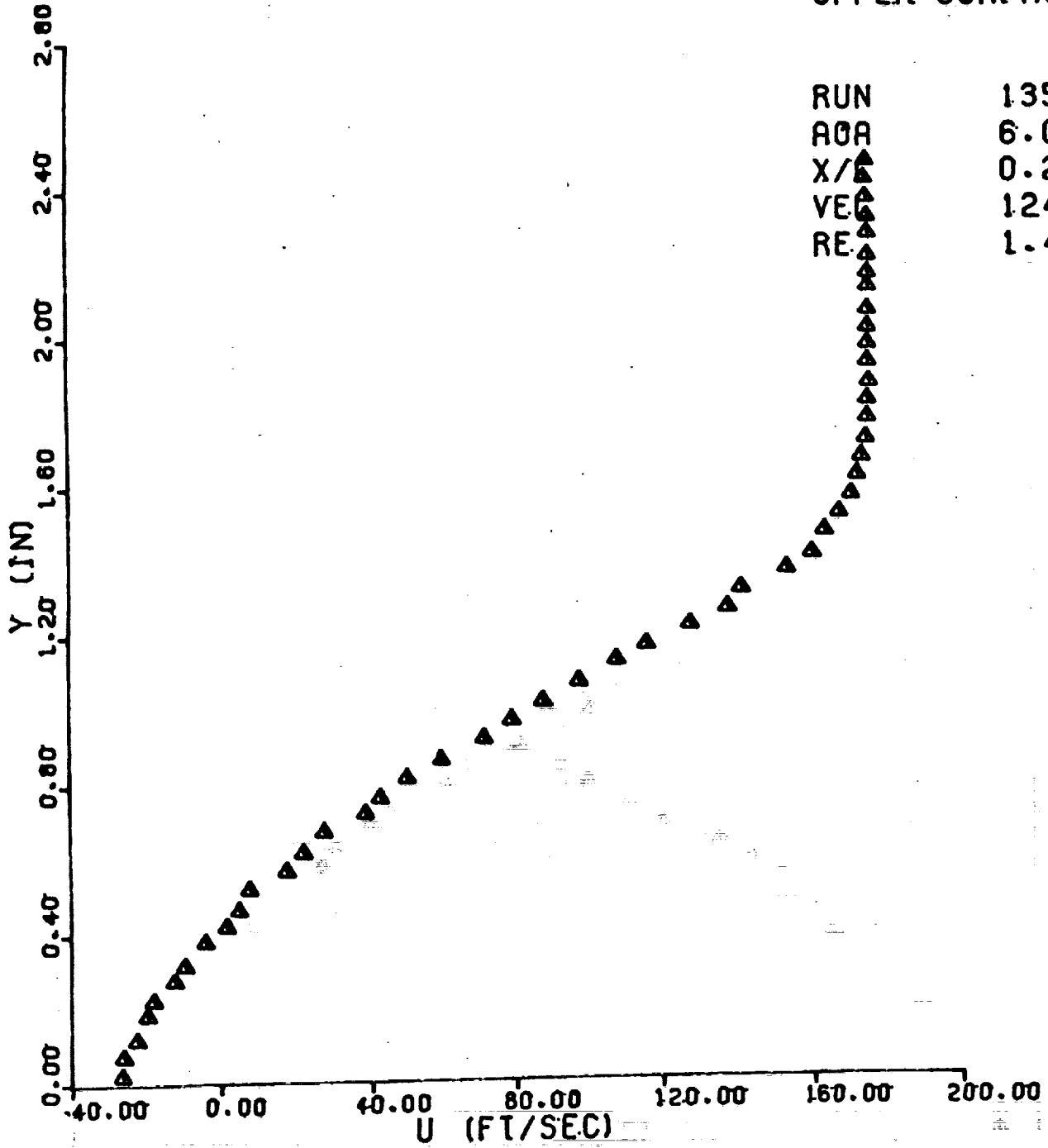
RUN	1357
AOA	6.000
X/C	0.2200
VEL	124.9
RE	1.47

NACA 0012
UPPER SURFACE



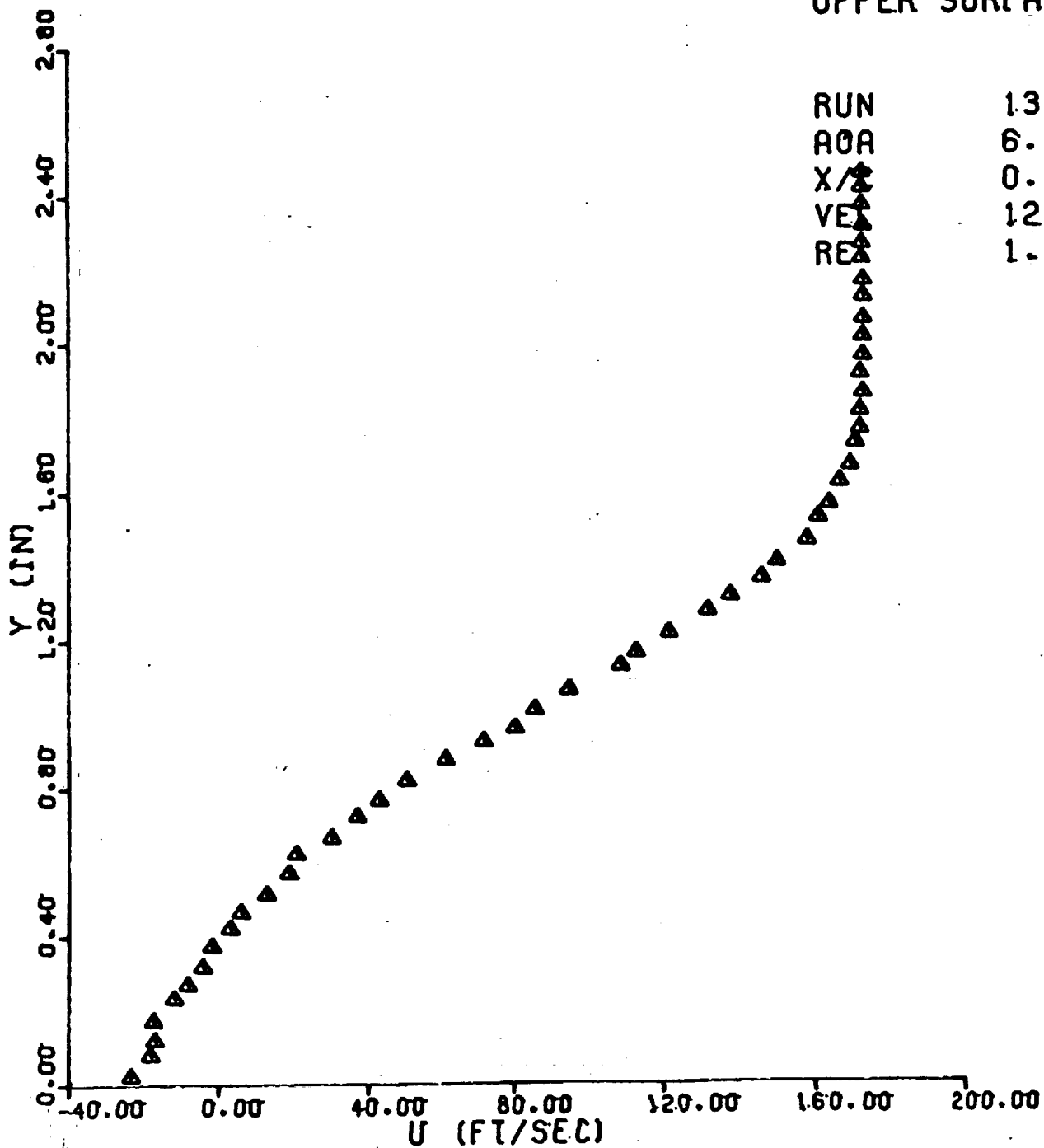
RUN 1358
AOA 6.000
X/C 0.2400
VELOCITY 124.1
REYNOLDS 1.48

NACA 0012
UPPER SURFACE



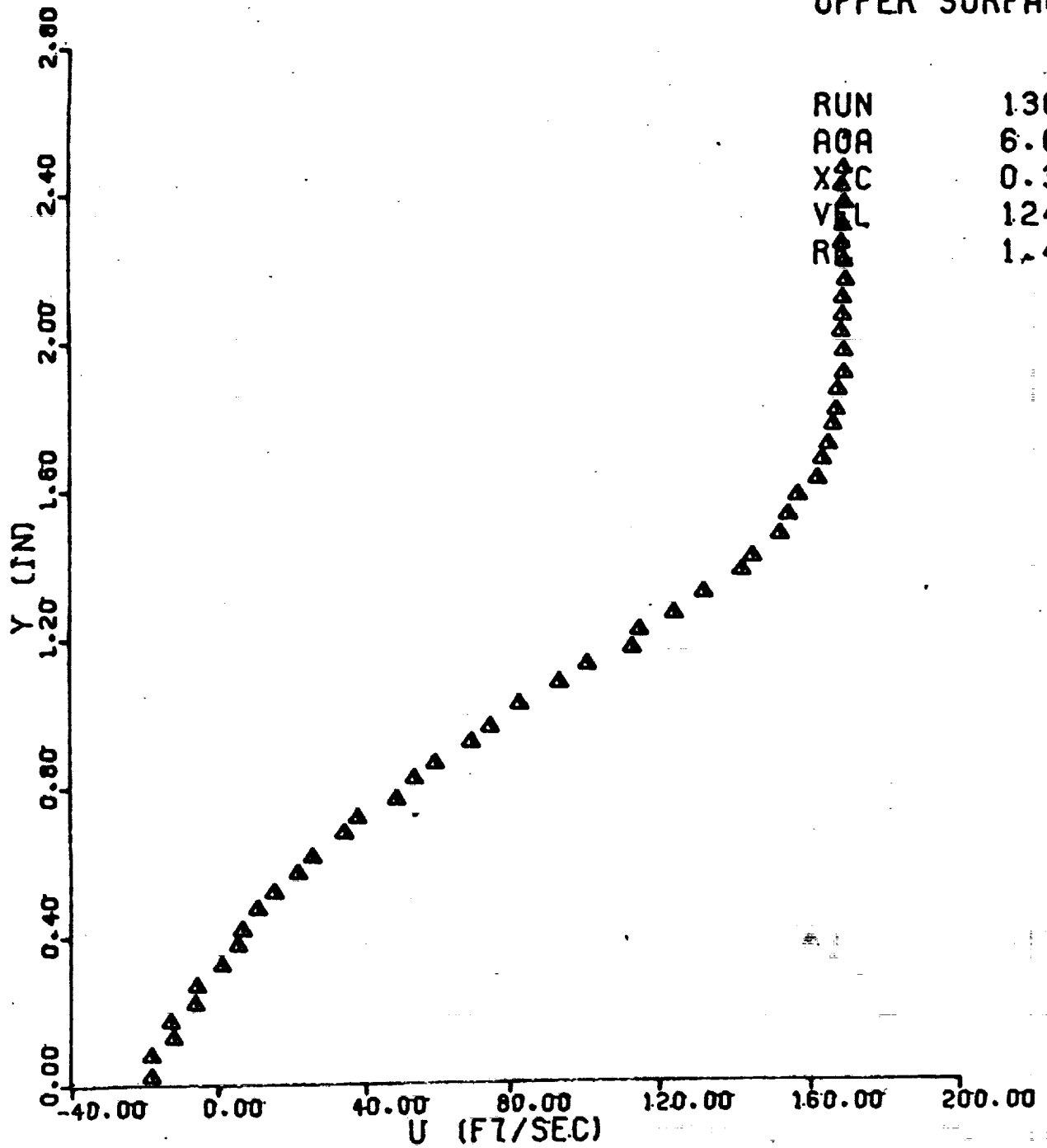
RUN 1359
AOA 6.000
X/▲ 0.2600
VE▲ 124.8
RE▲ 1.47

NACA 0012
UPPER SURFACE



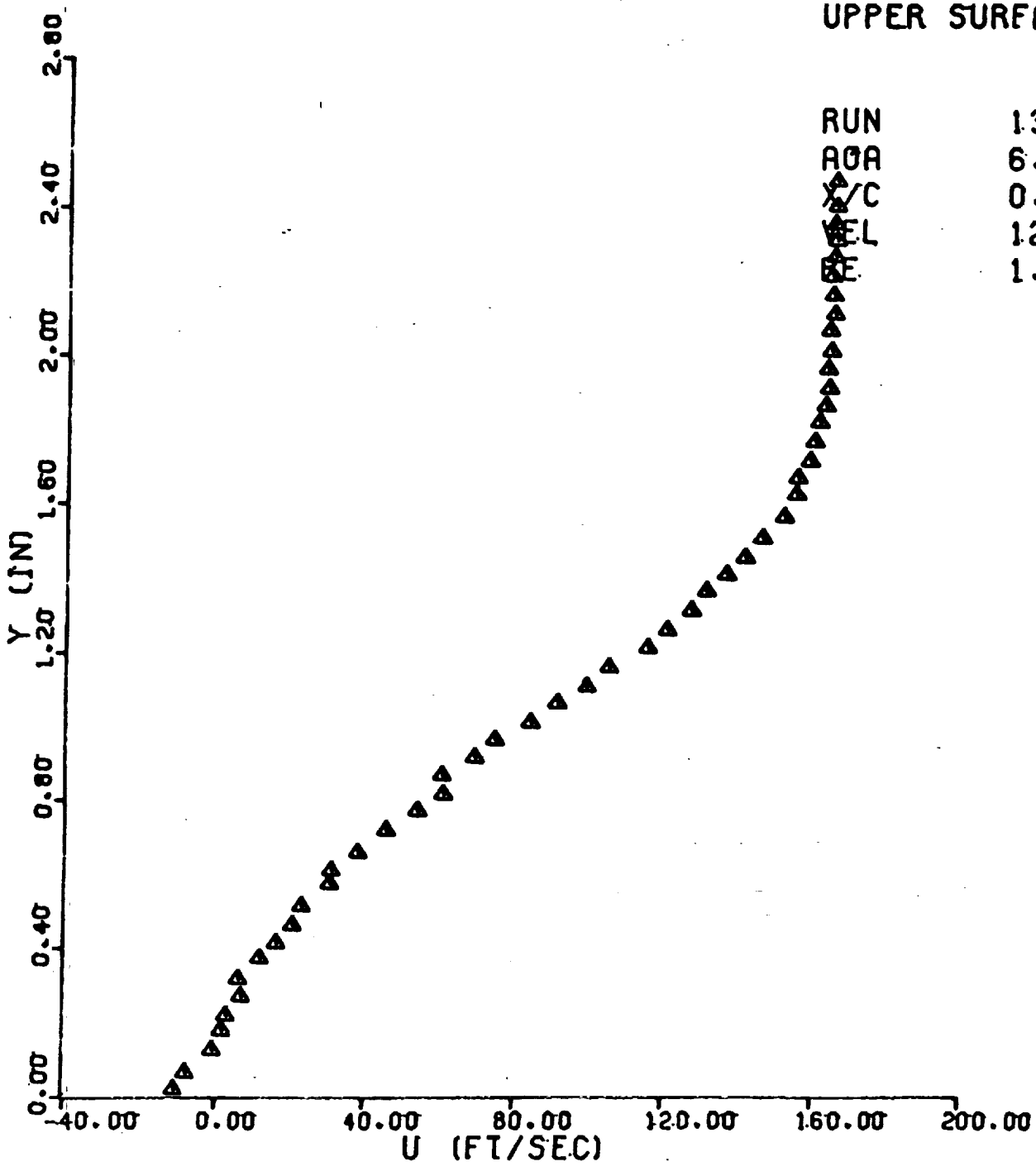
RUN 1.360
AOA 6.000
X/2 0.2800
VEL 124.3
REA 1.48

NACA 0012
UPPER SURFACE



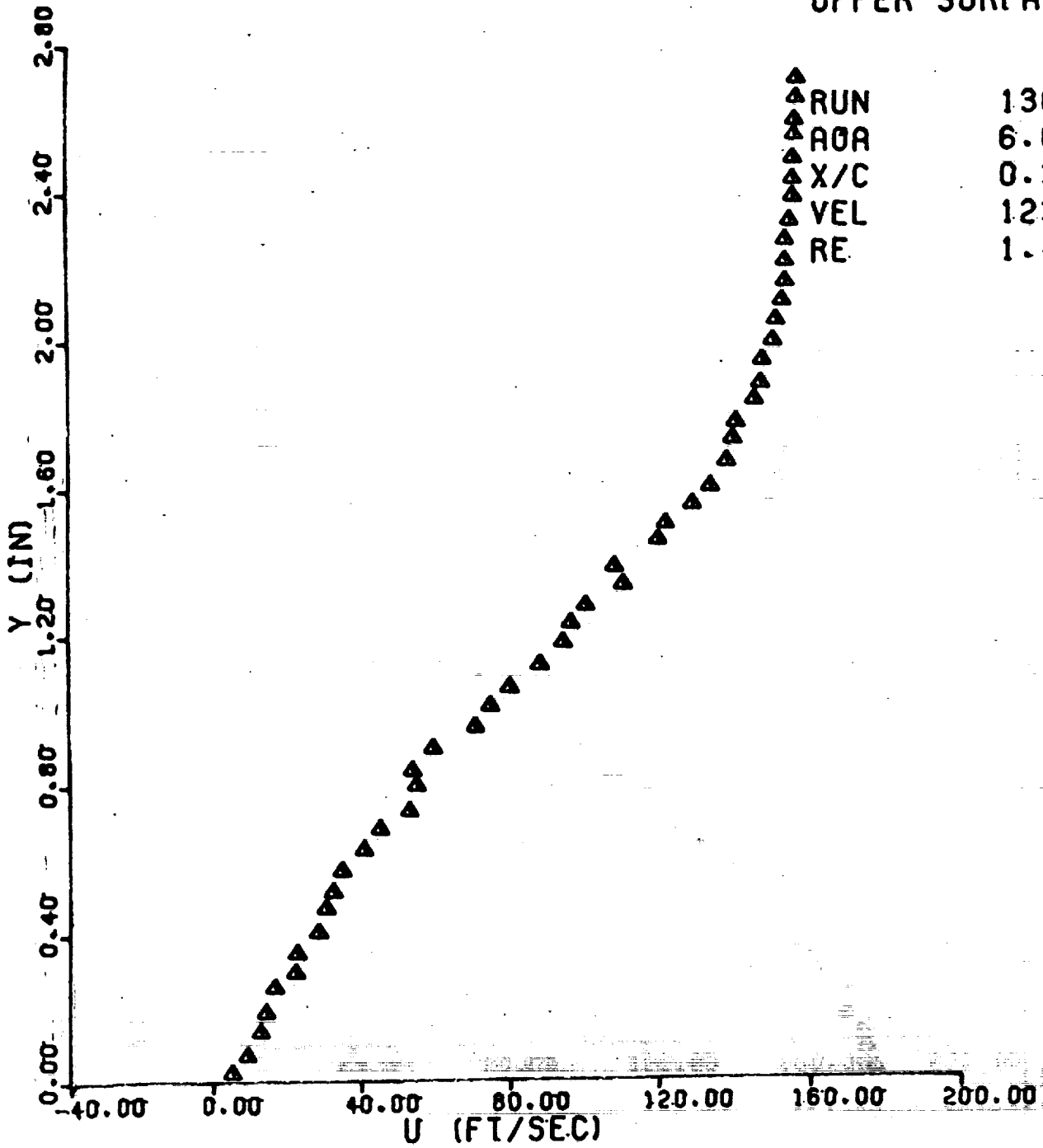
RUN 1361
AOA 6.000
X/C 0.3000
VEL 124.3
RE 1.47

NACA 0012
UPPER SURFACE

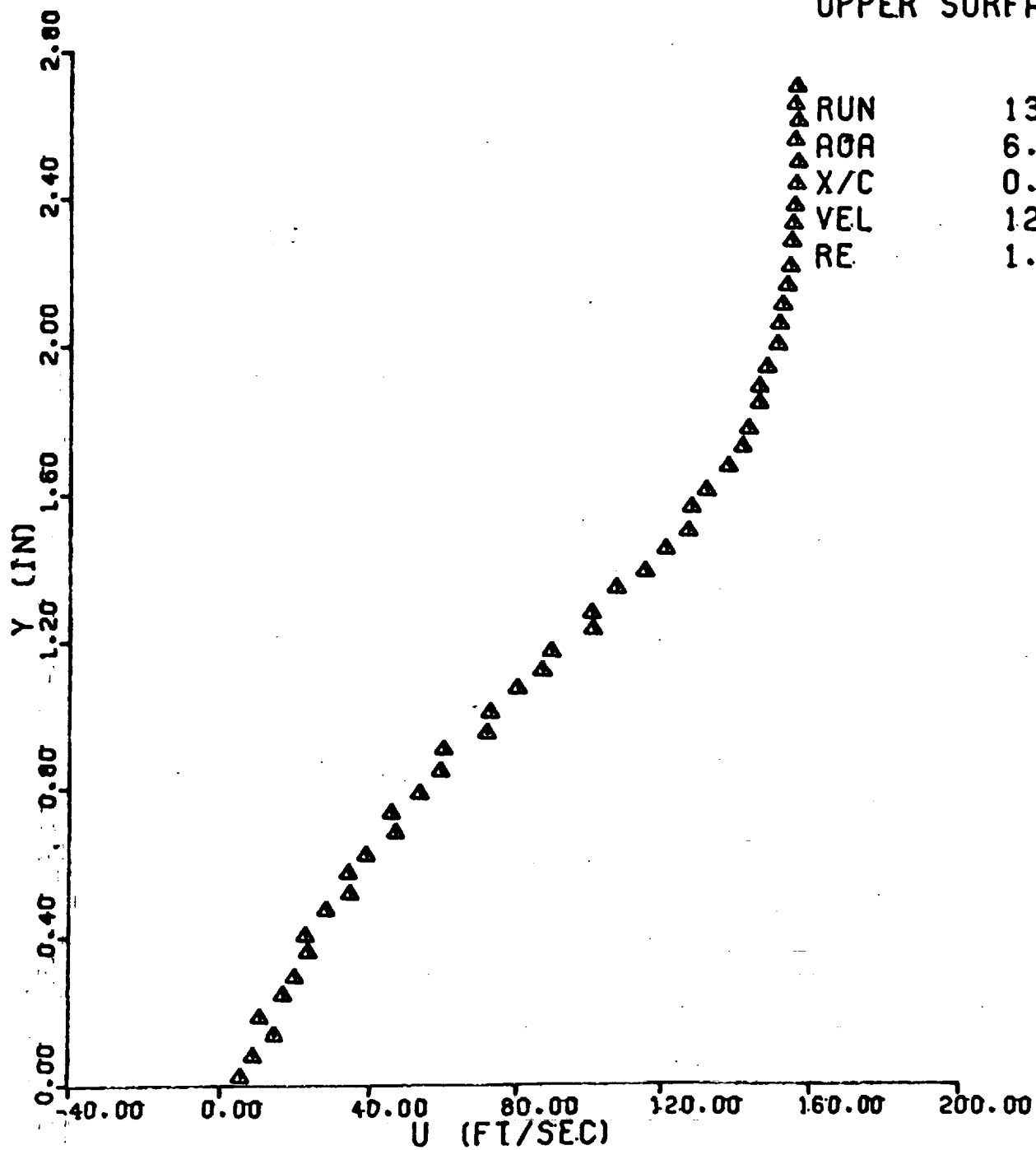


RUN	1362
AOA	6.000
X/C	0.3400
VEL	124.0
RE	1.46

NACA 0012
UPPER SURFACE

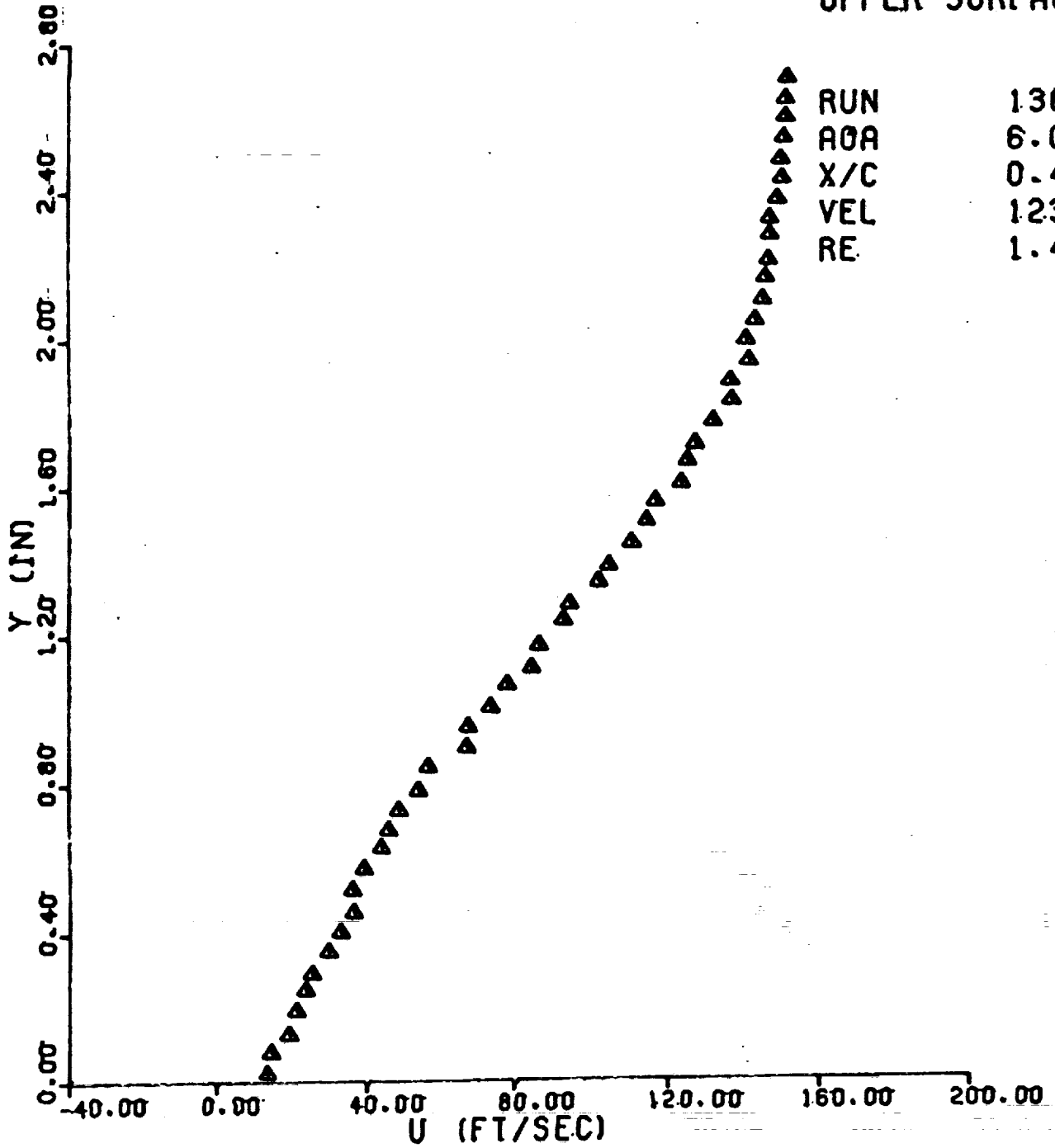


NACA 0012
UPPER SURFACE



▲	RUN	1364
▲	AOA	6.000
▲	X/C	0.4200
▲	VEL	123.4
▲	RE	1.46

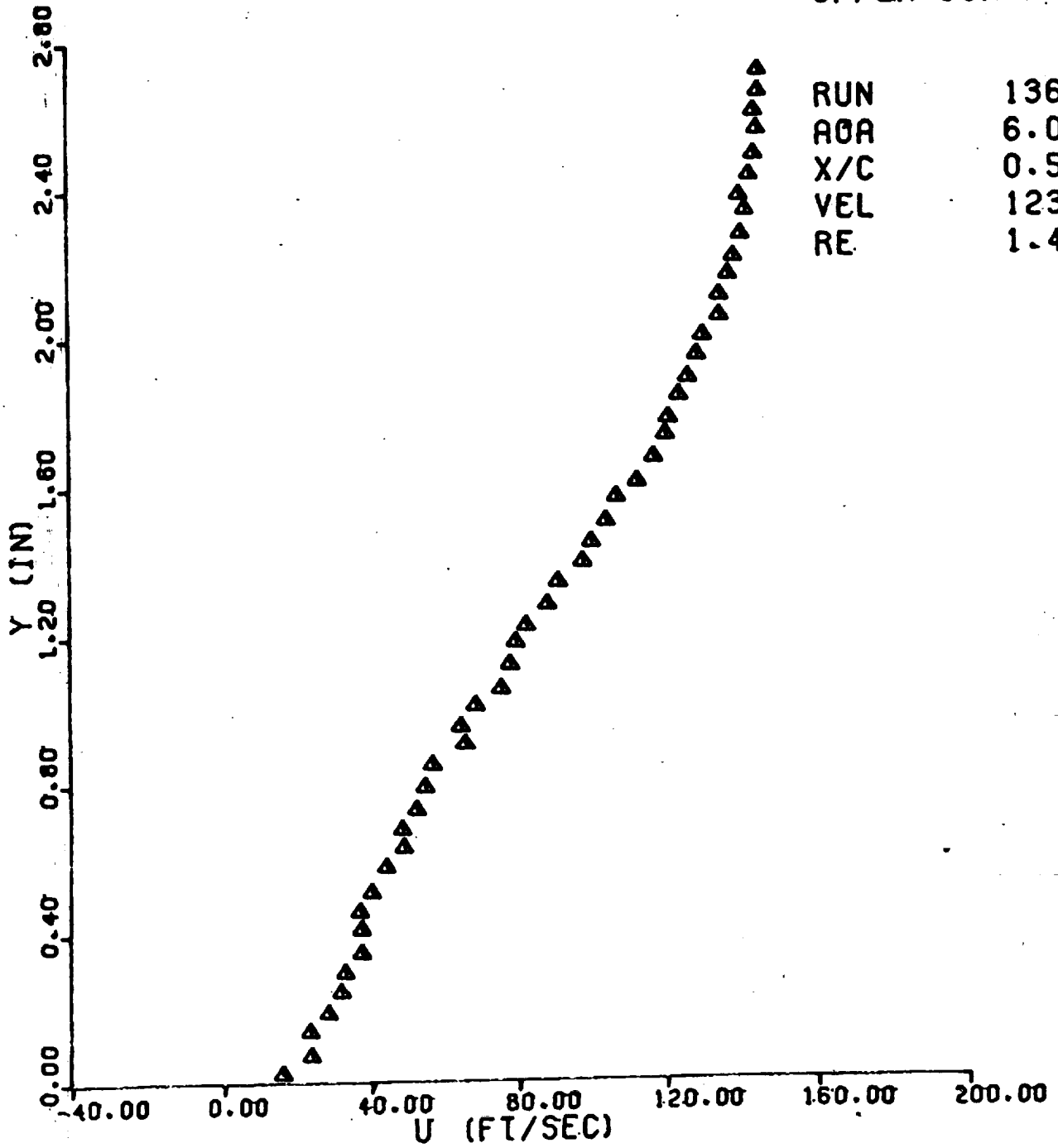
NACA 0012
UPPER SURFACE



RUN	1365
AOA	6.000
X/C	0.4700
VEL	123.7
RE.	1.48

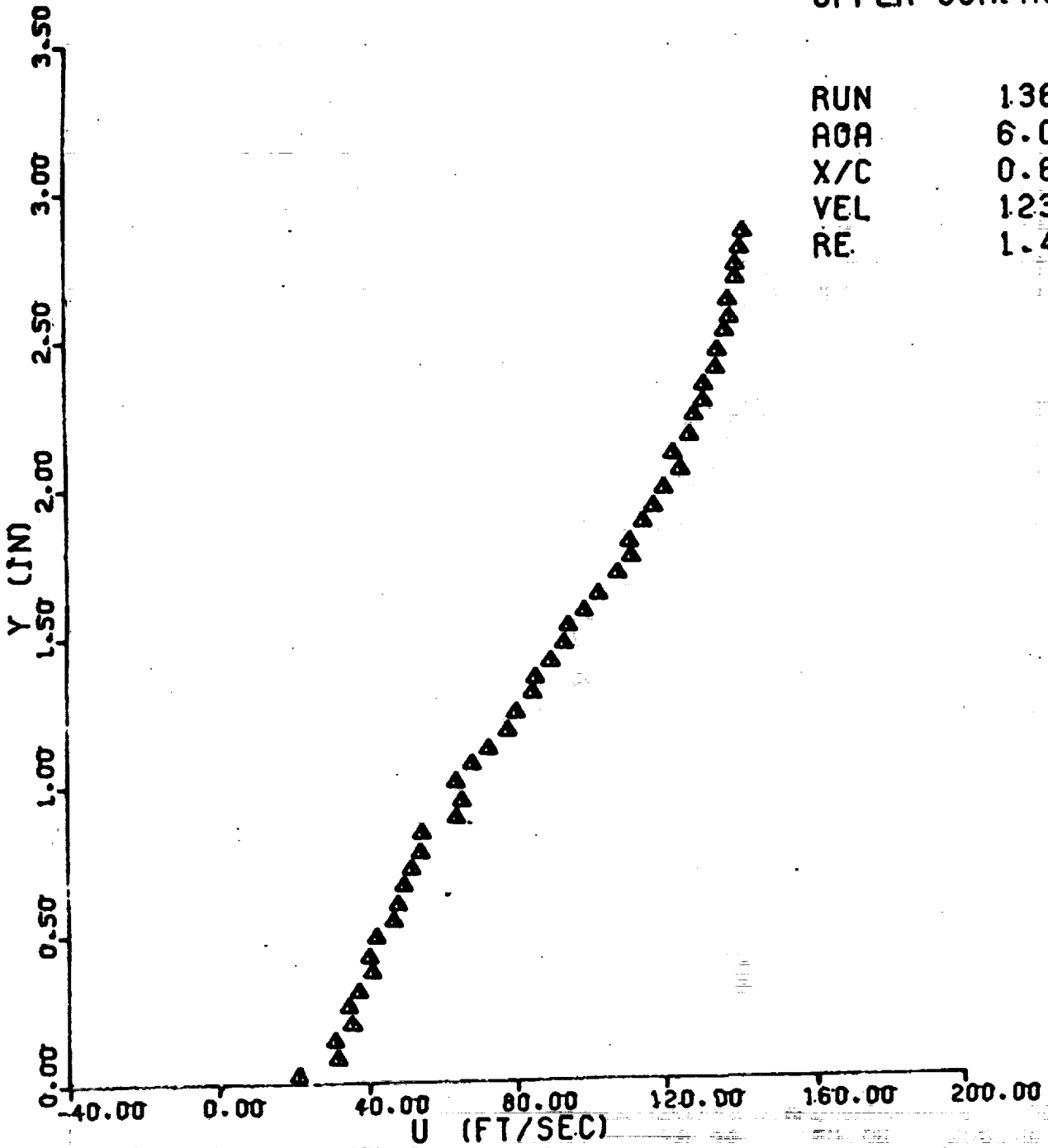
NACA 0012
UPPER SURFACE

RUN	1366
AOA	6.000
X/C	0.5300
VEL	123.0
RE	1.45

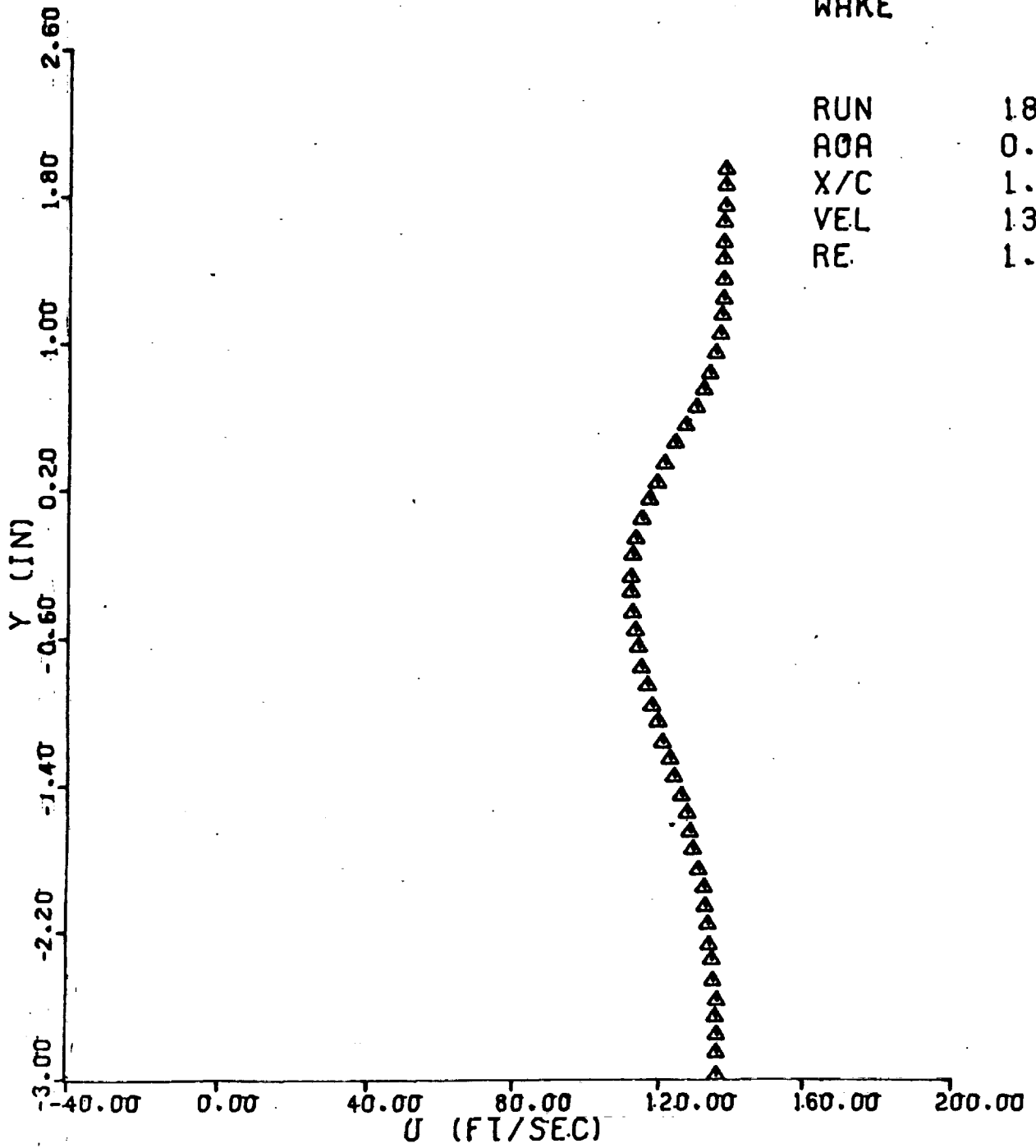


NACA 0012
UPPER SURFACE

RUN	1.367
AOA	6.000
X/C	0.6000
VEL	123.2
RE	1.48

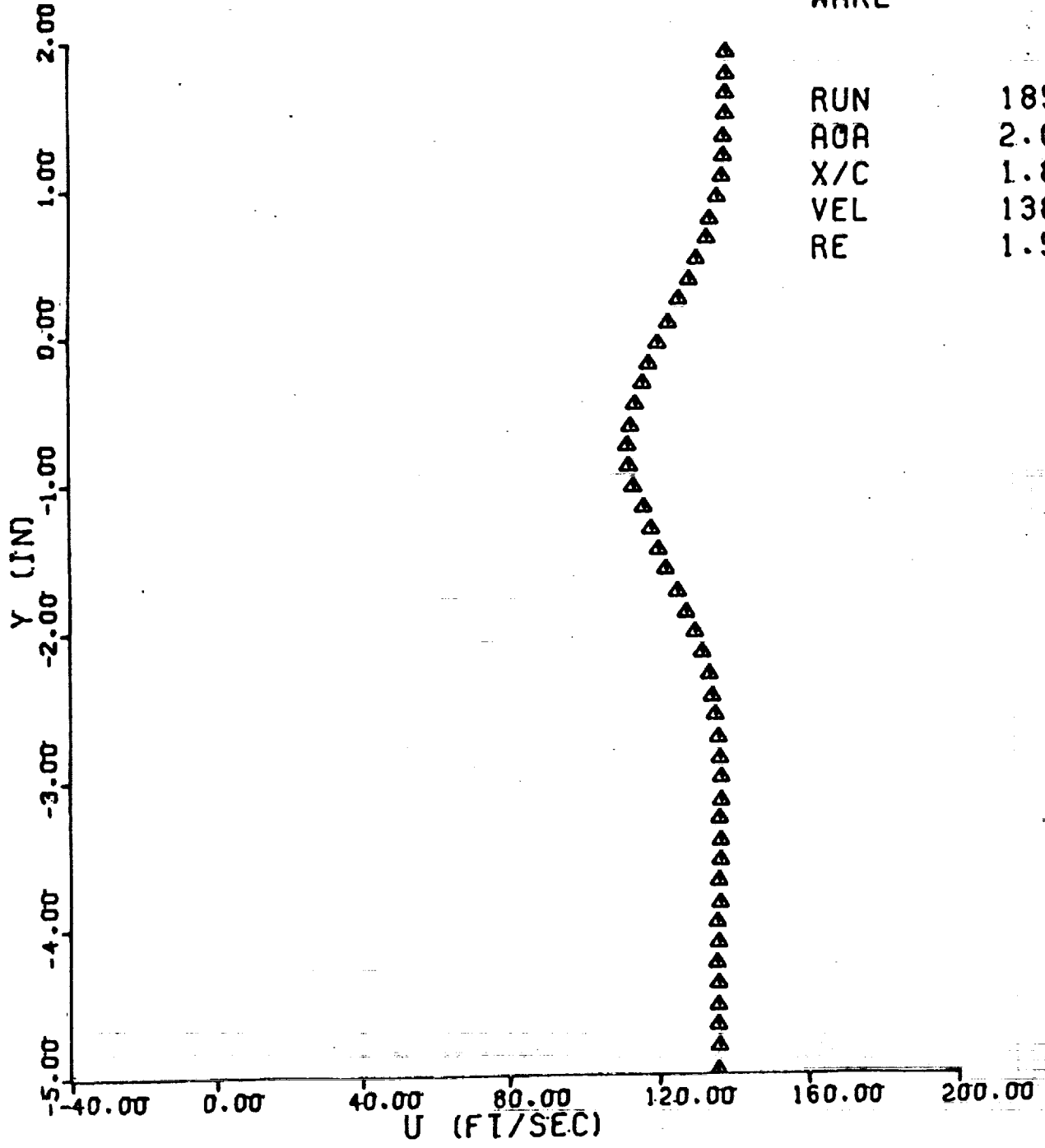


NACA 0012
WAKE



RUN	1850
AOA	0.000
X/C	1.8000
VEL	138.4
RE	1.57

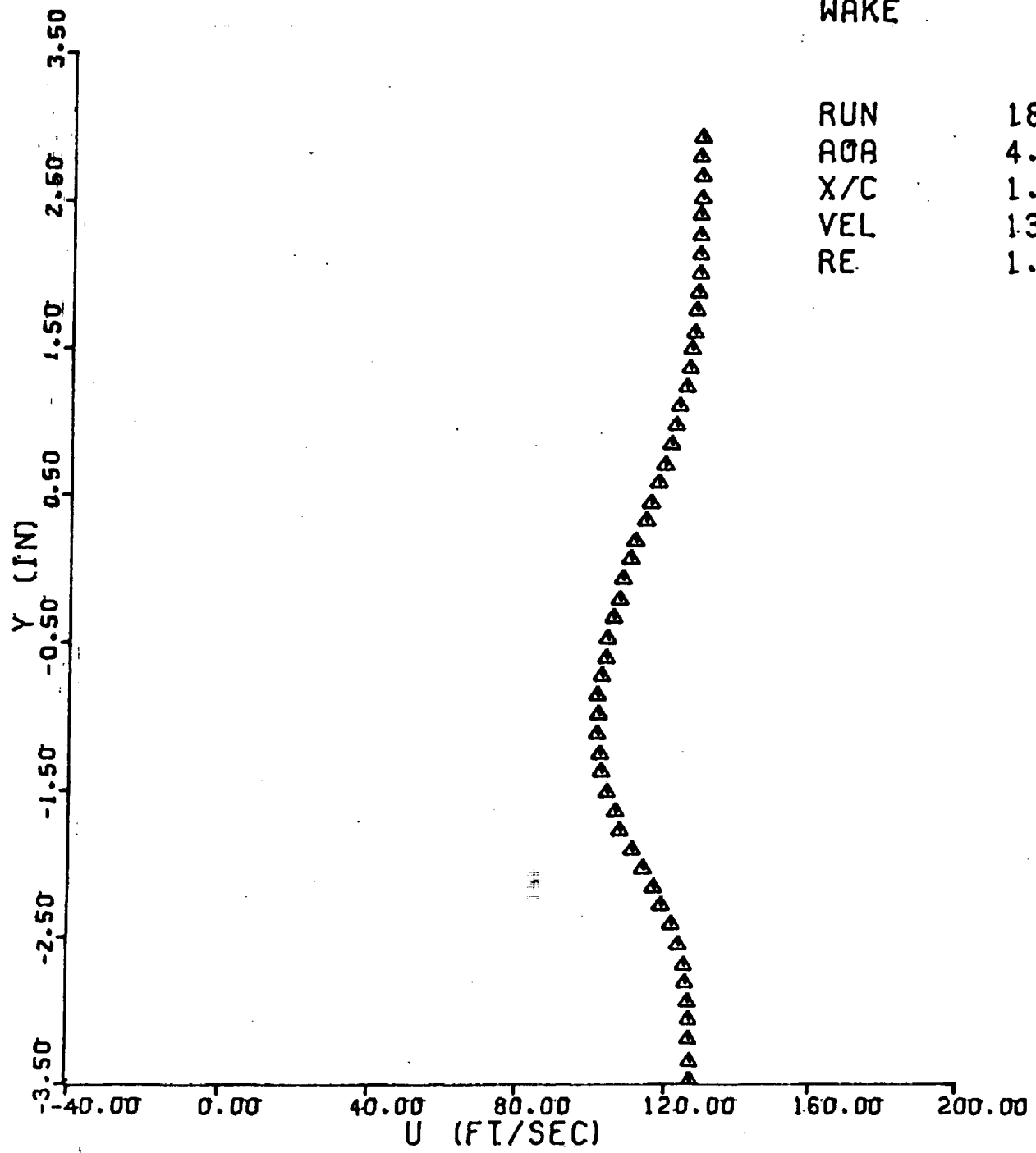
NACA 0012
WAKE



RUN	1852
AOA	2.000
X/C	1.8000
VEL	138.7
RE	1.57

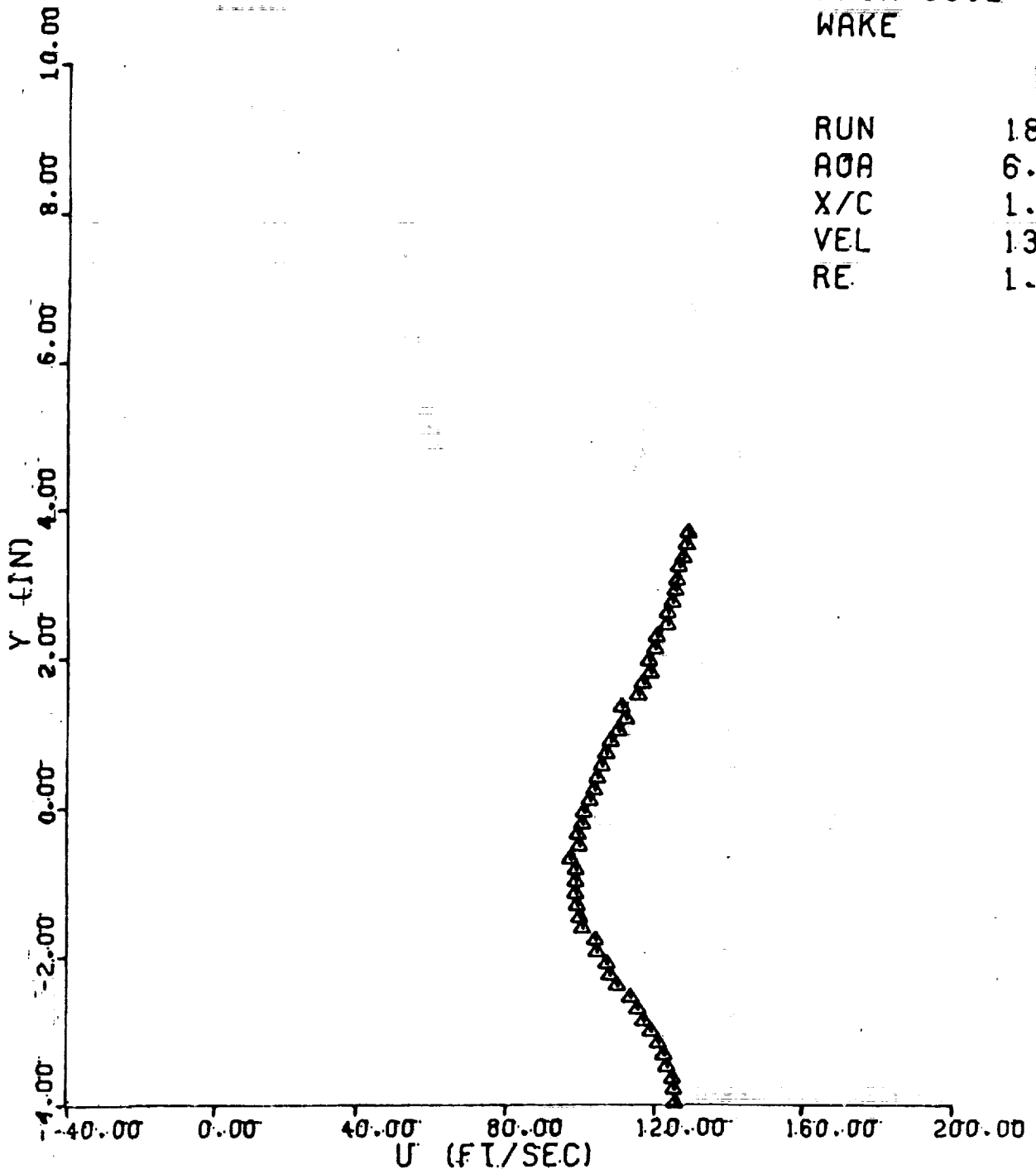
NACA 0012
WAKE

RUN	1856
AOA	4.000
X/C	1.8000
VEL	138.6
RE	1.61

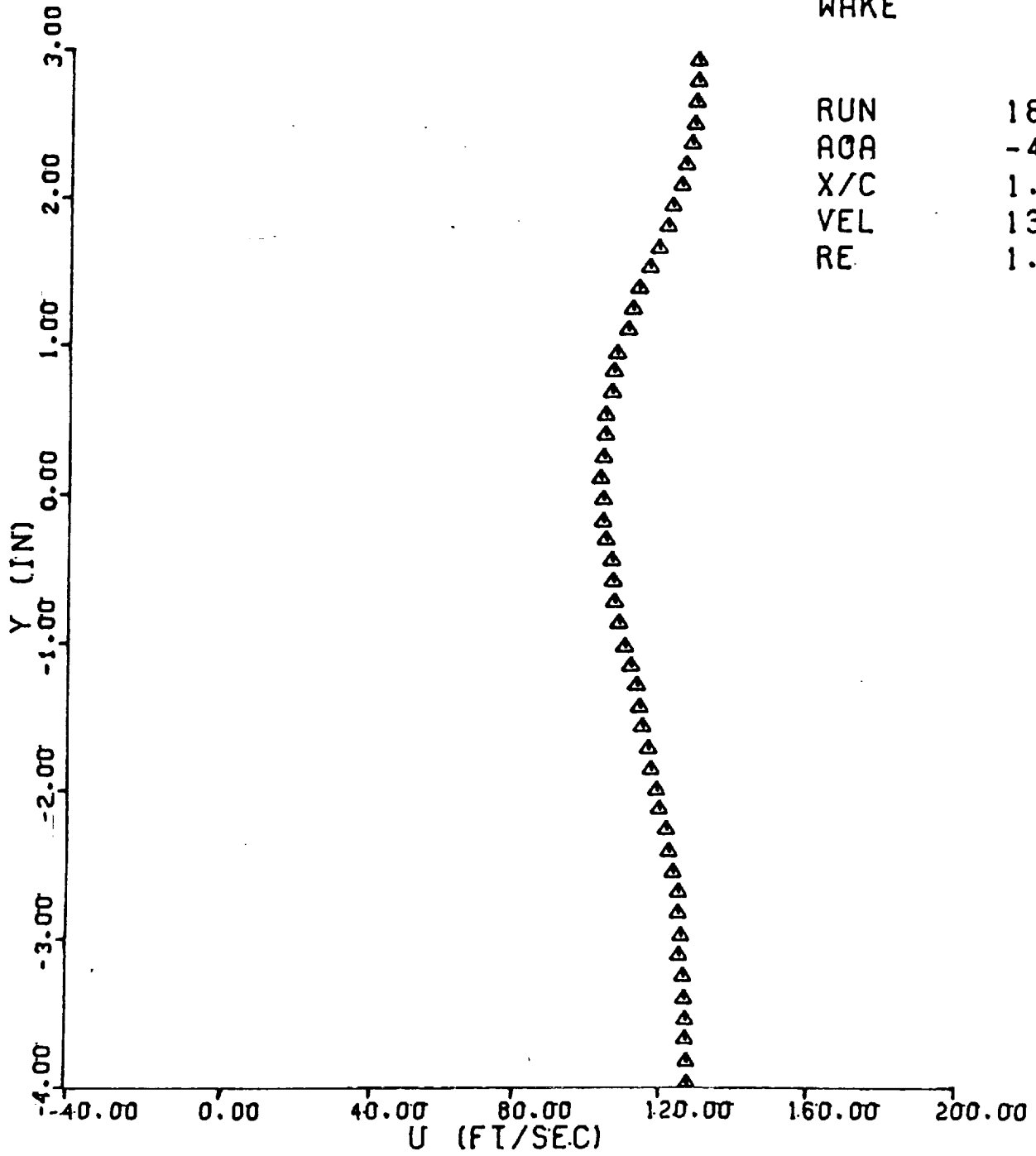


NACA 0012
WAKE

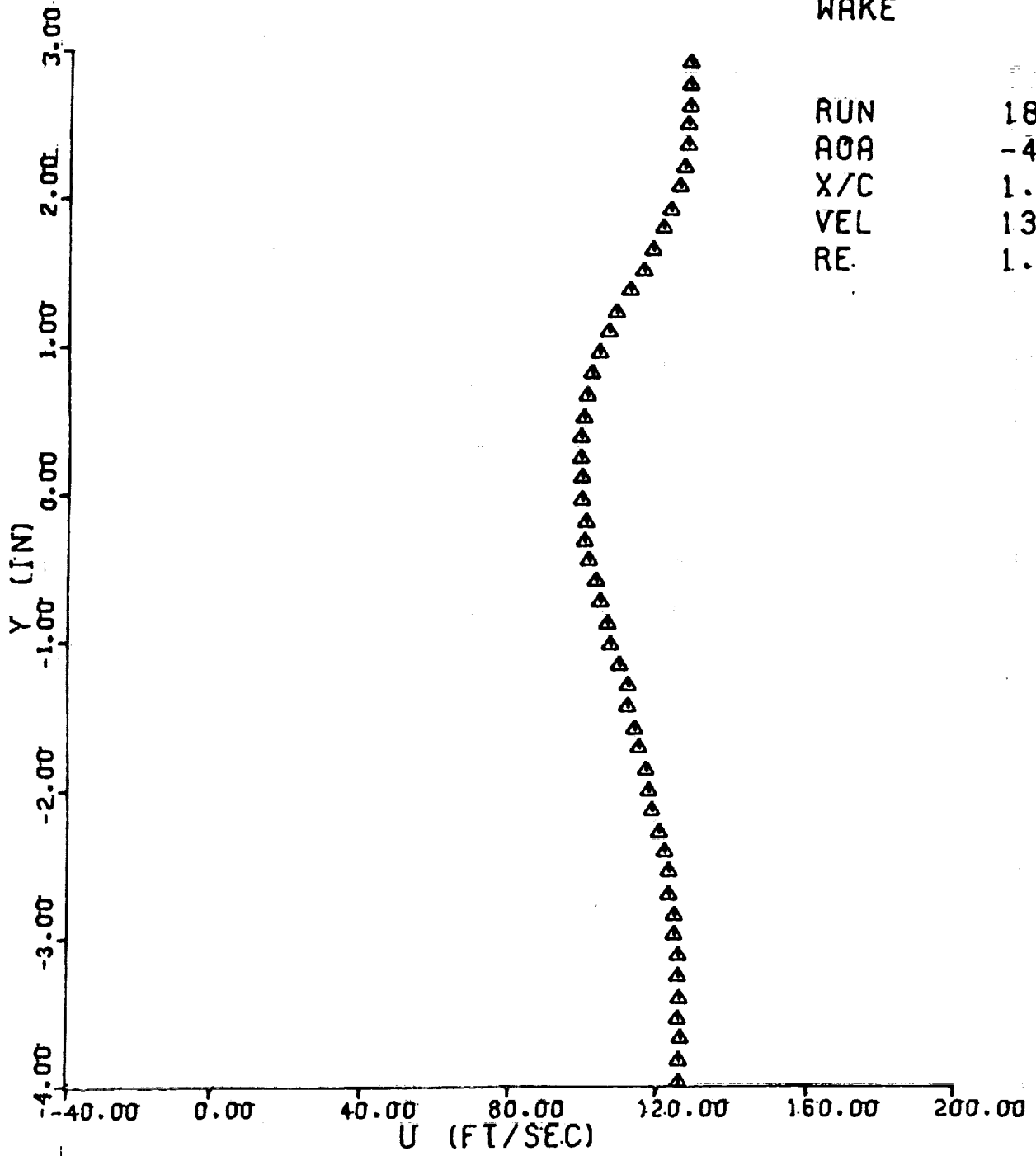
RUN	1858
AOA	6.000
X/C	1.8000
VEL	136.9
RE	1.59



NACA 0012
WAKE

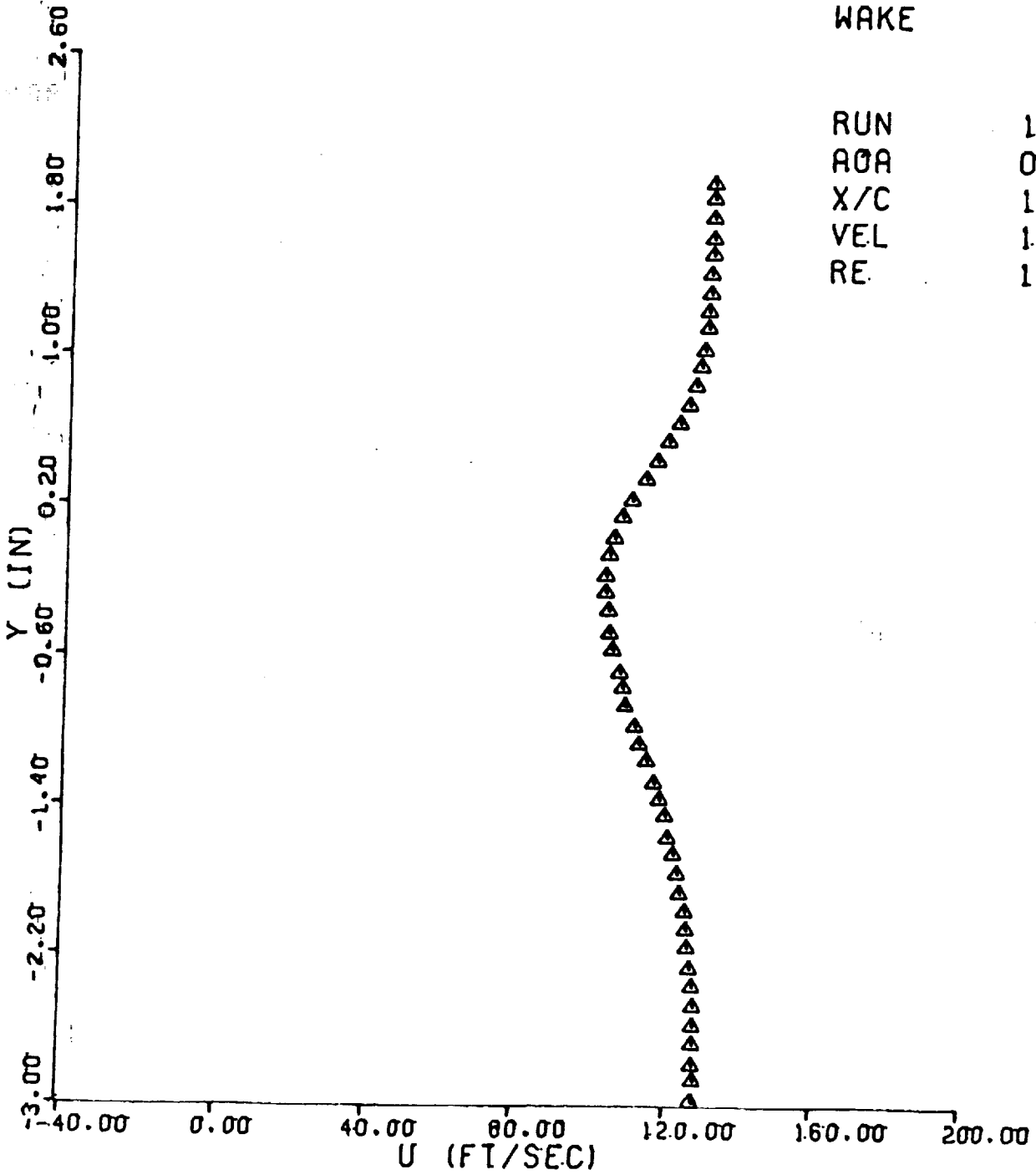


RUN	1859
AOA	-4.000
X/C	1.8000
VEL	138.2
RE	1.61



NACA 0012
WAKE

RUN	1860
AOA	-4.000
X/C	1.6000
VEL	139.3
RE	1.62

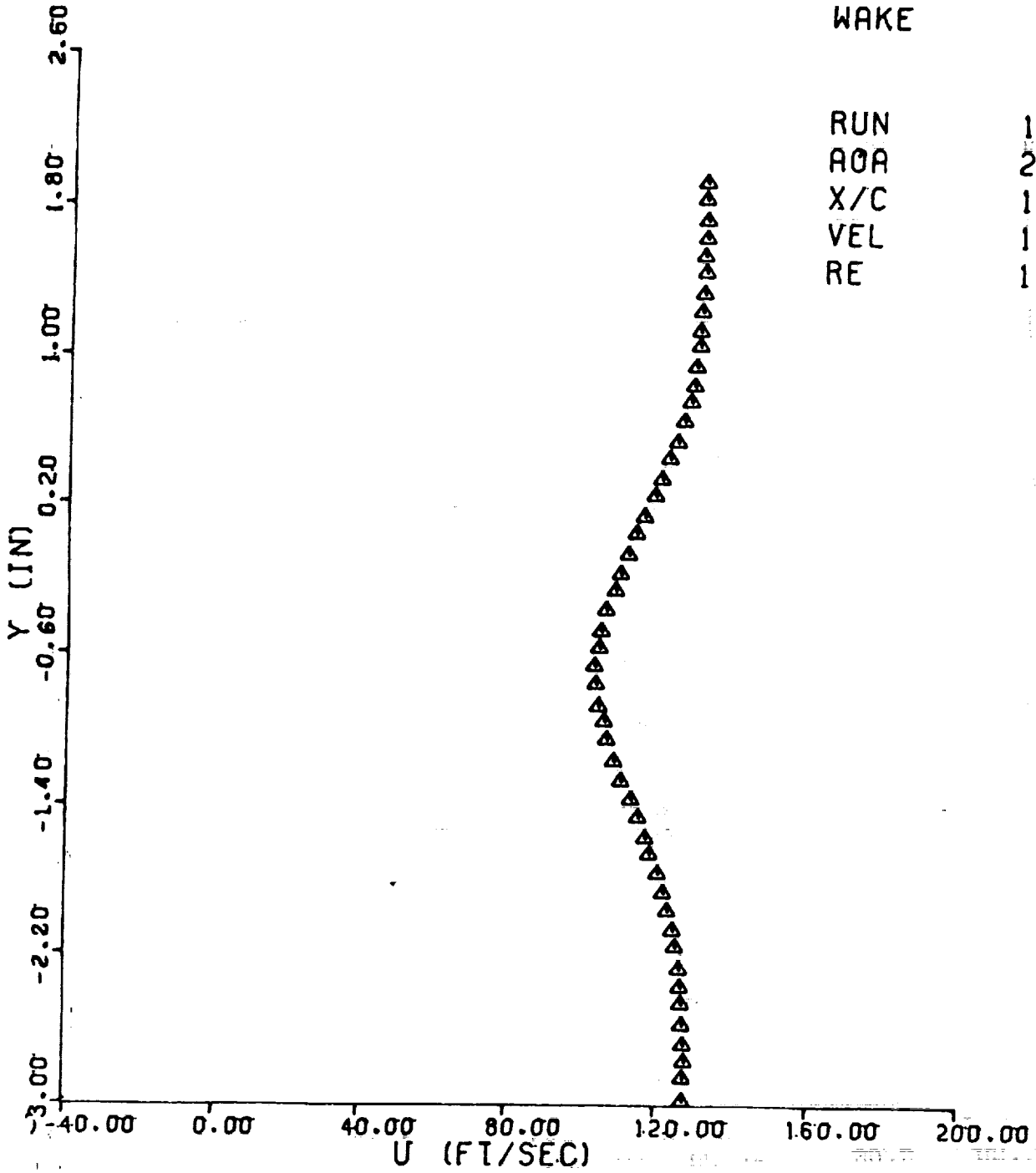


NACA 0012
WAKE

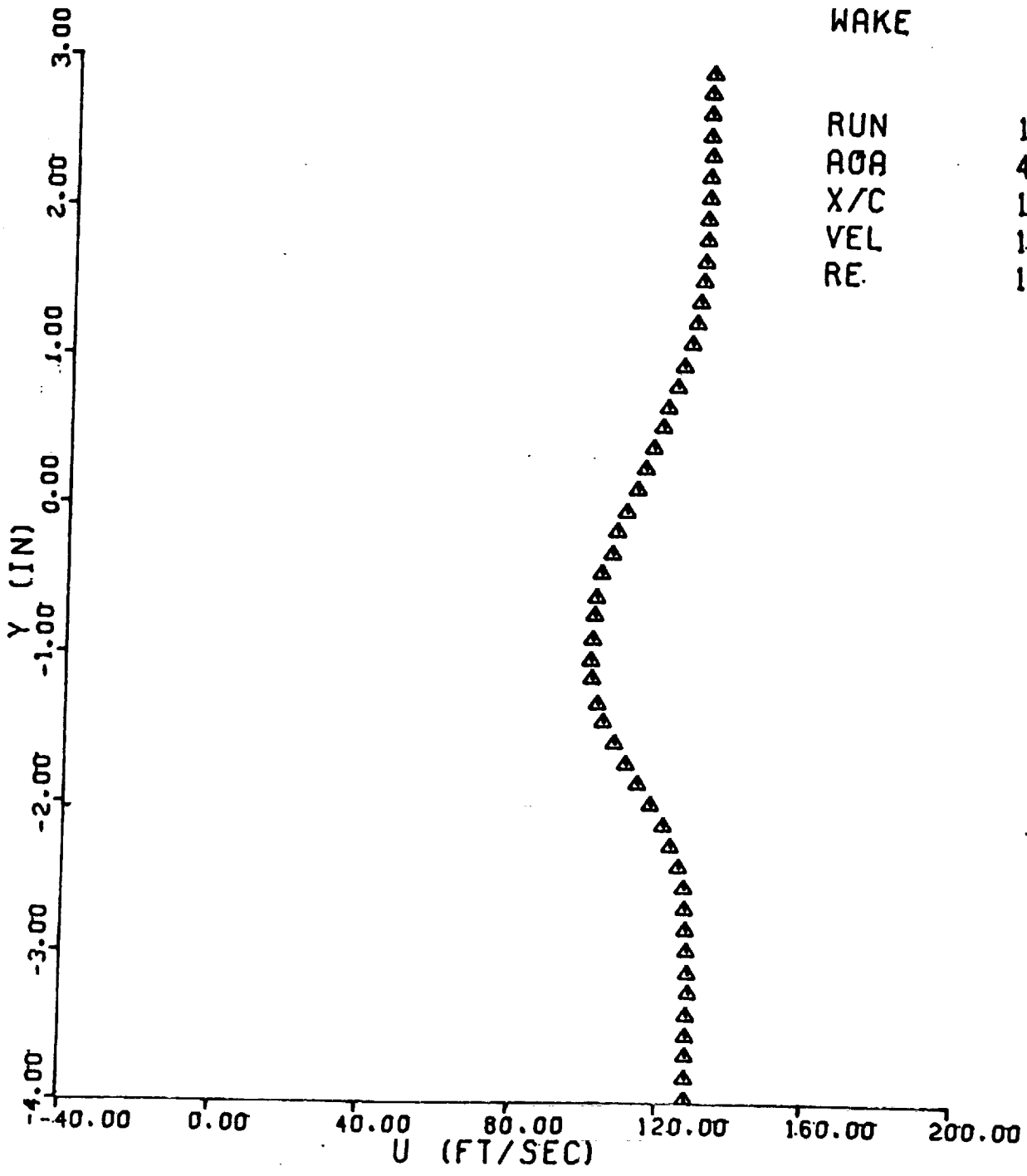
RUN	1862
AOA	0.000
X/C	1.6000
VEL	139.5
RE	1.62

