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TABULATED PRESSURE DATA FOR SEVERAL FLAP-TYPE TRAILING-EDGE CONTROLS ON A TRAPEZOIDAL WING AT MACH NUMBERS OF 1.61 AND 2.01

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NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

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TABULATED PRESSURE DATA FOR SEVERAL FLAP-TYPE TRAILING-EDGE CONTROLS ON A TRAPEZOIDAL WING AT MACH NUMBERS OF 1.61 AND 2.01

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SUMMARY

An investigation has been made at Mach numbers of 1.61 and 2.01 for a range of Reynolds number from 1.7×10^6 to 5.6×10^6 to determine the pressure distributions at several spanwise stations for a series of 25.4-percent-chord trailing-edge controls on a trapezoidal wing having a 23° sweptback leading edge, aspect ratio of 3.1, and taper ratio of 0.4. Pressure-distribution measurements were made at angles of attack from 0° to ±15° for control deflections from -30° to 30°. This report contains the tabulated pressure data for the complete range of test variables.

INTRODUCTION

As part of a general program of research on controls, an investigation is underway in the Langley 4- by 4-foot supersonic pressure tunnel to determine the important parameters in the design of controls for use on a trapezoidal wing at supersonic speeds. The first results of the tests were reported in reference 1 and showed the control effectiveness and hinge-moment characteristics for a series of flap-type trailing-edge controls on a wing having a 23° sweptback leading edge, an aspect ratio of 3.1, and a taper ratio of 0.4.

The pressure distributions and chordwise and spanwise loadings associated with the wing-control configurations of reference 1 are presented in reference 2. The analysis in reference 2 did not require the inclusion of all the available data and these were therefore omitted for the sake of clearness and simplicity. In order to make the data available, the present report presents the complete tabulated pressure data for the range of the test variables.

The wing angle-of-attack range for these tests was from 0° to $\pm 12^\circ$ or $\pm 15^\circ$ and the control deflection range, relative to the wing, was from -30° to 30°. The tests were conducted at Mach numbers of 1.61 and 2.01 for a Reynolds number range from 1.7×10^6 to 5.6×10^6, based on the wing mean aerodynamic chord of 11.72 inches.

SYMBOLS

$b/2$	wing semispan
c_R	wing root chord
M	stream Mach number
p	stream static pressure
p_l	local surface pressure
P	pressure coefficient, $\frac{p_l - p}{q}$
q	stream dynamic pressure
R	Reynolds number (based on wing mean aerodynamic chord)
x	distance in chordwise direction from wing apex
y	distance in spanwise direction from wing root chord
α	wing angle of attack, deg
δ	control deflection relative to wing (positive when control trailing edge is down), deg

APPARATUS

Wind Tunnel

This investigation was conducted in the Langley 4- by 4-foot supersonic pressure tunnel, which is a rectangular, closed-throat, single-return type of wind tunnel with provisions for the control of the pressure, temperature, and humidity of the enclosed air. Flexible nozzle walls were adjusted to give the desired test-section Mach numbers of 1.61

and 2.01. During the tests, the dewpoint was kept below -20° F at atmospheric pressure so that the effects of water condensation in the supersonic nozzle were negligible.

Model and Model Mounting

The model used in this investigation consisted of a trapezoidal wing having six interchangeable trailing-edge controls and various associated control adapters (or replacement sections) required to fit the controls to the basic wing. A sketch of the six model configurations is shown in figure 1 with the shaded areas denoting the moveable controls.

The basic wing had a 23° sweptback leading edge, a root chord of 15.88 inches, a tip chord of 6.17 inches, and a semispan of 17.02 inches. The wing section was a modified hexagon having a constant ratio of local thickness to local chord of 4.5 percent. The flat midsection extended from 30-percent chord to 70-percent chord and the corners joining the flat midsection to the leading- and trailing-edge wedges were rounded to a 22.5-inch radius. The unswept hinge lines were located at the 74.6-percent-chord line for all control configurations. As shown in figure 1 control configurations 4, 5, and 6 had identical plan forms, but varying amounts of trailing-edge thickness; $t = 0$, 0.5, and 1.0, respectively. The hinge-line gap was maintained at 0.01 inch (0.08 percent $\bar{c}$) for all configurations except for one series of tests with configuration 4 in which the gap was increased to 0.20 inch (1.71 percent $\bar{c}$) by moving the control and hinge line rearward.

The model was constructed of steel, with the pressure-tube installations made in grooves in the surface which were faired over with a transparent plastic material. The 144 to 169 pressure orifices were located at five spanwise stations on the main wing ahead of the control hinge line and at five to eight spanwise stations behind the hinge line, depending on the configuration being tested. The chordwise locations of the pressure orifices are listed in table I and the spanwise locations of the orifice stations are shown in figure 2. All screw holes, pits, and mating lines were filled with dental plaster and faired smooth.

The semispan wing was mounted horizontally in the tunnel from a turntable in a steel boundary-layer bypass plate which was located vertically in the test section about 10 inches from the side wall as shown in figure 3. A photograph of model configuration 2 mounted for testing is shown in figure 4. Although the clearness of the plastic material over the tubing installations makes it appear that the wing surface is rough, actually the finish was very smooth.

TESTS

Techniques

The model angle of attack was changed by rotating the turntable in the bypass plate on which the wing was mounted (see figure 3). The angle of attack was measured by a vernier on the outside of the tunnel, inasmuch as the angular deflection of the wing under load was negligible. Control deflection was changed by a gear mechanism mounted on the pressure box which rotated the strain-gage balance, the torque tube, and the control as a unit. The control angles were set with the aid of an electrical control-position indicator mounted inside the wing at the hinge line and were checked with a cathetometer mounted outside the tunnel. The pressure distributions were determined from photographs of the multiple-tube manometer boards to which the pressure leads from the model orifices were connected.

Most of the controls were equipped with orifices on one surface only, because structural limitations made it impossible to get the necessary pressure tubes through the torque tube to instrument both surfaces. For these models, the tests were run at positive and negative angles of attack over the control-deflection range.

Range of Conditions

The majority of the test configurations had a control deflection range from -30° to 30° for angles of attack of 0°, $\pm 6^\circ$, and $\pm 12^\circ$ and an angle-of-attack range from 0° to $\pm 15^\circ$ for 0° control deflection. Most of the tests were made at tunnel stagnation pressures of 13.0 and 15.1 pounds per square inch at Mach numbers of 1.61 and 2.01, respectively, corresponding to a Reynolds number of 3.6×10^6 based on the wing mean aerodynamic chord. Additional tests were made with configuration 4 in which the tunnel stagnation pressure was varied to give Reynolds numbers of 1.7×10^6 and 5.6×10^6 at $M = 1.61$ and Reynolds numbers of 1.7×10^6 and 4.5×10^6 at $M = 2.01$. In order to insure a turbulent boundary layer over the model during the tests, 3/16-inch-wide strips of number 60 carborundum were attached to the wing upper and lower surfaces at a distance of 1/4 inch from the leading edge. These strips completely spanned the model except within 1/4 inch of the orifice stations.

PRECISION OF DATA

The mean Mach numbers in the region occupied by the model are estimated from calibrations to be 1.61 and 2.01 with local variations being smaller than ±0.02. There is no evidence of any significant flow angularities. The estimated accuracies in setting the wing angle of attack and control deflection are ±0.05° and ±0.1°, respectively. The basic measured quantity P is believed accurate to ±0.01.

PRESENTATION OF DATA

The recorded pressure data are presented in tables II through XV as values of pressure coefficient P measured on the surfaces of the test configurations. The chordwise locations of the pressure orifices were previously listed in table I and the spanwise locations of the orifice stations were shown in figure 1(b). Tables II through VIII present the pressure data for the seven basic configurations at $M = 1.61$ and $R = 3.6 \times 10^6$. Tables IX and X contain the data for the extreme Reynolds numbers tested (1.7×10^6 and 5.6×10^6) at $M = 1.61$. Tables XI through XIII are for the data obtained on configurations 2, 3, and 4 at $M = 2.01$ and $R = 3.6 \times 10^6$. Finally, tables XIV and XV present the data for the extreme Reynolds numbers tested (1.7×10^6 and 4.5×10^6) at $M = 2.01$.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., September 21, 1955.

REFERENCES

1. Lord, Douglas R., and Czarnecki, K. R.: Aerodynamic Characteristics of Several Flap-Type Trailing-Edge Controls on a Trapezoidal Wing at Mach Numbers of 1.61 and 2.01. NACA RM L54D19, 1954.

2. Lord, Douglas R., and Czarnecki, K. R.: Pressure Distributions and Aerodynamic Loadings for Several Flap-Type Trailing-Edge Controls on a Trapezoidal Wing at Mach Numbers of 1.61 and 2.01. NACA RM L55J03, 1955.

TABLE I

CHORDWISE LOCATIONS OF ORIFICES (x/c_R)

[Station spanwise locations shown in figure 2]

Orifice number		Stations							
Upper surface	Lower surface	1	2	3	4	5	6	7	8
1	17	0.034		0.157	0.275			0.394	0.469
2	18	.093		.203	.308			.414	.482
3	19	.162		.260	.354			.449	.509
4	20	.260		.342	.420			.499	.549
5	21	.358		.423	.485			.548	.588
6	22	.456		.505	.551			.598	.628
7	23	.554		.586	.617			.648	.667
8	24	.603		.627	.650			.673	.687
9	25	.652		.667	.682			.697	.707
10	26	.701		.708	.715			.722	.727
11	27	.737		.737	.737			.737	.737
12	28	.757	0.751	.751	.750	0.749	0.749	.748	.747
13	29	.774	.770	.769	.764	.762	.762	.760	.756
14	30	.838	.825	.822	.807	.798	.798	.792	.782
15	31	.902	.879	.875	.850	.835	.835	.824	.808
16	32	.976	.940	.934	.893	.870	.870	.852	.826

TABLE II

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -15$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.752		1.031	1.077			1.059	.844	1
2	.666		.850	.925			.961	.650	2
3	.714		.758	.811			.834	.516	3
4	.619		.608	.650			.668	.353	4
5	.439		.436	.493			.534	.234	5
6	.471		.480	.502			.480	.163	6
7	.483		.485	.518			.461	.135	7
8	.478		.509	.511			.438	.100	8
9	.462		.466	.451			.434	.127	9
10	.391		.397	.409			.331	.111	10
11	.414		.397	.354			.285	.072	11
12	.324		.341	.308	.247	.326	.267	.085	12
13	.272		.294	.297	.282	.279	.189	-.017	13
14	.274		.268	.285	.249	.250	.212	.025	14
15	.284		.284	.277	.235	.252	.217	.015	15
16	.280		.288	.257	.242	.249	.213	.004	16
17	-.243		-.315	-.334			-.350	-.330	17
18	-.173		-.251	-.283			-.270	-.213	18
19	-.179		-.244	-.248			-.254	-.232	19
20	-.200		-.250	-.261			-.259	-.263	20
21	-.249		-.306	-.299			-.296	-.316	21
22	-.250		-.311	-.308				-.369	22
23	-.252			-.313			-.304	-.396	23
24	-.253		-.291	-.311			-.312	-.410	24
25	-.252		-.285	-.321			-.291	-.385	25
26	-.274		-.300	-.327			-.285	-.407	26

$\alpha = -12$ $\delta = -35$

1	.607		.860	.933			.940	.755	1
2	.516		.704	.800			.853	.564	2
3	.531		.636	.701			.733	.441	3
4	.508		.515	.553			.577	.294	4
5	.348		.349	.407			.444	.181	5
6	.351		.338	.369			.372	.096	6
7	.344		.333	.368			.804	.414	7
8	.330		.348	.360			.860	.383	8
9	.315		.316	.316			.877	.496	9
10	.252		.253	.331			.855	.496	10
11	.289		.253	.347			.870	.459	11
12	.198		.228	.381	.503	.330	.208	.472	12
13	.169		.182	.399	.507	.734	.880	.638	13
14	.163		.166	.445	.204	1.200	1.181	.997	14
15	.158		.171	.416	.009	.943	1.170	.834	15
16	.164		.221	.335	-.062	.791	.982	.704	16
17	-.181		-.213	-.229			-.229	-.203	17
18	-.119		-.182	-.187			-.179	-.085	18
19	-.129		-.184	-.177			-.176	-.136	19
20	-.153		-.194	-.200			-.194	-.171	20
21	-.214		-.249	-.237			-.240	-.238	21
22	-.206		-.260	-.254				-.299	22
23	-.212			-.259			-.249	-.318	23
24	-.214		-.240	-.260			-.259	-.323	24
25	-.213		-.240	-.267			-.240	-.304	25
26	-.246		-.261	-.281			-.244	-.316	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = -25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.604		.861	.941			.943	.750	1
2	.518		.707	.801			.853	.571	2
3	.535		.641	.707			.738	.435	3
4	.513		.524	.561			.577	.284	4
5	.350		.350	.407			.446	.186	5
6	.353		.340	.372			.375	.098	6
7	.349		.341	.367			.346	.077	7
8	.333		.347	.360			.370	.164	8
9	.323		.318	.317			.697	.394	9
10	.258		.262	.284			.754	.419	10
11	.288		.262	.246			.763	.389	11
12	.199		.223	.197	.378	.655	.754	.391	12
13	.171		.181	.174	.441	.778	.810	.488	13
14	.158		.167	.255	.231	.854	1.014	.768	14
15	.167		.174	.355	.064	.705	.921	.678	15
16	.169		.174	.333	.019	.613	.787	.579	16
17	-.185	-.217	-.239			-.236	-.224		17
18	-.130	-.184	-.193			-.186	-.102		18
19	-.129	-.183	-.182			-.176	-.138		19
20	-.149	-.194	-.197			-.196	-.177		20
21	-.212	-.247	-.239			-.237	-.244		21
22	-.203	-.252	-.254				-.312		22
23	-.210		-.262			-.251	-.329		23
24	-.212	-.236	-.263			-.258	-.361		24
25	-.214	-.235	-.269			-.245	-.325		25
26	-.240	-.257	-.282			-.242	-.310		26

$\alpha = -12$ $\delta = -15$

1	.604		.857	.935			.943	.758	1
2	.519		.705	.802			.851	.568	2
3	.529		.639	.703			.742	.444	3
4	.505		.521	.555			.579	.288	4
5	.342		.345	.405			.448	.183	5
6	.343		.342	.370			.376	.100	6
7	.344		.338	.367			.347	.070	7
8	.329		.347	.365			.320	.049	8
9	.311		.316	.316			.311	.070	9
10	.254		.262	.285			.283	.051	10
11	.283		.262	.252			.563	.159	11
12	.197		.228	.197	.330	.633	.628	.272	12
13	.173		.183	.183	.361	.629	.701	.431	13
14	.167		.169	.171	.294	.527	.703	.465	14
15	.163		.176	.193	.111	.447	.614	.405	15
16	.164		.179	.258	.042	.406	.542	.355	16
17	-.182	-.218	-.233			-.240	-.214		17
18	-.135	-.187	-.196			-.188	-.097		18
19	-.132	-.181	-.178			-.176	-.142		19
20	-.156	-.196	-.196			-.194	-.177		20
21	-.218	-.257	-.241			-.238	-.238		21
22	-.206	-.261	-.254				-.305		22
23	-.213		-.260			-.250	-.336		23
24	-.218	-.240	-.262			-.258	-.359		24
25	-.217	-.239	-.272			-.243	-.340		25
26	-.242	-.261	-.285			-.248	-.354		26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.602		.859	.939			.947	.758	1
2	.517		.705	.806			.856	.576	2
3	.525		.639	.705			.743	.450	3
4	.505		.524	.559			.580	.307	4
5	.339		.340	.409			.453	.197	5
6	.350		.339	.374			.378	.105	6
7	.342		.337	.369			.349	.078	7
8	.330		.343	.362			.325	.049	8
9	.315		.318	.315			.316	.067	9
10	.249		.258	.286			.226	.052	10
11	.286		.258	.258			.196	.020	11
12	.207		.237	.212	.151	.227	.194	.040	12
13	.178		.192	.191	.178	.183	.120	-.064	13
14	.173		.172	.179	.157	.151	.123	-.040	14
15	.172		.177	.178	.141	.151	.123	-.029	15
16	.174		.183	.172	.132	.142	.105	-.044	16
17	-.182		-.216	-.231			-.235	-.209	17
18	-.136		-.185	-.194			-.190	-.092	18
19	-.134		-.183	-.180			-.175	-.137	19
20	-.157		-.196	-.194			-.197	-.176	20
21	-.217		-.254	-.240			-.237	-.239	21
22	-.209		-.257	-.251				-.302	22
23	-.217			-.261			-.251	-.335	23
24	-.218		-.243	-.261			-.261	-.359	24
25	-.218		-.240	-.270			-.242	-.339	25
26	-.246		-.259	-.283			-.243	-.356	26

$\alpha = -12$ $\delta = 5$

1	.606		.864	.939			.948	.763	1
2	.517		.709	.803			.852	.568	2
3	.527		.641	.712			.741	.445	3
4	.510		.525	.559			.582	.290	4
5	.350		.351	.409			.446	.179	5
6	.351		.340	.373			.377	.102	6
7	.344		.342	.369			.349	.076	7
8	.332		.350	.363			.323	.039	8
9	.320		.320	.315			.316	.064	9
10	.258		.262	.282			.228	.047	10
11	.288		.262	.257			.195	.019	11
12	.203		.231	.201	.136	.065	.024	-.083	12
13	.174		.188	.189	.120	.044	-.044	-.186	13
14	.166		.161	.174	.077	.022	-.044	-.169	14
15	.161		.177	.172	.049	.009	-.044	-.164	15
16	.164		.179	.157	.021	-.057	-.051	-.167	16
17	-.181		-.213	-.233			-.236	-.216	17
18	-.133		-.185	-.195			-.192	-.095	18
19	-.129		-.181	-.183			-.177	-.140	19
20	-.155		-.194	-.198			-.199	-.176	20
21	-.211		-.253	-.243			-.238	-.250	21
22	-.206		-.258	-.258				-.315	22
23	-.214			-.263			-.258	-.336	23
24	-.213		-.240	-.264			-.261	-.369	24
25	-.216		-.241	-.273			-.243	-.349	25
26	-.242		-.262	-.284			-.245	-.366	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 15$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.606		.863	.942			.951	.745	1
2	.517		.710	.803			.856	.561	2
3	.531		.638	.710			.740	.434	3
4	.509		.520	.558			.583	.287	4
5	.341		.349	.412			.448	.176	5
6	.350		.342	.376			.381	.097	6
7	.345		.339	.373			.351	.070	7
8	.330		.348	.366			.328	.034	8
9	.320		.319	.317			.317	.056	9
10	.256		.262	.285			.229	.044	10
11	.290		.262	.252			.197	.006	11
12	.197		.232	.207	.138 - .152	-	.193 -	.248	12
13	.164		.186	.188	.092 - .177	-	.258 -	.329	13
14	.164		.161	.171	.031 - .197	-	.249 -	.293	14
15	.156		.169	.173	- .006 - .248	-	.258 -	.273	15
16	.166		.177	.152	- .031 - .284	-	.267 -	.278	16
17	- .184	- .219	- .234			-	.239 -	.233	17
18	- .136	- .188	- .197			-	.193 -	.106	18
19	- .134	- .187	- .181			-	.177 -	.150	19
20	- .156	- .196	- .198			-	.200 -	.188	20
21	- .215	- .253	- .242			-	.242 -	.259	21
22	- .210	- .258	- .253				-	.324	22
23	- .217		- .260			-	.257 -	.349	23
24	- .217	- .240	- .266			-	.264 -	.375	24
25	- .215	- .237	- .274			-	.247 -	.351	25
26	- .242	- .259	- .283			-	.243 -	.374	26

$\alpha = -12$ $\delta = 25$

1	.609		.867	.947			.959	.736	1
2	.517		.710	.806			.866	.571	2
3	.536		.643	.714			.750	.441	3
4	.516		.530	.560			.587	.299	4
5	.349		.350	.412			.457	.182	5
6	.357		.349	.376			.383	.105	6
7	.350		.348	.376			.357	.077	7
8	.336		.353	.371			.331	.039	8
9	.325		.324	.321			.322	.062	9
10	.258		.265	.293			.234	.052	10
11	.289		.265	.262			.203	.017	11
12	.202		.239	.213	.140 - .303	-	.307 -	.338	12
13	.173		.187	.186	.093 - .310	-	.369 -	.355	13
14	.173		.161	.183	.032 - .330	-	.359 -	.371	14
15	.169		.179	.174	- .009 - .360	-	.374 -	.351	15
16	.172		.186	.162	- .032 - .389	-	.358 -	.340	16
17	- .181	- .212	- .234			-	.237 -	.232	17
18	- .134	- .184	- .187			-	.188 -	.107	18
19	- .133	- .185	- .174			-	.176 -	.148	19
20	- .148	- .193	- .194			-	.195 -	.186	20
21	- .211	- .250	- .241			-	.237 -	.257	21
22	- .202	- .252	- .252				-	.325	22
23	- .212		- .260			-	.249 -	.345	23
24	- .212	- .235	- .258			-	.254 -	.366	24
25	- .209	- .238	- .268			-	.047 -	.349	25
26	- .237	- .257	- .282				.009 -	.366	26

TABLE II.- Continued.

