

cSc

# Structural Load Control During Construction

**Martin Mikulas**

*Very specific problem being  
addressed. Cost energy  
absorber on a long track.*

**Third Annual Symposium  
November 21 & 22, 1991**

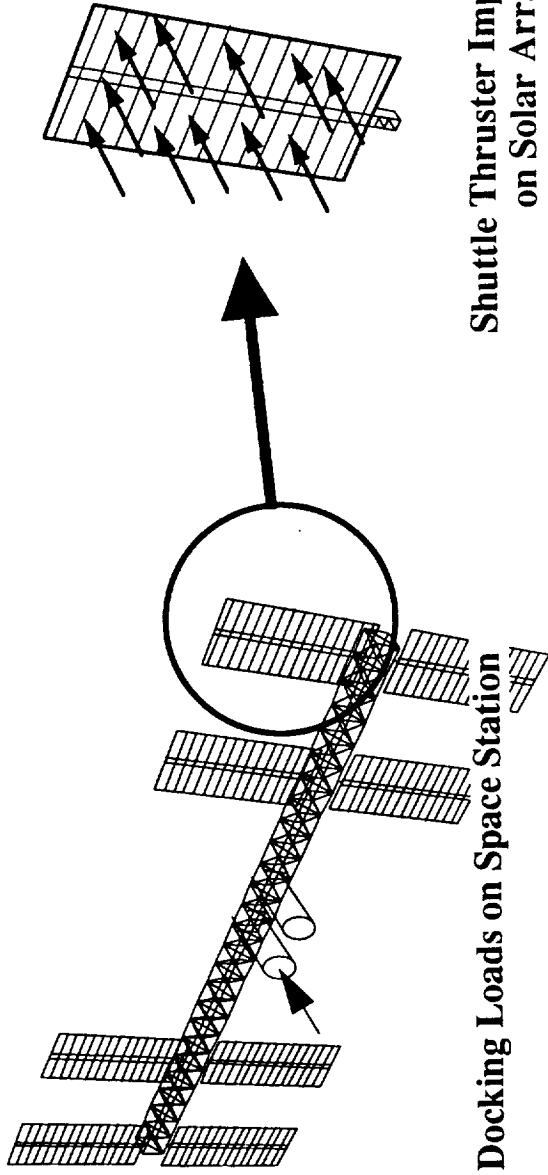
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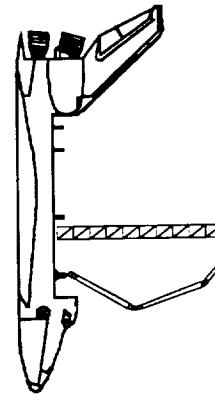
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# EXAMPLES OF HIGH TRANSIENT LOADINGS ON LARGE SPACE STRUCTURES

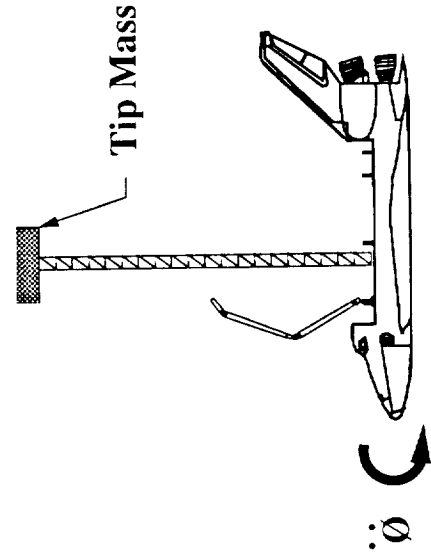


Docking Loads on Space Station

Shuttle Thruster Impingement  
on Solar Arrays



Side Loads  
From Tethers



Shuttle Accelerations Applied  
to Attached Beam

# **ENERGY ABSORBING/LOAD LIMITING STRUT RESEARCH OBJECTIVES**

**Explore feasibility of using energy-absorbing/load-limiting struts in large space structures subjected to transient loadings**

**Develop analytical and design capability for energy absorbing struts**

**Develop several energy absorbing strut concepts ( passive & active)**

**Experimentally demonstrate application of energy absorbing struts**

## **SCOPE OF RESEARCH ON ENERGY ABSORBING STRUTS TO DATE**

**Rigid body analysis developed to scope problem**

**Initial contacts made with LeRC to understand solar array  
problem**

*Kornel Nagy*

**Visit made to JSC to understand their effort on energy  
absorbers**

**Preliminary finite element analysis conducted on uniform  
beam solar array model**

**Studies conducted to size springs in energy absorbers**

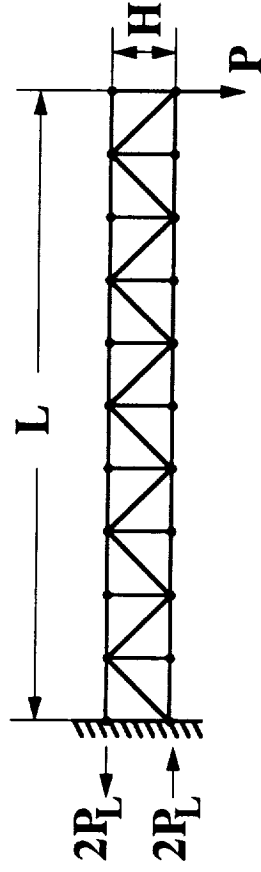
**Test bed for energy absorbers designed and under  
construction**