NACA 0012
WAKE

RUN	1863
AOA	2.000
X/C	1.6000
VEL	139.3
RE	1.62



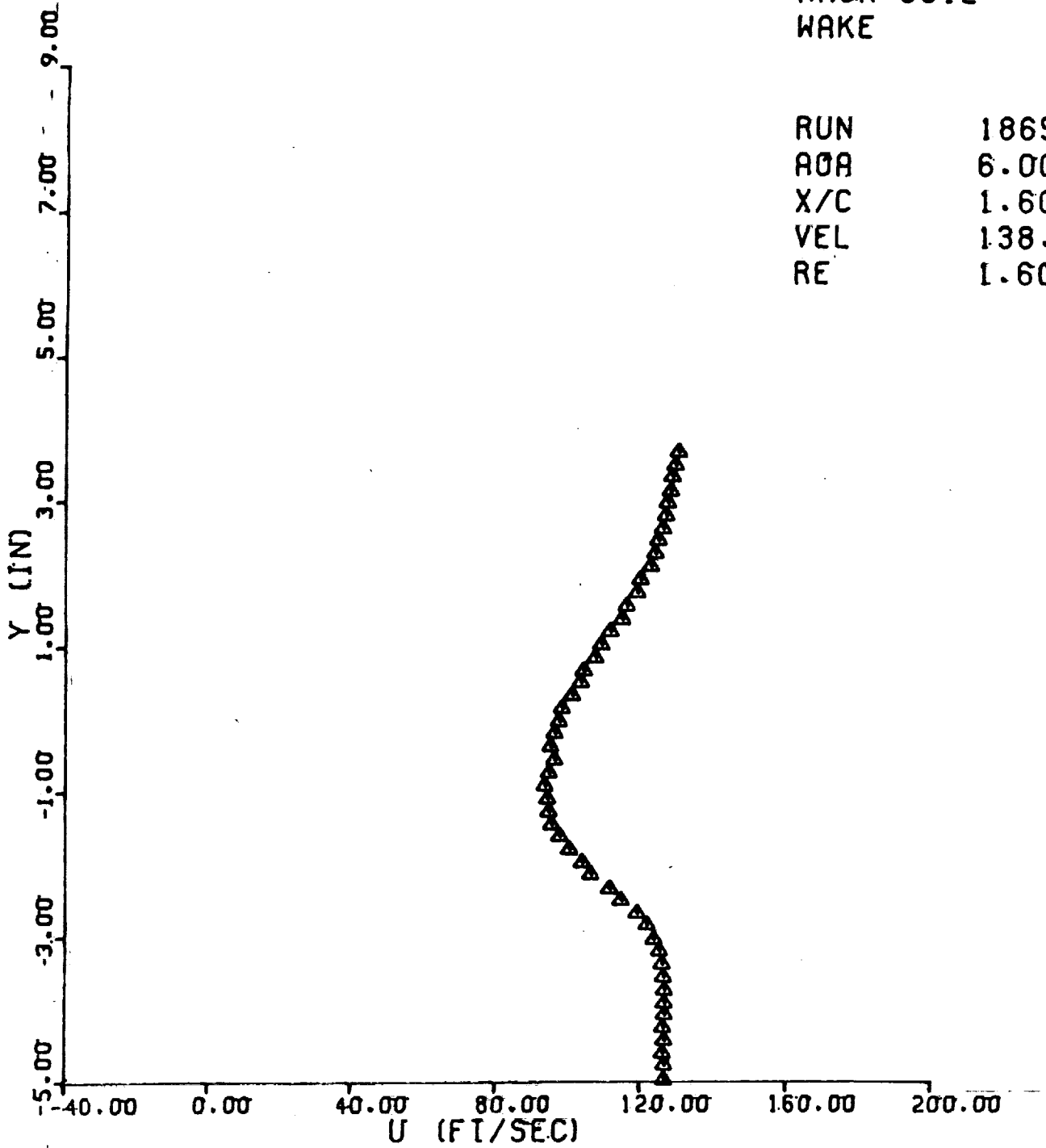
NACA 0012
WAKE



RUN	1864
AOA	4.000
X/C	1.6000
VEL	139.6
RE.	1.62

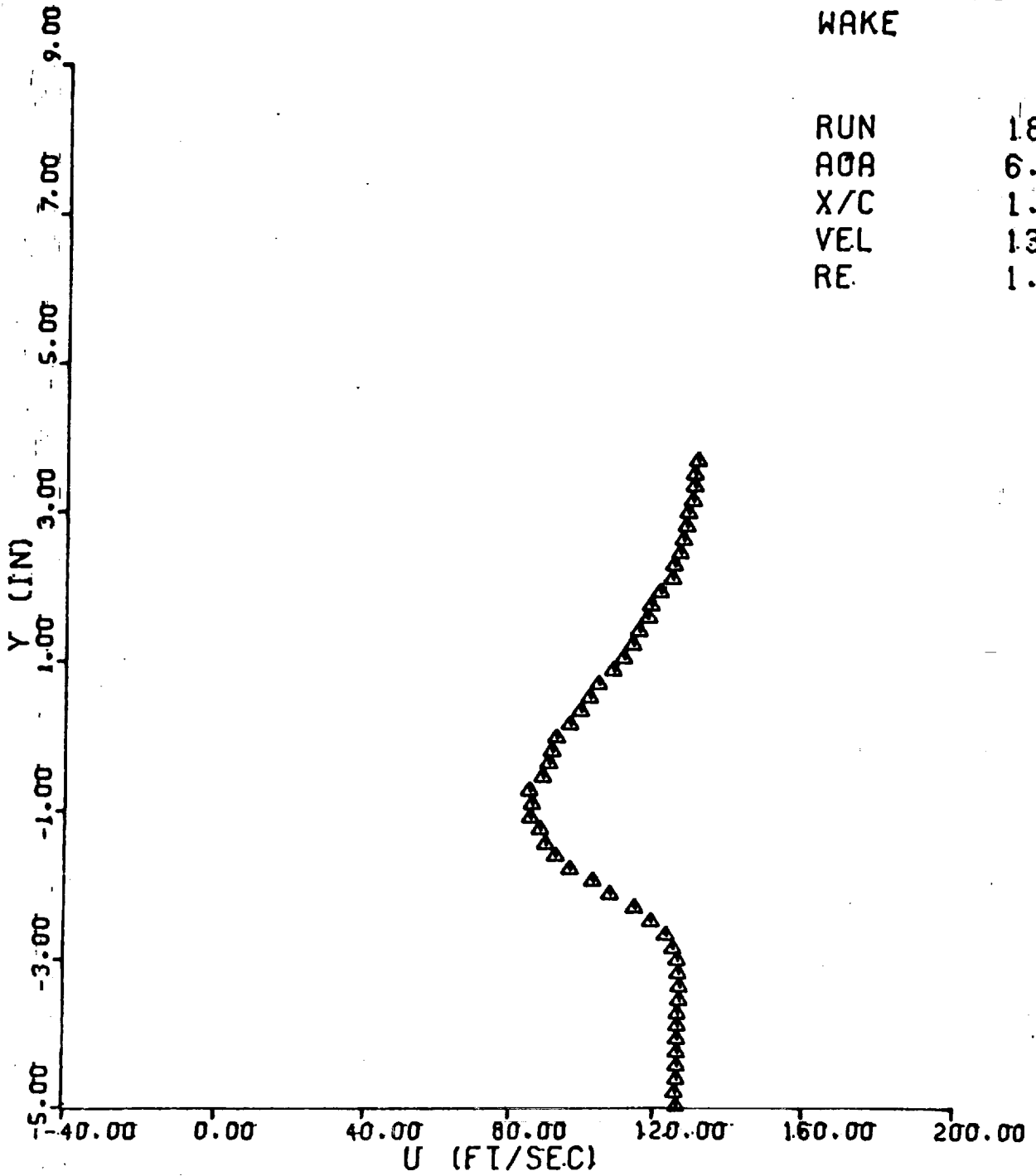
NACA 0012
WAKE

RUN	1865
AOA	6.000
X/C	1.6000
VEL	138.0
RE	1.60

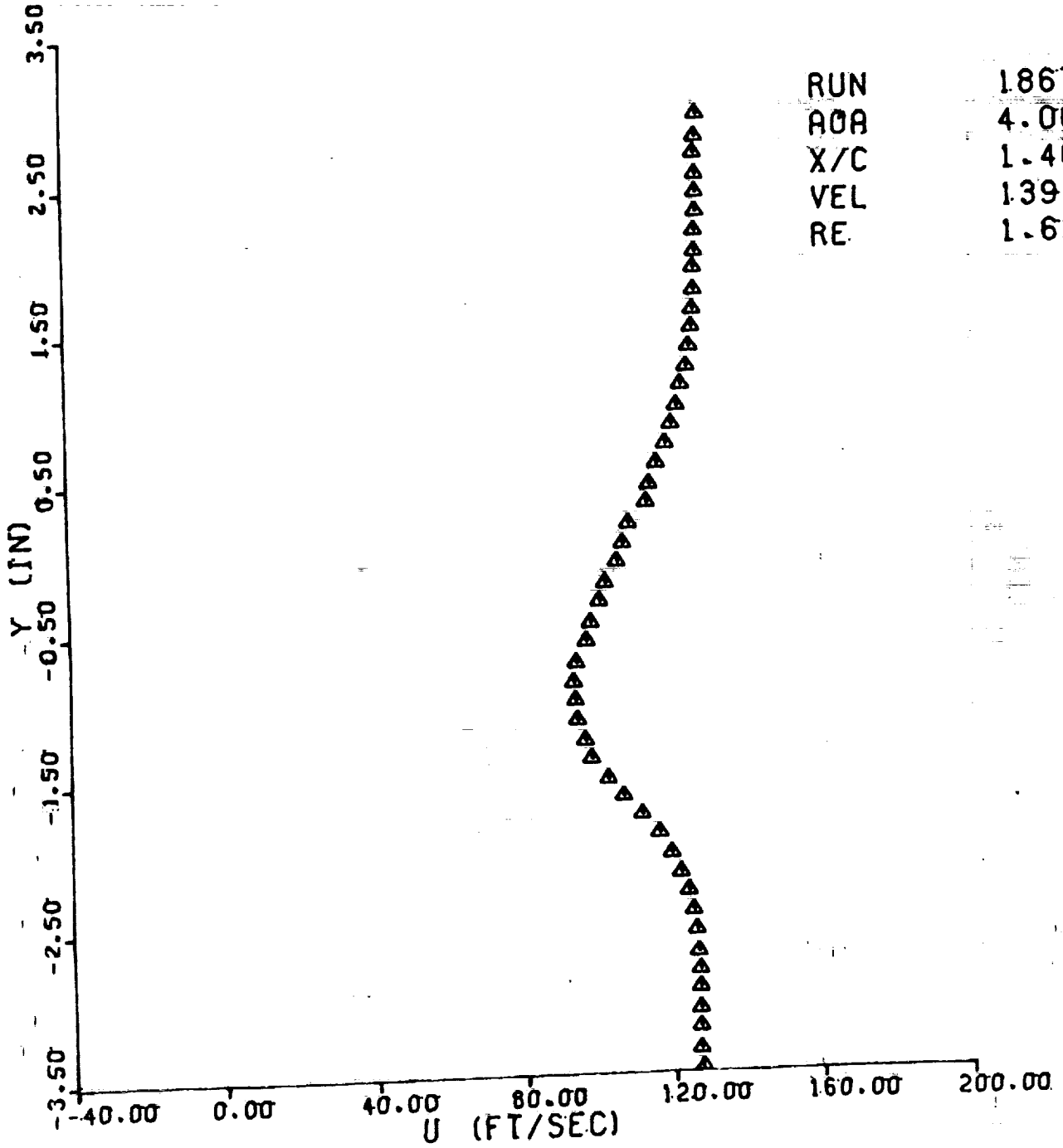


NACA 0012
WAKE

RUN	1866
AOA	6.000
X/C	1.4000
VEL	137.6
RE.	1.60



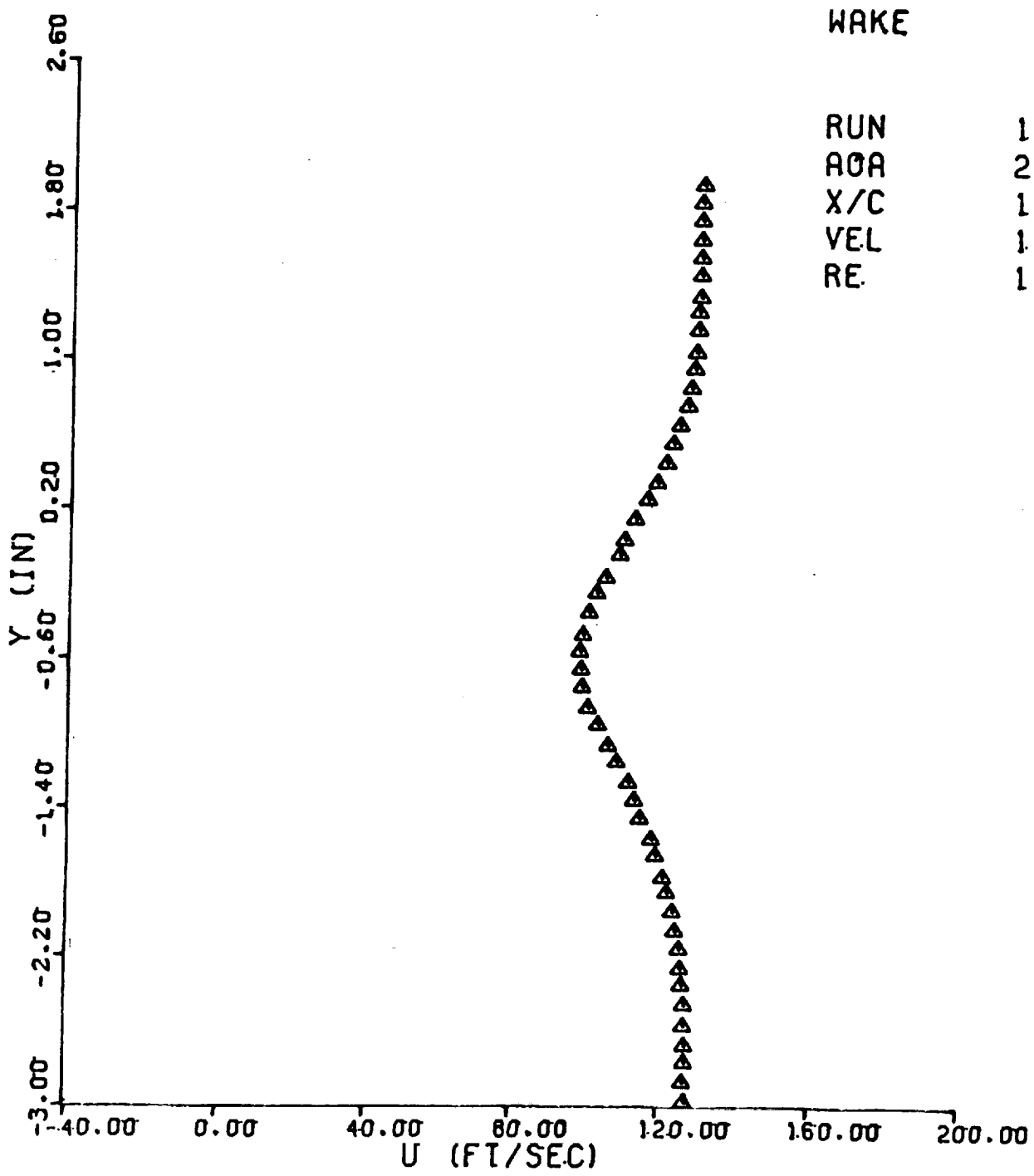
NACA 0012
WAKE



RUN	1867
AOA	4.000
X/C	1.4000
VEL	139.2
RE	1.62

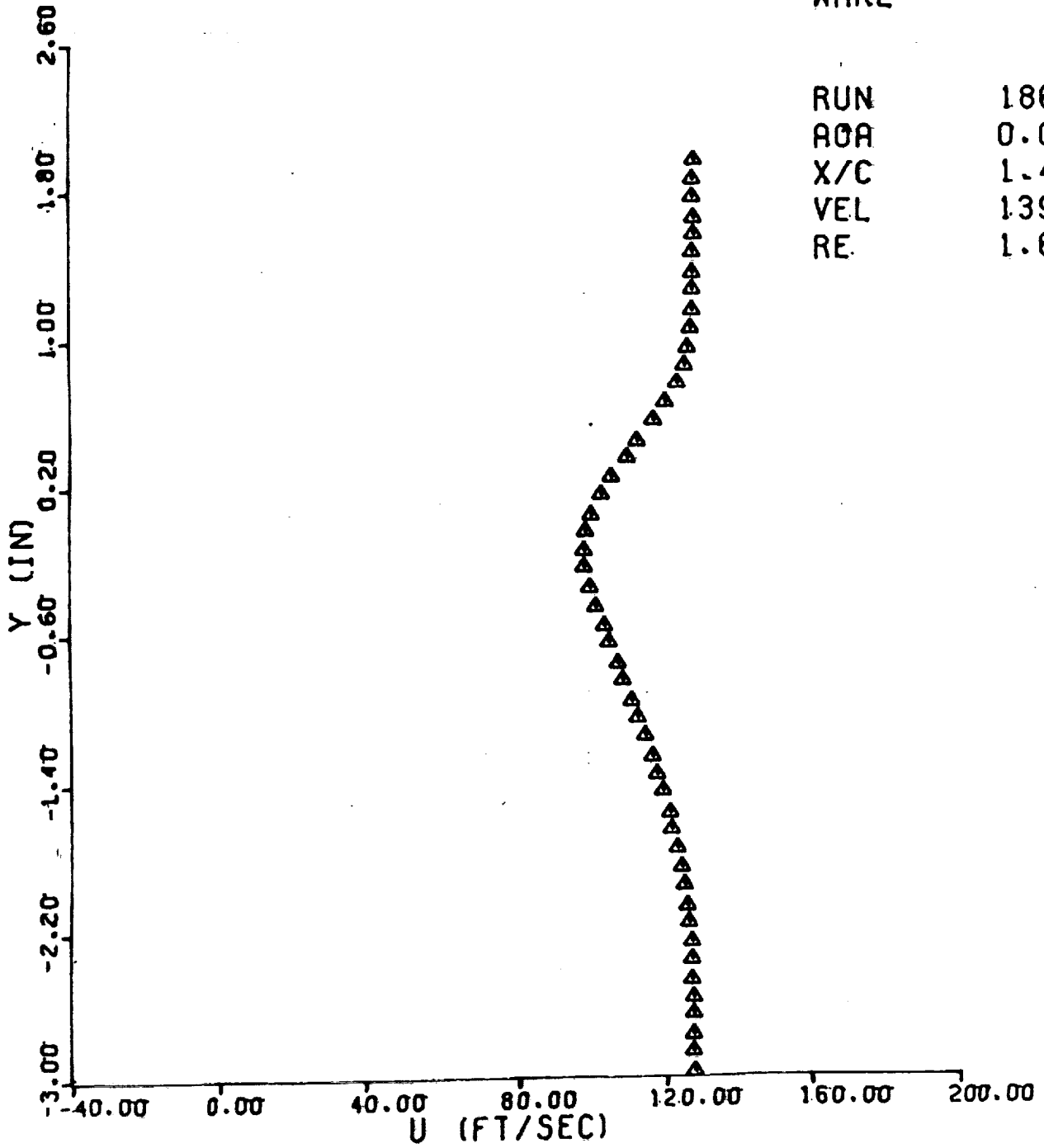
NACA 0012
WAKE

RUN	1868
AOA	2.000
X/C	1.4000
VEL	139.9
RE	1.63

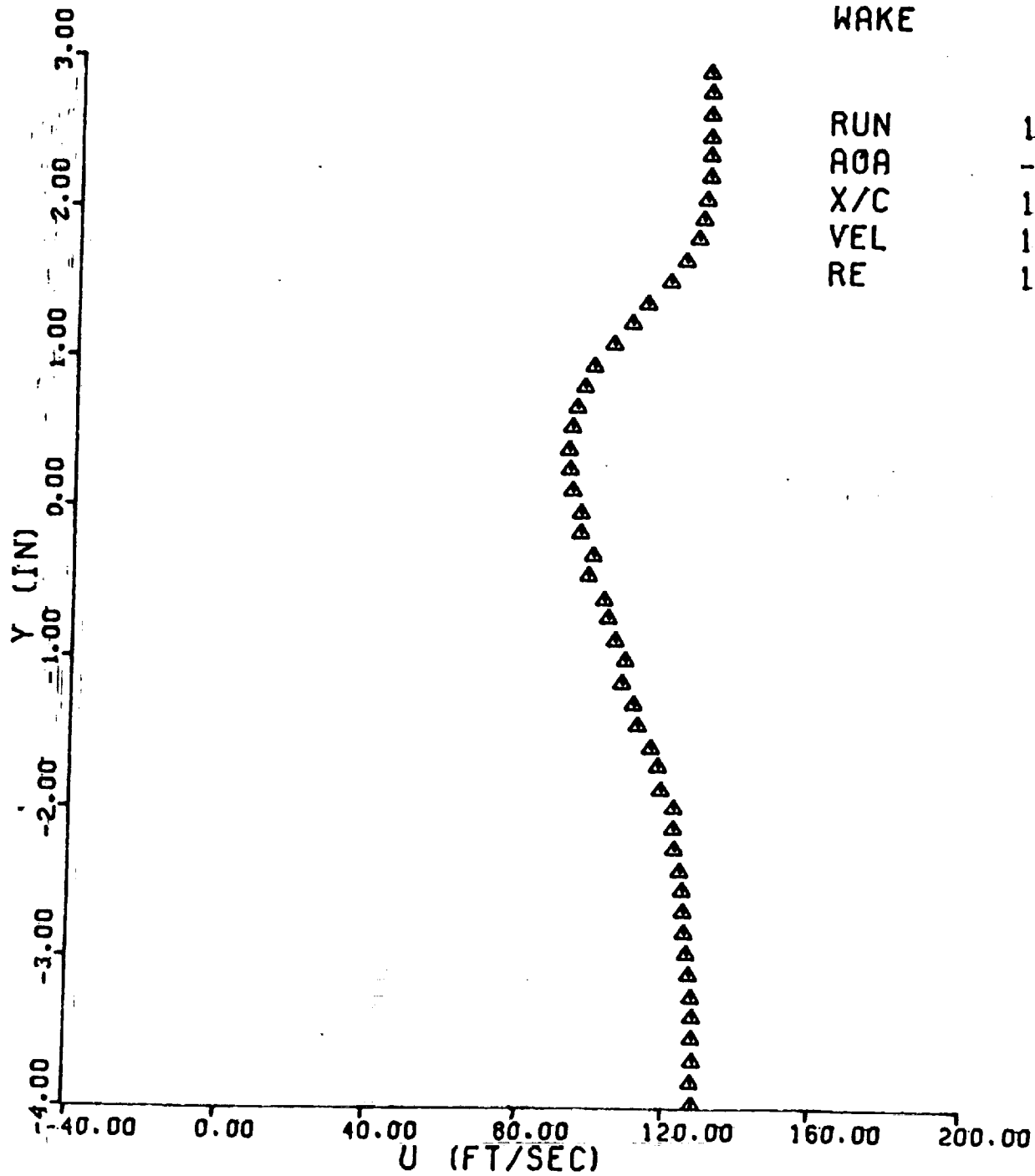


NACA 0012
WAKE

RUN	1869
AOA	0.000
X/C	1.4000
VEL	139.5
RE	1.62



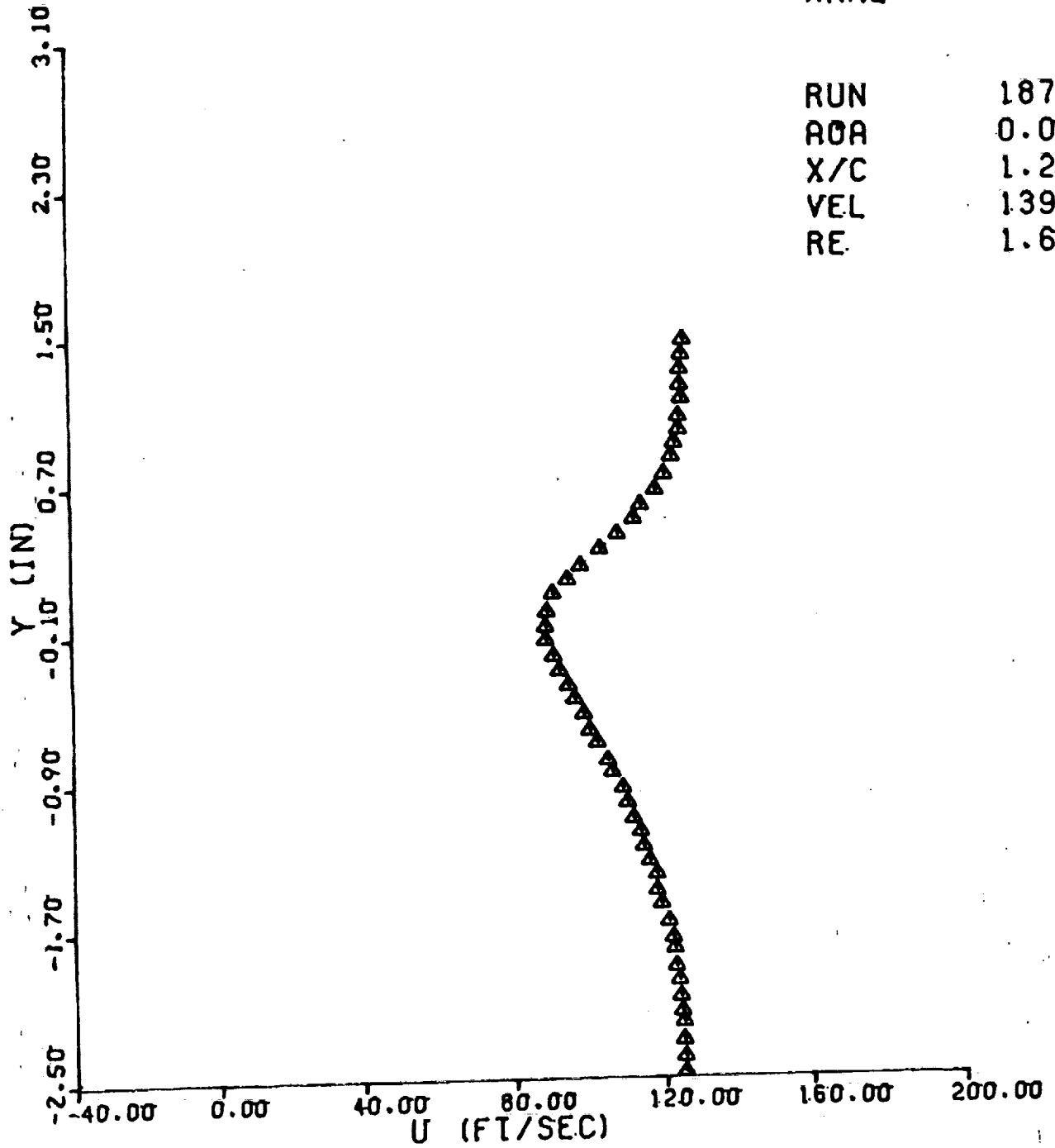
NACA 0012
WAKE



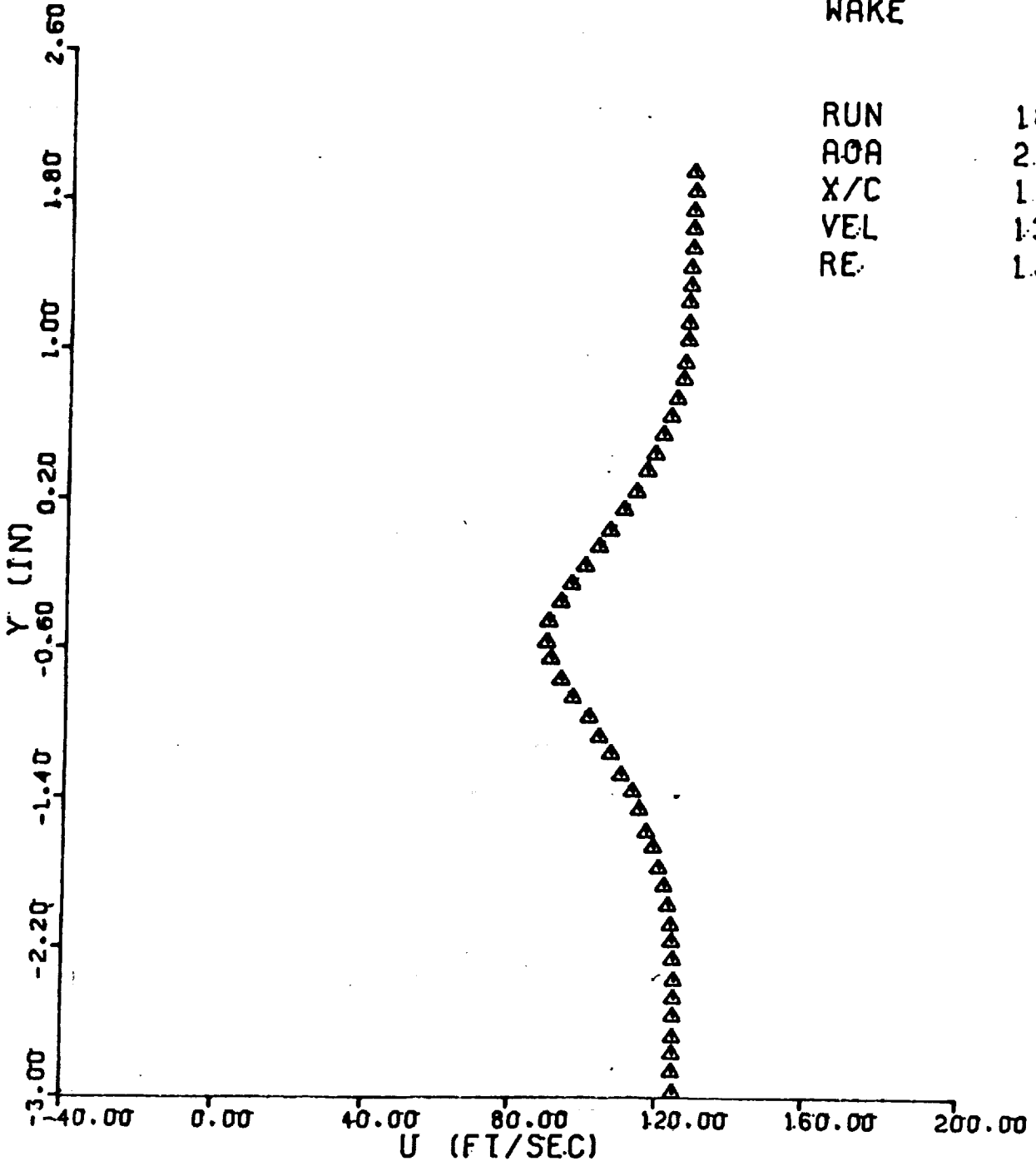
RUN	1870
AOA	-4.000
X/C	1.4000
VEL	139.0
RE	1.62