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.482		.710	.779			.798	.650	1
2	.407		.581	.666			.729	.487	2
3	.415		.522	.601			.642	.376	3
4	.406		.440	.478			.499	.228	4
5	.267		.274	.331			.376	.137	5
6	.263		.261	.293			.304	.062	6
7	.263		.255	.283			.271	.034	7
8	.247		.260	.273			.246	.004	8
9	.244		.232	.236			.235	.025	9
10	.185		.184	.206			.156	.016	10
11	.222		.184	.180			.128	-.015	11
12	.140		.162	.142	.098	.121	.125	.007	12
13	.117		.116	.111	.085	.085	.060	-.095	13
14	.111		.105	.120	.066	.080	.054	-.080	14
15	.082		.112	.113	.071	.083	.060	-.069	15
16	.093		.108	.100	.159	.080	.037	-.078	16
17	-.123	-.127	-.139			-.134	-.105		17
18	-.075	-.126	-.124			-.110	-.015		18
19	-.083	-.123	-.121			-.117	-.060		19
20	-.110	-.136	-.141			-.142	-.101		20
21	-.171	-.200	-.193			-.188	-.161		21
22	-.167	-.202	-.206				-.228		22
23	-.171		-.212			-.202	-.262		23
24	-.173	-.197	-.212			-.208	-.290		24
25	-.175	-.202	-.221			-.197	-.262		25
26	-.205	-.225	-.236			-.207	-.289		26

$\alpha = -6$ $\delta = -32.5$

1	.360		.499	.513			.511	.432	1
2	.308		.447	.506			.515	.329	2
3	.311		.403	.461			.491	.273	3
4	.299		.328	.371			.391	.178	4
5	.171		.185	.240			.287	.096	5
6	.173		.167	.201			.235	.025	6
7	.172		.154	.194			.266	.263	7
8	.160		.168	.186			.594	.288	8
9	.155		.143	.145			.627	.329	9
10	.105		.106	.120			.617	.293	10
11	.140		.106	.100			.626	.248	11
12	.070		.076	.064	.242	.449	.523	.280	12
13	.039		.031	.066	.273	.540	.642	.310	13
14	.057		.031	.177	.059	.930	.957	.650	14
15	.010		.031	.192	-.066	.806	1.075	.845	15
16	.010		.031	.204	-.115	.667	.911	.730	16
17	-.047	-.040	-.051			-.041	-.027		17
18	-.017	-.043	-.049			-.031	.031		18
19	-.025	-.047	-.045			-.036	.014		19
20	-.049	-.064	-.068			-.067	-.027		20
21	-.124	-.136	-.120			-.119	-.059		21
22	-.121	-.138	-.141				-.091		22
23	-.120		-.144			-.137	-.138		23
24	-.127	-.138	-.145			-.142	-.088		24
25	-.124	-.147	-.156			-.138	-.012		25
26	-.158	-.171	-.171			-.151	-.153		26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = -22.5$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.362		.501	.518			.513	.441	1
2	.305		.447	.505			.519	.336	2
3	.317		.404	.466			.497	.279	3
4	.302		.324	.375			.396	.176	4
5	.170		.193	.245			.284	.096	5
6	.177		.168	.201			.238	.030	6
7	.172		.161	.195			.196	-.004	7
8	.161		.169	.183			.171	.036	8
9	.159		.145	.147			.210	.062	9
10	.101		.107	.120			.494	.275	10
11	.141		.106	.103			.532	.250	11
12	.074		.075	.061	.206	.456	.525	.252	12
13	.037		.030	.030	.226	.587	.602	.371	13
14	.060		.035	.044	.080	.621	.806	.549	14
15	.005		.039	.078	-.047	.520	.765	.559	15
16	.020		.034	.140	-.067	.451	.664	.498	16
17	-.045	-.044	-.051			-.039	-.024		17
18	-.021	-.045	-.048			-.033	.034		18
19	-.032	-.045	-.043			-.037	.014		19
20	-.056	-.063	-.067			-.065	-.024		20
21	-.125	-.135	-.121			-.115	-.056		21
22	-.118	-.137	-.146				-.096		22
23	-.119		-.145			-.135	-.133		23
24	-.126	-.136	-.145			-.143	-.167		24
25	-.124	-.146	-.156			-.136	-.137		25
26	-.159	-.172	-.171			-.150	-.164		26

$\alpha = -6$ $\delta = -12.5$

1	.355		.506	.519			.515	.430	1
2	.304		.448	.508			.519	.326	2
3	.316		.403	.463			.491	.280	3
4	.301		.327	.376			.393	.174	4
5	.172		.188	.243			.288	.093	5
6	.174		.171	.202			.235	.031	6
7	.171		.160	.195			.195	.001	7
8	.161		.168	.187			.168	-.010	8
9	.155		.142	.148			.157	-.007	9
10	.109		.105	.123			.088	-.015	10
11	.141		.105	.099			.122	-.021	11
12	.071		.083	.066	.132	.375	.405	.242	12
13	.036		.027	.035	.162	.396	.426	.259	13
14	.062		.027	.040	.111	.295	.444	.265	14
15	-.001		.027	.040	.006	.250	.392	.237	15
16	.020		.027	.057	-.052	.212	.359	.206	16
17	-.054	-.051	-.056			-.042	-.010		17
18	-.027	-.049	-.048			-.039	.026		18
19	-.031	-.048	-.045			-.042	.015		19
20	-.054	-.060	-.074			-.075	-.026		20
21	-.125	-.135	-.126			-.121	-.060		21
22	-.124	-.140	-.148				-.093		22
23	-.125		-.148			-.146	-.143		23
24	-.125	-.140	-.151			-.152	-.179		24
25	-.125	-.151	-.162			-.148	-.156		25
26	-.165	-.173	-.176			-.163	-.194		26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.360		.503	.524			.523	.429	1
2	.305		.445	.512			.530	.326	2
3	.319		.406	.468			.504	.274	3
4	.301		.328	.375			.404	.172	4
5	.170		.184	.244			.295	.103	5
6	.178		.169	.197			.238	.021	6
7	.171		.157	.199			.203 -	.007	7
8	.160		.169	.190			.174 -	.007	8
9	.158		.146	.154			.167 -	.005	9
10	.104		.107	.124			.100 -	.021	10
11	.139		.107	.104			.079 -	.032	11
12	.062		.080	.076	.042	.117	.071 -	.035	12
13	.031		.026	.044	.042	.067	.017 -	.091	13
14	.059		.031	.052	.030	.036	.009 -	.085	14
15	.007		.036	.046	.014	.027	.009 -	.075	15
16	.019		.035	.042	.011	.021 -	.002 -	.067	16
17 -	.051	-	.046 -	.050			- .039 -	.034	17
18 -	.027	-	.053 -	.050			- .033	.019	18
19 -	.030	-	.051 -	.044			- .036	.006	19
20 -	.054	-	.064 -	.072			- .067 -	.032	20
21 -	.124	-	.140 -	.121			- .118 -	.072	21
22 -	.119	-	.138 -	.141			-	.108	22
23 -	.123		-	.142			- .136 -	.151	23
24 -	.126	-	.139 -	.142			- .144 -	.188	24
25 -	.126	-	.148 -	.154			- .140 -	.159	25
26 -	.159	-	.173 -	.170			- .152 -	.197	26

$\alpha = -6$ $\delta = 7.5$

1	.360		.504	.525			.515	.445	1
2	.306		.447	.511			.526	.344	2
3	.316		.406	.466			.498	.288	3
4	.300		.327	.376			.394	.182	4
5	.171		.188	.245			.291	.103	5
6	.175		.167	.198			.233	.032	6
7	.175		.161	.198			.201	.005	7
8	.160		.171	.189			.171 -	.004	8
9	.157		.147	.151			.163	.002	9
10	.109		.108	.125			.092 -	.009	10
11	.138		.108	.103			.073 -	.034	11
12	.065		.081	.062	.039 -	.081 -	.126 -	.169	12
13	.034		.034	.041	.009 -	.111 -	.188 -	.239	13
14	.060		.034	.041 -	.041 -	.122 -	.188 -	.188	14
15	.005		.037	.040 -	.066 -	.146 -	.188 -	.143	15
16	.020		.042	.036 -	.086 -	.161 -	.201 -	.120	16
17 -	.047	-	.044 -	.057			- .046 -	.025	17
18 -	.024	-	.046 -	.052			- .039	.026	18
19 -	.028	-	.048 -	.047			- .042	.010	19
20 -	.049	-	.064 -	.074			- .076 -	.029	20
21 -	.125	-	.139 -	.127			- .125 -	.062	21
22 -	.117	-	.138 -	.146			-	.103	22
23 -	.123		-	.148			- .141 -	.150	23
24 -	.124	-	.140 -	.148			- .150 -	.184	24
25 -	.125	-	.148 -	.158			- .143 -	.156	25
26 -	.164	-	.177 -	.171			- .156 -	.196	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 17.5$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.354		.505	.524			.521	.446	1
2	.306		.452	.510			.528	.339	2
3	.316		.404	.467			.505	.287	3
4	.301		.331	.377			.402	.188	4
5	.170		.189	.241			.291	.105	5
6	.174		.171	.200			.236	.035	6
7	.175		.162	.199			.200	.007	7
8	.160		.166	.190			.178	-.005	8
9	.158		.143	.153			.163	.004	9
10	.109		.105	.125			.096	-.010	10
11	.138		.105	.101			.080	-.040	11
12	.071		.086	.065	.026	-.258	-.278	-.290	12
13	.040		.035	.040	-.016	-.275	-.334	-.314	13
14	.065		.030	.050	-.072	-.290	-.335	-.249	14
15	.009		.040	.044	-.101	-.308	-.341	-.209	15
16	.021		.044	.035	-.126	-.359	-.348	-.224	16
17	-.052	-.046	-.057				-.044	-.024	17
18	-.025	-.053	-.047				-.034	.029	18
19	-.031	-.049	-.045				-.041	.012	19
20	-.053	-.062	-.077				-.075	-.029	20
21	-.124	-.142	-.124				-.126	-.069	21
22	-.119	-.143	-.145					-.106	22
23	-.122		-.147				-.136	-.150	23
24	-.124	-.140	-.150				-.146	-.186	24
25	-.123	-.149	-.159				-.140	-.161	25
26	-.164	-.175	-.174				-.026	-.202	26

$\alpha = -6$ $\delta = 27.5$

1	.359		.508	.529			.527	.456	1
2	.307		.450	.513			.531	.350	2
3	.317		.405	.469			.505	.300	3
4	.302		.330	.379			.401	.191	4
5	.177		.192	.249			.297	.117	5
6	.181		.174	.204			.241	.041	6
7	.173		.159	.198			.198	.019	7
8	.163		.170	.190			.175	-.004	8
9	.157		.149	.150			.167	.011	9
10	.108		.112	.124			.094	-.004	10
11	.141		.112	.101			.079	-.030	11
12	.078		.081	.069	.024	-.363	-.375	-.385	12
13	.047		.035	.049	-.019	-.384	-.411	-.359	13
14	.070		.041	.049	-.078	-.351	-.392	-.330	14
15	.015		.047	.049	-.103	-.404	-.345	-.300	15
16	.025		.047	.036	-.116	-.416	-.331	-.331	16
17	-.049	-.044	-.056				-.048	-.012	17
18	-.027	-.049	-.050				-.037	.026	18
19	-.033	-.047	-.047				-.043	.016	19
20	-.051	-.063	-.074				-.071	-.031	20
21	-.120	-.137	-.128				-.125	-.060	21
22	-.122	-.134	-.147					-.103	22
23	-.121		-.148				-.134	-.138	23
24	-.123	-.137	-.148				-.162	-.179	24
25	-.121	-.146	-.162				-.184	-.161	25
26	-.158	-.177	-.174				-.184	-.037	26

TABLE II.- Continued.

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-3$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.231		.292	.299			.308	.238	1
2	.185		.279	.279			.288	.176	2
3	.204		.270	.300			.289	.155	3
4	.194		.212	.258			.239	.101	4
5	.074		.080	.151			.164	.034	5
6	.004		.072	.097			.128	-.001	6
7	.060		.062	.093			.107	-.017	7
8	.069		.073	.084			.089	-.049	8
9	.066		.050	.036			.080	-.022	9
10	.025		.020	.030			.016	-.021	10
11	.054		.020	.011			.011	-.059	11
12	-.016		-.011	-.025	-.040	.017	-.009	-.040	12
13	-.047		-.057	-.039	-.031	-.016	-.066	-.091	13
14	-.022		-.057	-.047	-.037	-.039	-.066	-.077	14
15	-.071		-.052	-.047	-.061	-.051	-.066	-.066	15
16	-.066		-.042	-.039	-.055	-.052	-.076	-.060	16
17	.054		.058	.048			.058	.032	17
18	.165		.060	.053			.143	.077	18
19	.048		.056	.059			.060	.047	19
20	.025		.030	.030			.021	.015	20
21	-.060		-.057	-.042			-.032	-.012	21
22	-.058		-.068	-.059				-.017	22
23	-.055			-.061			-.059	-.021	23
24	-.057		-.073	-.066			-.068	-.050	24
25	-.058		-.084	-.074			-.070	-.029	25
26	-.099		-.110	-.096			-.098	-.066	26

$\alpha=0$ $\delta=-30$

1	.148		.152	.163			.154	.112	1
2	.105		.153	.160			.156	.097	2
3	.119		.156	.162			.151	.095	3
4	.103		.122	.132			.111	.054	4
5	-.009		.011	.047			.047	.015	5
6	.001		.004	.019			.016	.005	6
7	.002		-.009	.011			.016	.064	7
8	-.011		-.006	.005			.280	.254	8
9	-.003		-.026	-.023			.373	.269	9
10	-.040		-.049	-.049			.381	.240	10
11	-.014		-.050	-.066			.383	.207	11
12	-.081		-.085	-.116	.046	.233	.348	.174	12
13	-.113		-.123	-.121	.059	.268	.412	.226	13
14	-.092		-.123	-.064	-.096	.629	.780	.437	14
15	-.128		-.120	-.037	-.164	.660	.935	.545	15
16	-.121		-.120	-.017	-.203	.541	.815	.513	16
17	.139		.162	.146			.159	.125	17
18	.116		.158	.148			.163	.138	18
19	.113		.158	.155			.157	.097	19
20	.101		.119	.125			.122	.052	20
21	.006		.010	.046			.042	.014	21
22	.007		.005	.017				.004	22
23	.006			.013			.016	.002	23
24	.000		-.013	.009			.000	.000	24
25	.001		-.017	-.012			-.013	.126	25
26	-.050		-.055	-.041			-.041	.122	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=-20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.144		.151	.164			.156	.116	1
2	.105		.157	.157			.159	.100	2
3	.115		.153	.160			.153	.097	3
4	.105		.118	.133			.115	.056	4
5	.003		.011	.053			.047	.015	5
6	.003		.005	.018			.015	.001	6
7	.002	- .008	.011				.013	- .010	7
8 -	.009	- .005	.005				- .003	.001	8
9 -	.006	- .027	- .024				.007	.001	9
10 -	.038	- .047	- .042				.229	.097	10
11 -	.017	- .047	- .058				.293	.228	11
12 -	.081	- .083	- .110	.001	.240		.289	.287	12
13 -	.115	- .118	- .121	- .006	.349		.361	.360	13
14 -	.091	- .123	- .120	- .076	.358		.536	.371	14
15 -	.126	- .117	- .116	- .173	.308		.564	.303	15
16 -	.121	- .116	- .077	- .186	.269		.513	.268	16
17	.141		.161	.146			.159	.122	17
18	.119		.160	.151			.162	.135	18
19	.119		.159	.157			.156	.096	19
20	.102		.119	.125			.119	.047	20
21	.001		.012	.049			.044	.012	21
22	.008		.004	.021				.005	22
23	.008			.016			.016	.001	23
24	.002	- .009		.010			.001	- .011	24
25	.001	- .018	- .012				- .010	.006	25
26 -	.053	- .051	- .041				- .043	- .015	26

$\alpha=0$ $\delta=-10$

1	.145		.152	.164			.163	.118	1
2	.106		.160	.156			.166	.103	2
3	.122		.158	.161			.159	.098	3
4	.108		.122	.131			.119	.060	4
5	.005		.012	.045			.055	.017	5
6	.004		.005	.017			.024	.002	6
7	.005	- .007		.012			.019	- .006	7
8 -	.008	- .007		.005			.006	.000	8
9 -	.004	- .023	- .024				.004	- .012	9
10 -	.036	- .046	- .042				- .042	- .006	10
11 -	.015	- .046	- .057				- .007	- .017	11
12 -	.082	- .085	- .113	- .062	.102		.147	.152	12
13 -	.112	- .120	- .121	- .052	.135		.168	.156	13
14 -	.091	- .121	- .118	- .070	.072		.189	.095	14
15 -	.123	- .117	- .117	- .122	.050		.194	.066	15
16 -	.122	- .115	- .112	- .146	.026		.181	.041	16
17	.144		.161	.147			.164	.122	17
18	.116		.155	.154			.170	.137	18
19	.121		.157	.159			.161	.097	19
20	.102		.117	.123			.124	.052	20
21	.011		.014	.049			.047	.015	21
22	.008		.008	.024				.006	22
23	.009			.017			.023	.001	23
24	.002	- .011		.011			.008	- .012	24
25	.005	- .016	- .011				- .002	.005	25
26 -	.051	- .052	- .039				- .036	- .017	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.142		.156	.164			.161	.117	1
2	.115		.157	.162			.166	.098	2
3	.118		.157	.163			.159	.096	3
4	.108		.124	.133			.118	.056	4
5	.000		.009	.050			.056	.014	5
6	.002		.004	.020			.025	.002	6
7	.002	- .011		.015			.020	- .009	7
8	- .009	- .004		.010			.004	.001	8
9	- .003	- .024	-	.019			.001	- .015	9
10	- .038	- .042	-	.043			- .043	- .012	10
11	- .015	- .045	-	.057			- .047	- .032	11
12	- .082	- .082	-	.102	- .110	- .081	- .091	- .064	12
13	- .111	- .118	-	.115	- .106	- .105	- .136	- .078	13
14	- .090	- .120	-	.113	- .120	- .121	- .131	- .065	14
15	- .125	- .116	-	.116	- .125	- .122	- .135	- .060	15
16	- .120	- .116	-	.116	- .125	- .125	- .137	- .064	16
17	.146		.162	.146			.158	.116	17
18	.122		.158	.152			.167	.137	18
19	.122		.158	.156			.158	.095	19
20	.102		.118	.125			.118	.045	20
21	.007		.013	.044			.047	.011	21
22	.011		.003	.022				.004	22
23	.008			.015			.018	.000	23
24	.000	- .011		.011			.004	- .014	24
25	.003	- .018	-	.012			- .010	- .006	25
26	- .052	- .051	-	.040			- .040	- .017	26

$\alpha = 0$ $\delta = 10$

1	.140		.152	.163			.159	.122	1
2	.107		.154	.161			.165	.103	2
3	.116		.154	.162			.156	.098	3
4	.105		.116	.132			.113	.060	4
5	.002		.005	.048			.052	.015	5
6	- .003	- .001		.015			.023	.002	6
7	.003	- .019		.009			.019	- .011	7
8	- .009	- .007		.006			.003	- .001	8
9	- .004	- .031	-	.027			- .001	- .015	9
10	- .042	- .051	-	.043			- .048	- .011	10
11	- .020	- .051	-	.059			- .046	- .034	11
12	- .085	- .083	-	.112	- .126	- .240	- .239	- .213	12
13	- .111	- .120	-	.121	- .151	- .259	- .303	- .219	13
14	- .091	- .123	-	.121	- .178	- .258	- .294	- .158	14
15	- .125	- .118	-	.118	- .192	- .239	- .304	- .193	15
16	- .116	- .116	-	.121	- .189	- .274	- .309	- .309	16
17	.141		.155	.136			.154	.115	17
18	.115		.153	.148			.159	.133	18
19	.116		.150	.152			.152	.092	19
20	.099		.113	.119			.115	.047	20
21	- .003		.010	.042			.040	.015	21
22	- .002		.004	.019				.004	22
23	.003			.011			.014	- .001	23
24	- .005	- .017		.005			- .004	- .015	24
25	- .004	- .025	-	.015			- .012	.004	25
26	- .061	- .054	-	.049			- .043	- .017	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.139		.153	.162			.163	.127	1
2	.102		.156	.157			.166	.106	2
3	.121		.154	.160			.160	.097	3
4	.104		.120	.131			.121	.061	4
5	.006		.007	.046			.056	.015	5
6	.002		.004	.013			.025	.004	6
7	.004		-.010	.011			.025	-.006	7
8	-.010		-.007	.007			.009	.000	8
9	-.005		-.028	-.022			.008	-.012	9
10	-.041		-.049	-.045			-.044	-.007	10
11	-.017		-.050	-.058			-.037	-.026	11
12	-.083		-.081	-.107	-.135	-.364	-.368	-.320	12
13	-.113		-.117	-.120	-.162	-.380	-.414	-.259	13
14	-.091		-.121	-.117	-.196	-.373	-.394	-.333	14
15	-.122		-.116	-.117	-.212	-.392	-.313	-.449	15
16	-.120		-.115	-.121	-.214	-.430	-.299	-.471	16
17	.141		.155	.141			.156	.113	17
18	.113		.150	.148			.162	.135	18
19	.117		.152	.152			.155	.093	19
20	.097		.112	.115			.118	.047	20
21	.001		.008	.045			.047	.015	21
22	.003		-.001	.019				.007	22
23	.005			.009			.016	.002	23
24	-.001		-.014	.009			-.001	-.010	24
25	-.003		-.026	-.015			-.008	.007	25
26	-.056		-.055	-.044			.305	.209	26