*Robert Davis*

**Cooperative agreement made with Honeywell to co-develop  
an energy absorber**

# ENERGY CHARACTERISTICS OF CANTILEVERED TRUSSES WITH A TIP LOAD.

Standard Truss



$$2R_L H = PL \Rightarrow P_L = \frac{PL}{2H}$$

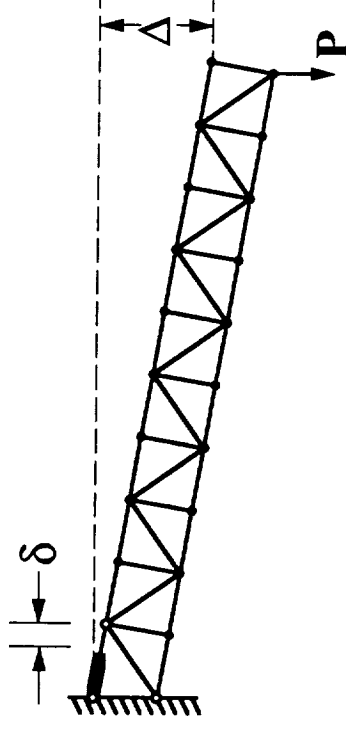
Truss strain energy is:

$$\Pi = \frac{1}{2} P_L \Delta$$

Where

$$\Delta = \frac{PL^3}{3EI}$$

Energy Absorbing Truss



$$\frac{\delta}{H} = \frac{\Delta}{L} \Rightarrow \Delta = \frac{L}{H} \delta$$

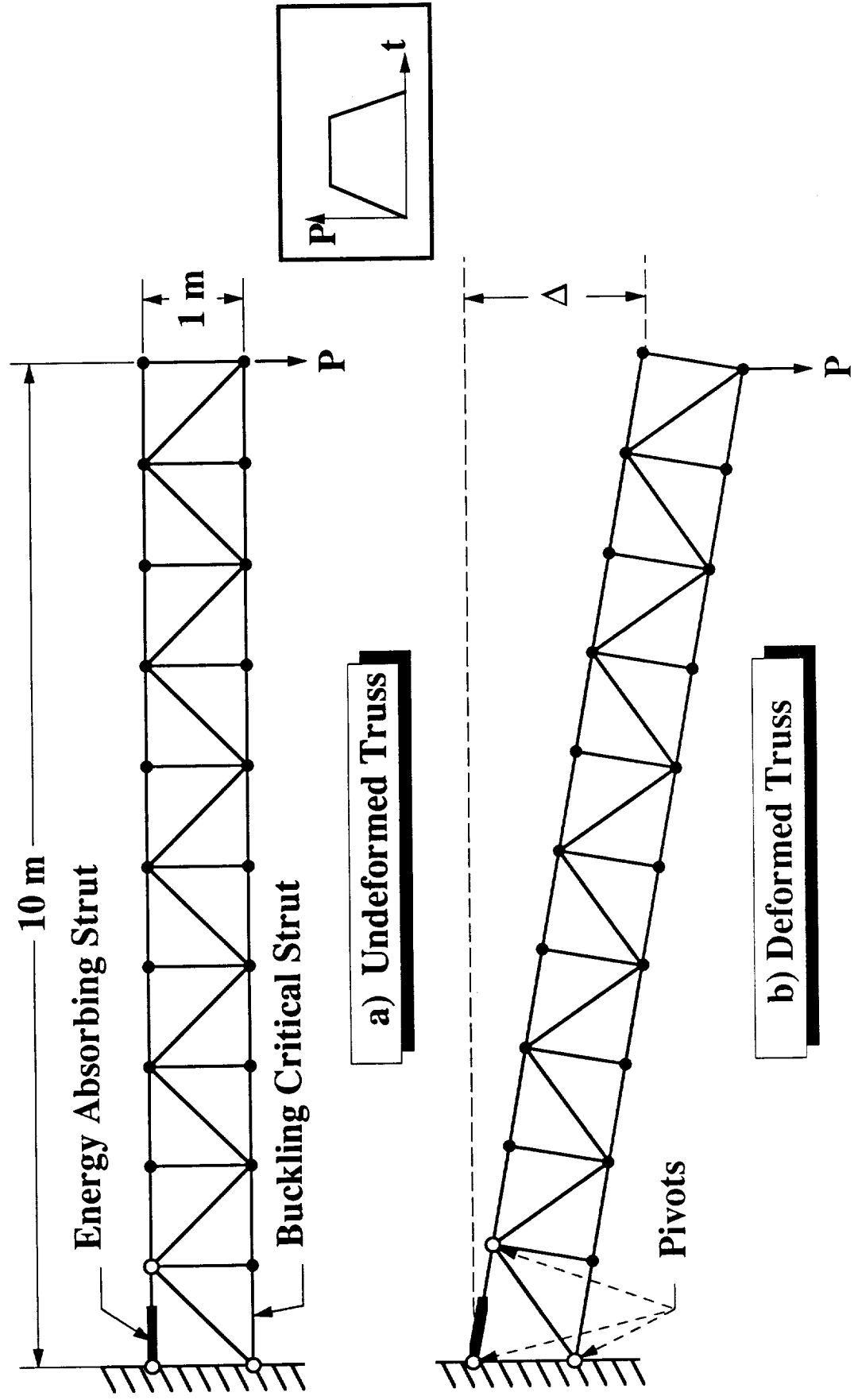
Truss absorbed energy is:

$$E = P\Delta$$

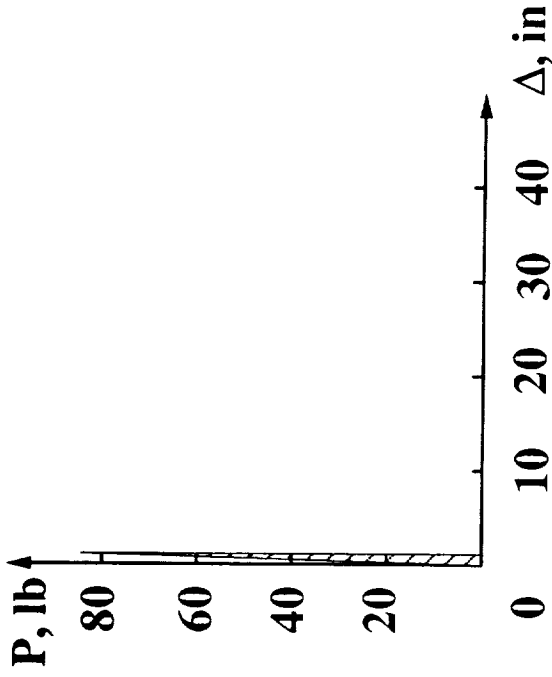
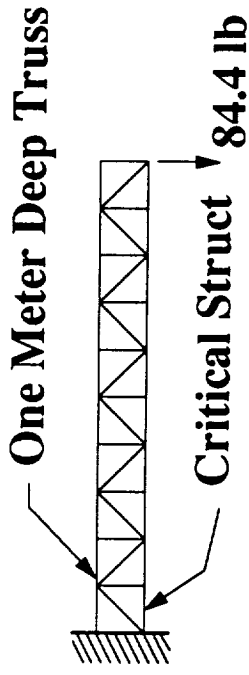
or