NACA 0012
WAKE

RUN	1872
AOA	0.000
X/C	1.2000
VEL	139.5
RE	1.62



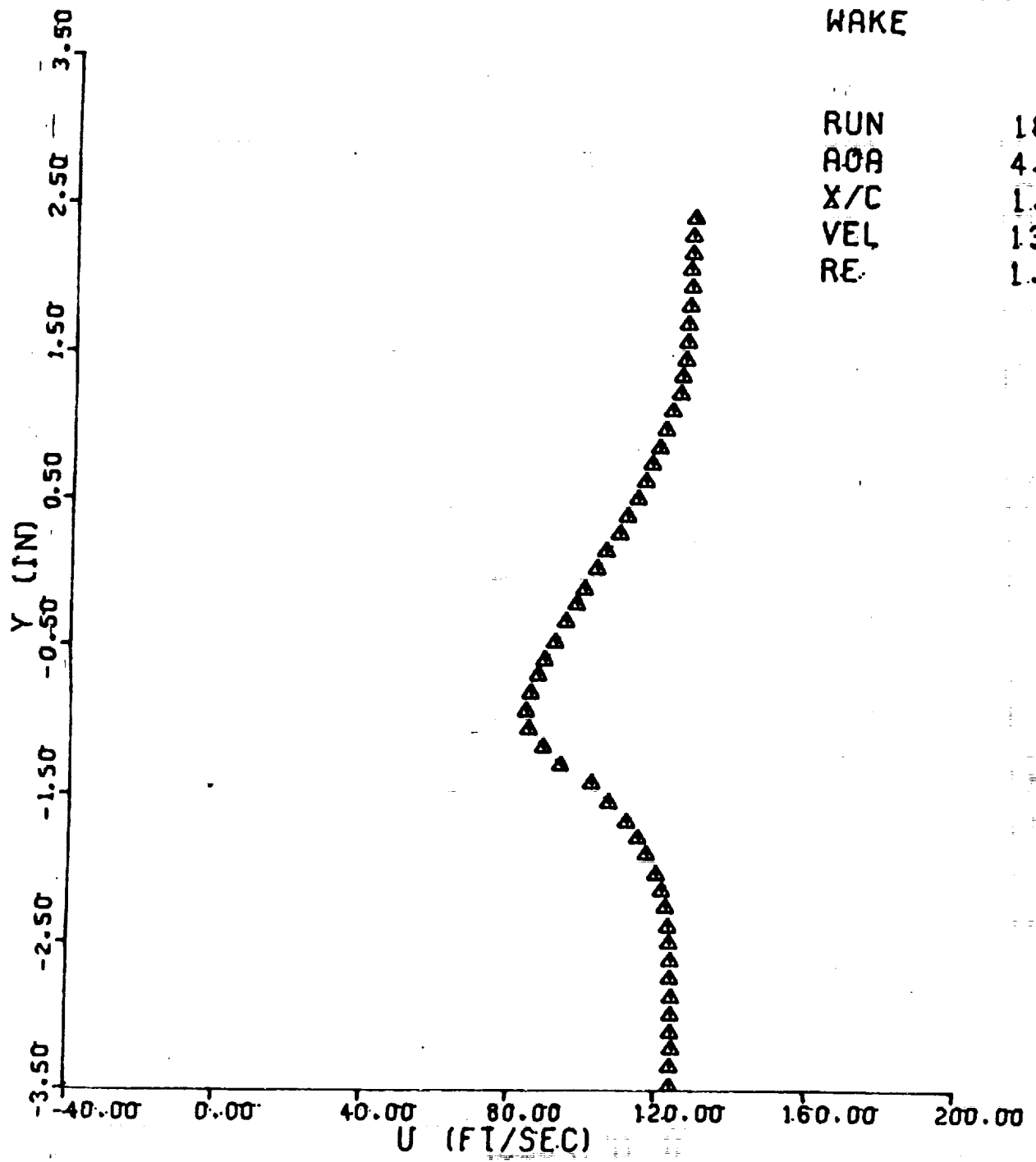
NACA 0012
WAKE



RUN	1873
AOA	2.000
X/C	1.2000
VEL	139.7
RE	1.62

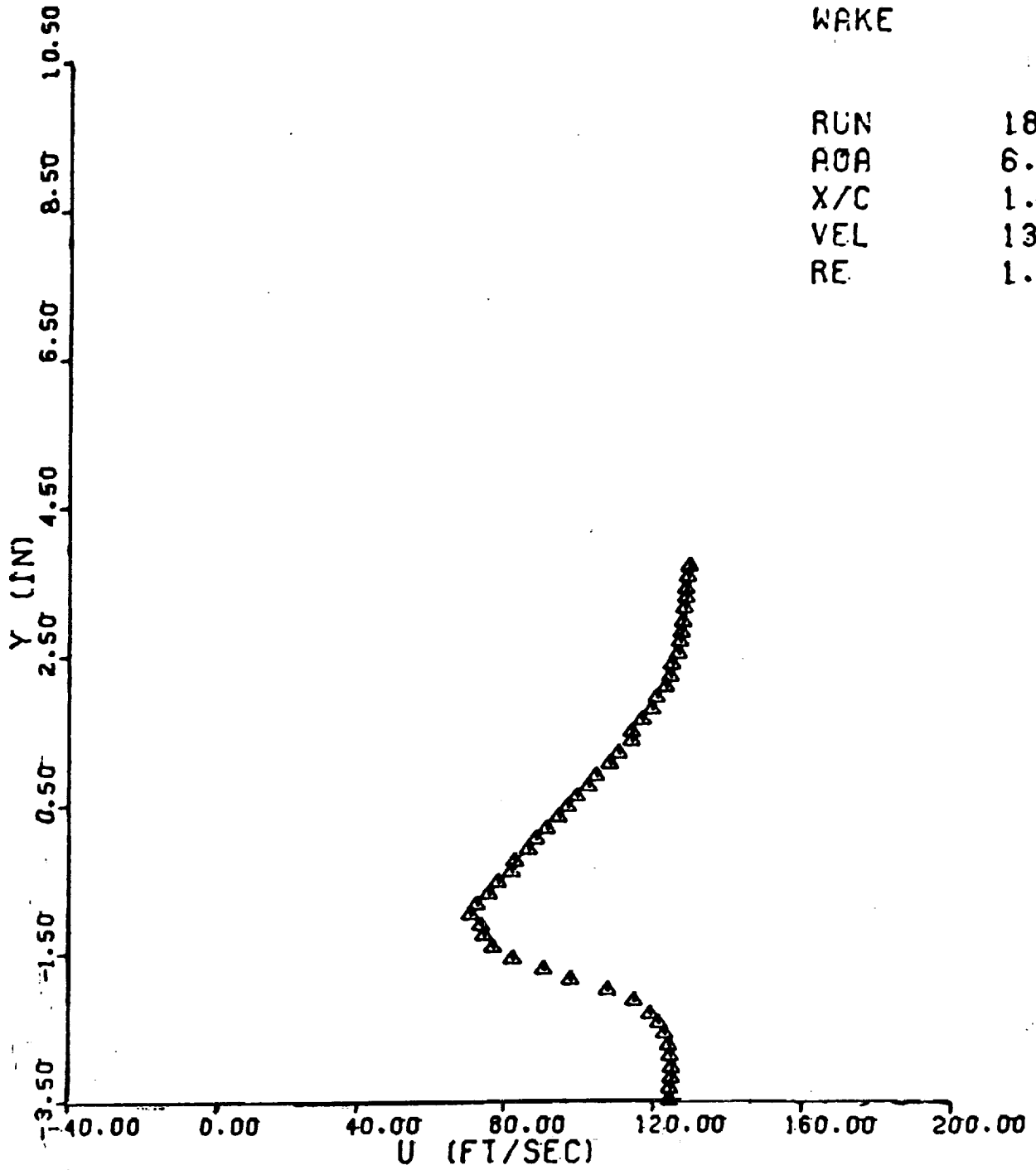
NACA 0012
WAKE

RUN 1874
AOA 4.000
X/C 1.2000
VEL 139.2
RE 1.62



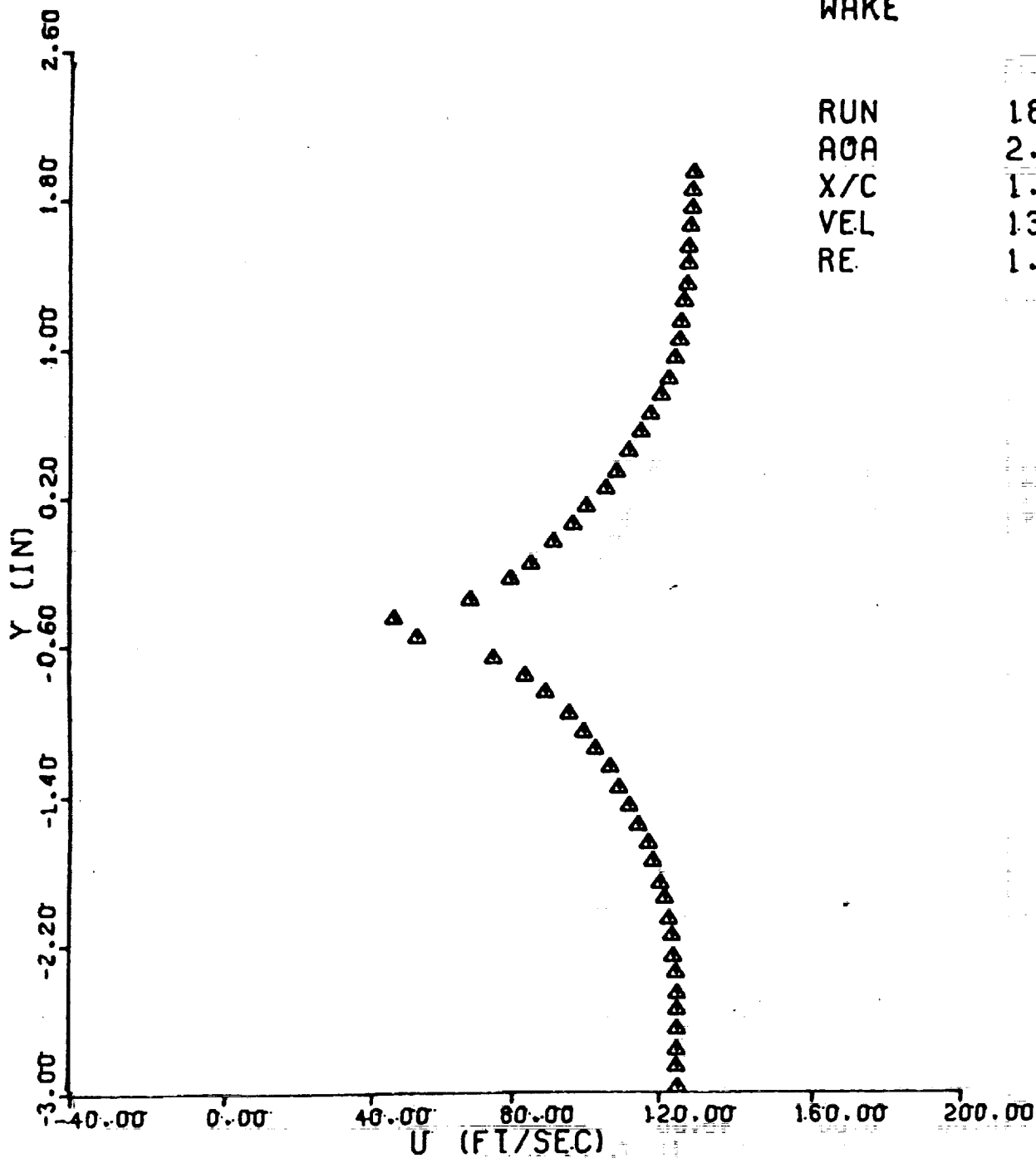
NACA 0012
WAKE

RUN	1876
AOA	6.000
X/C	1.2000
VEL	137.8
RE	1.60



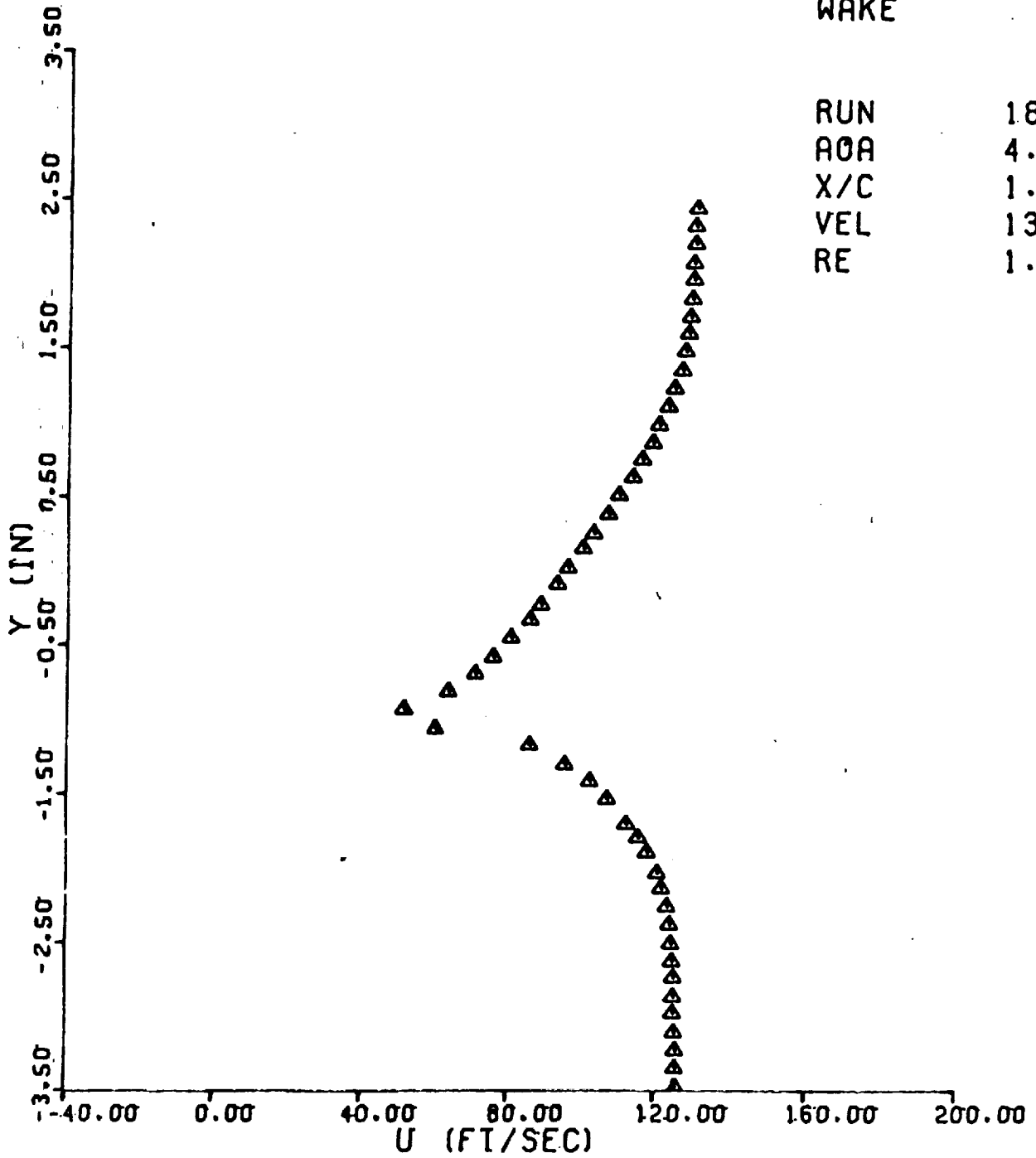
NACA 0012
WAKE

RUN	1879
AOA	2.000
X/C	1.0000
VEL	139.5
RE	1.62



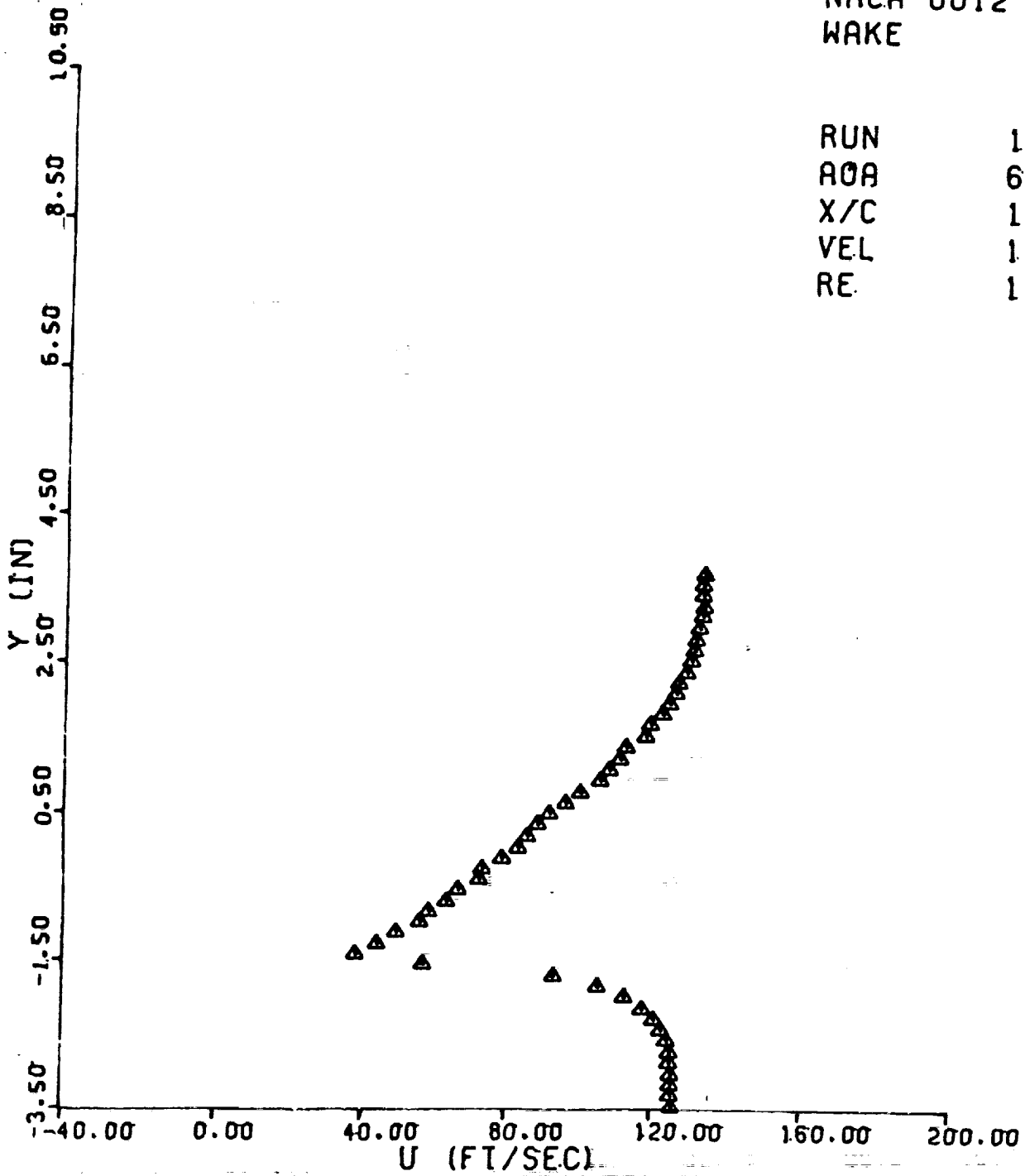
NACA 0012
WAKE

RUN 1880
AOA 4.000
X/C 1.0000
VEL 139.2
RE 1.62



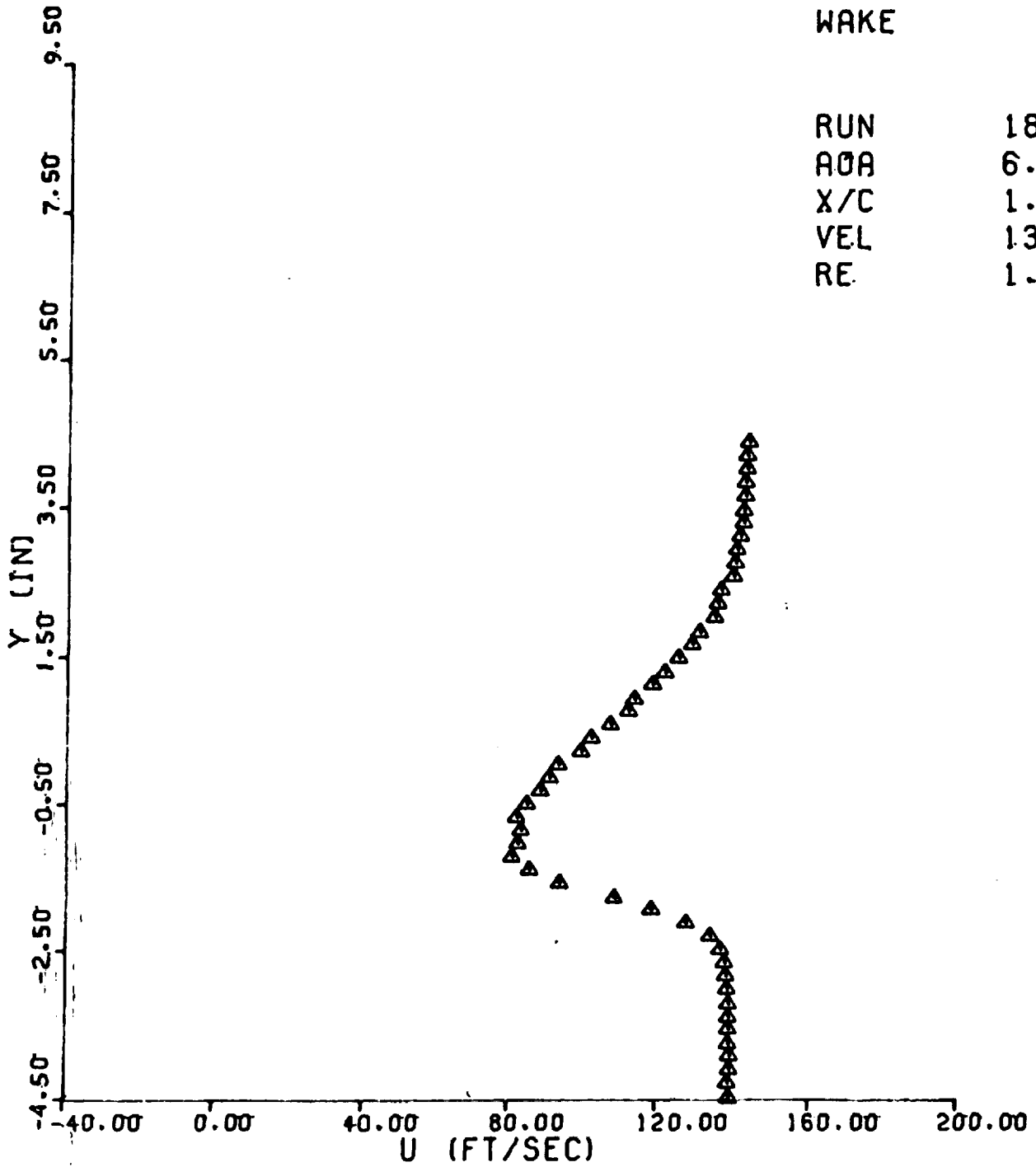
NACA 0012
WAKE

RUN	1881
AOA	6.000
X/C	1.0000
VEL	138.0
RE	1.60



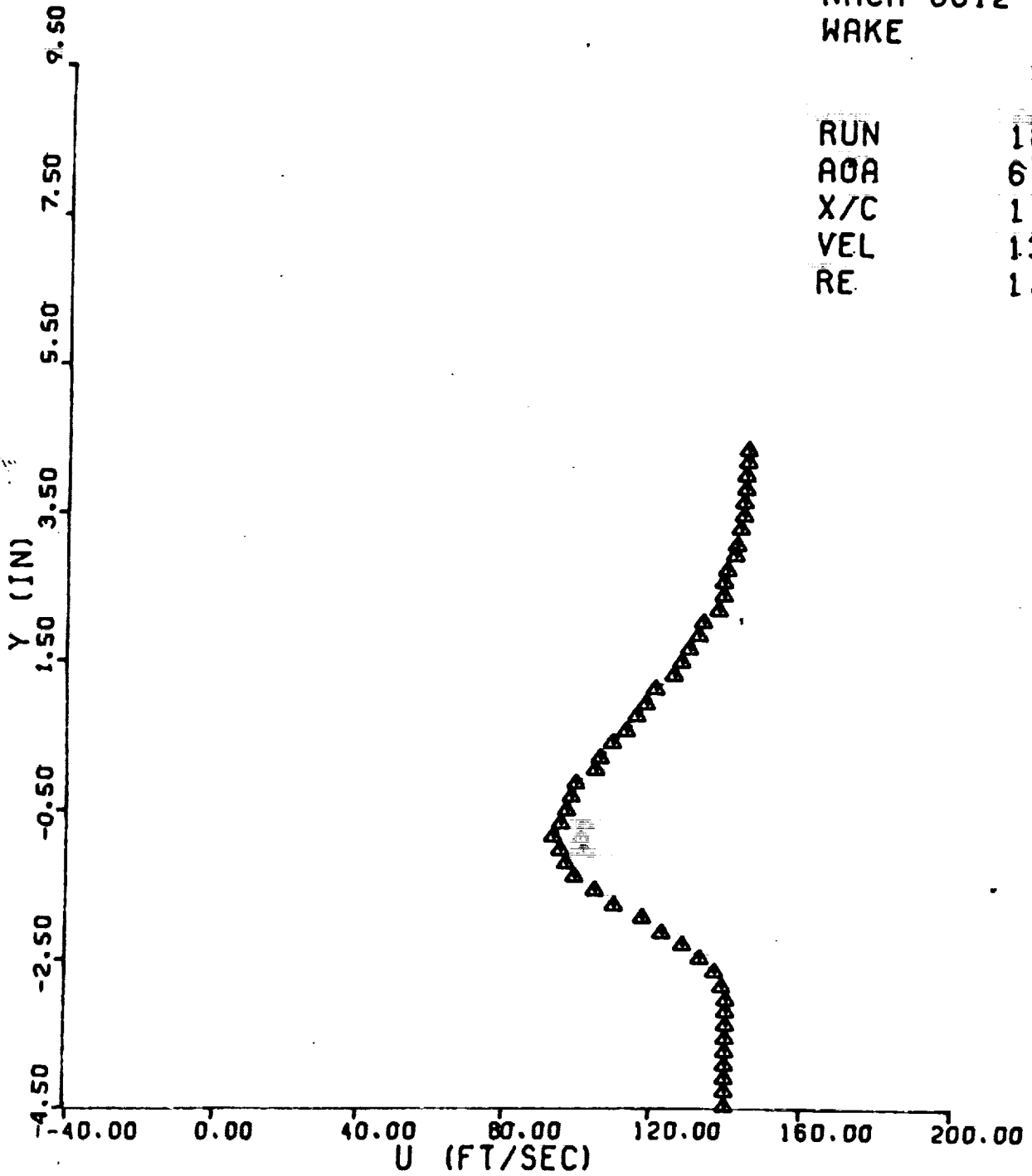
NACA 0012
WAKE

RUN	1885
AOA	6.000
X/C	1.2000
VEL	138.3
RE	1.55



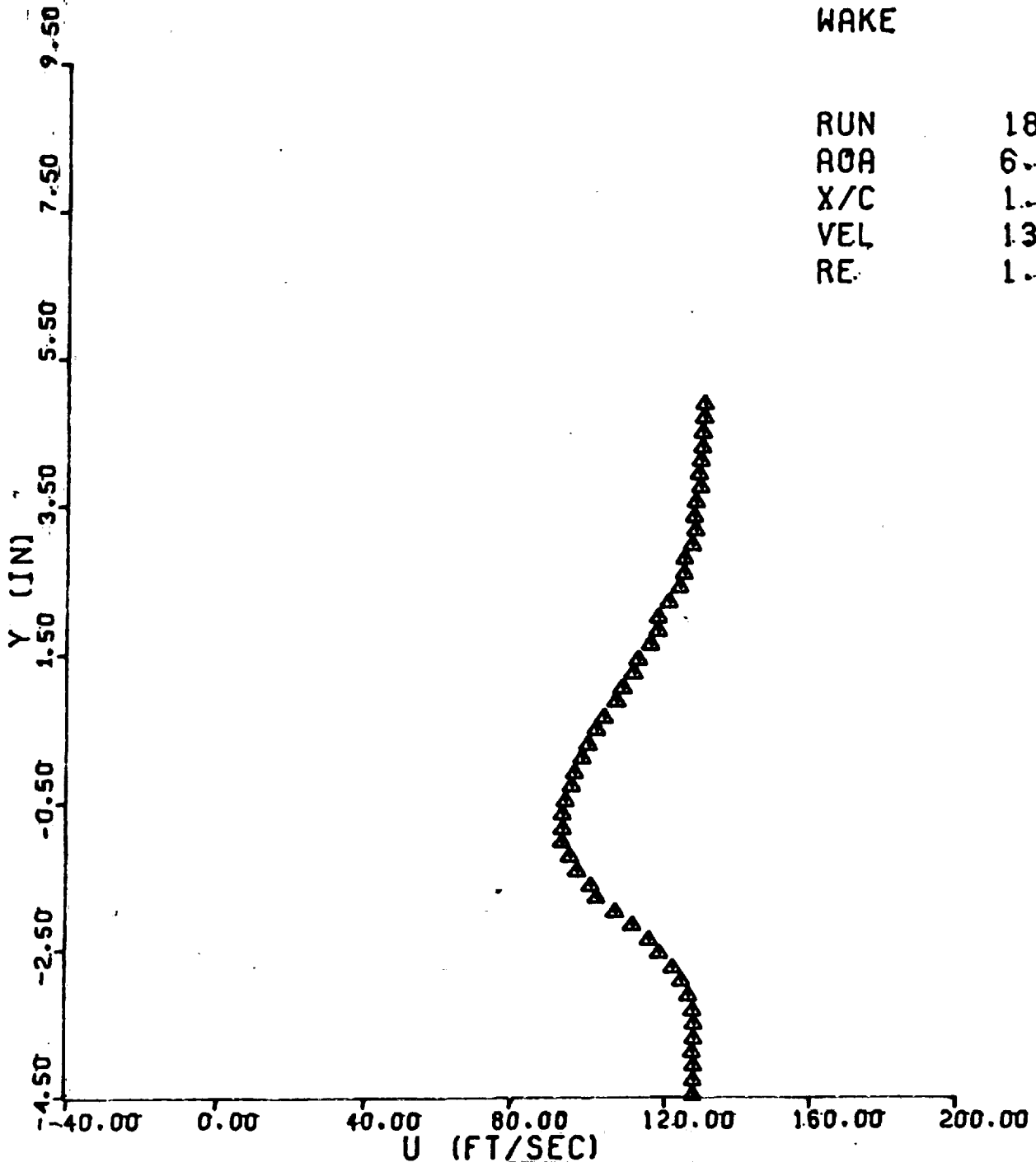
NACA 0012
WAKE

RUN	1886
AOA	6.000
X/C	1.4000
VEL	137.8
RE	1.54



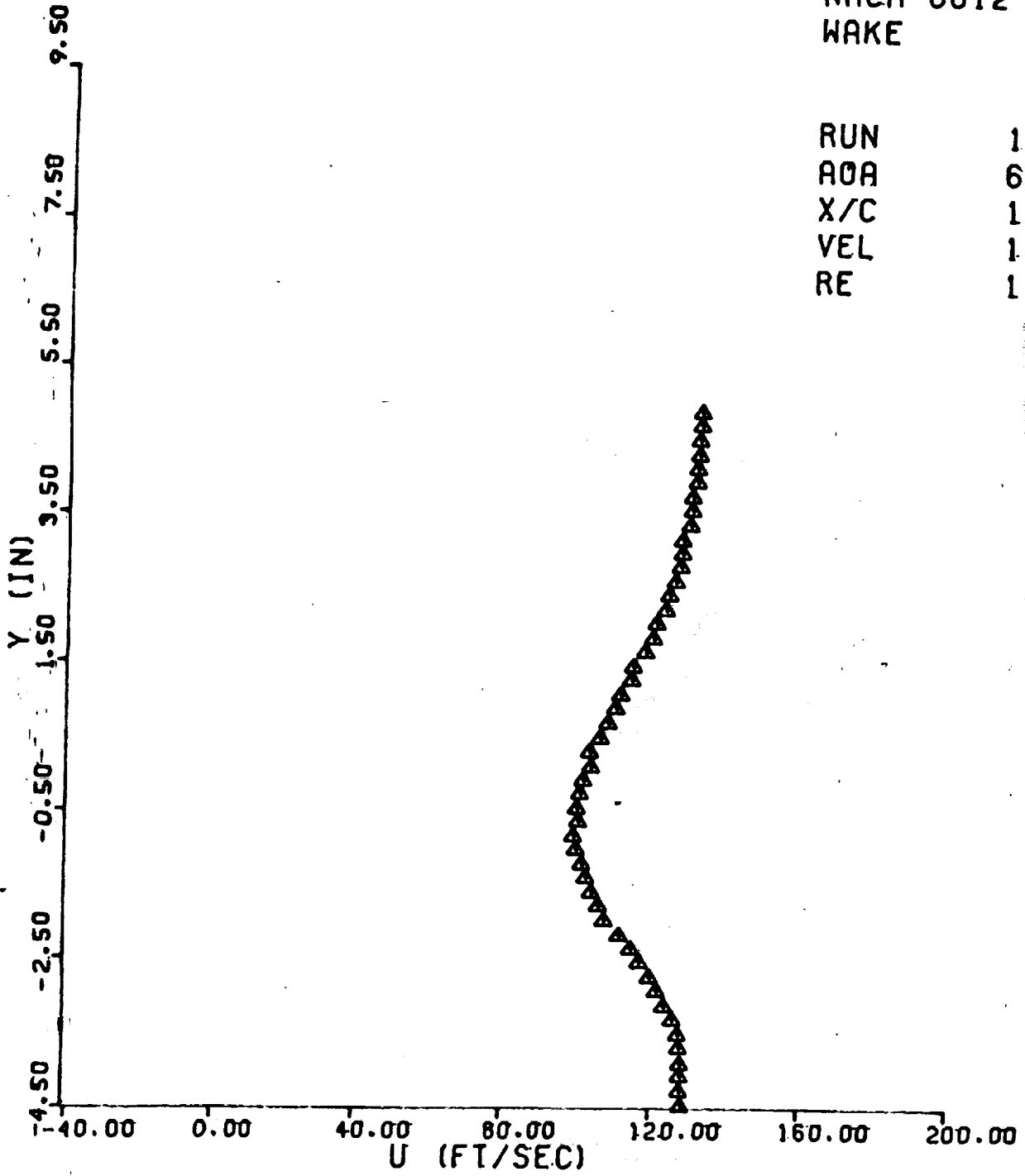
NACA 0012
WAKE

RUN	1887
AOA	6.000
X/C	1.6000
VEL	138.0
RE	1.60



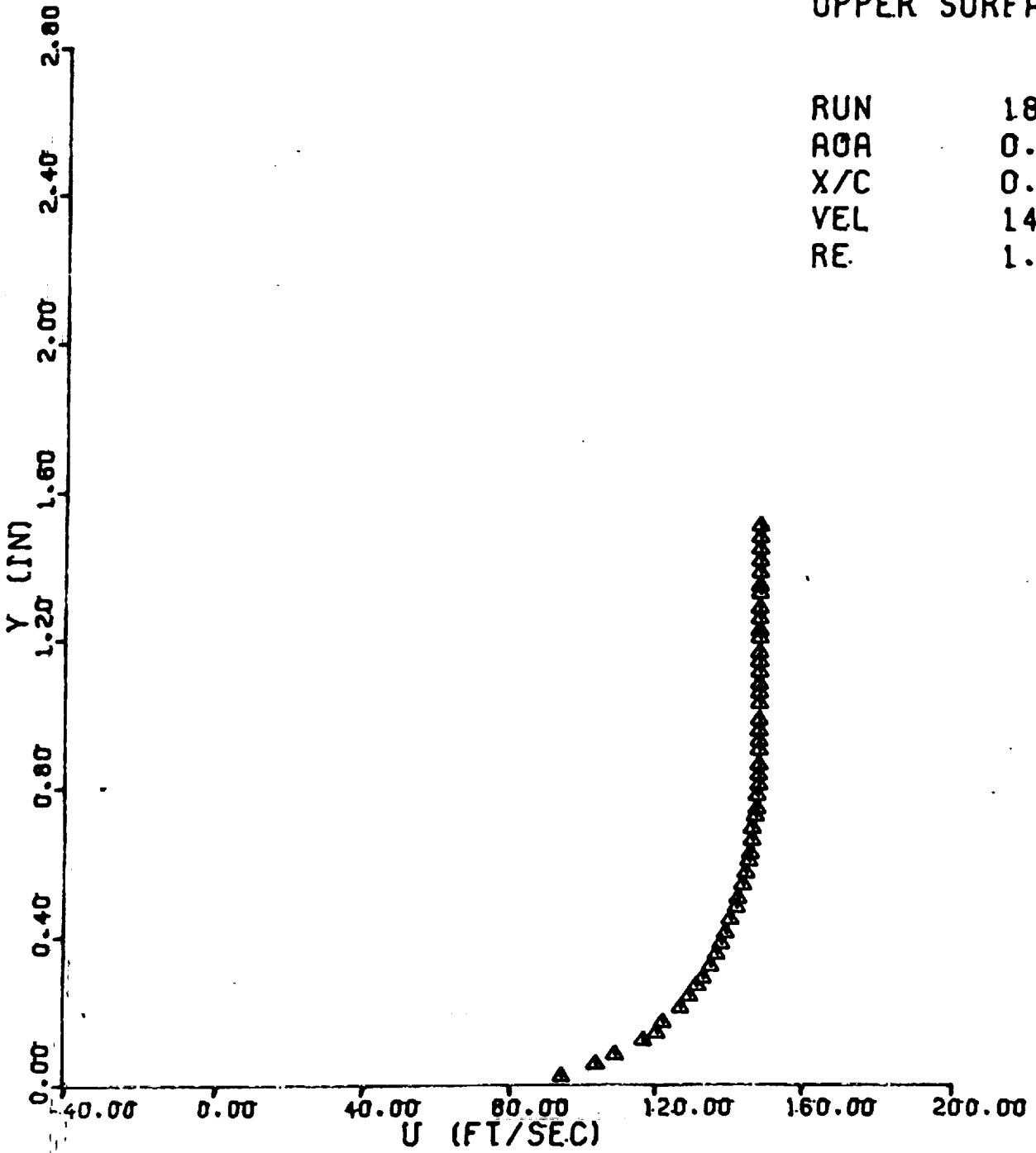
NACA 0012
WAKE

RUN	1888
AOA	6.000
X/C	1.8000
VEL	138.1
RE	1.60



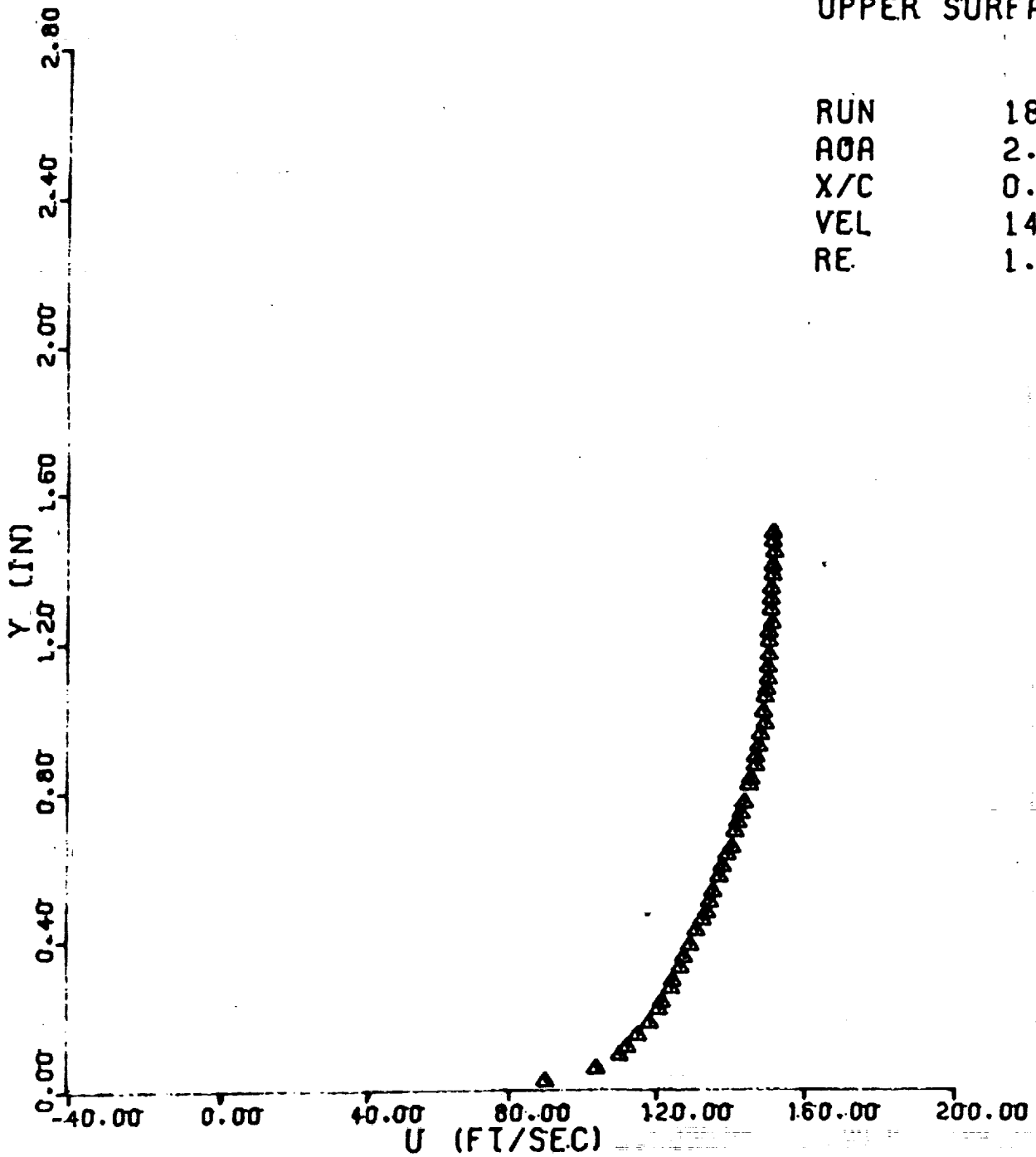
NACA 0012
UPPER SURFACE

RUN	1892
AOA	0.000
X/C	0.6000
VEL	140.5
RE	1.63

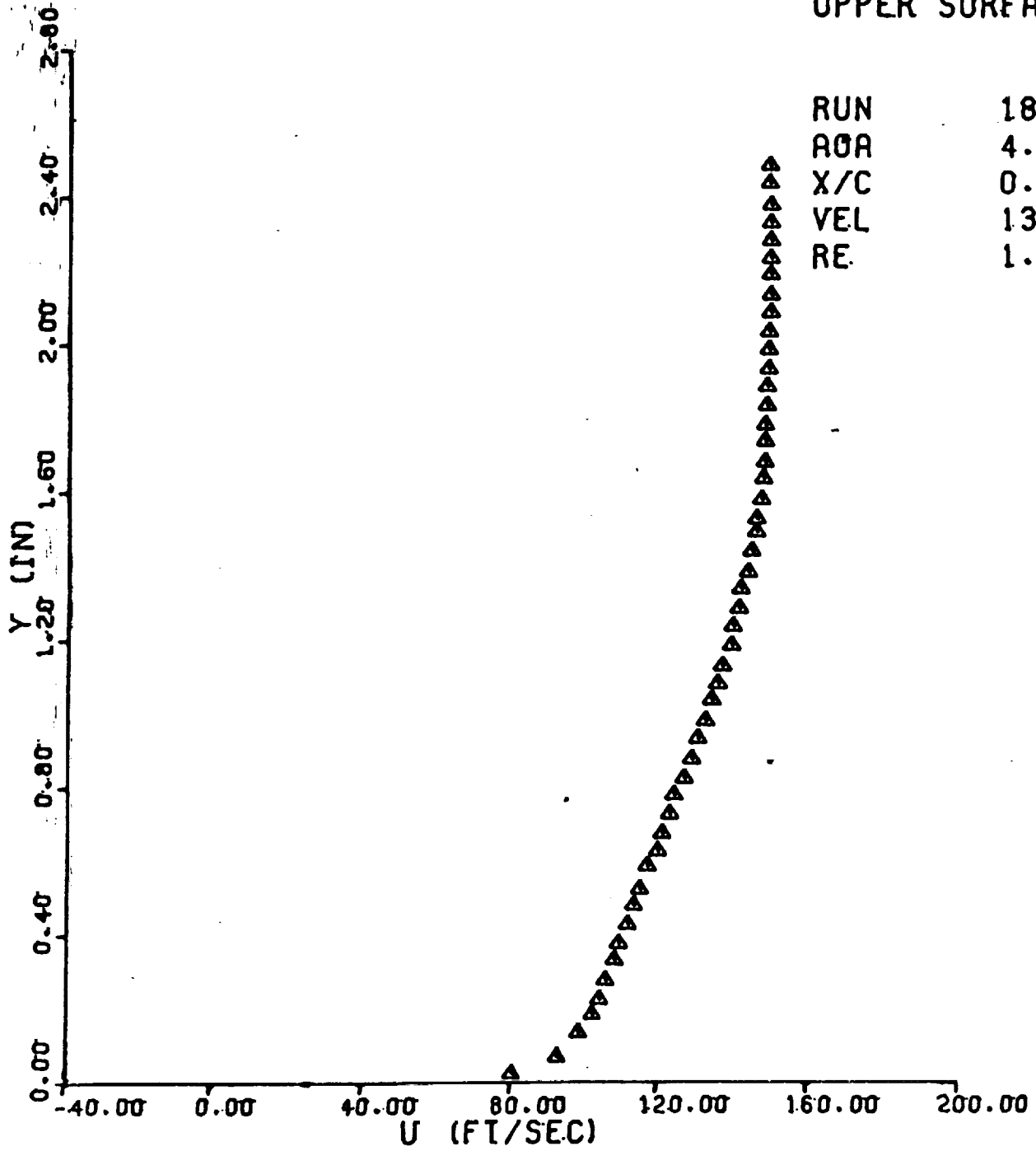


NACA 0012
UPPER SURFACE

RUN	1893
AOA	2.000
X/C	0.6000
VEL	140.3
RE	1.63

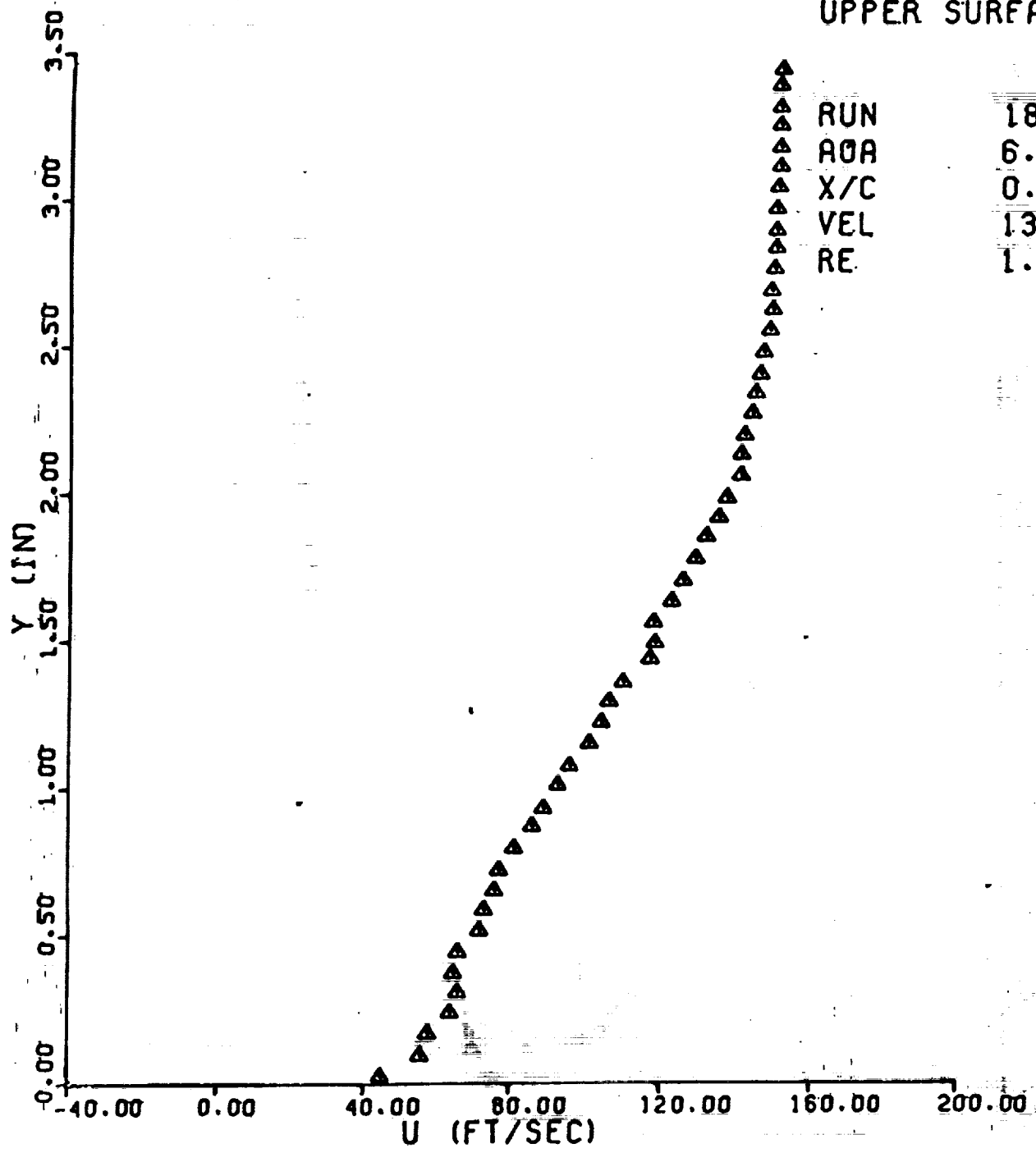


NACA 0012
UPPER SURFACE



RUN	1894
AOA	4.000
X/C	0.6000
VEL	139.8
RE.	1.62

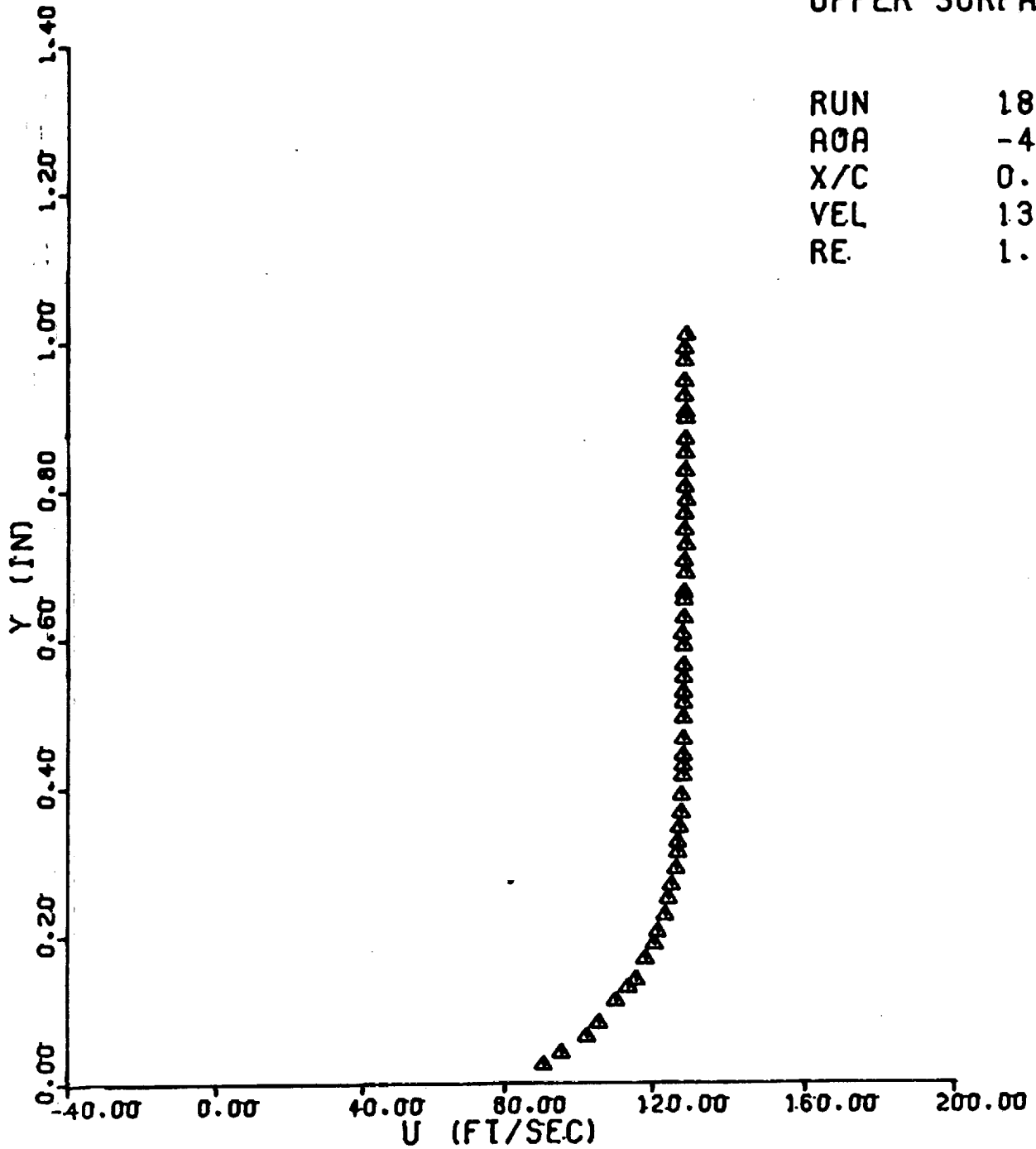
NACA 0012
UPPER SURFACE



RUN	1895
AOA	6.000
X/C	0.6000
VEL	138.8
RE	1.61

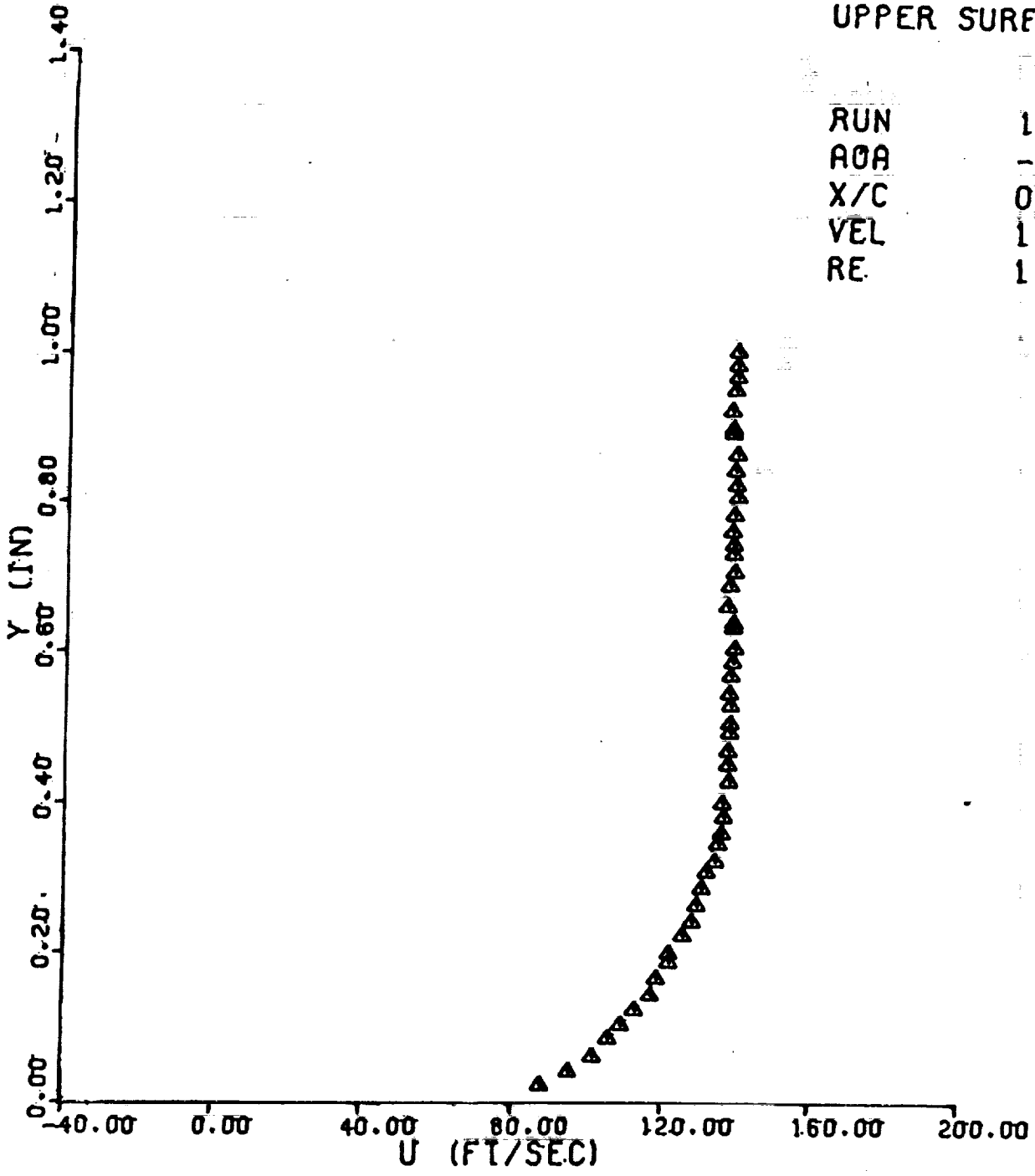
NACA 0012
UPPER SURFACE

RUN 1897
AOA -4.000
X/C 0.6000
VEL 139.3
RE. 1.68



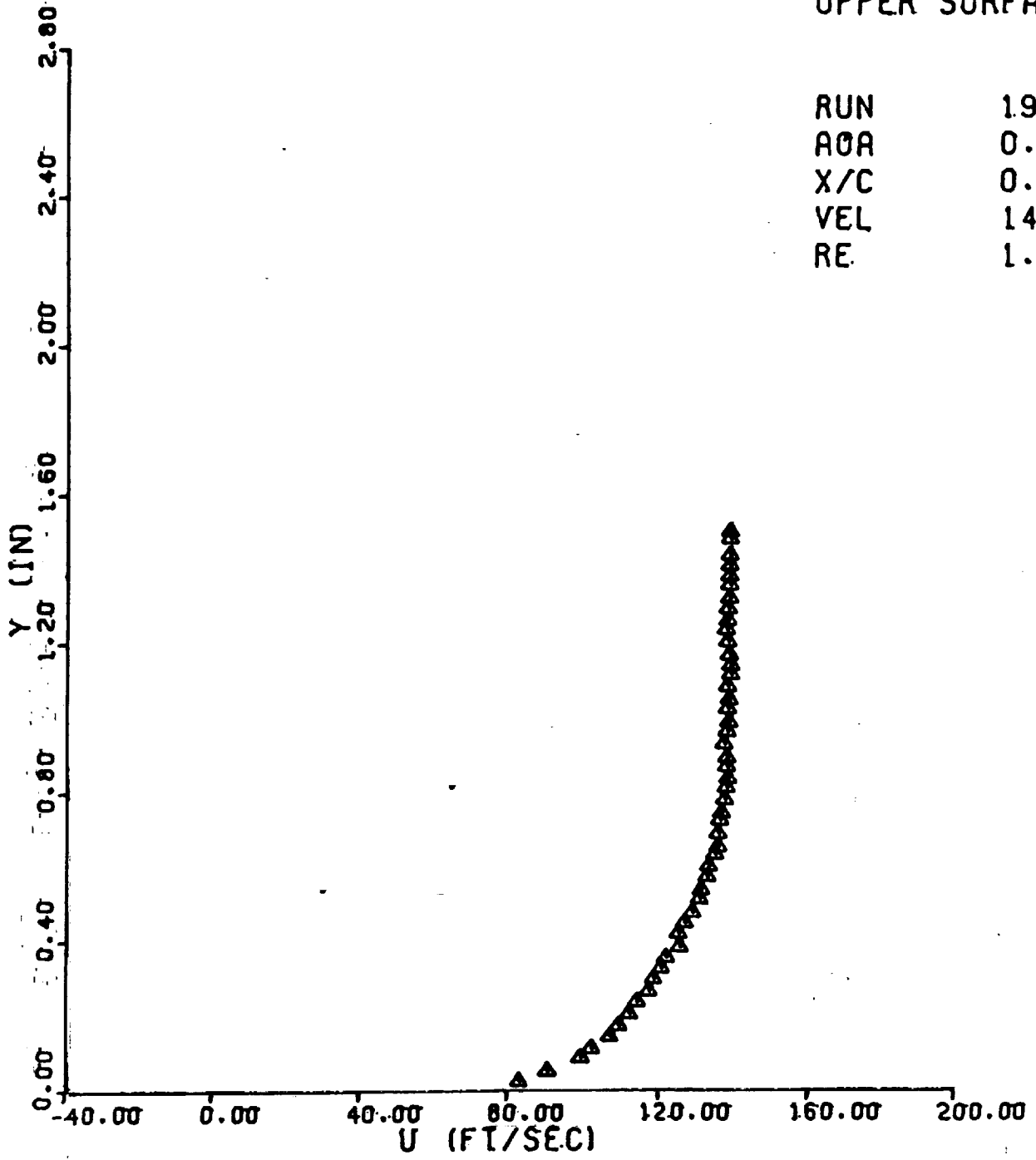
NACA 0012
UPPER SURFACE

RUN	1899
AOA	-4.000
X/C	0.8000
VEL	142.1
RE	1.67



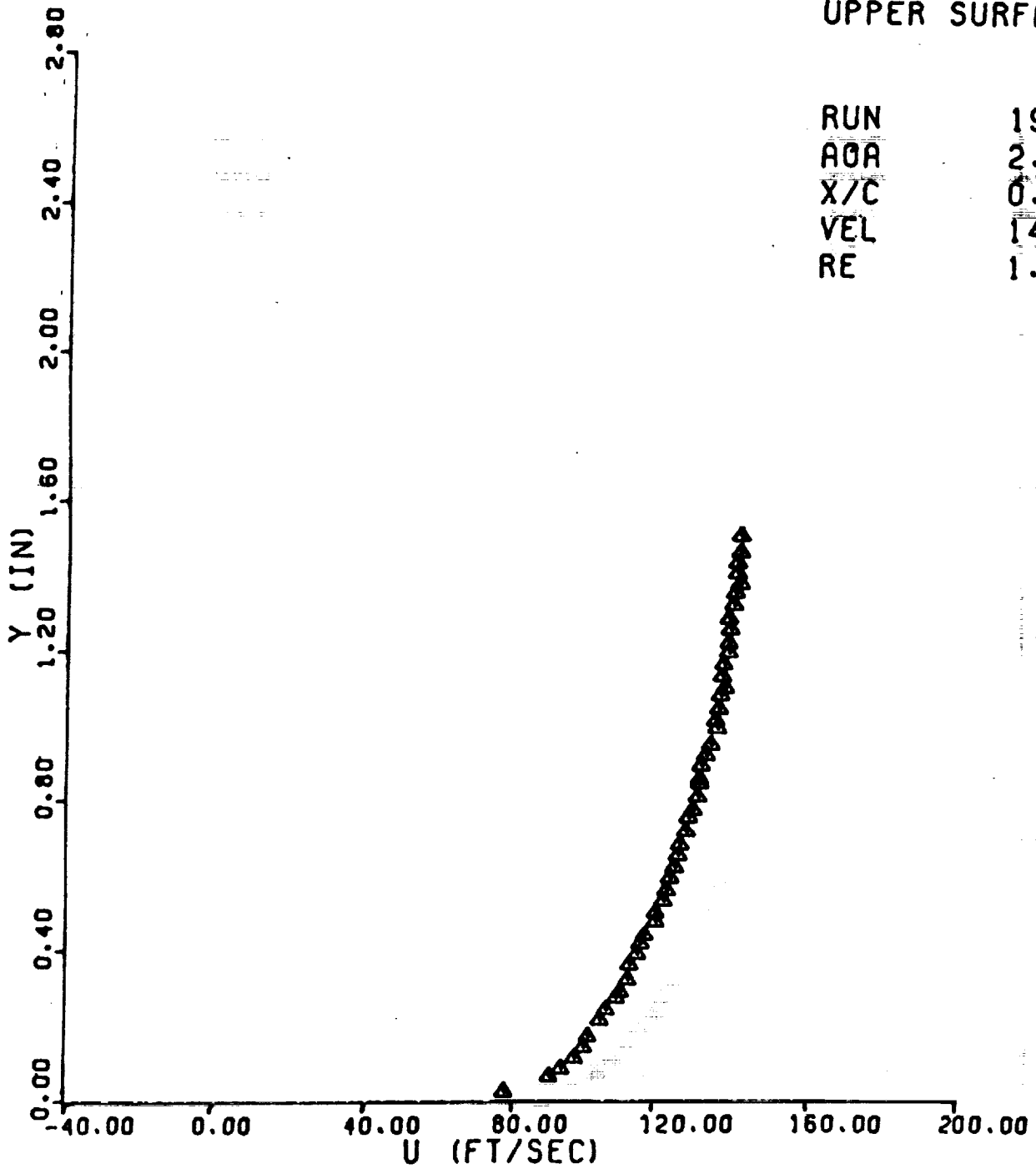
NACA 0012
UPPER SURFACE

RUN 1900
AOA 0.000
X/C 0.8000
VEL 143.1
RE 1.68



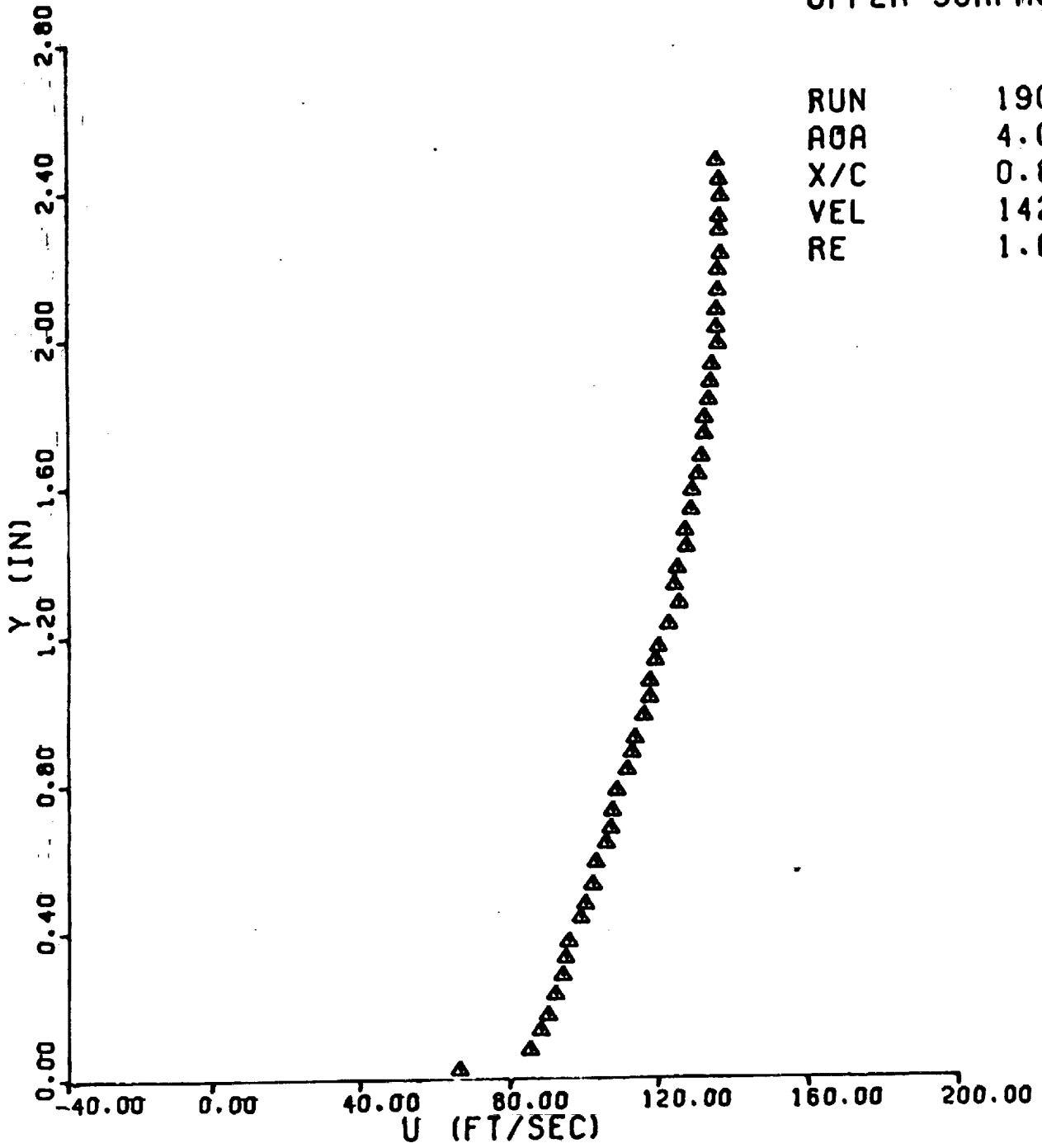
NACA 0012
UPPER SURFACE

RUN	1901
AOA	2.000
X/C	0.8000
VEL	142.3
RE	1.67



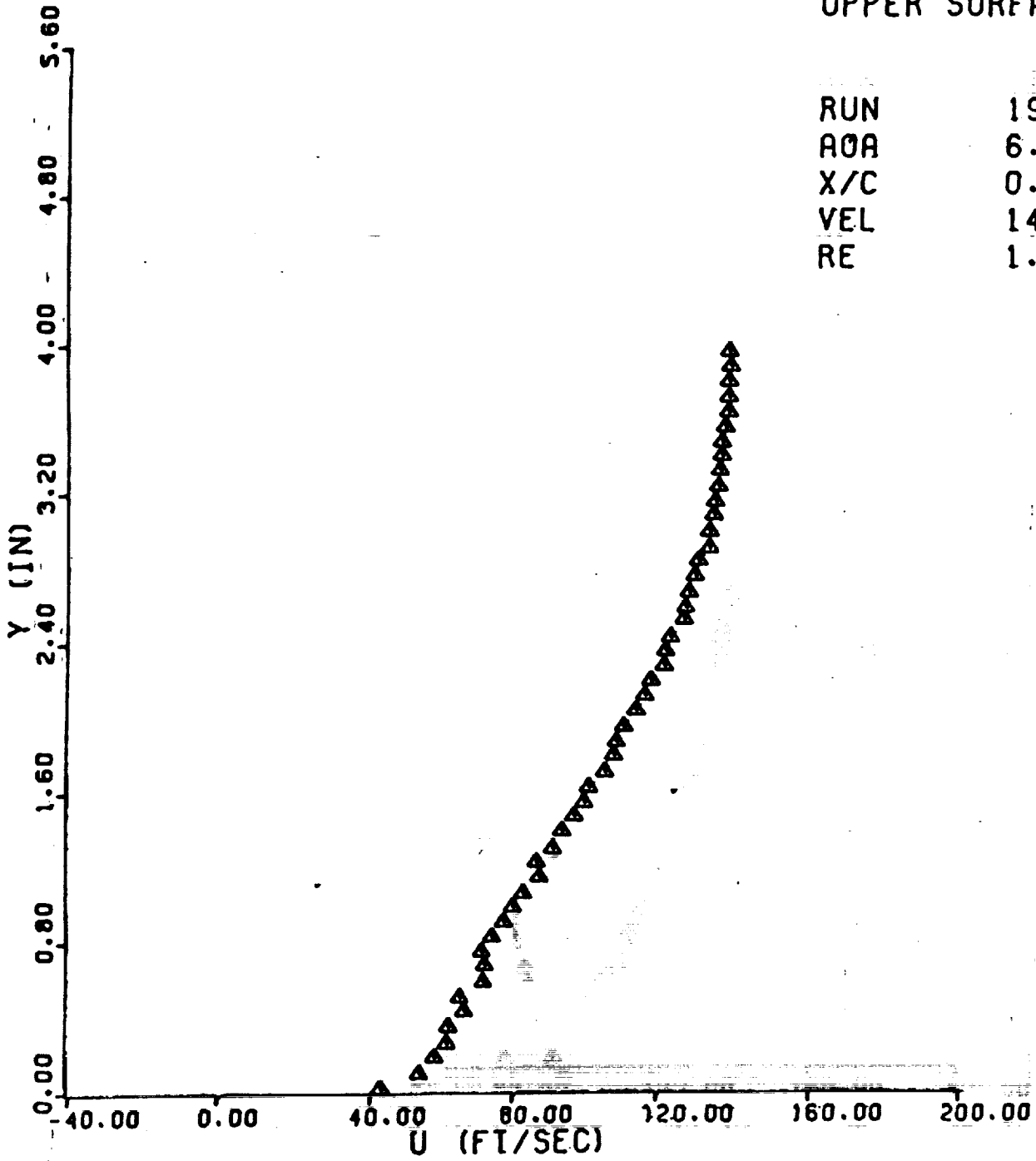
NACA 0012
UPPER SURFACE

RUN	1902
AOA	4.000
X/C	0.8000
VEL	142.1
RE	1.69



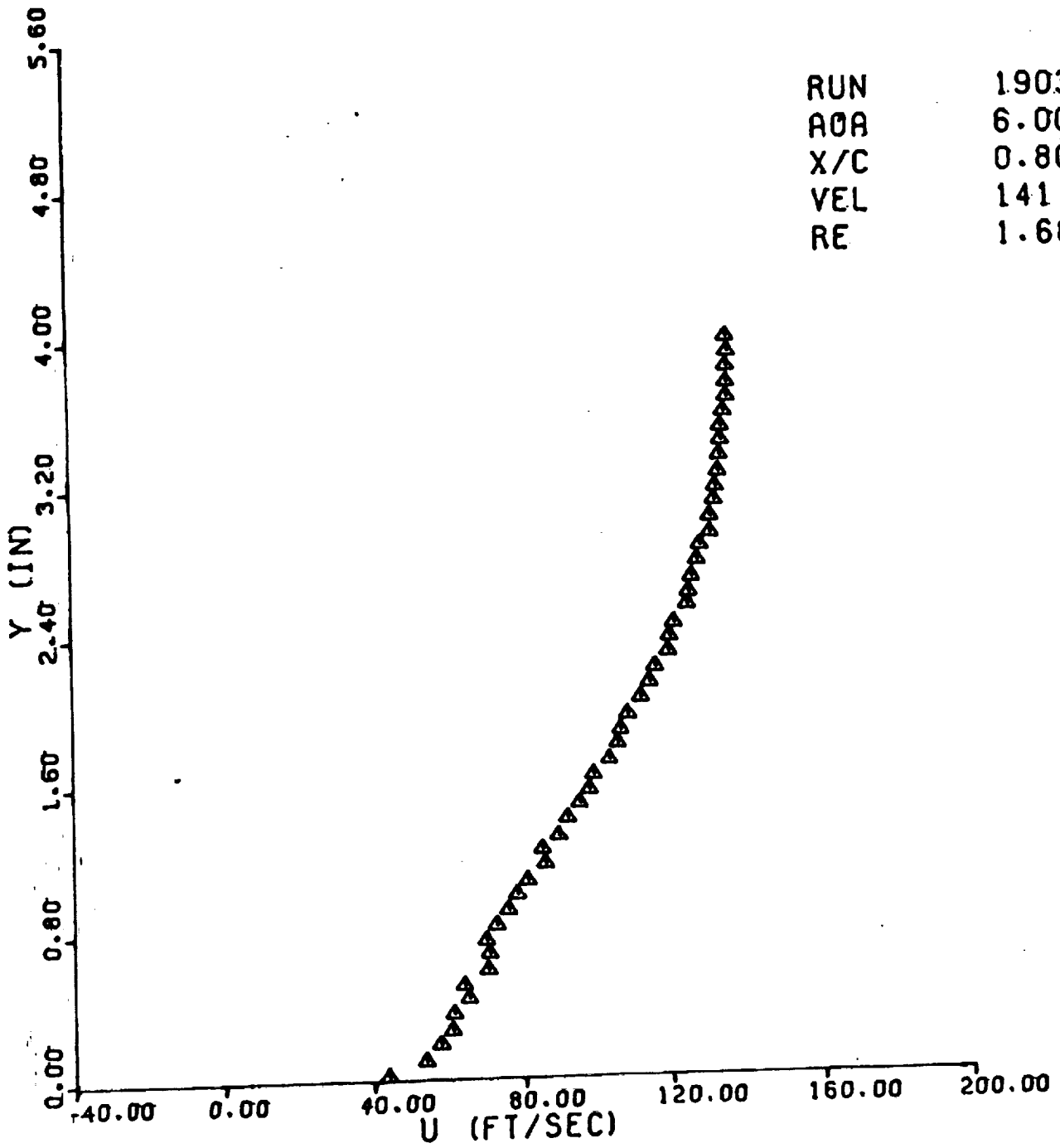
NACA 0012
UPPER SURFACE

RUN	1903
AOA	6.000
X/C	0.8000