$\alpha = 0$ $\delta = 30$

1	.139		.151	.159			.161	.118	1
2	.103		.157	.159			.165	.100	2
3	.117		.154	.161			.158	.096	3
4	.101		.121	.134			.121	.057	4
5	-.008		.010	.049			.055	.014	5
6	-.002		.002	.017			.022	-.001	6
7	.001		-.020	.006			.022	-.011	7
8	-.009		-.006	.006			.005	.059	8
9	-.007		-.027	-.019			.005	.128	9
10	-.039		-.047	-.042			-.044	.095	10
11	-.023		-.047	-.059			-.039	.029	11
12	-.087		-.083	-.113	-.133	-.427	-.388	-.344	12
13	-.115		-.122	-.126	-.159	-.425	-.389	-.312	13
14	-.093		-.125	-.125	-.196	-.350	-.368	-.411	14
15	-.128		-.121	-.122	-.211	-.416	-.365	-.455	15
16	-.125		-.118	-.125	-.208	-.391	-.373	-.460	16
17	.142		.157	.140			.152	.111	17
18	.112		.156	.150			.159	.131	18
19	.118		.153	.155			.152	.088	19
20	.098		.117	.119			.115	.046	20
21	-.003		.010	.045			.043	.011	21
22	.001		.003	.016				.001	22
23	.003			.009			.014	.234	23
24	-.002		-.017	.008			.308	.249	24
25	-.001		-.026	-.015			.362	.267	25
26	-.059		-.054	-.043			.387	.232	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=3$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.055		.054	.059			.053	.025	1
2	.036		.057	.060			.060	.042	2
3	.048		.052	.055			.057	.045	3
4	.034		.034	.034			.018	.021	4
5	-.059		-.052	-.041			-.032	-.021	5
6	-.056		-.067	-.065			-.064	-.027	6
7	-.056		-.065	-.072			-.061	-.051	7
8	-.067		-.068	-.072			-.077	-.050	8
9	-.065		-.084	-.095			-.073	-.065	9
10	-.091		-.104	-.109			-.107	-.074	10
11	-.080		-.104	-.125			-.097	-.097	11
12	-.141		-.142	-.173	-.172	-.143	-.147	-.123	12
13	-.168		-.177	-.186	-.168	-.166	-.182	-.142	13
14	-.150		-.182	-.182	-.178	-.172	-.168	-.151	14
15	-.179		-.177	-.183	-.178	-.178	-.172	-.179	15
16	-.168		-.172	-.183	-.179	-.176	-.171	-.198	16
17	.247		.295	.273			.285	.222	17
18	.200		.288	.273			.278	.222	18
19	.202		.272	.282			.285	.143	19
20	.182		.205	.237			.239	.088	20
21	.080		.087	.144			.157	.036	21
22	.084		.079	.097				.007	22
23	.083			.091			.110	-.006	23
24	.075		.057	.076			.088	-.022	24
25	.075		.049	.059			.074	.002	25
26	.012		.017	.027			.034	-.026	26

$\alpha=6$ $\delta=-27.5$

1	-.039		-.046	-.036			-.043	-.057	1
2	-.034		-.043	-.035			-.034	-.017	2
3	-.027		-.044	-.040			-.038	-.009	3
4	-.041		-.061	-.066			-.074	-.034	4
5	-.132		-.132	-.118			-.111	-.081	5
6	-.120		-.138	-.140			-.138	-.132	6
7	-.122		-.138	-.147			-.139	-.183	7
8	-.135		-.130	-.147			-.077	-.199	8
9	-.129		-.149	-.164			.167	-.206	9
10	-.153		-.161	-.180			.170	-.142	10
11	-.146		-.162	-.193			.185	-.004	11
12	-.194		-.198	-.237	-.120	.067	.159	.017	12
13	-.221		-.232	-.252	-.082	.083	.174	.250	13
14	-.201		-.234	-.224	-.196	.274	.358	.262	14
15	-.227		-.229	-.198	-.274	.300	.511	.336	15
16	-.219		-.226	-.166	-.305	.267	.511	.414	16
17	.344		.490	.486			.506	.371	17
18	.296		.430	.484			.507	.338	18
19	.303		.381	.445			.485	.248	19
20	.281		.307	.350			.393	.158	20
21	.158		.174	.233			.276	.077	21
22	.167		.158	.199				.034	22
23	.160			.182			.188	.005	23
24	.152		.147	.177			.164	-.020	24
25	.151		.138	.157			.144	.006	25
26	.082		.102	.116			.097	-.027	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -17.5$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.040		-.043	-.040			-.044	-.060	1
2	-.034		-.037	-.035			-.035	-.021	2
3	-.026		-.044	-.040			-.040	-.011	3
4	-.035		-.060	-.062			-.073	-.040	4
5	-.130		-.135	-.114			-.116	-.086	5
6	-.126		-.137	-.143			-.141	-.137	6
7	-.124		-.136	-.149			-.143	-.186	7
8	-.131		-.131	-.149			-.149	-.213	8
9	-.130		-.149	-.169			-.134	-.209	9
10	-.156		-.162	-.184			-.133	-.209	10
11	-.141		-.162	-.194			-.075	-.214	11
12	-.197		-.202	-.240	-.177	.005	-.087	-.050	12
13	-.222		-.232	-.252	-.189	.075	-.159	-.105	13
14	-.202		-.237	-.244	-.217	.064	-.243	-.092	14
15	-.227		-.231	-.245	-.257	.042	-.268	-.086	15
16	-.219		-.228	-.235	-.277	.035	-.252	-.012	16
17	.350		.491	.487			.501	.369	17
18	.298		.436	.479			.508	.334	18
19	.306		.380	.444			.484	.244	19
20	.275		.308	.347			.384	.158	20
21	.160		.179	.233			.278	.074	21
22	.167		.162	.194				.034	22
23	.159			.181			.189	.004	23
24	.159		.149	.177			.161	-.026	24
25	.157		.139	.153			.143	.004	25
26	.082		.103	.116			.099	-.029	26

$\alpha = 6$ $\delta = -7.5$

1	-.043		-.043	-.032			-.040	-.050	1
2	-.037		-.037	-.034			-.031	-.010	2
3	-.025		-.045	-.036			-.035	.000	3
4	-.038		-.062	-.057			-.067	-.029	4
5	-.130		-.132	-.116			-.111	-.074	5
6	-.126		-.135	-.139			-.136	-.121	6
7	-.121		-.139	-.143			-.136	-.173	7
8	-.129		-.133	-.145			-.145	-.202	8
9	-.125		-.149	-.167			-.132	-.201	9
10	-.150		-.159	-.174			-.156	-.206	10
11	-.141		-.159	-.191			-.132	-.222	11
12	-.186		-.192	-.234	-.214	-.126	-.077	-.168	12
13	-.212		-.223	-.243	-.198	-.115	-.071	-.150	13
14	-.193		-.229	-.237	-.208	-.150	-.056	-.226	14
15	-.219		-.223	-.237	-.206	-.155	-.049	-.214	15
16	-.211		-.219	-.232	-.204	-.147	-.045	-.176	16
17	.349		.491	.492			.505	.378	17
18	.301		.437	.483			.508	.344	18
19	.301		.385	.448			.485	.249	19
20	.275		.311	.358			.388	.166	20
21	.160		.175	.235			.281	.081	21
22	.167		.162	.199				.042	22
23	.163			.182			.194	.011	23
24	.157		.150	.178			.166	-.015	24
25	.157		.139	.155			.146	.011	25
26	.087		.100	.120			.103	-.020	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.038		-.044	-.032			-.040	-.050	1
2	-.030		-.038	-.030			-.033	-.014	2
3	-.023		-.045	-.037			-.036	-.001	3
4	-.038		-.057	-.054			-.069	-.025	4
5	-.125		-.126	-.111			-.113	-.074	5
6	-.118		-.129	-.137			-.135	-.120	6
7	-.117		-.134	-.147			-.141	-.171	7
8	-.126		-.126	-.148			-.145	-.198	8
9	-.124		-.148	-.167			-.136	-.196	9
10	-.148		-.158	-.184			-.160	-.207	10
11	-.139		-.158	-.193			-.143	-.223	11
12	-.187		-.189	-.232	-.237	-.243	-.232	-.262	12
13	-.212		-.224	-.244	-.240	-.262	-.268	-.289	13
14	-.193		-.228	-.238	-.250	-.254	-.253	-.257	14
15	-.216		-.223	-.239	-.252	-.262	-.258	-.272	15
16	-.209		-.218	-.235	-.248	-.234	-.258	-.283	16
17	.347		.494	.485			.497	.374	17
18	.303		.445	.481			.506	.338	18
19	.306		.390	.445			.482	.249	19
20	.282		.310	.355			.391	.164	20
21	.162		.181	.238			.275	.085	21
22	.171		.165	.197				.039	22
23	.164			.180			.192	.011	23
24	.160		.150	.177			.162	-.015	24
25	.161		.141	.156			.143	.011	25
26	.093		.098	.118			.092	-.022	26

α=6 δ=0

1	-.042		-.045	-.037			-.040	-.051	1
2	-.038		-.041	-.035			-.029	-.011	2
3	-.024		-.045	-.042			-.035	-.002	3
4	-.039		-.055	-.062			-.068	-.027	4
5	-.123		-.127	-.117			-.111	-.074	5
6	-.125		-.138	-.143			-.132	-.125	6
7	-.125		-.136	-.147			-.137	-.173	7
8	-.128		-.129	-.145			-.145	-.201	8
9	-.127		-.150	-.164			-.130	-.201	9
10	-.156		-.162	-.181			-.156	-.207	10
11	-.143		-.162	-.192			-.139	-.226	11
12	-.192		-.192	-.233	-.229	-.207	-.181	-.237	12
13	-.216		-.226	-.244	-.227	-.222	-.213	-.265	13
14	-.194		-.228	-.239	-.235	-.224	-.199	-.248	14
15	-.219		-.223	-.239	-.235	-.234	-.202	-.242	15
16	-.209		-.219	-.237	-.240	-.226	-.201	-.248	16
17	.345		.490	.492			.501	.374	17
18	.300		.433	.484			.505	.338	18
19	.302		.380	.447			.483	.249	19
20	.274		.308	.353			.390	.162	20
21	.159		.179	.240			.279	.083	21
22	.169		.158	.200				.037	22
23	.163			.183			.193	.010	23
24	.154		.148	.177			.168	-.016	24
25	.154		.137	.158			.139	.009	25
26	.086		.100	.121			.096	-.021	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=6 δ=12.5

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.037		-.040	-.035			-.040	-.040	1
2	-.034		-.037	-.033			-.029	-.002	2
3	-.022		-.041	-.035			-.034	.006	3
4	-.035		-.060	-.055			-.068	-.021	4
5	-.122		-.130	-.111			-.115	-.067	5
6	-.124		-.136	-.138			-.136	-.112	6
7	-.122		-.134	-.145			-.139	-.163	7
8	-.127		-.125	-.151			-.146	-.192	8
9	-.123		-.145	-.165			-.133	-.188	9
10	-.152		-.159	-.180			-.159	-.193	10
11	-.156		-.160	-.194			-.139	-.213	11
12	-.187		-.187	-.226	-.249	-.358	-.341	-.350	12
13	-.208		-.221	-.239	-.270	-.375	-.392	-.349	13
14	-.187		-.224	-.234	-.288	-.375	-.384	-.381	14
15	-.214		-.218	-.235	-.292	-.338	-.385	-.400	15
16	-.207		-.216	-.232	-.265	-.420	-.248	-.401	16
17	.350		.490	.488			.497	.380	17
18	.301		.440	.482			.501	.339	18
19	.302		.382	.443			.481	.253	19
20	.278		.312	.351			.384	.171	20
21	.160		.181	.236			.276	.091	21
22	.171		.160	.196				.047	22
23	.164			.179			.183	.016	23
24	.159		.149	.174			.165	-.011	24
25	.155		.140	.151			.138	.015	25
26	.086		.098	.113			.092	-.016	26

α=6 δ=22.5

1	-.039		-.040	-.035			-.035	-.056	1
2	-.034		-.035	-.032			-.027	-.020	2
3	-.023		-.039	-.034			-.033	-.010	3
4	-.038		-.055	-.057			-.065	-.032	4
5	-.118		-.132	-.114			-.110	-.080	5
6	-.124		-.133	-.138			-.132	-.127	6
7	-.122		-.132	-.139			-.135	-.172	7
8	-.132		-.128	-.142			-.140	-.204	8
9	-.126		-.148	-.163			-.129	-.199	9
10	-.151		-.158	-.173			-.149	-.132	10
11	-.139		-.158	-.187			-.132	-.082	11
12	-.194		-.199	-.237	-.250	-.430	-.429	-.415	12
13	-.221		-.229	-.252	-.275	-.435	-.462	-.426	13
14	-.202		-.237	-.245	-.295	-.345	-.429	-.451	14
15	-.226		-.231	-.245	-.297	-.437	-.368	-.454	15
16	-.218		-.227	-.239	-.248	-.461	-.356	-.426	16
17	.350		.491	.487			.498	.361	17
18	.300		.441	.481			.505	.326	18
19	.300		.380	.444			.480	.242	19
20	.275		.309	.350			.388	.155	20
21	.162		.174	.238			.276	.076	21
22	.168		.158	.199				.030	22
23	.162			.185			.194	.001	23
24	.159		.147	.176			.164	-.019	24
25	.152		.140	.156			.414	.265	25
26	.080		.104	.117			.564	.289	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=6 δ=32.5

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.039		-.041	-.033			-.038	-.039	1
2	-.031		-.039	-.031			-.028	-.002	2
3	-.024		-.042	-.035			-.034	.016	3
4	-.033		-.057	-.056			-.066	-.014	4
5	-.118		-.130	-.109			-.111	-.062	5
6	-.119		-.131	-.140			-.135	-.116	6
7	-.119		-.133	-.144			-.139	-.098	7
8	-.131		-.130	-.146			-.146	-.020	8
9	-.125		-.148	-.165			-.130	-.091	9
10	-.154		-.159	-.178			-.155	-.168	10
11	-.138		-.160	-.192			-.140	-.227	11
12	-.177		-.173	-.211	-.226	-.414	-.446	-.451	12
13	-.203		-.207	-.233	-.248	-.421	-.447	-.449	13
14	-.177		-.221	-.221	-.270	-.370	-.407	-.461	14
15	-.206		-.212	-.221	-.259	-.462	-.389	-.425	15
16	-.206		-.198	-.221	-.223	-.439	-.374	-.388	16
17	.343		.486	.485			.495	.379	17
18	.301		.439	.477			.499	.340	18
19	.306		.379	.441			.480	.260	19
20	.277		.310	.352			.380	.173	20
21	.163		.181	.229			.274	.095	21
22	.171		.161	.194				.051	22
23	.164			.177			.538	.338	23
24	.158		.149	.175			.629	.308	24
25	.159		.139	.149			.637	.354	25
26	.089		.103	.116			.624	.293	26

α=9 δ=0

1	-.110		-.113	-.107			-.116	-.116	1
2	-.096		-.109	-.105			-.105	-.050	2
3			-.112	-.107			-.111	-.066	3
4	-.093		-.126	-.129			-.139	-.102	4
5	-.167		-.194	-.182			-.174	-.159	5
6	-.171		-.188	-.198			-.201	-.240	6
7	-.171		-.187	-.203			-.199	-.290	7
8	-.176		-.180	-.204			-.203	-.278	8
9	-.171		-.194	-.220			-.184	-.293	9
10	-.194		-.205	-.242			-.205	-.257	10
11	-.186		-.205	-.246			-.175	-.277	11
12	-.217		-.221	-.270	-.263	-.260	-.224	-.307	12
13	-.260		-.257	-.280	-.263	-.274	-.267	-.340	13
14	-.221		-.257	-.280	-.272	-.274	-.247	-.316	14
15	-.254		-.257	-.280	-.272	-.274	-.244	-.316	15
16	-.233		-.257	-.280	-.268	-.264	-.244	-.304	16
17	.463		.684	.744			.784	.586	17
18	.400		.554	.638			.704	.467	18
19	.409		.501	.574			.618	.334	19
20	.371		.422	.455			.483	.223	20
21	.249		.260	.330			.352	.122	21
22	.257		.249	.278				.075	22
23	.246			.264			.259	.042	23
24	.244		.240	.258			.233	.007	24
25	.239		.229	.235			.215	.066	25
26	.155		.183	.193			.166	.024	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.187		-.218	-.229			-.240	-.253	1
2	-.153		-.188	-.188			-.201	-.145	2
3	-.141		-.193	-.192			-.188	-.162	3
4	-.150		-.204	-.203			-.208	-.217	4
5	-.227		-.257	-.247			-.238	-.268	5
6	-.211		-.262	-.261			-.263	-.345	6
7	-.221		-.259	-.262			-.261	-.373	7
8	-.225		-.241	-.267			-.265	-.353	8
9	-.219		-.246	-.273			-.124	-.373	9
10	-.239		-.251	-.292			-.028	-.359	10
11	-.235		-.251	-.299			.004	-.303	11
12	-.253		-.265	-.312	-.224	-.082	-.006	-.212	12
13	-.292		-.290	-.330	-.197	-.076	.022	-.098	13
14	-.269		-.299	-.319	-.280	.060	.244	-.112	14
15	-.293		-.299	-.299	-.344	.107	.351	-.201	15
16	-.248		-.212	-.189	-.368	.085	.351	-.268	16
17	.611		.878	.952			.982	.724	17
18	.537		.711	.816			.871	.572	18
19	.554		.642	.714			.751	.430	19
20	.505		.514	.553			.598	.313	20
21	.350		.345	.413			.449	.181	21
22	.365		.346	.383				.126	22
23	.345			.376			.354	.102	23
24	.342		.345	.365			.329	.061	24
25	.333		.331	.342			.305	.103	25
26	.251		.279	.294			.253	.054	26

α=12 δ=-15

1	-.190		-.220	-.232			-.251	-.248	1
2	-.155		-.190	-.197			-.208	-.143	2
3	-.141		-.191	-.187			-.188	-.157	3
4	-.153		-.206	-.204			-.213	-.213	4
5	-.222		-.260	-.248			-.240	-.269	5
6	-.221		-.266	-.262			-.263	-.350	6
7	-.220		-.260	-.266			-.261	-.385	7
8	-.230		-.241	-.266			-.273	-.369	8
9	-.219		-.246	-.279			-.242	-.383	9
10	-.239		-.254	-.291			-.242	-.375	10
11	-.237		-.254	-.304			-.072	-.350	11
12	-.262		-.268	-.310	-.277	-.141	-.066	-.257	12
13	-.293		-.293	-.331	-.277	-.107	-.029	-.224	13
14	-.263		-.293	-.328	-.305	-.105	.034	-.245	14
15	-.292		-.292	-.328	-.308	-.120	.055	-.299	15
16	-.239		-.224	-.263	-.373	-.120	.055	-.320	16
17	.615		.878	.953			.976	.723	17
18	.536		.715	.814			.870	.582	18
19	.550		.647	.719			.749	.430	19
20	.502		.515	.555			.593	.316	20
21	.346		.350	.415			.447	.182	21
22	.360		.350	.384				.126	22
23	.342			.376			.349	.098	23
24	.344		.344	.368			.325	.069	24
25	.333		.333	.344			.304	.105	25
26	.248		.272	.301			.247	.052	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = -5$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.192		-.214	-.227			-.242	-.249	1
2	-.152		-.184	-.193			-.207	-.161	2
3	-.137		-.188	-.188			-.189	-.159	3
4	-.148		-.198	-.203			-.212	-.221	4
5	-.219		-.259	-.249			-.245	-.274	5
6	-.215		-.258	-.263			-.268	-.350	6
7	-.217		-.254	-.262			-.266	-.388	7
8	-.224		-.242	-.264			-.268	-.373	8
9	-.215		-.246	-.284			-.247	-.378	9
10	-.235		-.246	-.291			-.259	-.371	10
11	-.233		-.247	-.300			-.206	-.365	11
12	-.262		-.263	-.318	-.318	-.244	-.208	-.326	12
13	-.289		-.287	-.333	-.297	-.255	-.211	-.326	13
14	-.267		-.295	-.328	-.297	-.269	-.191	-.346	14
15	-.285		-.293	-.330	-.297	-.270	-.191	-.336	15
16	-.243		-.228	-.280	-.272	-.249	-.191	-.313	16
17	.616		.878	.951			.974	.715	17
18	.540		.720	.813			.861	.573	18
19	.549		.648	.715			.745	.425	19
20	.505		.513	.551			.595	.320	20
21	.356		.355	.409			.442	.178	21
22	.365		.354	.379				.126	22
23	.349			.376			.350	.097	23
24	.347		.345	.364			.317	.062	24
25	.339		.334	.342			.300	.097	25
26	.248		.282	.296			.247	.049	26

$\alpha = 12$ $\delta = 0$

1	-.192		-.216	-.234			-.240	-.239	1
2	-.149		-.187	-.197			-.203	-.136	2
3	-.142		-.192	-.190			-.185	-.152	3
4	-.155		-.202	-.203			-.209	-.213	4
5	-.218		-.262	-.245			-.242	-.255	5
6	-.217		-.262	-.263			-.261	-.341	6
7	-.218		-.259	-.262			-.262	-.376	7
8	-.223		-.244	-.267			-.269	-.370	8
9	-.217		-.246	-.280			-.243	-.371	9
10	-.239		-.249	-.291			-.254	-.370	10
11	-.237		-.249	-.300			-.213	-.366	11
12	-.257		-.264	-.310	-.305	-.284	-.265	-.353	12
13	-.280		-.288	-.328	-.299	-.312	-.297	-.366	13
14	-.262		-.300	-.323	-.320	-.300	-.267	-.349	14
15	-.289		-.300	-.326	-.312	-.314	-.279	-.348	15
16	-.232		-.222	-.295	-.300	-.214	-.279	-.329	16
17	.611		.876	.948			.977	.728	17
18	.536		.715	.810			.868	.573	18
19	.549		.641	.718			.749	.431	19
20	.502		.514	.552			.590	.313	20
21	.352		.349	.413			.445	.189	21
22	.365		.349	.382				.123	22
23	.347			.375			.351	.100	23
24	.344		.343	.363			.322	.071	24
25	.338		.333	.343			.299	.105	25
26	.253		.282	.291			.249	.055	26

TABLE II.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=15

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.186		-.219	-.229			-.240	-.250	1
2	-.151		-.191	-.194			-.207	-.151	2
3	-.141		-.191	-.187			-.189	-.162	3
4	-.148		-.209	-.203			-.210	-.223	4
5	-.219		-.261	-.243			-.240	-.279	5
6	-.216		-.262	-.261			-.265	-.346	6
7	-.222		-.259	-.263			-.266	-.390	7
8	-.226		-.244	-.267				-.374	8
9	-.223		-.251	-.279			-.243	-.391	9
10	-.241		-.247	-.290			-.259	-.374	10
11	-.233		-.248	-.302			-.218	-.365	11
12	-.263		-.264	-.313	-.312	-.388	-.376	-.399	12
13	-.297		-.294	-.335	-.333	-.407	-.415	-.405	13
14	-.265		-.310	-.328	-.349	-.330	-.374	-.425	14
15	-.292		-.294	-.329	-.307	-.310	-.349	-.420	15
16	-.249		-.218	-.263	-.289	-.379	-.314	-.401	16
17	.610		.875	.944			.971	.709	17
18	.534		.714	.808			.864	.562	18
19	.550		.644	.708			.747	.417	19
20	.500		.511	.550			.589	.305	20
21	.348		.344	.408			.447	.178	21
22	.363		.347	.378				.118	22
23	.344			.372			.345	.086	23
24	.345		.343	.357			.321	.047	24
25	.335		.331	.338			.285	.091	25
26	.249		.276	.292			.378	.177	26