$$E = P \frac{L}{H} \delta = 2P_L \delta$$

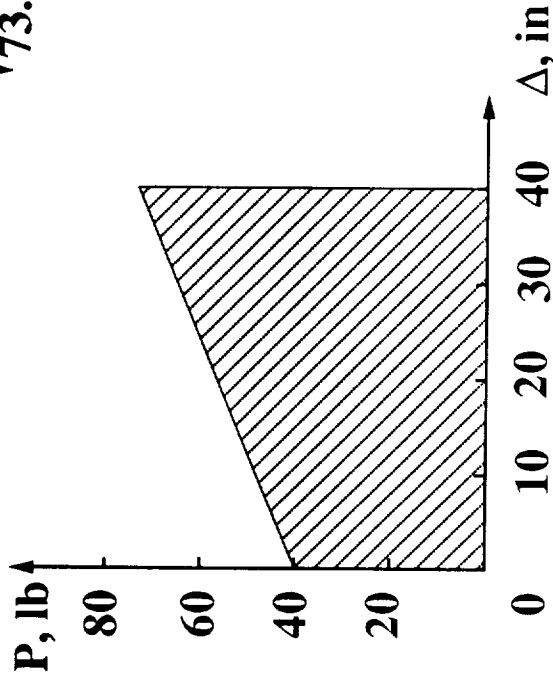
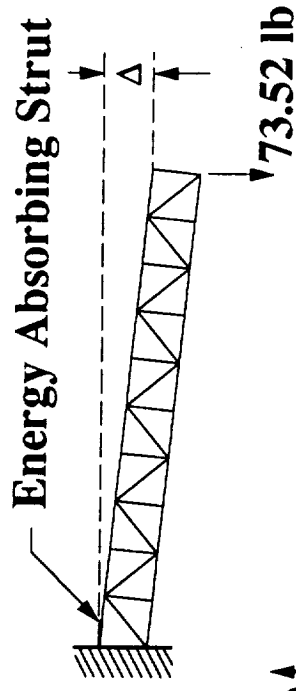
# TEN BAY LONG RESILIENT TRUSS EXAMPLE



# STORED ENERGY CHARACTERISTICS OF ONE METER DEEP TRUSS.

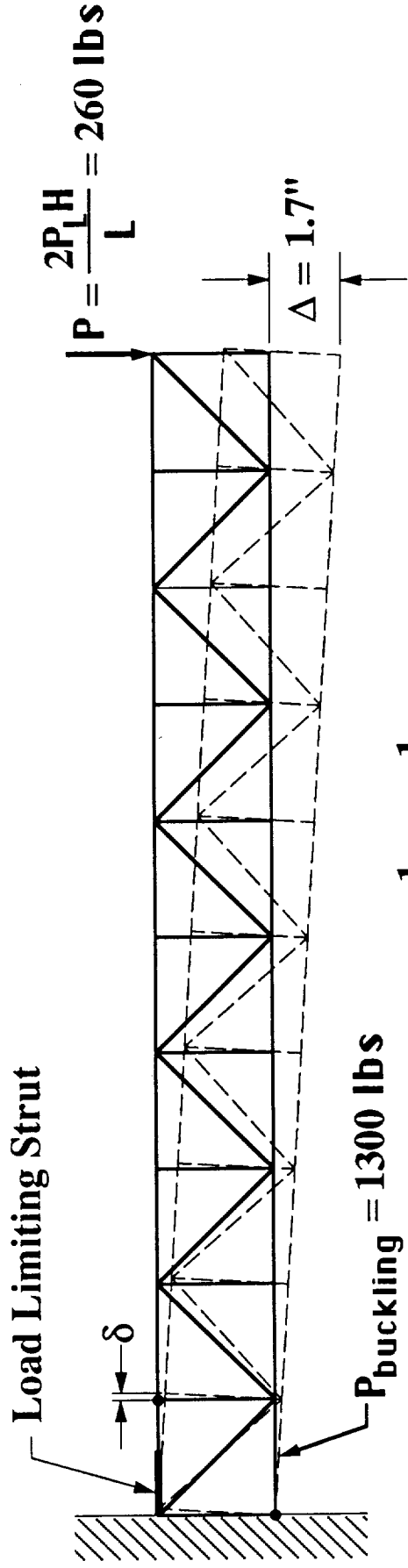


a) Strain energy stored in regular truss (50 in-lb)



b) Energy absorbed by resilient truss (2300 in-lb)