VEL	141.1
RE	1.68



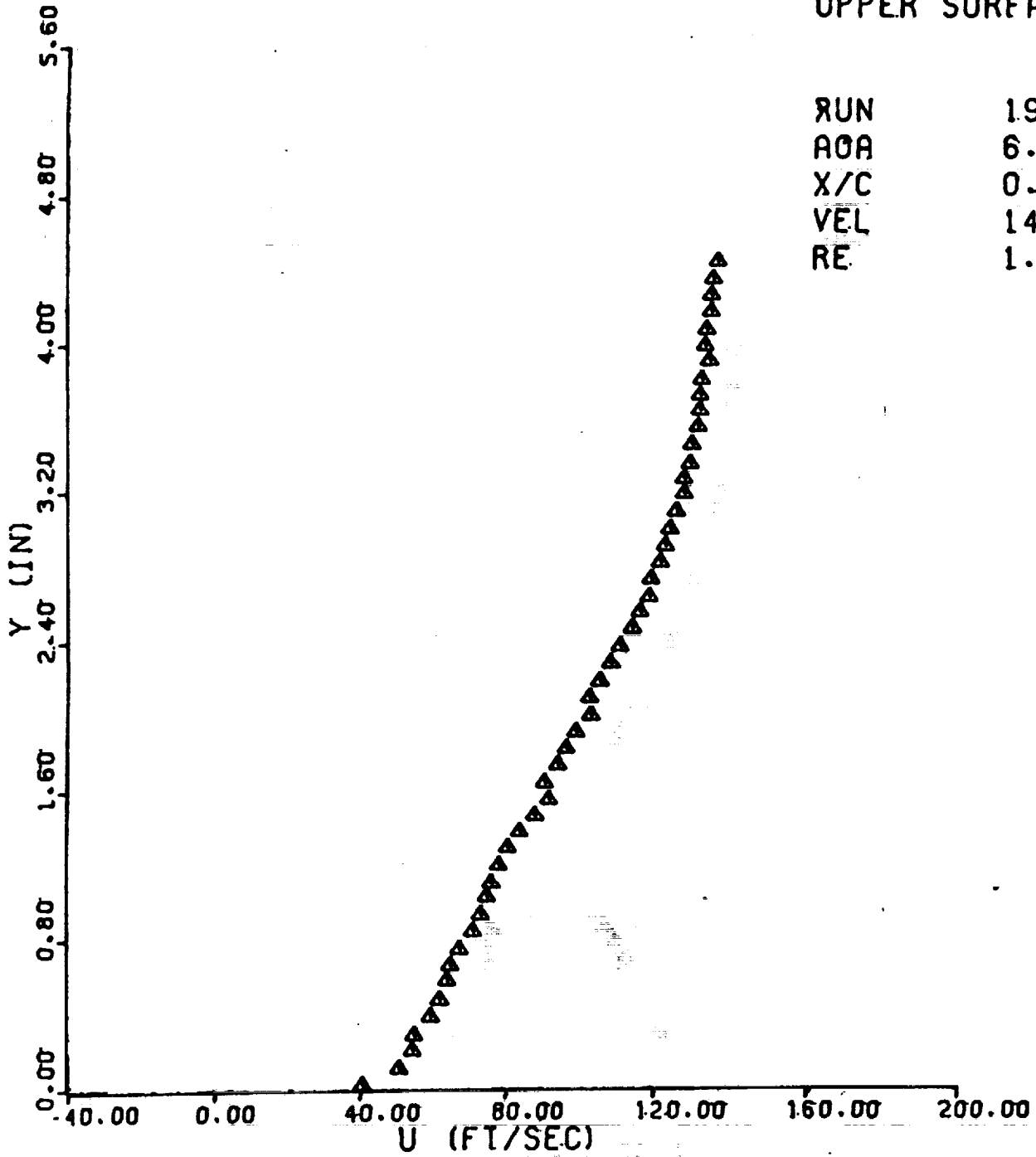
NACA 0012
UPPER SURFACE

RUN	1903
AOA	6.000
X/C	0.8000
VEL	141.1
RE	1.68



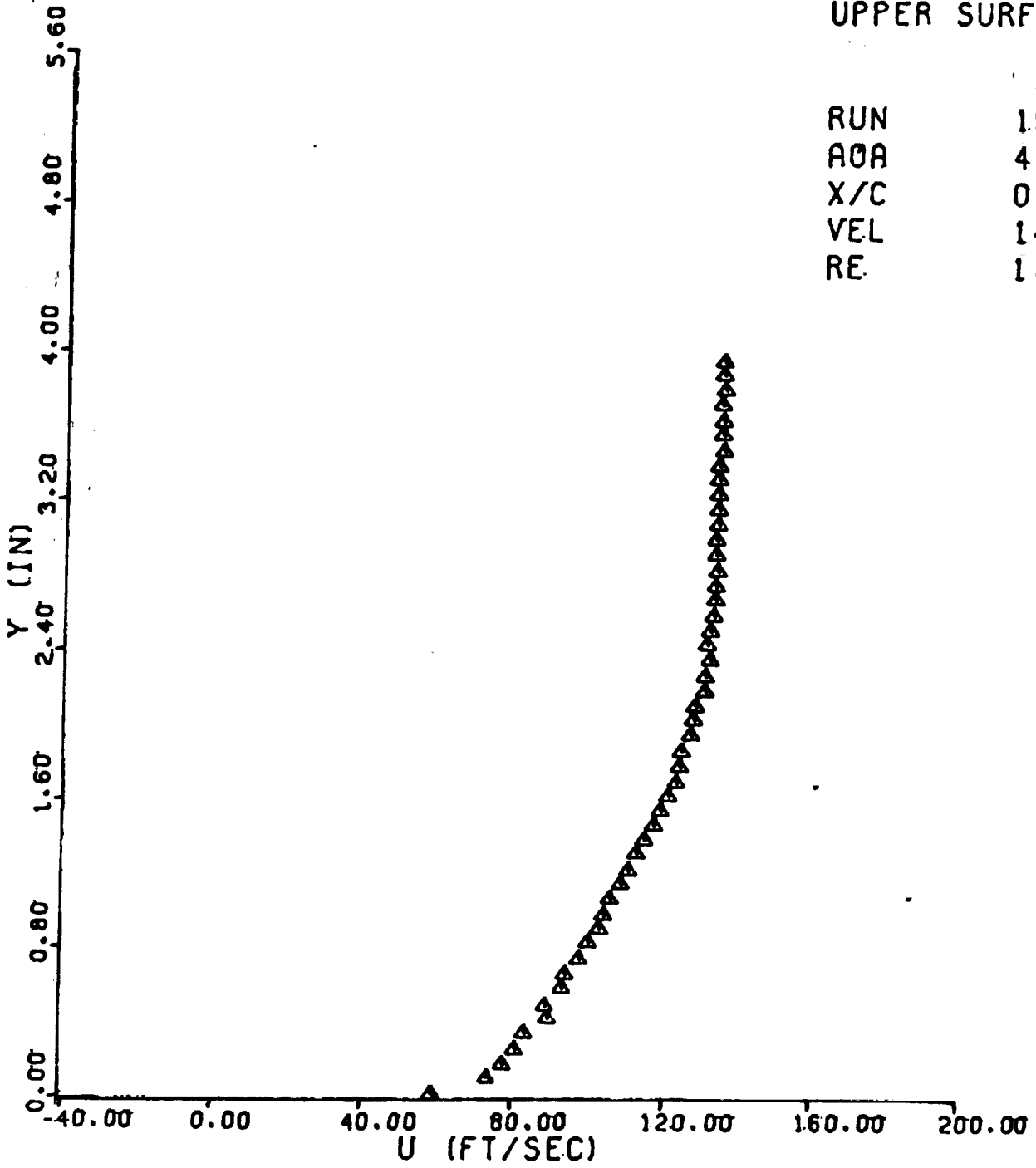
NACA 0012
UPPER SURFACE

RUN 1904
AOA 6.000
X/C 0.9000
VEL 140.9
RE 1.67



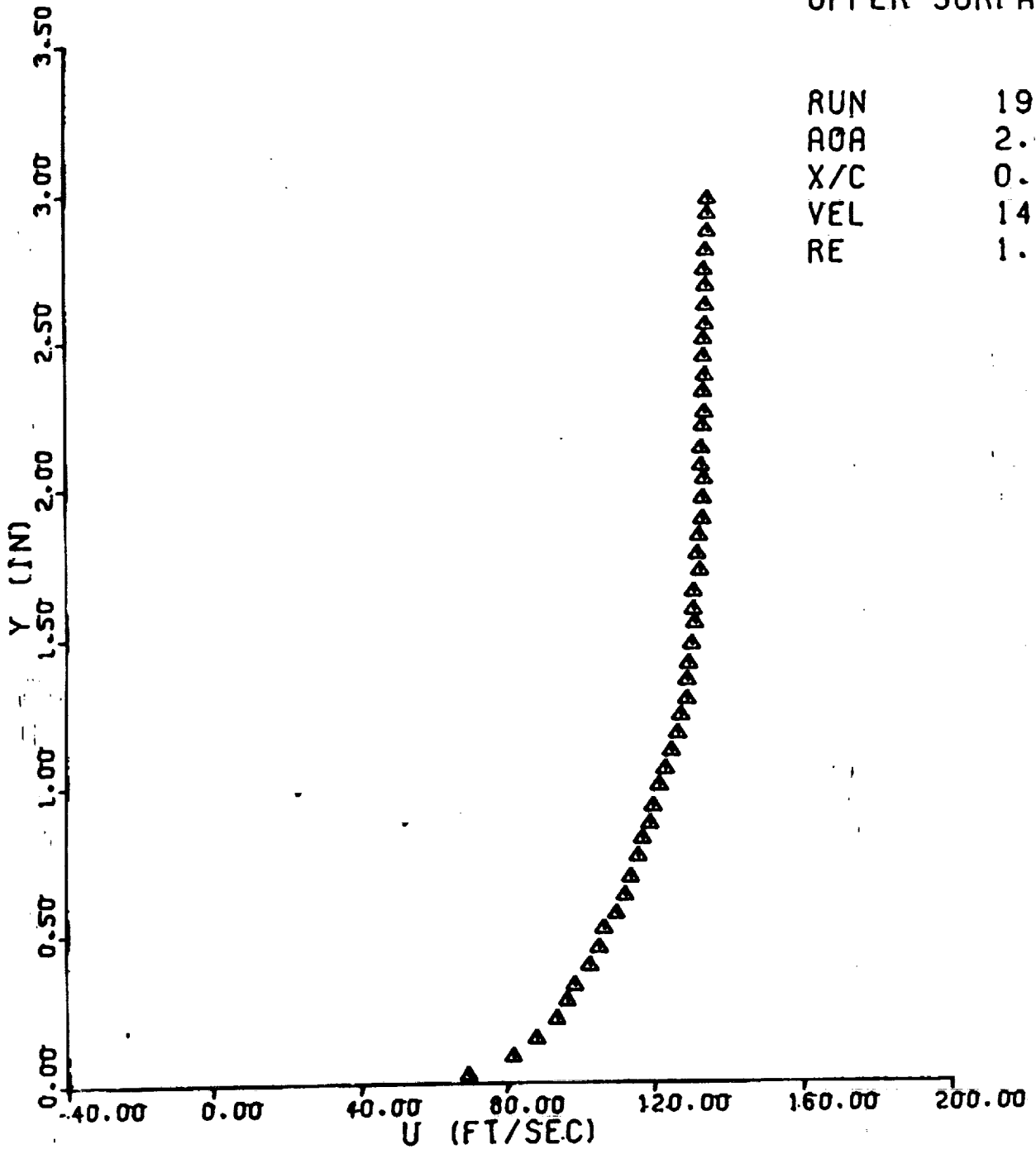
NACA 0012
UPPER SURFACE

RUN	1905
AOA	4.000
X/C	0.9000
VEL	141.7
RE	1.68



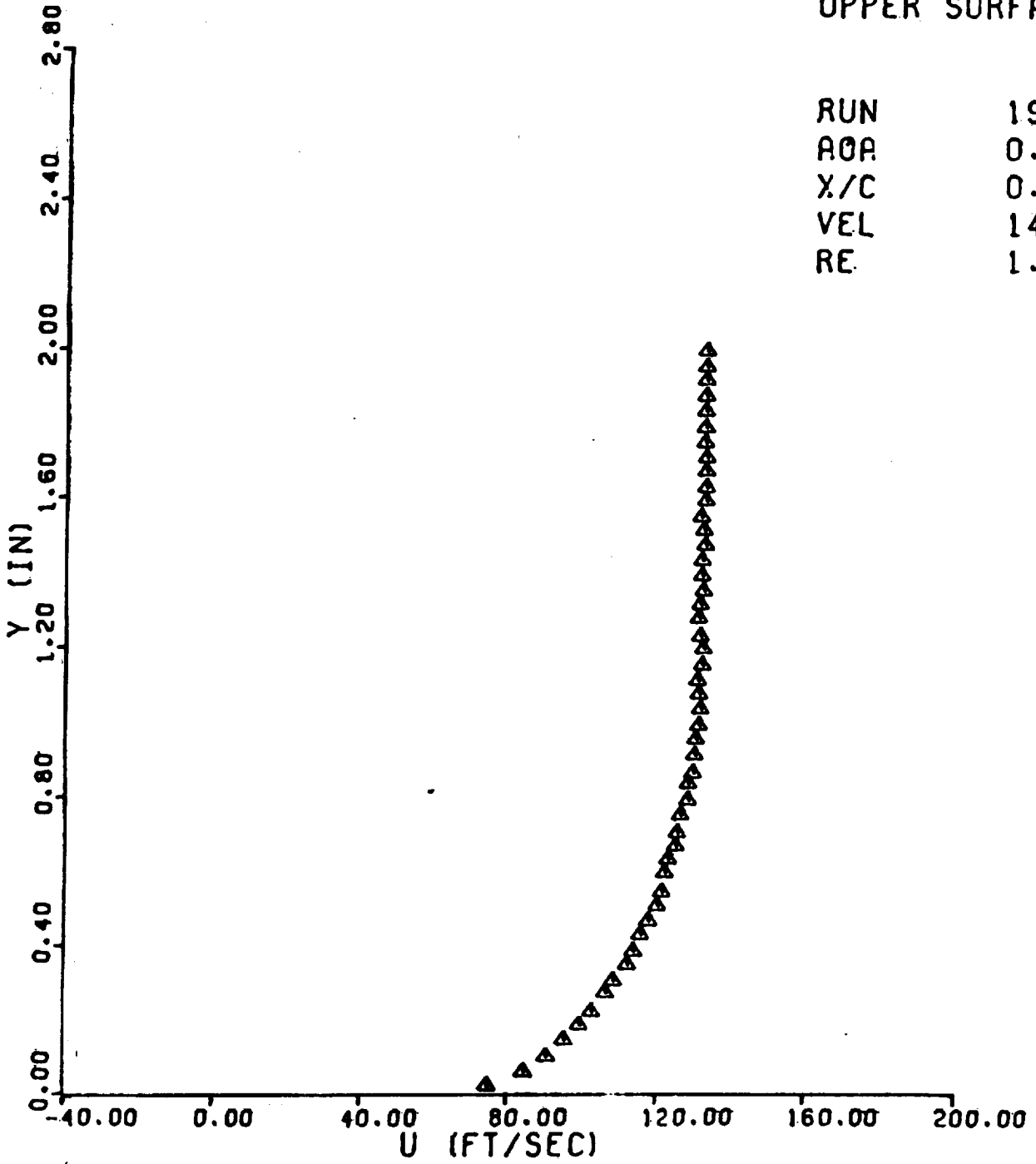
NACA 0012
UPPER SURFACE

RUN	1906
AOA	2.000
X/C	0.9000
VEL	142.7
RE	1.70



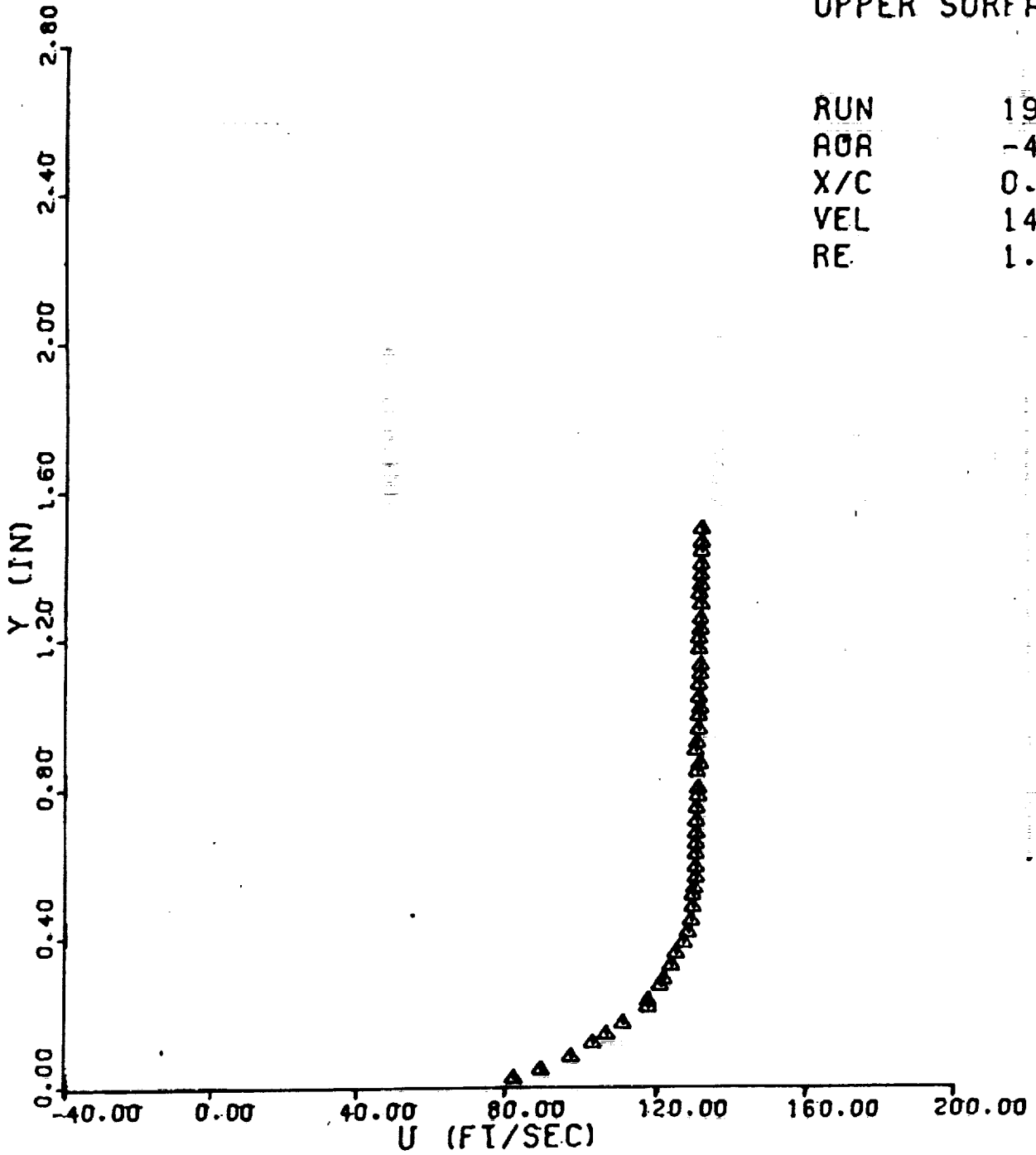
NACA 0012
UPPER SURFACE

RUN 1907
AOA 0.000
X/C 0.9000
VEL 141.8
RE 1.69



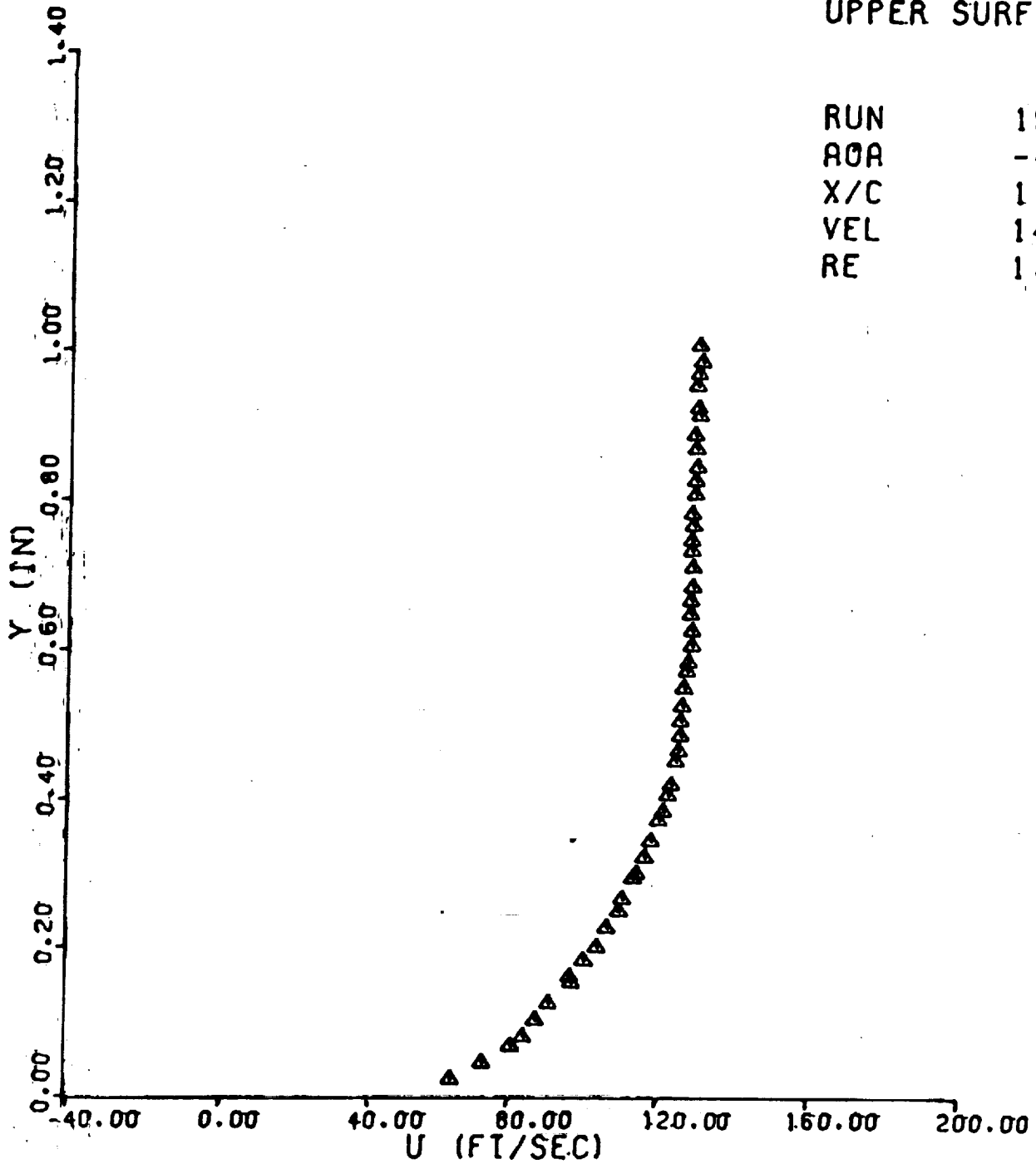
NACA 0012
UPPER SURFACE

RUN	1908
AOA	-4.000
X/C	0.9000
VEL	143.1
RE	1.70



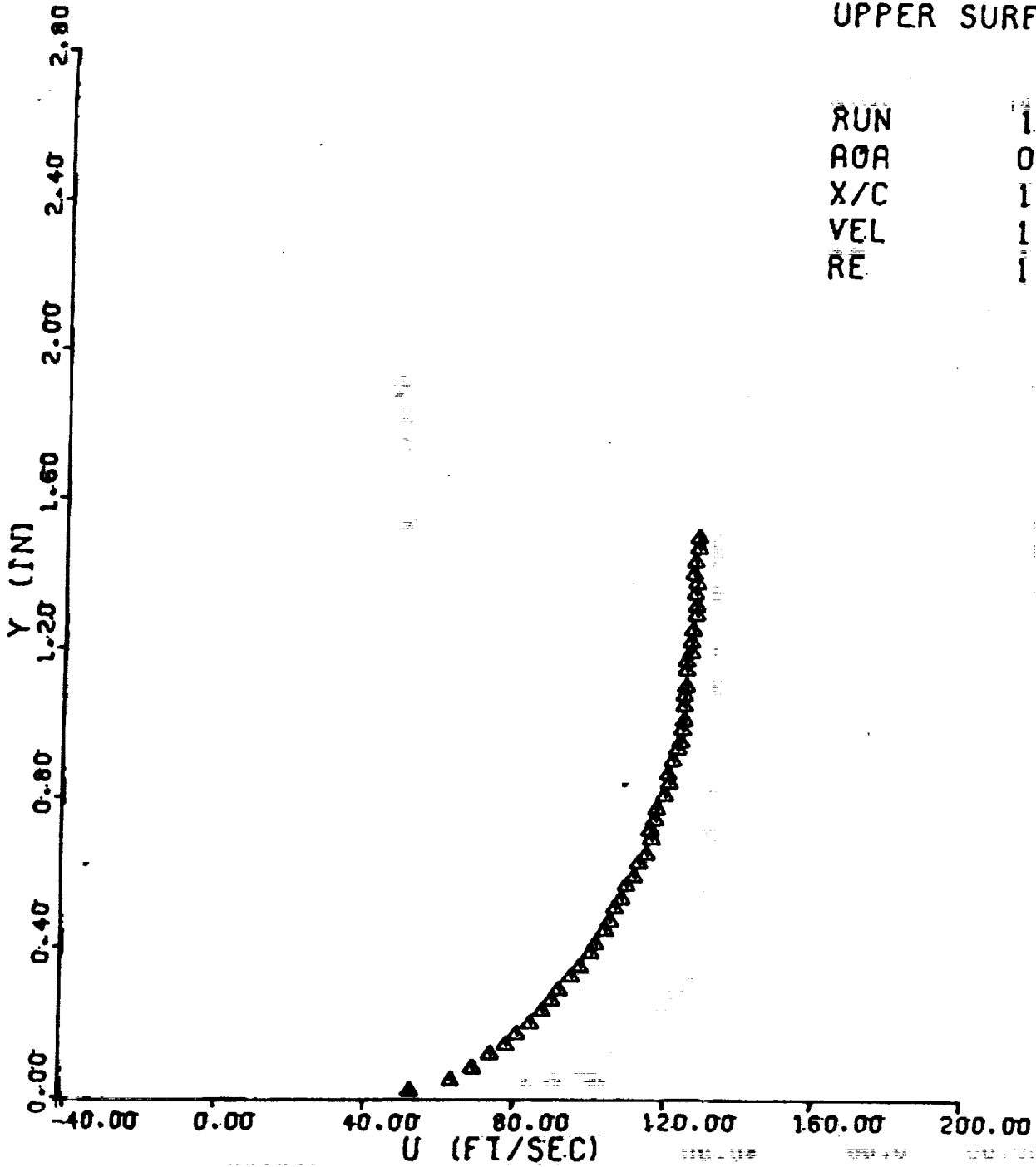
NACA 0012
UPPER SURFACE

RUN 1909
AOA -4.000
X/C 1.0000
VEL 142.8
RE 1.70

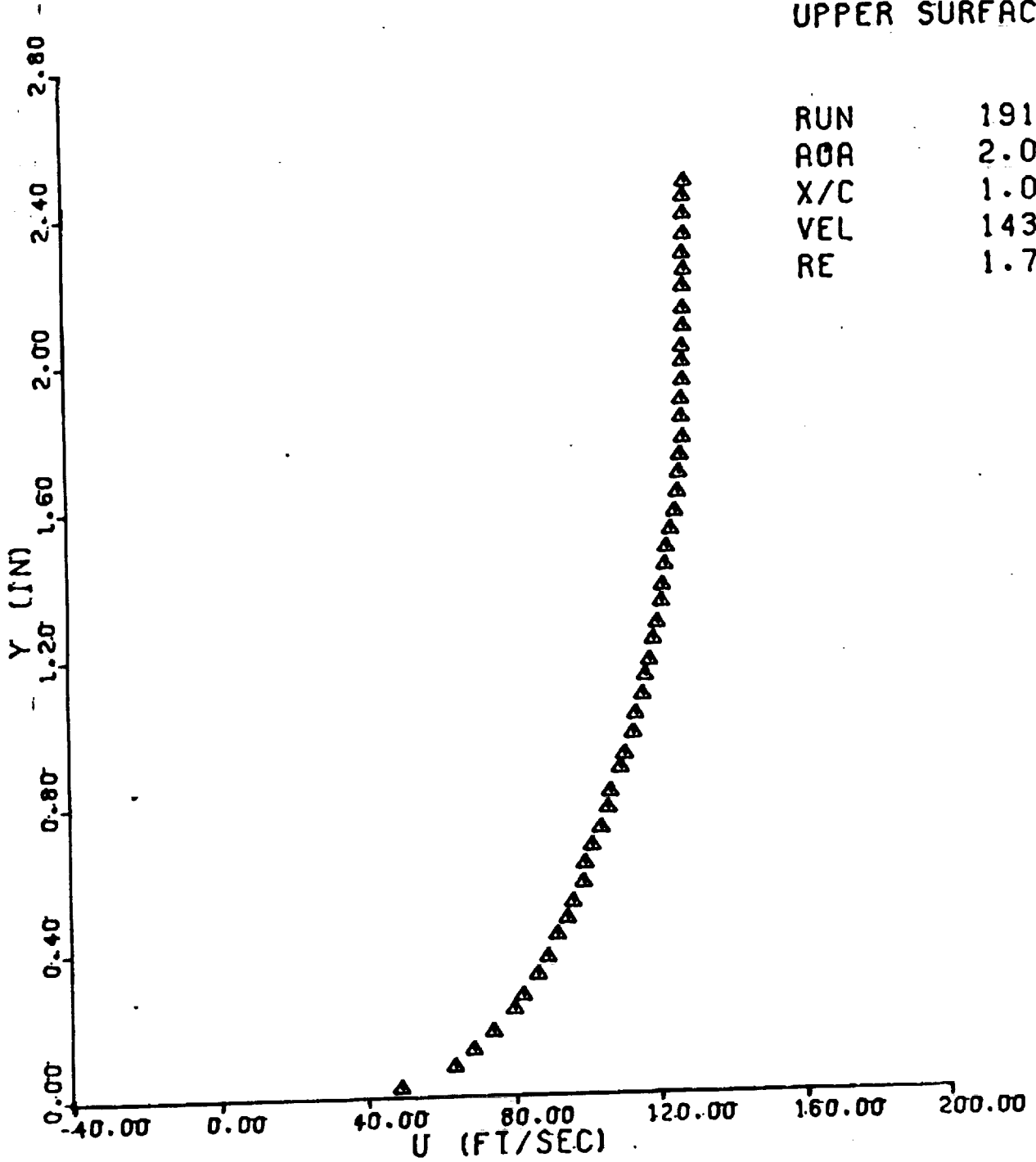


NACA 0012
UPPER SURFACE

RUN	1910
AOA	0.000
X/C	1.0000
VEL	143.3
RE	1.70



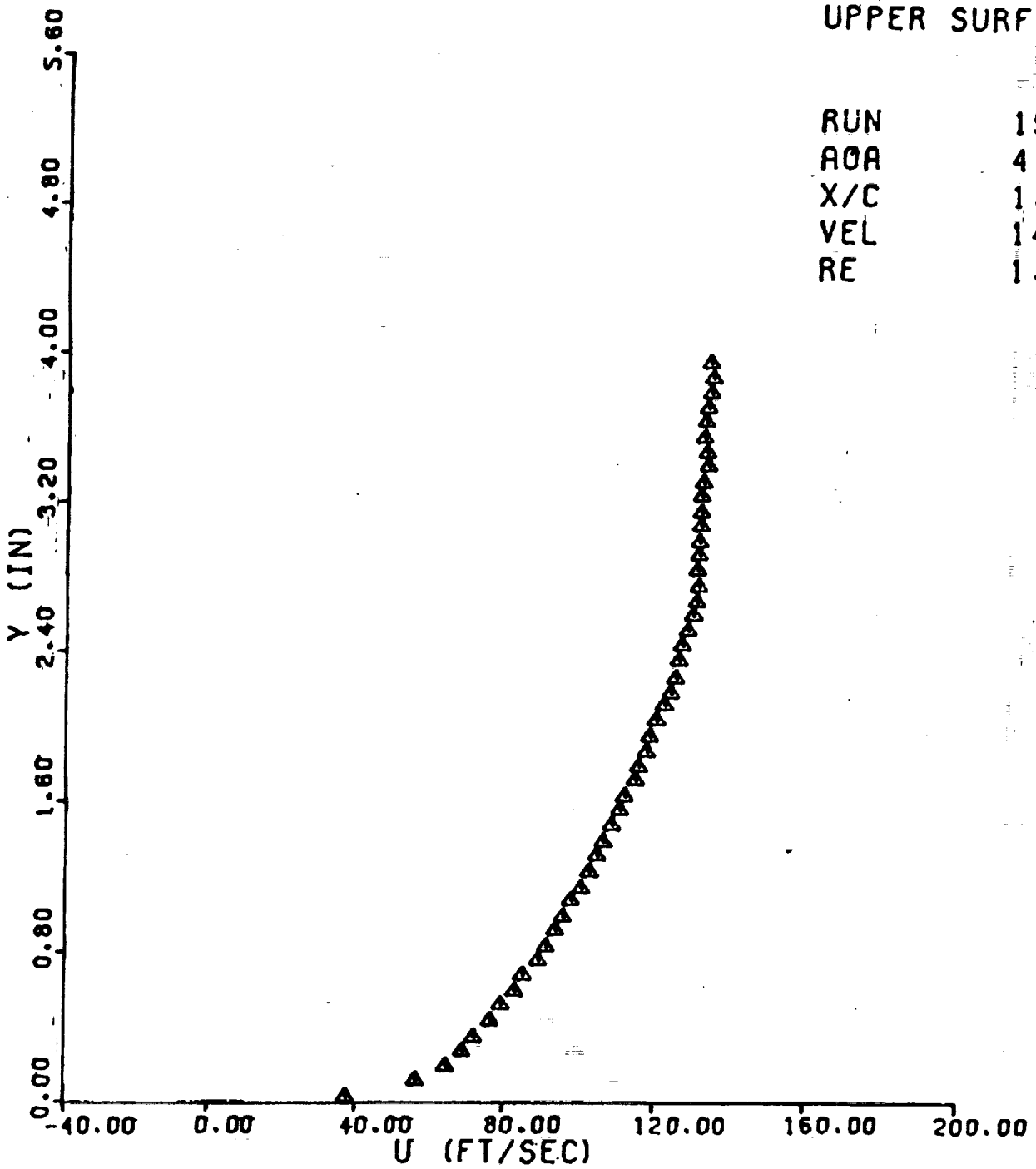
NACA 0012
UPPER SURFACE



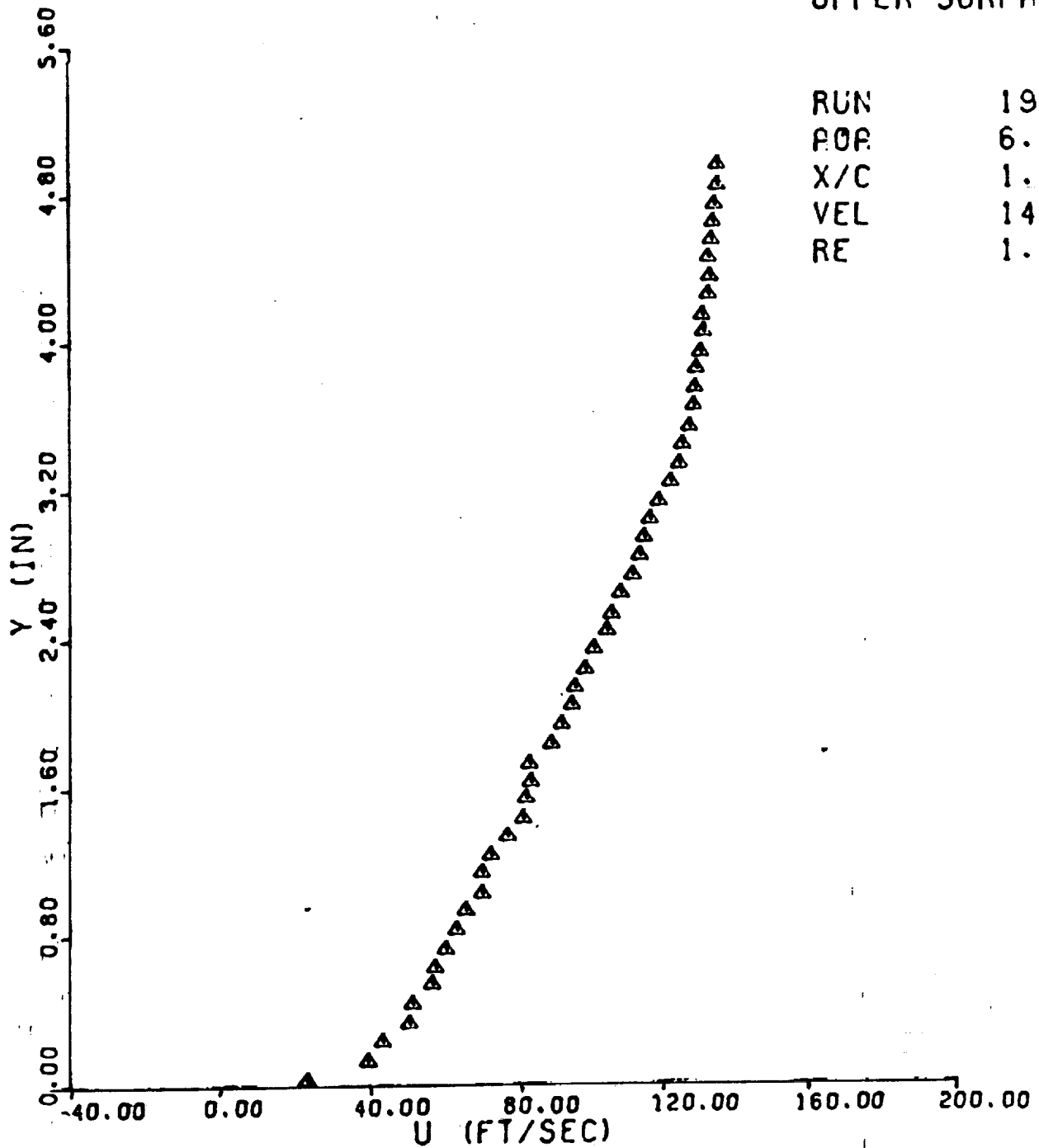
RUN	1911
AOA	2.000
X/C	1.0000
VEL	143.4
RE	1.70

NACA 0012
UPPER SURFACE

RUN 1912
AOA 4.000
X/C 1.0000
VEL 142.0
RE 1.69



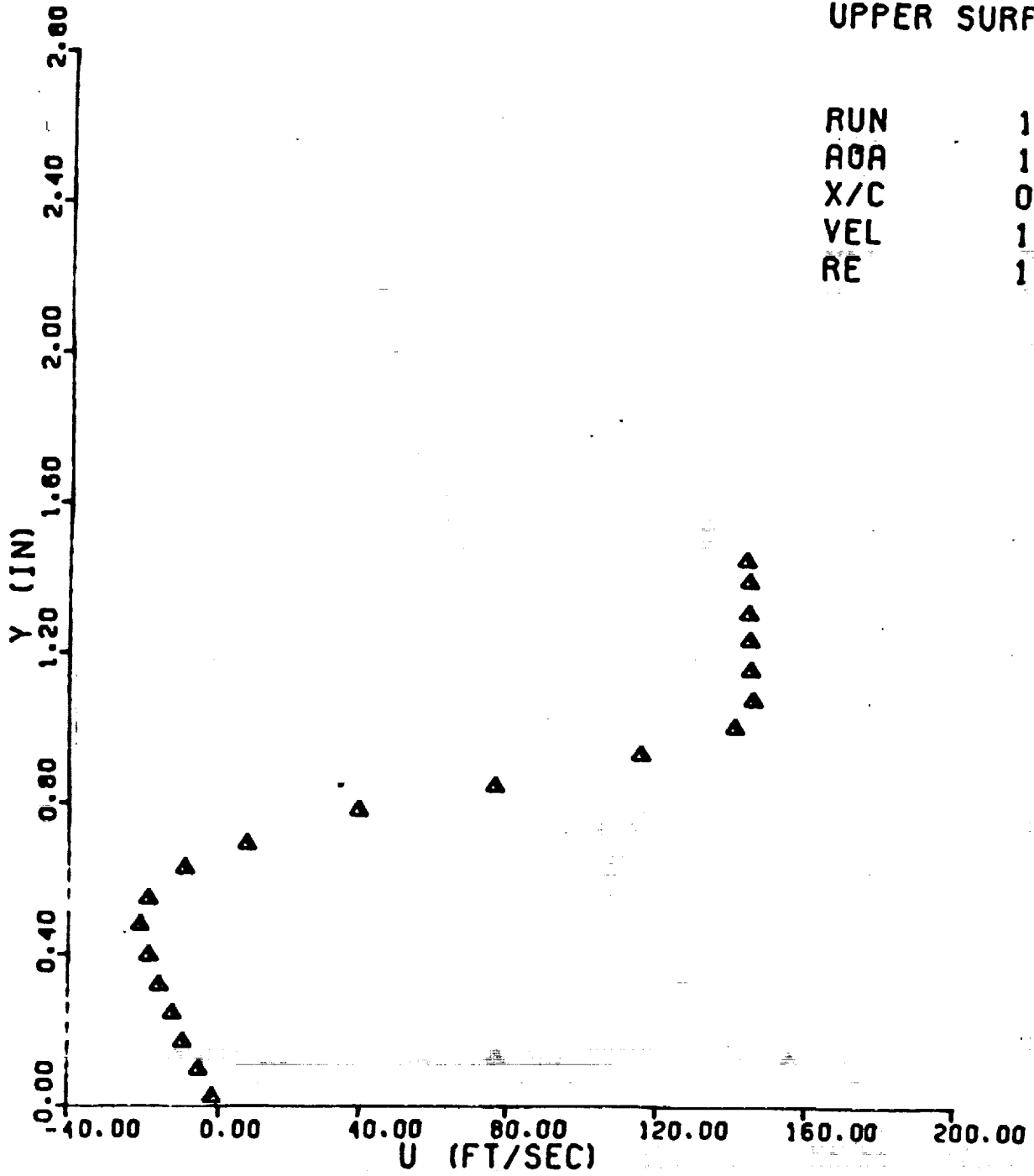
NACA 0012
UPPER SURFACE



RUN 1913
POA 6.000
X/C 1.0000
VEL 141.3
RE 1.68

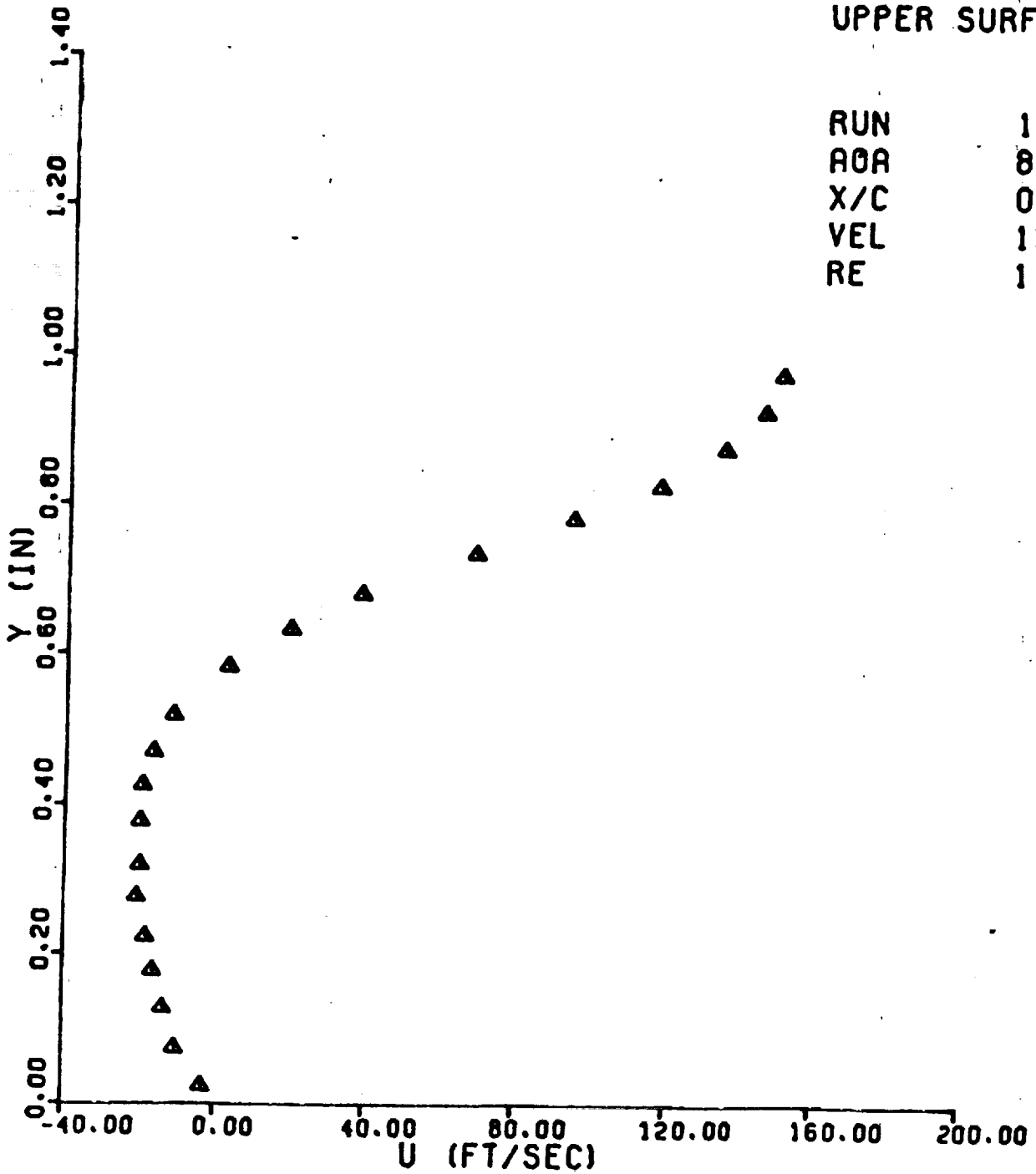
NACA 0012
UPPER SURFACE

RUN 1915
AOA 10.000
X/C 0.0400
VEL 136.2
RE 1.60



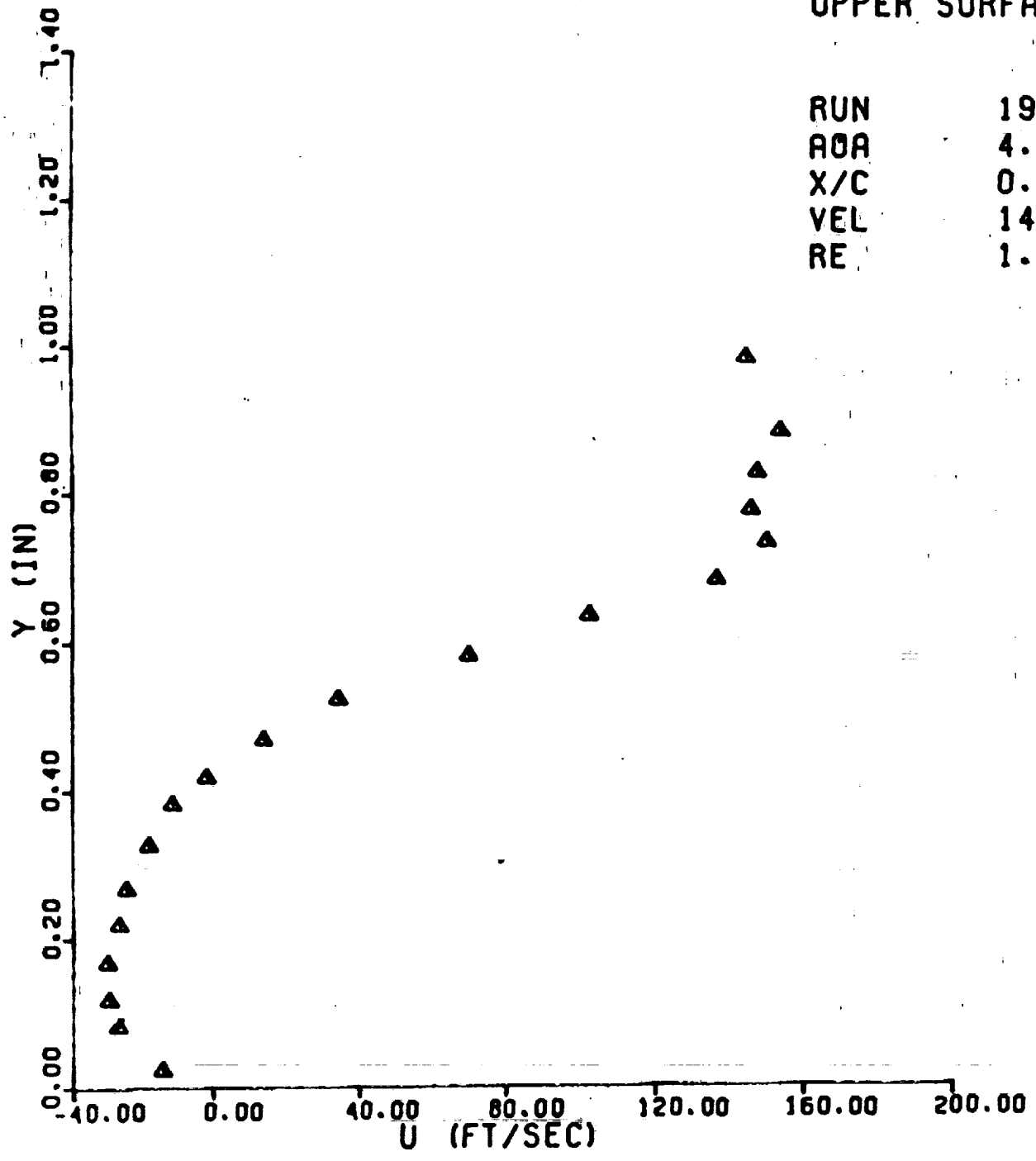
NACA 0012
UPPER SURFACE

RUN 1916
AOA 8.000
X/C 0.0400
VEL 137.0
RE 1.61



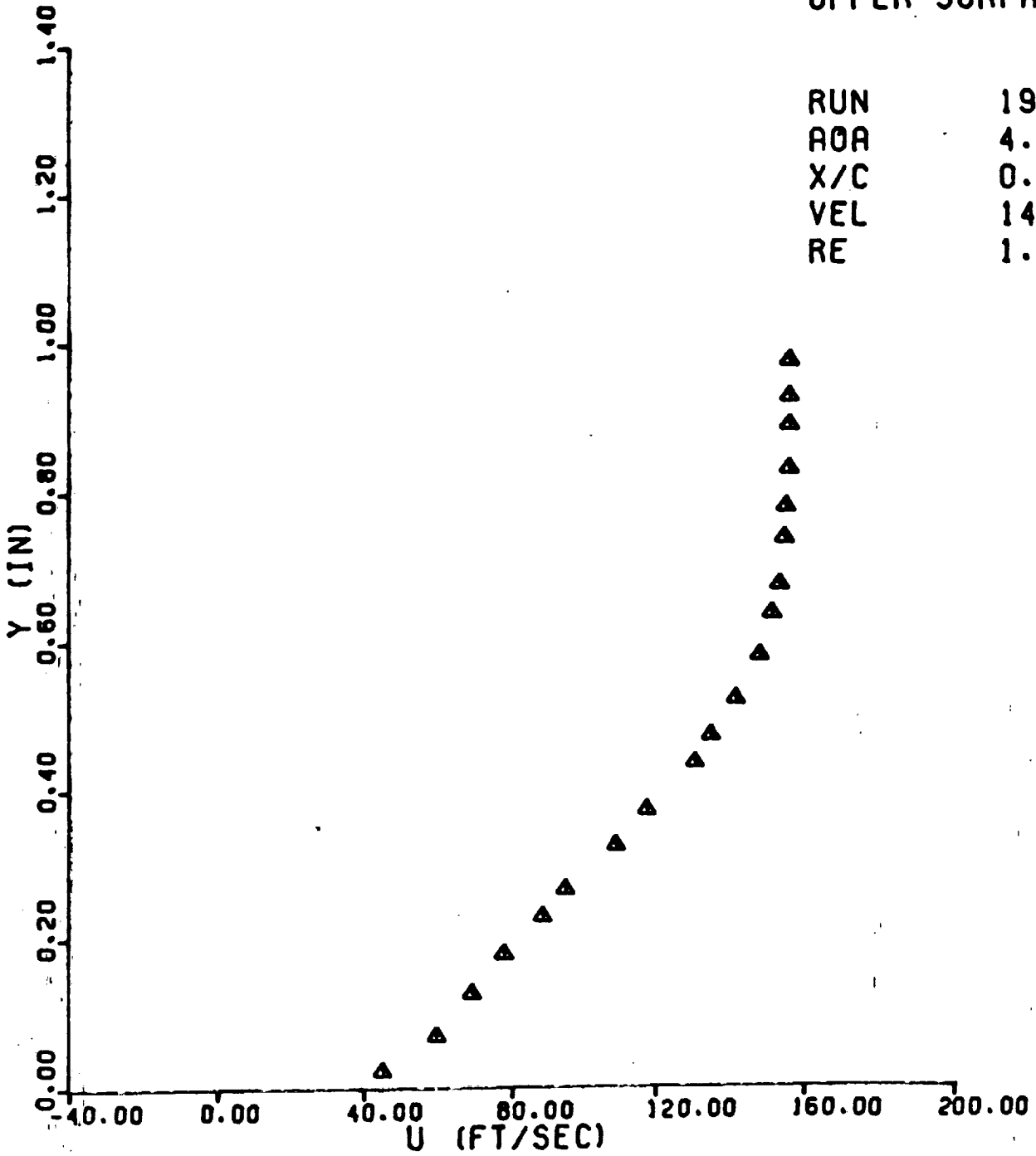
NACA 0012
UPPER SURFACE

RUN 1917
AOA 4.000
X/C 0.0400
VEL 141.1
RE 1.66

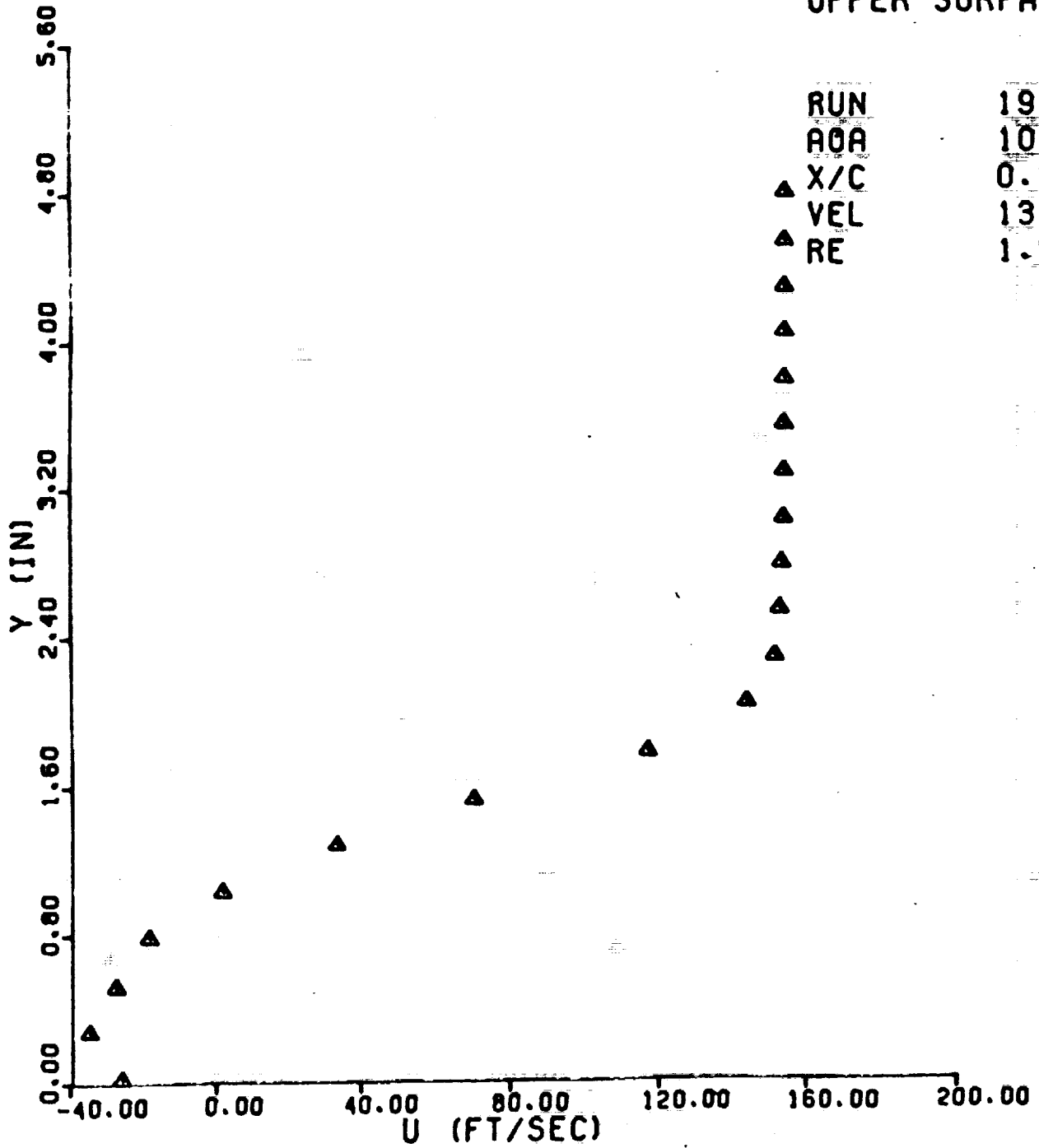


NACA 0012
UPPER SURFACE

RUN	1925
AOA	4.000
X/C	0.2000
VEL	141.1
RE	1.66

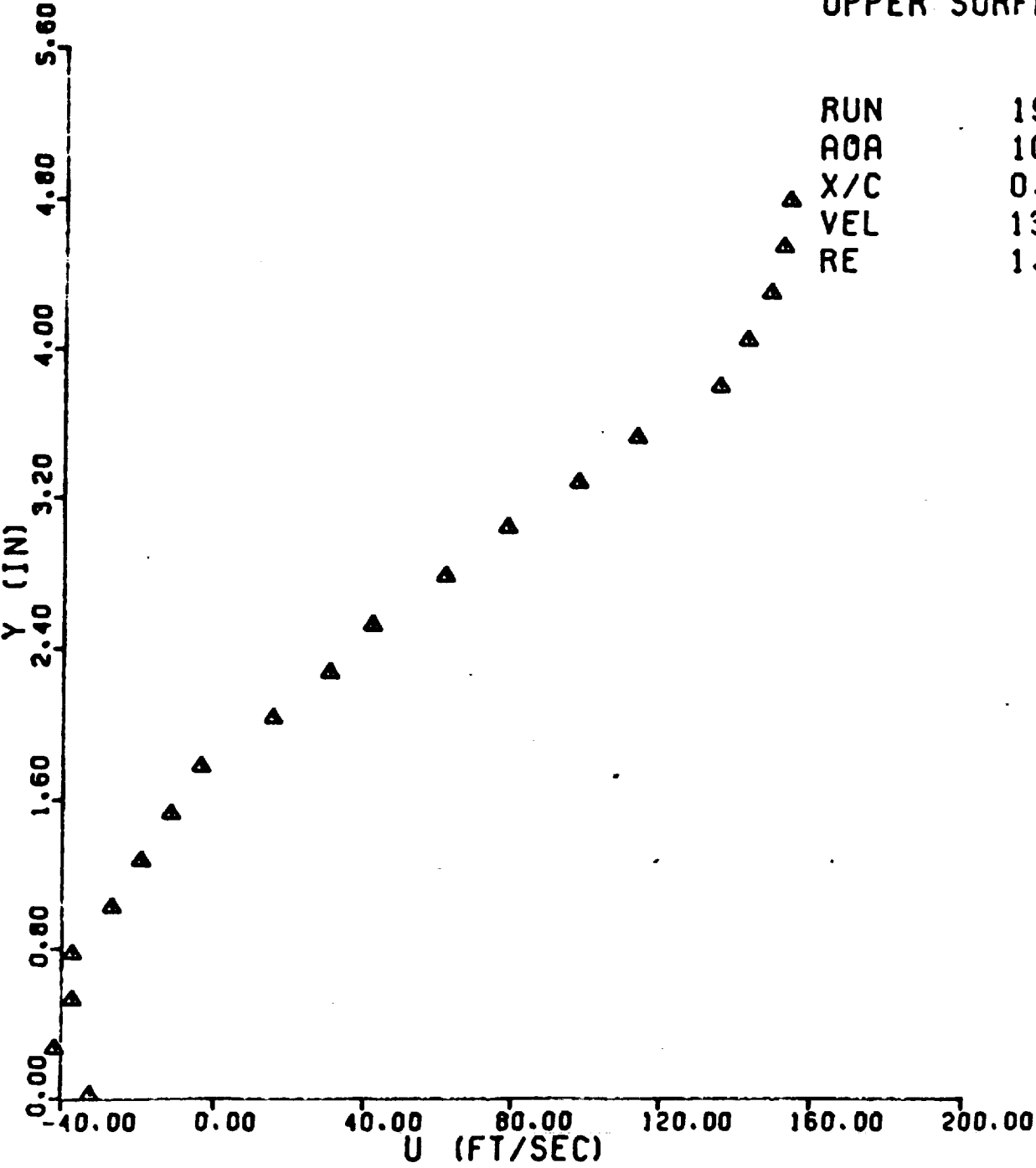


NACA 0012
UPPER SURFACE



RUN	1926
AOA	10.000
X/C	0.2000
VEL	135.6
RE	1.59

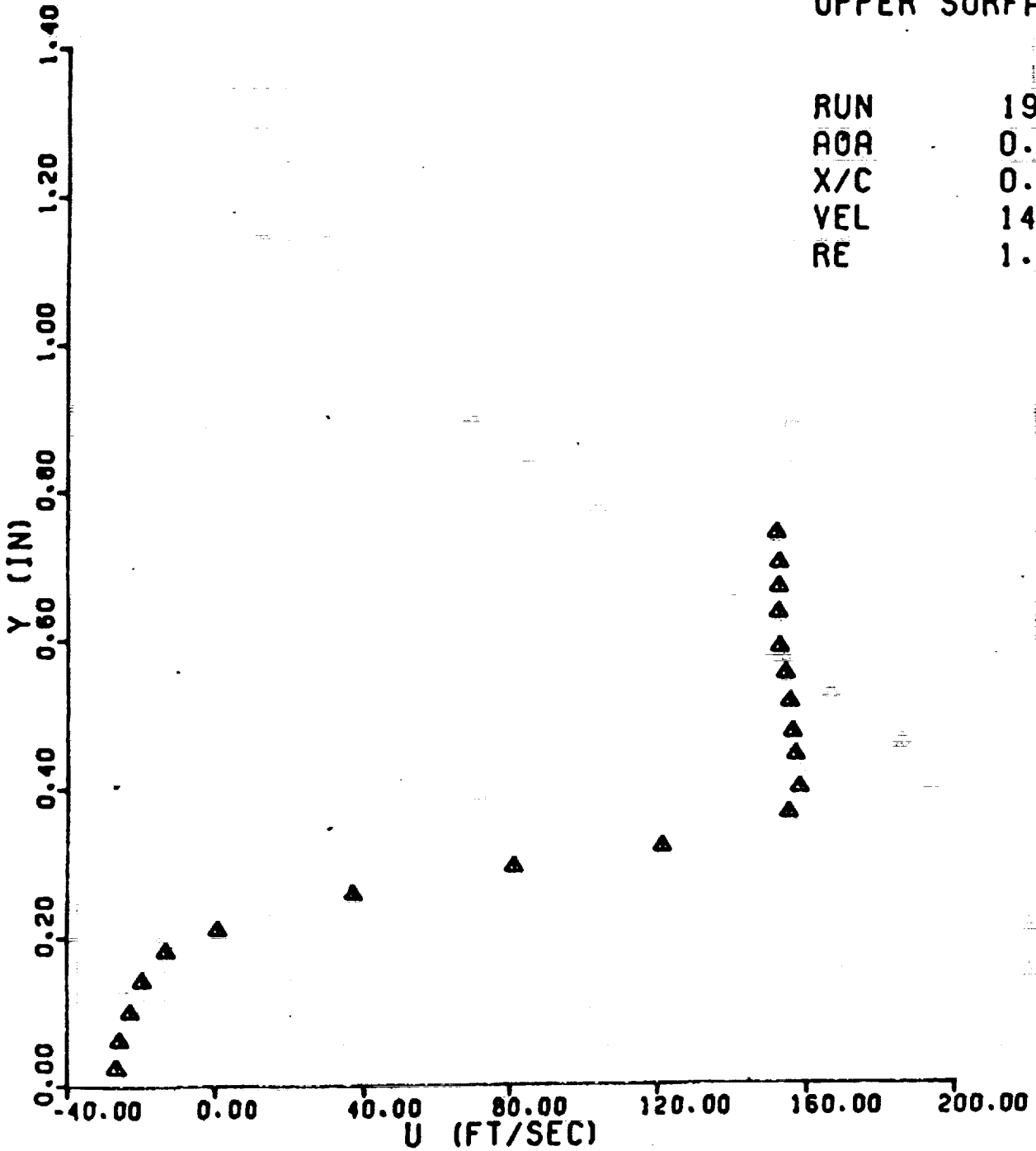
NACA 0012
UPPER SURFACE



RUN 1927
AOA 10.000
X/C 0.5000
VEL 135.3
RE 1.59

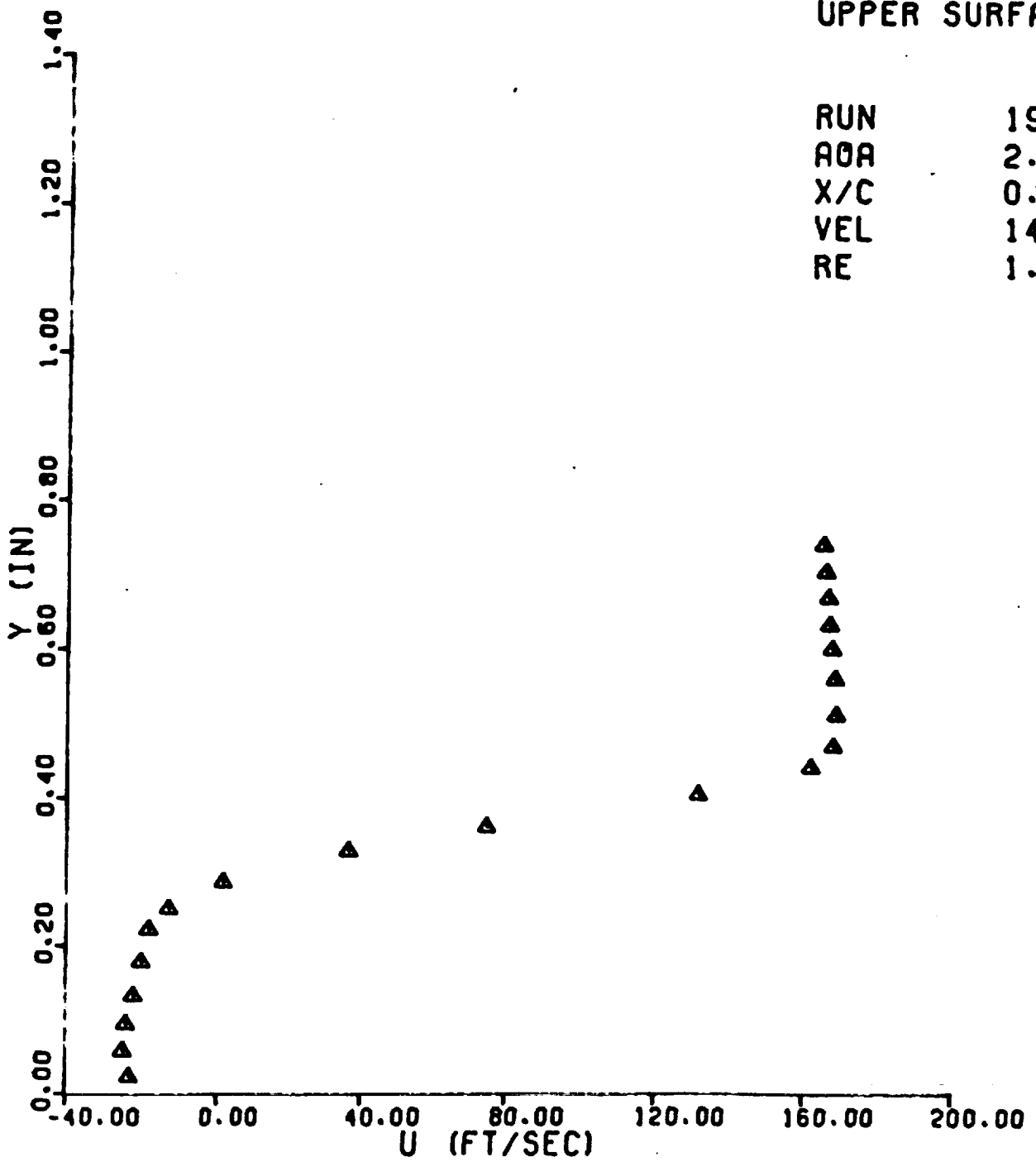
NACA 0012
UPPER SURFACE

RUN	1928
AOA	0.000
X/C	0.0000
VEL	140.5
RE	1.58

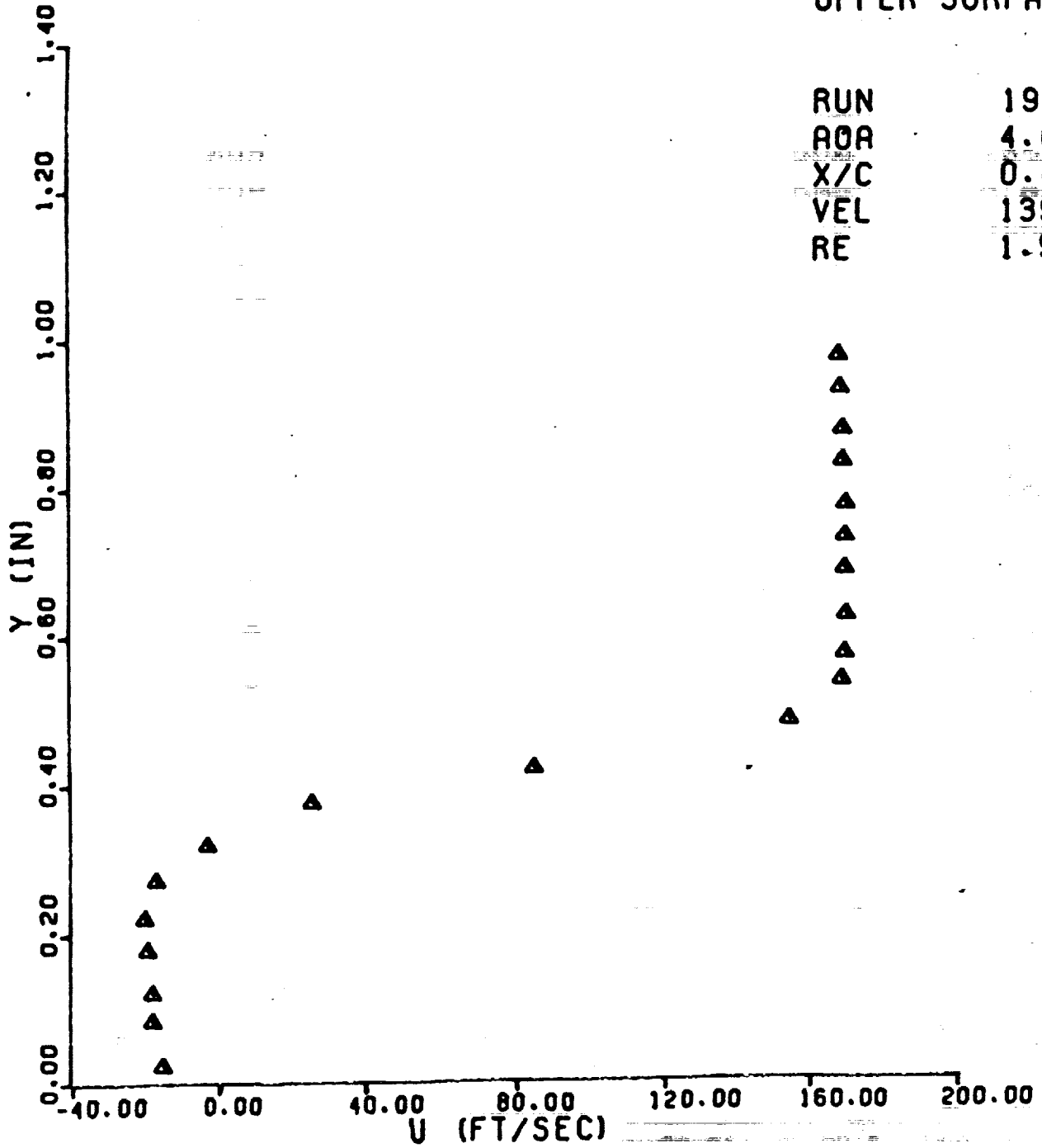


NACA 0012
UPPER SURFACE

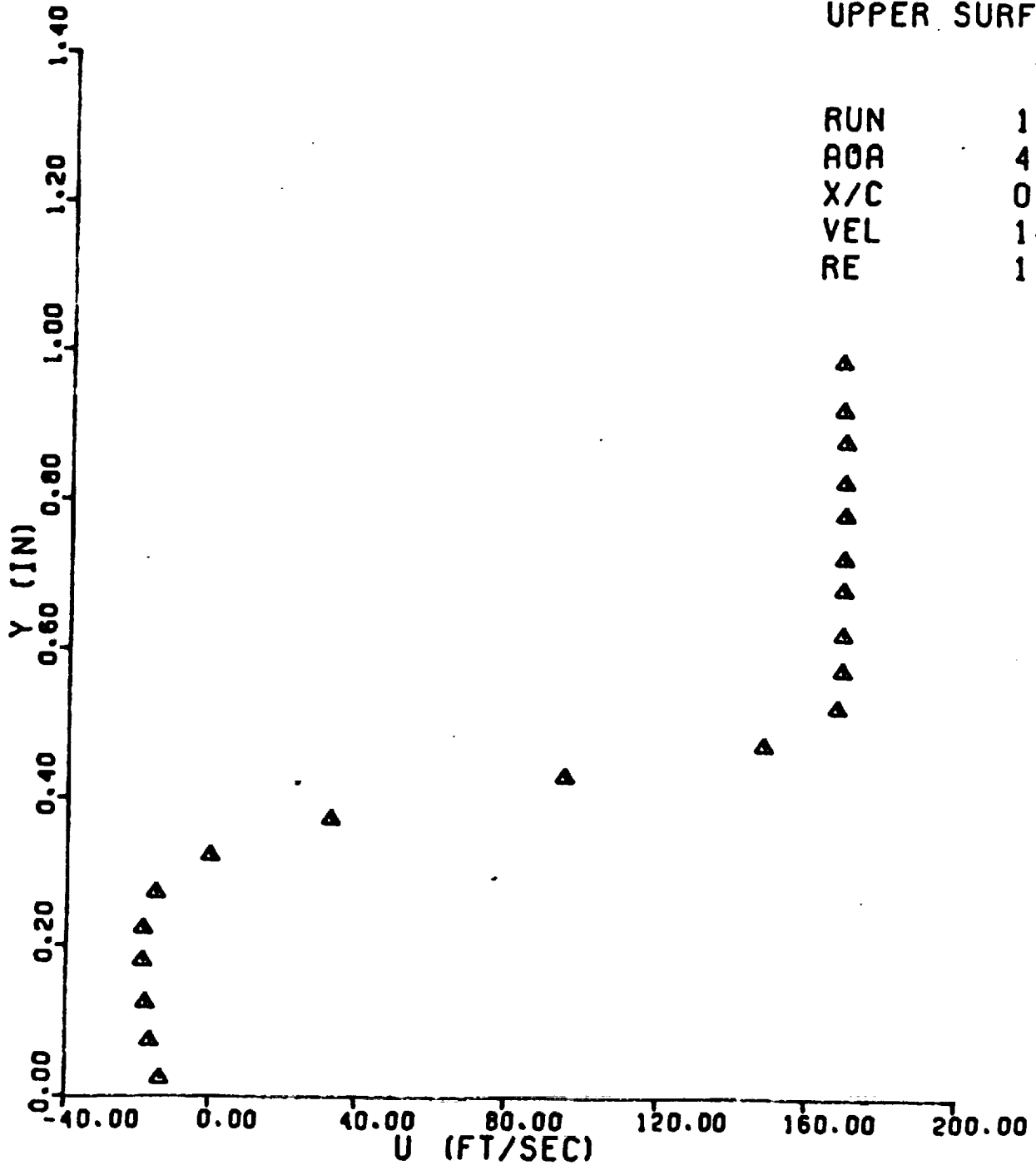
RUN 1929
AOA 2.000
X/C 0.0000
VEL 140.1
RE 1.58