α=12 δ=25

1	-.191		-.217	-.228			-.237	-.243	1
2	-.153		-.190	-.192			-.201	-.147	2
3	-.138		-.193	-.187			-.188	-.157	3
4	-.152		-.201	-.203			-.212	-.206	4
5	-.225		-.260	-.242			-.241	-.269	5
6	-.219		-.262	-.261			-.262	-.346	6
7	-.220		-.258	-.267			-.267	-.376	7
8	-.225		-.241	-.265			-.268	-.358	8
9	-.218		-.246	-.282			-.244	-.346	9
10	-.240		-.248	-.293			-.253	-.318	10
11	-.237		-.248	-.307			-.222	-.330	11
12	-.255		-.259	-.304	-.320	-.452	-.439	-.455	12
13	-.289		-.285	-.326	-.351	-.440	-.466	-.459	13
14	-.262		-.297	-.321	-.350	-.353	-.429	-.471	14
15	-.287		-.289	-.318	-.329	-.440	-.365	-.471	15
16	-.239		-.191	-.234	-.307	-.416	-.365	-.416	16
17	.611		.877	.944			.969	.710	17
18	.539		.715	.808			.862	.567	18
19	.548		.646	.712			.742	.426	19
20	.502		.513	.551			.582	.321	20
21	.351		.351	.408			.445	.184	21
22	.362		.349	.379				.128	22
23	.342			.370			.346	.103	23
24	.345		.344	.358			.505	.316	24
25	.338		.332	.337			.757	.437	25
26	.255		.280	.290			.802	.444	26

TABLE II.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 1.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=35

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.189		-.215	-.223			-.240	-.257	1
2	-.150		-.189	-.193			-.206	-.146	2
3	-.141		-.193	-.188			-.185	-.159	3
4	-.149		-.200	-.196			-.210	-.218	4
5	-.224		-.262	-.243			-.243	-.270	5
6	-.218		-.260	-.260			-.264	-.368	6
7	-.221		-.261	-.270			-.265	-.363	7
8	-.225		-.240	-.268				-.349	8
9	-.219		-.244	-.284			-.246	-.344	9
10	-.240		-.248	-.293			-.254	-.344	10
11	-.234		-.248	-.304			-.225	-.353	11
12	-.259		-.267	-.310	-.321	-.445	-.424	-.482	12
13	-.288		-.289	-.328	-.336	-.445	-.432	-.483	13
14	-.273		-.305	-.328	-.356	-.445	-.420	-.485	14
15	-.283		-.305	-.328	-.343	-.444	-.425	-.424	15
16	-.237		-.151	-.277	-.308	-.424	-.422	-.414	16
17	.605		.876	.938			.969	.714	17
18	.537		.716	.802			.859	.558	18
19	.546		.644	.704			.744	.410	19
20	.500		.514	.548			.585	.304	20
21	.353		.351	.408			.437	.166	21
22	.364		.351	.374				.133	22
23	.344			.371			.852	.467	23
24	.343		.345	.356			.896	.457	24
25	.338		.332	.357			.911	.535	25
26	.250		.277	.436			.880	.492	26

α=15 δ=0

1	-.243		-.311	-.333			-.357	-.359	1
2	-.195		-.256	-.262			-.288	-.262	2
3	-.179		-.245	-.252			-.258	-.253	3
4	-.191		-.256	-.260			-.268	-.303	4
5	-.260		-.305	-.295			-.290	-.346	5
6	-.244		-.307	-.307			-.309	-.402	6
7	-.253		-.305	-.307			-.308	-.431	7
8	-.261		-.290	-.308			-.320	-.401	8
9	-.253		-.288	-.317			-.295	-.426	9
10	-.273		-.279	-.331			-.298	-.411	10
11	-.271		-.279	-.338			-.244	-.397	11
12	-.282		-.299	-.345	-.350	-.331	-.307	-.424	12
13	-.325		-.326	-.378	-.345	-.354	-.339	-.414	13
14	-.299		-.334	-.364	-.363	-.340	-.313	-.425	14
15	-.323		-.324	-.368	-.360	-.343	-.324	-.397	15
16	-.193		-.182	-.242	-.280	-.213	-.299	-.401	16
17	.753		1.028	1.064			1.077	.795	17
18	.674		.845	.919			.960	.644	18
19	.698		.753	.809			.830	.478	19
20	.585		.591	.632			.668	.369	20
21	.440		.431	.486			.516	.232	21
22	.475		.471	.498				.187	22
23	.472			.514			.449	.158	23
24	.487		.498	.504			.425	.115	24
25	.471		.471	.480			.404	.169	25
26	.375		.397	.404			.347	.092	26

TABLE III

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -15$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.761		1.036	1.081			1.058	.846	1
2	.686		.859	.923			.955	.652	2
3	.717		.761	.819			.826	.517	3
4	.634		.606	.653			.666	.364	4
5	.449		.432	.506			.525	.246	5
6	.481		.486	.507			.476	.164	6
7	.482		.493	.517			.458	.144	7
8	.486		.510	.510			.461		8
9	.468		.473	.440			.334	.119	9
10	.403		.392	.418			.327	.128	10
11	.403		.392	.348			.282	.093	11
12	.289	.254	.311	.293	.303	.298	.286	.040	12
13	.279	.281	.300	.279	.285	.271	.231	.041	13
14	.289	.281	.290	.273	.255	.259	.224	.004	14
15	.298	.283	.291	.283	.263	.243	.228	.005	15
16	.291	.270	.291	.275	.245	.243	.214	- .013	16
17	- .250		- .323	- .359			- .365	- .319	17
18	- .176		- .261	- .292			- .286	- .206	18
19	- .183		- .253	- .268			- .271	- .236	19
20	- .197		- .252	- .276			- .280	- .261	20
21	- .250		- .308	- .308			- .304	- .317	21
22	- .239		- .318	- .325				- .374	22
23	- .252			- .330			- .315	- .388	23
24	- .258		- .299	- .330			- .325	- .400	24
25	- .255		- .287	- .335			- .313	- .385	25
26	- .279		- .303	- .331			- .301	- .398	26

$\alpha = -12$ $\delta = -30$

1	.593		.858	.937			.950	.756	1
2	.519		.712	.802			.849	.577	2
3	.536		.640	.709			.739	.452	3
4	.501		.521	.548			.572	.300	4
5	.348		.344	.397			.439	.191	5
6	.353		.331	.363			.372	.104	6
7	.339		.504	.819			.523	.076	7
8	.325		.739	.882			.527		8
9	.321		.782	.849			.541	.146	9
10	.444		.768	.913			.495	.156	10
11	.564		.768	.914			.425	.124	11
12	.649	.599	.754	.953	.802	.544	.468	.096	12
13	.669	.559	.809	.960	.821	.579	.460	.130	13
14	.654	.254	1.117	1.175	.976	.194	.434	.094	14
15	.592	.069	1.006	1.113	.817	.068	.373	.120	15
16	.459	.003	.793	.888	.666	- .106	.305	.111	16
17	- .192		- .233	- .247			- .251	- .215	17
18	- .143		- .202	- .200			- .204	- .098	18
19	- .143		- .197	- .195			- .192	- .138	19
20	- .166		- .206	- .207			- .205	- .180	20
21	- .220		- .269	- .252			- .247	- .244	21
22	- .212		- .269	- .262				- .313	22
23	- .225			- .270			- .263	- .334	23
24	- .225		- .255	- .273			- .274	- .357	24
25	- .229		- .251	- .280			- .261	- .335	25
26	- .252		- .271	- .296			- .264	- .358	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.604		.858	.944			.950	.754	1
2	.519		.713	.804			.854	.574	2
3	.541		.642	.709			.736	.445	3
4	.502		.517	.554			.578	.295	4
5	.340		.347	.405			.437	.186	5
6	.343		.336	.372			.374	.101	6
7	.341		.348	.377			.345	.074	7
8	.325		.349	.428			.334		8
9	.310		.428	.742			.253	.049	9
10	.249		.670	.794			.234	.065	10
11	.273		.670	.810			.263	.026	11
12	.171	.444	.722	.832	.732	.539	.317 -	.003	12
13	.175	.484	.796	.877	.737	.444	.328	.006	13
14	.268	.241	.816	.980	.743	.315	.368 -	.016	14
15	.505	.036	.707	.877	.615	.084	.350 -	.019	15
16	.447	- .006	.574	.719	.512	- .019	.305 -	.015	16
17	- .191		- .221	- .242			- .250 -	.218	17
18	- .149		- .197	- .206			- .205 -	.101	18
19	- .145		- .198	- .194			- .197 -	.143	19
20	- .163		- .207	- .210			- .213 -	.184	20
21	- .219		- .262	- .247			- .249 -	.249	21
22	- .212		- .269	- .264			-	.313	22
23	- .222			- .265			- .267 -	.337	23
24	- .225		- .248	- .272			- .271 -	.362	24
25	- .234		- .244	- .281			- .262 -	.343	25
26	- .251		- .264	- .298			- .262 -	.363	26

$\alpha = -12$ $\delta = -10$

1	.597		.864	.942			.950	.758	1
2	.513		.718	.802			.851	.585	2
3	.545		.638	.714			.741	.452	3
4	.507		.527	.555			.574	.306	4
5	.349		.347	.404			.447	.189	5
6	.351		.340	.373			.371	.108	6
7	.343		.338	.365			.346	.080	7
8	.328		.345	.357			.328		8
9	.318		.324	.455			.253	.058	9
10	.255		.261	.309			.221	.061	10
11	.279		.261	.488			.195	.028	11
12	.180	.309	.662	.682	.513	.348	.204 -	.016	12
13	.179	.329	.623	.729	.537	.328	.143 -	.011	13
14	.180	.323	.510	.678	.454	.306	.149 -	.035	14
15	.181	.101	.470	.599	.389	.164	.211 -	.044	15
16	.276	.049	.400	.518	.323	.081	.228 -	.066	16
17	- .184		- .230	- .247			- .253 -	.214	17
18	- .144		- .195	- .206			- .211 -	.096	18
19	- .142		- .198	- .198			- .194 -	.145	19
20	- .160		- .205	- .211			- .208 -	.184	20
21	- .222		- .265	- .248			- .247 -	.244	21
22	- .212		- .269	- .271			-	.313	22
23	- .219			- .273			- .265 -	.335	23
24	- .222		- .248	- .277			- .270 -	.358	24
25	- .226		- .248	- .279			- .260 -	.340	25
26	- .248		- .269	- .297			- .261 -	.360	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.597		.864	.947			.948	.756	1
2	.521		.710	.809			.854	.577	2
3	.544		.644	.716			.743	.448	3
4	.508		.523	.558			.578	.301	4
5	.345		.349	.413			.444	.190	5
6	.354		.341	.380			.375	.108	6
7	.343		.341	.370			.344	.076	7
8	.328		.344	.364			.332		8
9	.310		.313	.339			.256	.053	9
10	.251		.260	.288			.221	.058	10
11	.280		.260	.263			.189	.029	11
12	.176	.163	.201	.189	.208	.195	.198	.009	12
13	.171	.178	.188	.171	.191	.184	.140	.009	13
14	.178	.181	.174	.165	.164	.164	.133	.034	14
15	.169	.179	.181	.178	.156	.155	.130	.043	15
16	.178	.166	.176	.174	.154	.140	.114	.068	16
17	.190		.221	.259			.255	.221	17
18	.140		.195	.204			.210	.106	18
19	.143		.195	.194			.192	.144	19
20	.162		.204	.205			.212	.184	20
21	.213		.258	.247			.252	.253	21
22	.218		.263	.269				.318	22
23	.218			.272			.265	.340	23
24	.221		.248	.273			.274	.364	24
25	.230		.242	.284			.262	.348	25
26	.253		.263	.299			.264	.367	26

$\alpha = -12$ $\delta = 10$

1	.602		.859	.940			.952	.757	1
2	.517		.712	.802			.861	.580	2
3	.534		.635	.715			.750	.449	3
4	.498		.529	.552			.583	.300	4
5	.336		.341	.400			.445	.188	5
6	.351		.337	.368			.372	.100	6
7	.338		.336	.377			.348	.075	7
8	.325		.342	.365			.338		8
9	.310		.320	.333			.257	.049	9
10	.240		.251	.300			.223	.061	10
11	.271		.250	.255			.195	.028	11
12	.176	.146	.050	.041	.030	.190	.200	.016	12
13	.175	.100	.069	.086	.024	.141	.140	.011	13
14	.178	.069	.020	.076	.010	.071	.130	.039	14
15	.169	.035	.016	.089	.058	.053	.130	.045	15
16	.170	.010	.073	.076	.110	.028	.105	.070	16
17	.198		.226	.252			.261	.226	17
18	.141		.200	.197			.212	.106	18
19	.140		.199	.195			.191	.148	19
20	.165		.210	.211			.210	.190	20
21	.218		.264	.250			.260	.254	21
22	.221		.273	.276				.322	22
23	.224			.278			.267	.344	23
24	.230		.253	.276			.270	.367	24
25	.227		.255	.281			.259	.348	25
26	.256		.270	.295			.265	.368	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.604		.867	.947			.946	.756	1
2	.526		.712	.800			.862	.577	2
3	.545		.639	.716			.745	.448	3
4	.517		.520	.559			.581	.299	4
5	.351		.342	.409			.450	.190	5
6	.350		.339	.374			.373	.101	6
7	.348		.336	.377			.350	.075	7
8	.331		.346	.373			.337		8
9	.318		.322	.333			.251	.054	9
10	.254		.260	.300			.221	.059	10
11	.275		.260	.261			.199	.025	11
12	.179	.159	-.236	-.214	-.219	.195	.199	-.015	12
13	.176	.078	-.260	-.268	-.209	.125	.144	-.009	13
14	.175	.025	-.213	-.254	-.200	.021	.139	-.034	14
15	.170	-.019	-.219	-.274	-.245	-.001	.129	-.045	15
16	.171	-.040	-.243	-.260	-.240	-.025	.104	-.069	16
17	-.194		-.230	-.247			-.260	-.238	17
18	-.150		-.199	-.204			-.212	-.111	18
19	-.145		-.201	-.197			-.197	-.149	19
20	-.165		-.212	-.212			-.216	-.191	20
21	-.225		-.273	-.251			-.260	-.255	21
22	-.216		-.274	-.263				-.324	22
23	-.220			-.271			-.274	-.344	23
24	-.221		-.253	-.273			-.275	-.372	24
25	-.229		-.253	-.278			-.264	-.349	25
26	-.248		-.273	-.295			-.264	-.369	26

$\alpha = -12$ $\delta = 30$

1	.601		.864	.954			.950	.757	1
2	.526		.716	.809			.859	.583	2
3	.544		.643	.717			.749	.448	3
4	.505		.526	.561			.572	.303	4
5	.338		.351	.415			.450	.190	5
6	.349		.344	.377			.376	.106	6
7	.348		.338	.369			.342	.076	7
8	.327		.352	.365			.326		8
9	.316		.321	.327			.252	.049	9
10	.251		.254	.303			.221	.064	10
11	.275		.255	.258			.193	.029	11
12	.176	.163	-.354	-.334	-.339	.191	.204	-.008	12
13	.180	.075	-.380	-.383	-.339	.125	.145	-.009	13
14	.184	.018	-.347	-.375	-.330	.013	.140	-.035	14
15	.174	-.021	-.345	-.383	-.362	-.011	.129	-.046	15
16	.175	-.041	-.373	-.374	-.369	-.031	.104	-.068	16
17	-.193		-.224	-.260			-.270	-.229	17
18	-.146		-.201	-.219			-.222	-.116	18
19	-.145		-.194	-.205			-.209	-.154	19
20	-.166		-.206	-.220			-.222	-.193	20
21	-.224		-.255	-.262			-.263	-.258	21
22	-.225		-.265	-.273				-.325	22
23	-.221			-.276			-.281	-.353	23
24	-.226		-.250	-.278			-.286	-.374	24
25	-.221		-.077	-.077			-.276	-.350	25
26	-.254		-.045	-.048			-.277	-.369	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-9$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.465		.679	.757			.781	.632	1
2	.395		.560	.645			.709	.469	2
3	.407		.504	.583			.630	.368	3
4	.388		.416	.454			.481	.226	4
5	.246		.258	.322			.360	.130	5
6	.248		.247	.275			.289	.064	6
7	.245		.229	.272			.260	.026	7
8	.231		.244	.265			.237		8
9	.228		.220	.210			.183	.008	9
10	.171		.169	.212			.131	.021	10
11	.197		.169	.172			.117	- .010	11
12	.098	.094	.126	.128	.136	.119	.135	- .050	12
13	.108	.104	.114	.096	.123	.109	.076	- .040	13
14	.121	.103	.096	.106	.096	.089	.066	- .074	14
15	.083	.100	.111	.101	.086	.075	.064	- .066	15
16	.093	.095	.104	.106	.081	.069	.048	- .085	16
17	- .120		- .129	- .133			- .127	- .083	17
18	- .065		- .128	- .127			- .104	.004	18
19	- .080		- .123	- .122			- .117	- .043	19
20	- .107		- .138	- .142			- .143	- .088	20
21	- .173		- .208	- .185			- .195	- .143	21
22	- .173		- .200	- .204				- .206	22
23	- .175			- .211			- .205	- .244	23
24	- .176		- .201	- .211			- .208	- .270	24
25	- .178		- .203	- .219			- .202	- .245	25
26	- .208		- .222	- .221			- .212	- .274	26

$\alpha=-6$ $\delta=-30$

1	.349		.489	.508			.495	.404	1
2	.291		.438	.496			.503	.322	2
3	.302		.391	.455			.490	.273	3
4	.283		.313	.368			.385	.168	4
5	.162		.185	.235			.284	.094	5
6	.167		.162	.187			.233	.034	6
7	.166		.147	.538			.191	- .004	7
8	.153		.394	.604			.174		8
9	.150		.515	.622			.158	- .020	9
10	.096		.499	.617			.227	- .009	10
11	.131		.499	.617			.214	- .034	11
12	.030	.309	.474	.659	.500	.299	.226	- .065	12
13	.050	.248	.517	.632	.484	.357	.206	- .036	13
14	.215	.025	.847	.881	.761	.098	.188	- .091	14
15	.304	- .093	.861	1.026	.798	- .024	.160	- .076	15
16	.304	- .145	.666	.854	.647	- .100	.149	- .075	16
17	- .051		- .045	- .052			- .038	- .026	17
18	- .028		- .050	- .050			- .031	.028	18
19	- .028		- .055	- .038			- .034	.010	19
20	- .056		- .065	- .067			- .061	- .028	20
21	- .128		- .132	- .115			- .119	- .063	21
22	- .126		- .143	- .133				- .094	22
23	- .129			- .143			- .138	- .143	23
24	- .129		- .142	- .142			- .143	- .181	24
25	- .130		- .149	- .157			- .145	- .155	25
26	- .172		- .171	- .170			- .157	- .193	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.341		.485	.508			.491	.434	1
2	.280		.430	.498			.502	.343	2
3	.300		.382	.456			.484	.295	3
4	.286		.314	.368			.388	.200	4
5	.150		.183	.235			.279	.118	5
6	.163		.162	.194			.225	.053	6
7	.157		.149	.195			.191	.016	7
8	.146		.160	.191			.163		8
9	.142		.169	.495			.128	.004	9
10	.087		.375	.522			.082	.011	10
11	.121		.375	.539			.071 -	.015	11
12	.041	.218	.483	.560	.470	.296	.088 -	.064	12
13	.039	.226	.572	.609	.504	.216	.030 -	.045	13
14	.066	.066	.628	.778	.557	.143	.054 -	.094	14
15	.046 -	.091	.565	.774	.488 -	.023	.120 -	.071	15
16	.150 -	.126	.469	.654	.423 -	.085	.124 -	.081	16
17 -	.050	- .043	- .056			-	.039 -	.004	17
18 -	.034	- .046	- .057			-	.035	.040	18
19 -	.032	- .048	- .046			-	.039	.025	19
20 -	.054	- .060	- .068			-	.066 -	.011	20
21 -	.125	- .138	- .122			-	.120 -	.044	21
22 -	.121	- .143	- .139				-	.074	22
23 -	.128		- .143			-	.143 -	.120	23
24 -	.139	- .144	- .144			-	.153 -	.166	24
25 -	.133	- .151	- .155			-	.151 -	.134	25
26 -	.167	- .174	- .170			-	.157 -	.173	26