# ENERGY ABSORBING POTENTIAL FOR 10-BAY 5-METER DEEP TRUSS



$$E = \frac{1}{2} P \Delta = \frac{1}{2} 260 \times 1.7 = 220 \text{ in-lb}$$

For load limiting strut with preload of 500 lbs and  $\delta = 4''$

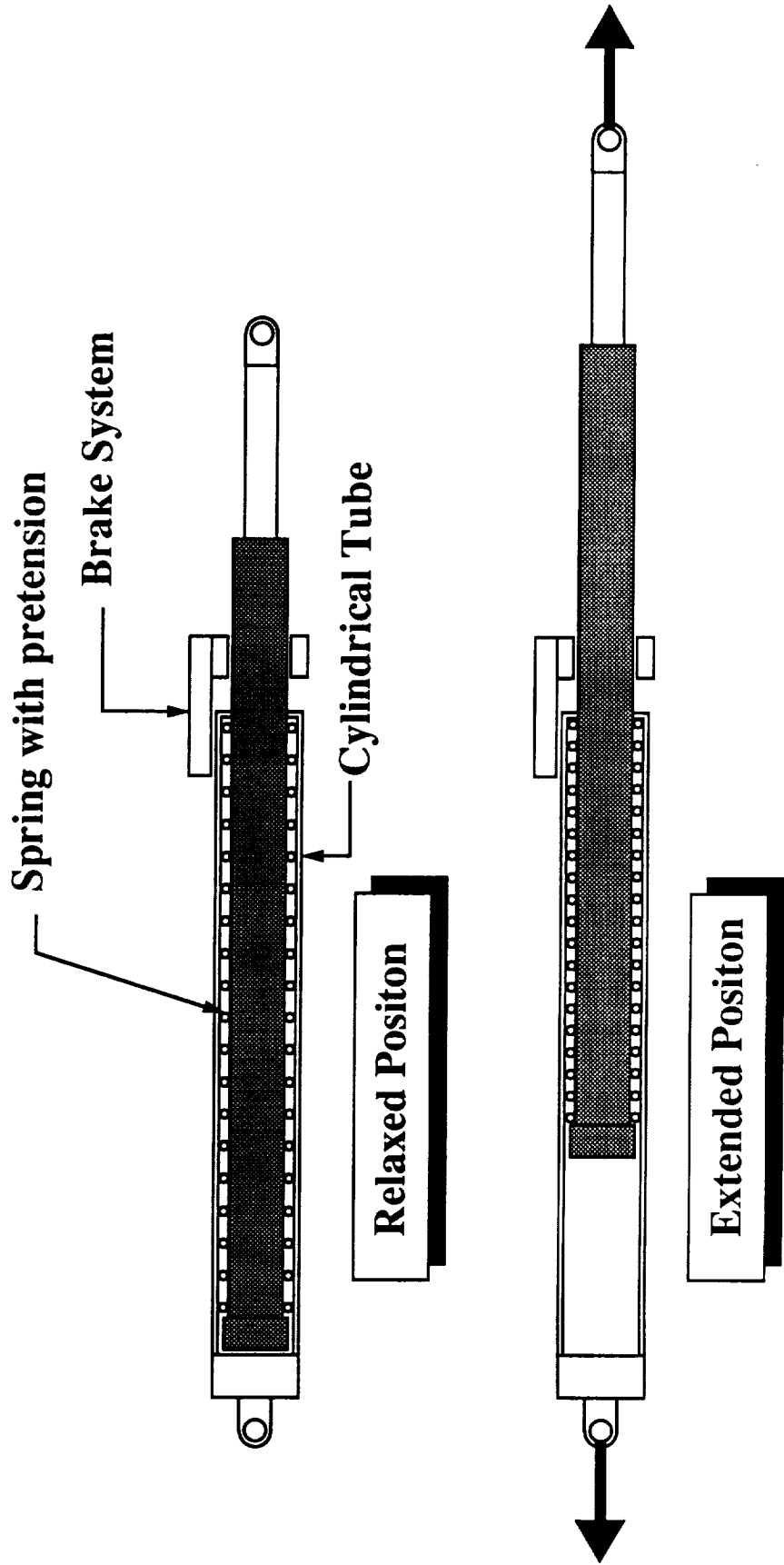
$$E = 2P_L \delta = 2 \times 500 \times 4 = 4000 \text{ in-lb}$$

$$\Delta = 10\delta = 40''$$

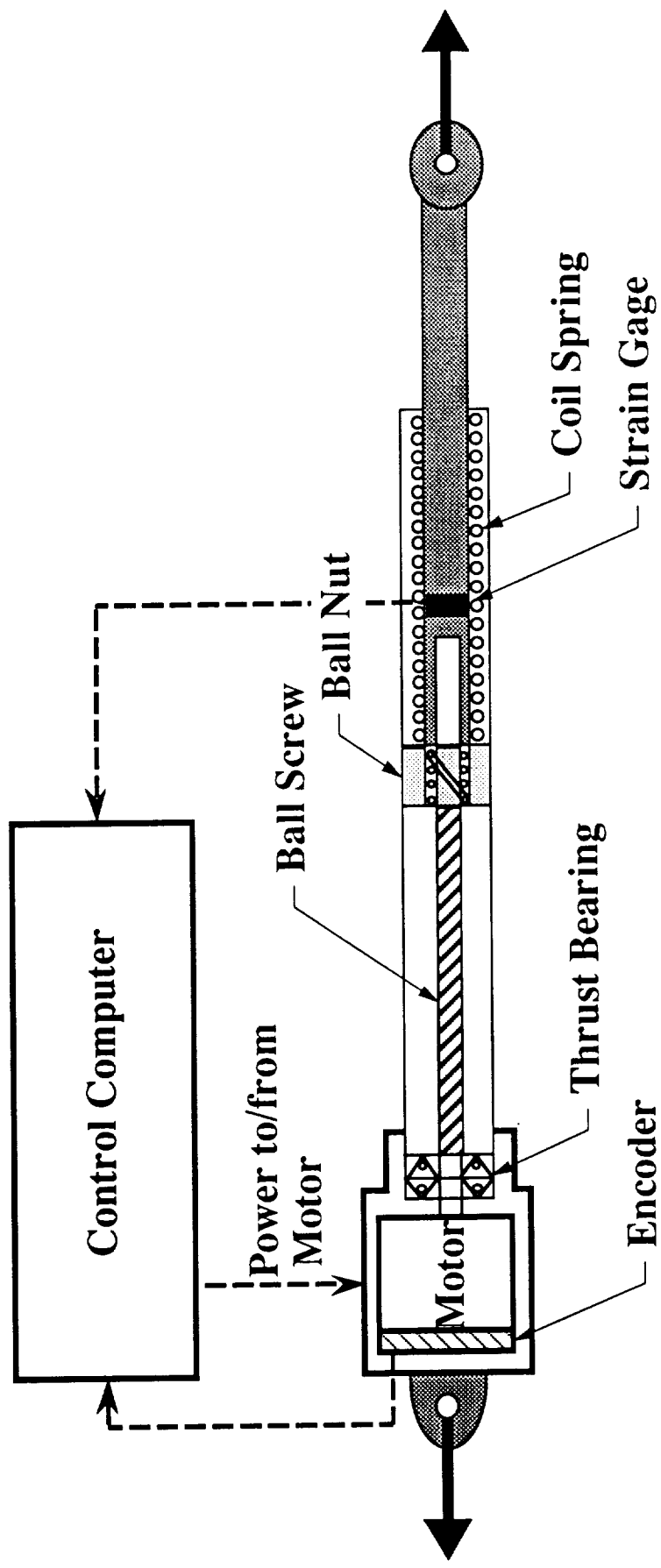
$$\frac{\Delta}{H} = \frac{40}{196} = .2$$