NACA 0012
UPPER SURFACE



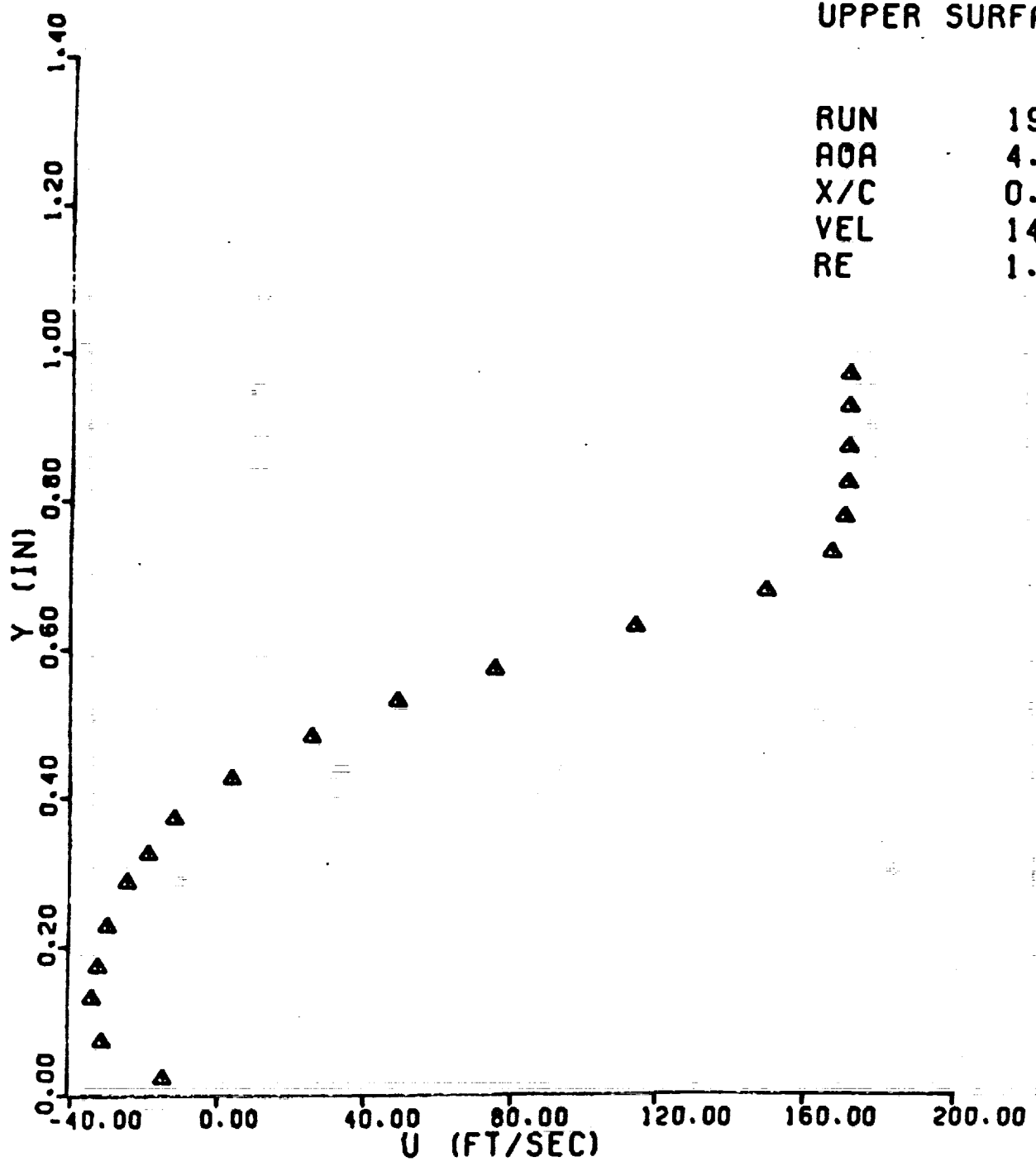
NACA 0012
UPPER SURFACE



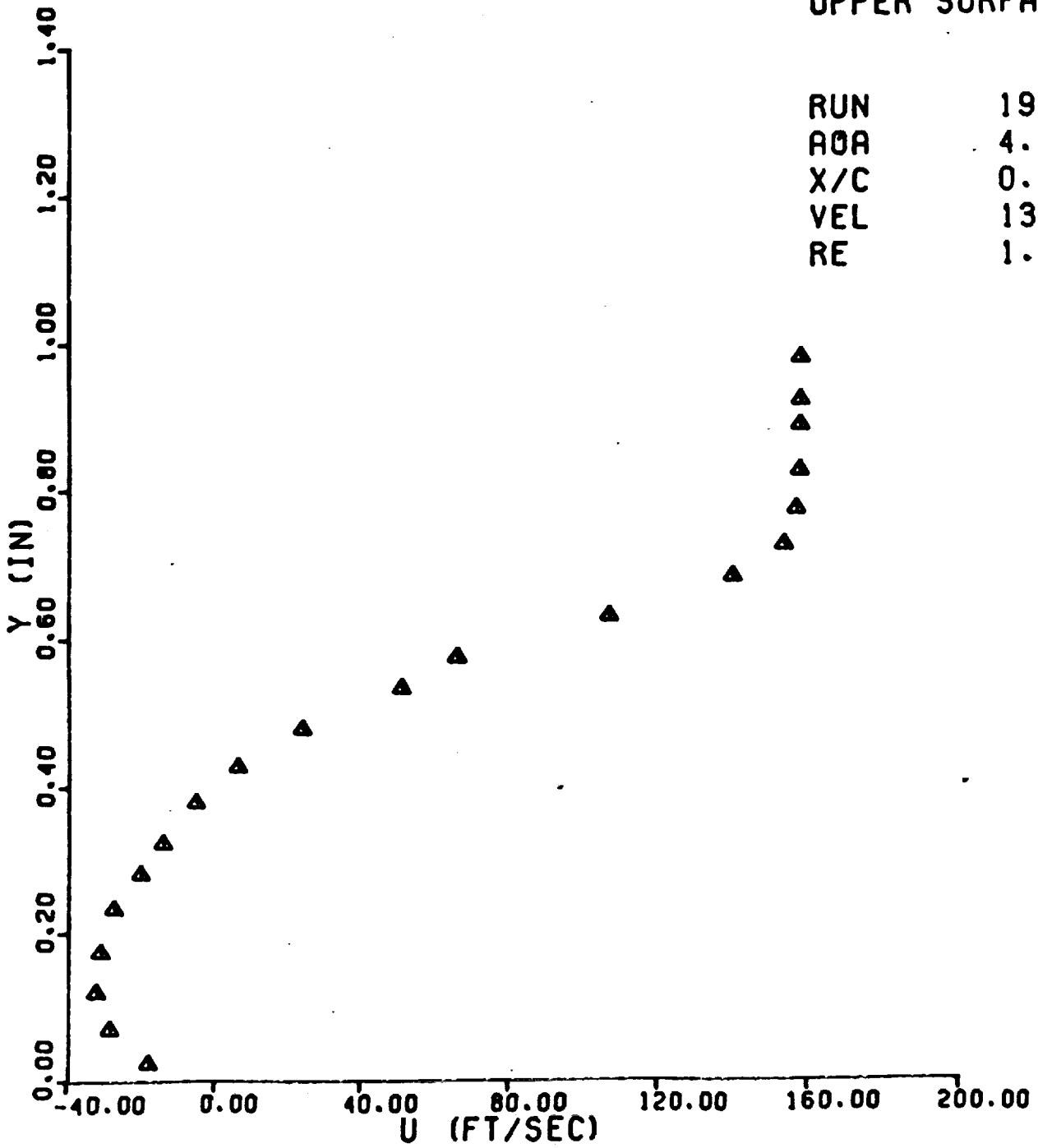
RUN 1931
 AOA 4.000
 X/C 0.0000
 VEL 140.5
 RE 1.58

NACA 0012
UPPER SURFACE

RUN 1932
AOA 4.000
X/C 0.0400
VEL 140.4
RE 1.58

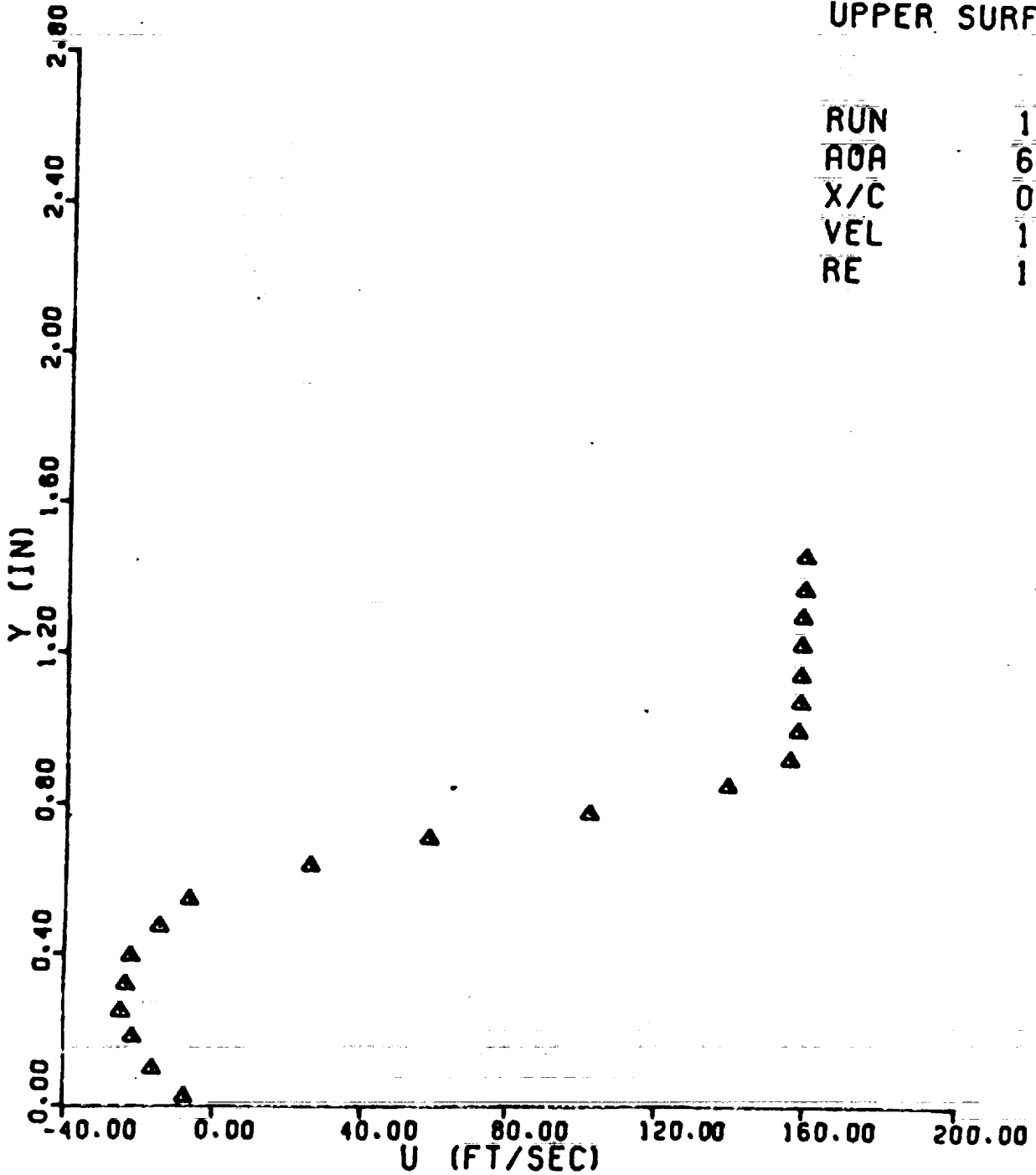


NACA 0012
UPPER SURFACE



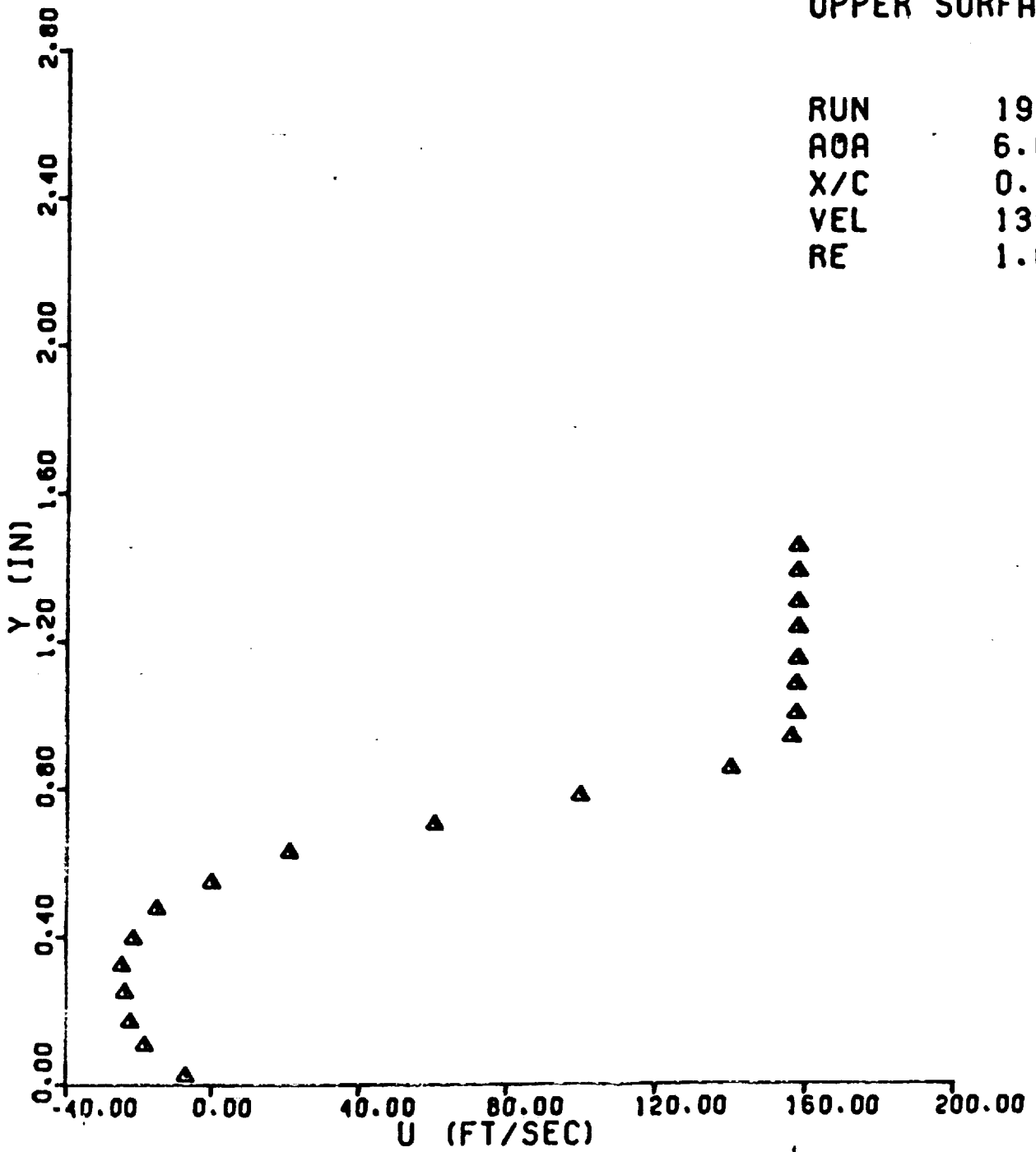
NACA 0012
UPPER SURFACE

RUN	1934
AOA	6.000
X/C	0.0400
VEL	139.5
RE	1.61



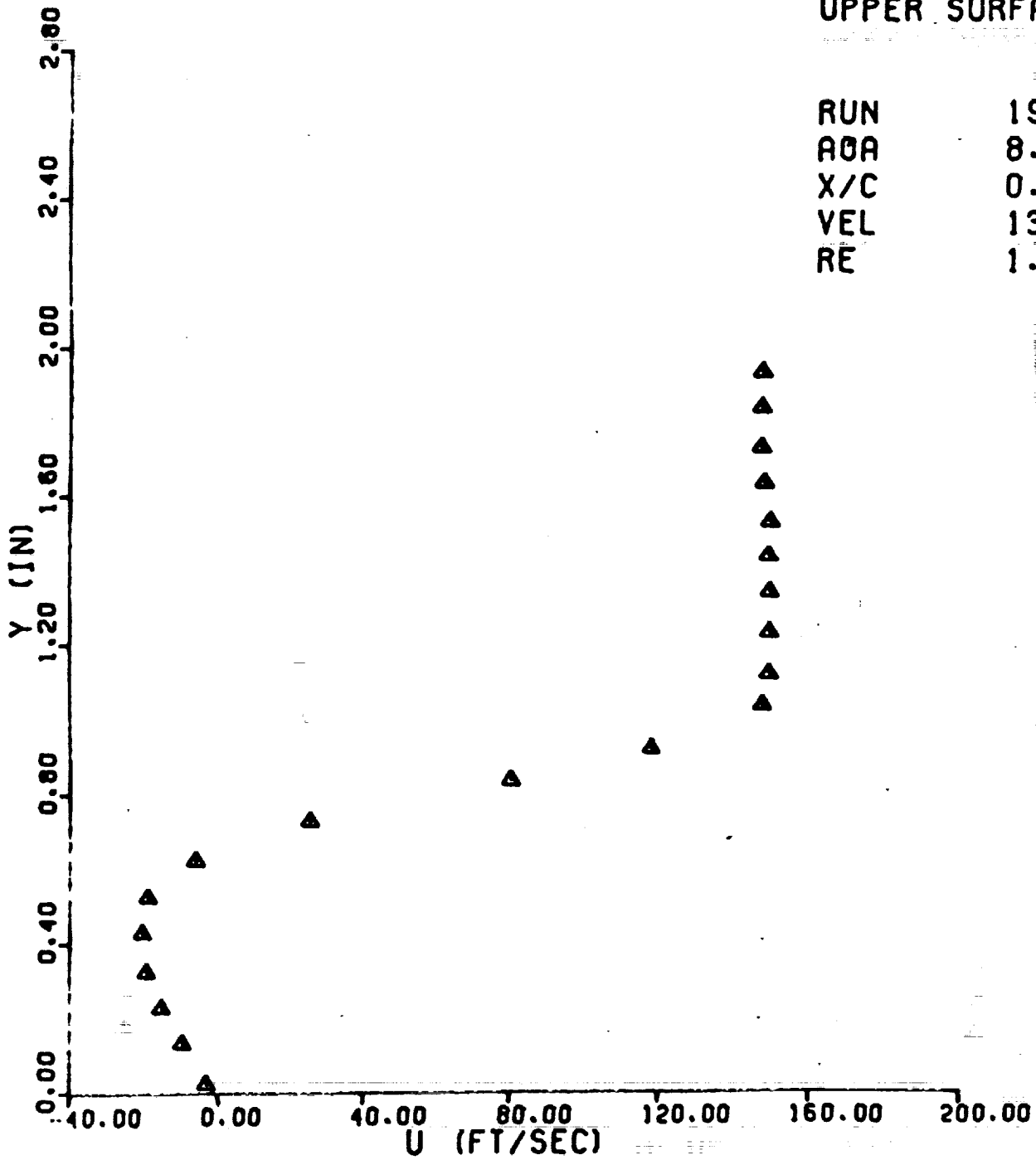
NACA 0012
UPPER SURFACE

RUN	1935
AOA	6.000
X/C	0.0400
VEL	139.3
RE	1.61



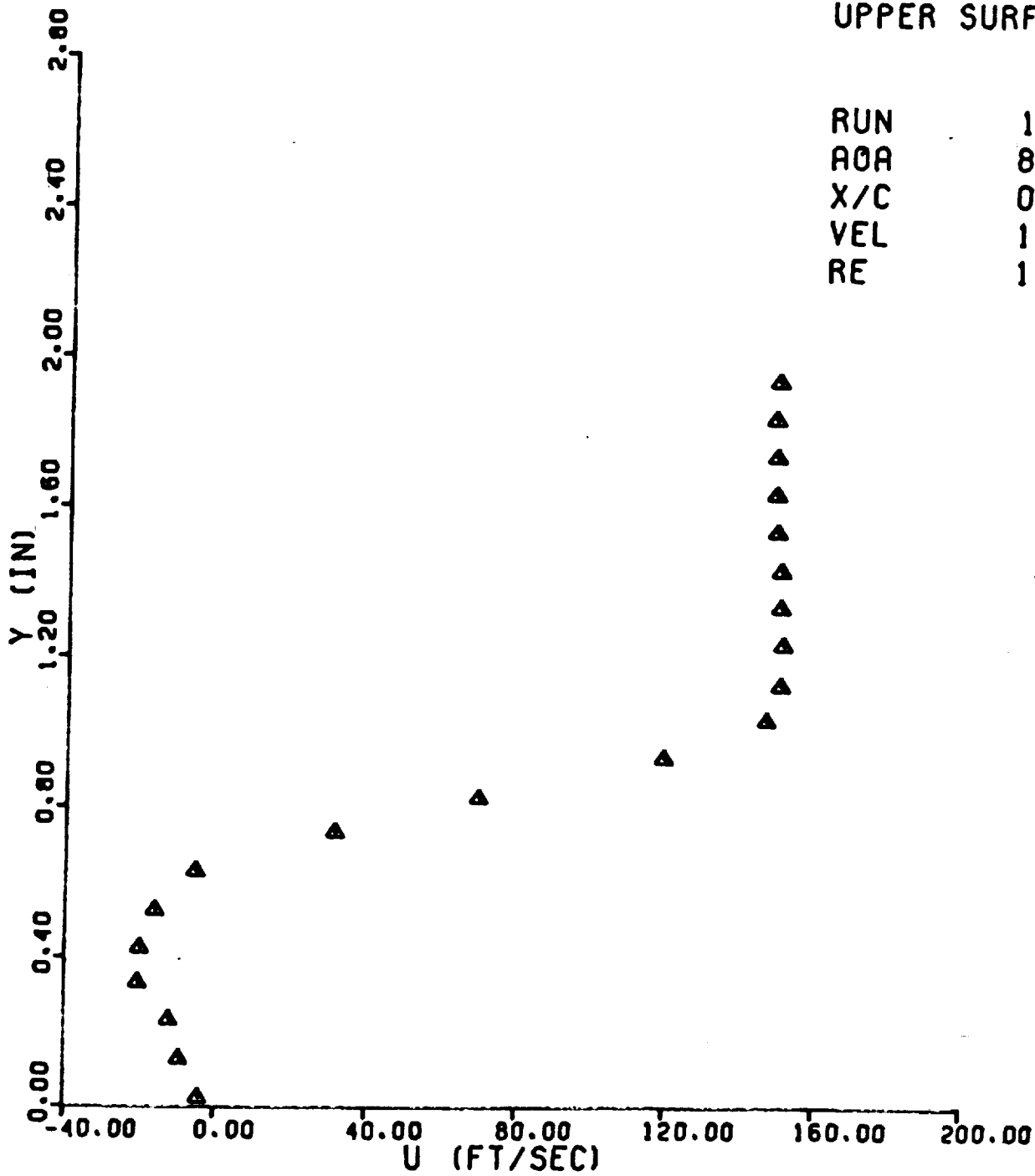
NACA 0012
UPPER SURFACE

RUN 1936
AOA 8.000
X/C 0.0400
VEL 136.9
RE 1.58



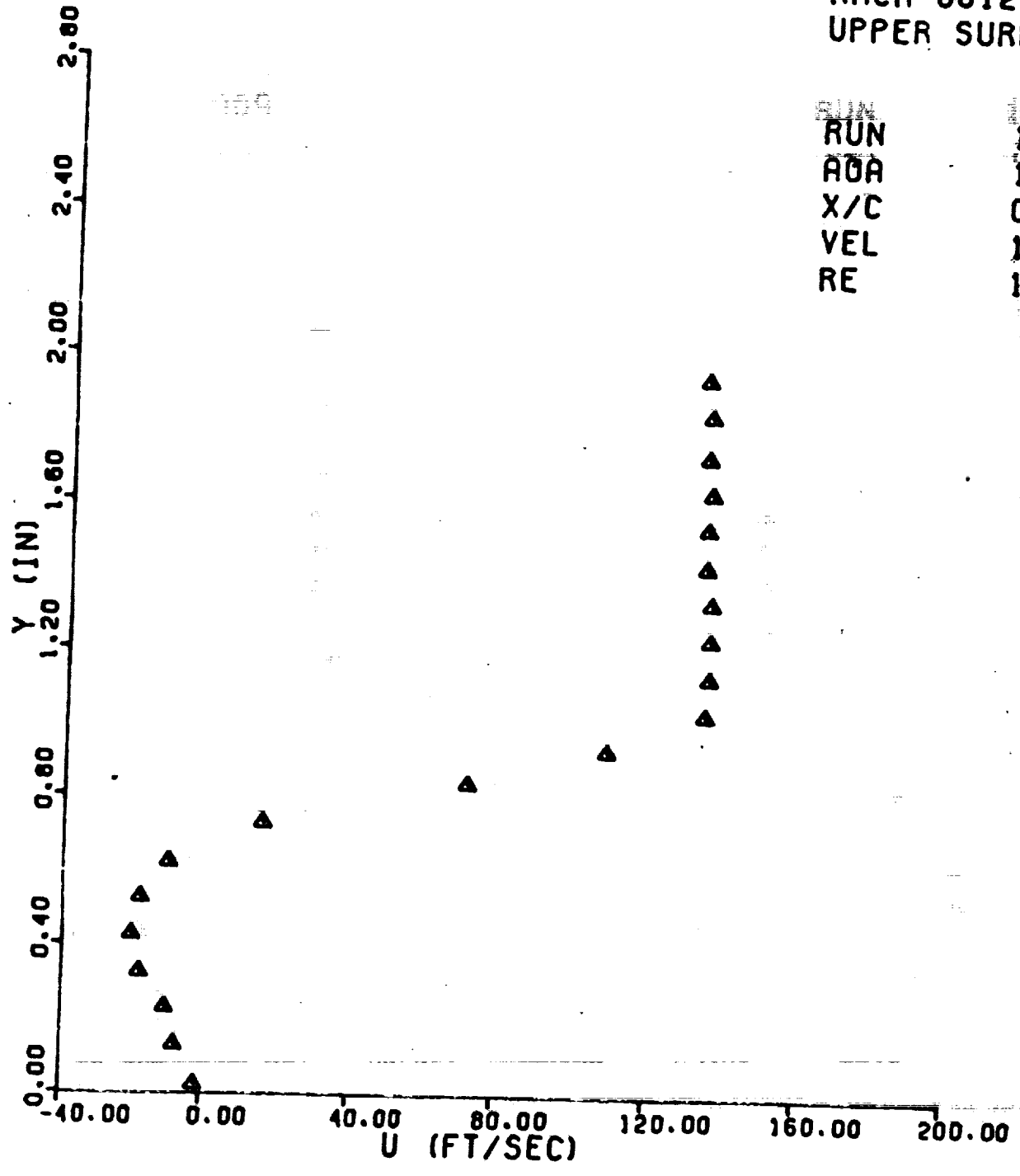
NACA 0012
UPPER SURFACE

RUN 1937
AOA 8.000
X/C 0.0400
VEL 135.4
RE 1.56



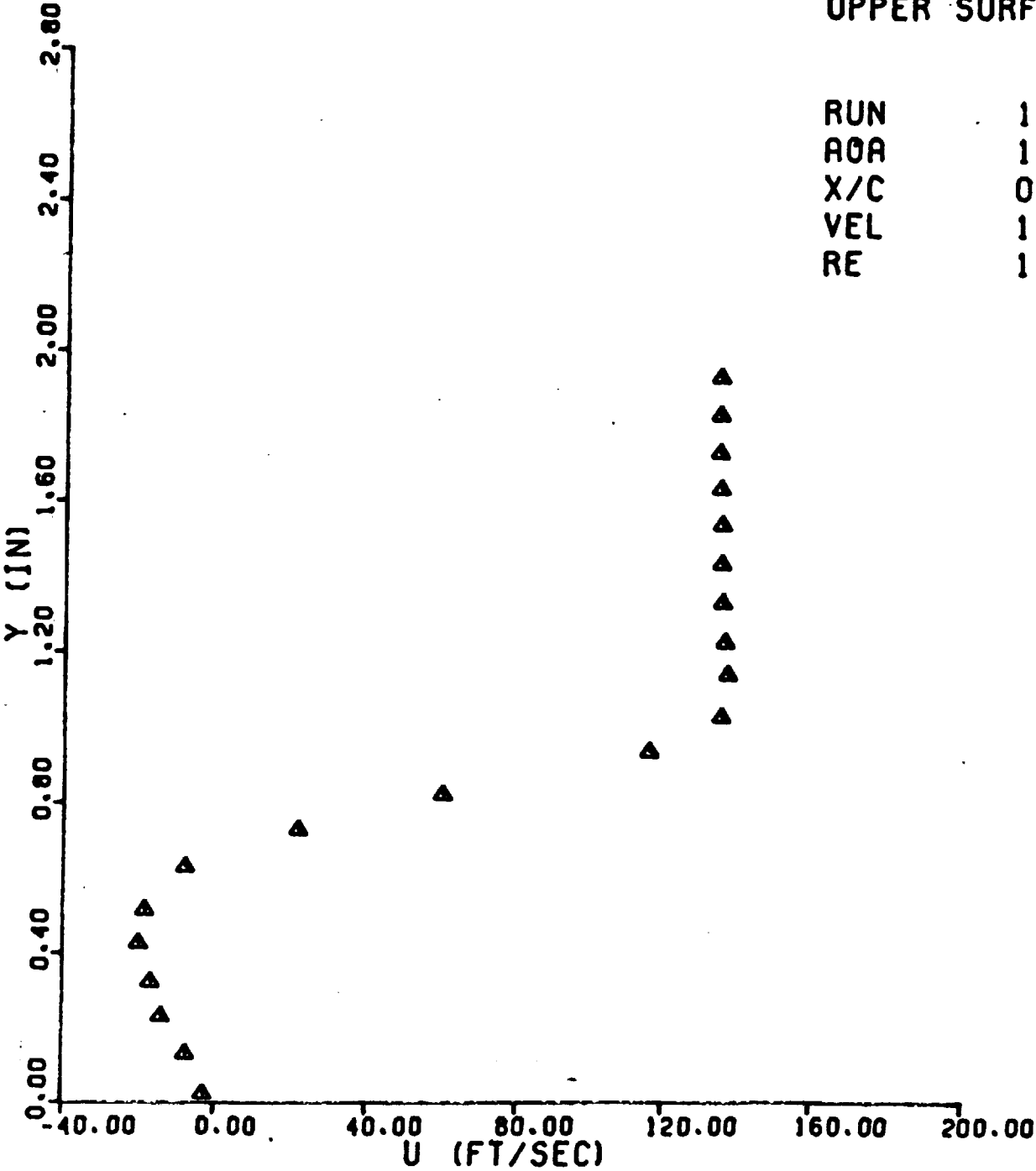
NACA 0012
UPPER SURFACE

RUN	1938
AOA	10.000
X/C	0.0400
VEL	135.1
RE	1.56



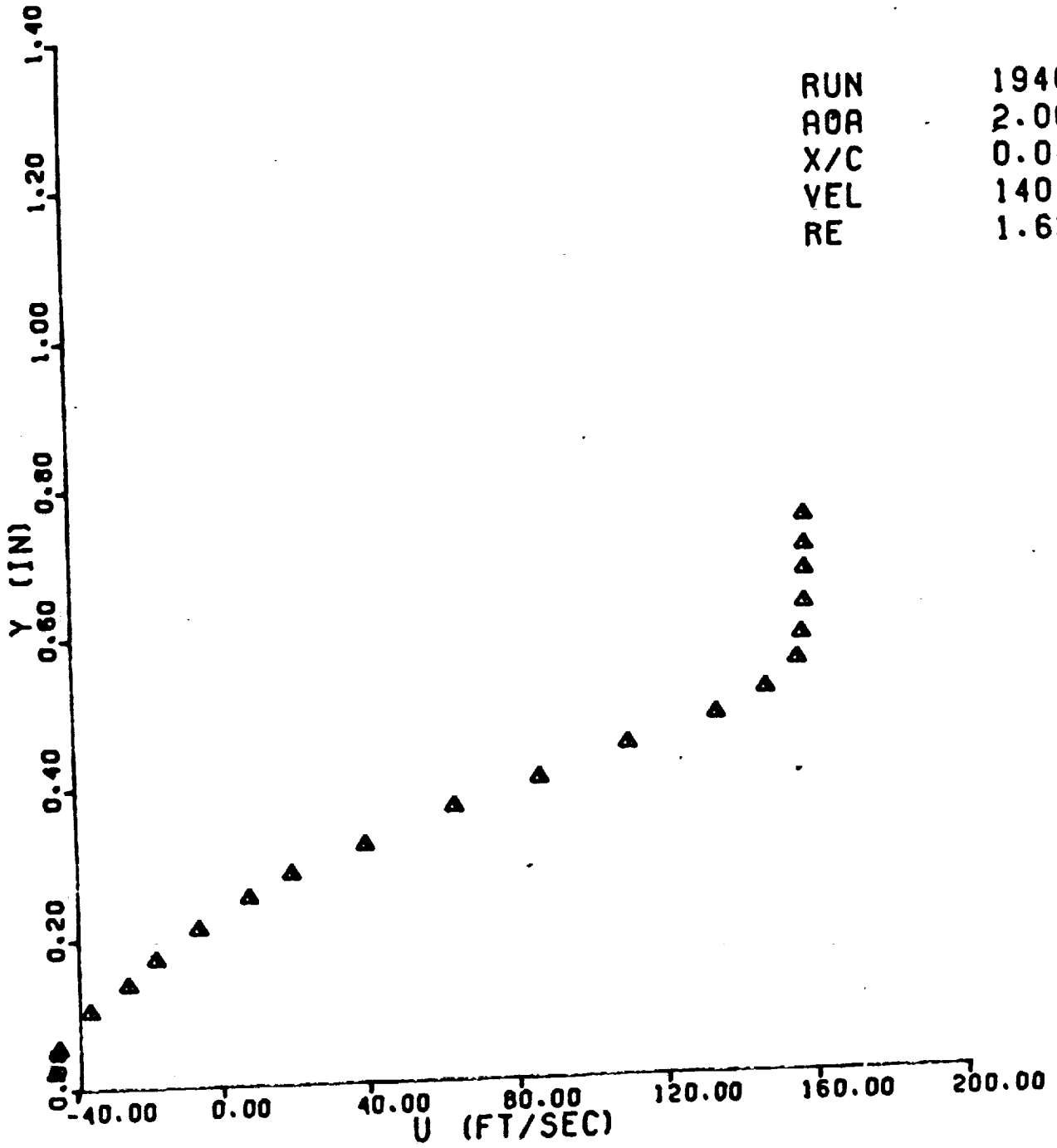
NACA 0012
UPPER SURFACE

RUN 1939
AOA 10.000
X/C 0.0400
VEL 134.3
RE 1.55



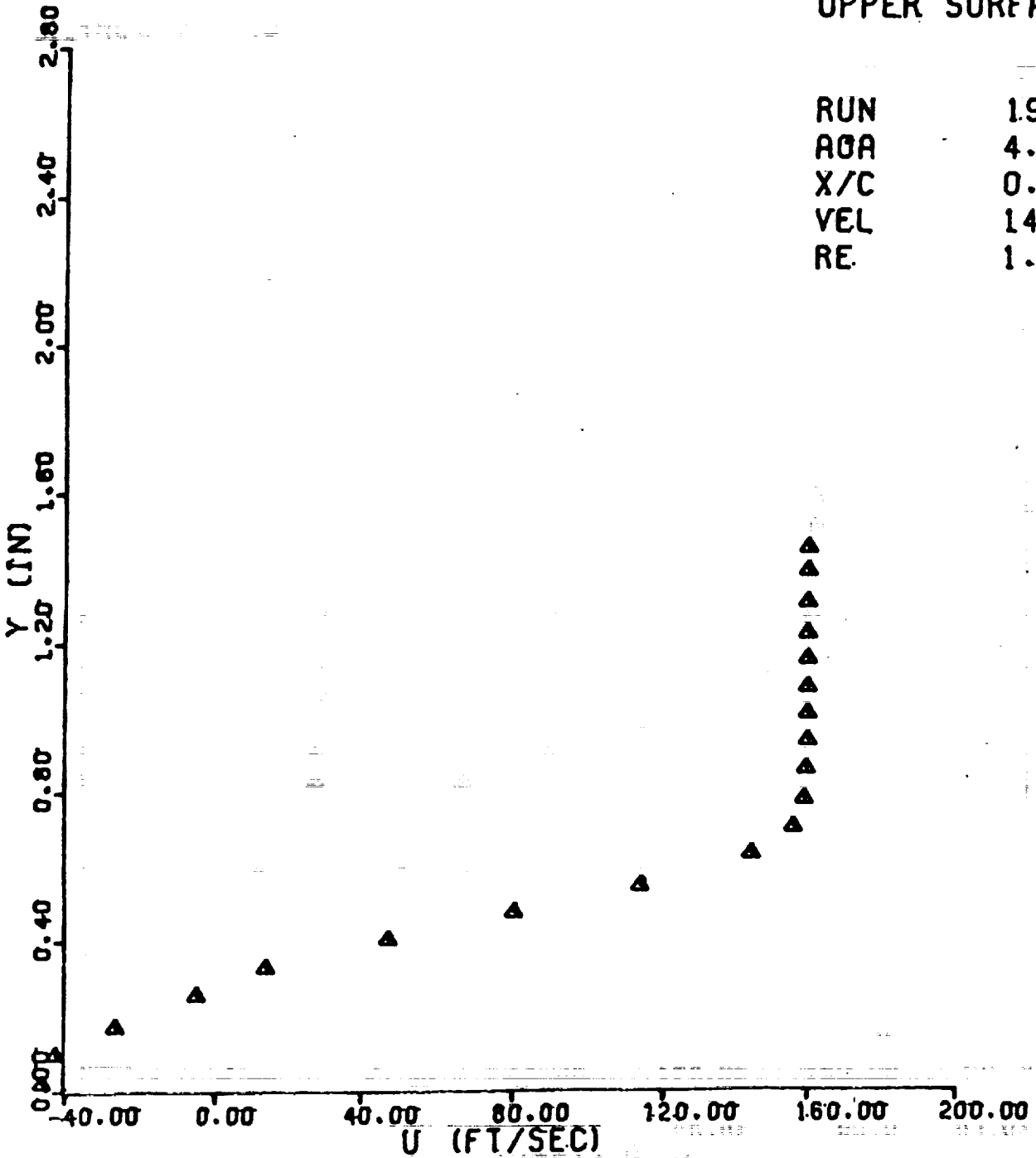
NACA 0012
UPPER SURFACE

RUN	1940
AOA	2.000
X/C	0.0400
VEL	140.0
RE	1.62



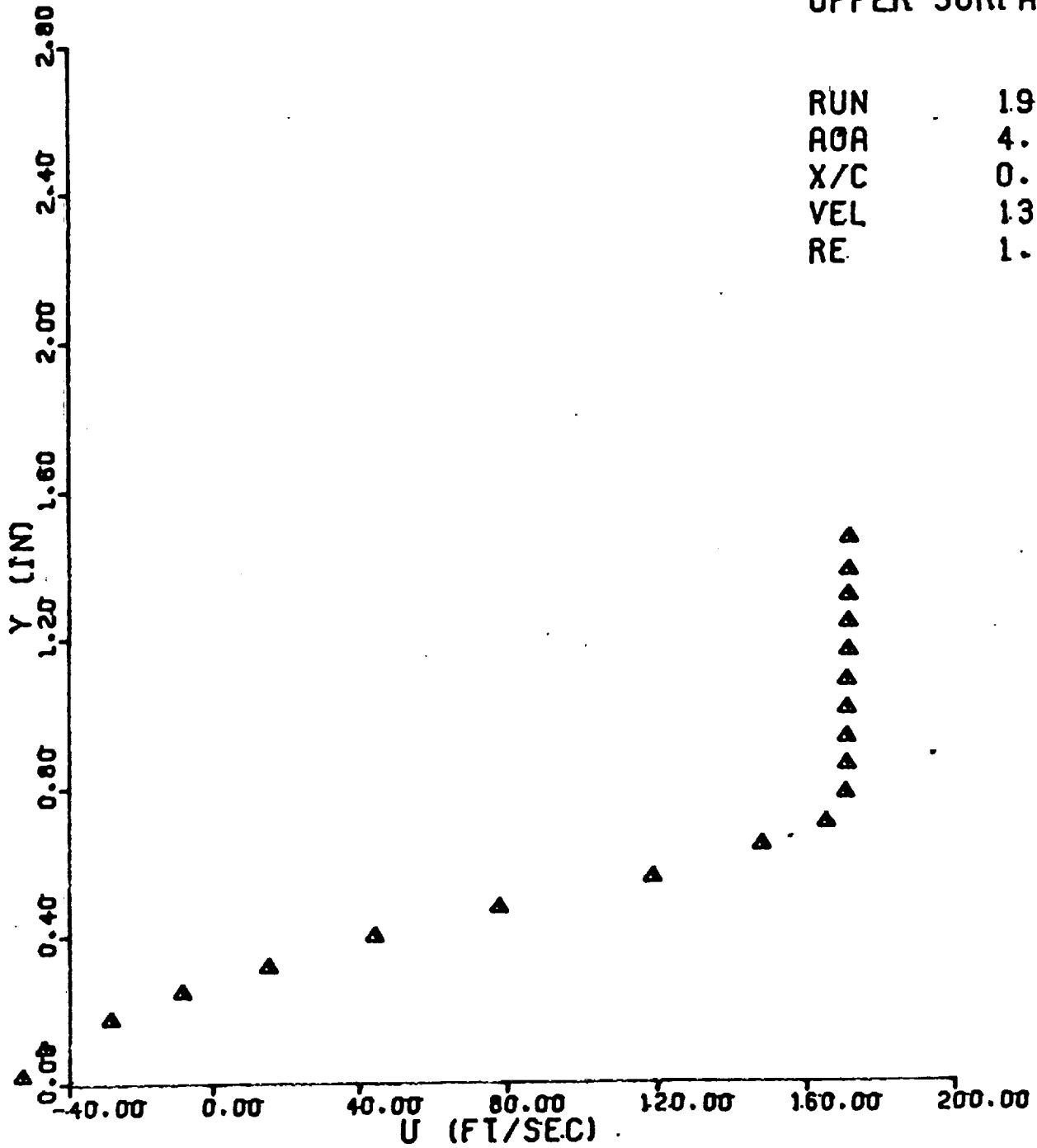
NACA 0012
UPPER SURFACE

RUN 1942
AOA 4.000
X/C 0.0800
VEL 140.2
RE 1.62

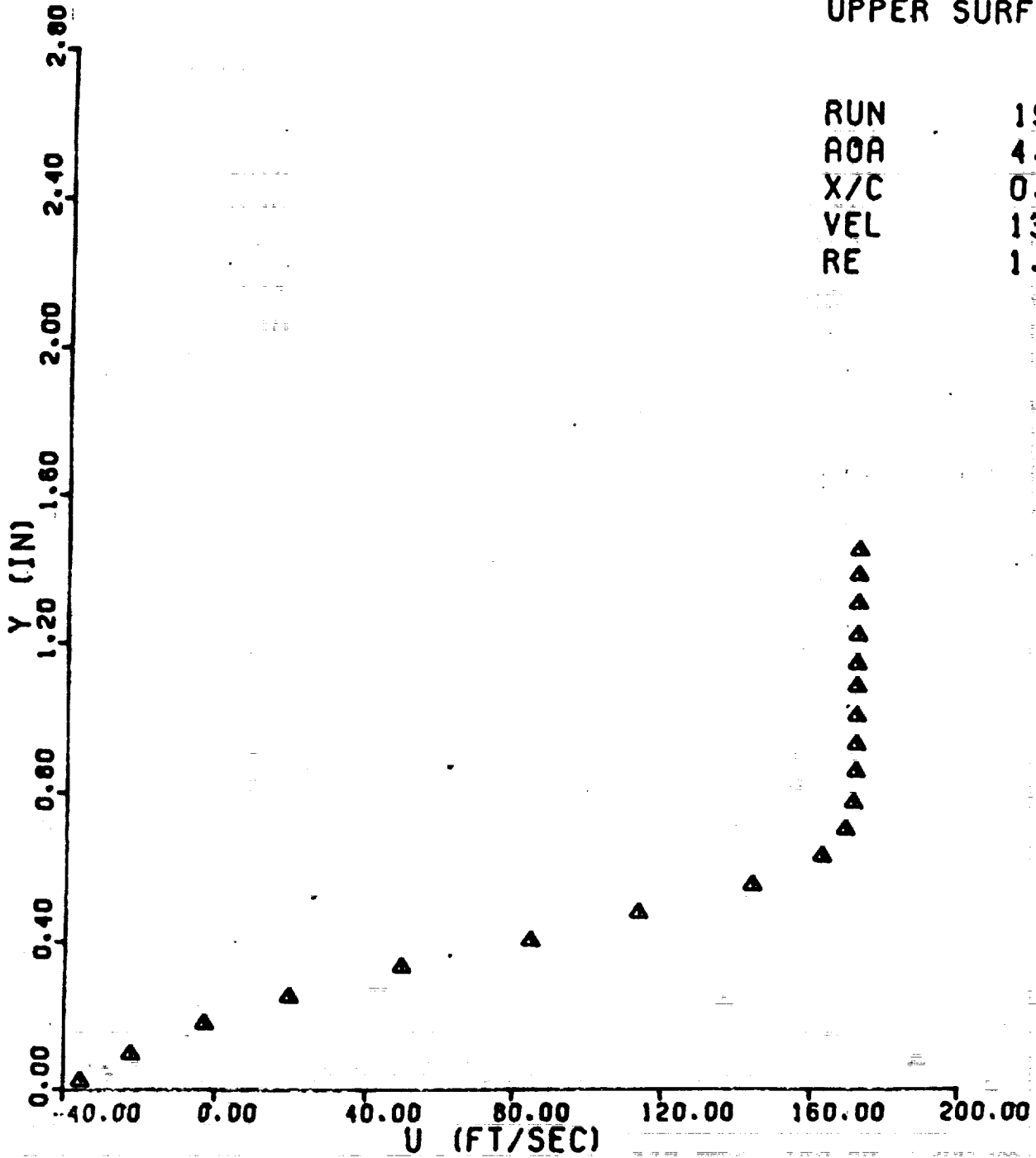


NACA 0012
UPPER SURFACE

RUN	1944
AOA	4.000
X/C	0.0800
VEL	138.9
RE	1.55



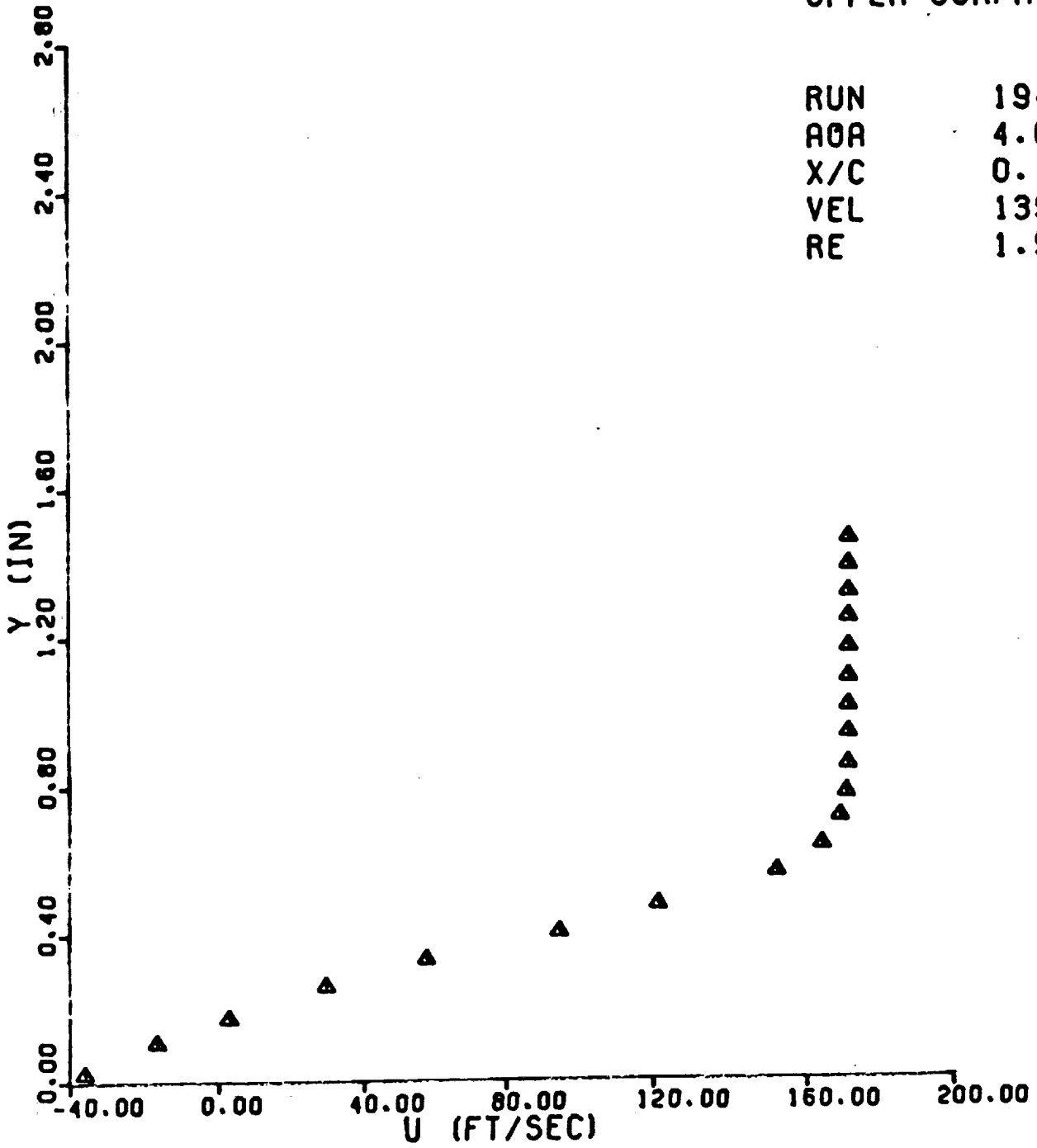
NACA 0012
UPPER SURFACE



RUN	1946
AOA	4.000
X/C	0.1200
VEL	138.6
RE	1.55

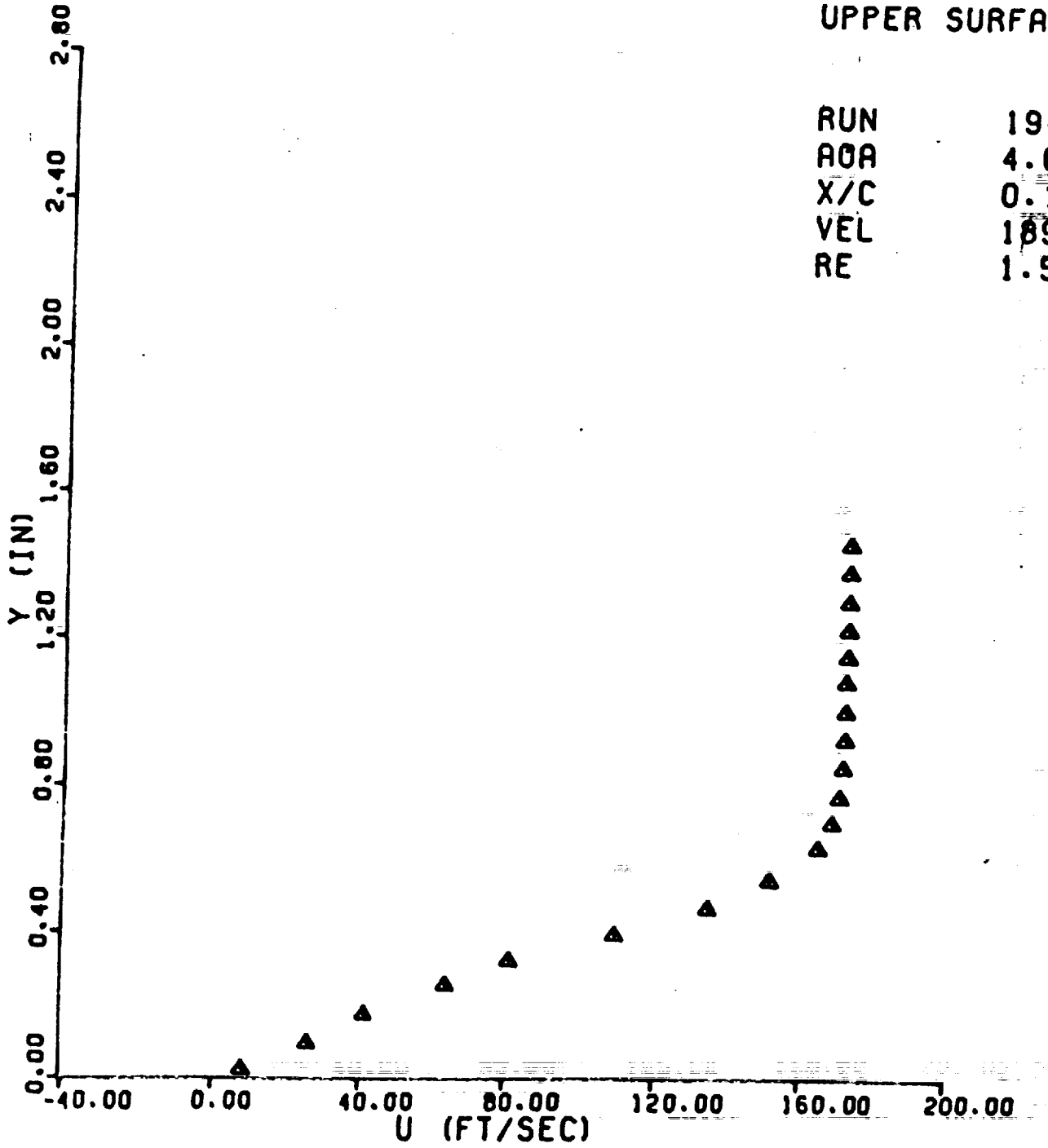
NACA 0012
UPPER SURFACE

RUN	1947
AOA	4.000
X/C	0.1200
VEL	139.1
RE	1.55



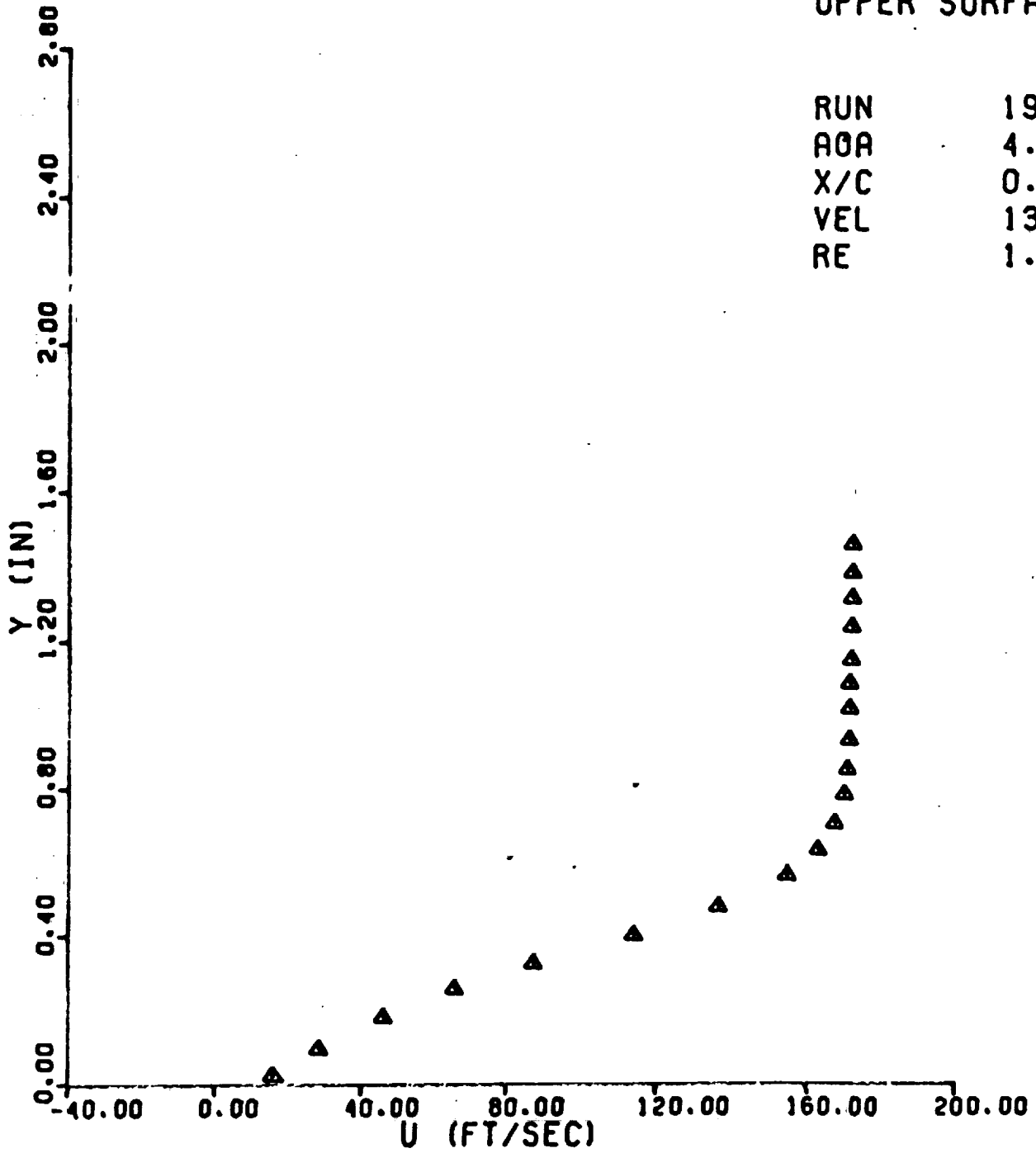
NACA 0012
UPPER SURFACE

RUN 1948
AOA 4.000
X/C 0.1600
VEL 189.6
RE 1.56



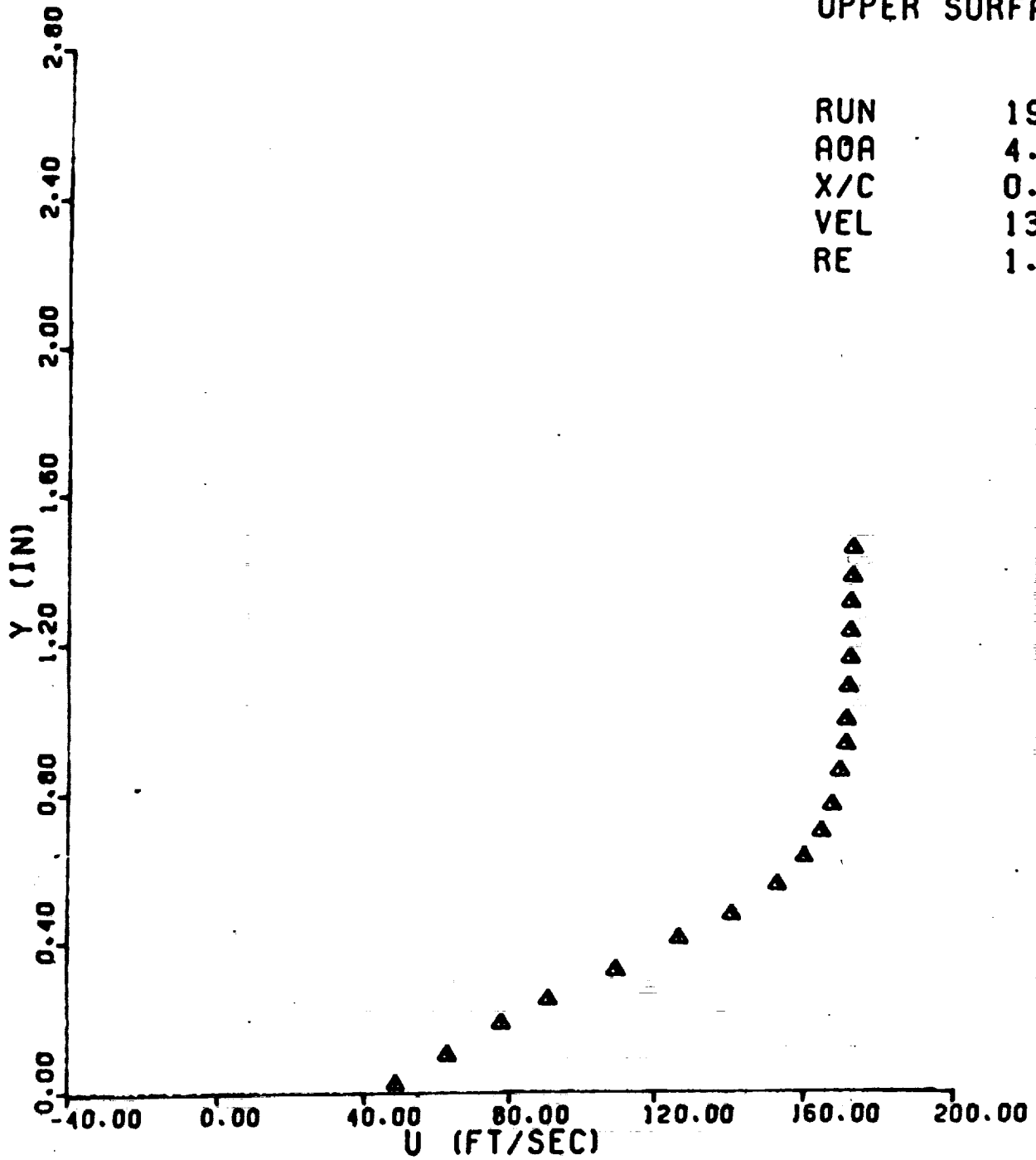
NACA 0012
UPPER SURFACE

RUN	1949
AOA	4.000
X/C	0.1600
VEL	138.5
RE	1.55



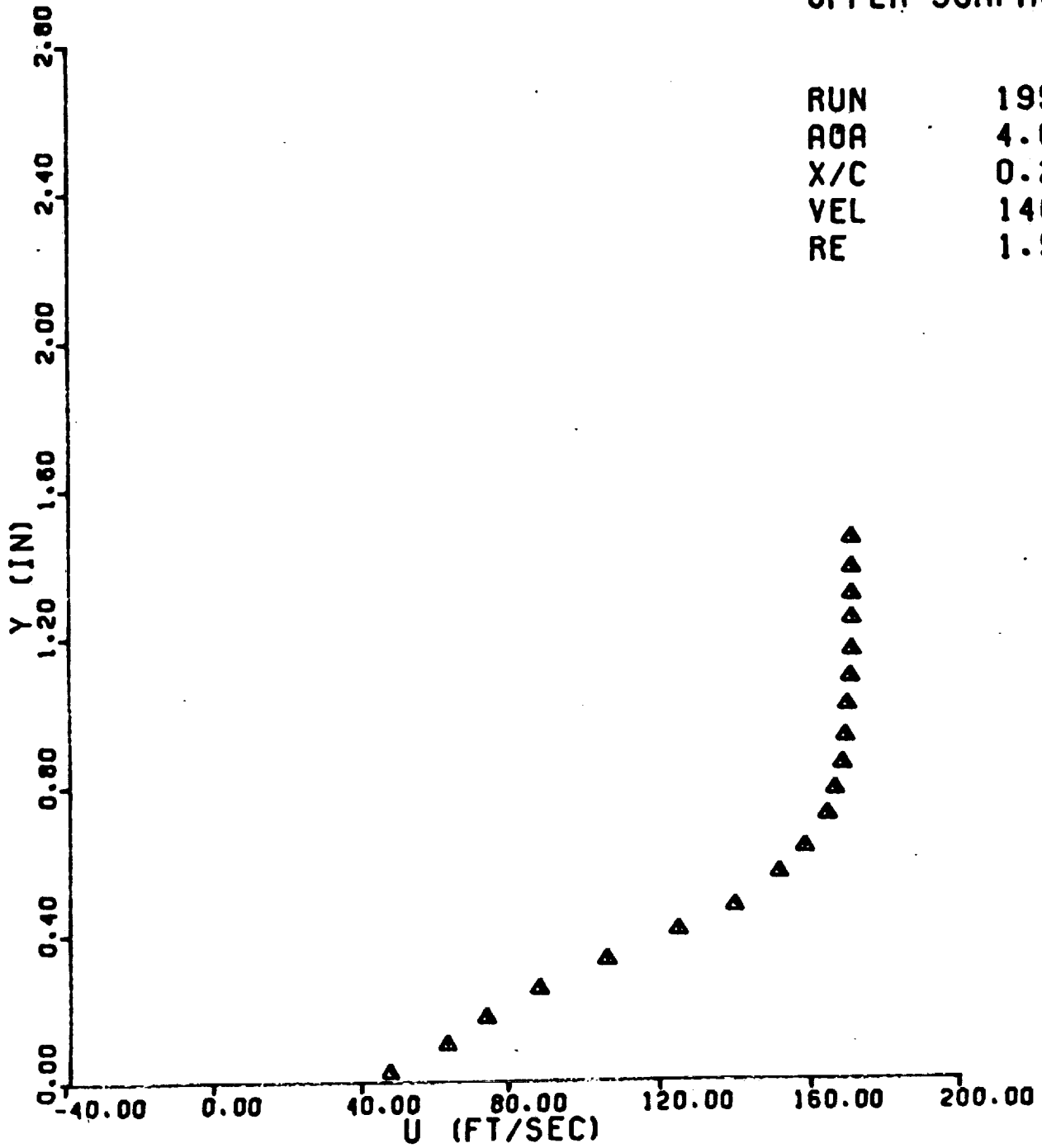
NACA 0012
UPPER SURFACE

RUN	1950
AOA	4.000
X/C	0.2000
VEL	138.5
RE	1.55



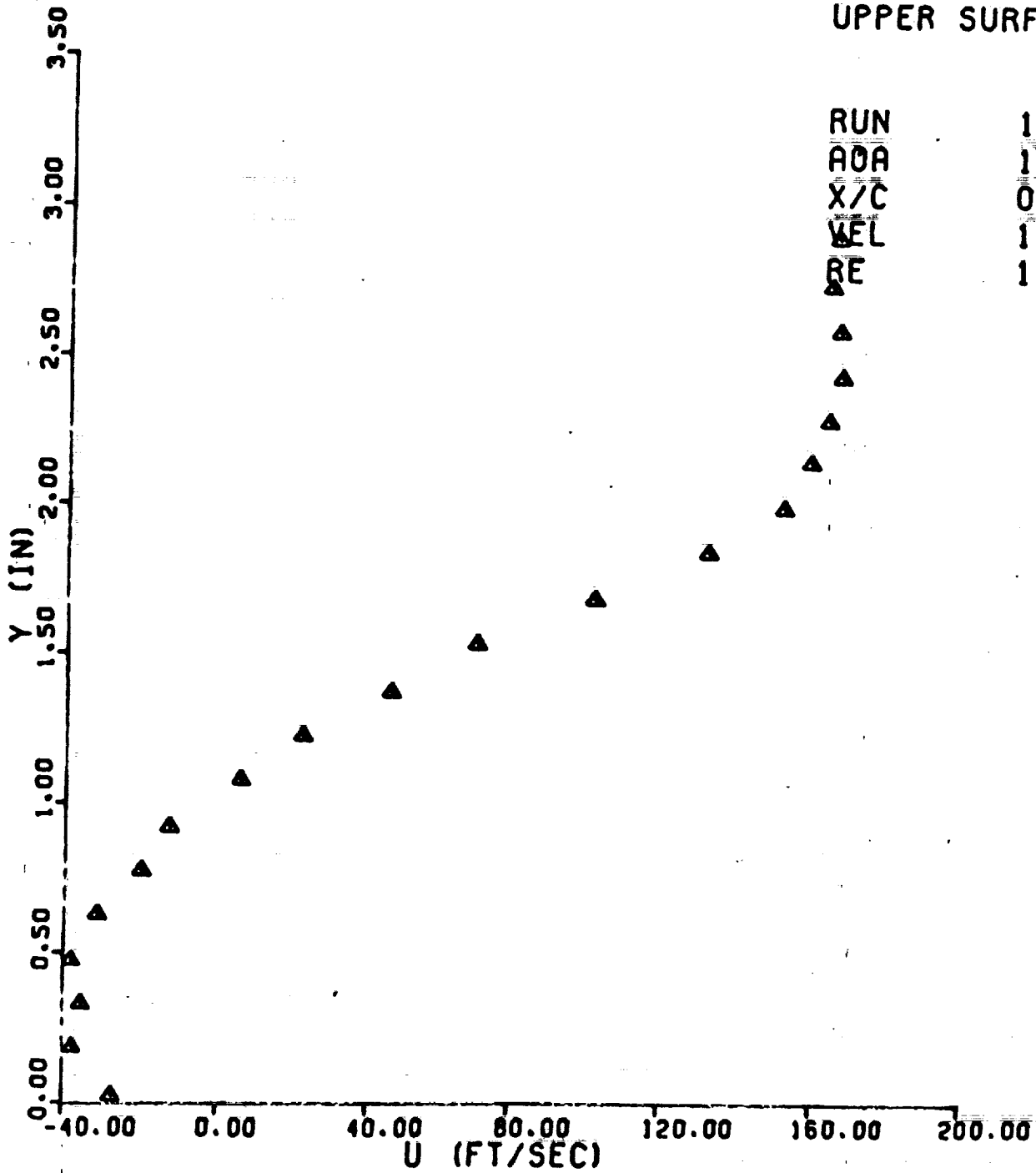
NACA 0012
UPPER SURFACE

RUN 1951
AOA 4.000
X/C 0.2000
VEL 140.1
RE 1.56

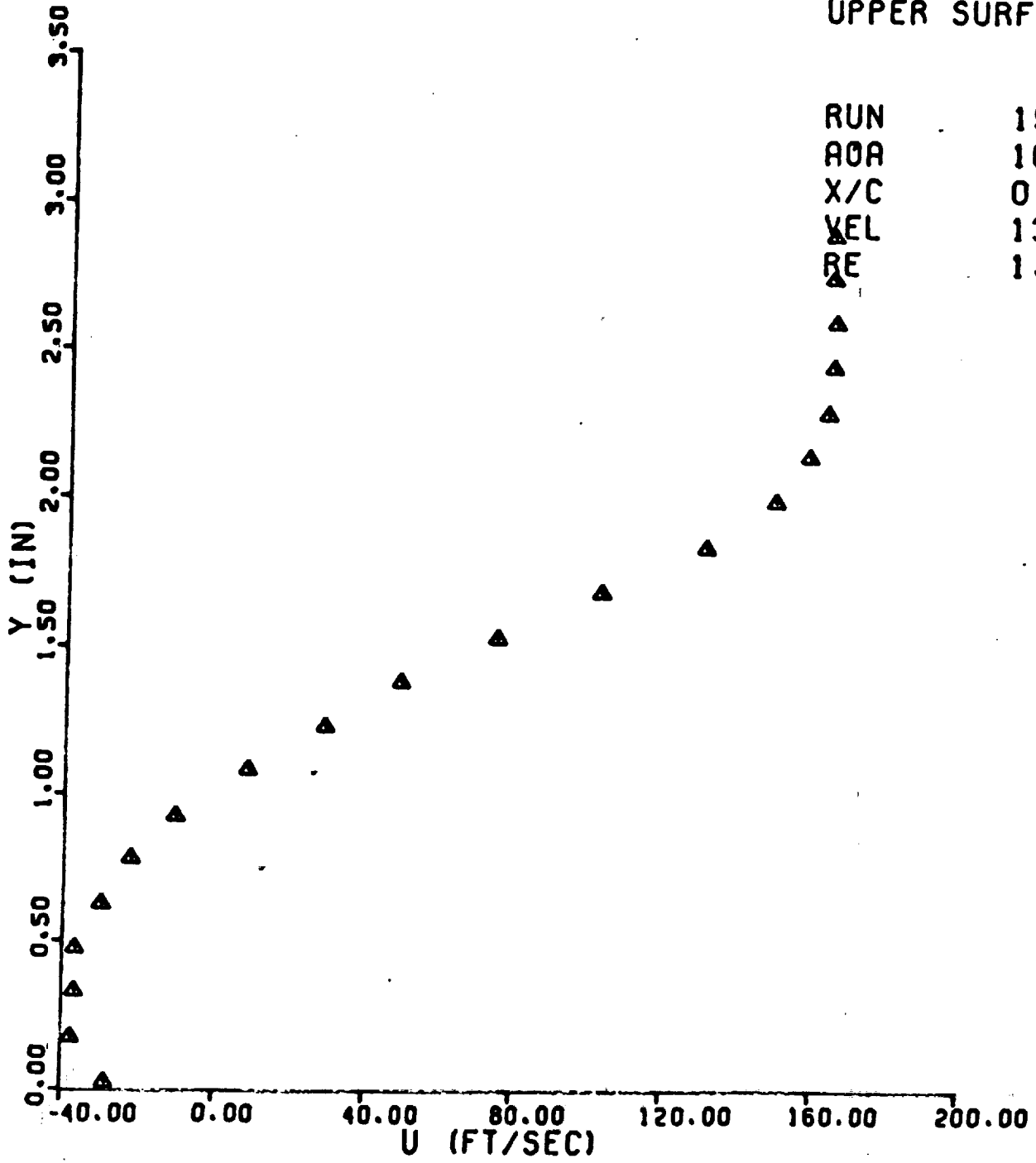


NACA 0012
UPPER SURFACE

RUN 1952
AOA 10.000
X/C 0.2000
VEL 133.7
RE 1.49



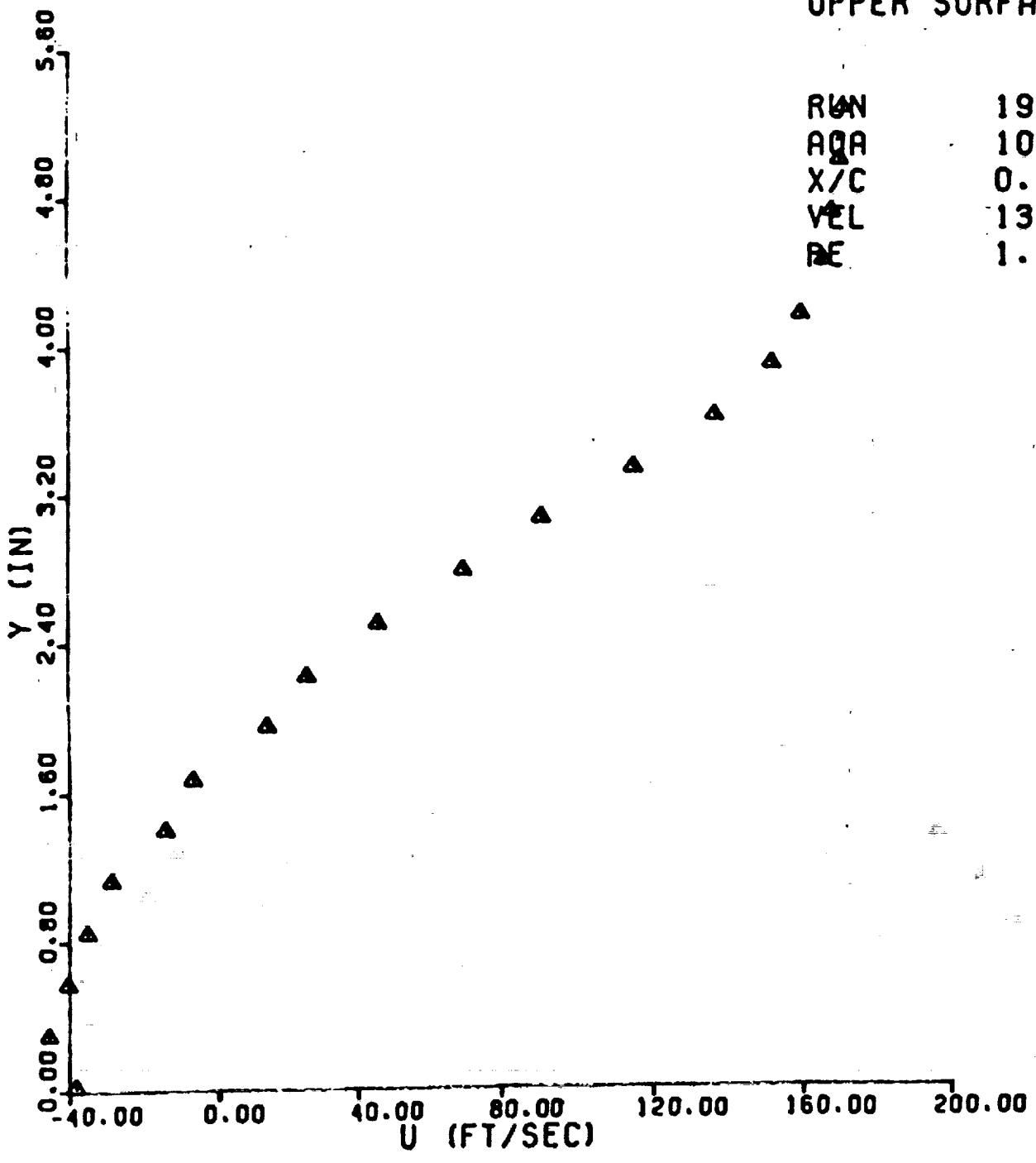
NACA 0012
UPPER SURFACE



RUN 1953
AOA 10.000
X/C 0.2000
VEL 133.4
RE 1.49

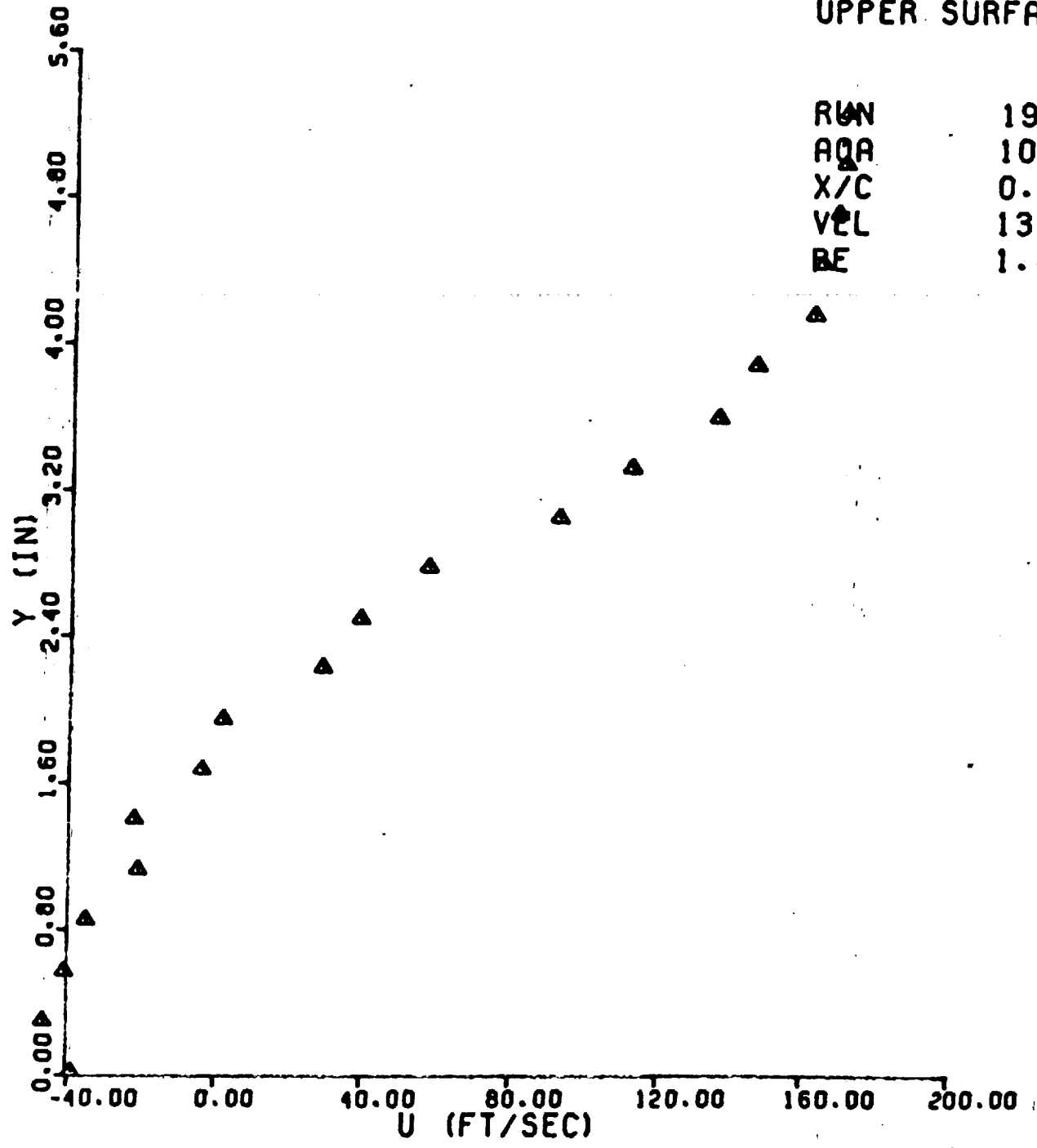
NACA 0012
UPPER SURFACE

RUN 1954
AOA 10.000
X/C 0.5000
VEL 134.1
RE 1.50



NACA 0012
UPPER SURFACE

RUN 1955
AQA 10.000
X/C 0.5000
VEL 133.8
BE 1.49



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2. Berkowitz, B., private communication, Cleveland, Ohio, August 28, 1987.
3. Bragg, M.B. and Spring, S.A., "An Experimental Study of the Flow Field about an Airfoil with Glaze Ice", AIAA-87-0100, paper presented at the 25th Aerospace Sciences Meeting, Reno, Nevada, January 12-15, 1987.
4. Bragg, M.B. and Khodadoust, A., "Experimental Measurements in a Large Separation Bubble Due to a Simulated Glaze Ice Accretion", AIAA-88-0116, paper presented at the 26th Aerospace Sciences Meeting, Reno, Nevada, January 11-14, 1988.
5. Spring, S.A., "An Experimental Mapping of the Flow Field Behind a Glaze Ice Shape on a NACA 0012 Airfoil", M.S. thesis, Ohio State University, June 1987 or NASA CR 180847, January 1988..
6. Khodadoust, A., "A Flow Visualization Study of the Leading Edge Separation Bubble on a NACA 0012 Airfoil with Simulated Glaze Ice", M.S. thesis, Ohio State University, June 1987 or NASA CR 180846, January 1988.
7. Rae, W.H., Jr. and Pope, A., "Low-Speed Wind Tunnel Testing", 2nd ed., John Wiley and Sons, New York, 1984.