α=-6 δ=-10

1	.363		.499	.512			.494	.427	1
2	.300		.448	.501			.502	.332	2
3	.311		.396	.461			.487	.285	3
4	.294		.330	.373			.383	.184	4
5	.169		.188	.241			.285	.105	5
6	.172		.170	.198			.224	.030	6
7	.169		.156	.186			.191 -	.001	7
8	.154		.169	.176			.161		8
9	.154		.148	.304			.125 -	.005	9
10	.099		.107	.119			.073	.001	10
11	.135		.107	.128			.066 -	.025	11
12	.033	.100	.393	.330	.289	.143	.073 -	.059	12
13	.038	.124	.358	.395	.324	.143	.020 -	.051	13
14	.058	.111	.290	.415	.246	.113 -	.008 -	.093	14
15	.009 -	.028	.265	.402	.216	.014	.009 -	.065	15
16	.043 -	.081	.233	.353	.169 -	.048	.020 -	.083	16
17 -	.037	- .040	- .052			-	.045 -	.011	17
18 -	.025	- .045	- .049			-	.037	.030	18
19 -	.020	- .046	- .043			-	.045	.019	19
20 -	.041	- .060	- .072			-	.072 -	.019	20
21 -	.125	- .128	- .120			-	.126 -	.048	21
22 -	.117	- .137	- .143				-	.084	22
23 -	.115		- .149			-	.146 -	.124	23
24 -	.118	- .137	- .158			-	.156 -	.175	24
25 -	.121	- .145	- .159			-	.154 -	.141	25
26 -	.162	- .169	- .177			-	.167 -	.180	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.351		.498	.507			.486	.428	1
2	.283		.446	.507			.503	.340	2
3	.306		.394	.459			.483	.294	3
4	.292		.323	.379			.377	.196	4
5	.168		.181	.243			.276	.109	5
6	.169		.169	.195			.221	.044	6
7	.168		.148	.189			.187	.011	7
8	.159		.161	.178			.159		8
9	.156		.143	.173			.126	-.001	9
10	.092		.100	.123			.072	.004	10
11	.124		.100	.090			.059	-.020	11
12	.034	.026	.048	.045	.080	.065	.080	-.063	12
13	.036	.033	.035	.014	.060	.055	.028	-.050	13
14	.055	.040	.026	.031	.028	.033	.009	-.088	14
15	.020	.028	.040	.021	.020	.023	.018	-.066	15
16	.029	.025	.030	.030	.013	.001	-.004	-.080	16
17	-.041		-.040	-.054			-.045	-.009	17
18	-.027		-.045	-.053			-.046	.035	18
19	-.020		-.048	-.054			-.048	.023	19
20	-.046		-.062	-.081			-.079	-.018	20
21	-.119		-.129	-.131			-.131	-.048	21
22	-.119		-.139	-.143				-.081	22
23	-.119			-.157			-.145	-.124	23
24	-.125		-.139	-.157			-.155	-.175	24
25	-.128		-.149	-.168			-.158	-.134	25
26	-.160		-.171	-.181			-.169	-.181	26

$\alpha=-6$ $\delta=10$

1	.352		.490	.508			.494	.428	1
2	.285		.441	.501			.519	.332	2
3	.306		.394	.454			.498	.278	3
4	.287		.319	.370			.392	.180	4
5	.161		.183	.240			.288	.100	5
6	.164		.159	.197			.228	.039	6
7	.163		.147	.195			.192	-.001	7
8	.151		.160	.192			.166		8
9	.144		.139	.169			.130	-.010	9
10	.101		.097	.133			.079	.000	10
11	.127		.098	.106			.070	-.029	11
12	.034	.016	-.161	-.145	-.148	.061	-.066	-.068	12
13	.033	-.033	-.195	-.200	-.141	.024	-.024	-.066	13
14	.053	-.063	-.154	-.180	-.131	-.046	-.003	-.095	14
15	.010	-.088	-.141	-.199	-.155	-.068	-.010	-.078	15
16	.023	-.098	-.154	-.191	-.173	-.086	-.014	-.088	16
17	-.046		-.046	-.052			-.039	-.016	17
18	-.029		-.051	-.045			-.035	.030	18
19	-.028		-.050	-.038			-.039	.013	19
20	-.050		-.067	-.073			-.063	-.028	20
21	-.127		-.132	-.118			-.123	-.053	21
22	-.118		-.140	-.140				-.091	22
23	-.118			-.148			-.139	-.135	23
24	-.123		-.140	-.151			-.149	-.180	24
25	-.127		-.151	-.153			-.148	-.149	25
26	-.169		-.177	-.173			-.155	-.188	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.357		.491	.516			.500	.442	1
2	.293		.443	.503			.515	.344	2
3	.301		.390	.455			.492	.296	3
4	.291		.319	.372			.391	.191	4
5	.169		.179	.236			.289	.119	5
6	.162		.163	.198			.229	.049	6
7	.164		.149	.193			.193	.013	7
8	.153		.163	.184			.169		8
9	.146		.136	.156			.132	.004	9
10	.096		.102	.125			.077	.011	10
11	.126		.103	.098			.070	-.026	11
12	.043	.025	-.298	-.274	-.285	.075	.084	-.063	12
13	.046	-.039	-.327	-.329	-.276	.024	.033	-.053	13
14	.066	-.084	-.296	-.320	-.264	-.071	.011	-.091	14
15	.021	-.118	-.269	-.323	-.293	-.101	.018	-.075	15
16	.034	-.128	-.303	-.322	-.327	-.118	-.011	-.074	16
17	-.044		-.044	-.060			-.048	-.003	17
18	-.030		-.050	-.052			-.039	-.040	18
19	-.028		-.047	-.044			-.045	.026	19
20	-.051		-.064	-.075			-.066	-.008	20
21	-.135		-.135	-.125			-.121	-.049	21
22	-.127		-.144	-.147				-.083	22
23	-.126			-.155			-.145	-.129	23
24	-.133		-.144	-.155			-.154	-.170	24
25	-.139		-.151	-.160			-.152	-.141	25
26	-.167		-.172	-.174			-.164	-.184	26

$\alpha = -6$ $\delta = 30$

1	.356		.494	.518			.511	.438	1
2	.290		.449	.508			.522	.345	2
3	.310		.397	.466			.500	.294	3
4	.292		.317	.370			.392	.193	4
5	.160		.180	.244			.289	.114	5
6	.167		.169	.199			.231	.039	6
7	.164		.150	.193			.194	.010	7
8	.155		.164	.183			.169		8
9	.149		.141	.158			.130	-.001	9
10	.097		.107	.133			.077	.004	10
11	.123		.107	.106			.065	-.021	11
12	.035	.038	-.373	-.363	-.370	.069	.093	-.059	12
13	.039	-.034	-.399	-.400	-.369	.033	.034	-.046	13
14	.059	-.081	-.369	-.399	-.348	-.071	.020	-.083	14
15	.025	-.115	-.369	-.383	-.393	-.100	.025	-.066	15
16	.029	-.124	-.370	-.320	-.408	-.113	.005	-.074	16
17	-.054		-.045	-.064			-.052	-.010	17
18	-.034		-.054	-.055			-.041	.036	18
19	-.027		-.050	-.054			-.043	.024	19
20	-.051		-.066	-.072			-.072	-.016	20
21	-.128		-.139	-.126			-.129	-.050	21
22	-.127		-.145	-.144				-.091	22
23	-.124			-.156			-.148	-.136	23
24	-.130		-.146	-.061			-.160	-.178	24
25	-.134		.081	.137			-.156	-.146	25
26	-.167		.110	.155			-.161	-.186	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.240		.300	.321			.329	.264	1
2	.194		.292	.299			.295	.208	2
3	.210		.276	.309			.298	.176	3
4	.199		.216	.261			.247	.114	4
5	.073		.094	.153			.177	.069	5
6	.085		.079	.109			.144	.028	6
7	.092		.063	.103			.123	.006	7
8	.083		.077	.093			.095		8
9	.070		.057	.073			.072	-.009	9
10	.025		.018	.051			.022	-.004	10
11	.048		.018	.026			.016	-.019	11
12	-.035	-.040	-.015	-.020	-.014	-.014	.015	-.049	12
13	-.038	-.050	-.043	-.050	-.018	-.015	-.036	-.050	13
14	-.025	-.046	-.054	-.043	-.033	-.040	-.045	-.089	14
15	-.056	-.054	-.035	-.050	-.048	-.045	-.044	-.068	15
16	-.046	-.049	-.045	-.044	-.059	-.059	-.058	-.070	16
17	.049		.048	.041			.045	.041	17
18	.043		.048	.042			.058	.079	18
19	.038		.043	.050			.051	.063	19
20	.019		.024	.030			.015	.024	20
21	-.057		-.059	-.044		-.045	-.010		21
22	-.063		-.068	-.062			-.010		22
23	-.064			-.073		-.065	-.020		23
24	-.064		-.083	-.072		-.078	-.049		24
25	-.065		-.093	-.079		-.083	-.026		25
26	-.108		-.124	-.105		-.102	-.064		26

$\alpha = 0$ $\delta = -30$

1	.143		.152	.162			.155	.126	1
2	.114		.161	.162			.155	.111	2
3	.119		.161	.162			.155	.105	3
4	.109		.125	.135			.103	.064	4
5	.006		.019	.049			.048	.023	5
6	.006		.003	.015			.017	.015	6
7	.006		-.008	.006			.013	.003	7
8	-.003		-.008	.268		-.002			8
9	-.003			.235	.352		-.016	-.009	9
10	-.029			.297	.362		-.053	-.004	10
11	-.021			.298	.362		-.053	-.020	11
12	-.100	.080		.282	.383	.292	.115	-.055	-.028	12
13	-.101	.115		.342	.393	.293	.110	-.088	-.040	13
14	-.081	-.108		.618	.618	.528	-.019	-.015	-.049	14
15	-.065	-.198		.640	.785	.581	-.130	-.003	-.044	15
16	.034	-.230		.513	.709	.508	-.178	-.013	-.044	16
17	.146			.166	.140			.156	.124	17
18	.120			.155	.150			.156	.154	18
19	.118			.156	.155			.156	.104	19
20	.099			.122	.124			.107	.055	20
21	.003			.018	.047			.041	.026	21
22	.009			.001	.026				.016	22
23	.009				.007			.011	.016	23
24	.003		-.015		.007			.000	-.004	24
25	.003		-.022	-.019			-.013	-.011	25
26	-.042		-.054	-.040			-.045	-.009	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.136		.152	.166			.159	.135	1
2	.109		.154	.154			.158	.118	2
3	.118		.151	.167			.158	.116	3
4	.104		.117	.134			.115	.081	4
5	.000		.013	.050			.054	.036	5
6	.006		.007	.015			.024	.025	6
7	.006		-.014	.008			.019	.015	7
8	-.005		-.009	.008			-.003		8
9	-.005		-.020	.050			-.013	.005	9
10	-.045		-.040	-.024			-.051	.003	10
11	-.021		-.039	.232			-.055	-.015	11
12	-.098	.024	.275	.289	.213	.070	-.059	-.018	12
13	-.106	-.009	.363	.391	.289	.028	-.094	-.033	13
14	-.080	-.041	.333	.483	.288	-.016	-.109	-.041	14
15	-.109	-.200	.298	.480	.243	-.134	-.096	-.030	15
16	-.095	-.190	.265	.433	.204	-.153	-.088	-.041	16
17	.147		.161	.146			.151	.131	17
18	.114		.153	.154			.159	.159	18
19	.115		.153	.159			.159	.114	19
20	.100		.122	.126			.124	.071	20
21	.000		.011	.049			.049	.035	21
22	.010		.003	.018				.024	22
23	.003			.009			.011	.020	23
24	.004		-.011	.009			-.003	.005	24
25	-.005		-.022	-.013			-.019	.014	25
26	-.053		-.040	-.037			-.039	.003	26

$\alpha = 0$ $\delta = -15$

1	.128		.148	.160			.159	.139	1
2	.103		.153	.158			.159	.121	2
3	.111		.152	.158			.159	.111	3
4	.106		.120	.132			.121	.079	4
5	.004		.012	.042			.053	.031	5
6	.002		-.001	.012			.017	.024	6
7	.002		-.014	.012			.018	.008	7
8	-.003		-.014	.005			.003		8
9	-.004		-.031	-.010			-.014	-.006	9
10	-.052		-.047	-.034			-.052	.001	10
11	-.023		-.047	-.027			-.052	-.018	11
12	-.091	-.038	.234	.188	.119	-.013	-.064	-.023	12
13	-.101	-.038	.264	.278	.202	-.009	-.100	-.043	13
14	-.078	-.040	.200	.314	.157	-.031	-.110	-.049	14
15	-.110	-.182	.172	.310	.130	-.120	-.104	-.041	15
16	-.109	-.174	.136	.284	.093	-.145	-.106	-.049	16
17	.142		.155	.146			.151	.136	17
18	.113		.152	.153			.158	.160	18
19	.113		.152	.156			.158	.118	19
20	.098		.100	.126			.118	.068	20
21	-.006		.011	.056			.049	.033	21
22	.003		-.003	.022				.018	22
23	.003			.016			.013	.023	23
24	.003		-.017	.007			-.002	.001	24
25	-.003		-.026	-.010			-.013	.020	25
26	-.051		-.055	-.041			-.046	-.001	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.154		.152	.168			.159	.131	1
2	.128		.159	.158			.159	.114	2
3	.129		.160	.159			.159	.109	3
4	.111		.124	.136			.118	.069	4
5	.016		.020	.054			.057	.029	5
6	.016		.012	.020			.026	.021	6
7	.014		-.009	.013			.018	.008	7
8	.006		-.002	.013			.007		8
9	.005		-.023	-.016			-.011	-.011	9
10	-.035		-.044	-.032			-.055	-.003	10
11	-.013		-.045	-.054			-.055	-.016	11
12	-.099	-.074	.130	.069	.043	-.065	-.060	-.024	12
13	-.103	-.064	.111	.113	.088	-.029	-.099	-.040	13
14	-.081	-.048	.066	.130	.051	-.040	-.110	-.055	14
15	-.113	-.110	.048	.130	.024	-.071	-.098	-.045	15
16	-.108	-.139	.031	.128	-.001	-.118	-.104	-.046	16
17	.153		.158	.145			.149	.129	17
18	.125		.158	.153			.154	.158	18
19	.129		.158	.161			.154	.110	19
20	.102		.117	.123			.129	.056	20
21	.004		.013	.043			.058	.026	21
22	.011		-.001	.025				.014	22
23	.011			.017			.013	.014	23
24	.011		-.011	.012			.002	-.001	24
25	.002		-.026	-.016			-.016	-.016	25
26	-.044		-.047	-.045			-.050	-.003	26

$\alpha = 0$ $\delta = 0$

1	.144		.160	.169			.153	.138	1
2	.117		.160	.167			.158	.115	2
3	.132		.160	.166			.158	.114	3
4	.110		.117	.135			.116	.076	4
5	.005		.016	.052			.058	.033	5
6	.008		.005	.021			.025	.020	6
7	.008		-.003	.005			.021	.009	7
8	-.001		-.003	.005			.001		8
9	.000		-.022	-.025			-.013	-.001	9
10	-.036		-.043	-.039			-.054	-.003	10
11	-.011		-.042	-.064			-.054	-.019	11
12	-.093	-.091	-.095	-.100	-.109	-.076	-.063	-.019	12
13	-.100	-.100	-.121	-.119	-.104	-.086	-.103	-.035	13
14	-.086	-.106	-.116	-.120	-.106	-.095	-.104	-.048	14
15	-.111	-.113	-.106	-.118	-.113	-.104	-.100	-.039	15
16	-.105	-.109	-.108	-.113	-.116	-.111	-.106	-.036	16
17	.154		.161	.140			.147	.126	17
18	.124		.154	.146			.153	.150	18
19	.126		.154	.149			.153	.111	19
20	.100		.128	.114			.116	.058	20
21	.008		.014	.049			.047	.024	21
22	.008		.002	.014				.013	22
23	.008			.006			.006	.015	23
24	.008		-.011	.007			.000	-.005	24
25	.000		-.020	-.015			-.014	-.018	25
26	-.040		-.046	-.045			-.048	-.004	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.139		.147	.158			.154	.120	1
2	.102		.159	.158			.160	.111	2
3	.115		.156	.158			.150	.104	3
4	.105		.113	.126			.110	.070	4
5	.002		.006	.039			.045	.023	5
6	.002		.000	.014			.013	.015	6
7	.002		-.014	.010			.008	.001	7
8	-.012		-.007	-.004			-.007		8
9	-.012		-.026	-.021			-.020	-.010	9
10	-.045		-.047	-.044			-.060	-.009	10
11	-.012		-.047	-.071			-.060	-.026	11
12	-.100	-.105	-.094	-.100	-.090	-.089	-.056	-.034	12
13	-.105	-.106	-.111	-.124	-.098	-.088	-.101	-.051	13
14	-.085	-.110	-.118	-.124	-.106	-.103	-.109	-.053	14
15	-.118	-.116	-.116	-.121	-.114	-.105	-.105	-.051	15
16	-.114	-.114	-.119	-.121	-.119	-.114	-.108	-.050	16
17	.143		.151	.142			.143	.121	17
18	.105		.151	.146			.148	.150	18
19	.117		.149	.155			.148	.101	19
20	.092		.106	.121			.107	.060	20
21	-.006		.005	.041			.035	.020	21
22	.000		-.006	.010				.015	22
23	-.001			.010			.000	.013	23
24	-.003		-.022	.005			-.015	-.010	24
25	-.009		-.028	-.017			-.028	-.011	25
26	-.051		-.058	-.047			-.047	-.014	26

$\alpha = 0$ $\delta = 10$

1	.144		.152	.162			.162	.124	1
2	.108		.152	.162			.160	.113	2
3	.117		.152	.163			.160	.109	3
4	.107		.116	.129			.113	.069	4
5	.006		.017	.054			.056	.029	5
6	.006		.007	.018			.015	.015	6
7	.006		-.014	.010			.016	.001	7
8	-.004		-.009	.010			.003		8
9	-.007		-.022	-.013			-.016	-.011	9
10	-.042		-.046	-.029			-.057	-.005	10
11	-.021		-.046	-.054			-.056	-.019	11
12	-.099	-.108	-.253	-.247	-.254	-.075	-.059	-.019	12
13	-.095	-.141	-.280	-.277	-.232	-.099	-.103	-.039	13
14	-.085	-.163	-.257	-.284	-.232	-.150	-.105	-.045	14
15	-.111	-.192	-.244	-.284	-.213	-.162	-.101	-.045	15
16	-.106	-.172	-.230	-.278	-.250	-.163	-.105	-.041	16
17	.148		.156	.147			.147	.119	17
18	.117		.148	.146			.153	.155	18
19	.117		.148	.156			.153	.113	19
20	.092		.109	.120			.114	.060	20
21	-.011		.011	.038			.041	.030	21
22	.001		-.001	.020				.016	22
23	.001			.012			.012	.016	23
24	-.003		-.015	.005			.001	-.003	24
25	-.003		-.024	-.017			-.016	-.018	25
26	-.053		-.050	-.044			-.052	-.005	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.144		.156	.171			.159	.141	1
2	.111		.156	.164			.165	.121	2
3	.125		.156	.164			.163	.113	3
4	.105		.118	.139			.121	.073	4
5	.009		.011	.054			.053	.030	5
6	.009		.003	.018			.028	.019	6
7	.002		-.008	.011			.024	.006	7
8	-.007		-.008	.011			.009		8
9	-.008		-.027	-.016			-.009	-.006	9
10	-.038		-.039	-.031			-.056	-.003	10
11	-.022		-.039	-.051			-.055	-.015	11
12	-.094	-.116	-.369	-.351	-.362	-.070	-.054	-.018	12
13	-.099	-.163	-.392	-.391	-.353	-.101	-.099	-.033	13
14	-.081	-.182	-.381	-.396	-.327	-.168	-.104	-.043	14
15	-.101	-.204	-.338	-.396	-.354	-.189	-.101	-.043	15
16	-.105	-.190	-.347	-.278	-.404	-.190	-.104	-.044	16
17	.139		.156	.134			.147	.125	17
18	.112		.156	.142			.151	.150	18
19	.117		.155	.156			.151	.106	19
20	.092		.109	.118			.111	.058	20
21	-.001		.018	.039			.035	.025	21
22	.000		.008	.012				.021	22
23	.000			.010			.011	.019	23
24	.000		-.017	.000			-.013	.003	24
25	-.004		-.025	-.022			-.030	.021	25
26	-.050		.128	.273			-.051	.000	26

$\alpha = 0$ $\delta = 20$

1	.143		.156	.169			.167	.131	1
2	.111		.156	.161			.169	.115	2
3	.124		.152	.167			.159	.109	3
4	.110		.117	.128			.116	.073	4
5	.007		.013	.044			.060	.025	5
6	.007		.005	.012			.025	.018	6
7	.007		-.006	.015			.024	.005	7
8	.000		-.006	.010			.009		8
9	.000		-.023	-.013			-.011	-.009	9
10	-.045		-.048	-.033			-.048	.000	10
11	-.022		-.048	-.054			-.055	-.016	11
12	-.098	-.111	-.358	-.344	-.344	-.068	-.058	-.026	12
13	-.110	-.158	-.382	-.382	-.344	-.099	-.099	-.041	13
14	-.083	-.189	-.364	-.384	-.323	-.174	-.110	-.048	14
15	-.119	-.209	-.314	-.382	-.325	-.188	-.108	-.041	15
16	-.114	-.196	-.342	-.274	-.394	-.186	-.111	-.044	16
17	.141		.155	.139			.147	.121	17
18	.111		.149	.151			.154	.144	18
19	.117		.149	.156			.154	.103	19
20	.102		.104	.122			.116	.054	20
21	.004		.009	.037			.038	.023	21
22	.004		-.003	.017				.008	22
23	.003			.007			.013	.009	23
24	.003		-.018	.007			-.006	-.005	24
25	-.006		-.027	-.016			-.019	.010	25
26	-.057		-.043	.145			-.051	.006	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.148		.155	.164			.159	.131	1
2	.108		.159	.164			.162	.115	2
3	.124		.154	.164			.157	.108	3
4	.112		.123	.133			.117	.068	4
5	.012		.011	.052			.061	.024	5
6	.010		.004	.010			.013	.015	6
7	.010		-.012	.014			.015	.000	7
8	-.006		-.007	.008			-.002		8
9	-.005		-.017	-.017			-.019	-.011	9
10	-.039		-.045	-.033			-.053	-.004	10
11	-.022		-.045	-.061			-.057	-.025	11
12	-.103	-.124	-.428	-.417	-.423	-.080	-.056	-.034	12
13	-.105	-.166	-.434	-.437	-.425	-.106	-.099	-.041	13
14	-.088	-.201	-.398	-.405	-.369	-.179	-.108	-.050	14
15	-.111	-.215	-.374	-.392	-.435	-.196	-.103	-.045	15
16	-.074	-.205	-.369	-.368	-.459	-.198	-.109	-.044	16
17	.146		.153	.133			.136	.115	17
18	.106		.148	.140			.143	.143	18
19	.119		.148	.149			.143	.103	19
20	.099		.099	.114			.102	.055	20
21	.001		.002	.044			.032	.019	21
22	.004		-.002	-.002				.009	22
23	.004			.032			-.001	.009	23
24	.004		-.002	.328			-.014	-.008	24
25	-.005		.295	.364			-.026	.015	25
26	-.051		.286	.374			-.046	-.011	26