# SCHEMATIC OF ENERGY ABSORBING STRUT

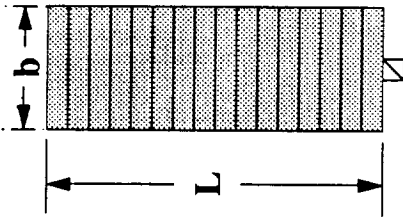


# LINEAR LOAD AND MOTION CONTROL ACTUATOR ( Energy Absorbing Strut )



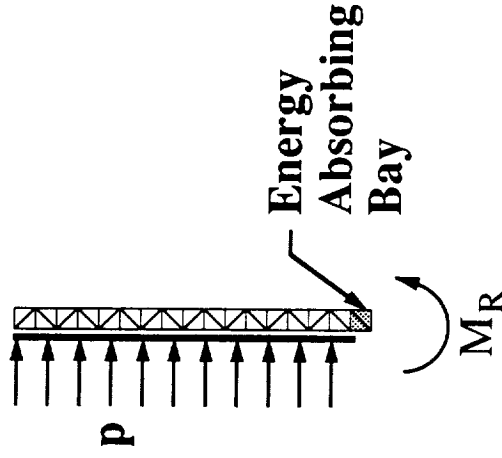
# RIGID BODY RESPONSE OF A SOLAR ARRAY TO THE SHUTTLE THRUSTER PRESSURE IMPINGEMENT.

Front View

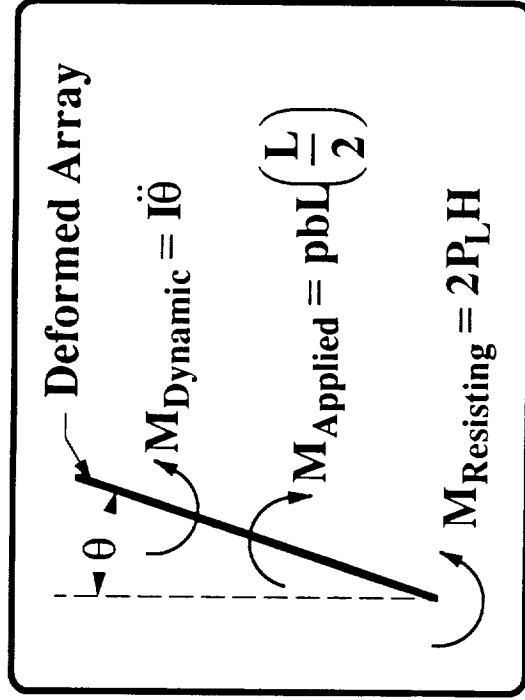
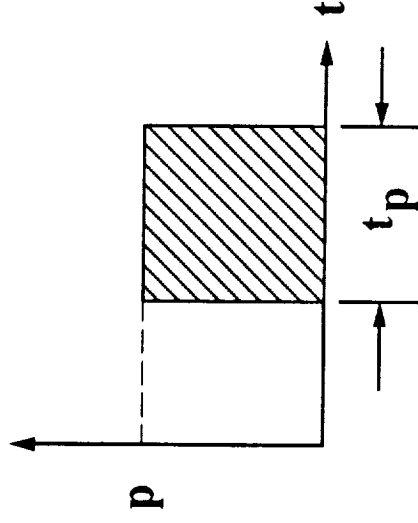


Solar Array

Side View



Applied Pressure Impulse



(1)  $M_A - M_R = I\ddot{\theta}$

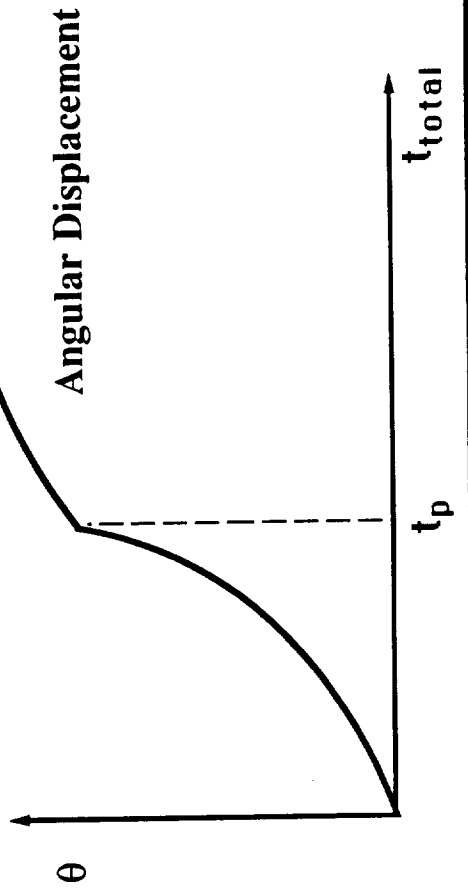
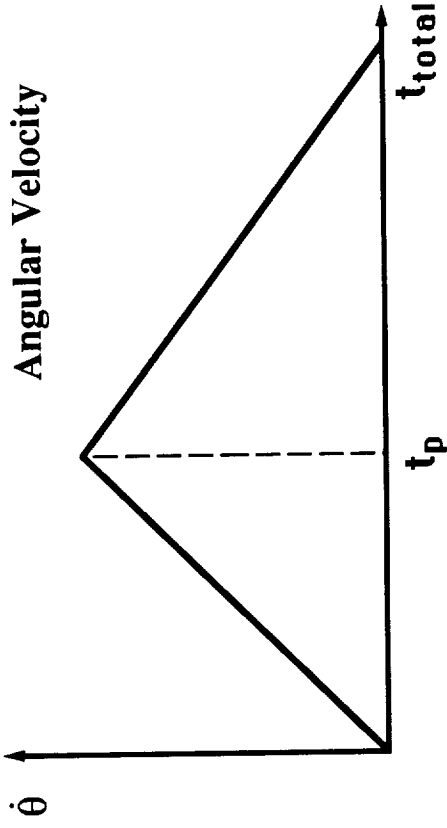
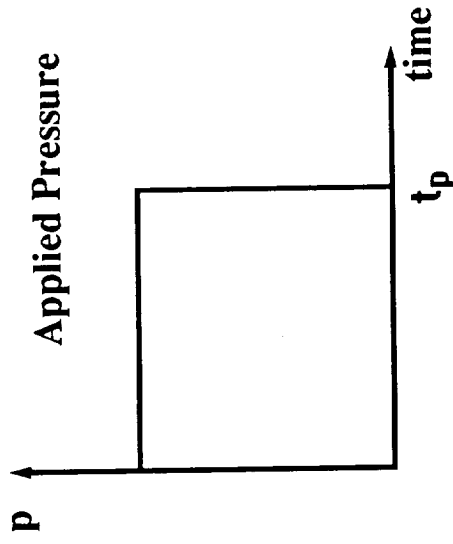
Integration Yields:

(2)  $\theta = \frac{M_A t_p^2}{2I} \left( \frac{M_A - 1}{M_R} \right)$

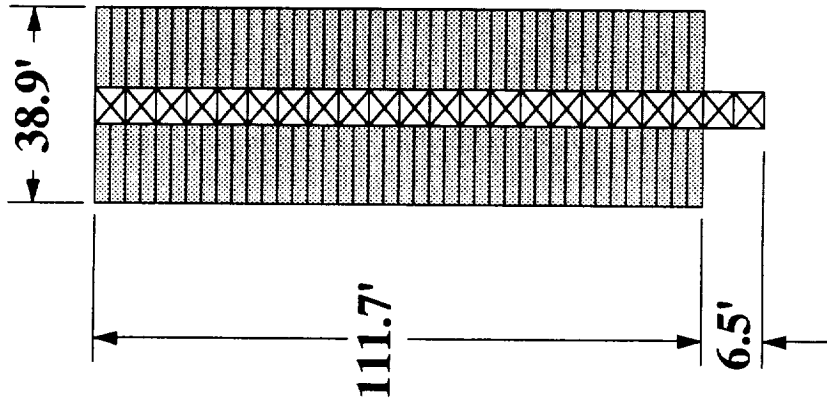
or

(3)  $\delta = \frac{M_A t_p^2}{2I} H \left( \frac{M_A - 1}{M_R} \right)$

# SOLAR ARRAY PIECEWISE LINEAR RESPONSE

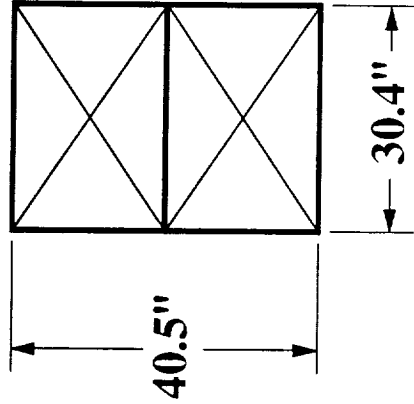


# SOLAR ARRAY CHARACTERISTICS



Array Weight, lbs	
Tip	31
Truss beam	315.78
Canister	534.65
Array Blanket	1246.57
<b>Total</b>	<b>2128</b>

Array Beam ( one bay )



Longeron properties  
 Area =  $.5 \times .5 = .25 \text{ in}^2$   
 $E = 10e6$   
 $P_{crit} = 1250 \text{ lbs}$

Truss bending stiffness  
 $EI = .43 \times EI(\text{theoretical})$   
 $= 98 \text{ lb-in}^2$  (Tom Irvine)

# SOLAR ARRAY TIP DEFLECTION AND REQUIRED ACTUATOR STROKE

$$\delta = \frac{M_A t_p^2 H}{2I} \left( \frac{M_R}{M_A} - 1 \right)$$

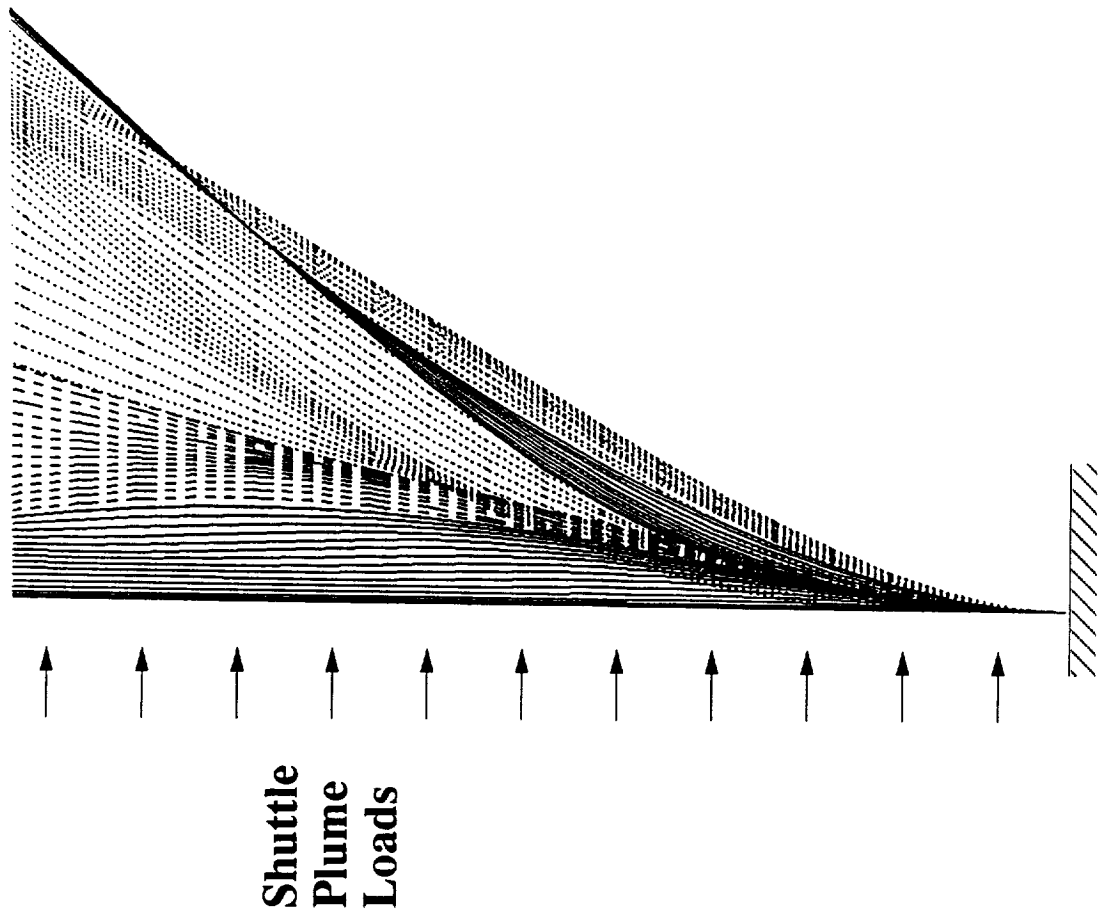
## Array input quantities

tp = .75 sec  
Plume pressure = .0002 psi  
Total load on array = 104 lbs  
Assumed actuator preload = 300lb