APPENDIX A:
LEWICE GENERATED ICE SHAPE DATA

TABLE A-1 NACA 0012 WITH LEWICE GENERATED
ICE SHAPE

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
1	-0.0397258	0.0209887	-0.0397258	0.0209887
2	-0.0395021	0.0219327	-0.0394368	0.0187739
3	-0.0392784	0.0228768	-0.0391477	0.0165590
4	-0.0371860	0.0264358	-0.0384261	0.0144708
5	-0.0361336	0.0281729	-0.0377044	0.0123827
6	-0.0349663	0.0297330	-0.0370520	0.0118487
7	-0.0337991	0.0312931	-0.0363997	0.0113148
8	-0.0318727	0.0327903	-0.0358748	0.0109145
9	-0.0299463	0.0342875	-0.0353499	0.0105142
10	-0.0260944	0.0362561	-0.0353385	0.0107334
11	-0.0243584	0.0366475	-0.0354435	0.0109035
12	-0.0226224	0.0370390	-0.0350549	0.0104569
13	-0.0210185	0.0361053	-0.0346663	0.0100104
14	-0.0194146	0.0351717	-0.0342506	0.0097410
15	-0.0176209	0.0332288	-0.0338380	0.0094130
16	-0.0158271	0.0312859	-0.0331251	0.0085507
17	-0.0132960	0.0296543	-0.0326558	0.0080585
18	-0.0113360	0.0302507	-0.0321865	0.0075664
19	-0.0093761	0.0308472	-0.0318099	0.0075295
20	-0.0084920	0.0294908	-0.0318234	0.0075901
21	-0.0076084	0.0281344	-0.0313443	0.0067959
22	-0.0067246	0.0267780	-0.0311566	0.0065360
23	-0.0058408	0.0254216	-0.0309690	0.0062762
24	-0.0012267	0.0205534	-0.0306249	0.0058211
25	0.0027277	0.0202355	-0.0304601	0.0056235
26	0.0058190	0.0192381	-0.0302954	0.0054260
27	0.0084181	0.0190704	-0.0300480	0.0051661
28	0.0150000	0.0207970	-0.0297849	0.0048846
29	0.0200000	0.0237260	-0.0294323	0.0045890
30	0.0250000	0.0262300	-0.0290796	0.0042935
31	0.0300000	0.0284620	-0.0288989	0.0040803

TABLE A-1 (Cont.)

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
32	0.0350000	0.0304960	-0.0287181	0.0038671
33	0.0400000	0.0323620	-0.0278992	0.0036483
34	0.0450000	0.0340820	-0.0270803	0.0034296
35	0.0500000	0.0356740	-0.0274596	0.0032822
36	0.0600000	0.0385350	-0.0278388	0.0031348
37	0.0699999	0.0410380	-0.0273462	0.0025971
38	0.0799999	0.0432520	-0.0268727	0.0021552
39	0.0899999	0.0452280	-0.0263840	0.0017444
40	0.0999998	0.0470040	-0.0260379	0.0014901
41	0.1249999	0.0507320	-0.0258168	0.0012597
42	0.1499999	0.0536360	-0.0253123	0.0008046
43	0.1749998	0.0558790	-0.0248285	0.0004446
44	0.1999999	0.0575700	-0.0245602	0.0002429
45	0.2249998	0.0587940	-0.0242336	-0.0000399
46	0.2499999	0.0596120	-0.0237143	-0.0004378
47	0.2749999	0.0600760	-0.0228825	-0.0009938
48	0.2999998	0.0602260	-0.0222731	-0.0013331
49	0.3249999	0.0600940	-0.0214813	-0.0019043
50	0.3499998	0.0597070	-0.0209003	-0.0022729
51	0.3749999	0.0590900	-0.0200925	-0.0026773
52	0.3999999	0.0582620	-0.0192844	-0.0029136
53	0.4249998	0.0572430	-0.0187588	-0.0031224
54	0.4499999	0.0560510	-0.0187727	-0.0034259
55	0.4749998	0.0546980	-0.0167400	-0.0044982
56	0.4999999	0.0531980	-0.0151551	-0.0057894
57	0.5249999	0.0515600	-0.0135177	-0.0075600
58	0.5499999	0.0497930	-0.0128491	-0.0081216
59	0.5749999	0.0479060	-0.0122501	-0.0085348
60	0.5999998	0.0459040	-0.0116415	-0.0088872
61	0.6249999	0.0437950	-0.0114056	-0.0090624
62	0.6499999	0.0415850	-0.0113411	-0.0091992
63	0.6749999	0.0392810	-0.0108557	-0.0096547
64	0.6999999	0.0368870	-0.0104663	-0.0100318

TABLE A-1 (Cont.)

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
65	0.7249998	0.0344110	-0.0102387	-0.0102853
66	0.7499999	0.0318550	-0.0100506	-0.0105385
67	0.7749999	0.0292210	-0.0097993	-0.0108486
68	0.7999999	0.0265150	-0.0095997	-0.0111196
69	0.8249999	0.0237390	-0.0094684	-0.0113200
70	0.8499998	0.0208880	-0.0093277	-0.0115877
71	0.8749999	0.0179530	-0.0088601	-0.0121522
72	0.8999999	0.0149080	-0.0085053	-0.0125218
73	0.9249999	0.0117000	-0.0080397	-0.0130707
74	0.9499999	0.0082510	-0.0071573	-0.0138387
75	0.9699998	0.0052390	-0.0067184	-0.0142036
76	0.9799999	0.0036110	-0.0065683	-0.0144199
77	0.9899997	0.0018740	-0.0066512	-0.0143157
78	1.0000000	0.0000000	-0.0067529	-0.0146004
79			-0.0056217	-0.0170565
80			-0.0050705	-0.0189836
81			-0.0039896	-0.0227000
82			-0.0032762	-0.0251463
83			-0.0024487	-0.0282429
84			0.0031550	-0.0357178
85			0.0096623	-0.0410241
86			0.0163364	-0.0445028
87			0.0225710	-0.0467179
88			0.0282904	-0.0487042
89			0.0343906	-0.0506315
90			0.0410188	-0.0502881
91			0.0470315	-0.0477098
92			0.0578462	-0.0466736
93			0.0687209	-0.0471658
94			0.0793683	-0.0467616
95			0.0898905	-0.0457813
96			0.0999998	-0.0470040
97			0.1249999	-0.0507320

TABLE A-1 (Cont.)

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
98			0.1499999	-0.0536360
99			0.1749998	-0.0558790
100			0.1999999	-0.0575700
101			0.2249998	-0.0587940
102			0.2499999	-0.0596120
103			0.2749999	-0.0600760
104			0.2999998	-0.0602260
105			0.3249999	-0.0600940
106			0.3499998	-0.0597070
107			0.3749999	-0.0590900
108			0.3999999	-0.0582620
109			0.4249998	-0.0572430
110			0.4499999	-0.0560510
111			0.4749998	-0.0546980
112			0.4999999	-0.0531980
113			0.5249999	-0.0515600
114			0.5499999	-0.0497930
115			0.5749999	-0.0479060
116			0.5999998	-0.0459040
117			0.6249999	-0.0437950
118			0.6499999	-0.0415850
119			0.6749999	-0.0392810
120			0.6999999	-0.0368870
121			0.7249998	-0.0344110
122			0.7499999	-0.0318550
123			0.7749999	-0.0292210
124			0.7999999	-0.0265150
125			0.8249999	-0.0237390
126			0.8499998	-0.0208880
127			0.8749999	-0.0179530
128			0.8999999	-0.0149080
129			0.9249999	-0.0117000
130			0.9499999	-0.0082510

TABLE A-1 (Cont.)

No.	X _{upper}	Y _{upper}	X _{lower}	Y _{lower}
131			0.9699998	-0.0052390
132			0.9799999	-0.0036110
133			0.9899998	-0.0018740
134			1.0000000	0.0000000

NACA 0012 MODEL - LEWICE GENERATED ICE SHAPE

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1714	0.00	-0.01	-0.023	-0.022	-----	-----	-----	0.0002	0.132	1.622
1715	0.00	-0.01	-0.029	-0.028	0.0227	0.0221	-.0007	-.0009	0.132	1.624
1716	1.00	1.03	0.087	0.083	0.0238	0.0232	0.0061	0.0066	0.132	1.625
1717	2.00	2.07	0.200	0.191	0.0262	0.0255	0.0136	0.0148	0.132	1.616
1718	3.00	3.11	0.304	0.289	0.0311	0.0302	0.0203	0.0221	0.131	1.604
1719	4.00	4.15	0.425	0.403	0.0414	0.0402	0.0275	0.0299	0.131	1.608
1720	5.00	5.18	0.530	0.501	0.0552	0.0534	0.0323	0.0353	0.129	1.591
1721	5.00	5.18	0.530	0.501	0.0544	0.0527	0.0298	0.0328	0.131	1.605
1722	6.00	6.19	0.604	0.569	0.0781	0.0752	0.0231	0.0267	0.129	1.589
1723	7.00	7.17	0.659	0.616	0.1100	0.1053	-.0097	-.0047	0.129	1.583
1724	7.00	7.17	0.671	0.626	0.1176	0.1124	-.0090	-.0040	0.128	1.592
1725	8.00	8.13	0.653	0.606	0.1453	0.1381	-.0444	-.0380	0.127	1.587
1726	9.00	9.11	0.635	0.587	0.1602	0.1518	-.0583	-.0513	0.126	1.566
1727	10.00	10.11	0.650	0.598	0.1852	0.1747	-.0657	-.0579	0.126	1.566
1728	8.00	8.16	0.687	0.638	0.1385	0.1318	-.0299	-.0239	0.126	1.577
1729	6.00	6.19	0.601	0.566	0.0728	0.0702	0.0235	0.0271	0.130	1.614
1730	0.00	-0.01	-0.026	-0.025	0.0215	0.0209	0.0007	0.0005	0.131	1.636
1731	-1.00	-1.04	-0.135	-0.128	0.0236	0.0230	-.0057	-.0066	0.132	1.650
1732	-2.00	-2.07	-0.229	-0.217	0.0248	0.0241	-.0084	-.0099	0.131	1.630
1733	-3.00	-3.11	-0.350	-0.333	0.0267	0.0260	-.0123	-.0146	0.132	1.637
1734	-4.00	-4.15	-0.472	-0.449	0.0252	0.0245	-.0164	-.0194	0.133	1.650
1735	-5.00	-5.19	-0.590	-0.561	0.0275	0.0268	-.0230	-.0267	0.132	1.638
1736	-6.00	-6.21	-0.681	-0.647	0.0300	0.0292	-.0241	-.0285	0.132	1.635
1737	-7.00	-7.25	-0.794	-0.754	0.0339	0.0329	-.0266	-.0317	0.132	1.636
1738	-8.00	-8.27	-0.870	-0.825	0.0401	0.0389	-.0290	-.0345	0.132	1.636
1739	-9.00	-9.29	-0.957	-0.906	0.0501	0.0485	-.0301	-.0362	0.131	1.628
1740	-10.00	-10.31	-1.019	-0.962	0.0628	0.0607	-.0291	-.0355	0.131	1.628
1741	-8.00	-8.27	-0.876	-0.830	0.0404	0.0392	-.0290	-.0346	0.131	1.624
1742	-6.00	-6.21	-0.683	-0.649	0.0287	0.0279	-.0235	-.0279	0.132	1.642
1743	-4.00	-4.14	-0.462	-0.439	0.0250	0.0243	-.0166	-.0196	0.131	1.630
1744	-2.00	-2.08	-0.245	-0.233	0.0227	0.0221	-.0083	-.0099	0.132	1.641
1745	-2.00	-2.07	-0.236	-0.225	0.0244	0.0238	-.0081	-.0096	0.132	1.636

NACA 0012 MODEL - LEWICE GENERATED ICE SHAPE, 36 GRIT ROUGHNESS

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1746	-2.34	-2.43	-0.289	-0.275	0.0306	0.0298	-.0129	-.0147	0.131	1.609
1747	-1.34	-1.40	-0.176	-0.167	0.0267	0.0260	-.0078	-.0089	0.130	1.594
1748	-0.34	-0.36	-0.071	-0.068	0.0263	0.0256	-.0021	-.0026	0.132	1.622
1749	0.66	0.67	0.035	0.034	0.0265	0.0258	0.0035	0.0037	0.131	1.608

NACA 0012 MODEL - LEWICE GENERATED ICE SHAPE, 36 GRIT ROUGHNESS

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re x10 ⁻⁶
1750	1.66	1.72	0.157	0.149	0.0282	0.0274	0.0112	0.0121	0.131	1.610
1751	2.66	2.76	0.278	0.264	0.0316	0.0307	0.0188	0.0204	0.131	1.603
1752	3.66	3.79	0.371	0.352	0.0373	0.0362	0.0253	0.0274	0.132	1.615
1753	4.66	4.83	0.474	0.449	0.0454	0.0440	0.0331	0.0357	0.131	1.603
1754	5.66	5.85	0.569	0.536	0.0646	0.0624	0.0320	0.0352	0.130	1.596
1755	6.66	6.84	0.626	0.586	0.1015	0.0973	0.0043	0.0085	0.129	1.582
1756	7.66	7.80	0.638	0.594	0.1268	0.1210	-0.0281	-0.0226	0.128	1.572
1757	8.66	8.77	0.604	0.559	0.1511	0.1435	-0.0512	-0.0448	0.126	1.548
1758	9.66	9.75	0.547	0.505	0.1701	0.1609	-0.0542	-0.0479	0.126	1.544
1759	10.66	10.74	0.512	0.470	0.1936	0.1823	-0.0560	-0.0496	0.125	1.531
1760	9.66	9.75	0.530	0.489	0.1702	0.1610	-0.0529	-0.0468	0.126	1.568
1761	7.66	7.80	0.637	0.594	0.1235	0.1179	-0.0295	-0.0239	0.128	1.592
1762	5.66	5.85	0.558	0.526	0.0657	0.0635	0.0327	0.0358	0.131	1.625
1763	3.66	3.79	0.380	0.360	0.0373	0.0362	0.0262	0.0283	0.131	1.630
1764	1.66	1.72	0.160	0.152	0.0286	0.0278	0.0106	0.0115	0.132	1.645
1765	-0.34	-0.36	-0.070	-0.067	0.0256	0.0249	-0.0032	-0.0036	0.132	1.644
1766	-2.34	-2.43	-0.288	-0.273	0.0303	0.0295	-0.0129	-0.0147	0.132	1.643
1767	-2.34	-2.43	-0.279	-0.265	0.0314	0.0305	-0.0086	-0.0104	0.128	1.505
1768	-2.34	-2.43	-0.298	-0.283	0.0303	0.0295	-0.0113	-0.0132	0.128	1.512
1769	-3.34	-3.47	-0.406	-0.385	0.0367	0.0357	-0.0160	-0.0185	0.127	1.504
1770	-4.34	-4.50	-0.496	-0.470	0.0428	0.0415	-0.0202	-0.0233	0.127	1.503
1771	-5.34	-5.52	-0.570	-0.539	0.0531	0.0514	-0.0233	-0.0268	0.126	1.483
1772	-6.34	-6.53	-0.634	-0.597	0.0723	0.0697	-0.0162	-0.0202	0.125	1.479
1773	-7.34	-7.49	-0.660	-0.617	0.1108	0.1061	0.0260	0.0205	0.124	1.468
1774	-7.34	-7.50	-0.666	-0.621	0.1174	0.1122	0.0237	0.0182	0.126	1.483
1775	-8.34	-8.46	-0.639	-0.594	0.1401	0.1333	0.0474	0.0410	0.123	1.455
1776	-9.34	-9.43	-0.561	-0.519	0.1559	0.1479	0.0610	0.0544	0.123	1.462
1777	-7.34	-7.49	-0.659	-0.615	0.1161	0.1110	0.0230	0.0176	0.124	1.478
1778	-5.34	-5.52	-0.571	-0.540	0.0510	0.0494	-0.0235	-0.0270	0.127	1.519
1779	-3.34	-3.47	-0.389	-0.370	0.0345	0.0335	-0.0170	-0.0194	0.127	1.513
1780	-2.34	-2.43	-0.297	-0.282	0.0318	0.0309	-0.0115	-0.0134	0.128	1.531
1781	-3.34	-3.46	-0.386	-0.366	0.0352	0.0342	-0.0176	-0.0200	0.128	1.520

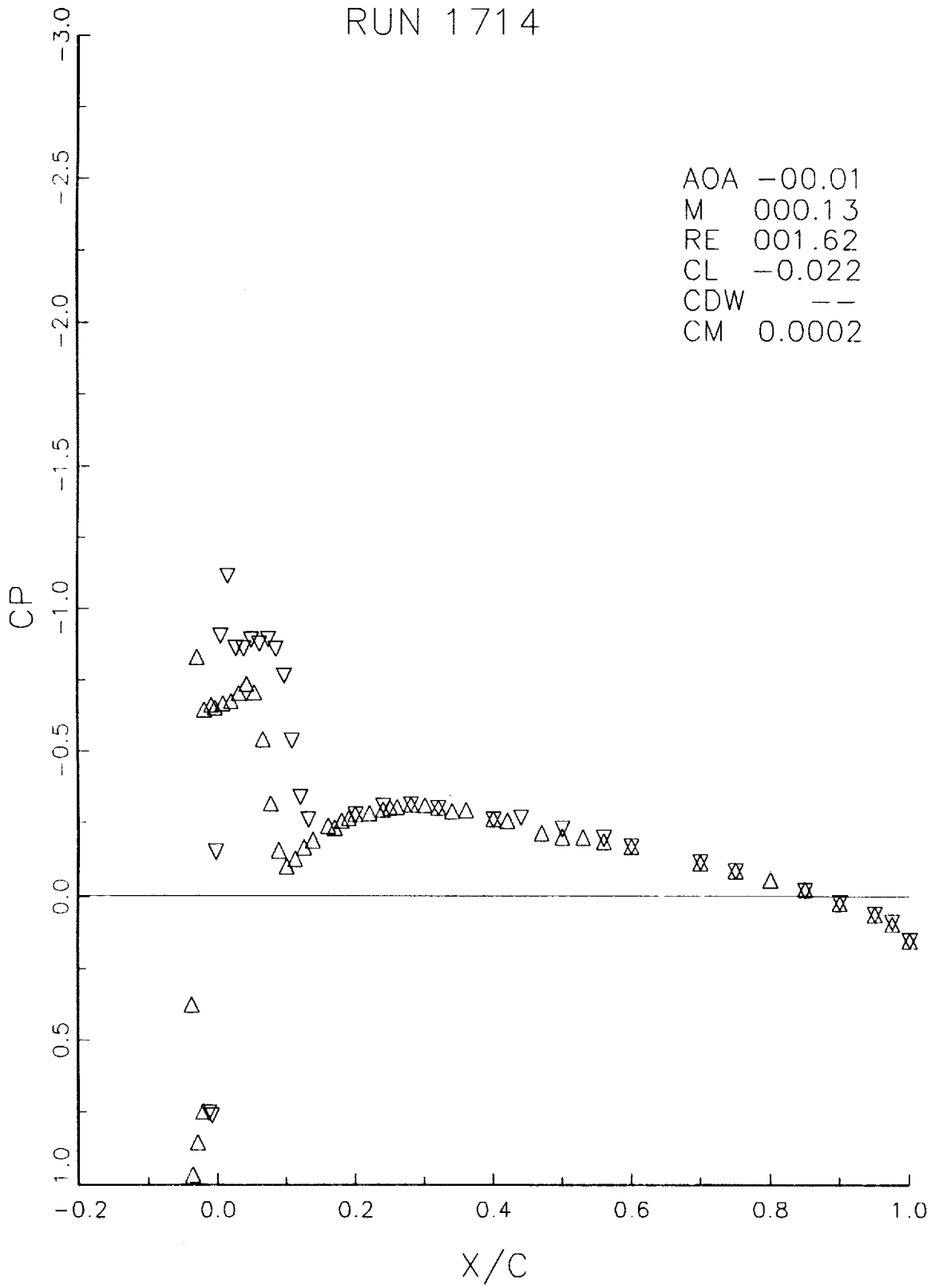
NACA 0012 MODEL - LEWICE GENERATED ICE SHAPE

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re x10 ⁻⁶
1782	-10.00	-10.31	-1.012	-0.956	0.0611	0.0591	-0.0319	-0.0382	0.128	1.559
1783	-11.00	-11.30	-1.012	-0.952	0.0795	0.0766	-0.0202	-0.0267	0.127	1.551
1784	-12.00	-12.29	-1.094	-1.026	0.0962	0.0924	0.0104	0.0024	0.125	1.523

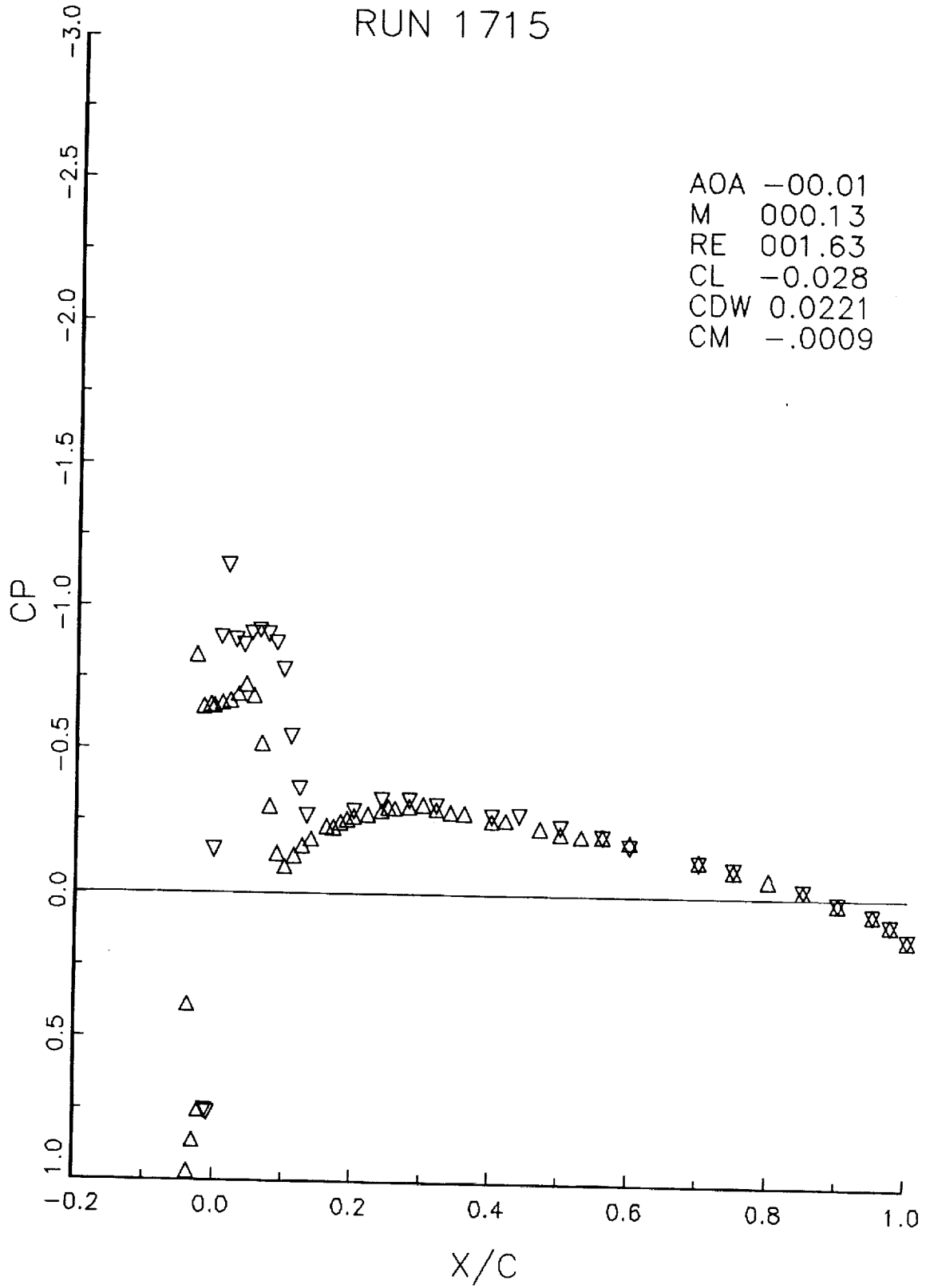
NACA 0012 MODEL - LEWICE GENERATED ICE SHAPE

RUN	α_u (deg)	α (deg)	C_{l_u}	C_l	C_{d_u}	C_d	C_{m_u}	C_m	MACH	Re $\times 10^{-6}$
1785	-12.00	-12.29	-1.092	-1.015	0.1364	0.1299	0.0101	0.0021	0.127	1.544
1786	-13.00	-13.23	-1.021	-0.944	0.1634	0.1548	0.0415	0.0325	0.124	1.506
1787	-14.00	-14.21	-1.022	-0.939	0.1948	0.1834	0.0676	0.0571	0.122	1.489
1788	-12.00	-12.29	-1.090	-1.014	0.1328	0.1266	0.0052	-.0026	0.125	1.526
1789	-11.00	-11.32	-1.080	-1.032	-----	-----	-.0272	-.0345	0.129	1.568
1790	-11.00	-11.32	-1.079	-1.014	0.0824	0.0793	-.0266	-.0334	0.127	1.551

RUN 1714

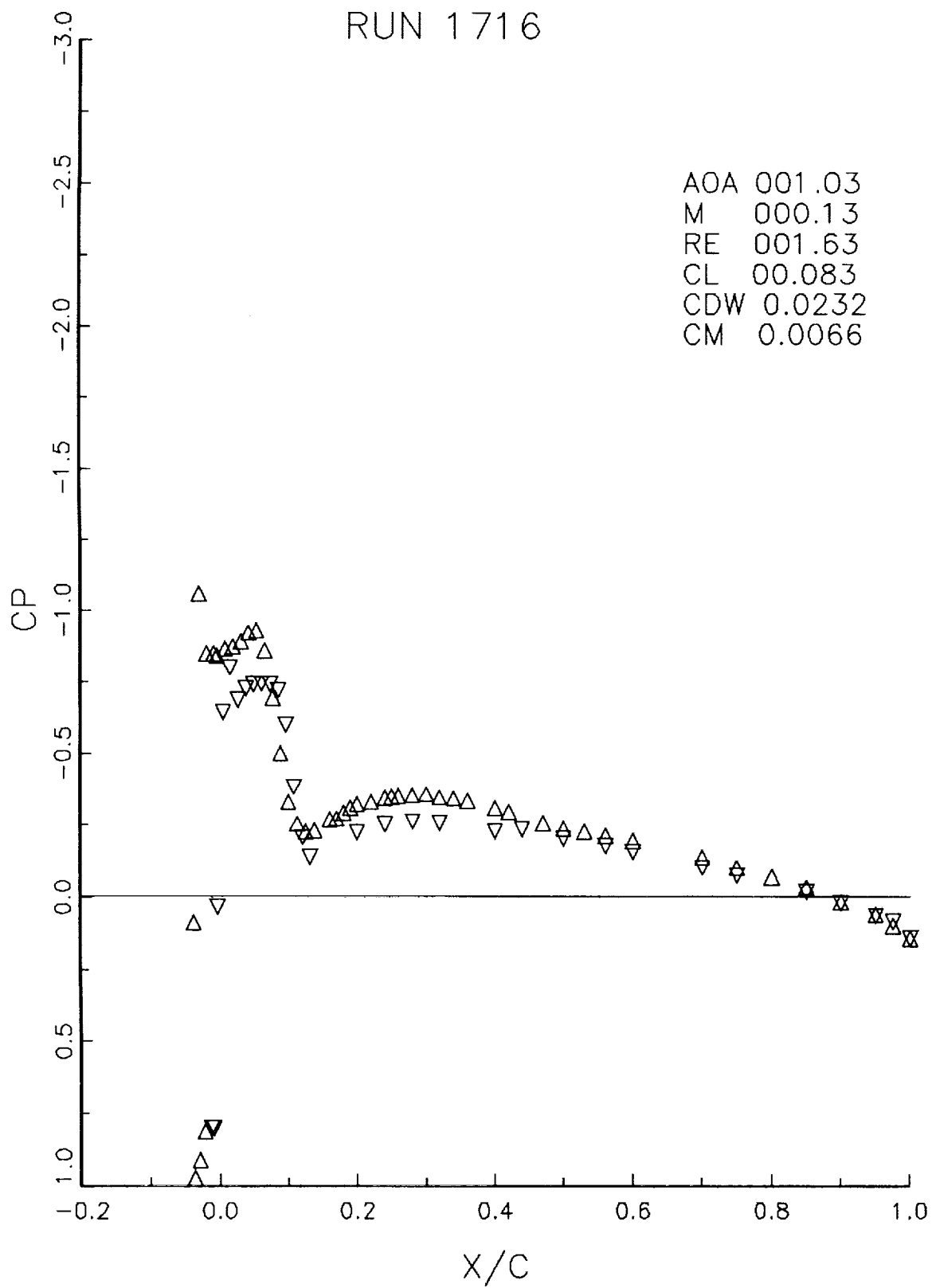


RUN 1715



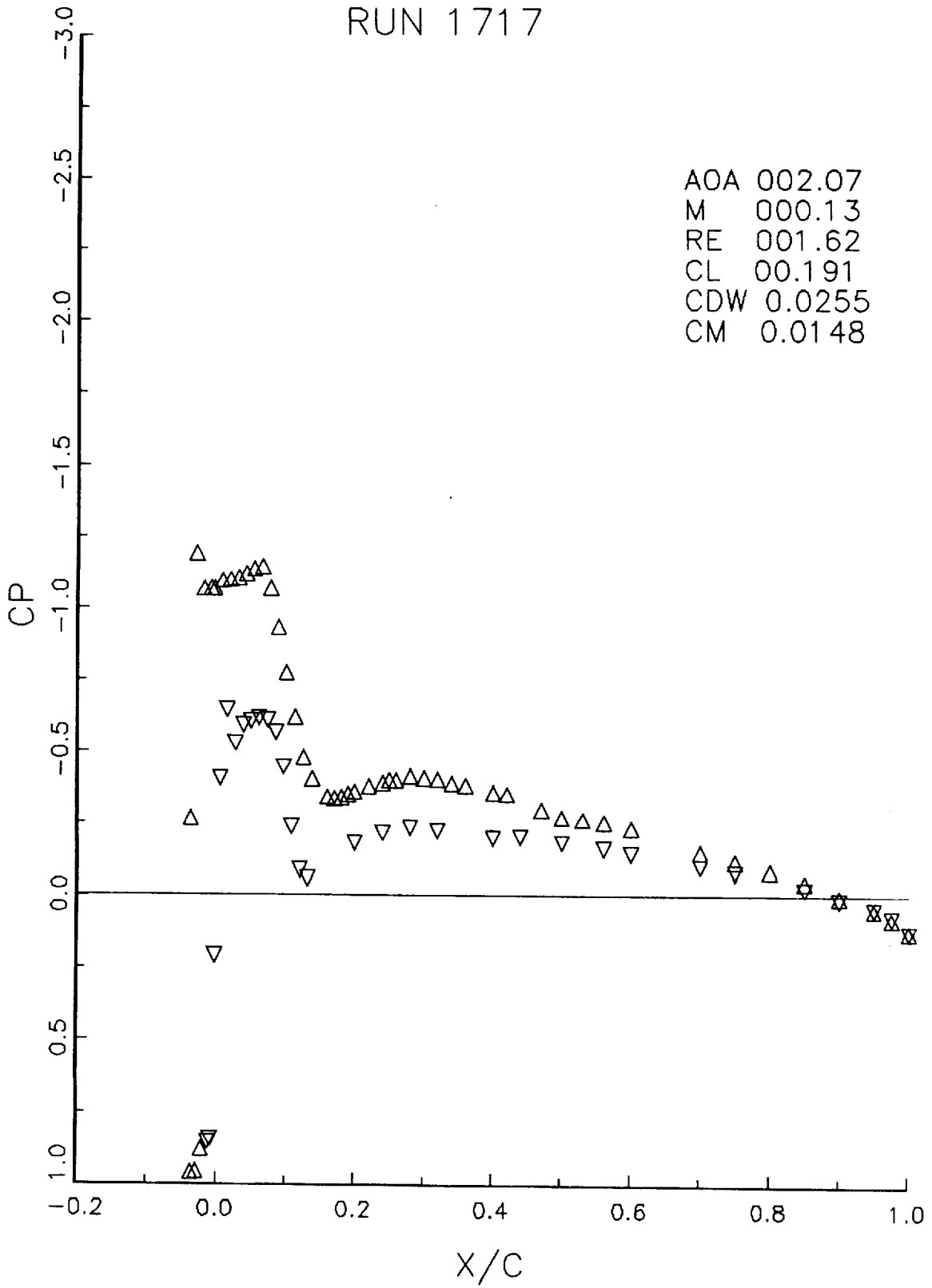
RUN 1716

AOA 001.03
M 000.13
RE 001.63
CL 00.083
CDW 0.0232
CM 0.0066



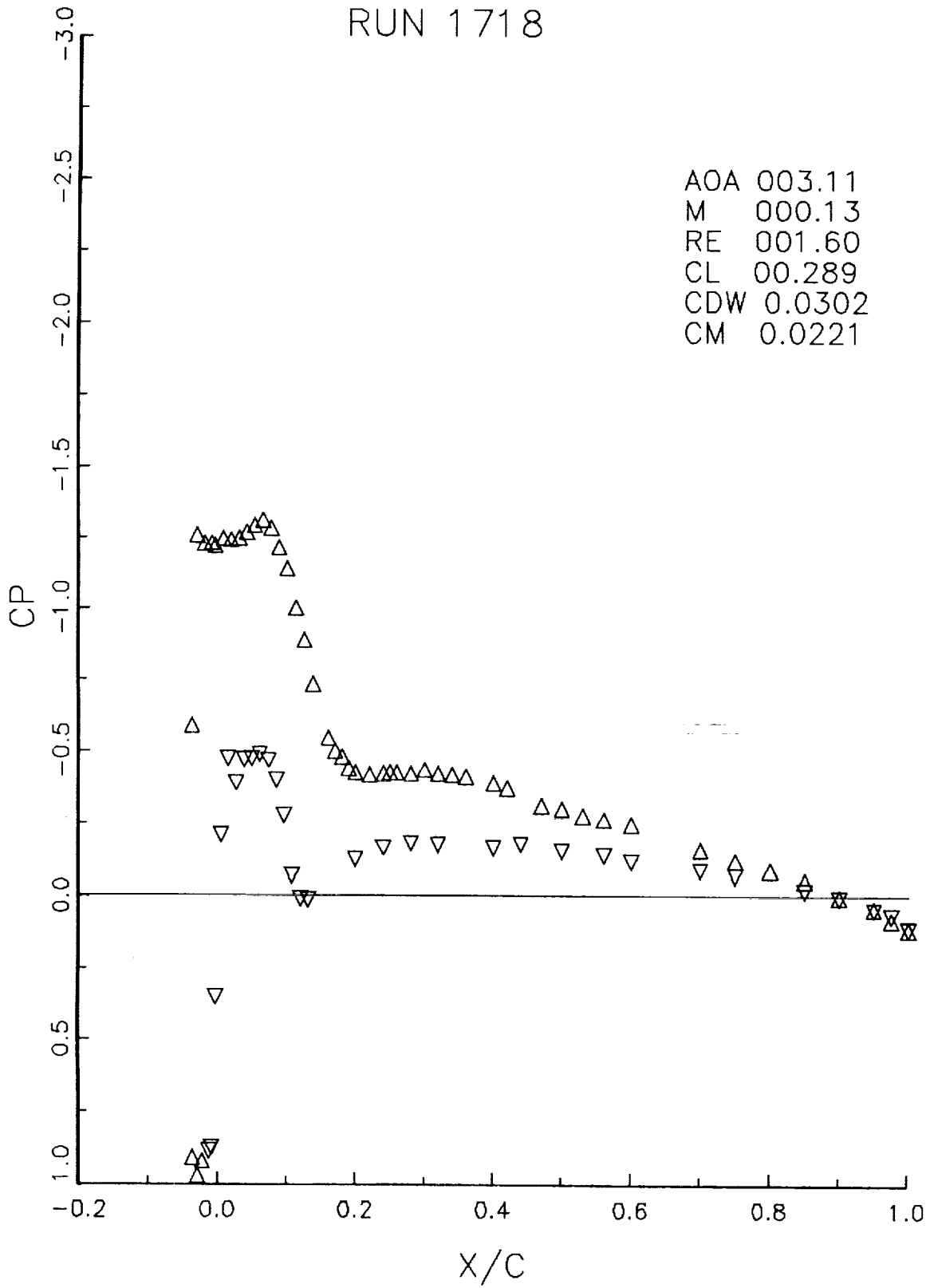
RUN 1717

AOA 002.07
M 000.13
RE 001.62
CL 00.191
CDW 0.0255
CM 0.0148

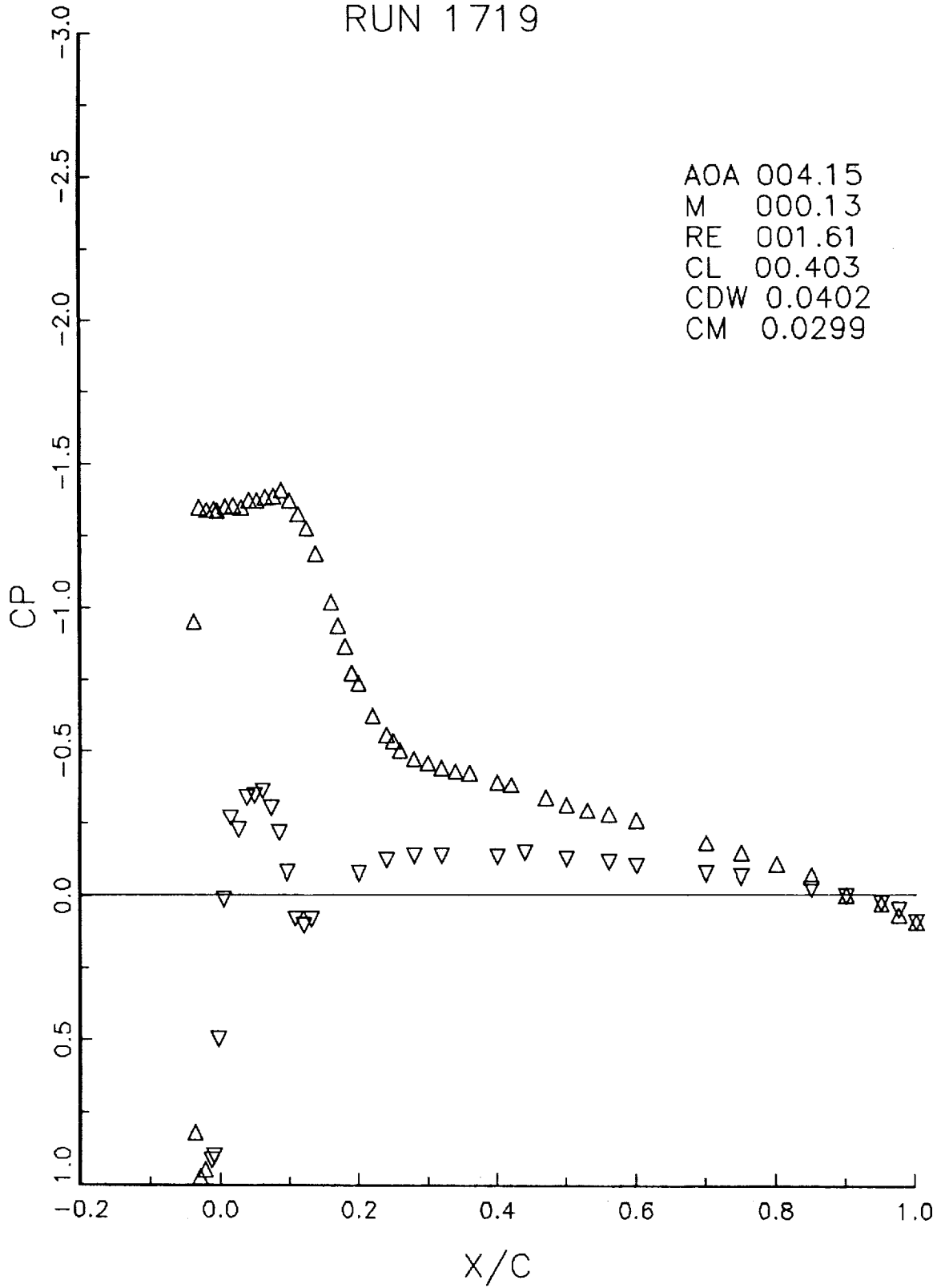


RUN 1718

AOA 003.11
M 000.13
RE 001.60
CL 00.289
CDW 0.0302
CM 0.0221

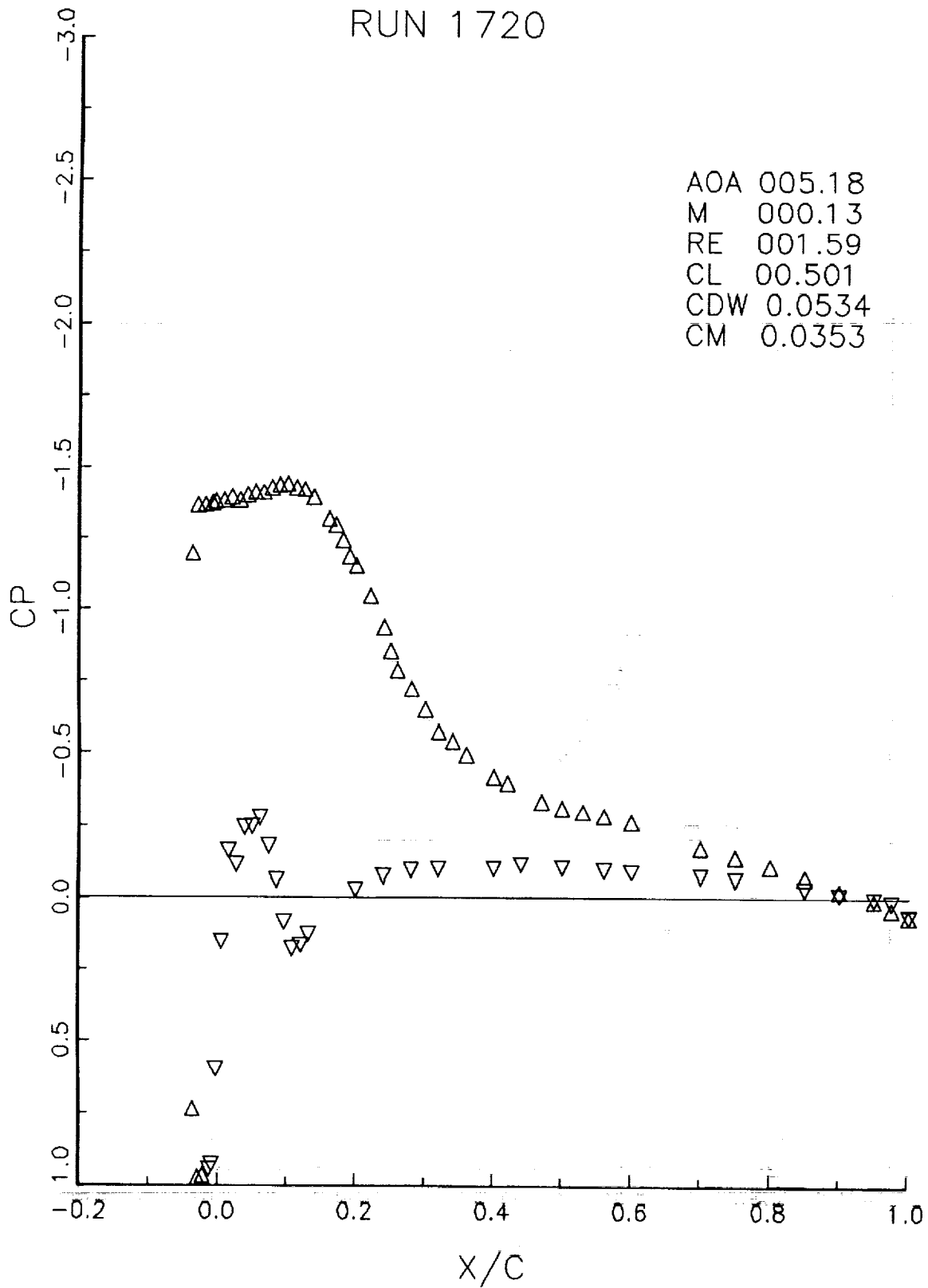


RUN 1719



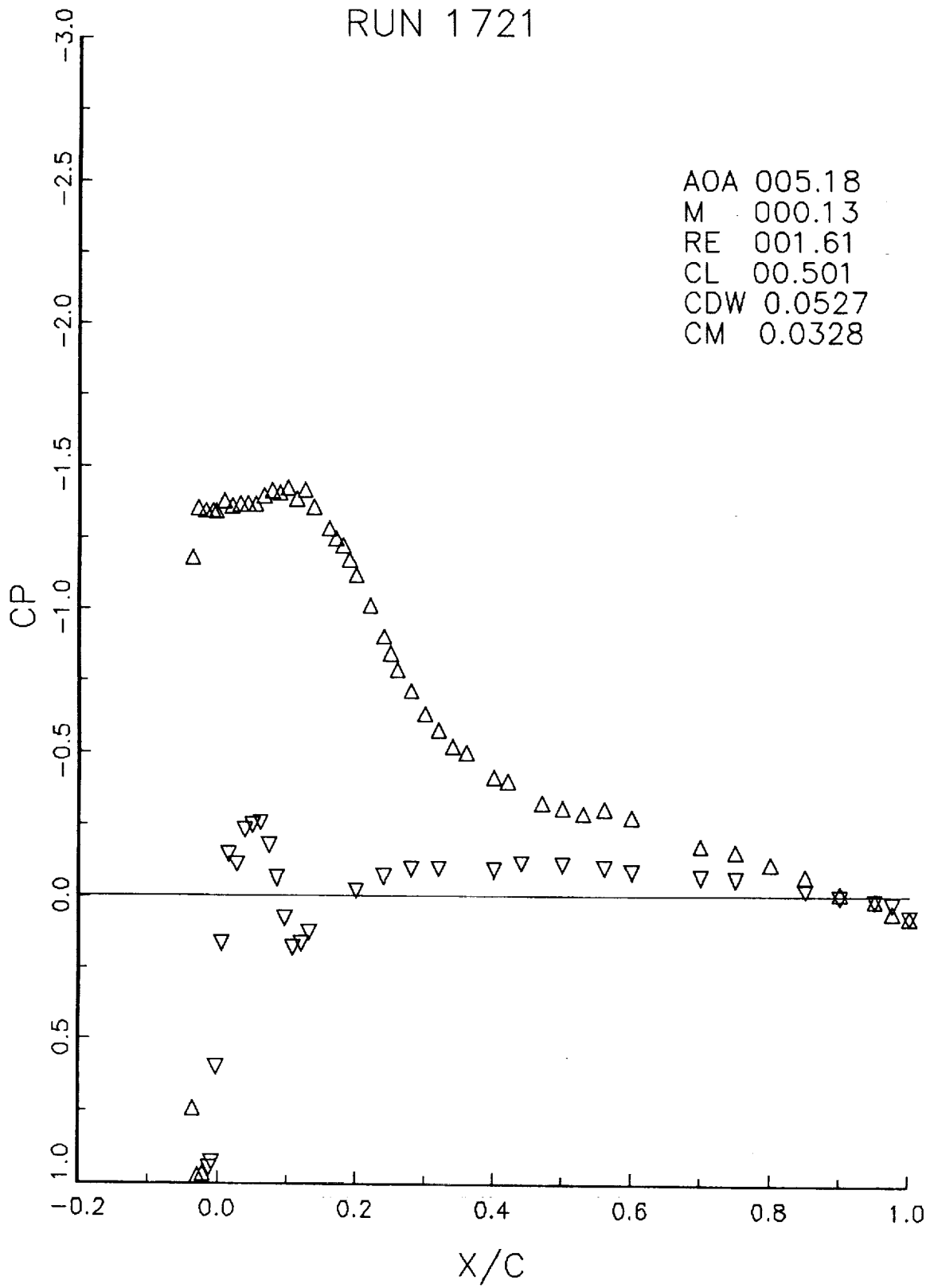
RUN 1720

AOA 005.18
M 000.13
RE 001.59
CL 00.501
CDW 0.0534
CM 0.0353



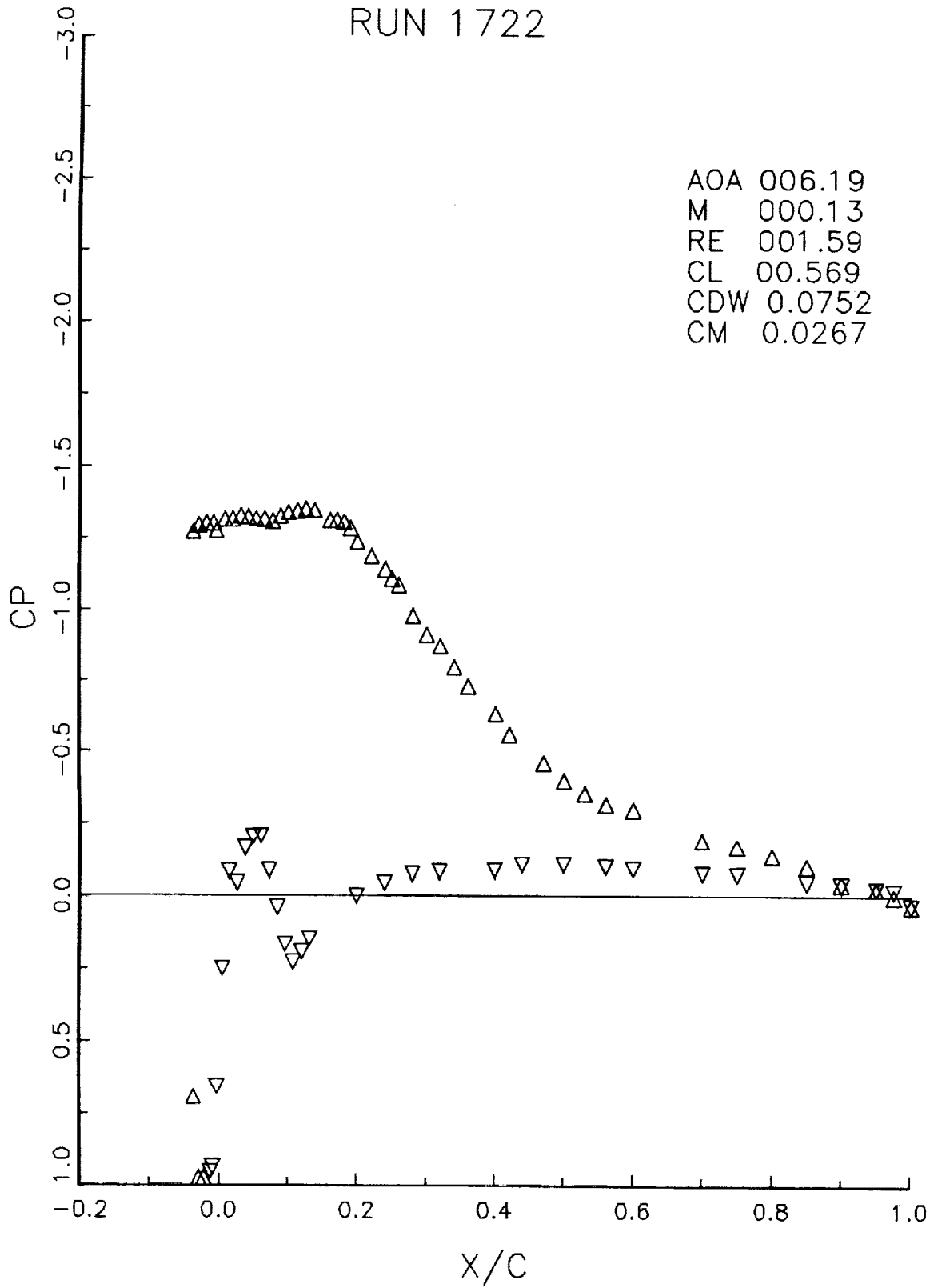
RUN 1721

AOA 005.18
M 000.13
RE 001.61
CL 00.501
CDW 0.0527
CM 0.0328



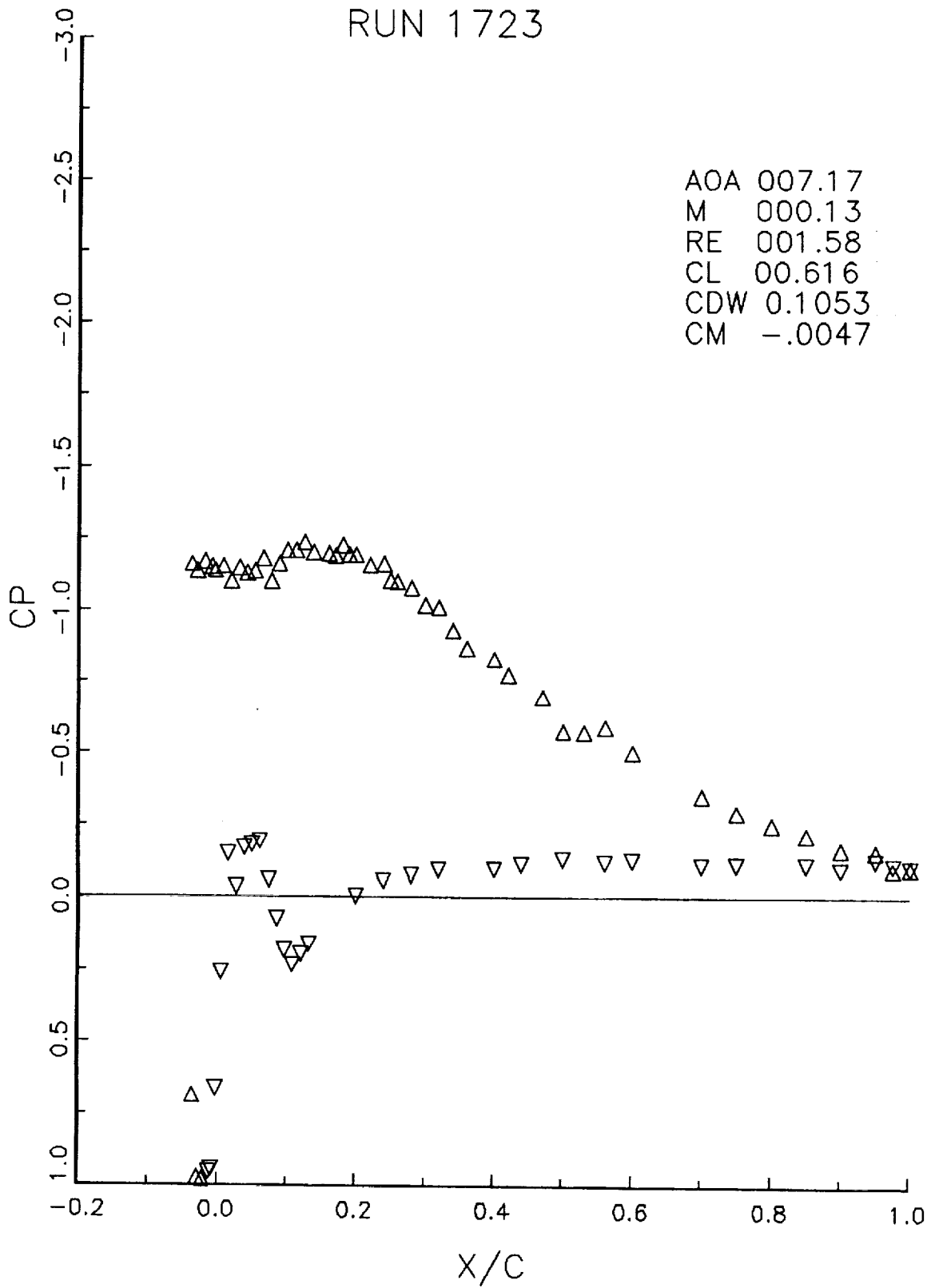
RUN 1722

AOA 006.19
M 000.13
RE 001.59
CL 00.569
CDW 0.0752
CM 0.0267

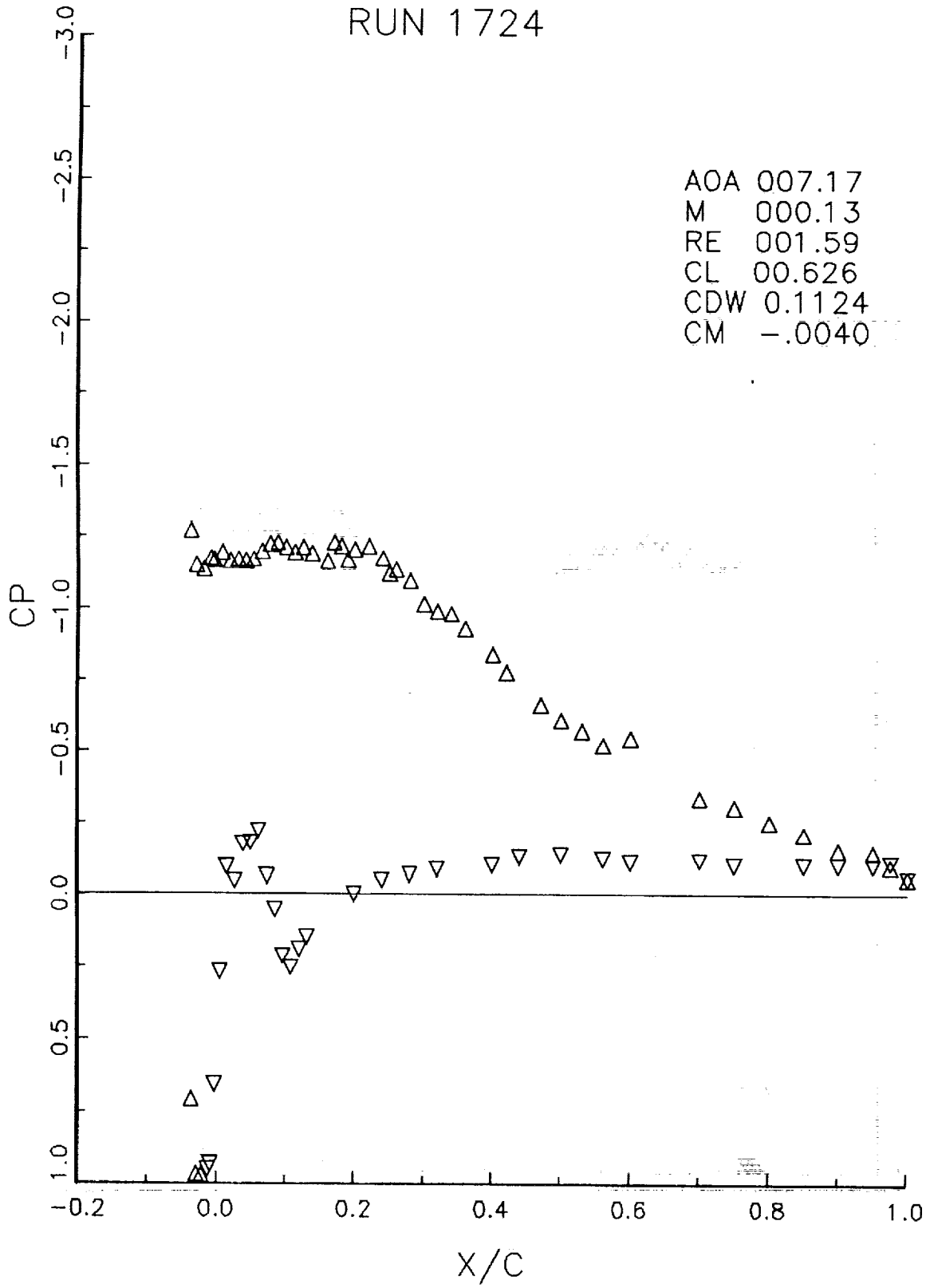


RUN 1723

AOA 007.17
M 000.13
RE 001.58
CL 00.616
CDW 0.1053
CM -.0047

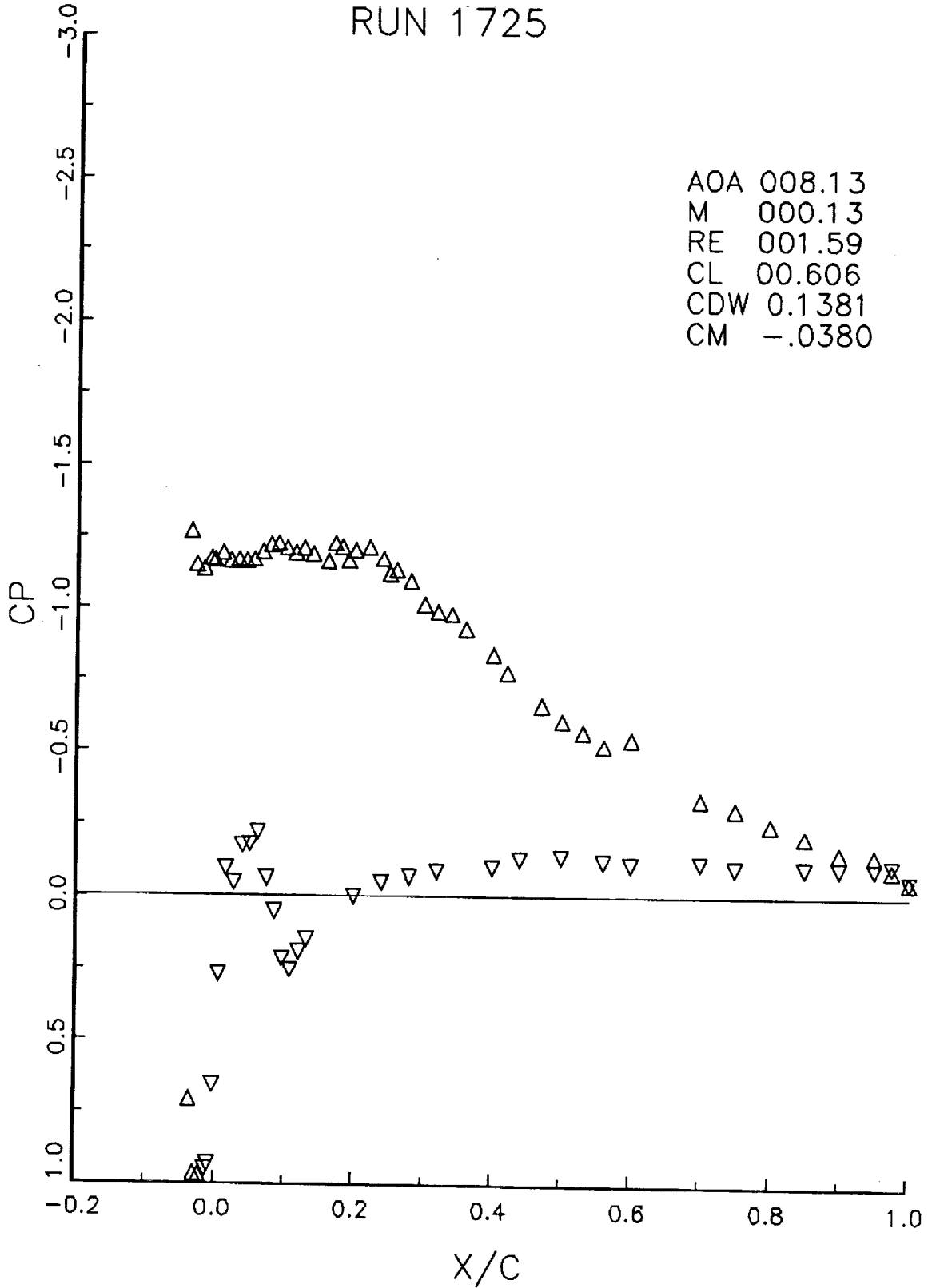


RUN 1724

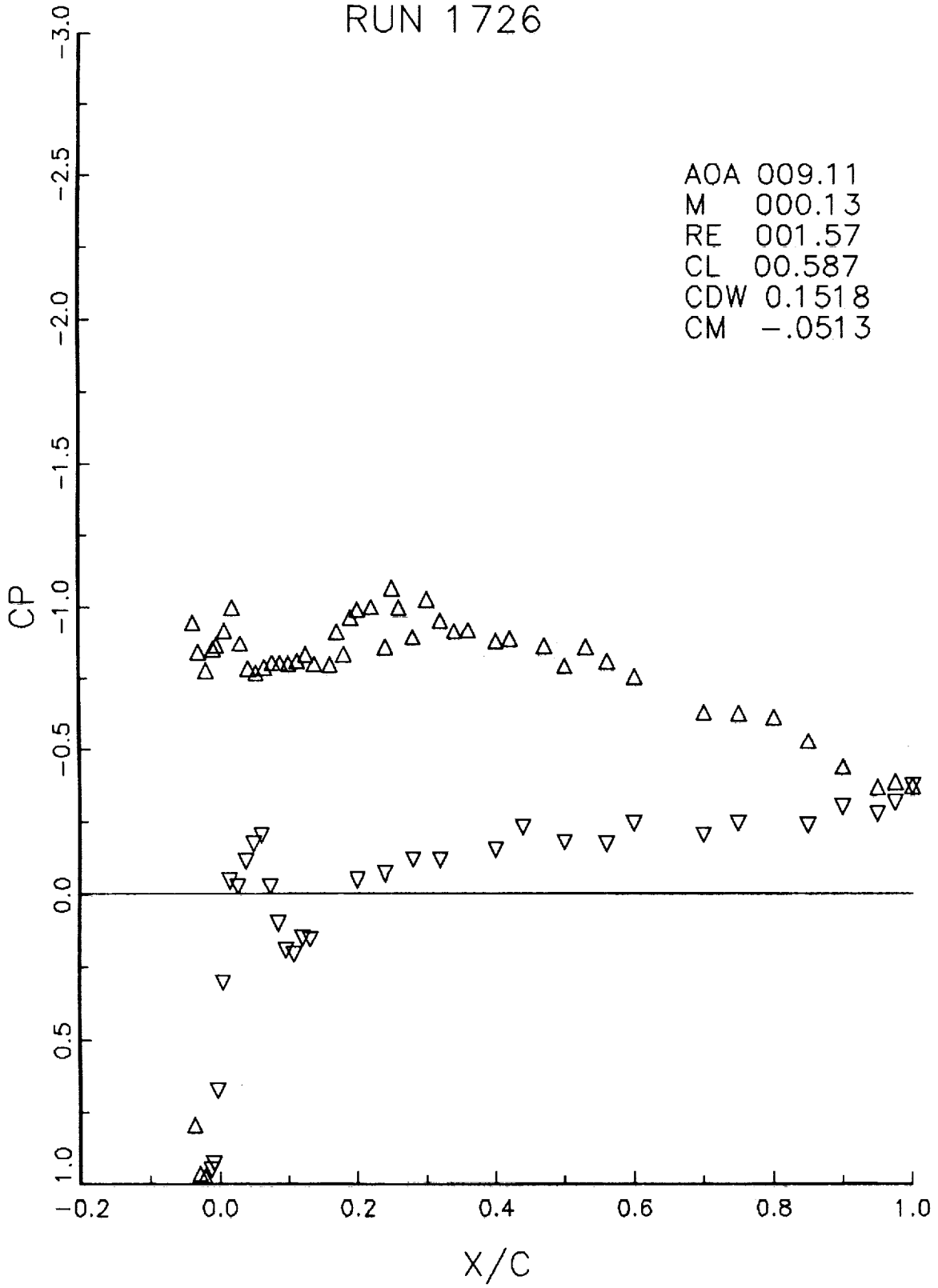


RUN 1725

AOA 008.13
M 000.13
RE 001.59
CL 00.606
CDW 0.1381
CM -0.0380

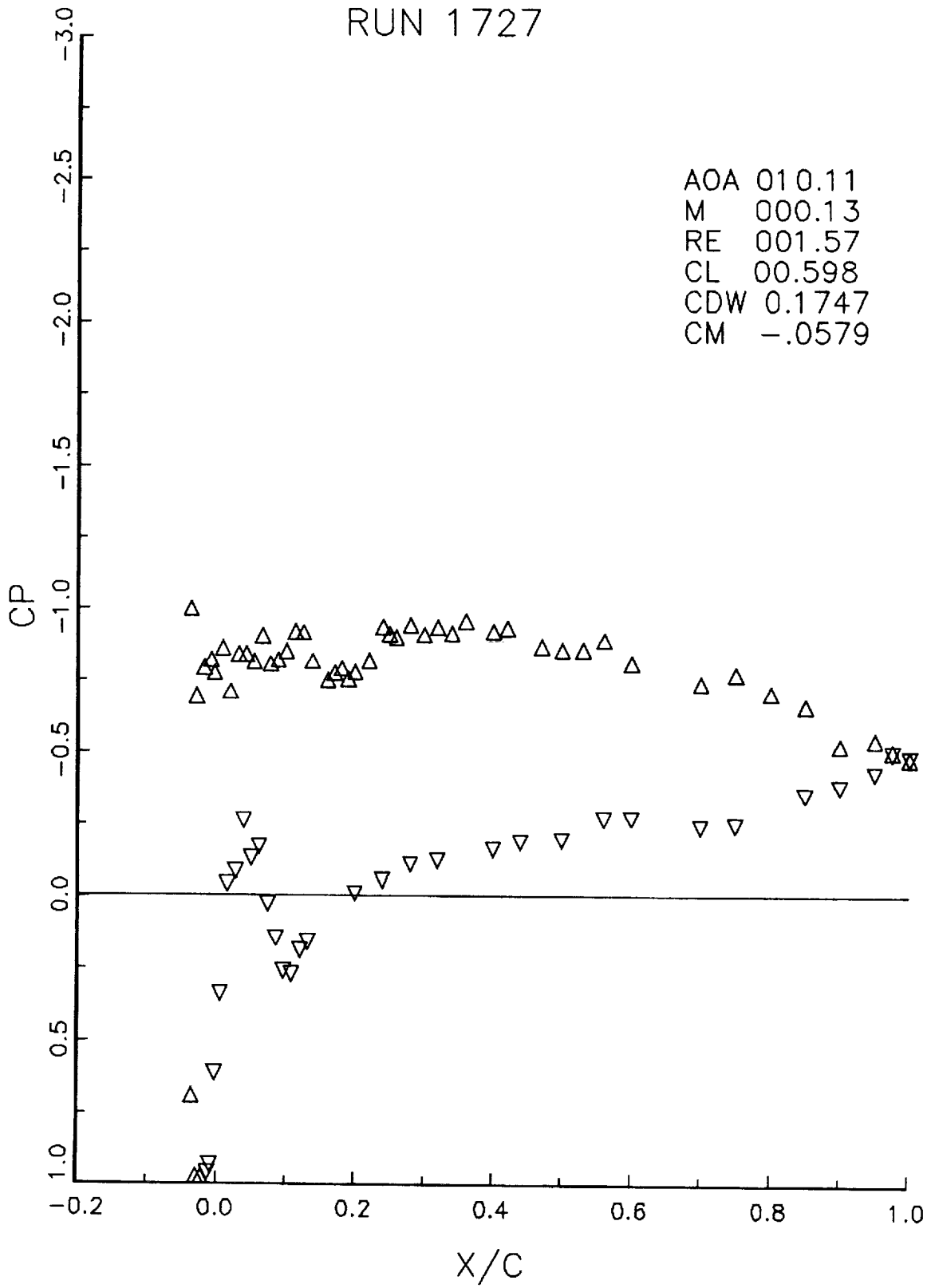


RUN 1726

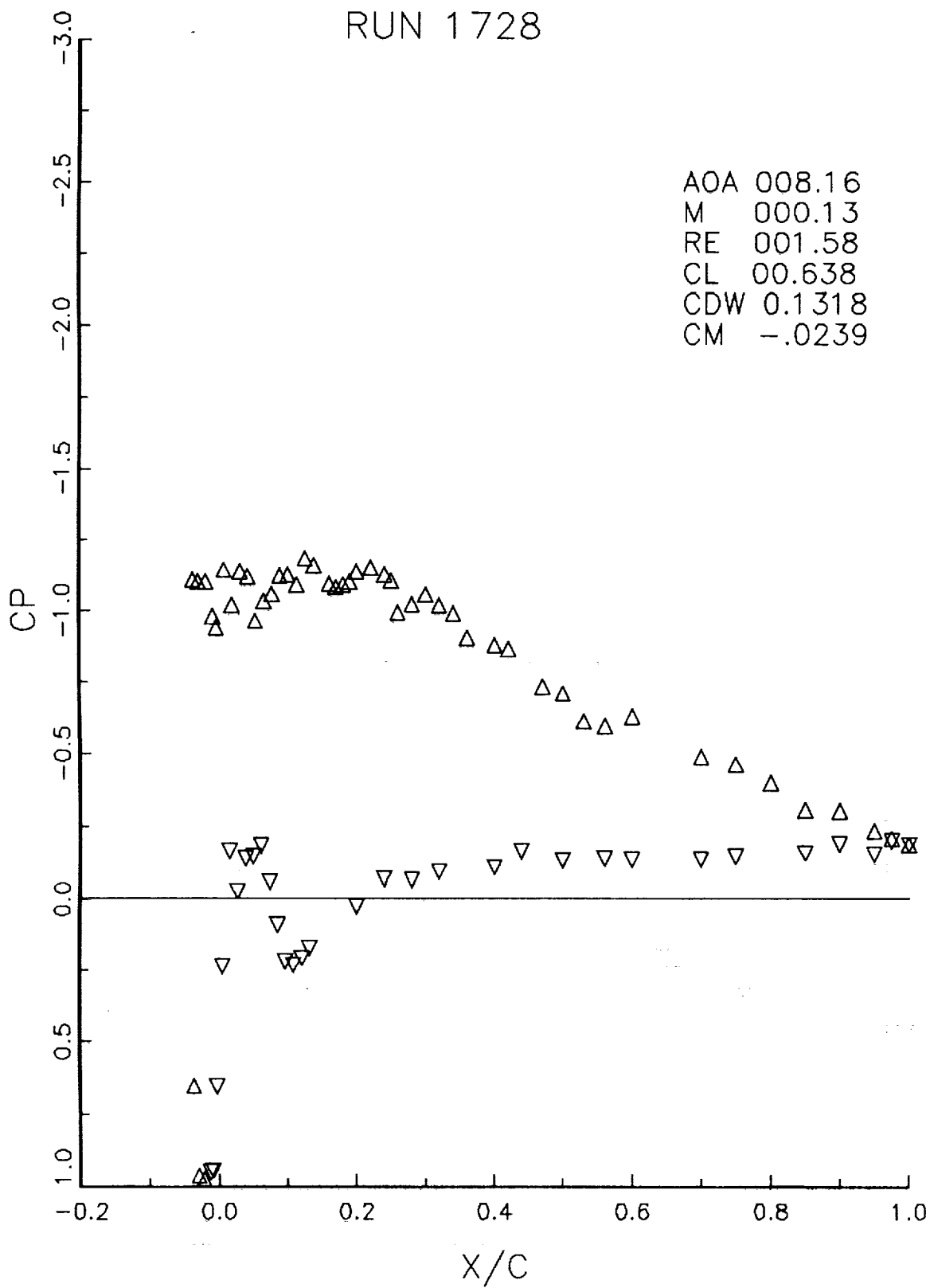


RUN 1727

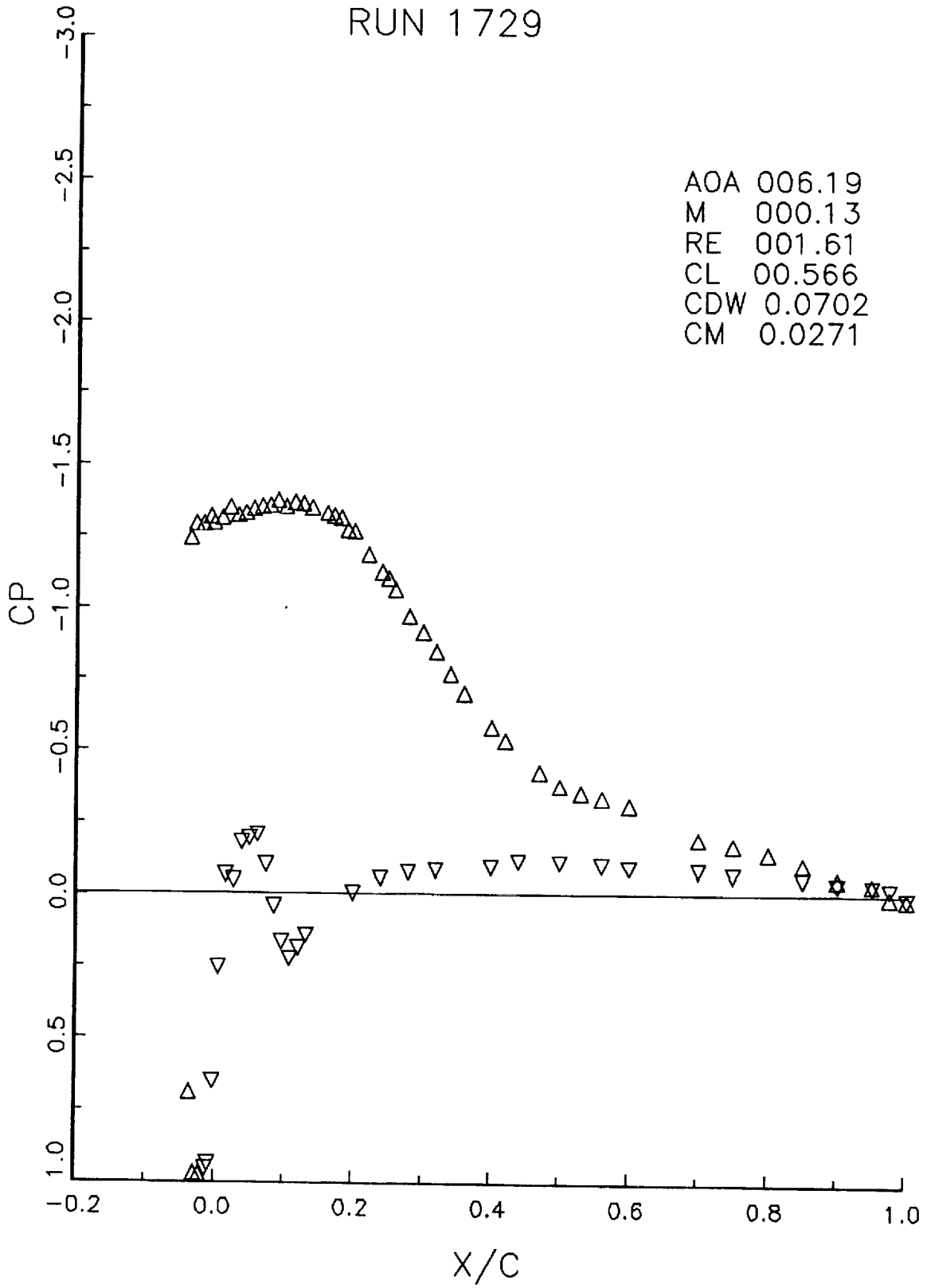
AOA 010.11
M 000.13
RE 001.57
CL 00.598
CDW 0.1747
CM -0.0579