$\alpha = 3$ $\delta = 0$

1	.046		.047	.051			.043	.043	1
2	.031		.048	.050			.054	.059	2
3	.043		.048	.050			.054	.066	3
4	.025		.026	.029			.025	.040	4
5	-.065		-.062	-.045			-.035	.004	5
6	-.054		-.072	-.065			-.057	-.003	6
7	-.058		-.072	-.071			-.066	-.034	7
8	-.073		-.076	-.075			-.085		8
9	-.072		-.088	-.055			-.085	-.049	9
10	-.093		-.107	-.107			-.114	-.059	10
11	-.090		-.107	-.128			-.110	-.079	11
12	-.149	-.164	-.138	-.136	-.158	-.150	-.116	-.101	12
13	-.148	-.166	-.168	-.166	-.164	-.150	-.154	-.100	13
14	-.136	-.159	-.163	-.166	-.168	-.166	-.154	-.135	14
15	-.156	-.166	-.168	-.168	-.170	-.166	-.149	-.163	15
16	-.151	-.165	-.164	-.165	-.169	-.161	-.151	-.176	16
17	.241		.295	.276			.286	.249	17
18	.186		.281	.280			.273	.239	18
19	.197		.272	.290			.290	.161	19
20	.173		.218	.237			.234	.118	20
21	.079		.091	.139			.152	.056	21
22	.080		.069	.101				.035	22
23	.080			.095			.110	.018	23
24	.069		.058	.082			.081	-.008	24
25	.070		.049	.062			.063	.020	25
26	.005		.003	.032			.027	-.001	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.051		-.053	-.039			-.045	-.030	1
2	-.039		-.046	-.039			-.035	.010	2
3	-.025		-.055	-.049			-.050	.018	3
4	-.047		-.055	-.065			-.077	-.008	4
5	-.139		-.145	-.123			-.113	-.060	5
6	-.109		-.145	-.145			-.124	-.105	6
7	-.120		-.143	-.148			-.141	-.170	7
8	-.143		-.143	-.040			-.157		8
9	-.137		-.003	-.016			-.146	-.193	9
10	-.159		.105	.150			-.170	-.193	10
11	-.150		.105	.150			-.159	-.219	11
12	-.191	-.073	.120	.180	.076	-.068	-.170	-.236	12
13	-.204	-.060	.165	.184	.095	-.096	-.203	-.218	13
14	-.191	-.214	.440	.398	.329	-.165	-.181	-.244	14
15	-.196	-.281	.474	.568	.387	-.239	-.140	-.238	15
16	-.060	-.286	.397	.550	.347	-.245	-.139	-.231	16
17	.347		.493	.494			.504	.407	17
18	.292		.436	.480			.504	.360	18
19	.301		.384	.451			.483	.268	19
20	.269		.305	.358			.393	.185	20
21	.154		.171	.230			.279	.096	21
22	.167		.155	.197				.055	22
23	.163			.186			.186	.020	23
24	.153		.145	.178			.162	-.003	24
25	.153		.136	.155			.141	.025	25
26	.082		.093	.114			.099	-.006	26

$\alpha = 6$ $\delta = -20$

1	-.043		-.051	-.048			-.058	-.044	1
2	-.043		-.051	-.048			-.043	-.008	2
3	-.018		-.051	-.048			-.044	.004	3
4	-.045		-.063	-.073			-.080	-.020	4
5	-.129		-.142	-.129			-.124	-.069	5
6	-.129		-.142	-.157			-.146	-.116	6
7	-.129		-.142	-.152			-.146	-.180	7
8	-.135		-.142	-.158			-.158		8
9	-.129		-.159	-.127			-.153	-.211	9
10	-.161		-.155	-.165			-.171	-.216	10
11	-.152		-.155	.062			-.161	-.233	11
12	-.199	-.114	.085	.096	.030	-.091	-.178	-.244	12
13	-.205	-.151	.190	.183	.096	-.135	-.205	-.228	13
14	-.190	-.188	.201	.286	.131	-.178	-.203	-.249	14
15	-.213	-.251	.174	.299	.104	-.218	-.194	-.238	15
16	-.204	-.266	.139	.290	.080	-.235	-.184	-.234	16
17	.350		.487	.491			.495	.390	17
18	.289		.432	.487			.500	.354	18
19	.301		.382	.441			.482	.266	19
20	.272		.299	.356			.392	.176	20
21	.156		.168	.228			.271	.090	21
22	.170		.155	.195				.040	22
23	.158			.177			.186	.020	23
24	.159		.143	.171			.154	-.009	24
25	.149		.132	.151			.130	.026	25
26	.082		.095	.120			.092	-.009	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.045		-.047	-.039			-.046	-.039	1
2	-.031		-.050	-.040			-.040	-.005	2
3	-.022		-.050	-.042			-.039	.010	3
4	-.045		-.059	-.065			-.069	-.015	4
5	-.132		-.141	-.128			-.114	-.068	5
6	-.130		-.140	-.147			-.132	-.105	6
7	-.126		-.148	-.147			-.146	-.175	7
8	-.135		-.138	-.153			-.157		8
9	-.128		-.158	-.164			-.147	-.198	9
10	-.158		-.169	-.179			-.170	-.213	10
11	-.144		-.169	-.179			-.159	-.233	11
12	-.196	-.178	-.030	-.081	-.103	-.183	-.170	-.235	12
13	-.206	-.179	-.021	-.048	-.060	-.170	-.204	-.225	13
14	-.190	-.168	-.053	-.024	-.081	-.178	-.209	-.248	14
15	-.211	-.174	-.066	-.019	-.098	-.170	-.191	-.235	15
16	-.211	-.211	-.085	-.016	-.104	-.176	-.193	-.230	16
17	.350		.489	.492			.499	.389	17
18	.288		.445	.482			.509	.355	18
19	.303		.388	.450			.486	.268	19
20	.279		.315	.361			.390	.180	20
21	.158		.176	.236			.272	.091	21
22	.171		.159	.195				.050	22
23	.159			.183			.191	.020	23
24	.158		.143	.177			.164	-.003	24
25	.144		.135	.146			.137	.021	25
26	.074		.087	.108			.095	-.006	26

$\alpha = 6$ $\delta = 0$

1	-.042		-.051	-.036			-.050	-.026	1
2	-.035		-.040	-.036			-.040	.008	2
3	-.024		-.041	-.043			-.040	.016	3
4	-.036		-.055	-.063			-.066	-.008	4
5	-.121		-.137	-.121			-.108	-.058	5
6	-.127		-.137	-.143			-.135	-.101	6
7	-.121		-.137	-.146			-.143	-.171	7
8	-.121		-.137	-.153			-.155		8
9	-.121		-.151	-.166			-.145	-.193	9
10	-.154		-.158	-.179			-.169	-.198	10
11	-.141		-.157	-.193			-.151	-.218	11
12	-.189	-.210	-.198	-.206	-.225	-.205	-.164	-.239	12
13	-.206	-.215	-.210	-.231	-.221	-.203	-.193	-.229	13
14	-.183	-.210	-.215	-.224	-.225	-.215	-.193	-.246	14
15	-.203	-.219	-.209	-.224	-.226	-.216	-.181	-.236	15
16	-.199	-.211	-.205	-.220	-.226	-.213	-.179	-.231	16
17	.352		.494	.492			.500	.397	17
18	.298		.442	.483			.507	.360	18
19	.302		.386	.444			.487	.265	19
20	.280		.313	.343			.392	.183	20
21	.160		.181	.242			.274	.100	21
22	.172		.165	.201				.055	22
23	.162			.183			.191	.026	23
24	.165		.149	.174			.157	.000	24
25	.153		.141	.150			.136	.028	25
26	.085		.091	.117			.092	-.003	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.047		-.053	-.048			-.047	-.040	1
2	-.034		-.047	-.047			-.038	.000	2
3	-.021		-.047	-.047			-.039	.010	3
4	-.041		-.069	-.065			-.068	-.014	4
5	-.126		-.139	-.131			-.105	-.058	5
6	-.126		-.139	-.149			-.138	-.100	6
7	-.126		-.141	-.143			-.147	-.170	7
8	-.133		-.141	-.149			-.147		8
9	-.133		-.157	-.168			-.147	-.193	9
10	-.162		-.169	-.175			-.175	-.204	10
11	-.149		-.169	-.191			-.157	-.221	11
12	-.196	-.223	-.317	-.329	-.334	-.198	-.160	-.238	12
13	-.195	-.249	-.347	-.362	-.328	-.214	-.196	-.225	13
14	-.186	-.255	-.332	-.364	-.332	-.258	-.196	-.251	14
15	-.204	-.261	-.311	-.362	-.289	-.264	-.183	-.231	15
16	-.196	-.224	-.194	-.230	-.377	-.251	-.179	-.229	16
17	.348		.490	.491			.494	.389	17
18	.295		.435	.483			.508	.352	18
19	.298		.381	.450			.480	.263	19
20	.272		.297	.353			.386	.176	20
21	.157		.169	.225			.273	.093	21
22	.164		.152	.201				.046	22
23	.160			.182			.187	.024	23
24	.155		.140	.174			.166	.001	24
25	.149		.131	.157			.137	.028	25
26	.077		.090	.113			.097	-.004	26

$\alpha = 6$ $\delta = 20$

1	-.048		-.054	-.045			-.043	-.045	1
2	-.028		-.042	-.045			-.038	-.003	2
3	-.014		-.045	-.045			-.038	.010	3
4	-.042		-.067	-.064			-.071	-.011	4
5	-.122		-.143	-.117			-.112	-.061	5
6	-.122		-.143	-.147			-.143	-.109	6
7	-.122		-.143	-.145			-.143	-.169	7
8	-.133		-.138	-.151			-.152		8
9	-.128		-.151	-.166			-.148	-.196	9
10	-.156		-.167	-.177			-.166	-.205	10
11	-.146		-.167	-.193			-.152	-.220	11
12	-.204	-.229	-.402	-.408	-.409	-.204	-.169	-.246	12
13	-.210	-.263	-.429	-.422	-.409	-.223	-.208	-.224	13
14	-.190	-.274	-.367	-.355	-.387	-.271	-.204	-.254	14
15	-.214	-.279	-.317	-.353	-.434	-.288	-.190	-.241	15
16	-.099	-.231	-.357	-.333	-.468	-.269	-.190	-.230	16
17	.347		.493	.486			.492	.384	17
18	.299		.437	.477			.501	.345	18
19	.299		.377	.445			.485	.263	19
20	.275		.307	.350			.392	.176	20
21	.155		.173	.227			.273	.091	21
22	.170		.161	.195				.046	22
23	.163			.178			.188	.024	23
24	.156		.142	.174			.159	-.006	24
25	.152		.132	.222			.133	.028	25
26	.084		.390	.527			.097	-.008	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61; R = 3.6 \times 10^6$.

$\alpha = 6 \quad \delta = 30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.041		-.042	-.038			-.041	-.050	1
2	-.031		-.040	-.038			-.034	-.009	2
3	-.023		-.040	-.038			-.034	.005	3
4	-.039		-.059	-.057			-.070	-.015	4
5	-.116		-.133	-.118			-.113	-.066	5
6	-.116		-.133	-.148			-.142	-.109	6
7	-.117		-.133	-.144			-.141	-.174	7
8	-.128		-.133	-.147			-.145		8
9	-.124		-.150	-.161			-.145	-.196	9
10	-.156		-.169	-.178			-.164	-.206	10
11	-.141		-.169	-.189			-.150	-.224	11
12	-.199	-.221	-.415	-.402	-.429	-.198	-.166	-.239	12
13	-.203	-.259	-.422	-.404	-.420	-.211	-.196	-.225	13
14	-.193	-.268	-.384	-.379	-.402	-.268	-.193	-.259	14
15	-.208	-.261	-.370	-.368	-.459	-.284	-.181	-.236	15
16	-.031	-.233	-.390	-.347	-.460	-.253	-.178	-.229	16
17	.354		.493	.488			.497	.380	17
18	.307		.441	.482			.505	.340	18
19	.306		.385	.447			.489	.261	19
20	.279		.301	.356			.401	.175	20
21	.162		.180	.226			.275	.093	21
22	.171		.155	.193				.051	22
23	.167			.534			.189	.015	23
24	.155		.424	.601			.158	-.009	24
25	.157		.523	.616			.209	.023	25
26	.091		.500	.609			.246	-.009	26

$\alpha = 9 \quad \delta = 0$

1	-.126		-.124	-.124			-.123	-.111	1
2	-.095		-.117	-.120			-.107	-.049	2
3	-.090		-.117	-.119			-.113	-.063	3
4	-.101		-.126	-.139			-.144	-.094	4
5	-.182		-.198	-.187			-.176	-.148	5
6	-.169		-.198	-.203			-.189	-.239	6
7	-.169		-.195	-.210			-.201	-.280	7
8	-.176		-.191	-.214			-.215		8
9	-.177		-.204	-.210			-.200	-.286	9
10	-.209		-.209	-.235			-.210	-.284	10
11	-.198		-.209	-.246			-.198	-.285	11
12	-.243	-.251	-.240	-.264	-.271	-.254	-.219	-.295	12
13	-.246	-.266	-.260	-.284	-.269	-.254	-.245	-.291	13
14	-.239	-.246	-.266	-.288	-.273	-.269	-.244	-.290	14
15	-.256	-.260	-.263	-.290	-.274	-.269	-.235	-.279	15
16	-.239	-.241	-.256	-.286	-.271	-.260	-.230	-.273	16
17	.469		.686	.739			.781	.587	17
18	.389		.556	.639			.704	.475	18
19	.406		.493	.569			.625	.344	19
20	.357		.421	.451			.486	.229	20
21	.241		.254	.317			.351	.119	21
22	.250		.237	.272				.071	22
23	.237			.263			.259	.051	23
24	.237		.229	.246			.229	.015	24
25	.235		.217	.230			.199	.048	25
26	.158		.163	.190			.157	.011	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = -30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.195		-.220	-.225			-.235	-.238	1
2	-.160		-.191	-.194			-.204	-.138	2
3	-.146		-.197	-.194			-.193	-.140	3
4	-.160		-.200	-.201			-.217	-.201	4
5	-.226		-.267	-.251			-.237	-.250	5
6	-.219		-.265	-.262			-.250	-.337	6
7	-.219		-.251	-.265			-.260	-.364	7
8	-.228		-.244	-.272			-.267		8
9	-.228		-.122	-.180			-.248	-.359	9
10	-.241		-.058	-.044			-.265	-.362	10
11	-.241		-.058	-.044			-.232	-.349	11
12	-.263	-.185	-.040	-.008	-.074	-.208	-.255	-.352	12
13	-.275	-.184	-.013	-.003	-.074	-.251	-.274	-.348	13
14	-.271	-.270	.228	.179	.135	-.271	-.278	-.348	14
15	-.284	-.339	.279	.315	.161	-.306	-.271	-.349	15
16	-.115	-.328	.239	.317	.134	-.309	-.245	-.333	16
17	.599		.862	.935			.958	.724	17
18	.521		.705	.800			.853	.580	18
19	.536		.632	.707			.741	.425	19
20	.488		.506	.543			.580	.319	20
21	.339		.342	.403			.438	.186	21
22	.354		.335	.375				.124	22
23	.335			.367			.336	.104	23
24	.335		.335	.355			.312	.064	24
25	.319		.320	.338			.295	.101	25
26	.237		.271	.286			.249	.059	26

$\alpha = 12$ $\delta = -20$

1	-.188		-.216	-.234			-.252	-.240	1
2	-.155		-.194	-.195			-.210	-.131	2
3	-.138		-.194	-.195			-.194	-.144	3
4	-.149		-.205	-.208			-.216	-.204	4
5	-.217		-.268	-.252			-.254	-.254	5
6	-.217		-.268	-.273			-.269	-.332	6
7	-.217		-.256	-.271			-.280	-.359	7
8	-.235		-.248	-.271			-.280		8
9	-.220		-.239	-.234			-.260	-.362	9
10	-.241		-.225	-.250			-.274	-.358	10
11	-.241		-.225	-.123			-.246	-.353	11
12	-.264	-.210	-.050	-.073	-.124	-.220	-.261	-.350	12
13	-.279	-.236	.019	-.029	-.066	-.244	-.276	-.355	13
14	-.264	-.244	.044	-.048	-.048	-.269	-.278	-.349	14
15	-.281	-.290	.028	-.065	-.059	-.276	-.273	-.344	15
16	-.181	-.328	.001	.066	-.074	-.288	-.271	-.332	16
17	.604		.866	.924			.953	.726	17
18	.530		.704	.792			.841	.577	18
19	.546		.633	.691			.724	.425	19
20	.485		.508	.537			.562	.322	20
21	.340		.341	.398			.426	.185	21
22	.352		.334	.367				.128	22
23	.339			.357			.322	.103	23
24	.335		.334	.349			.302	.074	24
25	.328		.320	.317			.273	.095	25
26	.240		.270	.285			.229	.055	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.190		-.210	-.219			-.241	-.231	1
2	-.151		-.189	-.188			-.202	-.129	2
3	-.134		-.195	-.186			-.187	-.139	3
4	-.147		-.196	-.195			-.212	-.196	4
5	-.224		-.262	-.243			-.242	-.251	5
6	-.215		-.262	-.259			-.260	-.339	6
7	-.215		-.256	-.265			-.269	-.362	7
8	-.227		-.247	-.265			-.269		8
9	-.221		-.251	-.260			-.255	-.363	9
10	-.241		-.251	-.284			-.267	-.362	10
11	-.236		-.251	-.278			-.234	-.350	11
12	-.275	-.274	-.154	-.208	-.230	-.286	-.263	-.353	12
13	-.273	-.256	-.148	-.188	-.210	-.268	-.284	-.354	13
14	-.274	-.255	-.168	-.175	-.219	-.275	-.281	-.357	14
15	-.288	-.223	-.181	-.178	-.220	-.253	-.278	-.348	15
16	-.209	-.298	-.175	-.176	-.205	-.236	-.275	-.329	16
17	.607		.862	.935			.956	.726	17
18	.529		.706	.798			.852	.574	18
19	.546		.638	.701			.728	.432	19
20	.490		.511	.534			.580	.319	20
21	.347		.345	.399			.437	.184	21
22	.358		.338	.370				.130	22
23	.336			.360			.329	.104	23
24	.336		.338	.351			.305	.064	24
25	.331		.323	.333			.284	.105	25
26	.245		.273	.288			.238	.063	26

$\alpha = 12$ $\delta = 0$

1	-.187		-.221	-.225			-.233	-.244	1
2	-.149		-.183	-.189			-.203	-.135	2
3	-.129		-.184	-.191			-.185	-.148	3
4	-.145		-.200	-.205			-.213	-.204	4
5	-.216		-.261	-.238			-.244	-.268	5
6	-.217		-.261	-.254			-.259	-.344	6
7	-.217		-.255	-.256			-.259	-.369	7
8	-.227		-.243	-.263			-.271		8
9	-.215		-.243	-.265			-.251	-.369	9
10	-.239		-.243	-.282			-.265	-.369	10
11	-.239		-.243	-.294			-.228	-.359	11
12	-.268	-.281	-.273	-.305	-.305	-.300	-.259	-.359	12
13	-.279	-.285	-.288	-.320	-.304	-.290	-.279	-.347	13
14	-.270	-.278	-.296	-.319	-.300	-.295	-.278	-.348	14
15	-.285	-.281	-.293	-.318	-.303	-.294	-.274	-.333	15
16	-.205	-.210	-.225	-.280	-.279	-.255	-.271	-.318	16
17	.600		.864	.935			.963	.716	17
18	.529		.704	.803			.853	.568	18
19	.541		.639	.707			.736	.423	19
20	.486		.508	.538			.579	.310	20
21	.345		.341	.398			.437	.181	21
22	.358		.341	.374				.123	22
23	.338			.367			.335	.094	23
24	.337		.339	.355			.305	.064	24
25	.326		.321	.332			.283	.091	25
26	.240		.271	.289			.238	.056	26

TABLE III.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = 10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .192		- .216	- .224			- .240	- .218	1
2	- .152		- .183	- .190			- .207	- .133	2
3	- .134		- .193	- .184			- .185	- .133	3
4	- .151		- .198	- .199			- .214	- .191	4
5	- .222		- .259	- .245			- .237	- .250	5
6	- .219		- .259	- .267			- .253	- .338	6
7	- .219		- .259	- .267			- .261	- .354	7
8	- .225		- .246	- .267			- .269		8
9	- .221		- .246	- .278			- .252	- .354	9
10	- .232		- .246	- .286			- .270	- .352	10
11	- .235		- .246	- .303			- .229	- .349	11
12	- .255	- .278	- .362	- .383	- .389	- .304	- .249	- .352	12
13	- .270	- .313	- .388	- .405	- .375	- .300	- .274	- .345	13
14	- .268	- .313	- .372	- .407	- .394	- .329	- .270	- .344	14
15	- .278	- .311	- .284	- .306	- .342	- .337	- .264	- .337	15
16	- .126	- .248	- .259	- .268	- .403	- .304	- .263	- .322	16
17	.601		.865	.934			.963	.724	17
18	.532		.709	.798			.852	.582	18
19	.542		.635	.697			.735	.427	19
20	.493		.511	.539			.576	.322	20
21	.346		.341	.398			.439	.188	21
22	.354		.341	.376				.129	22
23	.339			.361			.331	.109	23
24	.336		.341	.348			.303	.071	24
25	.327		.324	.333			.281	.106	25
26	.240		.271	.285			.234	.063	26