## Tip displacement

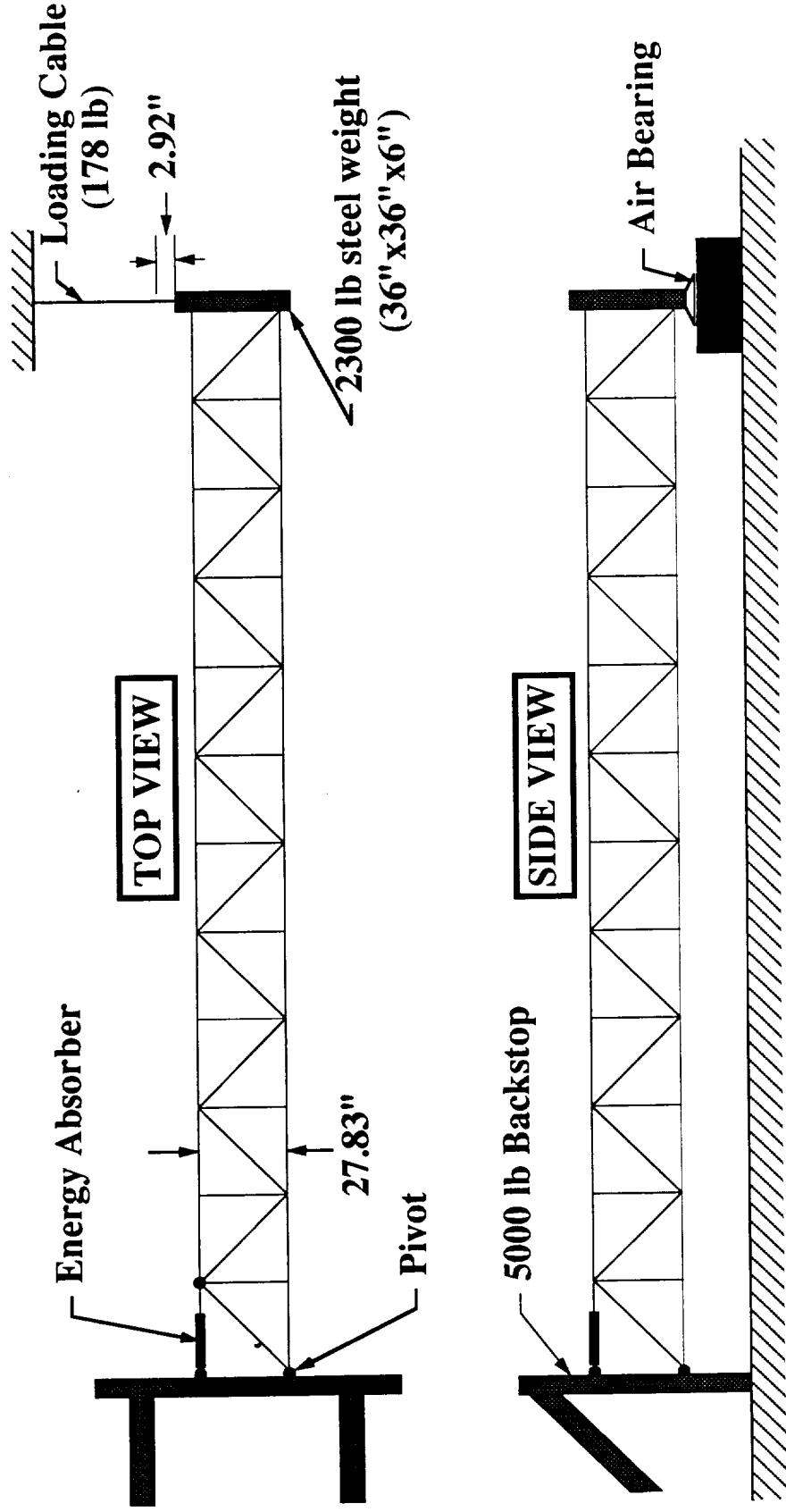
Rigid body - 31"  
Finite Element - 98"; Actuator stroke = 2.1"

# SOLAR ARRAY RESPONSE FROM FINITE ELEMENT ANALYSIS



# 12 BAY ENERGY ABSORBING TEST BED

( Beam Length = 27.83' )



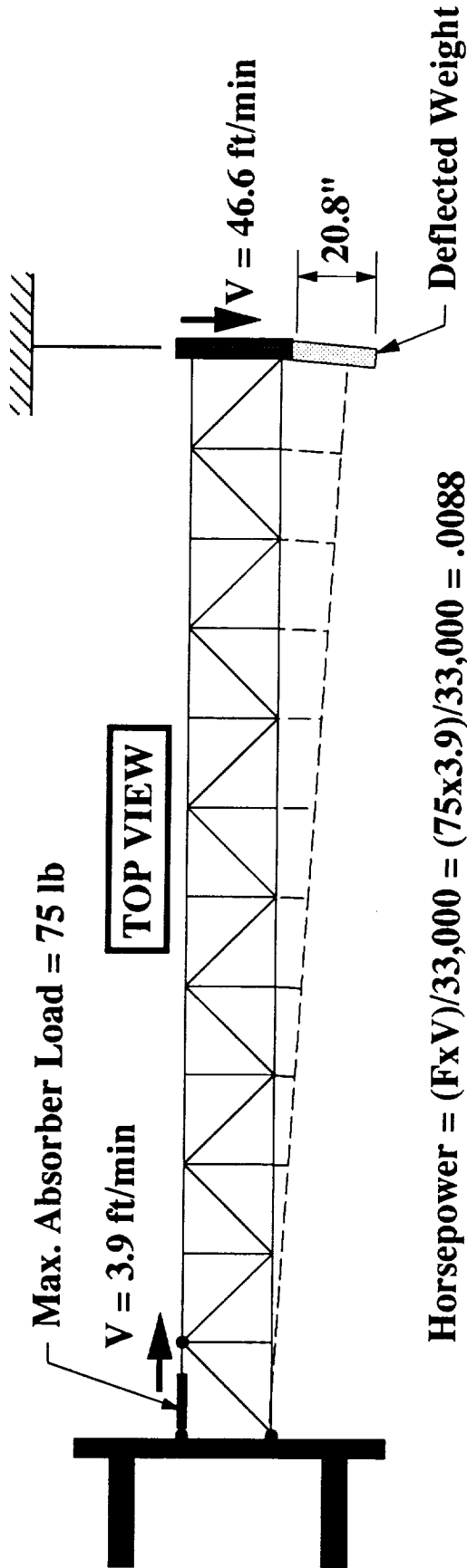
Beam Weight = 75.47 lb      Beam Frequency = . 5 Hz