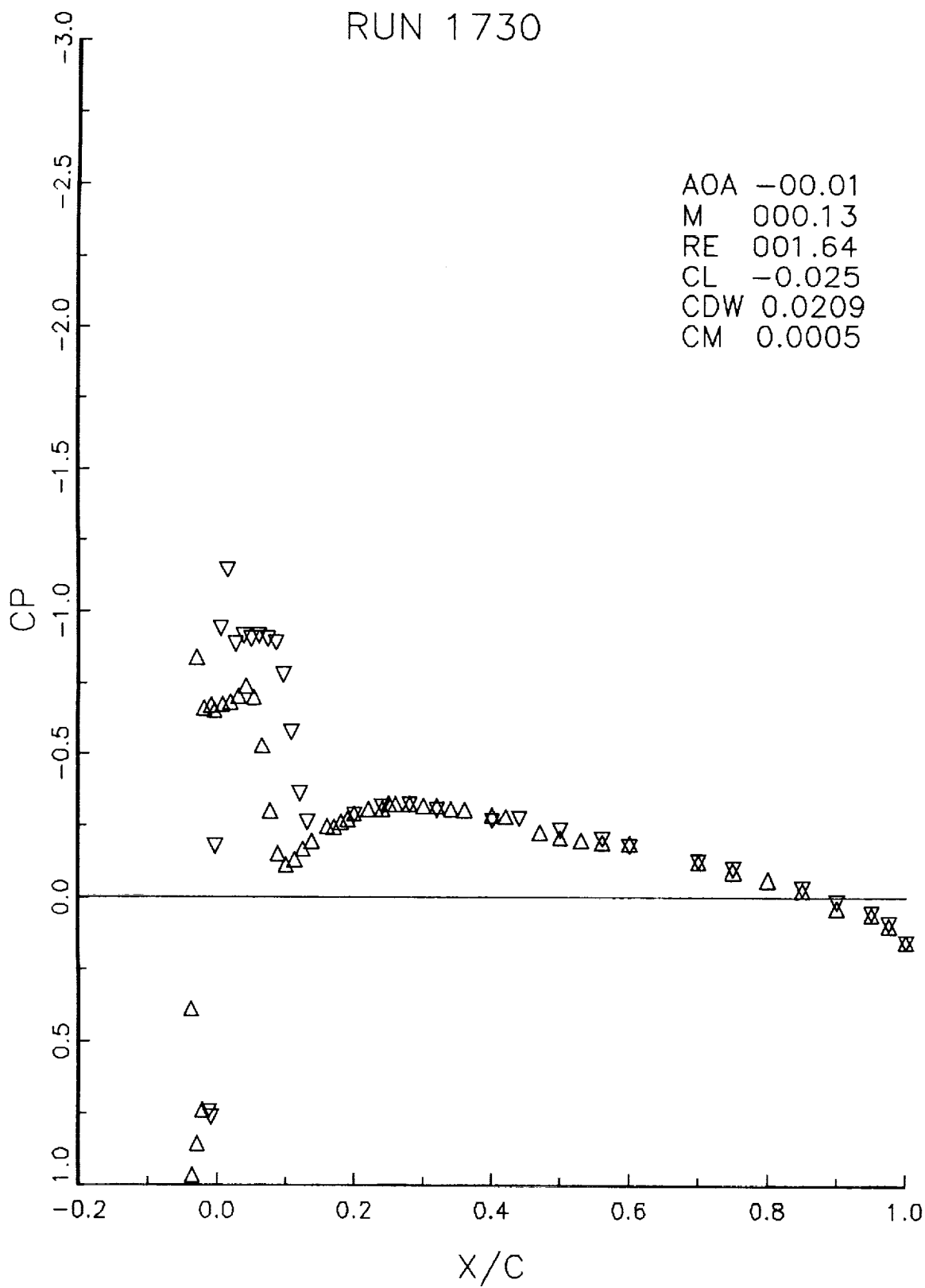
RUN 1728



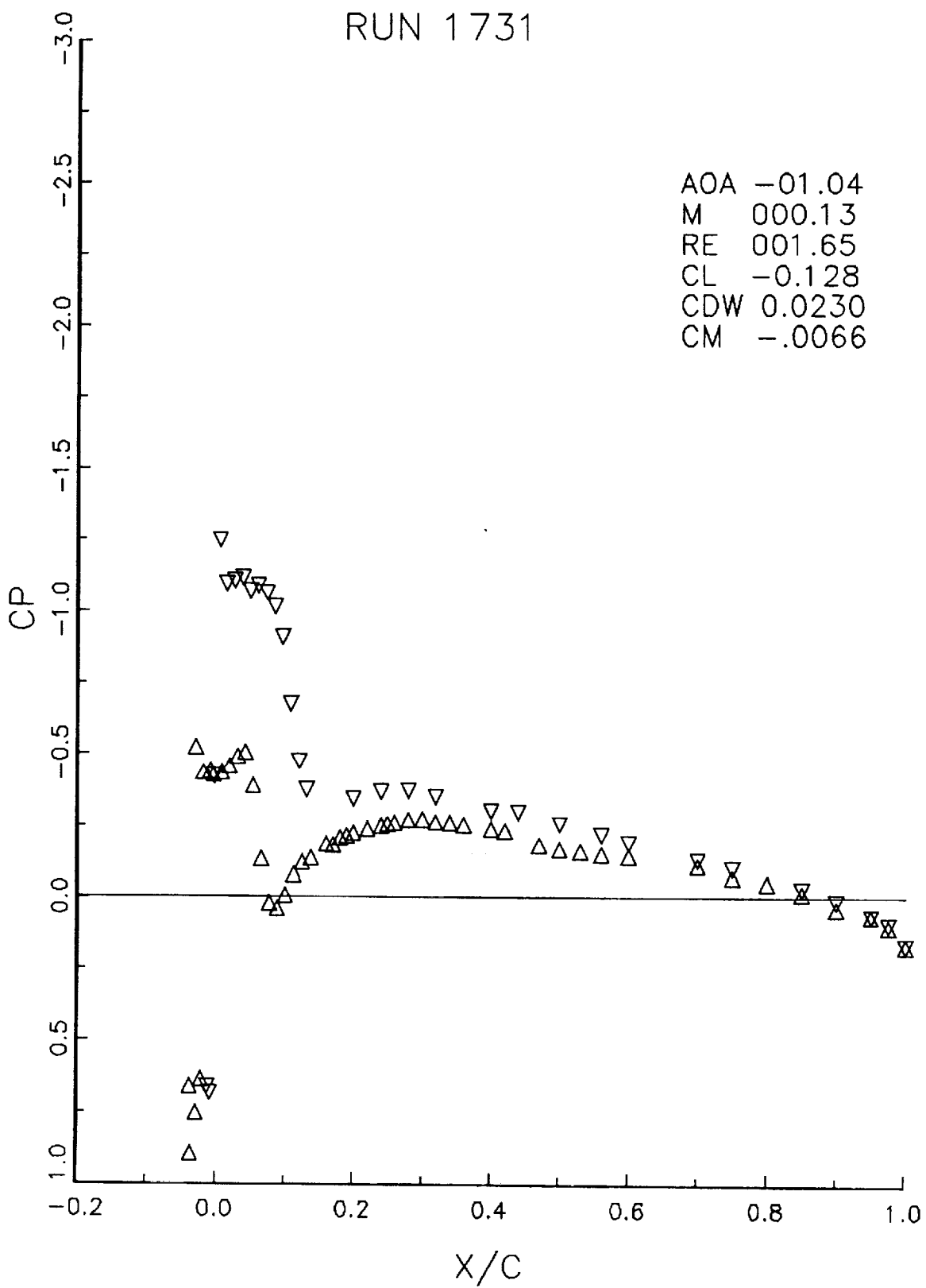
RUN 1729



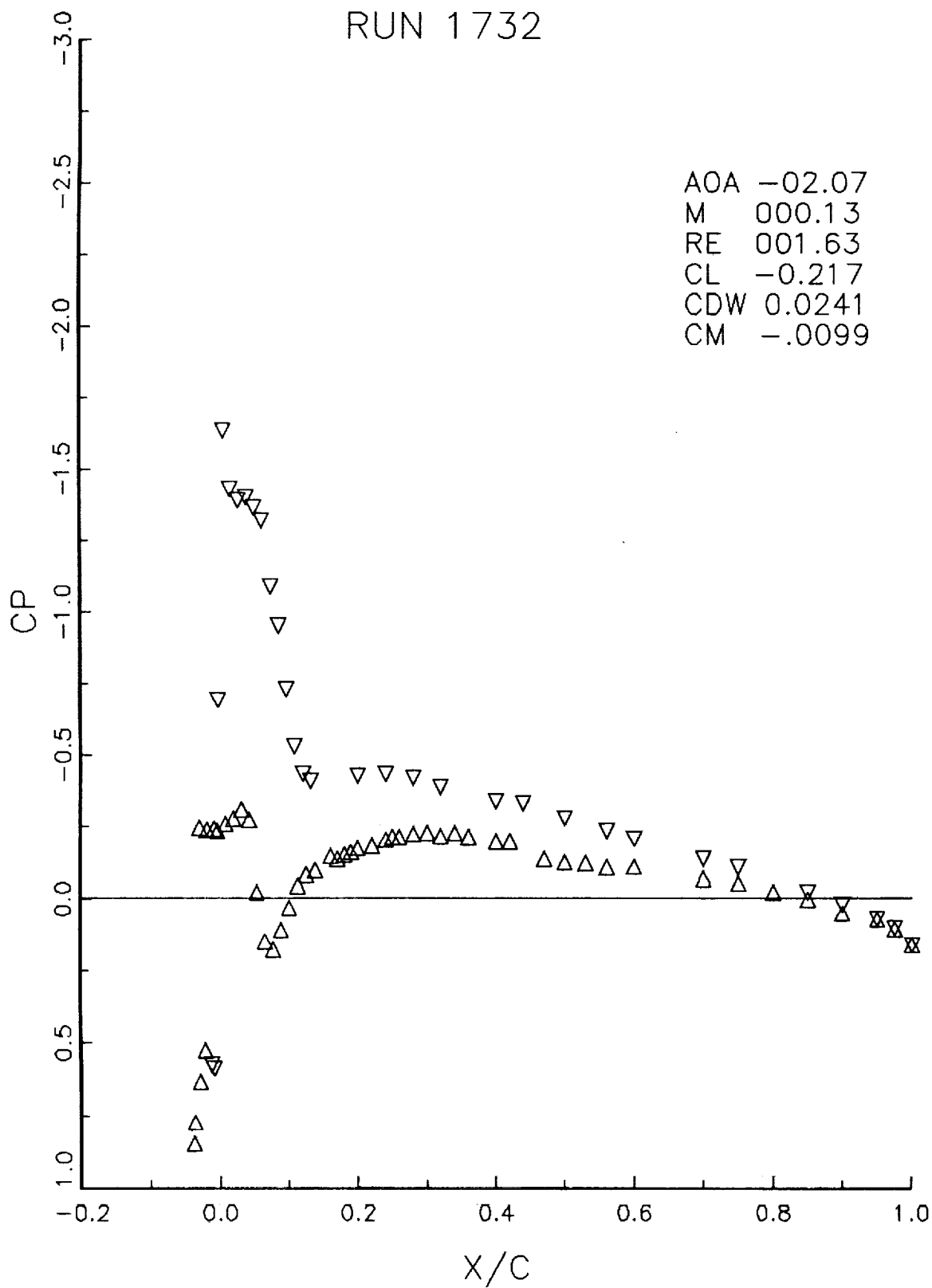
RUN 1730



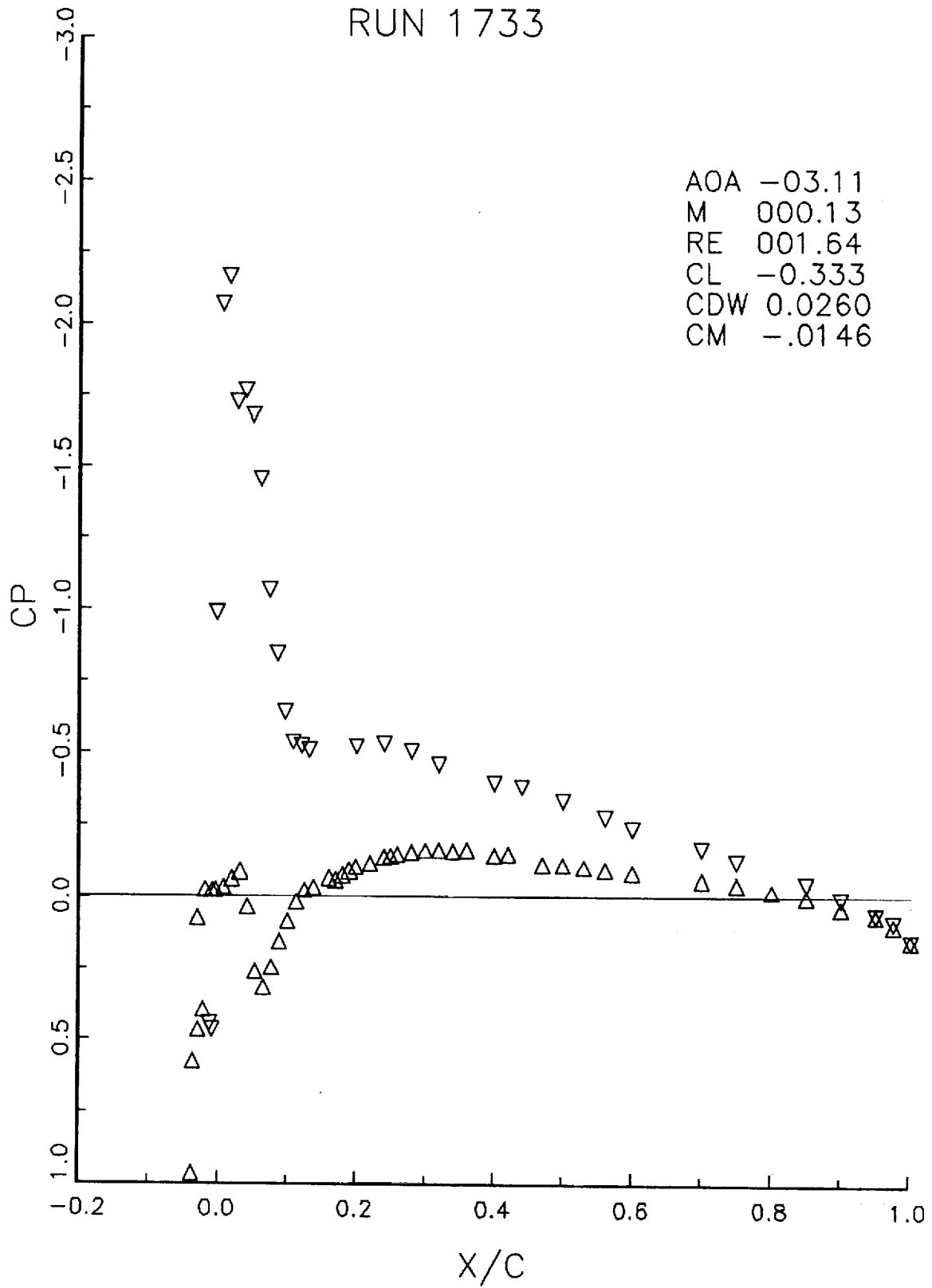
RUN 1731



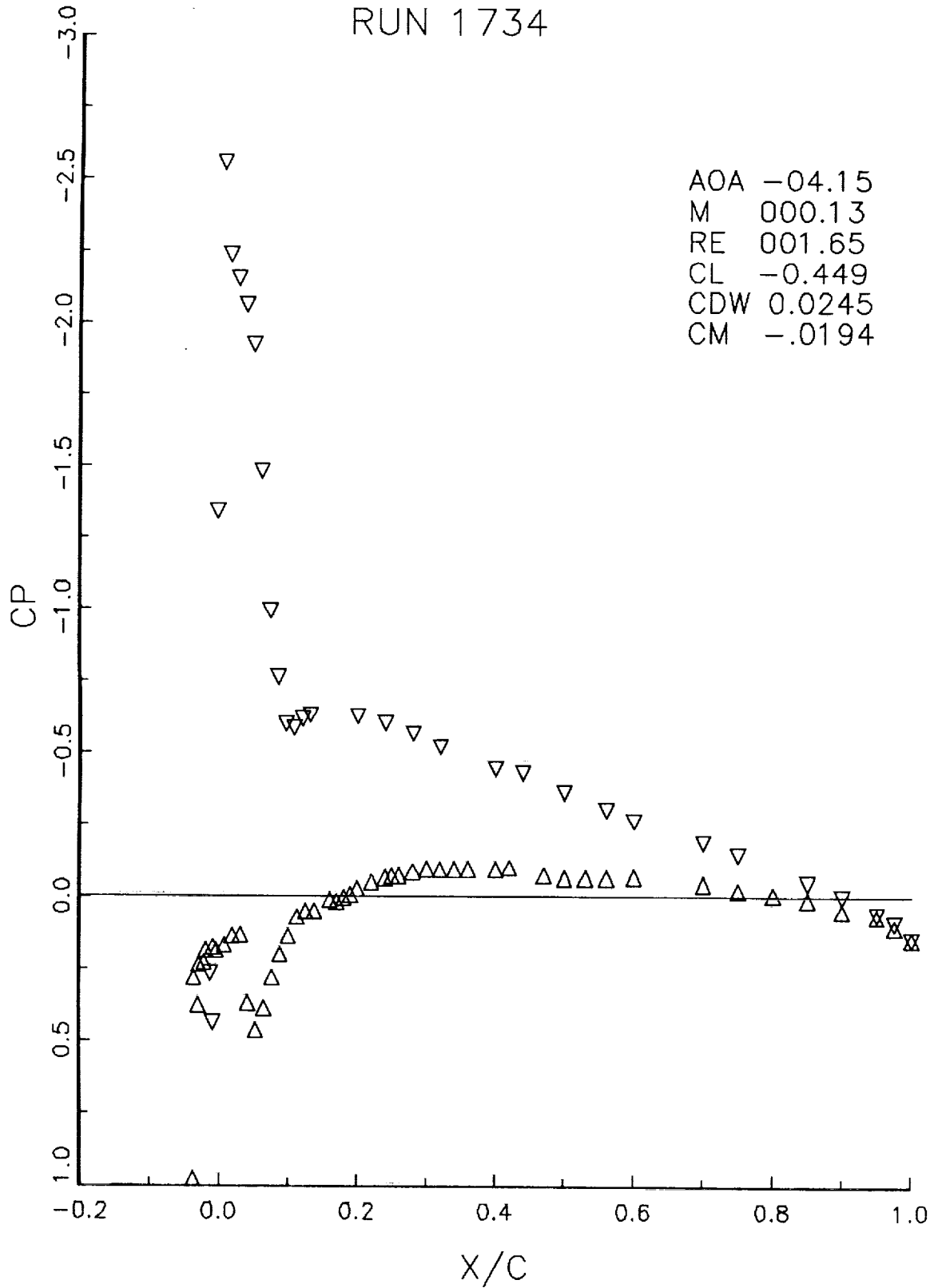
RUN 1732

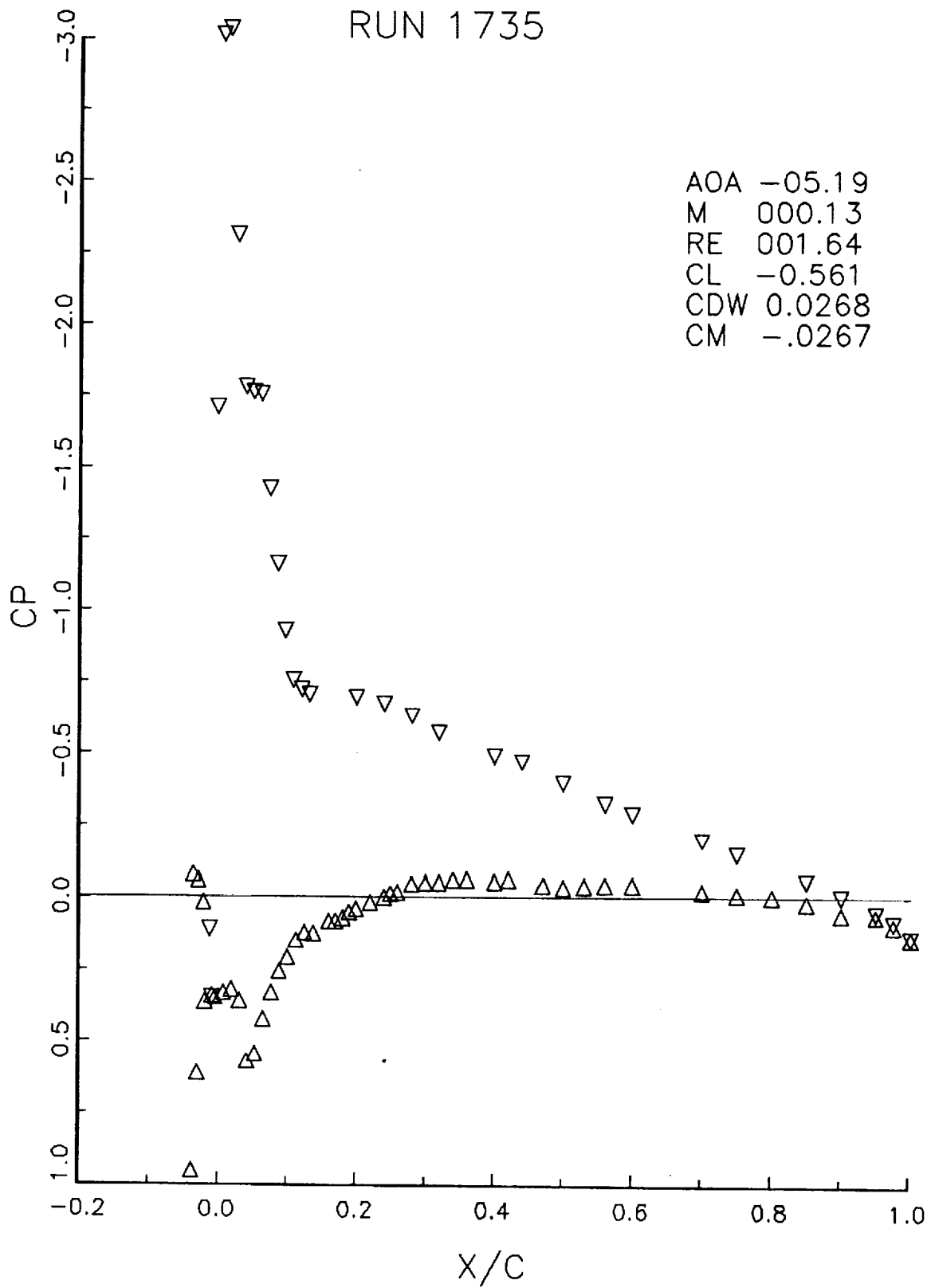


RUN 1733

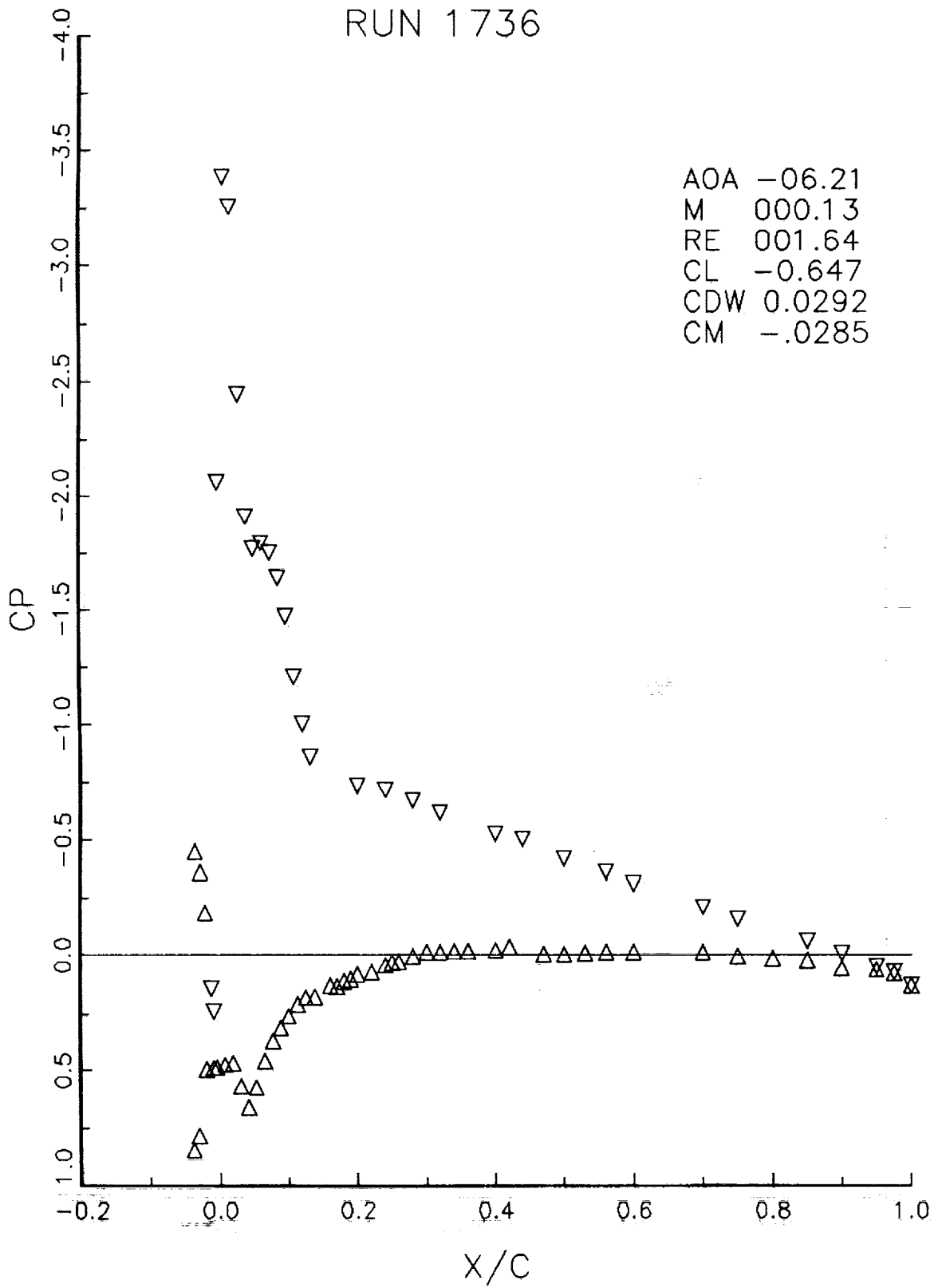


RUN 1734

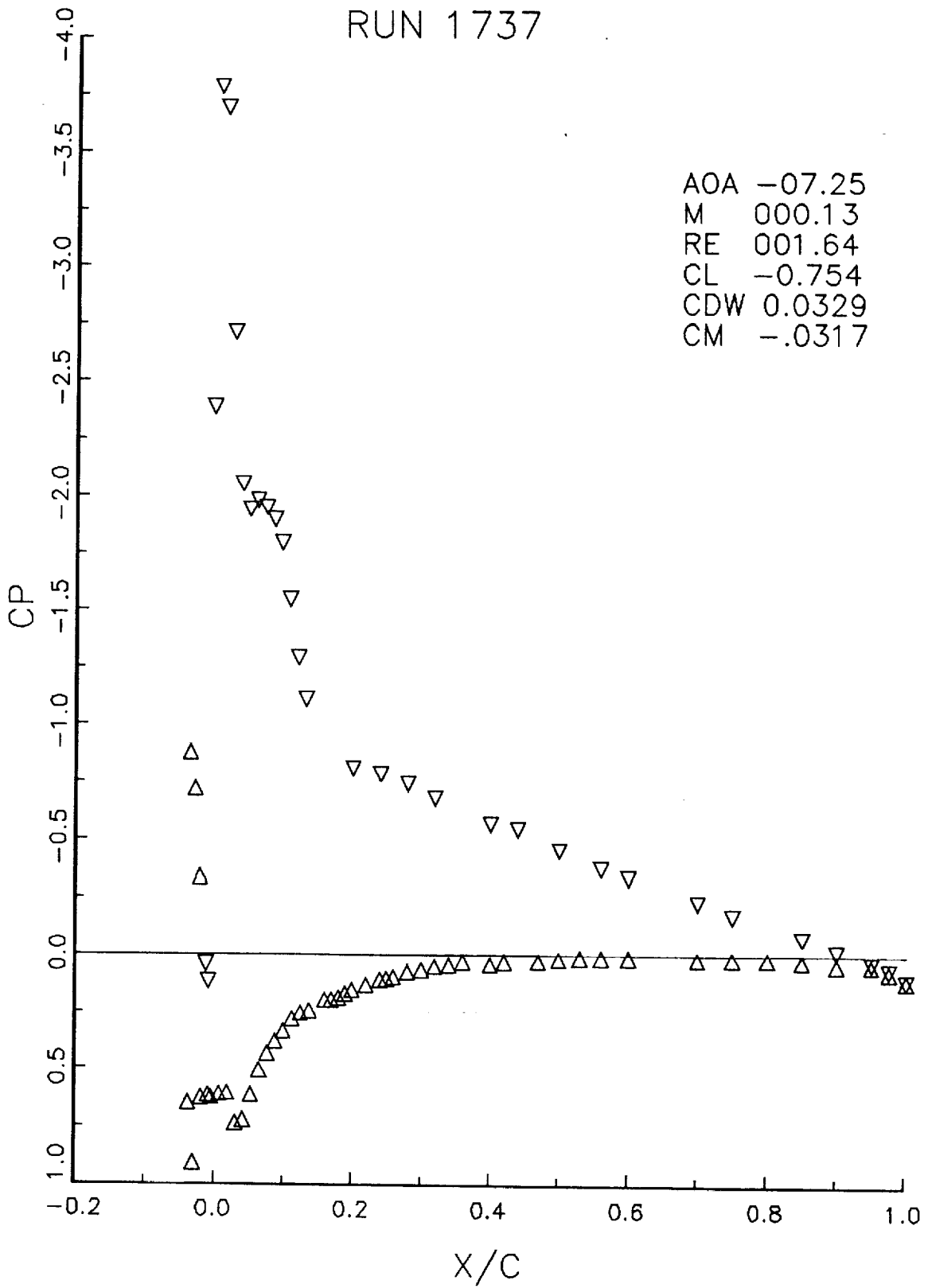




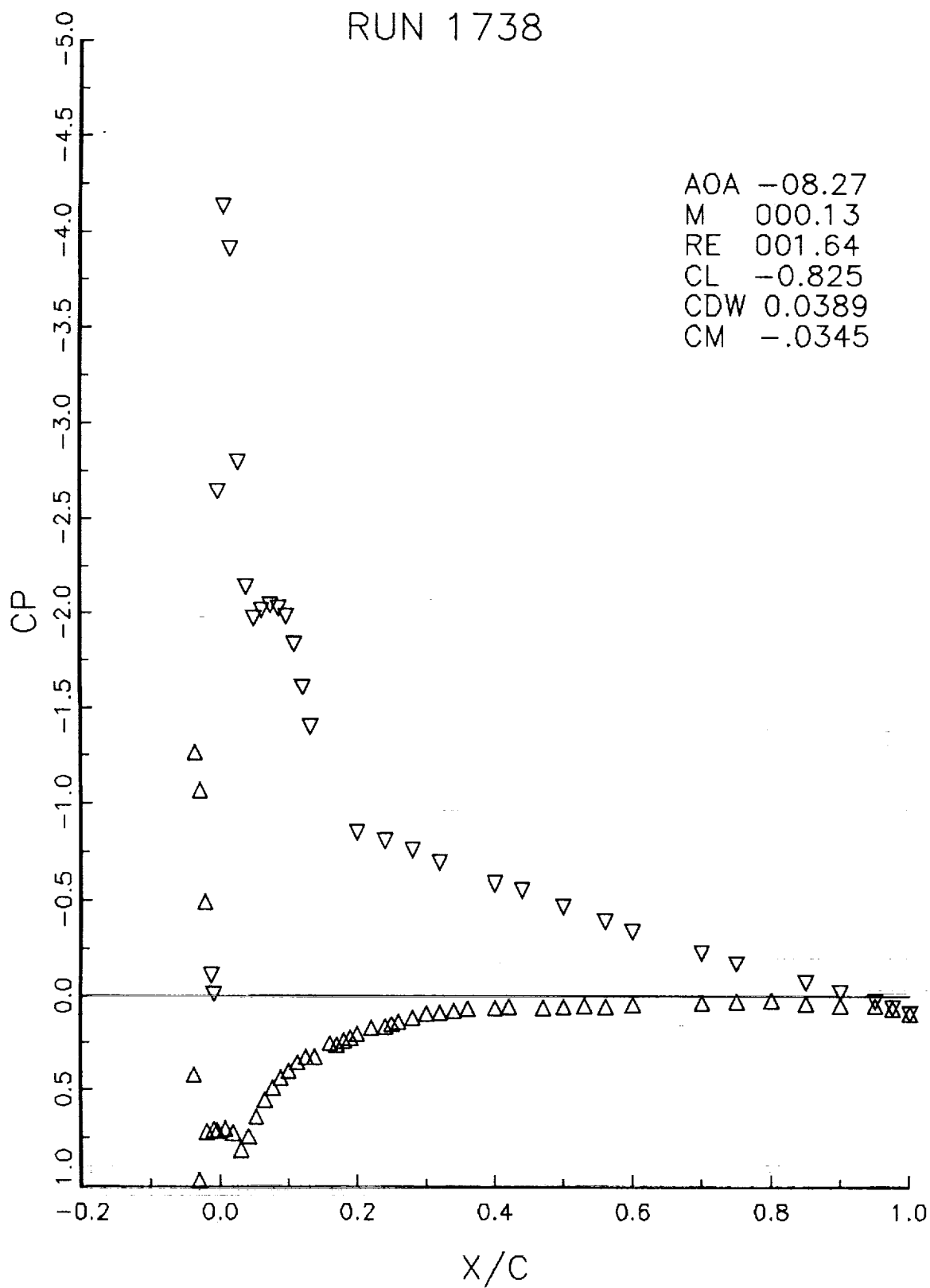
RUN 1736



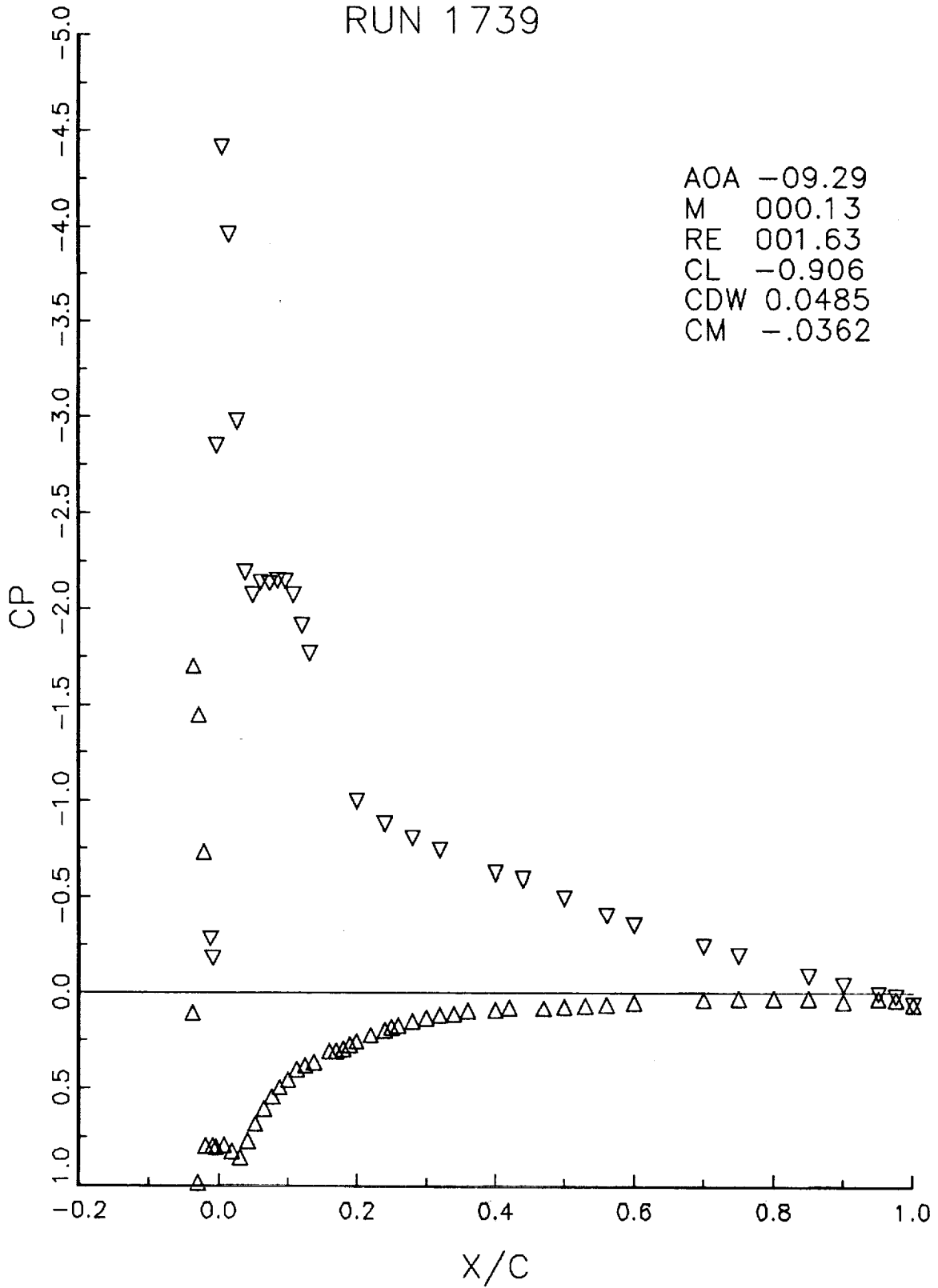
RUN 1737



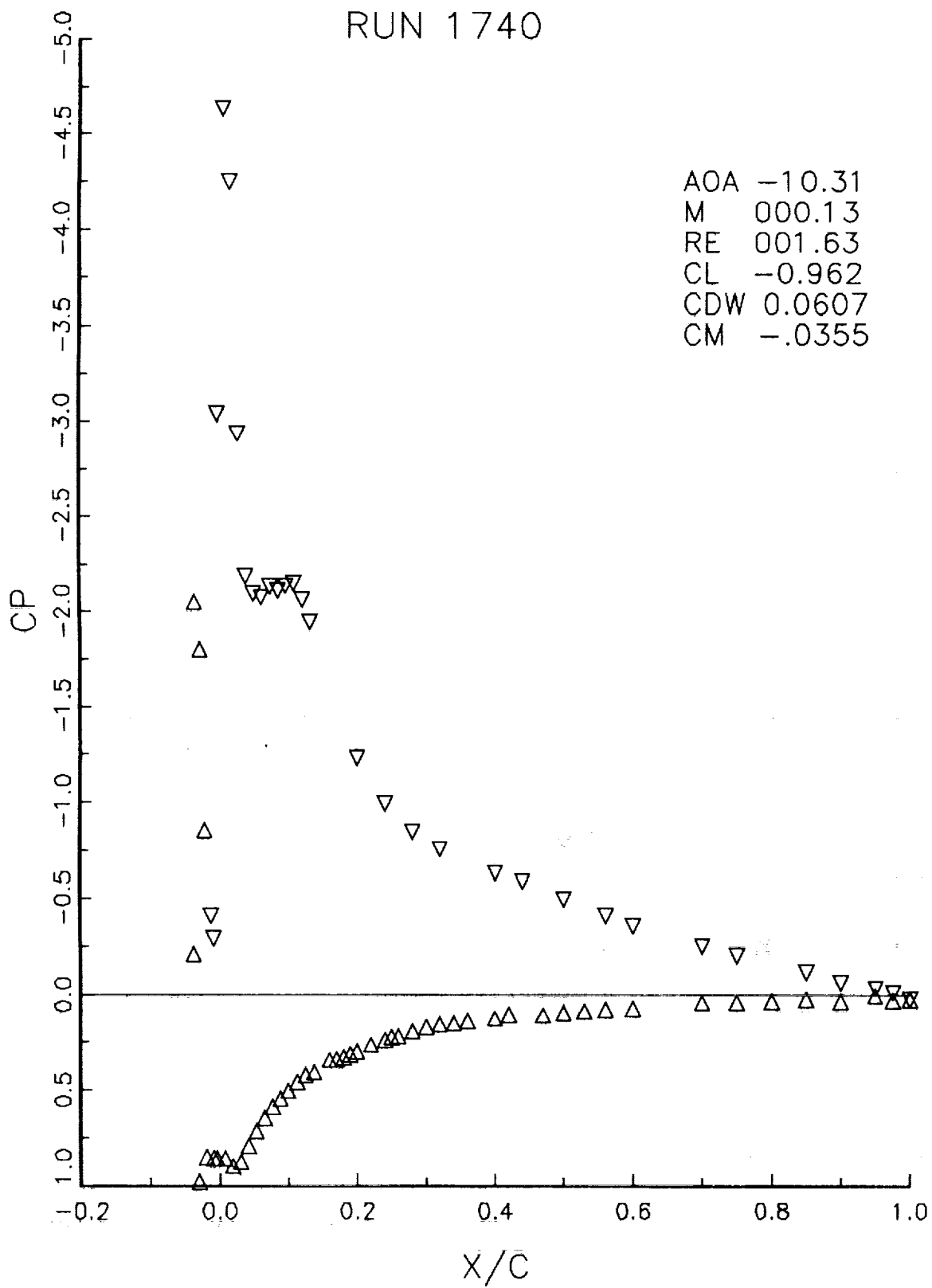
RUN 1738



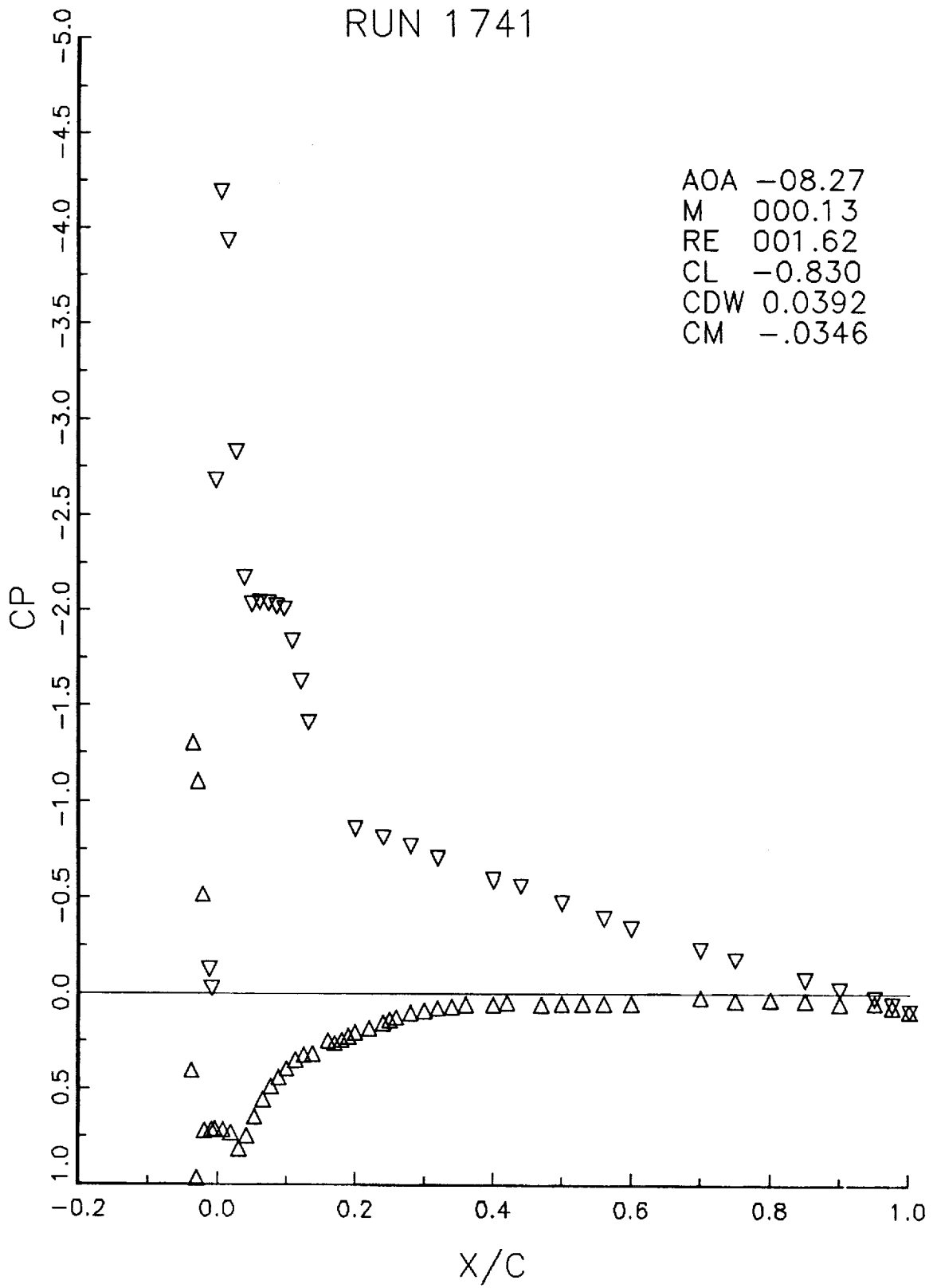
RUN 1739



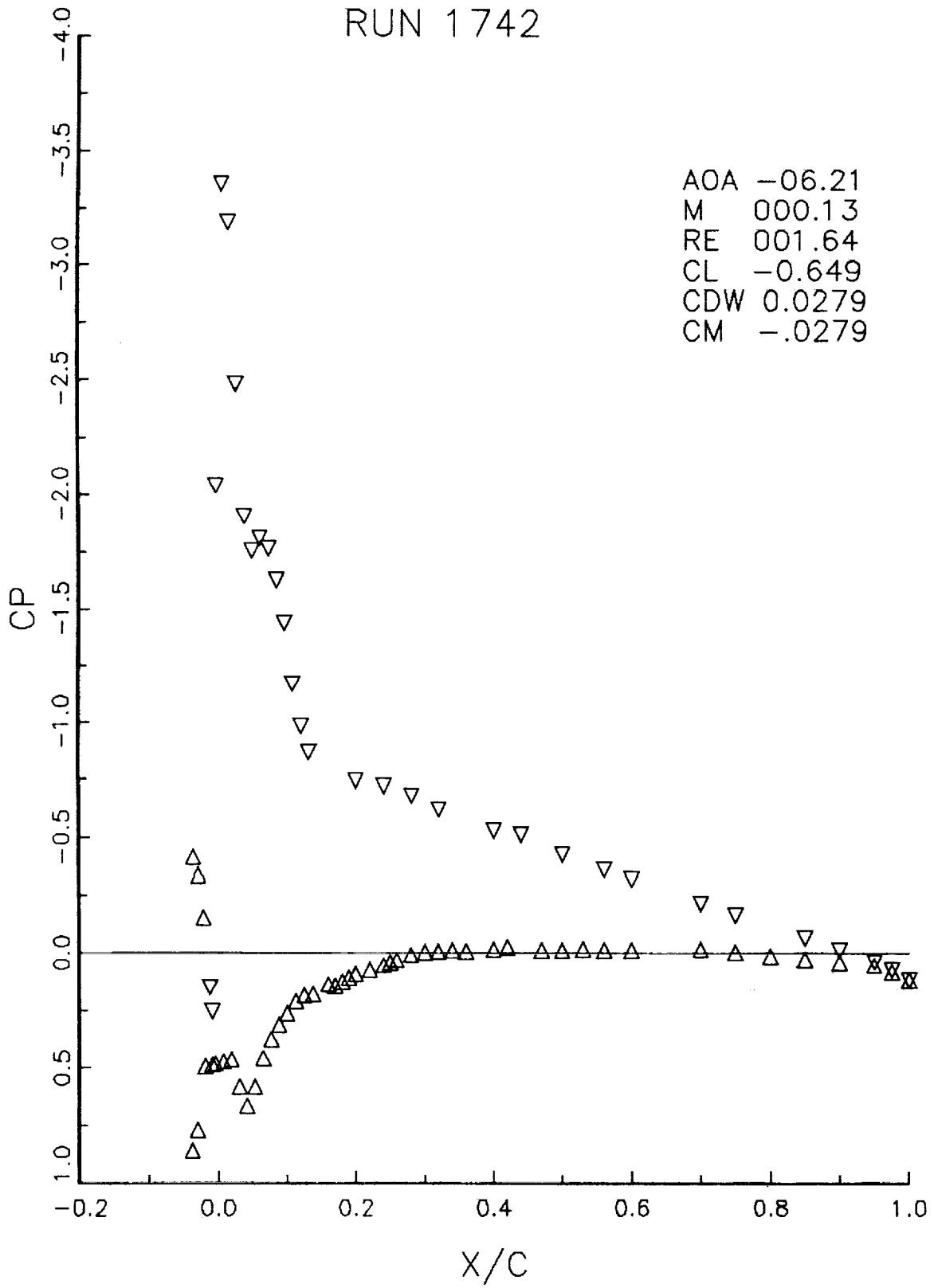
RUN 1740



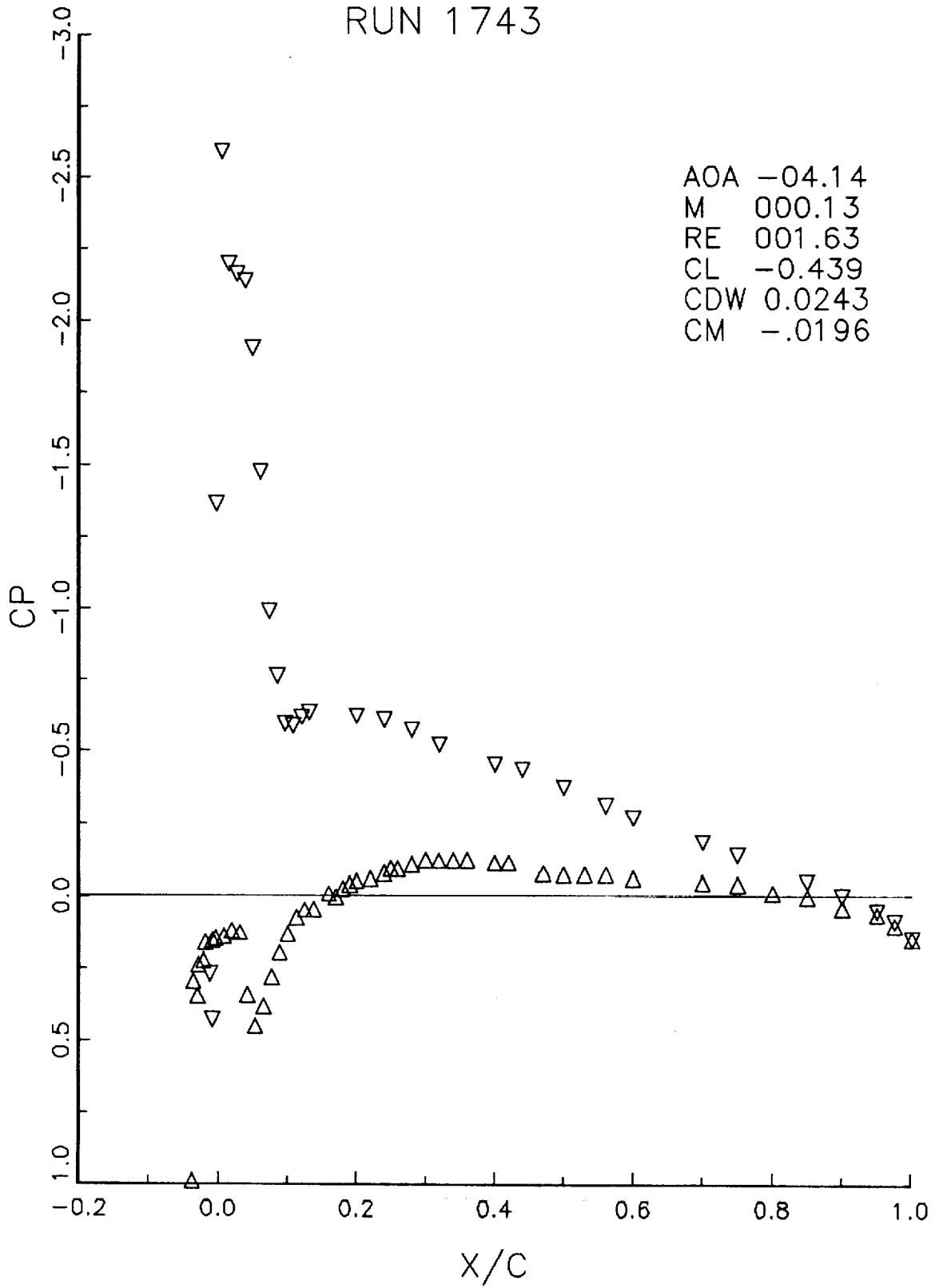
RUN 1741



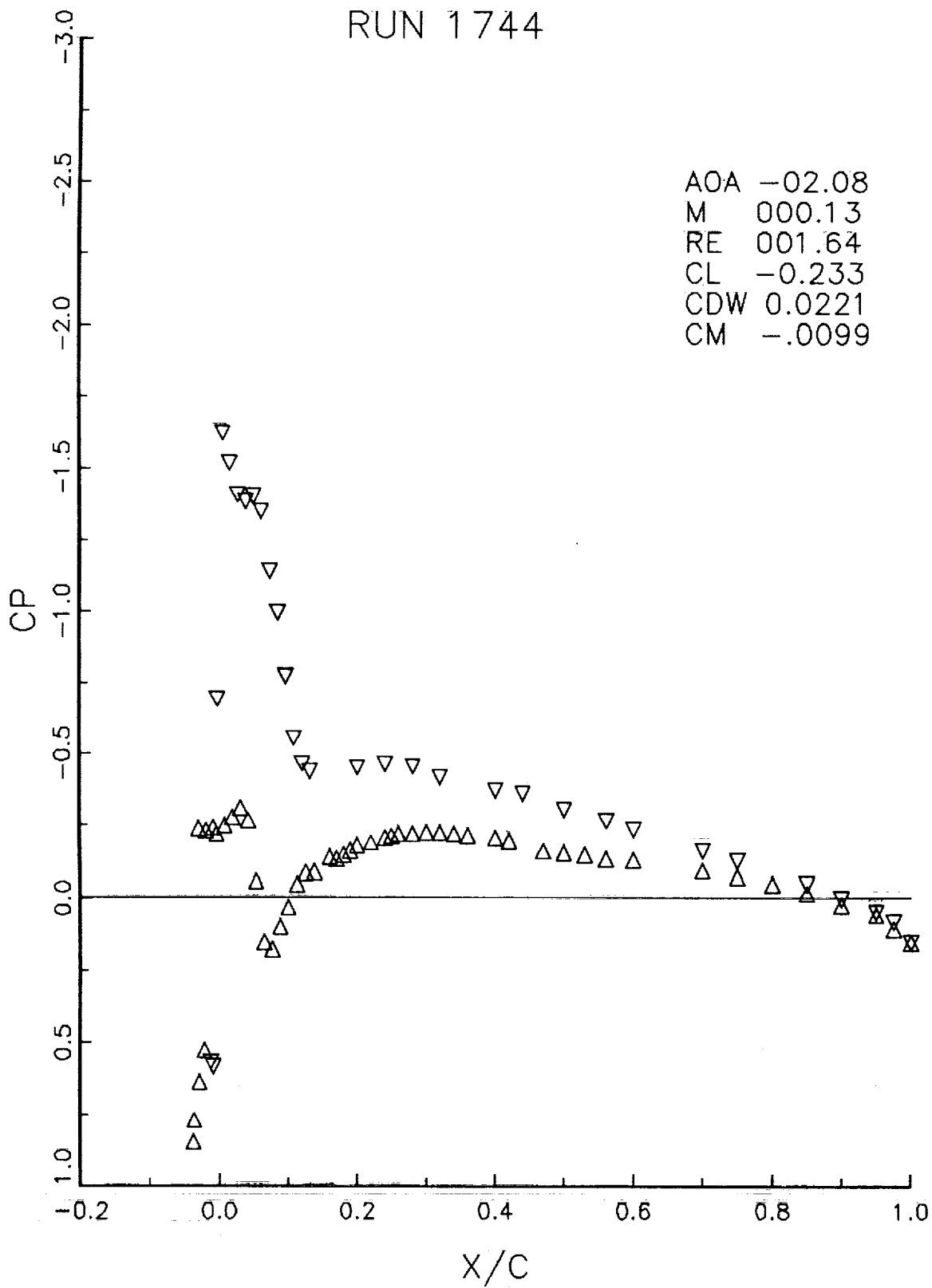
RUN 1742



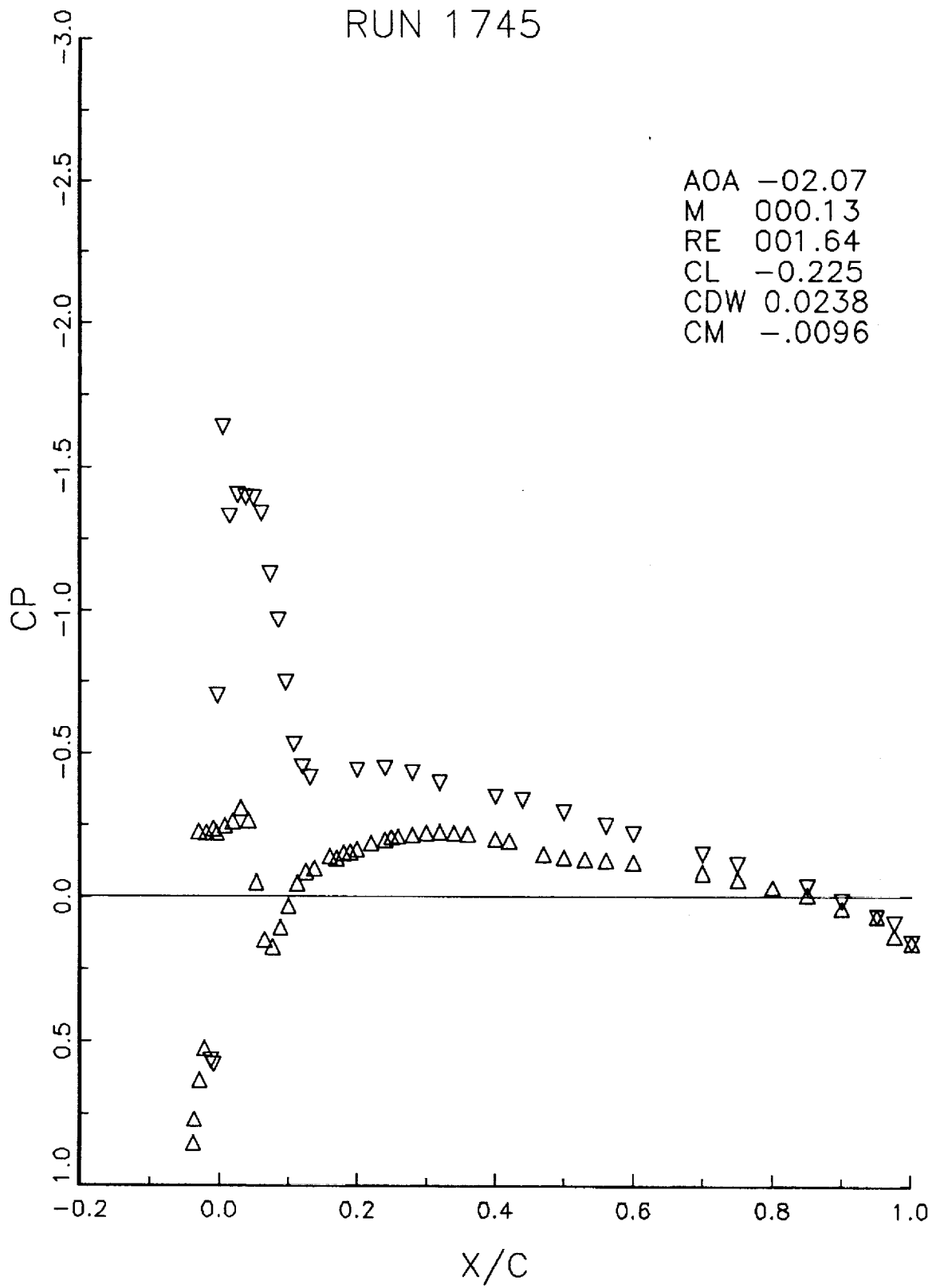
RUN 1743



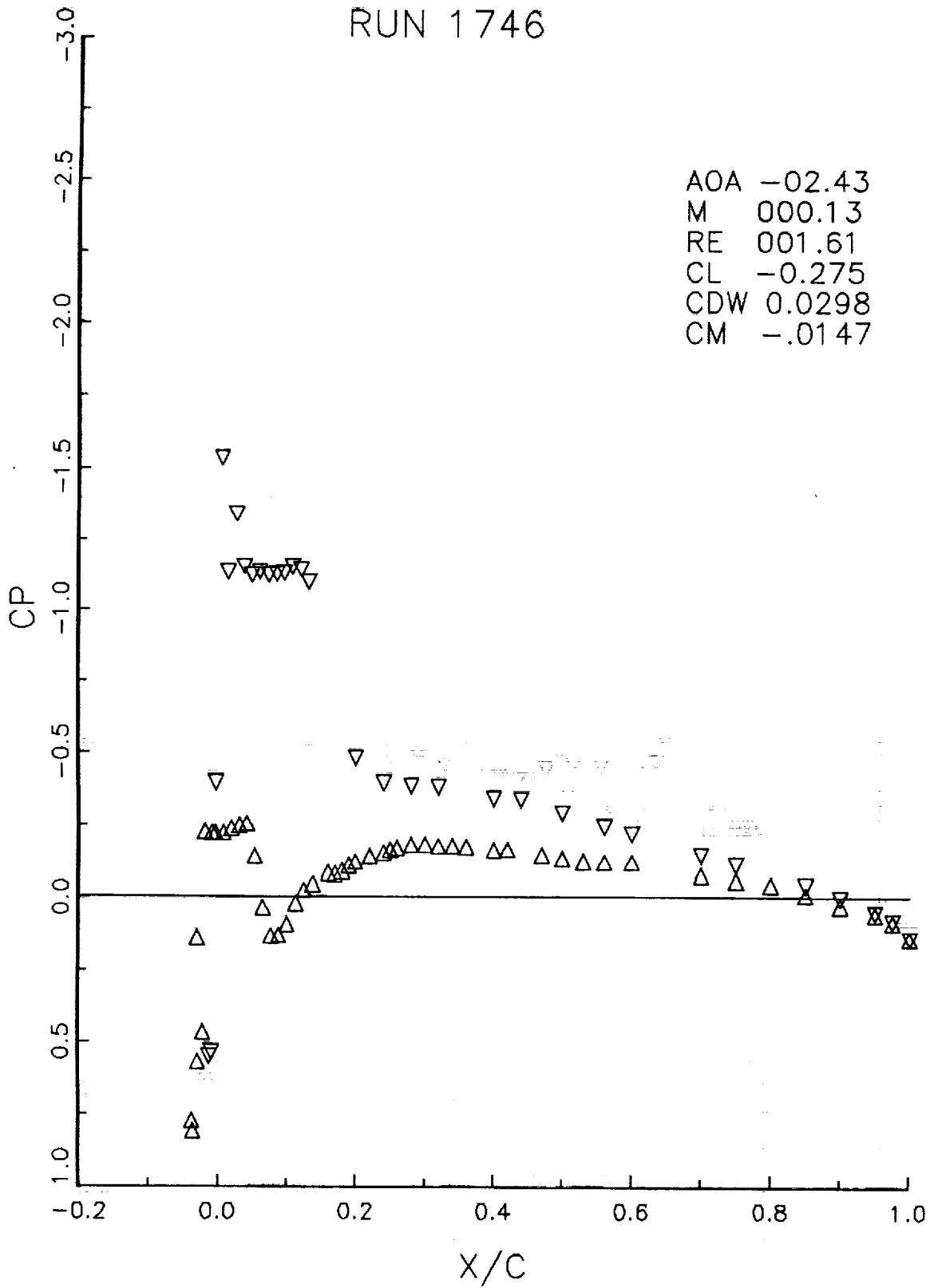
RUN 1744



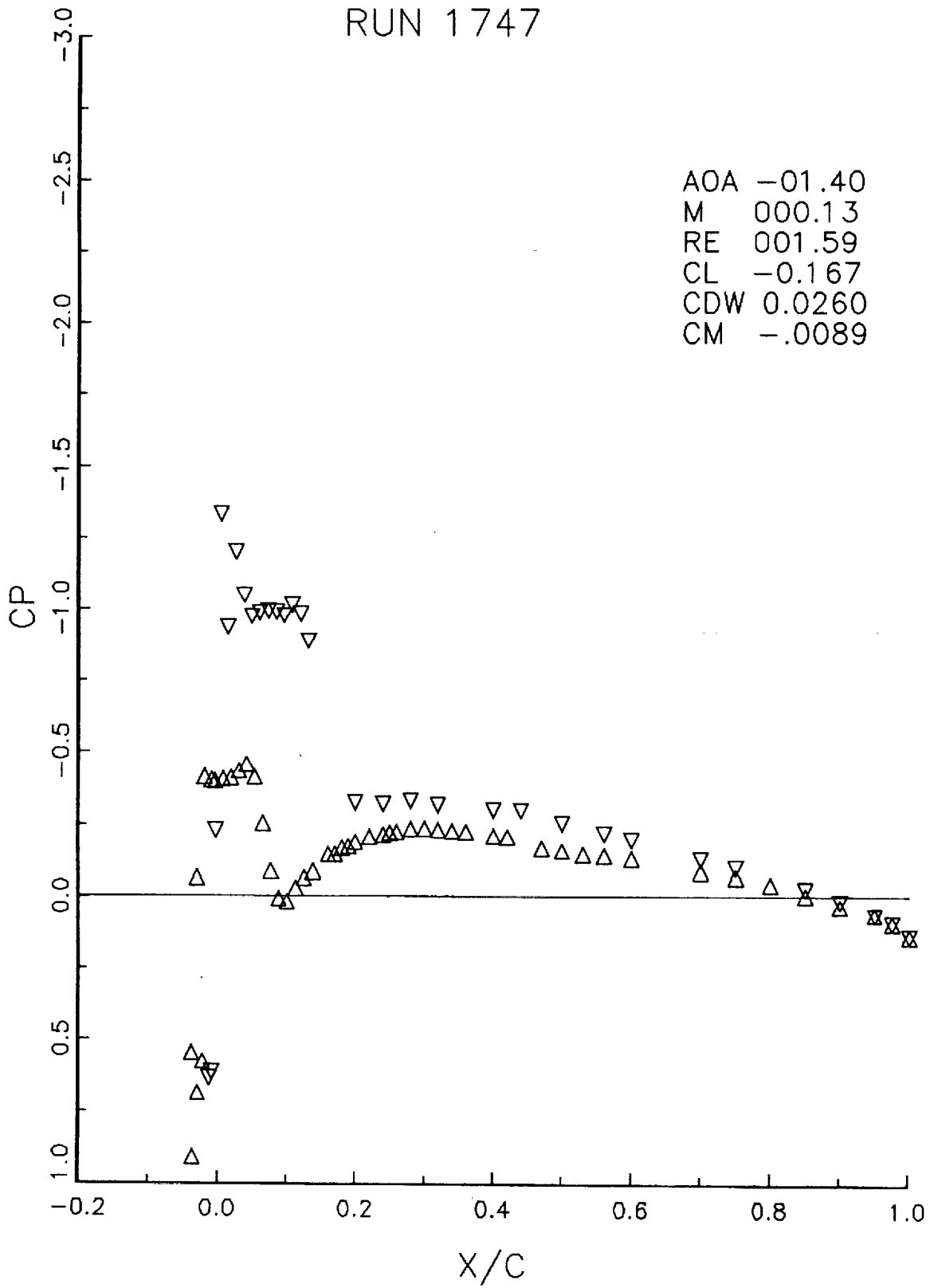
RUN 1745



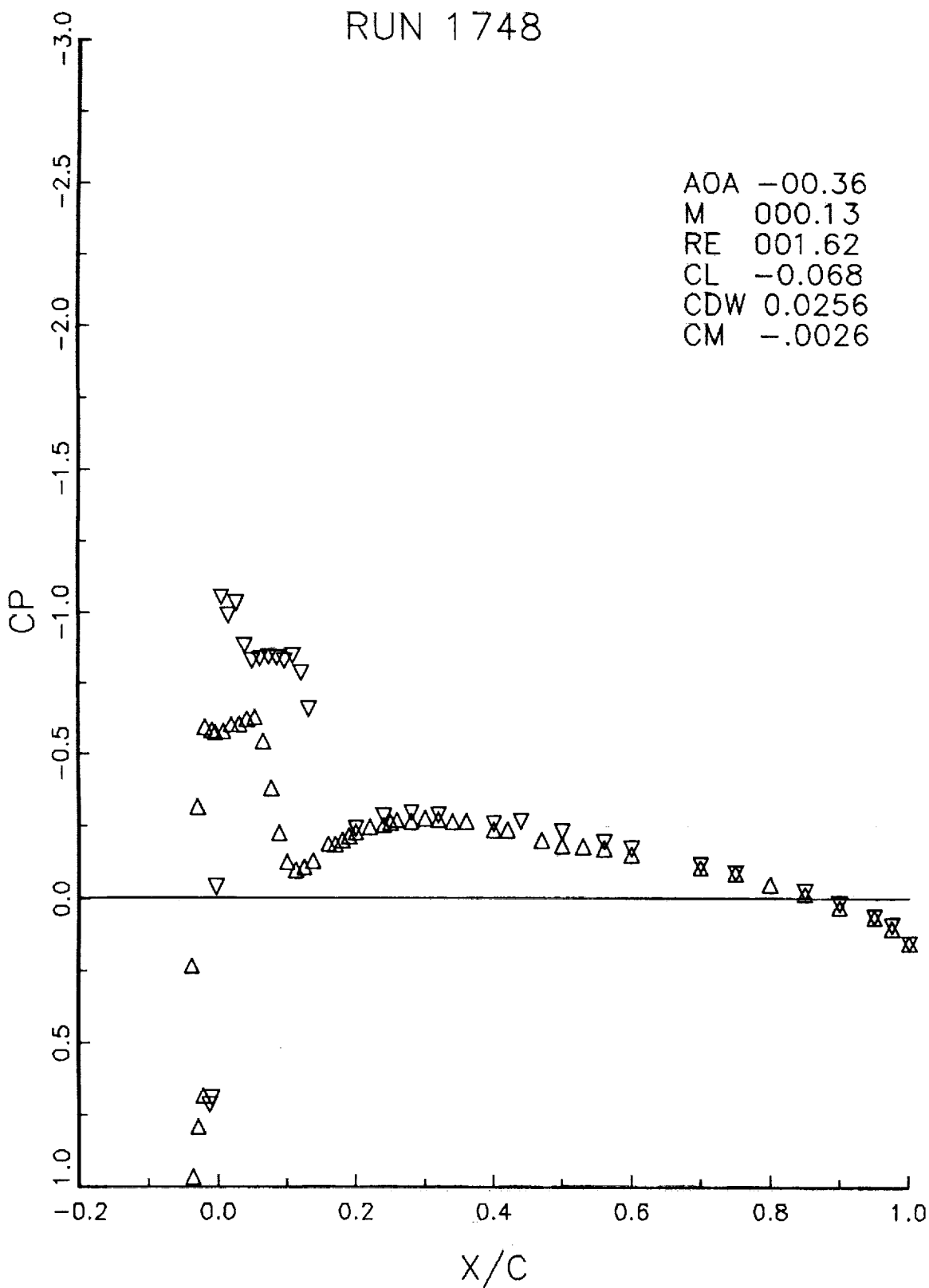
RUN 1746



RUN 1747

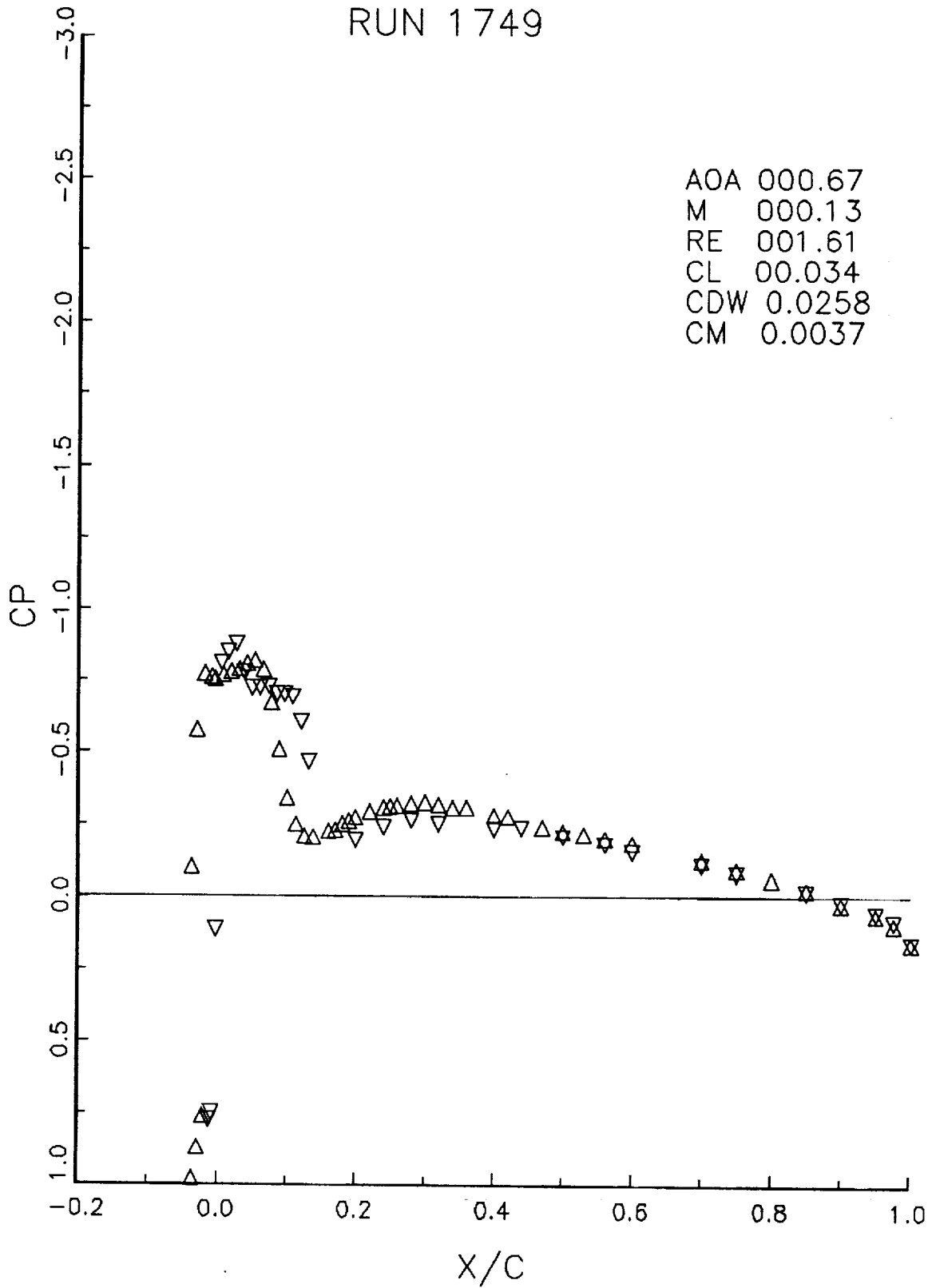


RUN 1748

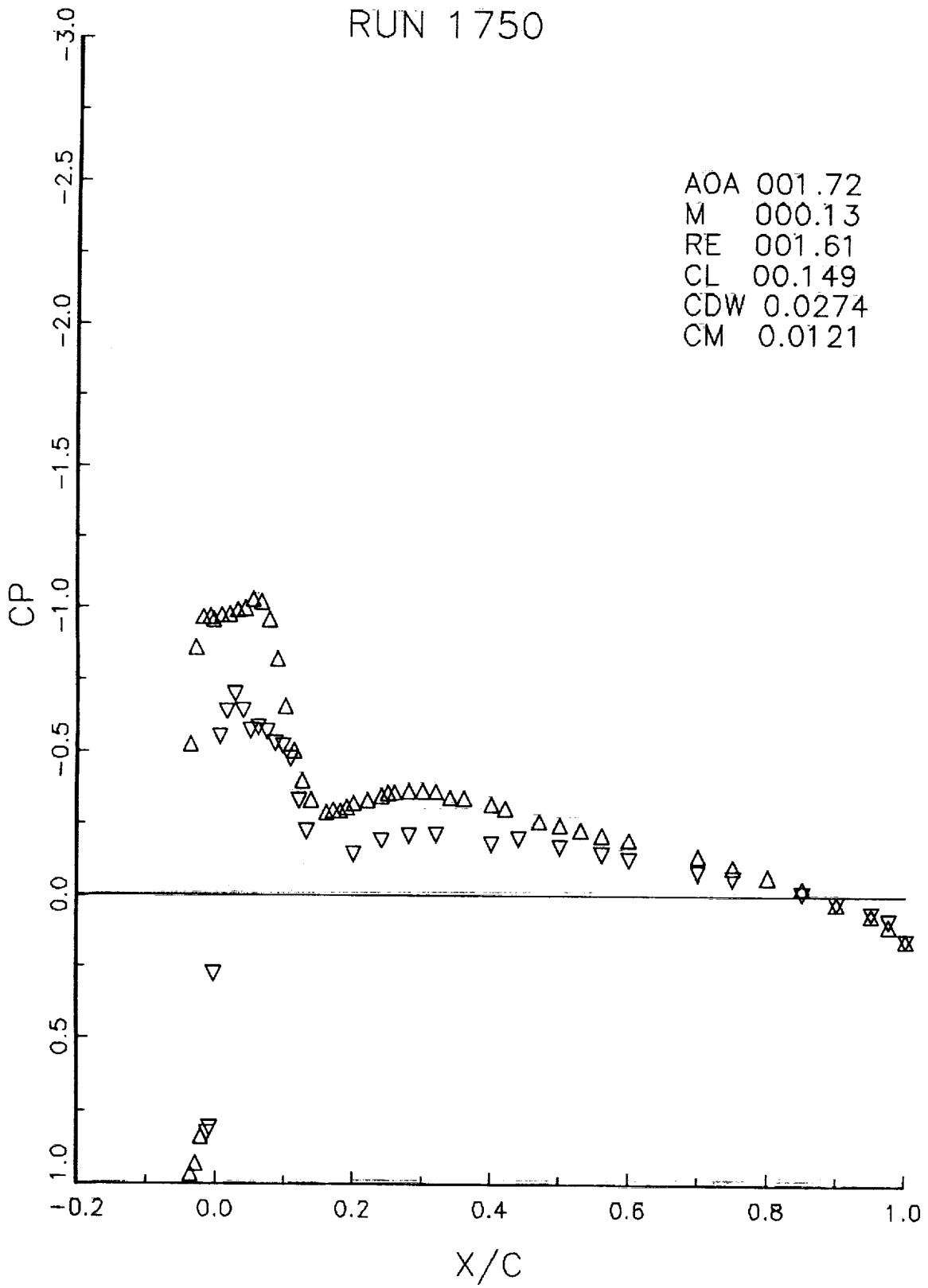


RUN 1749

AOA 000.67
M 000.13
RE 001.61
CL 00.034
CDW 0.0258
CM 0.0037

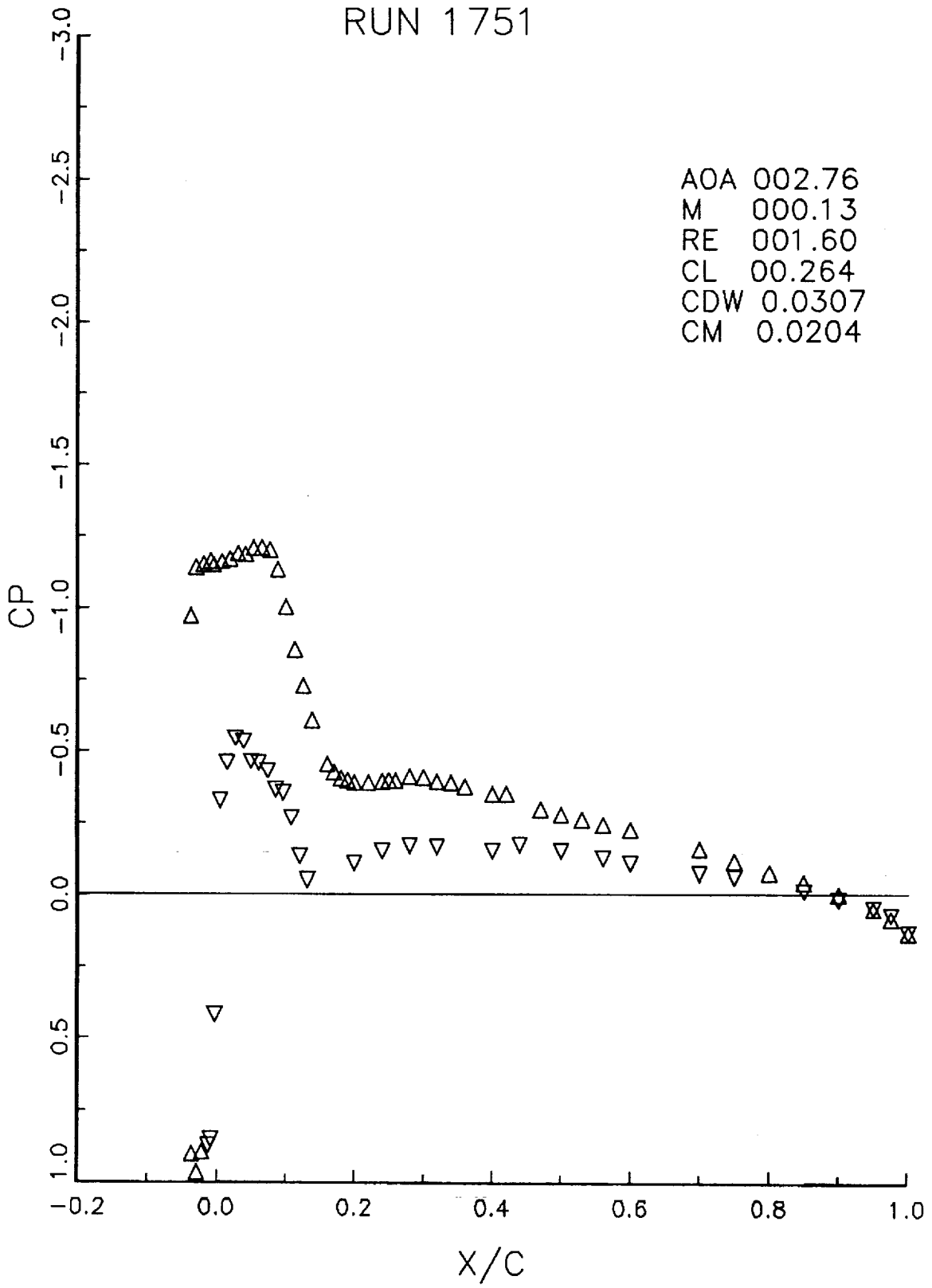


RUN 1750



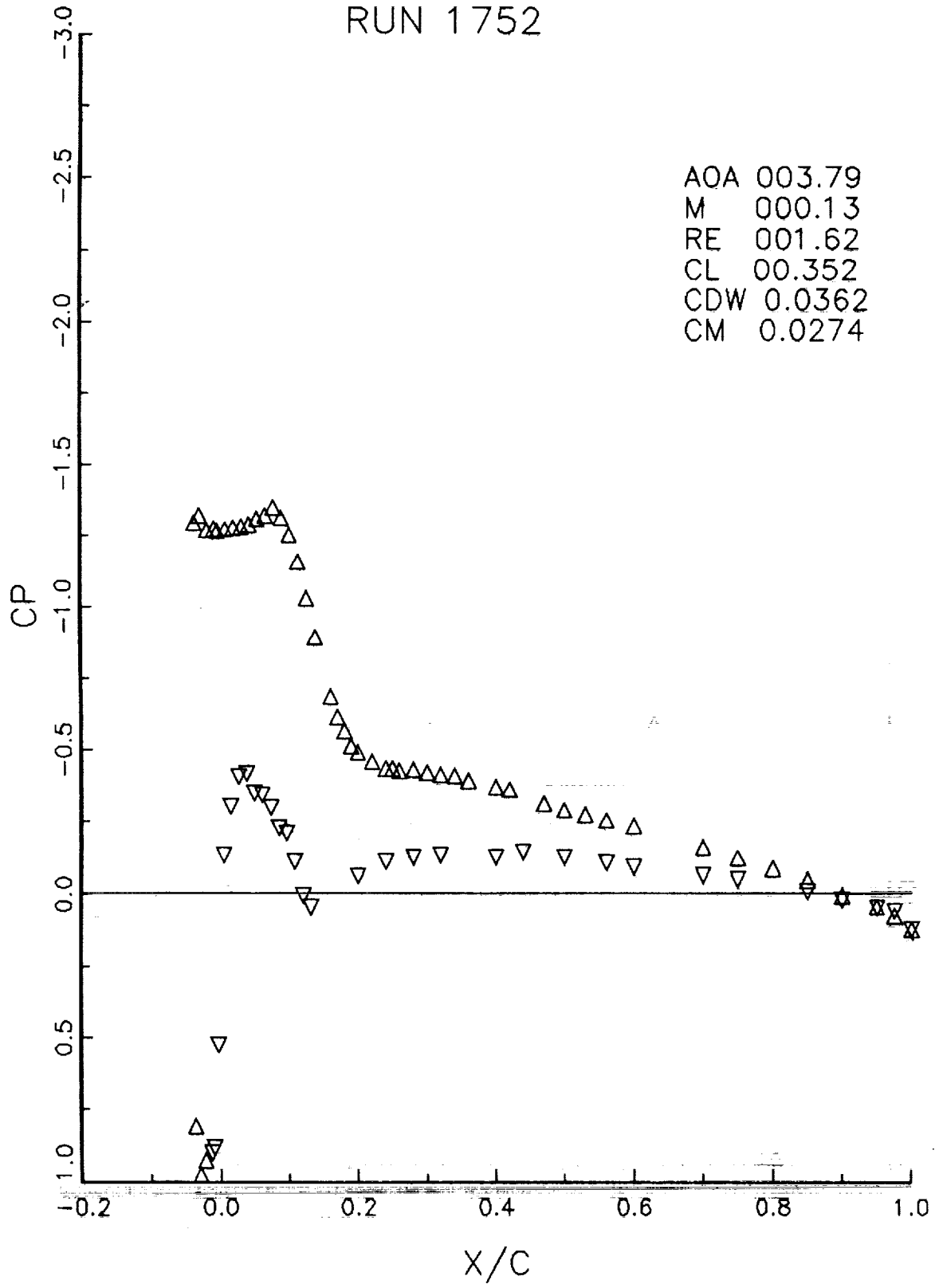
RUN 1751

AOA 002.76
M 000.13
RE 001.60
CL 00.264
CDW 0.0307
CM 0.0204



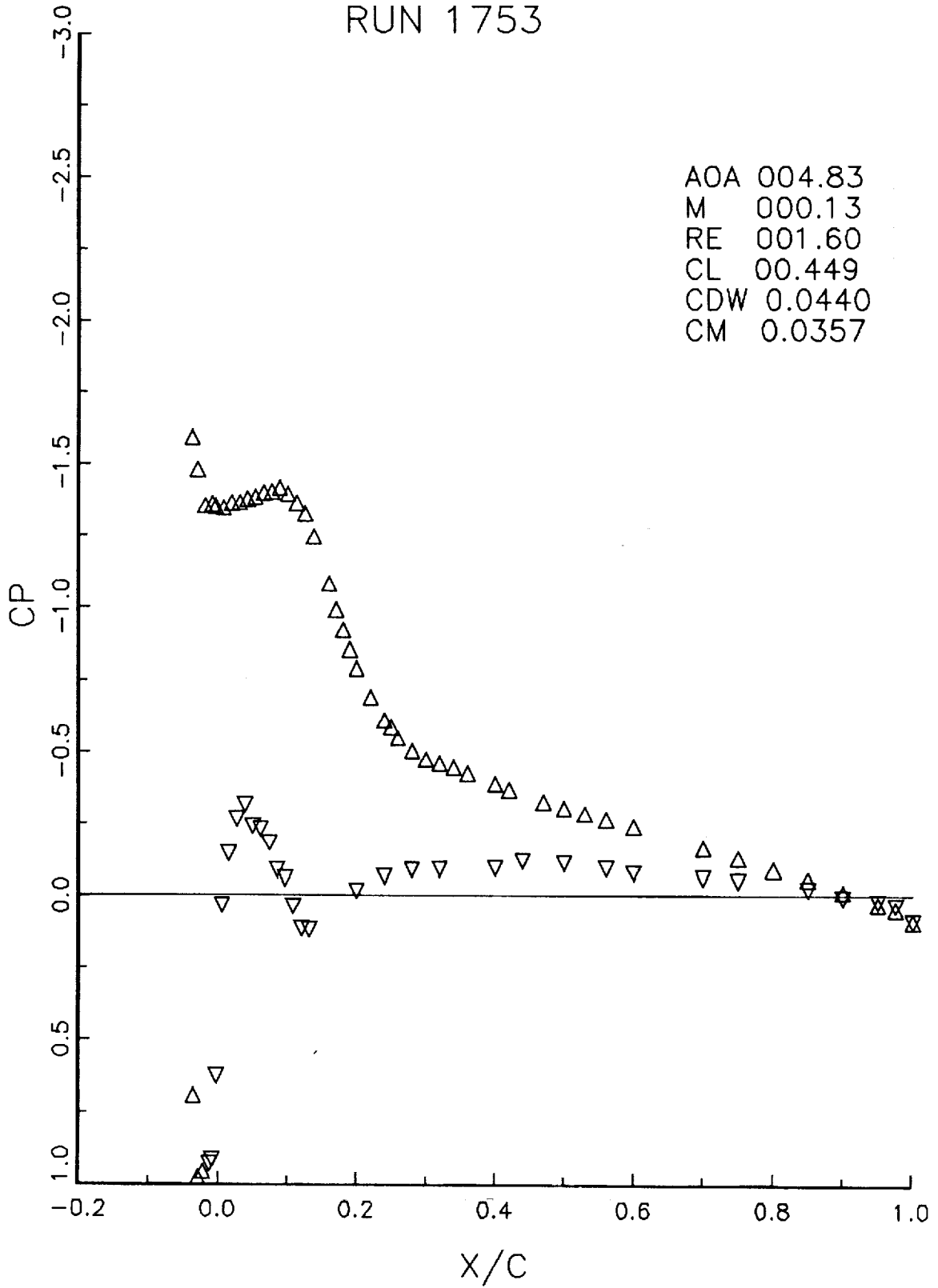
RUN 1752

AOA 003.79
M 000.13
RE 001.62
CL 00.352
CDW 0.0362
CM 0.0274

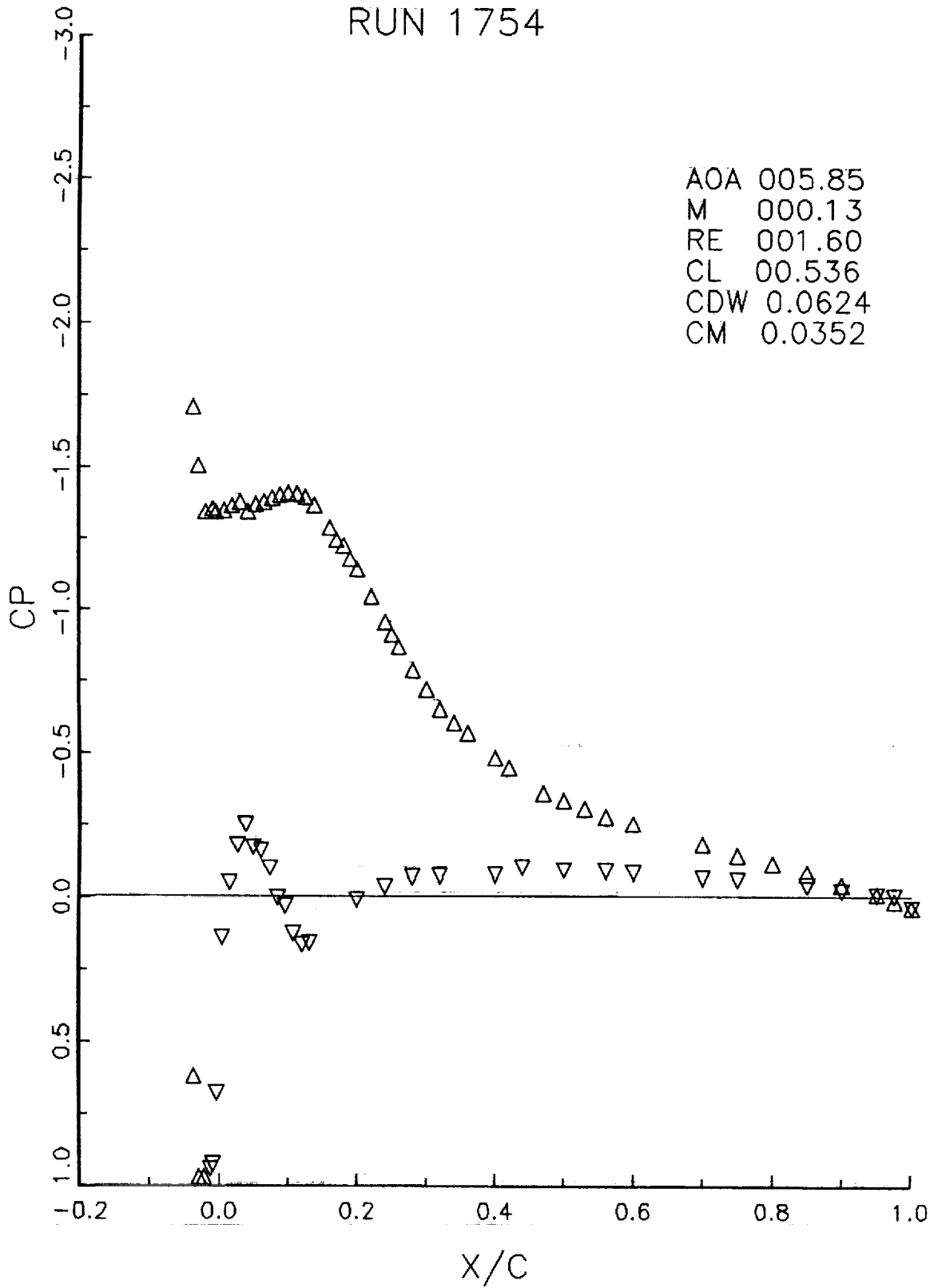


RUN 1753

AOA 004.83
M 000.13
RE 001.60
CL 00.449
CDW 0.0440
CM 0.0357

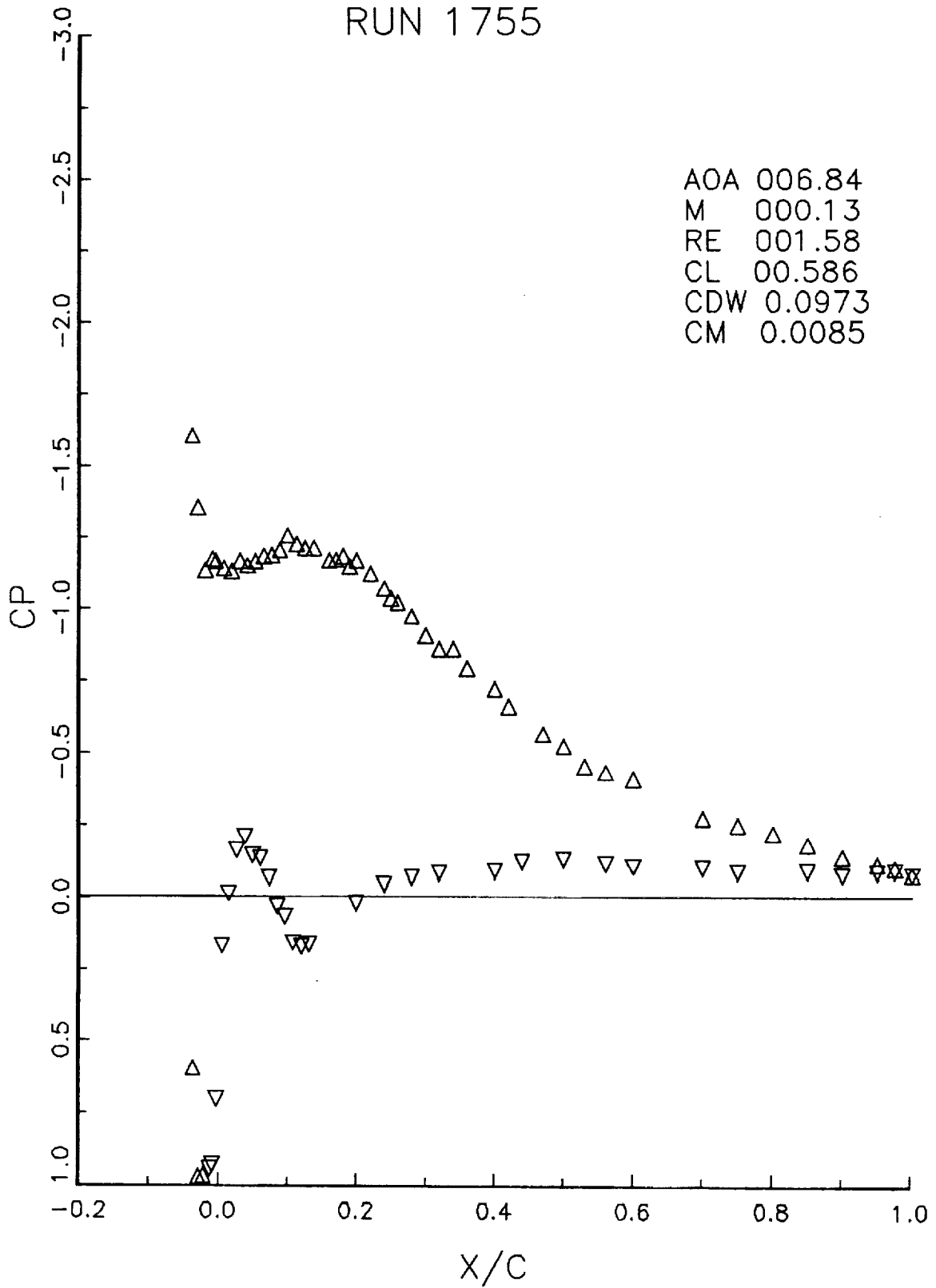


RUN 1754



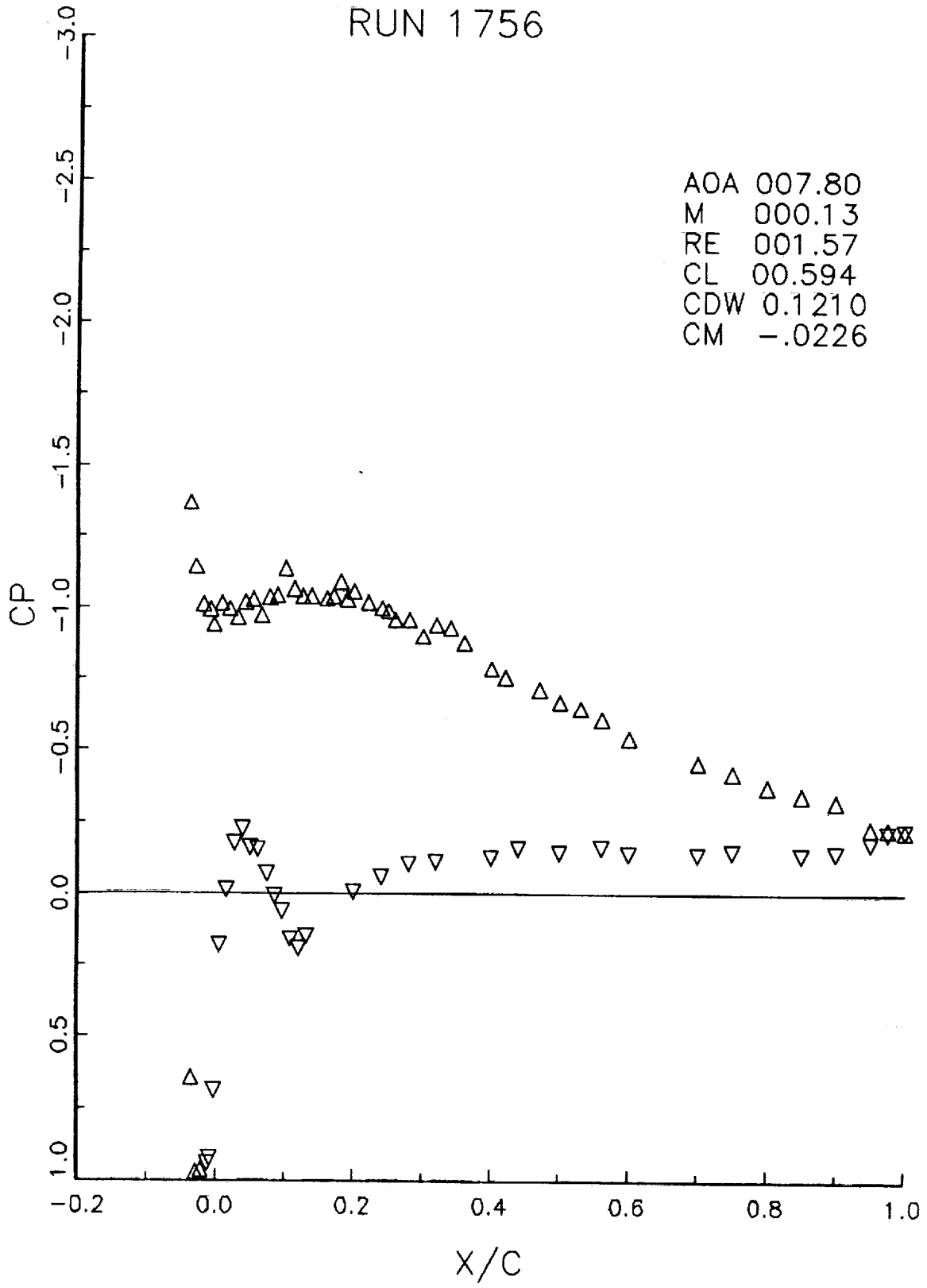
RUN 1755

AOA 006.84
M 000.13
RE 001.58
CL 00.586
CDW 0.0973
CM 0.0085



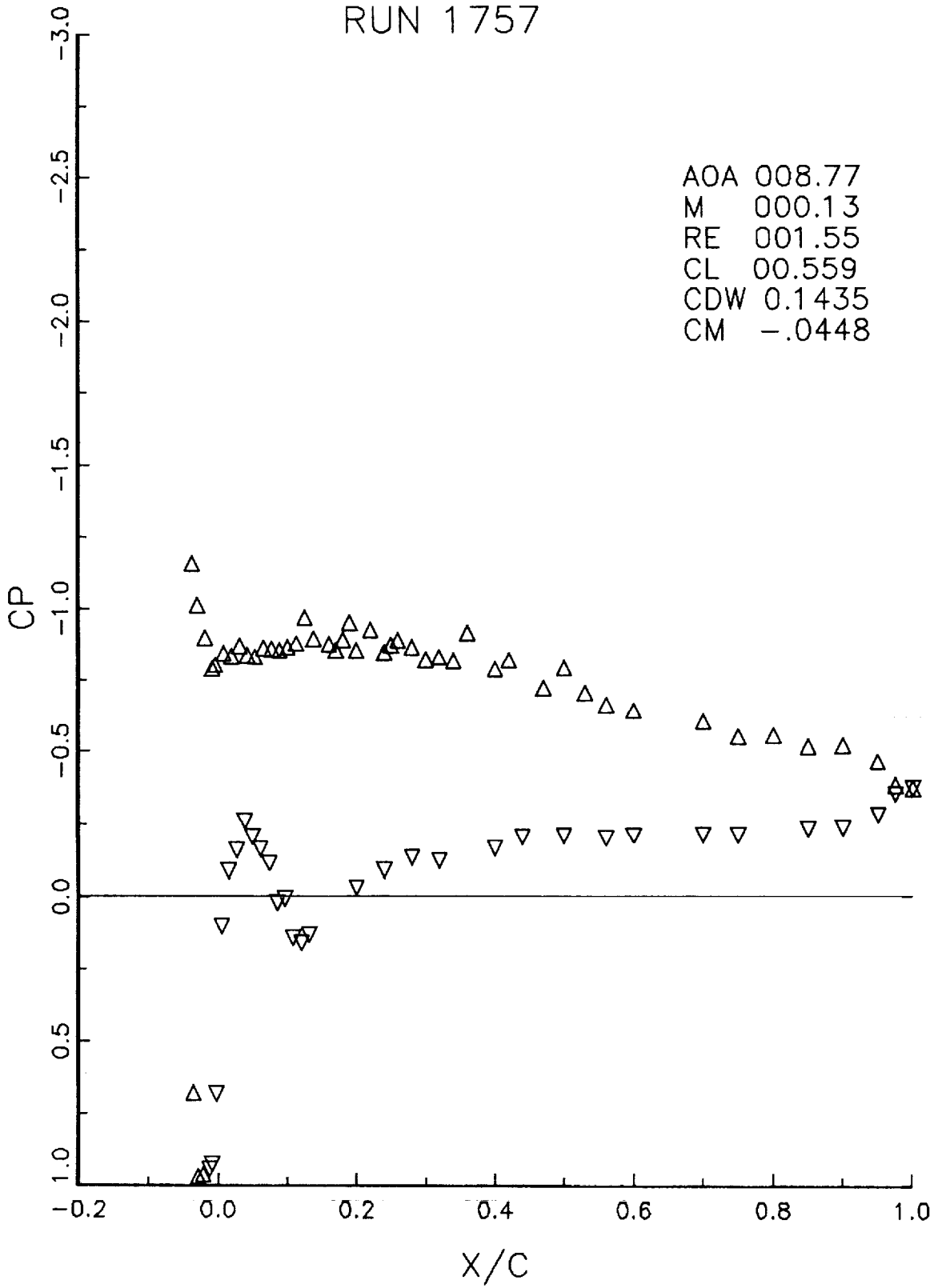
RUN 1756

AOA 007.80
M 000.13
RE 001.57
CL 00.594
CDW 0.1210
CM -.0226

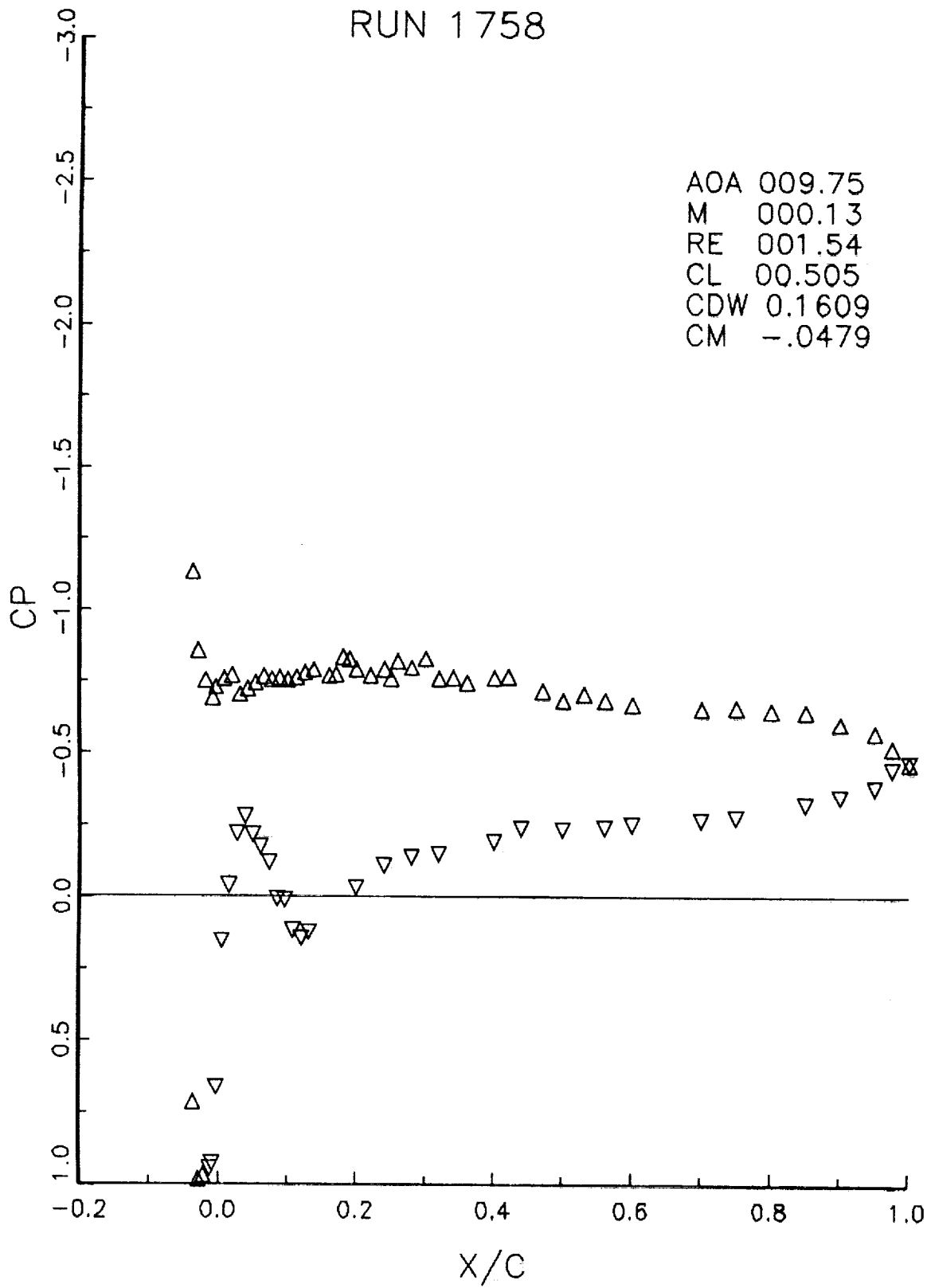


RUN 1757

AOA 008.77
M 000.13
RE 001.55
CL 00.559
CDW 0.1435
CM -0.0448

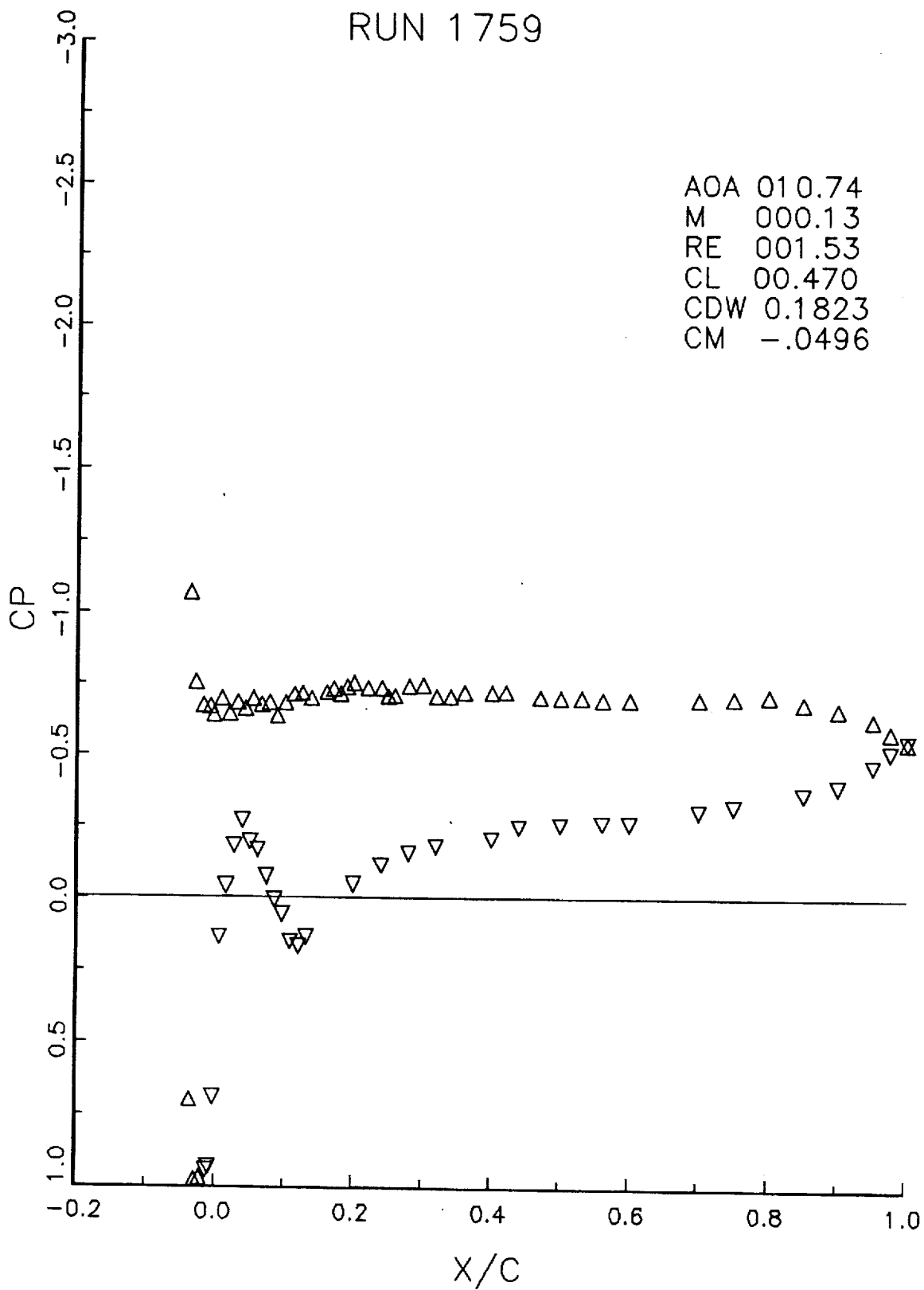


RUN 1758



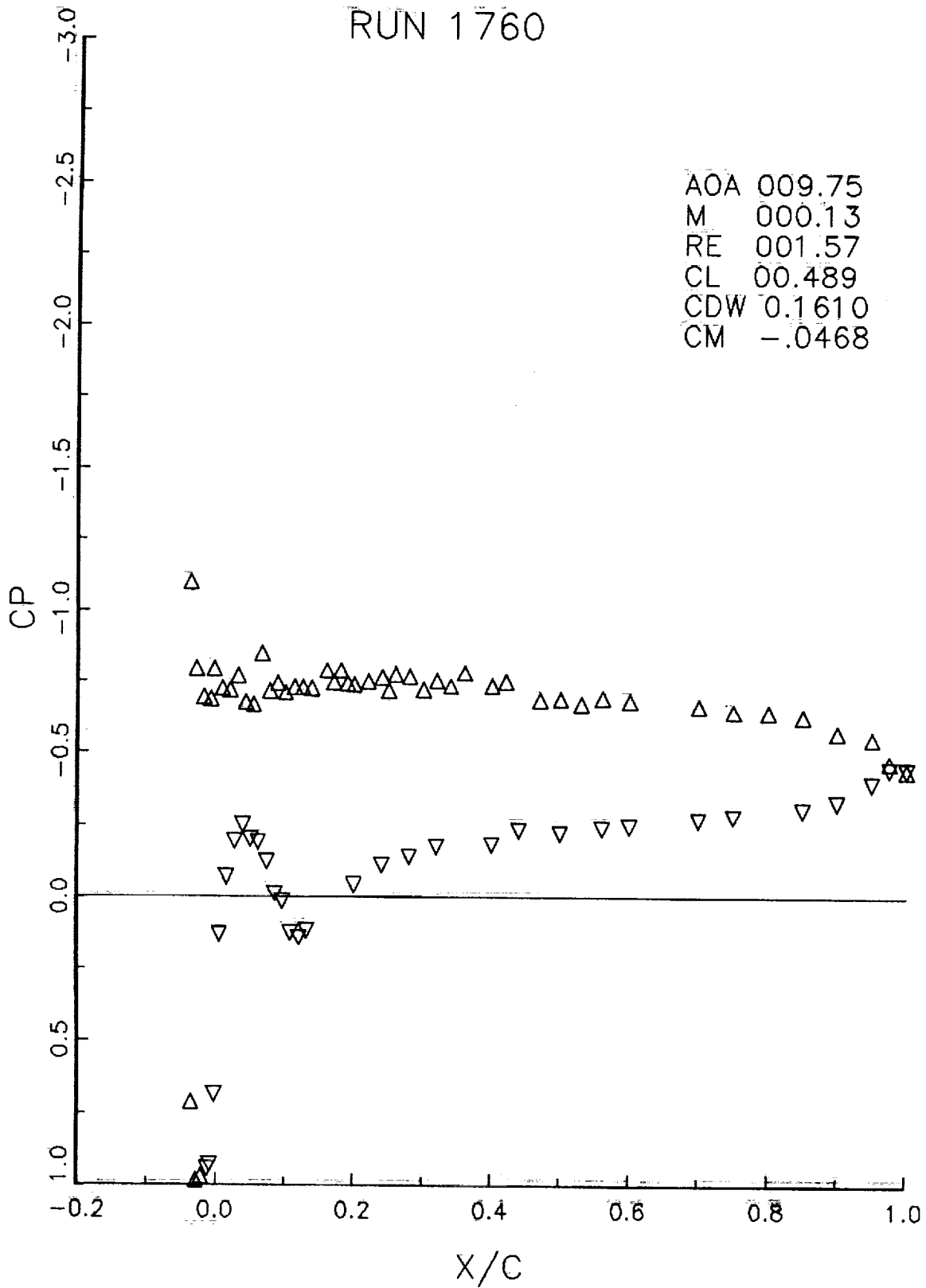
RUN 1759

AOA 010.74
M 000.13
RE 001.53
CL 00.470
CDW 0.1823
CM -0.0496



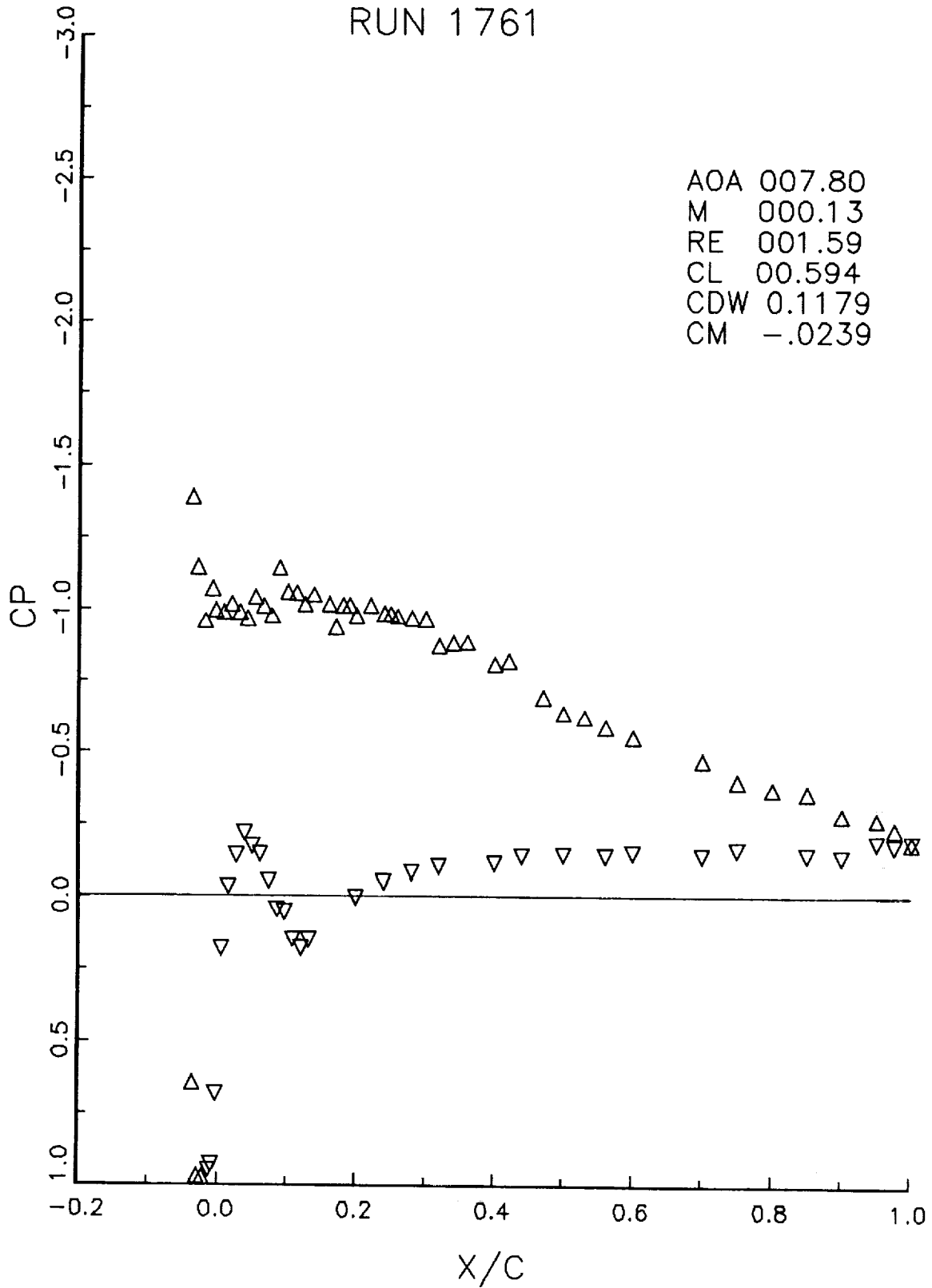
RUN 1760

AOA 009.75
M 000.13
RE 001.57
CL 00.489
CDW 0.1610
CM -0.0468



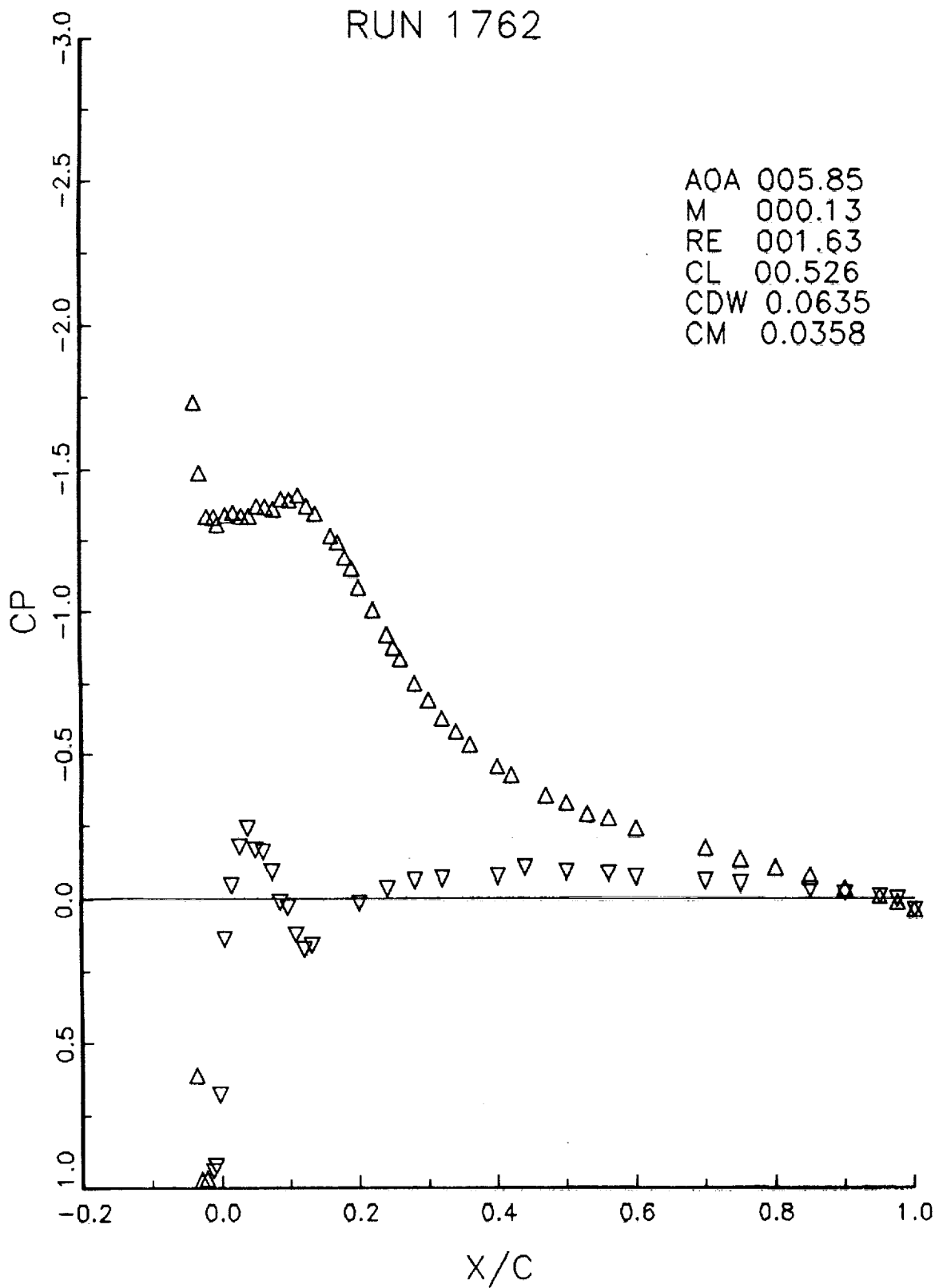
RUN 1761

AOA 007.80
M 000.13
RE 001.59
CL 00.594
CDW 0.1179
CM -.0239



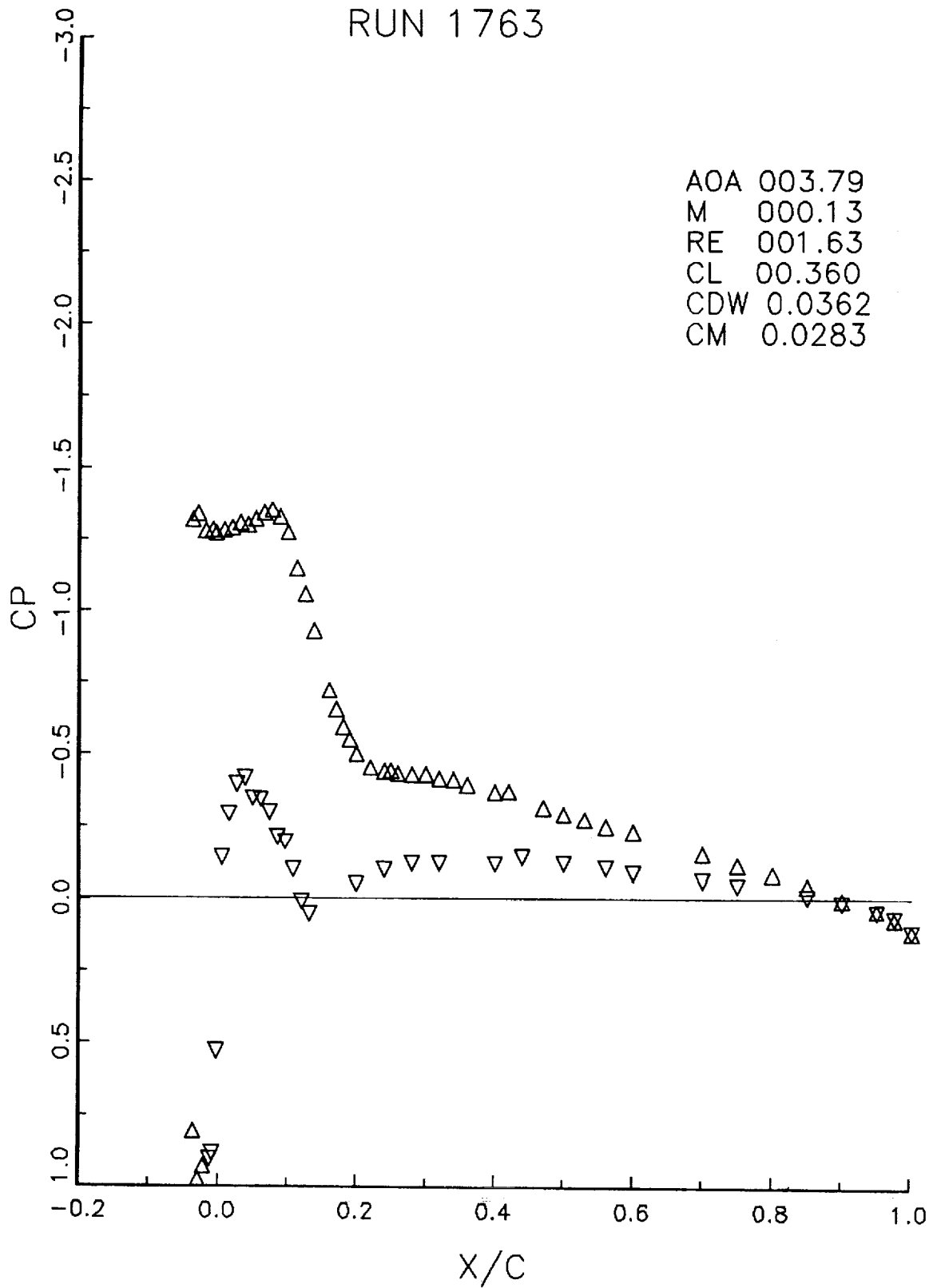
RUN 1762

AOA 005.85
M 000.13
RE 001.63
CL 00.526
CDW 0.0635
CM 0.0358

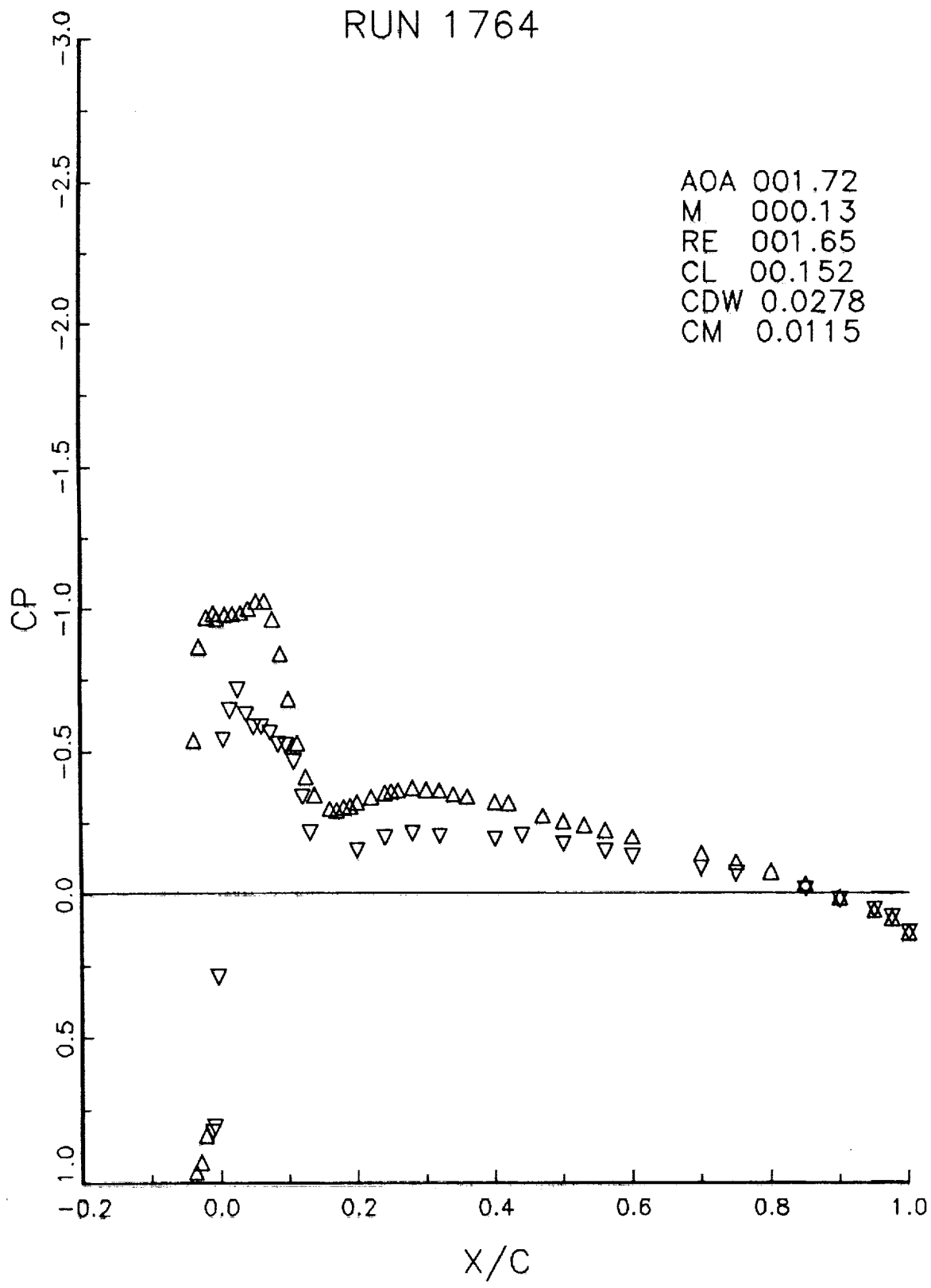


RUN 1763

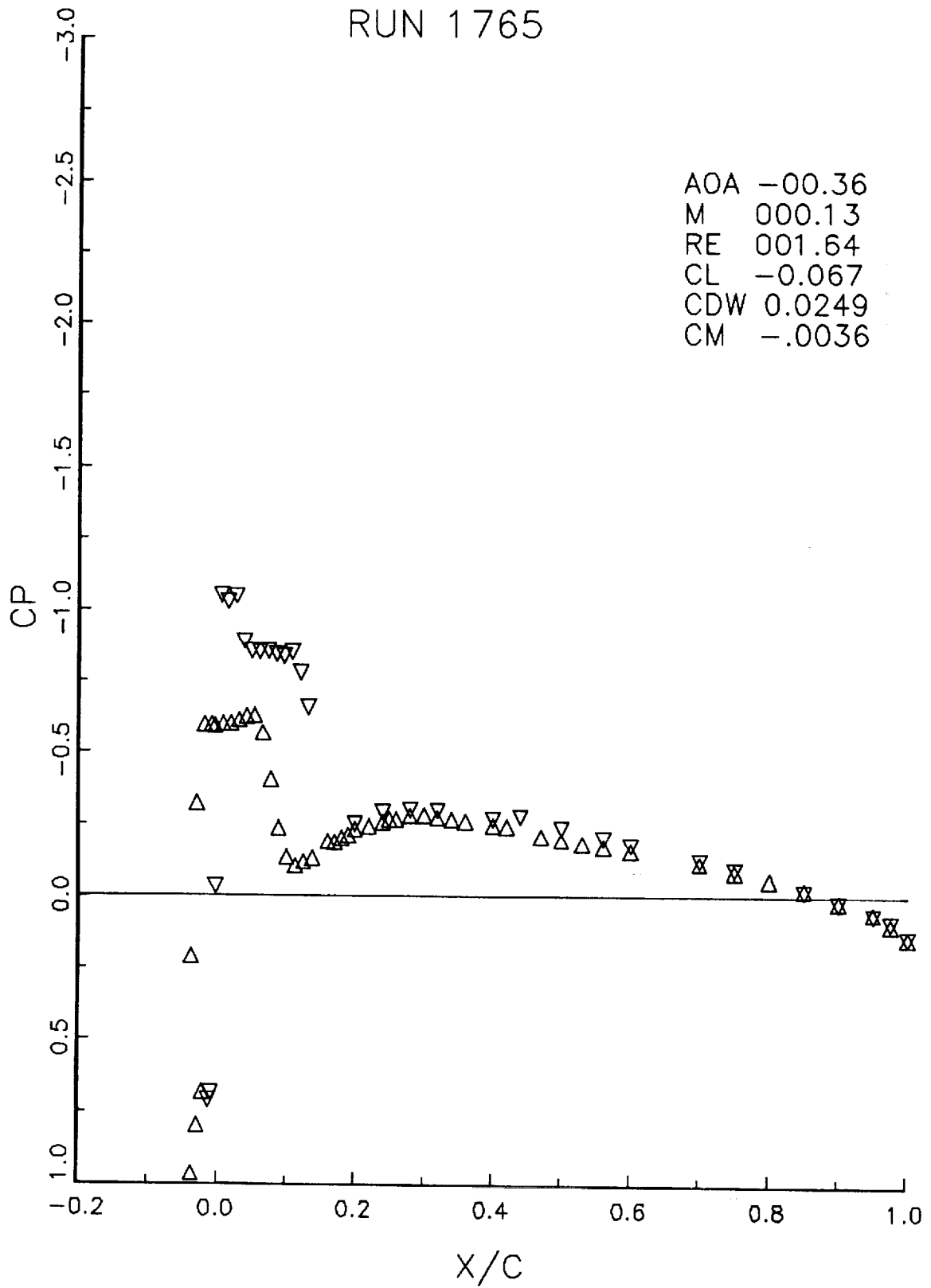
AOA 003.79
M 000.13
RE 001.63
CL 00.360
CDW 0.0362
CM 0.0283