$\alpha = 12$ $\delta = 20$

1	- .191		- .217	- .219			- .238	- .225	1
2	- .151		- .185	- .192			- .198	- .129	2
3	- .134		- .187	- .188			- .184	- .133	3
4	- .151		- .202	- .197			- .206	- .191	4
5	- .224		- .262	- .242			- .247	- .254	5
6	- .216		- .262	- .258			- .259	- .334	6
7	- .216		- .251	- .261			- .259	- .363	7
8	- .228		- .242	- .260			- .268		8
9	- .222		- .242	- .271			- .247	- .357	9
10	- .238		- .249	- .283			- .259	- .360	10
11	- .231		- .248	- .299			- .230	- .353	11
12	- .266	- .298	- .427	- .434	- .439	- .300	- .260	- .353	12
13	- .274	- .329	- .428	- .445	- .434	- .315	- .276	- .357	13
14	- .266	- .324	- .370	- .392	- .365	- .350	- .280	- .354	14
15	- .283	- .309	- .358	- .352	- .428	- .353	- .279	- .338	15
16	- .099	- .265	- .415	- .320	- .459	- .314	- .269	- .332	16
17	.600		.865	.934			.954	.721	17
18	.531		.705	.802			.851	.574	18
19	.544		.638	.695			.736	.419	19
20	.487		.509	.543			.571	.318	20
21	.335		.342	.402			.431	.181	21
22	.357		.342	.367				.124	22
23	.336			.356			.335	.105	23
24	.336		.335	.478			.309	.068	24
25	.324		.481	.742			.286	.101	25
26	.239		.686	.804			.299	.056	26

TABLE III.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = 30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.192		-.213	-.225			-.233	-.220	1
2	-.146		-.187	-.188			-.197	-.128	2
3	-.134		-.188	-.188			-.183	-.129	3
4	-.153		-.202	-.202			-.206	-.186	4
5	-.223		-.260	-.243			-.239	-.249	5
6	-.214		-.260	-.263			-.258	-.325	6
7	-.218		-.248	-.262			-.258	-.360	7
8	-.226		-.244	-.262			-.267		8
9	-.215		-.245	-.277			-.245	-.354	9
10	-.241		-.245	-.282			-.262	-.352	10
11	-.237		-.245	-.299			-.229	-.348	11
12	-.251	-.295	-.410	-.362	-.369	-.303	-.240	-.339	12
13	-.271	-.324	-.407	-.360	-.370	-.308	-.264	-.340	13
14	-.256	-.328	-.382	-.360	-.375	-.338	-.268	-.350	14
15	-.276	-.303	-.415	-.360	-.454	-.342	-.265	-.342	15
16	-.105	-.260	-.414	-.352	-.449	-.304	-.254	-.329	16
17	.596		.865	.925			.950	.723	17
18	.528		.705	.790			.843	.582	18
19	.540		.636	.701			.735	.434	19
20	.484		.508	.539			.573	.323	20
21	.344		.340	.400			.435	.189	21
22	.352		.340	.375				.129	22
23	.334			.842			.544	.103	23
24	.334		.758	.890			.569	.120	24
25	.346		.784	.917			.559	.211	25
26	.559		.761	.924			.493	.164	26

$\alpha = 15$ $\delta = 0$

1	-.240		-.307	-.319			-.338	-.318	1
2	-.201		-.241	-.259			-.259	-.219	2
3	-.181		-.250	-.255			-.249	-.216	3
4	-.186		-.238	-.259			-.262	-.263	4
5	-.251		-.308	-.299			-.289	-.309	5
6	-.234		-.313	-.301			-.286	-.383	6
7	-.246		-.296	-.305			-.300	-.397	7
8	-.258		-.296	-.312			-.311		8
9	-.258		-.290	-.289			-.295	-.397	9
10	-.273		-.283	-.323			-.301	-.388	10
11	-.280		-.283	-.334			-.253	-.385	11
12	-.303	-.311	-.314	-.338	-.345	-.333	-.288	-.369	12
13	-.303	-.323	-.314	-.359	-.339	-.327	-.304	-.372	13
14	-.304	-.306	-.322	-.352	-.345	-.333	-.308	-.385	14
15	-.320	-.325	-.322	-.353	-.348	-.344	-.305	-.372	15
16	-.174	-.176	-.185	-.240	-.256	-.224	-.306	-.363	16
17	.753		1.017	1.066			1.074	.793	17
18	.662		.844	.924			.959	.649	18
19	.690		.743	.801			.832	.485	19
20	.590		.587	.631			.664	.379	20
21	.435		.413	.492			.517	.228	21
22	.464		.459	.491				.188	22
23	.457			.500			.440	.155	23
24	.478		.482	.501			.426	.116	24
25	.461		.459	.470			.403	.159	25
26	.373		.383	.409			.348	.108	26

TABLE IV

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -15$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.773		1.037	1.087			1.064	.851	1
2	.687		.861	.938			.966	.666	2
3	.727		.765	.821			.837	.518	3
4	.626		.612	.650			.670	.369	4
5	.448		.443	.503			.534	.247	5
6	.493		.498	.527			.495	.172	6
7	.492		.498	.538			.477	.160	7
8	.492		.527	.527			.466		8
9	.469		.472	.461			.350	.131	9
10	.398		.380	.421			.328	.126	10
11	.401		.388	.360			.275	.086	11
12	.288	.284	.314	.313			.344	.024	12
13	.280	.284	.303	.287			.205	.009	13
14	.288	.284	.293	.280			.217	.000	14
15	.292	.279	.284	.283			.199	- .018	15
16	.289	.272	.287	.257			.189	- .020	16
17	- .258		- .344	- .355			- .385	- .339	17
18	- .198		- .282	- .304			- .304	- .224	18
19	- .198		- .270	- .273			- .290	- .250	19
20	- .220		- .270	- .280			- .290	- .284	20
21	- .272		- .319	- .307			- .325	- .343	21
22	- .254		- .321	- .325				- .391	22
23	- .265			- .331			- .332	- .399	23
24	- .263		- .314	- .330			- .332	- .416	24
25	- .264		- .299	- .330			- .321	- .406	25
26	- .288		- .313	- .340			- .319	- .412	26

$\alpha = -12$ $\delta = -30$

1	.595		.853	.928			.934	.760	1
2	.521		.706	.796			.843	.580	2
3	.533		.637	.703			.728	.444	3
4	.502		.516	.550			.568	.305	4
5	.340		.341	.403			.434	.189	5
6	.353		.328	.388			.621	.163	6
7	.343		.571	.844			.857	.426	7
8	.325		.751	.892			.928		8
9	.326		.780	.903			.964	.552	9
10	.535		.773	.975			.979	.593	10
11	.568		.773	.985			.986	.563	11
12	.657	.585	.642	1.012			.965	.537	12
13	.671	.572	.795	1.064			1.033	.689	13
14	.657	.277	1.082	1.233			1.132	.786	14
15	.592	.080	.982	1.118			1.039	.656	15
16	.453	.020	.756	.888			.875	.560	16
17	- .187		- .216	- .232			- .236	- .199	17
18	- .134		- .195	- .202			- .190	- .094	18
19	- .134		- .194	- .188			- .182	- .121	19
20	- .156		- .199	- .204			- .208	- .168	20
21	- .218		- .251	- .239			- .248	- .234	21
22	- .211		- .261	- .260				- .288	22
23	- .216			- .263			- .257	- .312	23
24	- .215		- .243	- .270			- .270	- .339	24
25	- .223		- .243	- .273			- .249	- .309	25
26	- .247		- .264	- .289			- .250	- .341	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61; R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.591		.852	.929			.939	.752	1
2	.504		.697	.794			.850	.577	2
3	.529		.630	.704			.734	.447	3
4	.499		.519	.550			.572	.305	4
5	.334		.340	.400			.439	.193	5
6	.348		.334	.361			.373	.105	6
7	.338		.325	.367			.352	.085	7
8	.325		.345	.578			.571		8
9	.314		.483	.763			.753	.354	9
10	.251		.685	.817			.804	.399	10
11	.276		.685	.838			.822	.373	11
12	.172	.433	.709	.873			.831	.368	12
13	.172	.468	.777	.918			.880	.470	13
14	.310	.254	.824	1.024			.969	.686	14
15	.521	.033	.720	.918			.884	.580	15
16	.448	-.033	.563	.756			.761	.501	16
17	-.188		-.222	-.241			-.234	-.208	17
18	-.139		-.195	-.203			-.202	-.094	18
19	-.134		-.195	-.190			-.184	-.134	19
20	-.164		-.200	-.207			-.204	-.163	20
21	-.215		-.257	-.250			-.246	-.237	21
22	-.210		-.264	-.259				-.298	22
23	-.217			-.278			-.262	-.319	23
24	-.221		-.247	-.275			-.272	-.343	24
25	-.221		-.247	-.275			-.250	-.329	25
26	-.253		-.265	-.292			-.254	-.310	26

$\alpha = -12$ $\delta = -10$

1	.576		.855	.932			.940	.762	1
2	.506		.708	.794			.851	.587	2
3	.519		.630	.707			.739	.457	3
4	.489		.510	.548			.566	.307	4
5	.333		.335	.398			.445	.203	5
6	.342		.329	.366			.371	.111	6
7	.328		.329	.366			.340	.083	7
8	.321		.343	.360			.329		8
9	.308		.300	.404			.247	.068	9
10	.238		.241	.286			.217	.071	10
11	.275		.245	.390			.244	.039	11
12	.174	.284	.605	.611			.521	.034	12
13	.173	.305	.582	.675			.561	.277	13
14	.173	.316	.483	.654			.572	.267	14
15	.173	.108	.433	.588			.536	.257	15
16	.247	.043	.369	.537			.502	.239	16
17	-.200		-.221	-.240			-.246	-.208	17
18	-.144		-.198	-.201			-.197	-.088	18
19	-.144		-.198	-.190			-.182	-.129	19
20	-.169		-.206	-.209			-.204	-.167	20
21	-.227		-.259	-.248			-.237	-.234	21
22	-.219		-.262	-.262				-.307	22
23	-.220			-.271			-.255	-.323	23
24	-.223		-.251	-.271			-.268	-.354	24
25	-.223		-.251	-.276			-.247	-.331	25
26	-.251		-.264	-.287			-.248	-.344	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.586		.855	.930			.940	.752	1
2	.511		.702	.800			.849	.572	2
3	.525		.630	.704			.741	.446	3
4	.507		.511	.548			.576	.304	4
5	.346		.337	.394			.442	.189	5
6	.346		.332	.372			.376	.110	6
7	.339		.325	.369			.341	.075	7
8	.321		.343	.359			.334		8
9	.309		.314	.329			.249	.054	9
10	.247		.252	.284			.222	.054	10
11	.273		.252	.254			.180	.020	11
12	.172	.183	.208	.222			.263	- .006	12
13	.170	.183	.202	.187			.129	- .019	13
14	.169	.183	.192	.182			.120	- .019	14
15	.153	.183	.183	.192			.114	- .050	15
16	.165	.163	.170	.178			.103	- .059	16
17	- .195		- .223	- .241		-	.241	- .217	17
18	- .146		- .191	- .197		-	.203	- .101	18
19	- .139		- .193	- .189		-	.187	- .130	19
20	- .165		- .203	- .204		-	.203	- .182	20
21	- .218		- .258	- .246		-	.234	- .243	21
22	- .218		- .264	- .257				- .318	22
23	- .218			- .270		-	.262	- .336	23
24	- .223		- .252	- .269		-	.261	- .371	24
25	- .223		- .252	- .277		-	.250	- .343	25
26	- .256		- .268	- .286		-	.250	- .372	26

$\alpha = -12$ $\delta = 10$

1	.593		.862	.940			.943	.752	1
2	.514		.708	.806			.850	.576	2
3	.534		.634	.709			.737	.448	3
4	.508		.520	.555			.568	.300	4
5	.342		.349	.408			.436	.199	5
6	.353		.338	.374			.370	.110	6
7	.343		.337	.372			.341	.079	7
8	.330		.347	.361			.331		8
9	.312		.323	.316			.250	.053	9
10	.247		.260	.284			.210	.053	10
11	.279		.260	.243			.181	.019	11
12	.173	.167	- .056	- .065			.010	- .217	12
13	.173	.101	- .085	- .111		-	.140	- .228	13
14	.173	.063	- .046	- .111		-	.140	- .225	14
15	.157	.020	- .048	- .111		-	.140	- .225	15
16	.158	- .006	- .114	- .111		-	.153	- .233	16
17	- .193		- .232	- .247		-	.262	- .223	17
18	- .144		- .199	- .210		-	.212	- .109	18
19	- .144		- .199	- .198		-	.204	- .151	19
20	- .168		- .210	- .215		-	.221	- .180	20
21	- .218		- .261	- .256		-	.258	- .247	21
22	- .218		- .272	- .273				- .327	22
23	- .218			- .273		-	.275	- .349	23
24	- .223		- .253	- .276		-	.282	- .363	24
25	- .223		- .255	- .286		-	.273	- .346	25
26	- .255		- .273	- .297		-	.273	- .369	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.594		.862	.946			.950	.775	1
2	.518		.710	.804			.859	.593	2
3	.534		.640	.708			.749	.462	3
4	.504		.518	.558			.583	.317	4
5	.343		.346	.407			.449	.194	5
6	.353		.340	.370			.376	.119	6
7	.341		.340	.378			.345	.083	7
8	.328		.340	.368			.336		8
9	.316		.313	.331			.265	.060	9
10	.242		.257	.294			.225	.060	10
11	.274		.257	.262			.188	.021	11
12	.173	.173	- .225	- .228		- .164	- .318		12
13	.173	.075	- .262	- .268		- .282	- .337		13
14	.173	.023	- .219	- .268		- .282	- .300		14
15	.173	- .021	- .234	- .278		- .293	- .308		15
16	.173	- .043	- .263	- .278		- .308	- .308		16
17	- .198		- .232	- .247		- .262	- .227		17
18	- .151		- .207	- .209		- .218	- .114		18
19	- .143		- .203	- .196		- .200	- .149		19
20	- .168		- .217	- .213		- .214	- .187		20
21	- .222		- .264	- .254		- .257	- .250		21
22	- .222		- .272	- .269			- .326		22
23	- .222			- .269		- .277	- .349		23
24	- .226		- .255	- .274		- .279	- .378		24
25	- .226		- .256	- .282		- .268	- .346		25
26	- .256		- .274	- .288		- .150	- .376		26

$\alpha = -12$ $\delta = 30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.592		.875	.954			.954	.769	1
2	.522		.722	.811			.859	.588	2
3	.539		.648	.715			.748	.458	3
4	.514		.522	.559			.588	.303	4
5	.348		.351	.413			.454	.199	5
6	.359		.348	.375			.383	.103	6
7	.345		.348	.379			.350	.079	7
8	.330		.348	.369			.344		8
9	.318		.324	.321			.263	.051	9
10	.256		.261	.292			.219	.051	10
11	.273		.261	.251			.189	.023	11
12	.172	.173	- .348	- .351		- .308	- .403		12
13	.172	.068	- .377	- .391		- .388	- .389		13
14	.172	.011	- .358	- .391		- .388	- .389		14
15	.169	- .023	- .359	- .391		- .392	- .389		15
16	.168	- .059	- .384	- .322		- .373	- .389		16
17	- .204		- .232	- .258		- .271	- .250		17
18	- .148		- .206	- .213		- .218	- .118		18
19	- .148		- .206	- .197		- .204	- .164		19
20	- .170		- .215	- .216		- .221	- .205		20
21	- .235		- .275	- .268		- .263	- .269		21
22	- .218		- .273	- .278			- .326		22
23	- .225			- .160		- .214	- .359		23
24	- .225		- .250	- .038		- .063	- .379		24
25	- .225		- .064	- .032		- .041	- .363		25
26	- .261		- .047	- .029		- .024	- .347		26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.482		.713	.783			.800	.654	1
2	.412		.585	.667			.728	.483	2
3	.423		.526	.605			.645	.377	3
4	.406		.436	.475			.487	.245	4
5	.265		.276	.335			.368	.139	5
6	.265		.259	.292			.301	.075	6
7	.262		.247	.284			.267	.035	7
8	.248		.263	.273			.253		8
9	.241		.235	.232			.190	.016	9
10	.176		.183	.211			.146	.019	10
11	.208		.185	.180			.119	-.011	11
12	.103	.114	.119	.139			.184	-.061	12
13	.111	.101	.119	.101			.060	-.073	13
14	.130	.103	.108	.103			.045	-.079	14
15	.094	.103	.108	.101			.040	-.084	15
16	.104	.090	.094	.101			.029	-.100	16
17	-.122		-.134	-.140		-	.136	-.104	17
18	-.073		-.126	-.126		-	.112	-.005	18
19	-.086		-.127	-.121		-	.125	-.060	19
20	-.115		-.138	-.143		-	.151	-.099	20
21	-.182		-.202	-.191		-	.198	-.155	21
22	-.169		-.207	-.208				-.232	22
23	-.173			-.213		-	.210	-.253	23
24	-.182		-.198	-.214		-	.214	-.287	24
25	-.181		-.198	-.226		-	.206	-.252	25
26	-.206		-.224	-.226		-	.214	-.289	26

$\alpha = -6$ $\delta = -30$

1	.351		.497	.515			.507	.426	1
2	.292		.438	.497			.508	.327	2
3	.310		.390	.455			.485	.272	3
4	.293		.318	.368			.385	.172	4
5	.161		.179	.236			.277	.096	5
6	.168		.154	.186			.234	.034	6
7	.158		.152	.545			.559	.224	7
8	.153		.403	.623			.624		8
9	.154		.514	.581			.645	.324	9
10	.095		.501	.652			.652	.324	10
11	.134		.503	.638			.659	.279	11
12	.033	.298	.384	.670			.652	.290	12
13	.049	.265	.505	.689			.674	.332	13
14	.219	.023	.774	.985			.823	.550	14
15	.293	-.080	.808	1.059			.934	.727	15
16	.312	-.135	.621	.855			.841	.654	16
17	-.055		-.060	-.063		-	.050	-.020	17
18	-.031		-.060	-.056		-	.040	-.024	18
19	-.039		-.060	-.049		-	.047	-.011	19
20	-.063		-.072	-.074		-	.074	-.029	20
21	-.133		-.144	-.124		-	.123	-.061	21
22	-.129		-.150	-.146				-.089	22
23	-.129			-.152		-	.144	-.131	23
24	-.136		-.150	-.152		-	.152	-.150	24
25	-.135		-.161	-.159		-	.152	-.041	25
26	-.176		-.179	-.179		-	.161	-.118	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.363		.503	.518			.505	.436	1
2	.294		.449	.503			.513	.339	2
3	.317		.397	.460			.487	.290	3
4	.298		.321	.370			.385	.190	4
5	.166		.183	.236			.280	.113	5
6	.175		.169	.195			.230	.038	6
7	.169		.155	.200			.192	.015	7
8	.161		.166	.191			.192		8
9	.154		.158	.394			.333	.046	9
10	.107		.407	.552			.518	.255	10
11	.136		.407	.576			.540	.240	11
12	.033	.235	.476	.583			.528	.238	12
13	.031	.213	.542	.637			.571	.316	13
14	.053	.085	.617	.795			.720	.437	14
15	.043	-.079	.563	.811			.762	.488	15
16	.153	-.109	.449	.686			.684	.448	16
17	-.049		-.053	-.059		-.048	-.014		17
18	-.036		-.053	-.052		-.038	.031		18
19	-.035		-.053	-.044		-.046	.018		19
20	-.055		-.068	-.073		-.073	-.019		20
21	-.134		-.139	-.125		-.122	-.056		21
22	-.127		-.148	-.150			-.096		22
23	-.129			-.151		-.143	-.134		23
24	-.129		-.144	-.151		-.157	-.169		24
25	-.129		-.155	-.160		-.146	-.134		25
26	-.171		-.184	-.179		-.162	-.154		26

$\alpha = -6$ $\delta = -10$

1	.356		.506	.519			.510	.436	1
2	.303		.453	.508			.516	.341	2
3	.310		.393	.460			.495	.280	3
4	.294		.327	.369			.388	.177	4
5	.169		.177	.240			.285	.101	5
6	.174		.164	.198			.232	.030	6
7	.168		.151	.198			.195	.000	7
8	.157		.168	.186			.167		8
9	.157		.143	.155			.127	-.009	9
10	.093		.101	.127			.077	-.009	10
11	.129		.101	.123			.082	-.033	11
12	.030	.109	.337	.288			.270	-.015	12
13	.040	.120	.359	.389			.319	.198	13
14	.048	.121	.292	.412			.341	.184	14
15	.005	-.018	.258	.403			.326	.144	15
16	.030	-.084	.210	.381			.309	.111	16
17	-.055		-.052	-.060		-.054	-.020		17
18	-.035		-.061	-.049		-.046	.018		18
19	-.035		-.062	-.049		-.046	.008		19
20	-.062		-.076	-.075		-.077	-.036		20
21	-.137		-.140	-.130		-.129	-.059		21
22	-.125		-.147	-.148			-.104		22
23	-.134			-.156		-.148	-.143		23
24	-.133		-.147	-.156		-.163	-.177		24
25	-.133		-.155	-.165		-.151	-.146		25
26	-.172		-.180	-.184		-.167	-.189		26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.361		.507	.521			.516	.454	1
2	.300		.454	.512			.524	.363	2
3	.312		.397	.459			.497	.292	3
4	.299		.327	.379			.391	.169	4
5	.171		.185	.248			.290	.115	5
6	.177		.168	.206			.236	.051	6
7	.173		.157	.199			.195	.019	7
8	.158		.166	.182			.174		8
9	.158		.146	.149			.131	.005	9
10	.099		.104	.123			.075	.005	10
11	.131		.104	.098			.058	-.023	11
12	.038	.049	.058	.079			.136	-.089	12
13	.046	.038	.050	.045			.019	-.064	13
14	.059	.045	.050	.049			-.001	-.073	14
15	.014	.045	.050	.049			.001	-.085	15
16	.029	.028	.034	.049			-.006	-.073	16
17	-.050		-.048	-.065			-.056	-.013	17
18	-.027		-.059	-.060			-.049	.031	18
19	-.029		-.050	-.053			-.048	.015	19
20	-.059		-.066	-.076			-.076	-.019	20
21	-.126		-.139	-.127			-.128	-.054	21
22	-.121		-.147	-.153				-.094	22
23	-.132			-.153			-.146	-.140	23
24	-.131		-.142	-.154			-.159	-.185	24
25	-.131		-.155	-.169			-.153	-.141	25
26	-.175		-.172	-.180			-.170	-.197	26