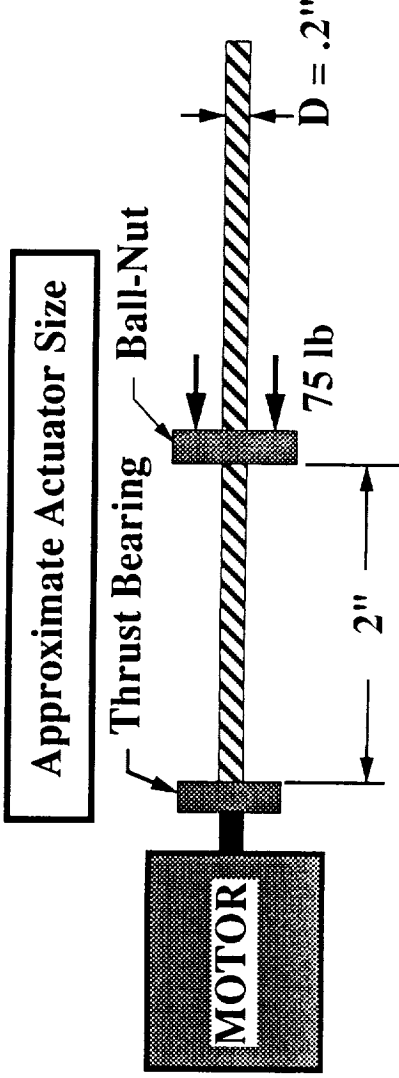
# 12 BAY ENERGY ABSORBING TEST BED DYNAMICS

( Beam Length = 27.83' )

Beam Strain Energy = 260 in-lb = 22 ft-lb

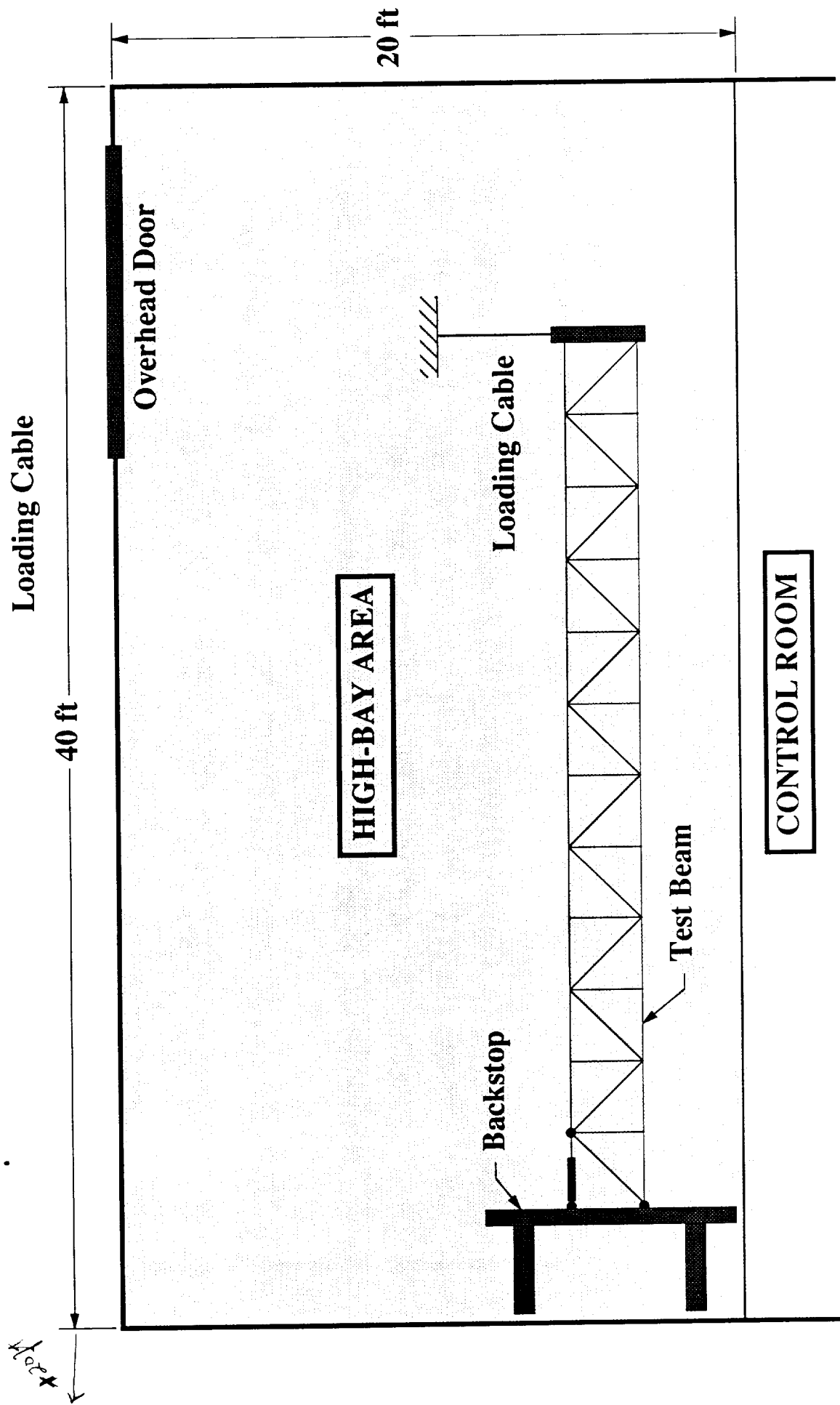


Horsepower =  $(F \times V) / 33,000 = (75 \times 3.9) / 33,000 = .0088$



Approximate Actuator Size

# NEW AERO-LAB WITH 12-BAY TEST BEAM



## **CONCLUDING REMARKS**

**All example cases analyzed to date indicate that there is a large payoff in efficiency and fail-safety by using energy absorbers as a "fuse" for limiting and absorbing transient loadings on space structures**

**Large scale experiments are needed to demonstrate the application of these devices**