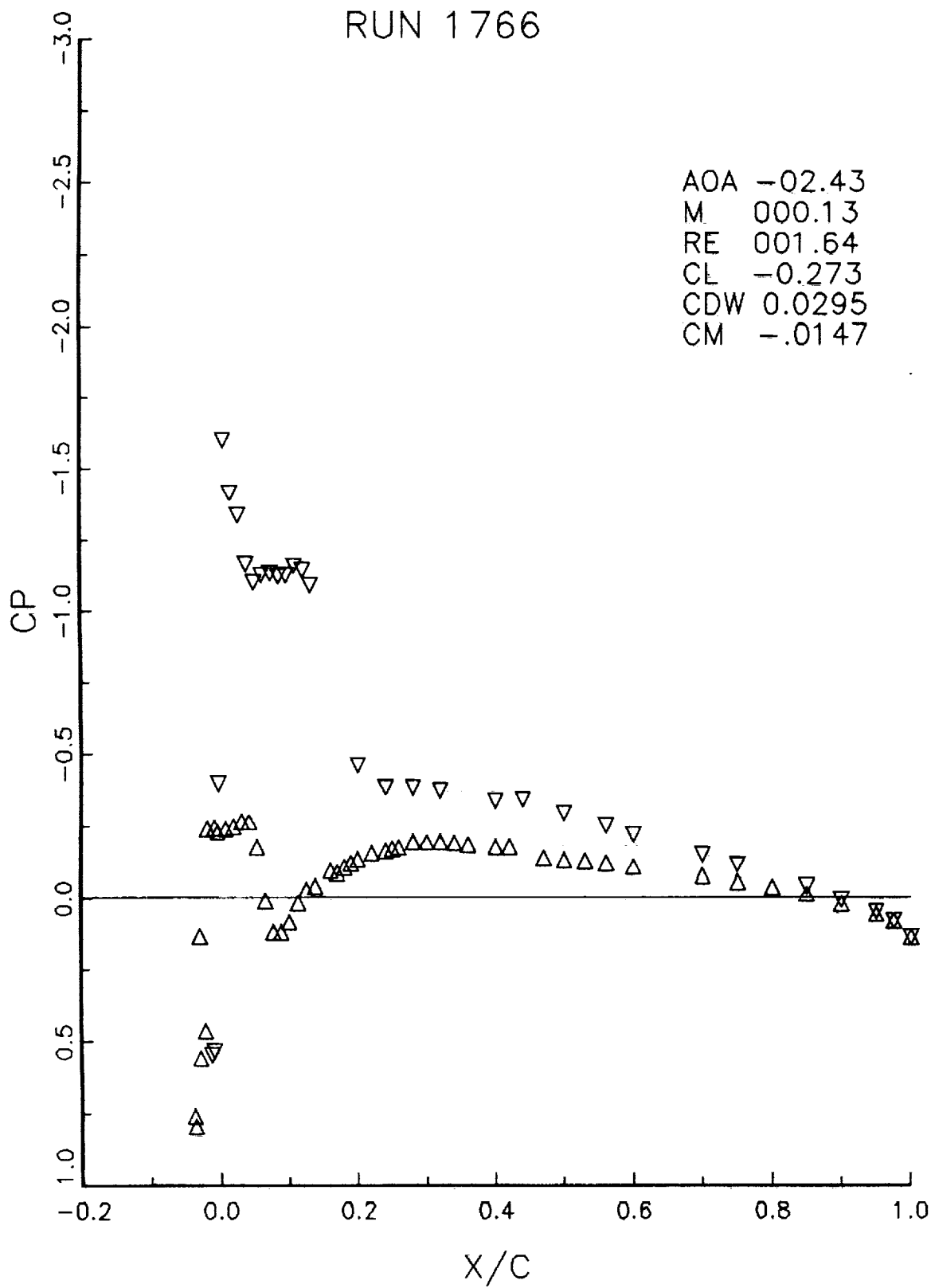
RUN 1764



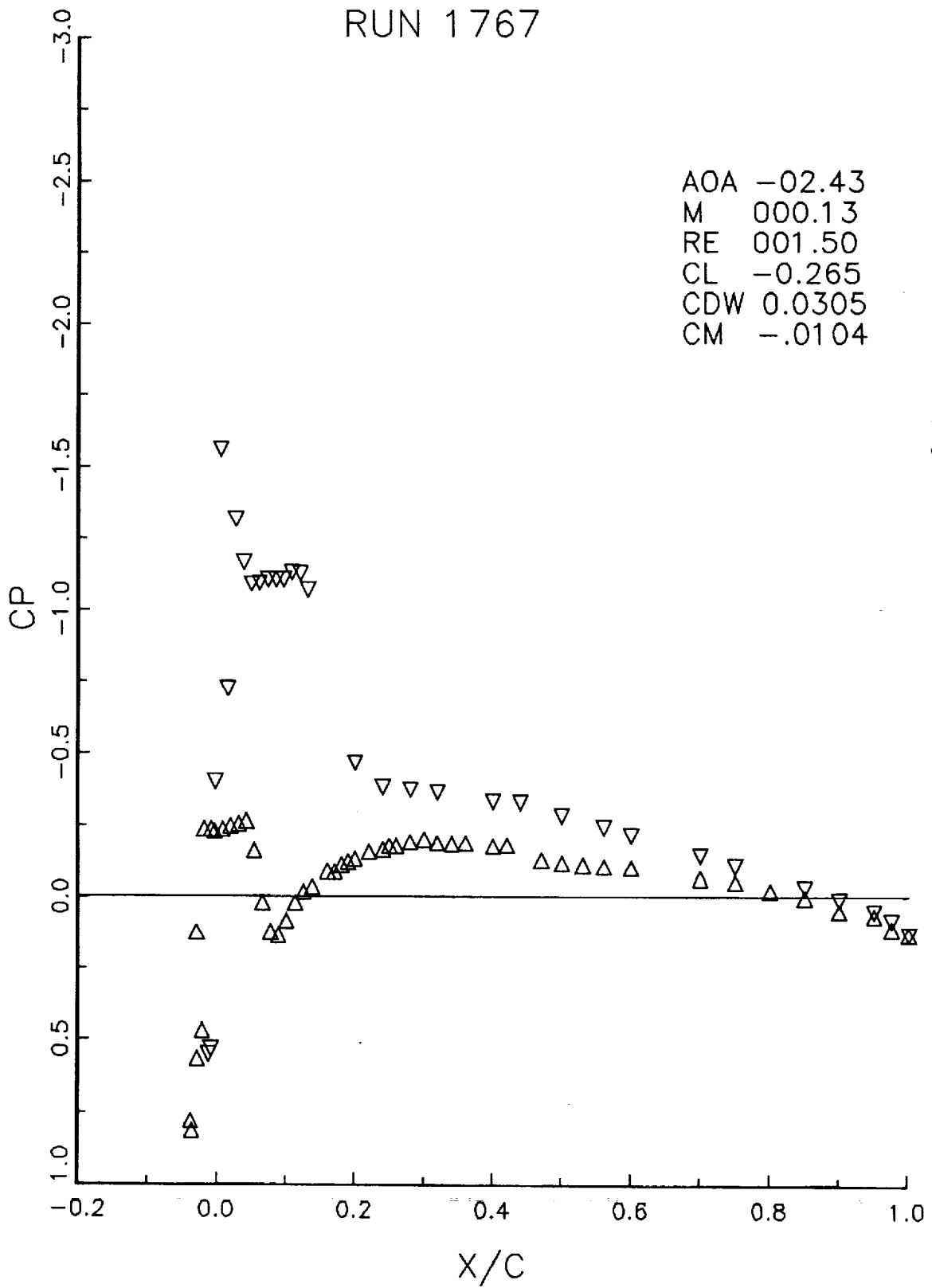
RUN 1765



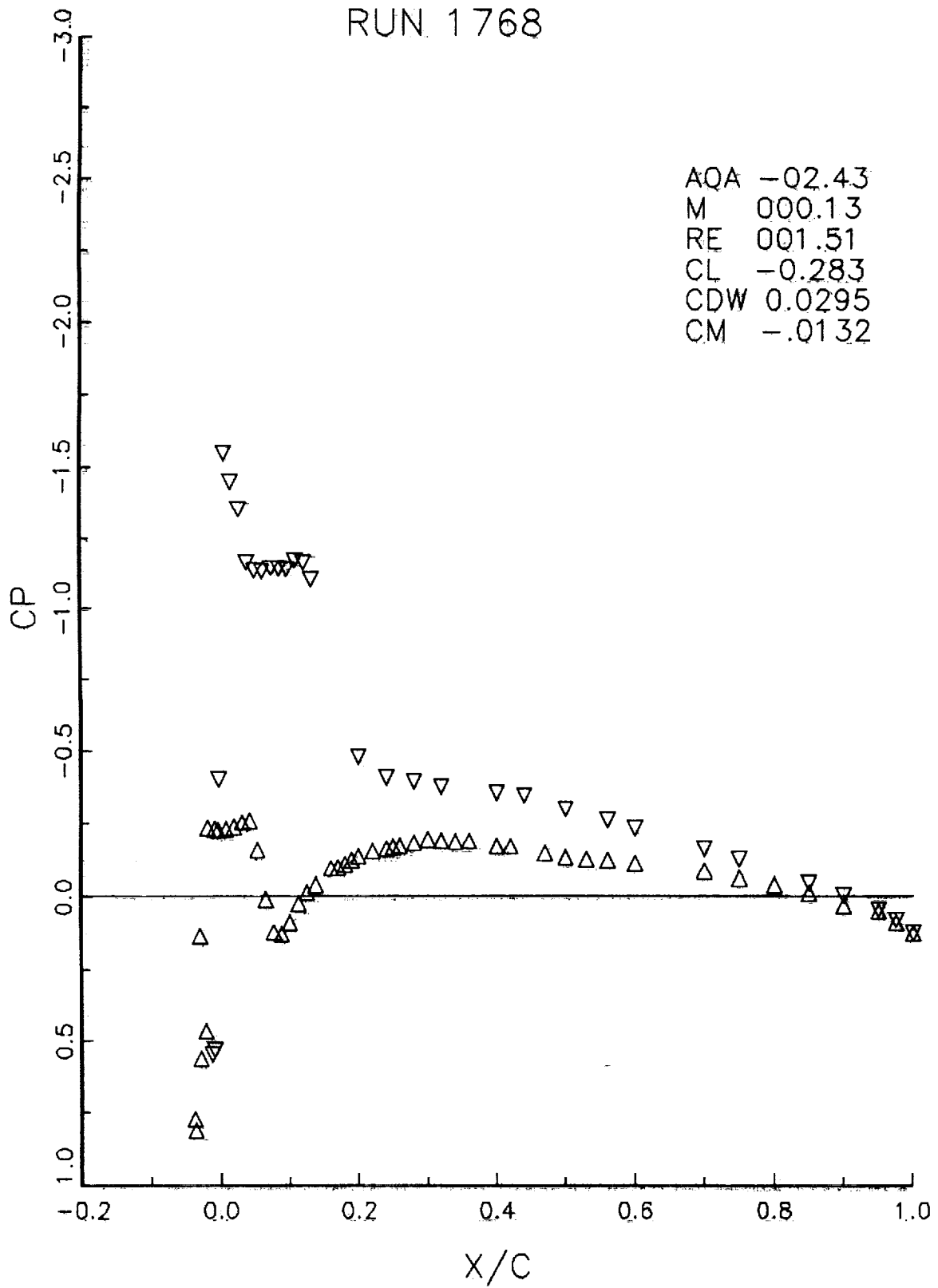
RUN 1766



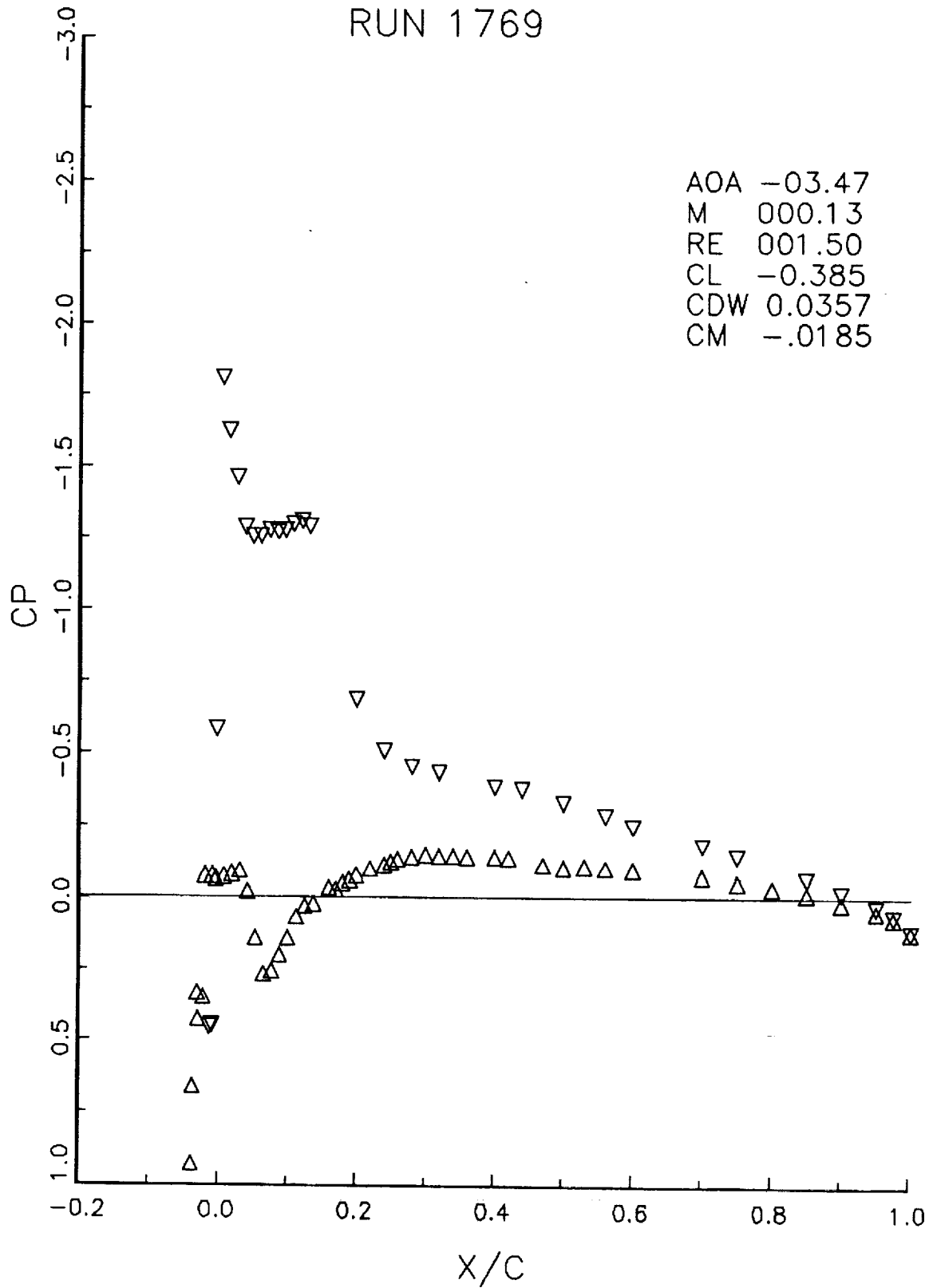
RUN 1767



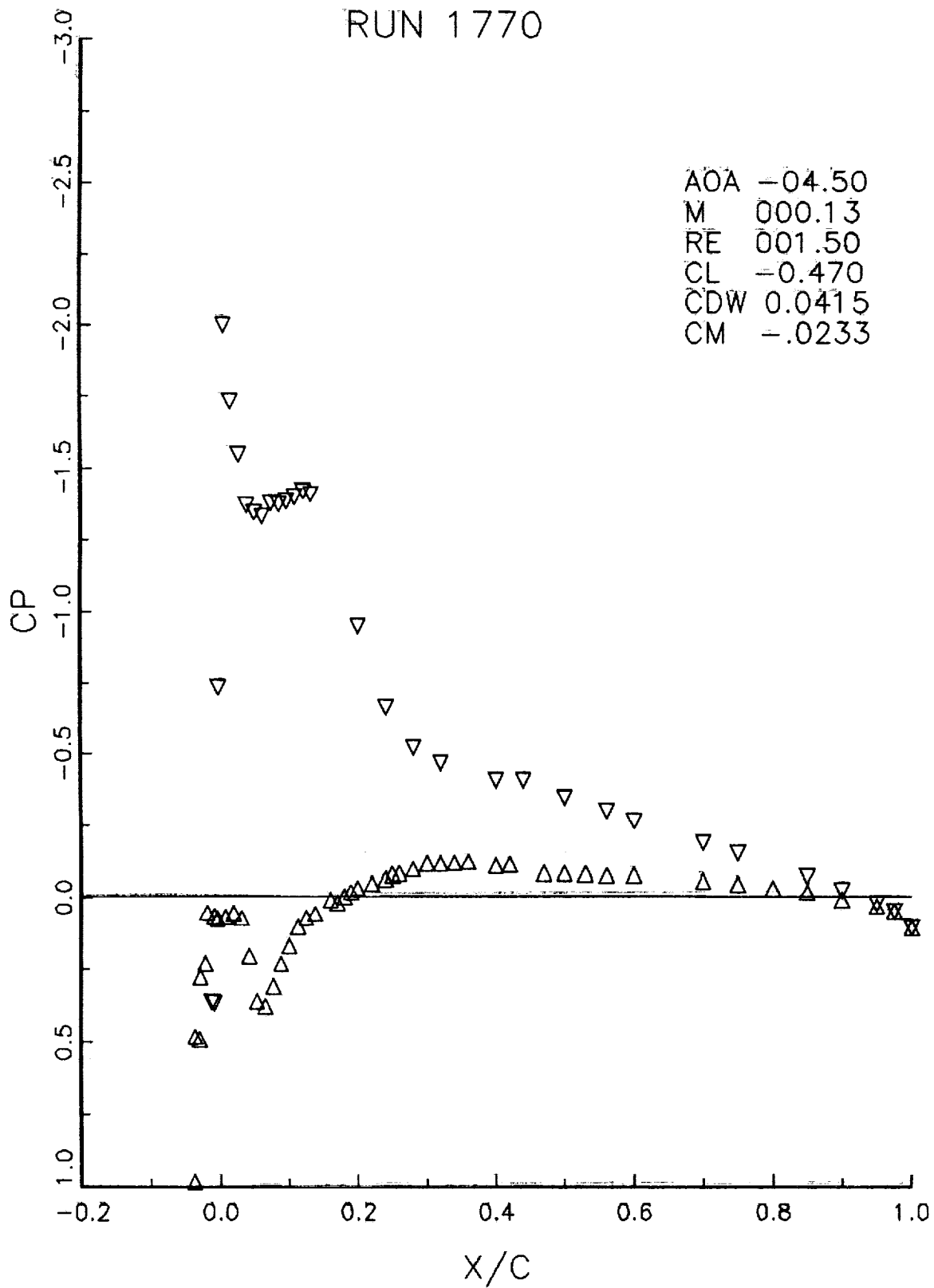
RUN. 1768

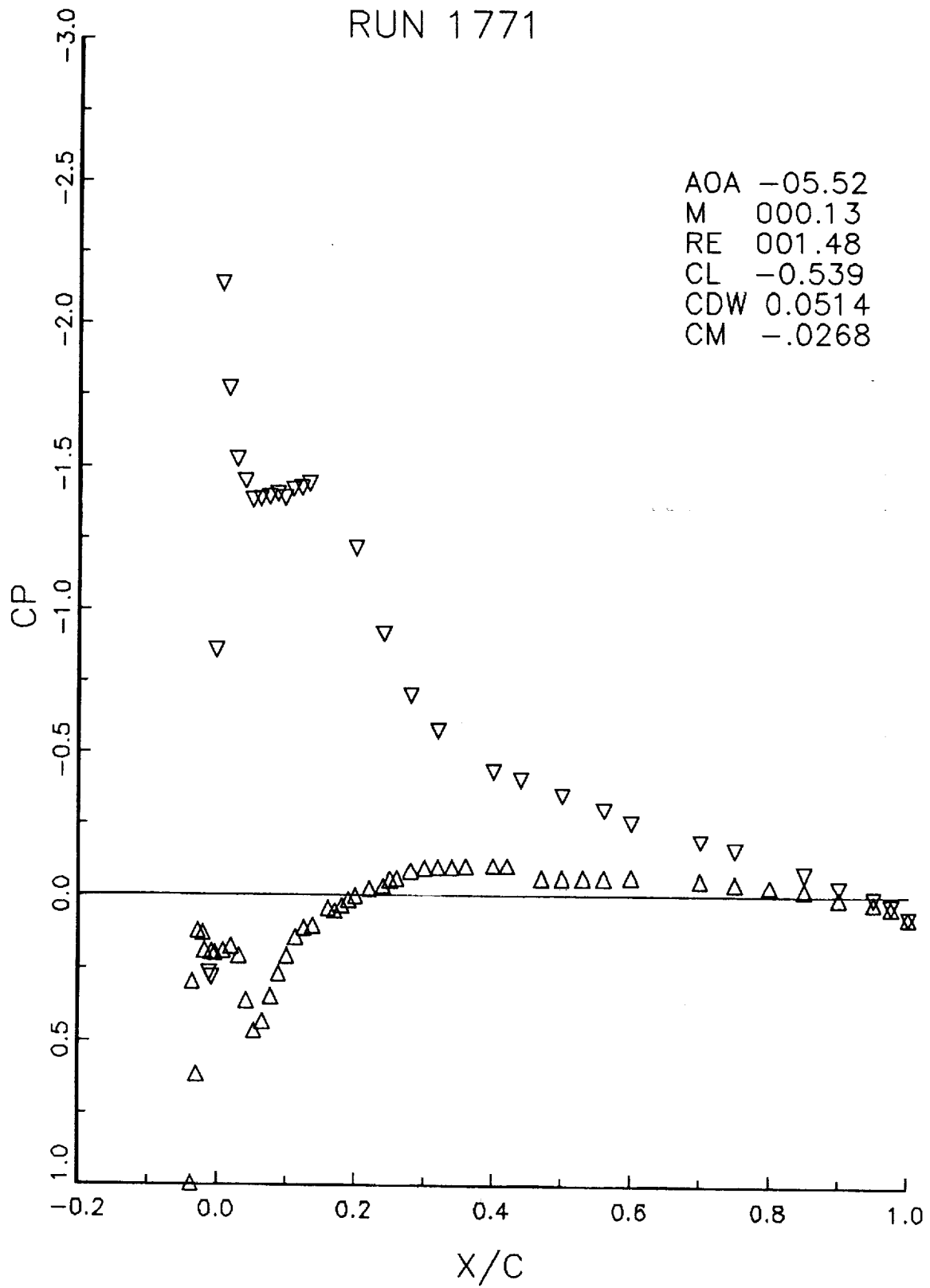


RUN 1769

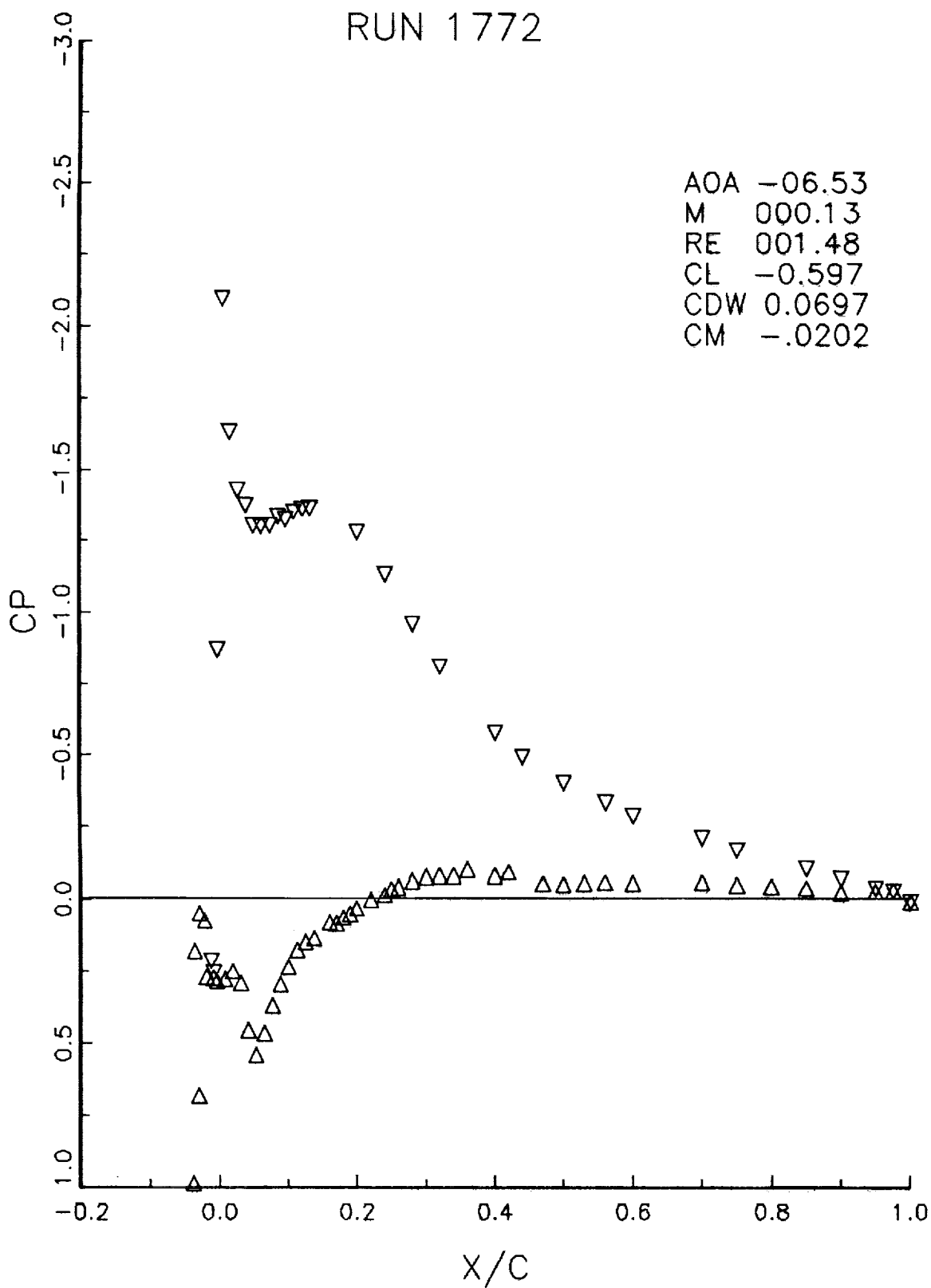


RUN 1770

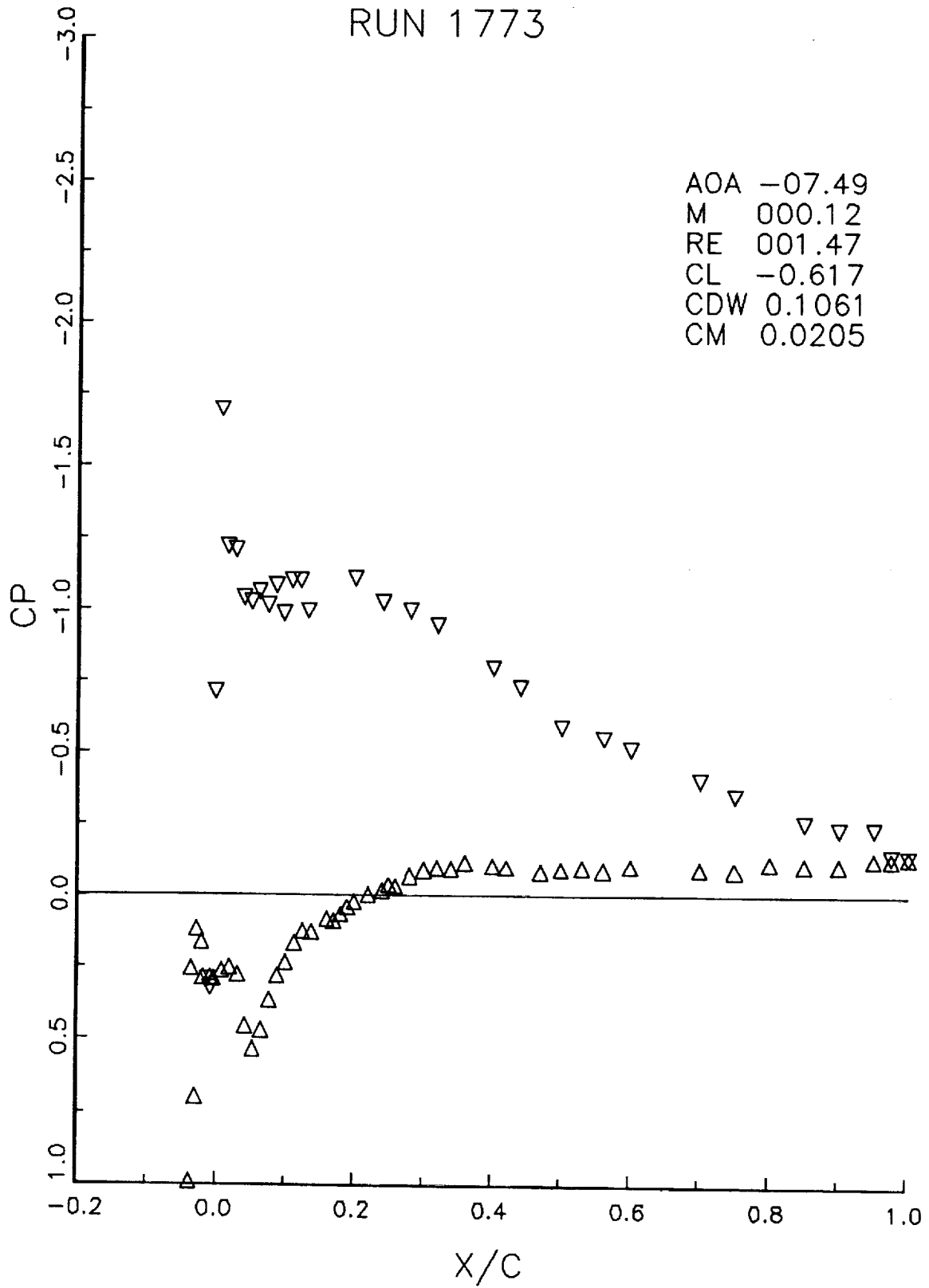




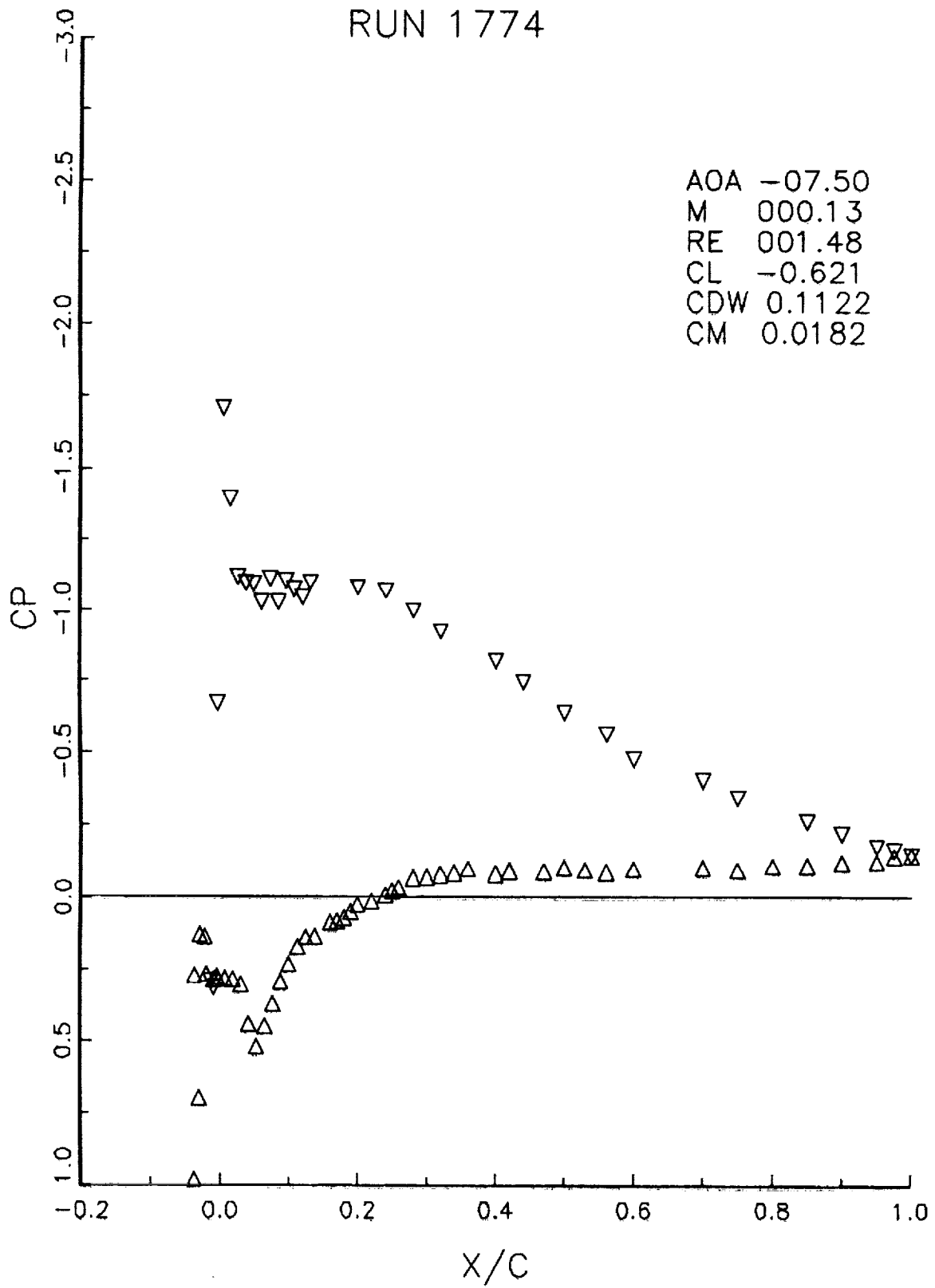
RUN 1772



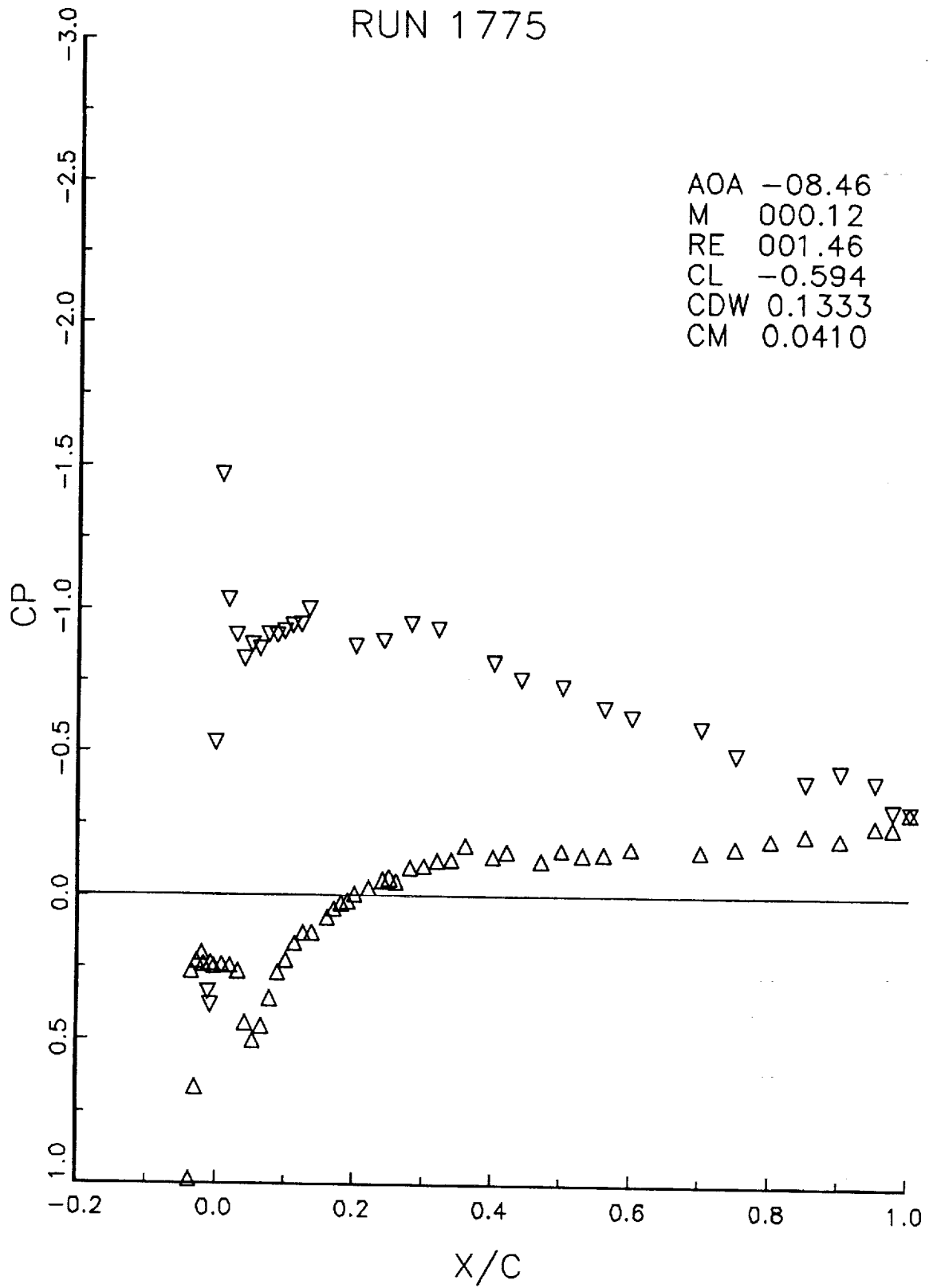
RUN 1773



RUN 1774

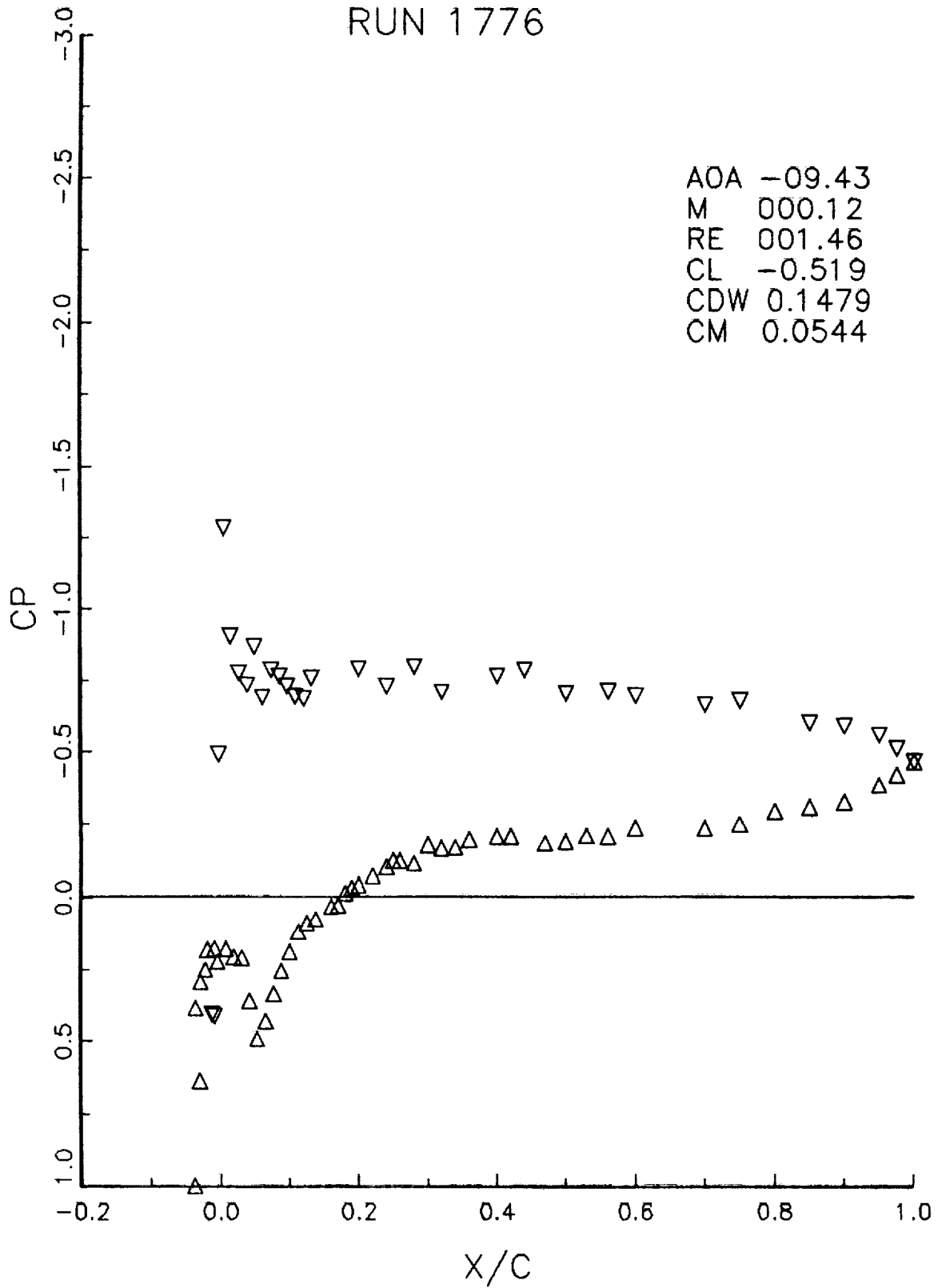


RUN 1775

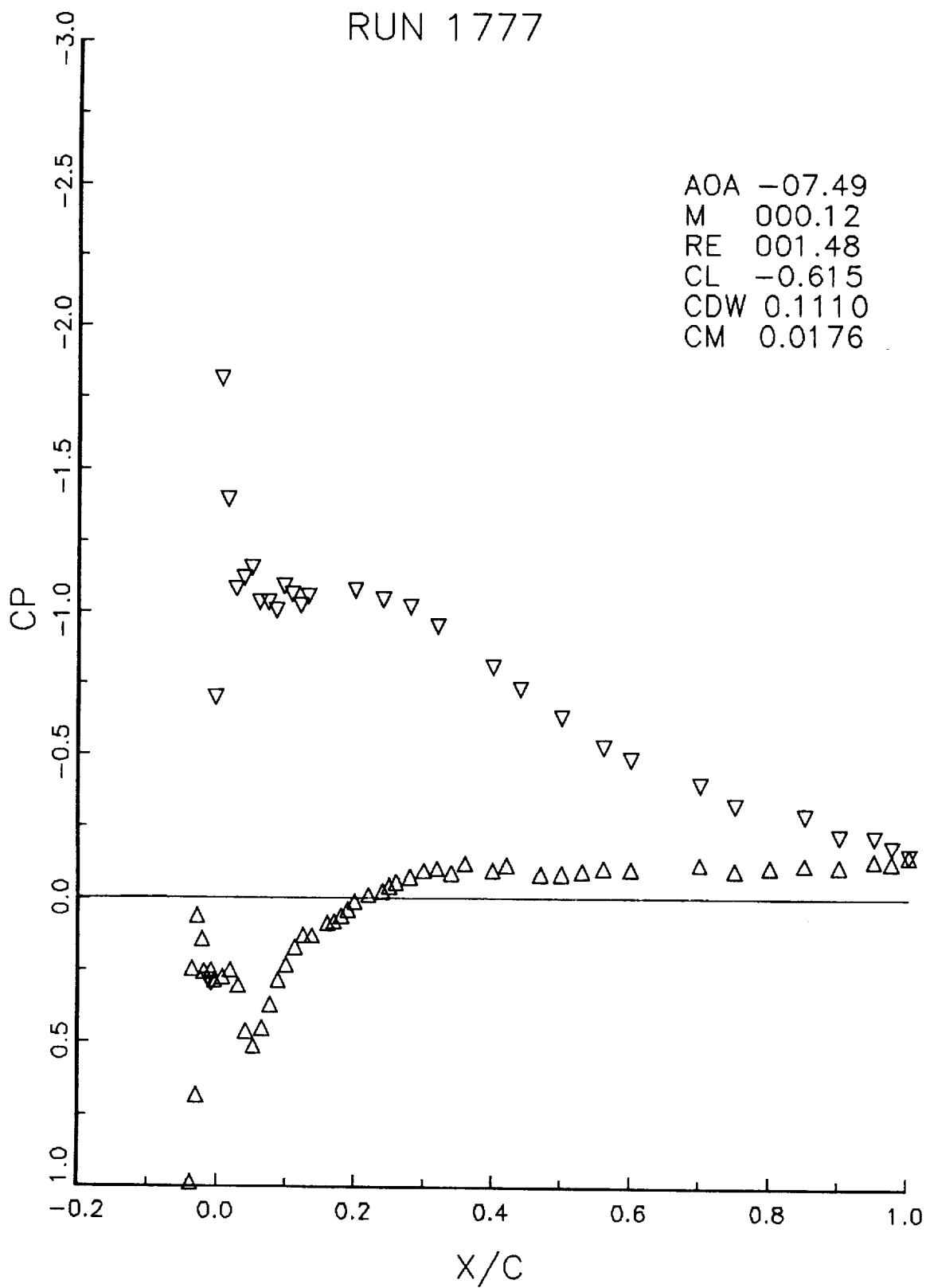


RUN 1776

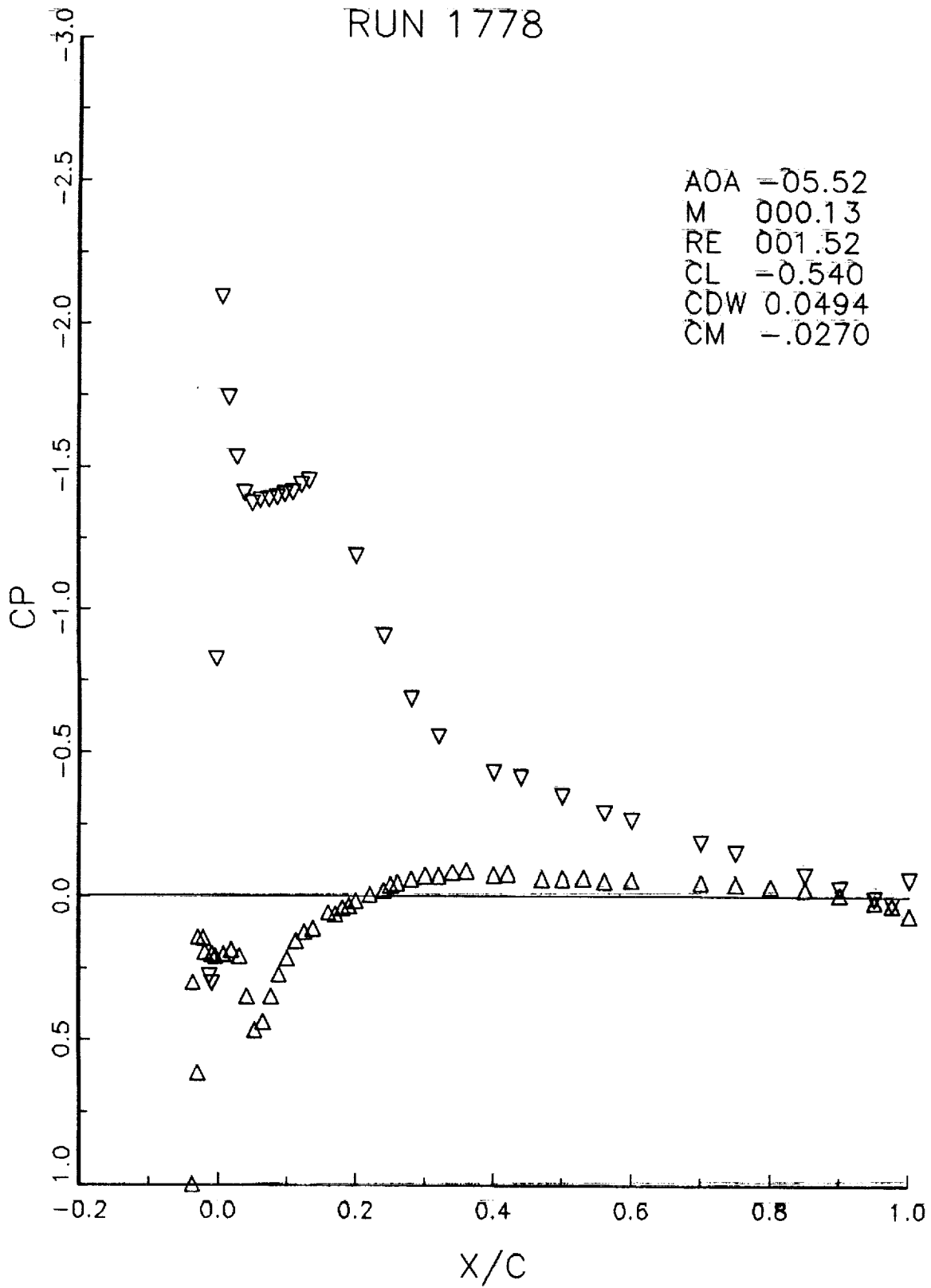
AOA -09.43
M 000.12
RE 001.46
CL -0.519
CDW 0.1479
CM 0.0544



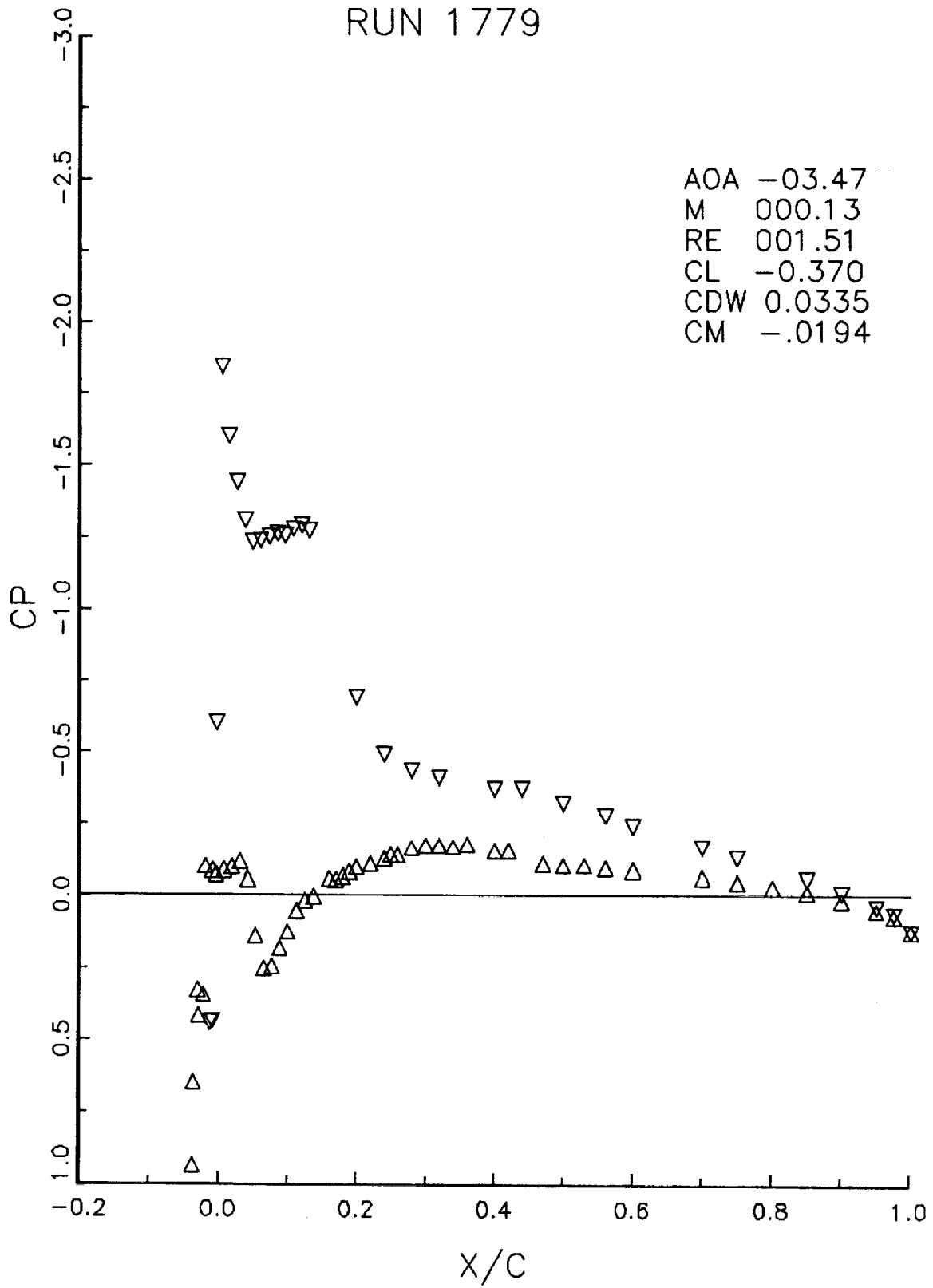
RUN 1777



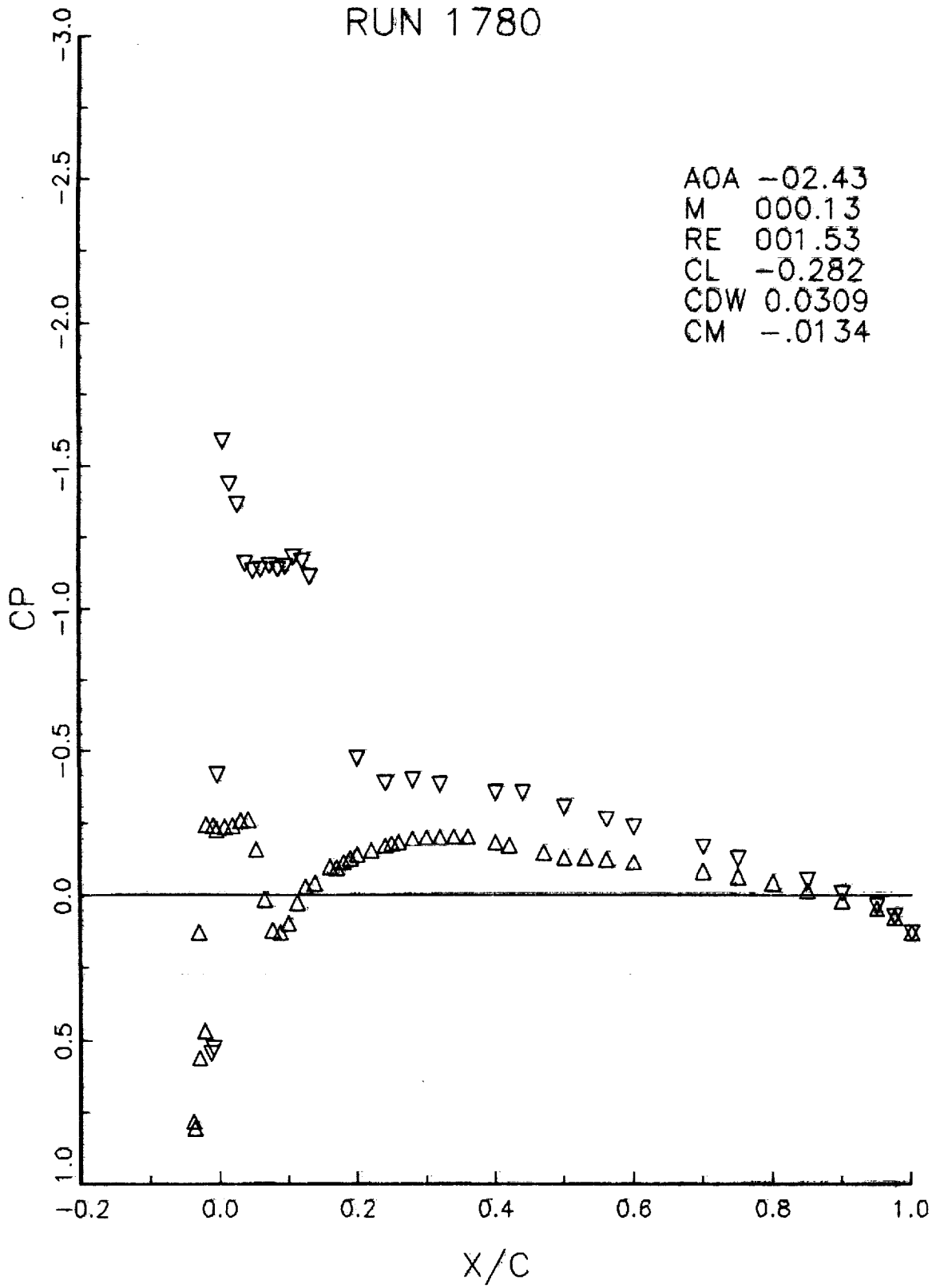
RUN 1778



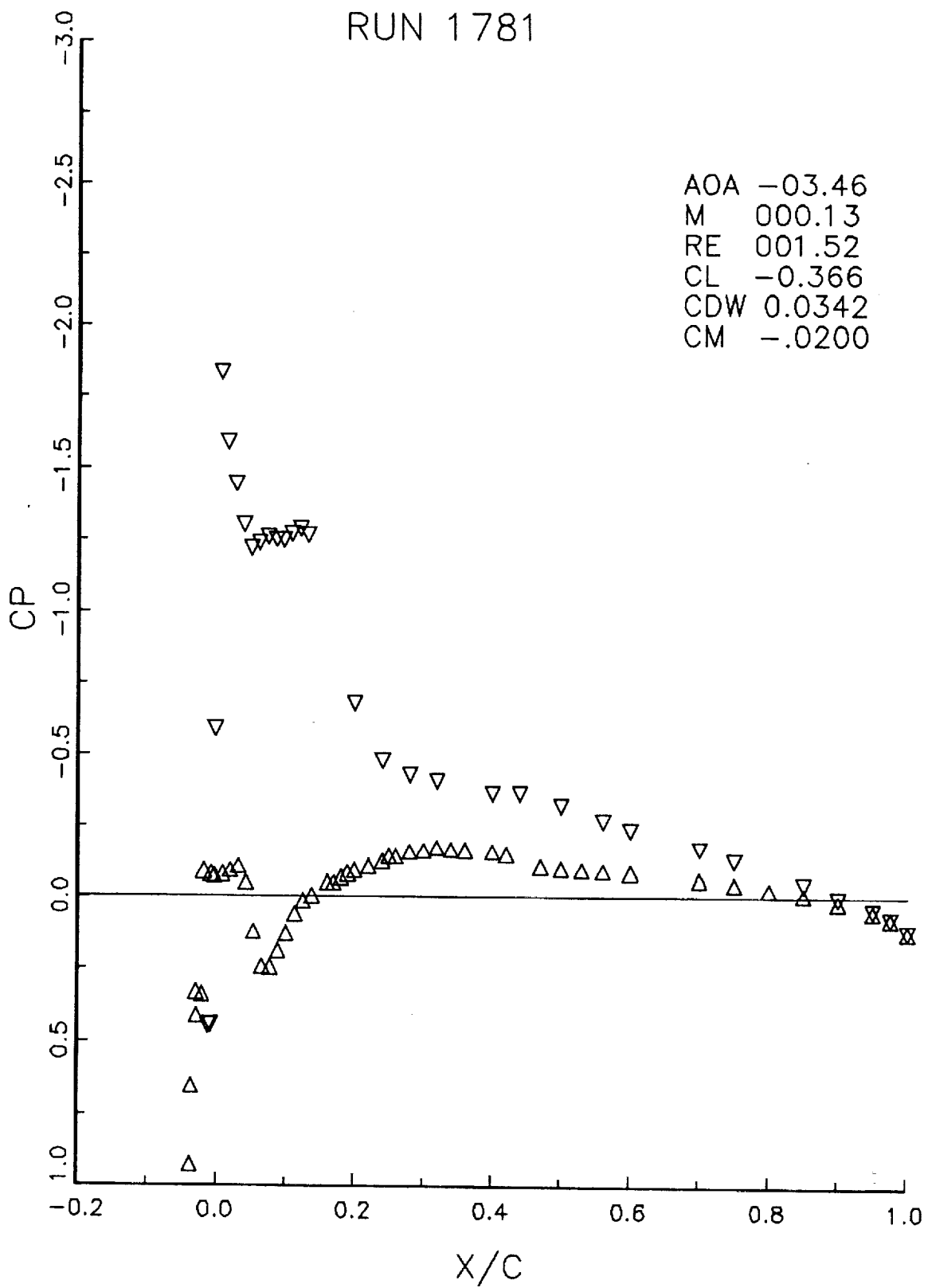
RUN 1779



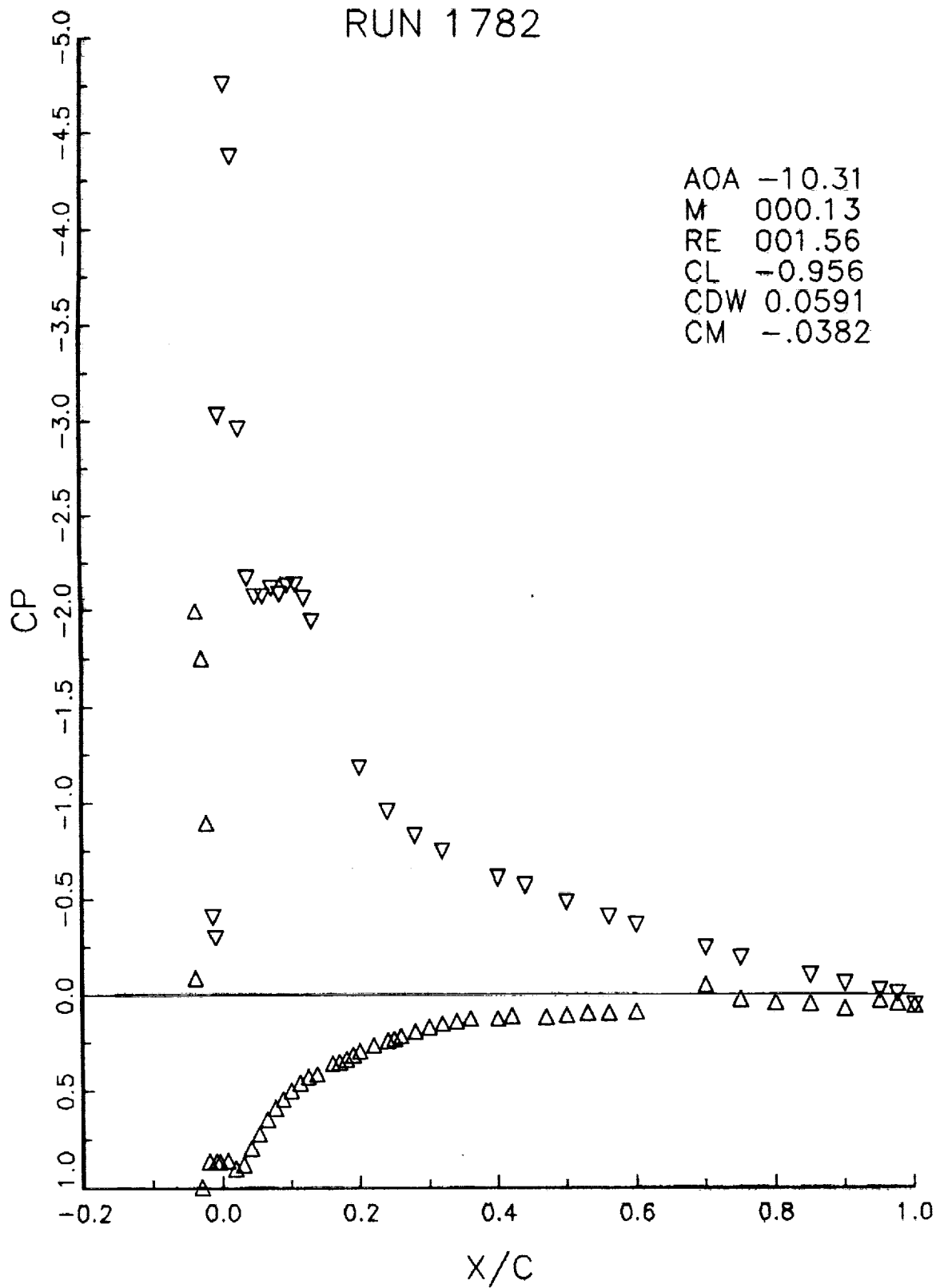
RUN 1780



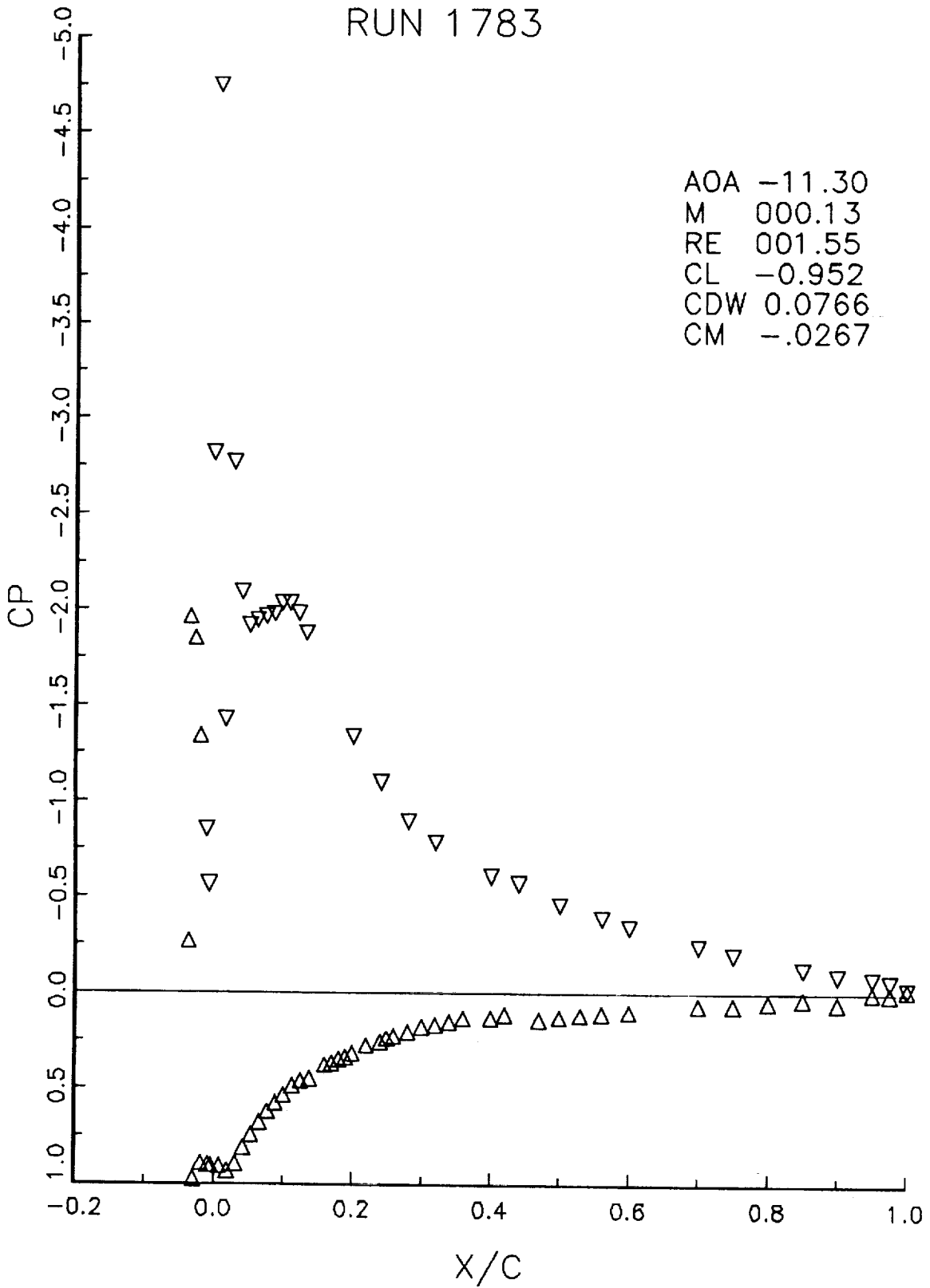
RUN 1781



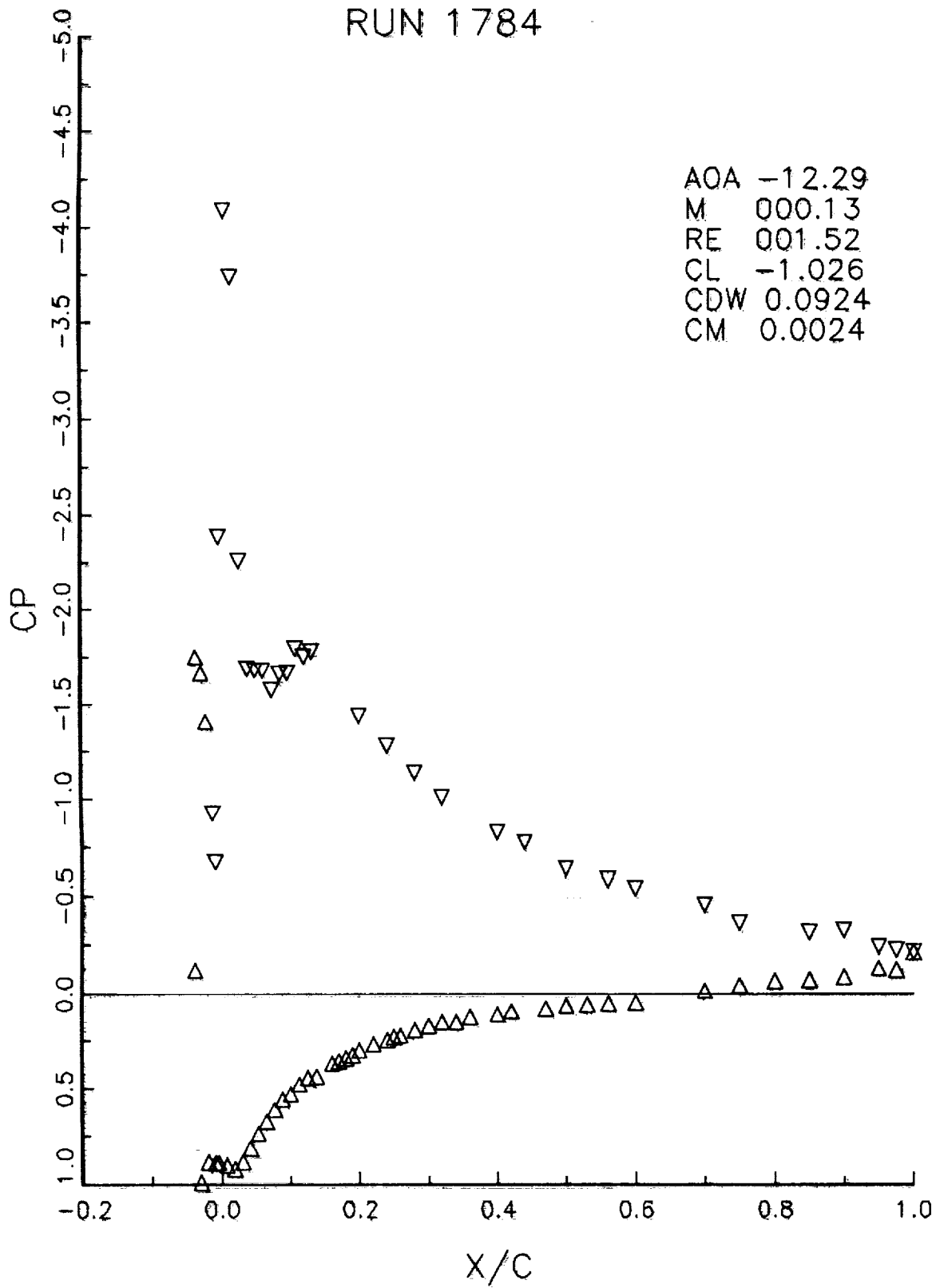
RUN 1782



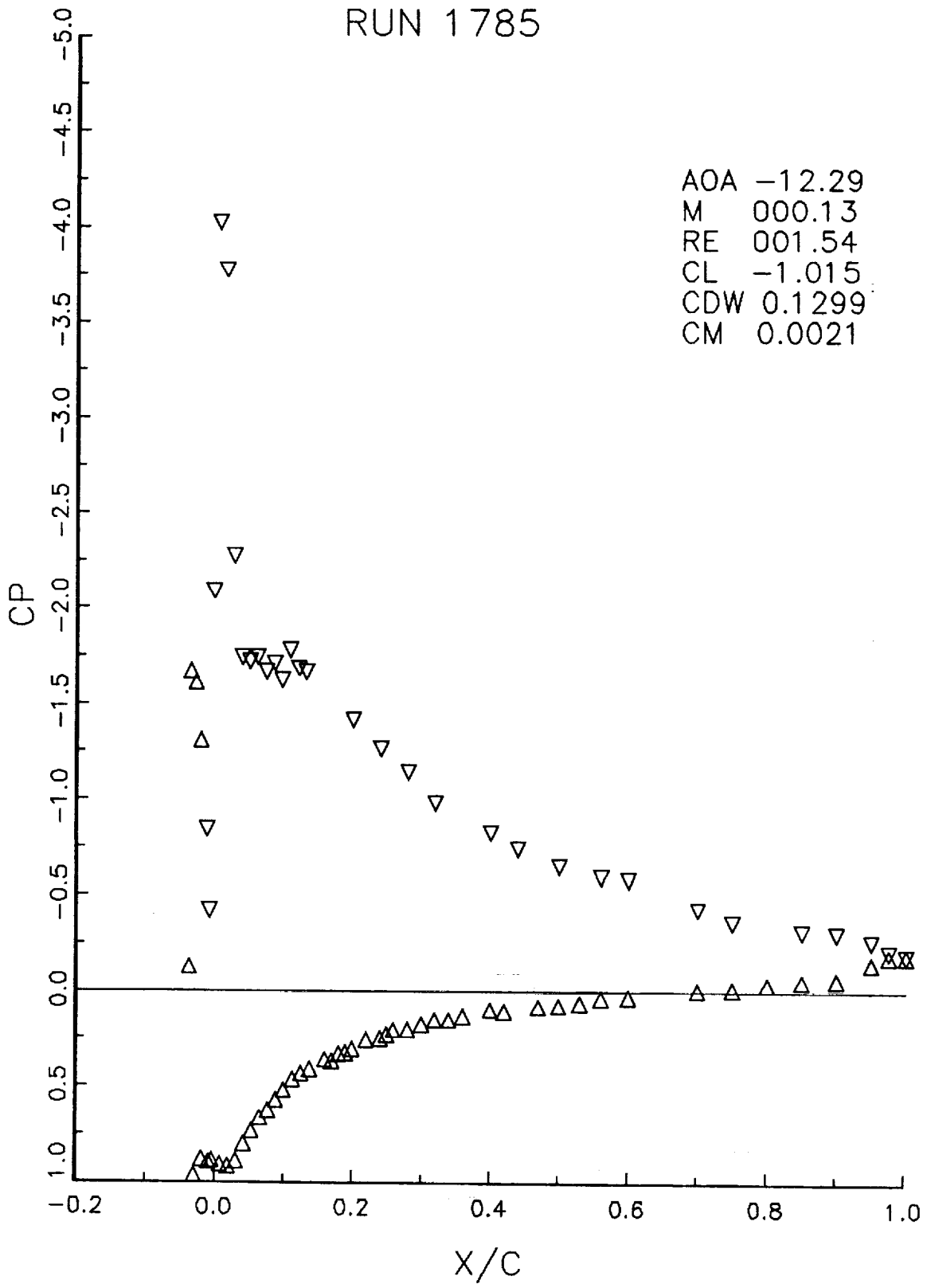
RUN 1783



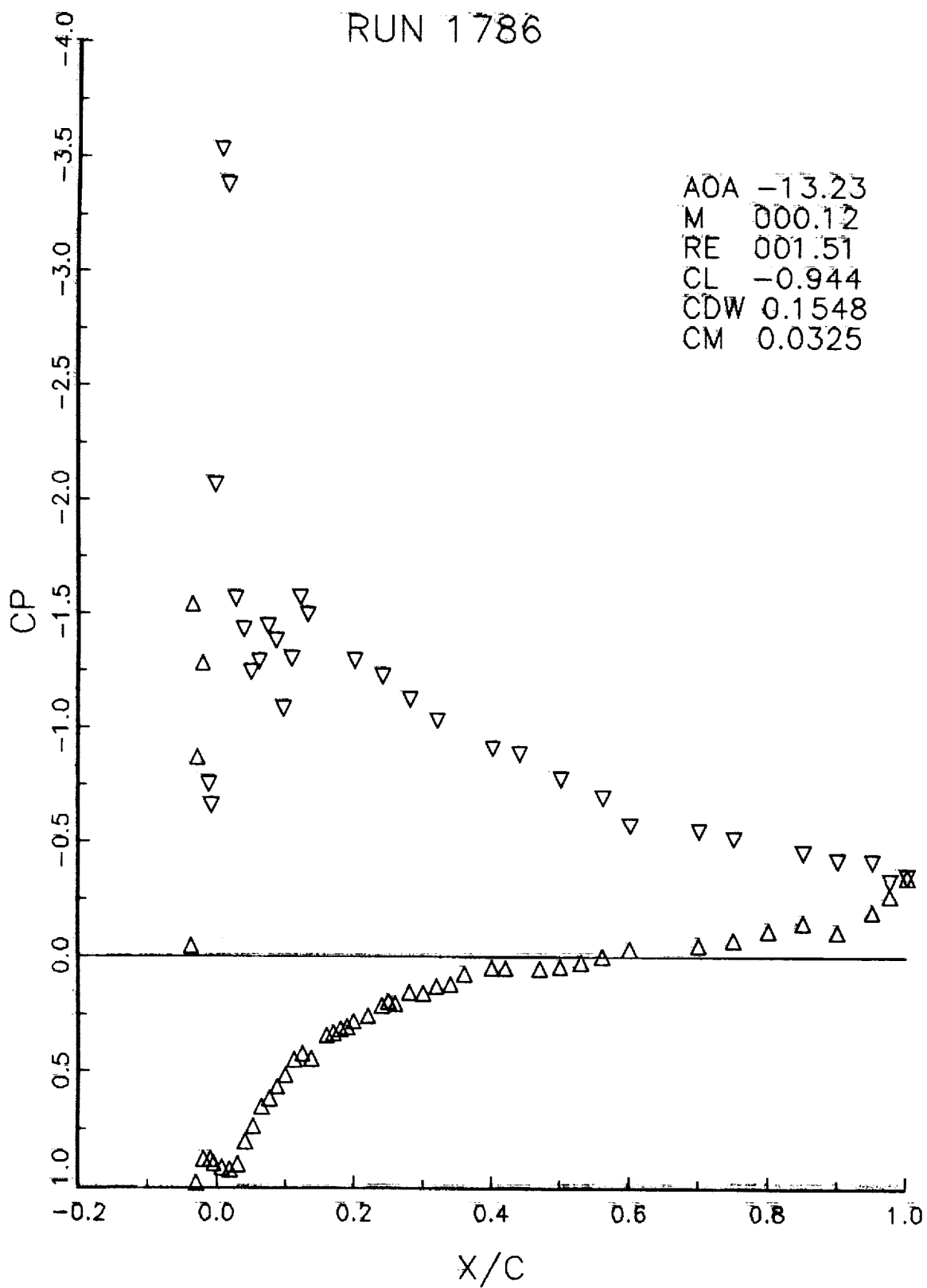
RUN 1784



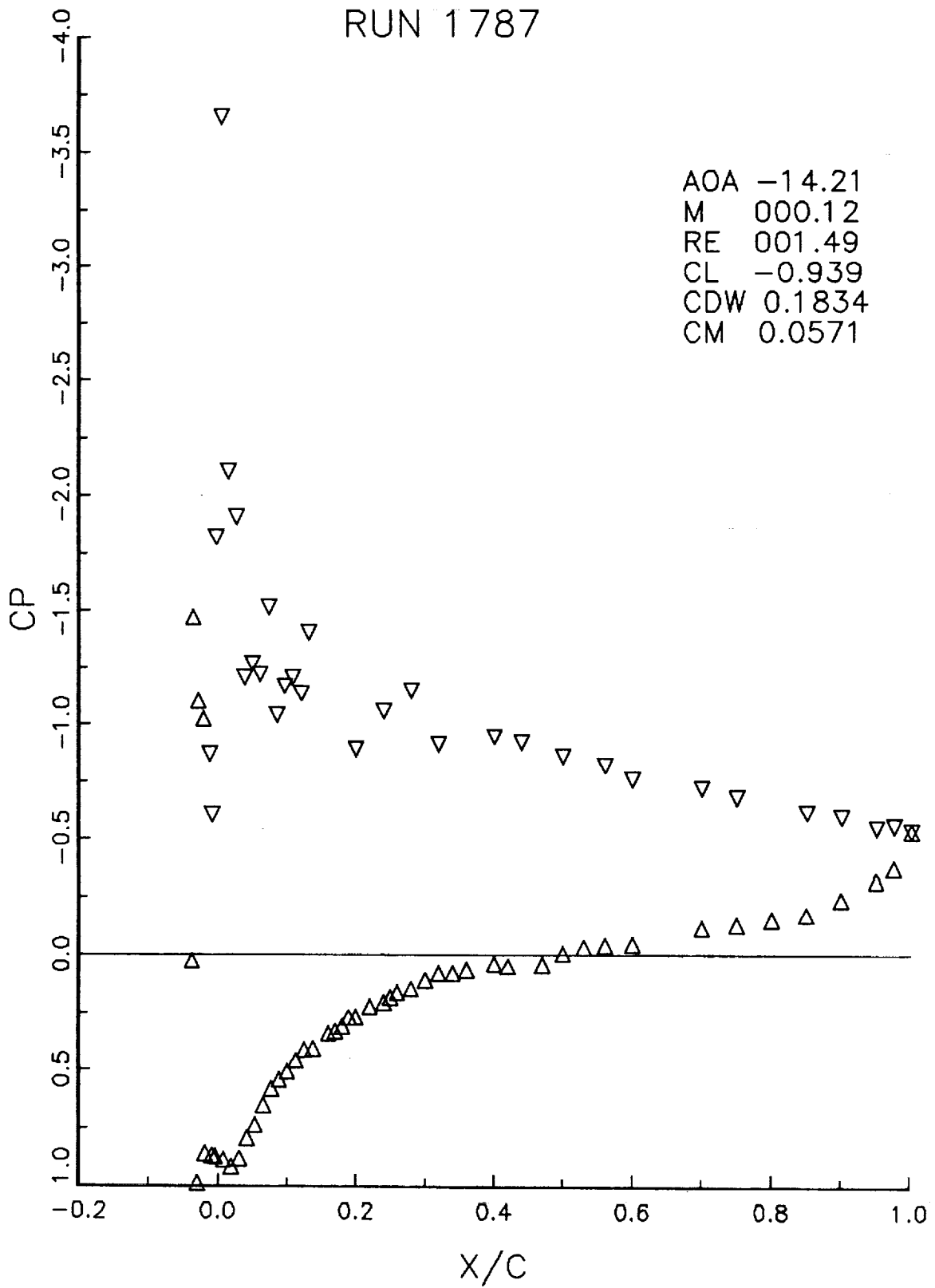
RUN 1785



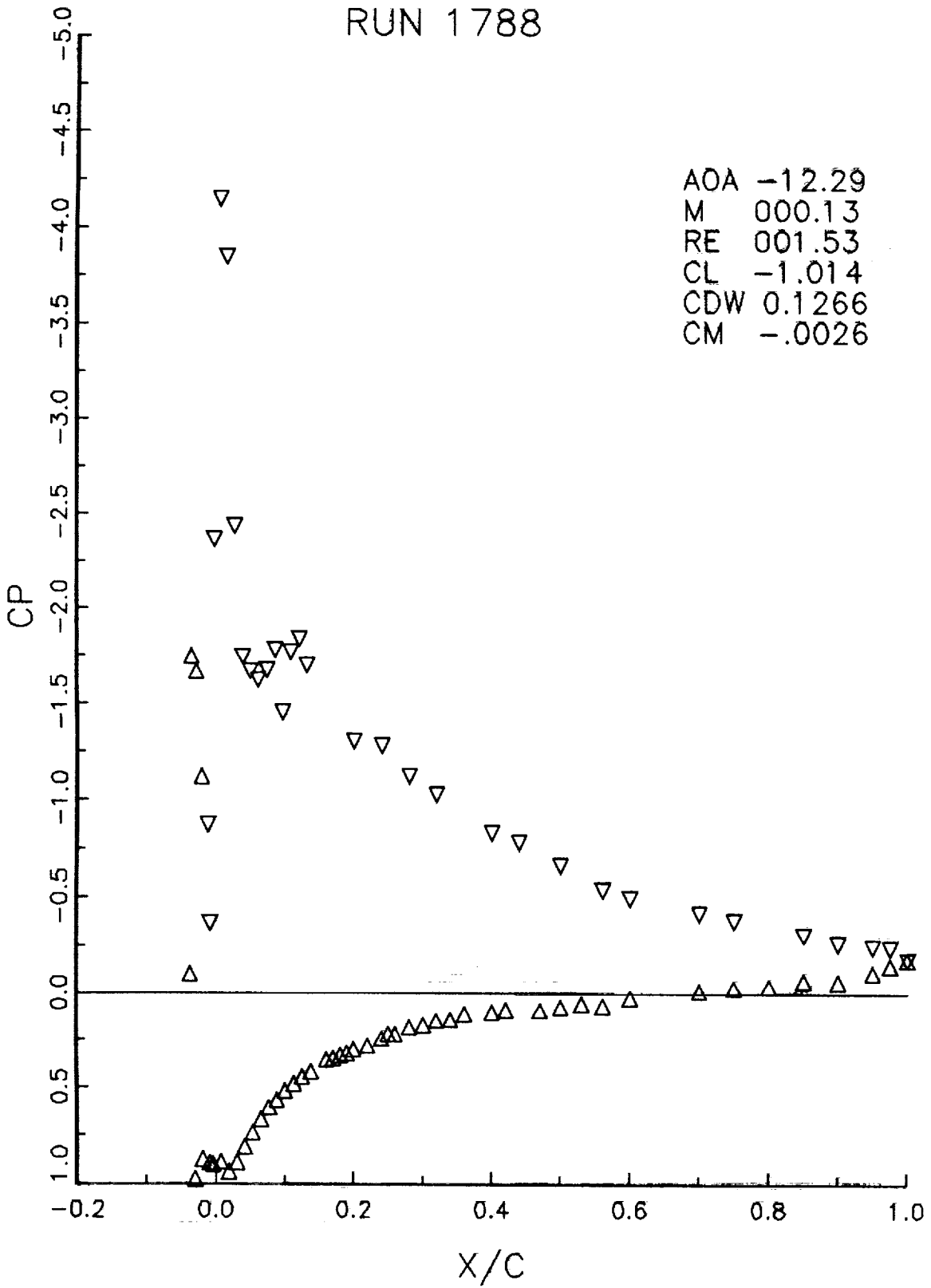
RUN 1786



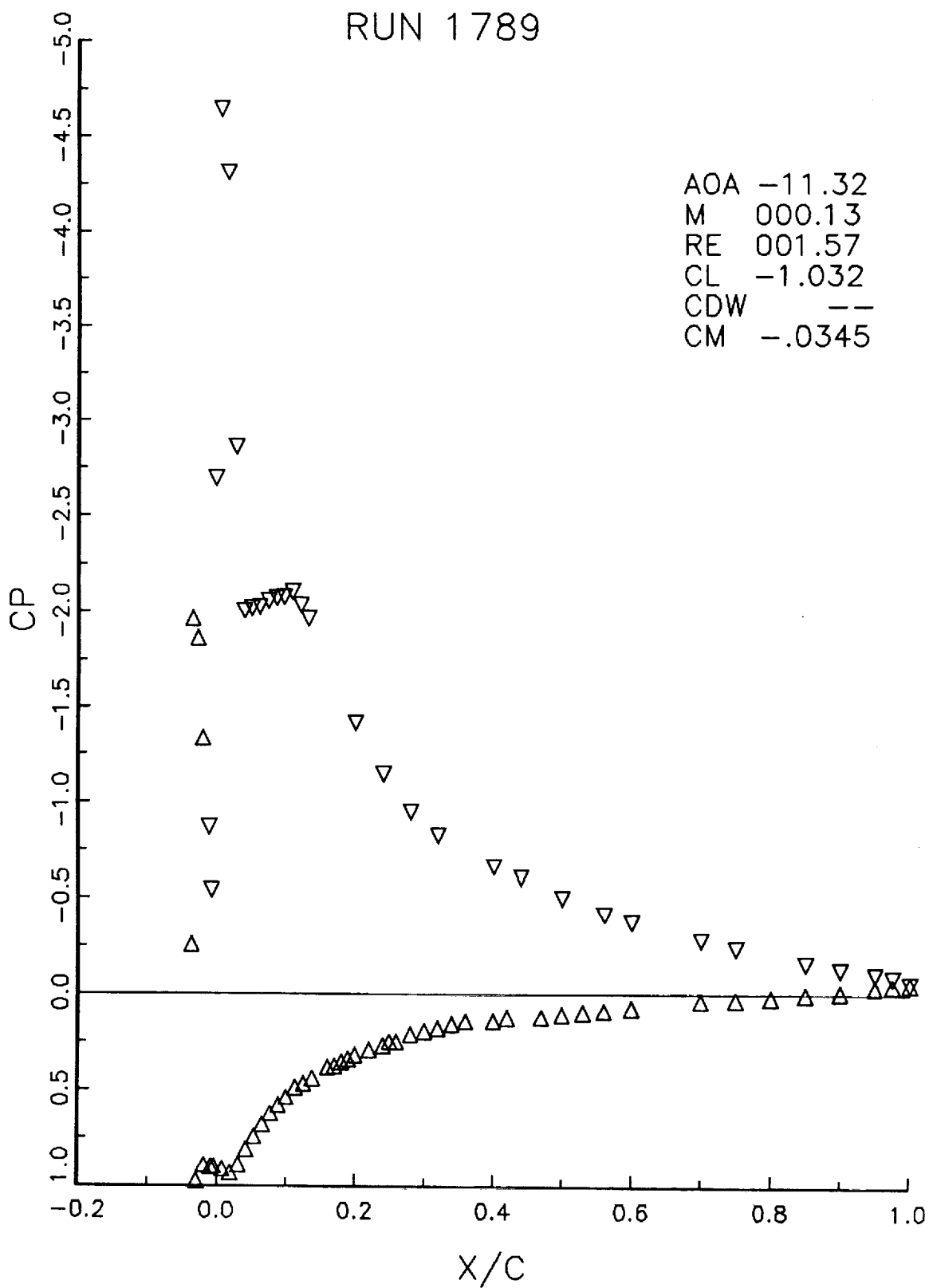
RUN 1787



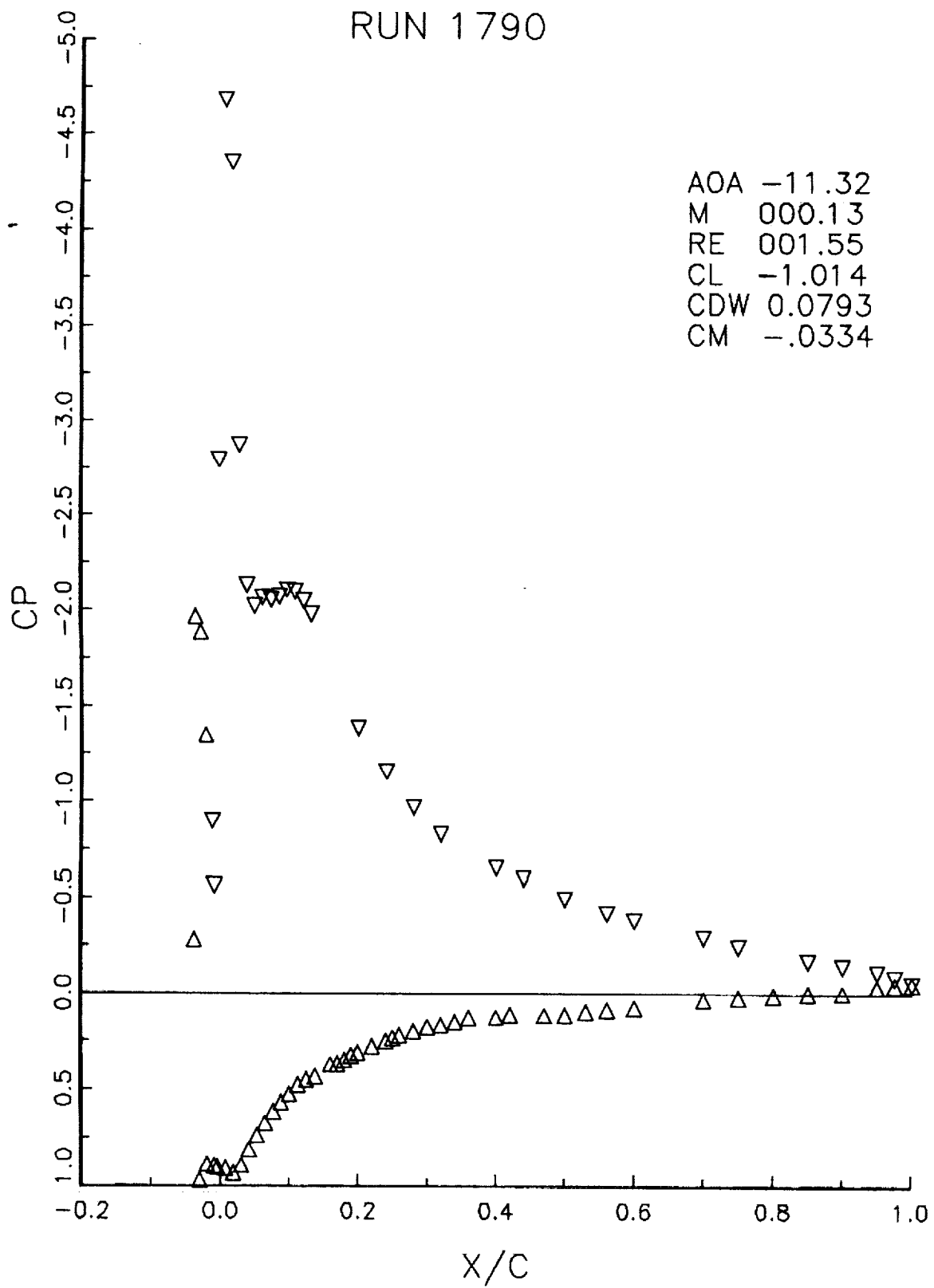
RUN 1788



RUN 1789



RUN 1790



**APPENDIX B:
NUMERICAL DATA**

IBM compatible disks, 3 1/2 (1.44 MB) or 5 1/4 (1.2 MB), are available upon request, with the numerical data contained in this report. The data are contained on two disks, in several files, in the format given on the following pages. The contents of the disks are:

<u>Disk No.</u>	<u>File Name</u>	<u>Contents</u>
1	DATA1.DAT	Runs 1118-1126
1	DATA2.DAT	Runs 1149-1164,1166-1171
1	DATA3.DAT	Runs 1172-1182,1184-1193
1	DATA4.DAT	Runs 1218-1238,1240-1250
1	DATA5.DAT	Runs 1251-1261,1263-1272, 1276-1287
1	DATA6.DAT	Runs 1288-1313
1	DATA7.DAT	Runs 1344,1346-1287
1	DATA8.DAT	Runs 1850,1852,1856,1858- 1860,1862-1870,1872- 1874,1876,1879-1881,1885- 1888
2	DATA9.DAT	Runs 1892-1995,1897,1899- 1913
2	DATA10.DAT	Runs 1915-1917,1925- 1942,1944,1946-1955
2	DATA11.DAT	Runs 1714-1734
2	DATA12.DAT	Runs 1735-1754
2	DATA13.DAT	Runs 1755-1774
2	DATA14.DAT	Runs 1775-1790
2	DATAFILE.HLP	List of formats for data files
2	TAB.ALL	Run Summary Tables
2	0012 COOR.DAT	NACA 0012 Airfoil Coordinates

THE REDUCED TUNNEL DATA FOR THE NACA 0012 RUNS LISTED IN THE ABOVE TABLES IS PRESENTED BELOW IN THE FOLLOWING FORMAT:

LINE 1	IRUN (I4)	RUN NUMBER
LINE 2	ICP,IW,IP,IS (4I1)	FOR WHICH A VALUE OF 0 DENOTES THE ABSENCE OF AND 1 DENOTES THE PRESENCE OF CP DATA, WAKE PROBE DATA, TOTAL PROBE BOUNDARY LAYER DATA, AND SPLIT FILM RESPECTIVELY.

FOR EACH VALUE OF 1 (FOR ICP,IW,IP,IS) THE RESPECTIVE DATA IMMEDIATELY FOLLOWS LINE 2. (IN THE CASE OF ICP=IW=1, THE WAKE DATA IMMEDIATELY FOLLOWS THE CP DATA; HOWEVER, CASES OF ICP=1,IW=0 ALSO EXIST. NO OTHER CASES OF SIMULTANEOUS DATA FOR A GIVEN RUN ARE PRESENT.)

[FOR ICP=1:]

LINE 3	NCPP (I5)	NUMBER OF CP DATA POINTS
LINE 4		HEADER LINE
LINES 5,6..NT	I, XOC, YOC, CP (1X, I5, 3F10.4)	NCPP LINES OF DATA WHERE: I - DATA POINT NUMBER XOC - TAP X/C-LOCATION YOC - TAP Y/C-LOCATION CP - PRESSURE COEFFICIENT

[FOR IW=1:]

LINE NT+1	NWP (I5)	NUMBER OF WAKE DATA POINTS
LINE NT+2		HEADER LINE
LINES NT+3, NT+4..	I, POS, QTUN, QWAK (I5, 3F10.3)	NWP LINES OF DATA WHERE: I - DATA POINT NUMBER POS - PROBE TRAVERSE POSITION (INCHES) QTUN - TUNNEL Q (PSI) QWAK - WAKE Q (PSI)

[FOR IP=1:]

LINE 3 NPP, AOA, XOC NPP - NUMBER OF TOTAL PROBE
 (I5, 2F10.7) DATA POINTS
 AOA - ANGLE OF ATTACK (DEG)
 XOC - TOTAL PROBE X/C-
 LOCATION

LINE 4 HEADER LINE

LINES 5,6.. I, YLOC, UBAR NPP LINES OF DATA WHERE:
 (I5, 2E15.6) I - DATA POINT NUMBER
 YLOC - PROBE Y-LOCATION
 (INCHES)
 UBAR - AVERAGE U VELOCITY
 (FT/SEC)

[FOR IS=1:]

LINE 3 NSP, AOA, XOC NSP - NUMBER OF SPLIT FILM
 DATA POINTS
 (I5, 2F10.7) AOA - ANGLE OF ATTACK (DEG)
 XOC - SPLIT FILM X/C-LOCATION

LINE 4 HEADER LINE

LINES 5,6.. I, YLOC, UBAR, NSP LINES OF DATA WHERE:
 SIGMA, URMS, UPBAR I - DATA POINT NUMBER
 (I5, 5E15.6) YLOC - SPLIT FILM Y-LOCATION
 (INCHES)
 UBAR - AVERAGE U VELOCITY
 (FT/SEC)
 SIGMA - TURBULENCE NO. (%)

 URMS - ROOT MEAN SQUARE
 U VELOCITY (FT/SEC)
 UPBAR - AVERAGE U PERTURBATION
 VELOCITY (FT/SEC)

APPENDIX C:
TECHNICAL PAPERS BASED ON THESE DATA

REPORT DOCUMENTATION PAGE

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