$\alpha = -6$ $\delta = 10$

1	.356		.503	.526			.532	.463	1
2	.298		.451	.510			.539	.351	2
3	.320		.400	.455			.502	.302	3
4	.290		.330	.372			.393	.188	4
5	.170		.187	.241			.299	.110	5
6	.170		.163	.199			.236	.044	6
7	.170		.154	.206			.203	.013	7
8	.154		.168	.188			.184		8
9	.154		.144	.156			.135	.003	9
10	.104		.103	.137			.078	.003	10
11	.129		.103	.110			.065	-.033	11
12	.035	.035	-.150	-.148			-.065	-.233	12
13	.040	-.020	-.182	-.187			-.200	-.254	13
14	.060	-.044	-.138	-.185			-.204	-.218	14
15	.019	-.069	-.133	-.185			-.212	-.162	15
16	.029	-.085	-.151	-.184			-.215	-.135	16
17	-.047		-.055	-.057			-.049	-.010	17
18	-.033		-.056	-.051			-.044	.028	18
19	-.036		-.056	-.047			-.044	.014	19
20	-.057		-.070	-.078			-.076	-.021	20
21	-.134		-.141	-.115			-.126	-.061	21
22	-.132		-.147	-.147				-.099	22
23	-.132			-.152			-.149	-.145	23
24	-.132		-.147	-.148			-.159	-.185	24
25	-.132		-.160	-.159			-.149	-.160	25
26	-.174		-.180	-.174			-.165	-.198	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-6$ $\delta=20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.377		.513	.542			.538	.478	1
2	.318		.467	.526			.539	.368	2
3	.333		.411	.481			.512	.305	3
4	.305		.341	.385			.398	.200	4
5	.190		.198	.252			.298	.116	5
6	.189		.181	.211			.236	.051	6
7	.183		.169	.212			.199	.018	7
8	.173		.185	.195			.178		8
9	.173		.162	.157			.137	.004	9
10	.114		.110	.135			.077	.004	10
11	.145		.112	.116			.077	-.028	11
12	.033	.039	-.279	-.278		-.229	-.324		12
13	.039	-.033	-.314	-.323		-.327	-.348		13
14	.076	-.089	-.285	-.324		-.326	-.303		14
15	.021	-.116	-.265	-.324		-.341	-.223		15
16	.033	-.126	-.305	-.324		-.341	-.217		16
17	-.036		-.040	-.058		-.056	-.013		17
18	-.021		-.041	-.051		-.043	.040		18
19	-.024		-.041	-.051		-.058	.018		19
20	-.043		-.064	-.071		-.076	-.020		20
21	-.119		-.129	-.121		-.135	-.063		21
22	-.115		-.135	-.157			-.096		22
23	-.115			-.152		-.155	-.151		23
24	-.115		-.134	-.152		-.160	-.187		24
25	-.115		-.142	-.162		-.155	-.157		25
26	-.159		-.169	-.163		-.023	-.194		26

$\alpha=-6$ $\delta=30$

1	.365		.507	.533			.537	.472	1
2	.312		.454	.512			.537	.362	2
3	.323		.405	.471			.509	.298	3
4	.299		.327	.378			.400	.203	4
5	.178		.191	.245			.294	.121	5
6	.183		.173	.206			.239	.060	6
7	.175		.160	.206			.196	.015	7
8	.165		.171	.190			.179		8
9	.154		.148	.156			.138	.010	9
10	.109		.110	.137			.078	.001	10
11	.137		.110	.108			.078	-.028	11
12	.029	.043	-.378	-.374		-.344	-.401		12
13	.036	-.046	-.411	-.404		-.413	-.382		13
14	.071	-.081	-.387	-.393		-.391	-.323		14
15	.023	-.120	-.381	-.343		-.349	-.328		15
16	.038	-.130	-.349	-.318		-.328	-.329		16
17	-.048		-.052	-.064		-.059	-.021		17
18	-.030		-.058	-.058		-.054	.029		18
19	-.030		-.058	-.054		-.054	.016		19
20	-.058		-.069	-.073		-.087	-.024		20
21	-.131		-.140	-.125		-.132	-.075		21
22	-.119		-.151	-.151			-.106		22
23	-.119			.049		.153	-.154		23
24	-.129		-.141	.161		.176	-.190		24
25	-.128		.108	.166		.178	-.128		25
26	-.160		.108	.167		.186	.008		26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.234		.296	.308			.312	.258	1
2	.196		.284	.281			.290	.212	2
3	.209		.272	.294			.285	.180	3
4	.195		.212	.257			.234	.124	4
5	.079		.085	.148			.162	.060	5
6	.083		.076	.096			.126	.023	6
7	.083		.066	.091			.107	.006	7
8	.069		.072	.079			.090		8
9	.069		.052	.050			.060	.000	9
10	.025		.018	.030			.013	.000	10
11	.046		.018	.014			-.009	-.021	11
12	-.035	-.043	-.035	-.009			.064	-.054	12
13	-.038	-.053	-.035	-.039			-.053	-.070	13
14	-.014	-.046	-.035	-.039			-.061	-.089	14
15	-.051	-.048	-.035	-.039			-.064	-.085	15
16	-.050	-.048	-.046	-.039			-.075	-.069	16
17	.051		.060	.035			.041	.056	17
18	.050		.046	.040			.057	.085	18
19	.050		.047	.050			.047	.066	19
20	.025		.025	.029			.018	.039	20
21	-.062		-.060	-.046			-.041	.003	21
22	-.059		-.070	-.065				-.004	22
23	-.059			-.073			-.071	-.018	23
24	-.060		-.079	-.073			-.083	-.040	24
25	-.060		-.090	-.079			-.083	-.021	25
26	-.106		-.116	-.109			-.104	-.045	26

$\alpha = 0$ $\delta = -30$

1	.142		.154	.158			.152	.130	1
2	.104		.157	.157			.156	.110	2
3	.121		.155	.157			.148	.106	3
4	.106		.117	.129			.109	.063	4
5	.004		.013	.044			.045	.021	5
6	.004		-.001	.012			.016	.016	6
7	.002		-.014	.044			.192	.006	7
8	-.008		-.009	.354			.377		8
9	-.003		.293	.391			.395	.295	9
10	-.043		.295	.393			.390	.279	10
11	-.022		.294	.391			.400	.239	11
12	-.101	.099	.193	.412			.384	.172	12
13	-.103	.086	.308	.412			.394	.234	13
14	-.073	-.129	.573	.616			.573	.379	14
15	-.030	-.189	.635	.791			.736	.464	15
16	.033	-.218	.506	.735			.710	.436	16
17	.142		.159	.146			.160	.141	17
18	.117		.151	.147			.168	.170	18
19	.119		.157	.160			.160	.120	19
20	.098		.116	.125			.124	.075	20
21	.002		.011	.039			.047	.036	21
22	.007		.003	.019				.023	22
23	.003			.013			.022	.023	23
24	-.001		-.018	.008			-.008	-.004	24
25	-.003		-.026	-.016			-.005	.115	25
26	-.055		-.056	-.048			-.037	.150	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.139		.149	.158			.145	.131	1
2	.103		.155	.156			.154	.114	2
3	.117		.151	.159			.149	.103	3
4	.101		.113	.130			.107	.073	4
5	.001		.005	.039			.046	.030	5
6	.001		.002	.012			.014	.014	6
7	-.001		-.019	.008			.010	.001	7
8	-.015		-.006	-.005		-.003			8
9	-.011		-.027	.010		-.016	.009		9
10	-.051		-.037	.224			.205	.030	10
11	-.024		-.037	.304			.303	.162	11
12	-.098	.006	.258	.316			.293	.238	12
13	-.106	-.049	.363	.374			.349	.323	13
14	-.089	-.111	.402	.522			.506	.313	14
15	-.114	-.238	.352	.567			.562	.233	15
16	-.095	-.238	.297	.521			.517	.204	16
17	.140		.158	.143			.152	.131	17
18	.115		.152	.145			.157	.165	18
19	.117		.153	.159			.155	.119	19
20	.098		.115	.126			.111	.078	20
21	-.009		.005	.045			.040	.026	21
22	.001		.002	.017				.013	22
23	-.002			.013			.014	.011	23
24	-.009		-.020	.007			.004	.001	24
25	-.010		-.026	-.019		-.013	.023		25
26	-.057		-.057	-.048		-.042	-.005		26

$\alpha = 0$ $\delta = -10$

1	.140		.147	.163			.154	.134	1
2	.102		.159	.155			.159	.113	2
3	.119		.157	.155			.154	.100	3
4	.110		.119	.127			.117	.070	4
5	.004		.013	.050			.053	.025	5
6	.008		.002	.015			.019	.013	6
7	.006		-.009	.015			.014	.001	7
8	-.009		-.002	.005			.004		8
9	-.007		-.023	-.024		-.012	.000		9
10	-.039		-.045	-.045		-.054	.000		10
11	-.024		-.045	-.052		-.031	-.013		11
12	-.105	-.066	.106	.083			.085	.036	12
13	-.105	-.054	.153	.151			.133	.151	13
14	-.091	-.054	.108	.165			.158	.095	14
15	-.119	-.130	.079	.172			.163	.041	15
16	-.119	-.157	.050	.172			.163	.033	16
17	.141		.162	.146			.156	.130	17
18	.116		.158	.147			.163	.163	18
19	.121		.155	.160			.155	.109	19
20	.103		.115	.123			.121	.061	20
21	.002		.012	.042			.045	.024	21
22	.010		.007	.019				.006	22
23	.008			.012			.018	.008	23
24	.002		-.011	.008			.003	-.005	24
25	.000		-.026	-.014		-.008		-.018	25
26	-.053		-.054	-.044		-.038		-.006	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.145		.152	.162			.159	.135	1
2	.107		.160	.160			.163	.120	2
3	.118		.156	.164			.160	.114	3
4	.107		.118	.132			.120	.076	4
5	-.002		.008	.045			.058	.033	5
6	.002		.008	.017			.023	.025	6
7	.003		-.010	.015			.019	.006	7
8	-.005		-.001	.006			.005		8
9	-.005		-.023	-.024			-.013	.006	9
10	-.045		-.047	-.041			-.050	.006	10
11	-.022		-.047	-.054			-.053	-.011	11
12	-.111	-.098	-.103	-.080			-.009	-.054	12
13	-.111	-.108	-.103	-.108			-.105	-.054	13
14	-.088	-.109	-.103	-.108			-.105	-.054	14
15	-.116	-.109	-.103	-.108			-.114	-.054	15
16	-.115	-.109	-.118	-.108			-.114	-.043	16
17	.146		.157	.147			.155	.131	17
18	.115		.151	.150			.162	.160	18
19	.117		.155	.161			.156	.108	19
20	.099		.117	.123			.118	.068	20
21	.004		.007	.043			.043	.024	21
22	.009		.002	.019				.015	22
23	.004			.012			.017	.015	23
24	.001		-.017	.005			.000	-.001	24
25	-.006		-.025	-.013			-.011	.015	25
26	.055		-.054	-.047			-.041	-.011	26

$\alpha = 0$ $\delta = 10$

1	.146		.151	.164			.164	.139	1
2	.107		.161	.159			.166	.121	2
3	.119		.159	.163			.159	.114	3
4	.112		.121	.134			.117	.089	4
5	.006		.011	.052			.059	.034	5
6	.007		.007	.019			.025	.019	6
7	.008		-.007	.013			.025	.009	7
8	-.010		-.001	.009			.007		8
9	-.005		-.023	-.021			-.015	.004	9
10	-.041		-.046	-.039			-.048	.004	10
11	-.022		-.046	-.054			-.045	-.013	11
12	-.100	-.114	-.235	-.233			-.159	-.230	12
13	-.100	-.154	-.270	-.270			-.268	-.230	13
14	-.083	-.175	-.238	-.277			-.267	-.143	14
15	-.113	-.197	-.234	-.277			-.278	-.148	15
16	-.105	-.169	-.214	-.269			-.289	-.228	16
17	.138		.159	.141			.151	.126	17
18	.117		.154	.149			.160	.158	18
19	.117		.156	.158			.152	.106	19
20	.101		.112	.121			.117	.065	20
21	-.008		.012	.041			.042	.020	21
22	.013		.001	.019				.009	22
23	.007			.012			.015	.010	23
24	.001		-.015	.005			-.002	-.004	24
25	-.004		-.029	-.014			-.012	.024	25
26	-.053		-.056	-.047			-.039	-.005	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.146		.154	.167			.164	.143	1
2	.102		.164	.163			.166	.129	2
3	.120		.158	.167			.163	.116	3
4	.110		.121	.140			.119	.074	4
5	-.002		.016	.053			.062	.033	5
6	.003		.008	.020			.022	.020	6
7	.008		-.013	.018			.017	-.003	7
8	-.002		-.005	.006			.010		8
9	-.005		-.024	-.024			-.008	.005	9
10	-.046		-.051	-.043			-.048	.006	10
11	-.022		-.051	-.050			-.030	.033	11
12	-.105	-.111	-.342	-.346			-.292	-.332	12
13	-.105	-.154	-.378	-.378			-.379	-.303	13
14	-.083	-.185	-.366	-.392			-.379	-.259	14
15	-.113	-.200	-.314	-.392			-.338	-.384	15
16	-.113	-.179	-.346	-.277			-.275	-.441	16
17	.143		.154	.138			.149	.124	17
18	.113		.150	.143			.156	.164	18
19	.119		.152	.153			.149	.108	19
20	.096		.114	.118			.111	.070	20
21	.002		.007	.039			.039	.028	21
22	.005		.001	.014				.020	22
23	.003			.009			.012	.018	23
24	.000		-.015	.007			-.003	-.003	24
25	-.006		-.028	-.020			-.016	.016	25
26	-.061		-.046	.179			.114	-.004	26

$\alpha = 0$ $\delta = 30$

1	.143		.157	.170			.166	.145	1
2	.108		.167	.164			.169	.123	2
3	.121		.160	.167			.163	.115	3
4	.111		.122	.138			.121	.085	4
5	.007		.011	.052			.063	.038	5
6	.007		.011	.017			.030	.023	6
7	.008		-.006	.017			.026	.008	7
8	-.007		.000	.004			.013		8
9	-.002		-.019	-.013			-.008	.157	9
10	-.042		-.041	-.037			-.043	.144	10
11	-.020		-.041	-.046			-.029	.090	11
12	-.103	-.128	-.417	-.408			-.381	-.368	12
13	-.103	-.172	-.428	-.417			-.397	-.264	13
14	-.084	-.197	-.381	-.378			-.362	-.374	14
15	-.105	-.223	-.353	-.366			-.351	-.444	15
16	-.073	-.195	-.331	-.356			-.351	-.458	16
17	.143		.157	.139			.145	.125	17
18	.116		.145	.147			.156	.165	18
19	.122		.150	.154			.145	.106	19
20	.098		.111	.120			.109	.070	20
21	.003		.012	.043			.038	.033	21
22	.007		.002	.013				.019	22
23	.005			.267			.345	.104	23
24	-.002		.010	.380			.384	.260	24
25	.001		.307	.397			.397	.300	25
26	-.054		.299	.397			.397	.289	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.047		.049	.060			.054	.029	1
2	.028		.057	.059			.061	.045	2
3	.044		.051	.052			.058	.050	3
4	.028		.037	.032			.019	.028	4
5	-.067		-.058	-.039		-	.031	.000	5
6	-.066		-.066	-.063		-	.063	- .014	6
7	-.058		-.068	-.068		-	.057	- .048	7
8	-.073		-.073	-.073		-	.073		8
9	-.073		-.086	-.092		-	.078	- .056	9
10	-.103		-.105	-.114		-	.109	- .074	10
11	-.090		-.105	-.123		-	.096	- .088	11
12	-.162	- .182	-.163	-.149		-	.088	- .101	12
13	-.162	- .194	-.173	-.173		-	.164	- .159	13
14	-.148	- .188	-.172	-.173		-	.153	- .138	14
15	-.169	- .188	-.172	-.173		-	.160	- .170	15
16	-.168	- .188	-.172	-.173		-	.160	- .178	16
17	.240		.302	.283			.299	.240	17
18	.199		.291	.281			.288	.240	18
19	.200		.274	.297			.298	.167	19
20	.185		.209	.251			.246	.109	20
21	.081		.091	.151			.165	.049	21
22	.078		.079	.106				.023	22
23	.080			.096			.118	.015	23
24	.079		.064	.083			.096	- .013	24
25	.075		.052	.067			.077	.019	25
26	.012		.025	.037			.038	- .010	26

$\alpha = 6$ $\delta = -30$

1	-.047		-.053	-.048		-	.052	- .035	1
2	-.043		-.048	-.039		-	.043	- .005	2
3	-.031		-.049	-.048		-	.047	.008	3
4	-.048		-.064	-.067		-	.078	- .019	4
5	-.131		-.139	-.126		-	.123	- .069	5
6	-.124		-.141	-.143		-	.144	- .129	6
7	-.127		-.140	-.145		-	.116	- .172	7
8	-.142		-.136	-.115			.158		8
9	-.129		-.046	-.087			.180	- .185	9
10	-.158		-.106	-.170			.180	- .031	10
11	-.153		-.106	-.170			.204	- .011	11
12	-.200	- .065	-.083	-.197			.205	.015	12
13	-.200	- .065	-.146	-.184			.195	.115	13
14	-.192	- .204	-.394	-.329			.332	.432	14
15	-.192	- .270	-.434	-.464			.476	.383	15
16	-.059	- .290	-.362	-.482			.502	.431	16
17	.355		.508	.520			.529	.434	17
18	.302		.450	.506			.531	.384	18
19	.311		.397	.462			.502	.274	19
20	.276		.316	.368			.403	.197	20
21	.165		.184	.244			.290	.110	21
22	.167		.169	.206				.061	22
23	.167			.196			.198	.033	23
24	.164		.155	.186			.169	.003	24
25	.158		.144	.163			.152	.028	25
26	.085		.111	.126			.107	- .010	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.047		-.054	-.045			-.053	-.054	1
2	-.043		-.047	-.042			-.041	-.013	2
3	-.032		-.052	-.045			-.046	-.001	3
4	-.041		-.065	-.065			-.079	-.034	4
5	-.128		-.138	-.122			-.121	-.080	5
6	-.131		-.140	-.147			-.142	-.133	6
7	-.130		-.140	-.147			-.146	-.175	7
8	-.135		-.135	-.154			-.147		8
9	-.130		-.151	-.079			-.115	-.204	9
10	-.158		-.133	-.051			.033	-.204	10
11	-.148		-.133	.088			.138	-.184	11
12	-.200	-.106	.079	.104			.125	-.048	12
13	-.209	-.160	.178	.145			.180	.174	13
14	-.200	-.200	.214	.273			.323	-.005	14
15	-.217	-.255	.175	.310			.364	-.046	15
16	-.205	-.278	.139	.310			.347	.040	16
17	.351		.505	.514			.528	.421	17
18	.307		.447	.505			.532	.378	18
19	.315		.398	.459			.503	.269	19
20	.286		.319	.368			.404	.187	20
21	.163		.182	.241			.292	.094	21
22	.175		.169	.207				.049	22
23	.167			.195			.201	.025	23
24	.164		.150	.184			.175	-.010	24
25	.159		.144	.163			.151	.029	25
26	.091		.108	.127			.110	-.019	26

$\alpha = 6$ $\delta = -10$

1	-.052		-.057	-.043			-.049	-.043	1
2	-.039		-.048	-.045			-.041	-.014	2
3	-.031		-.046	-.045			-.047	.006	3
4	-.044		-.068	-.065			-.077	-.030	4
5	-.127		-.139	-.120			-.125	-.075	5
6	-.128		-.139	-.143			-.143	-.125	6
7	-.125		-.143	-.151			-.148	-.177	7
8	-.134		-.138	-.153			-.157		8
9	-.129		-.152	-.169			-.149	-.200	9
10	-.160		-.167	-.187			-.163	-.224	10
11	-.148		-.166	-.186			-.124	-.239	11
12	-.213	-.210	-.053	-.071			-.053	-.165	12
13	-.213	-.205	-.021	-.033			-.001	-.089	13
14	-.202	-.205	-.046	-.020			.024	-.169	14
15	-.217	-.205	-.060	-.009			.034	-.245	15
16	-.217	-.239	-.075	-.005			.048	-.219	16
17	.357		.503	.509			.518	.417	17
18	.306		.446	.500			.525	.362	18
19	.309		.395	.461			.495	.277	19
20	.285		.312	.366			.397	.190	20
21	.164		.185	.242			.282	.104	21
22	.173		.169	.202				.055	22
23	.168			.195			.197	.026	23
24	.162		.153	.183			.165	-.003	24
25	.159		.144	.161			.146	.016	25
26	.092		.109	.123			.102	-.018	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .049		- .051	- .040			- .048	- .041	1
2	- .039		- .044	- .040			- .040	- .006	2
3	- .027		- .041	- .045			- .041	- .006	3
4	- .039		- .065	- .062			- .076	- .023	4
5	- .126		- .134	- .120			- .118	- .066	5
6	- .123		- .135	- .149			- .142	- .123	6
7	- .122		- .141	- .144			- .143	- .165	7
8	- .132		- .132	- .150			- .154		8
9	- .128		- .151	- .173			- .147	- .194	9
10	- .155		- .165	- .189			- .163	- .208	10
11	- .148		- .165	- .195			- .141	- .227	11
12	- .207	- .218	- .214	- .210			- .153	- .222	12
13	- .208	- .230	- .219	- .237			- .220	- .242	13
14	- .199	- .222	- .219	- .237			- .202	- .227	14
15	- .214	- .222	- .219	- .237			- .202	- .213	15
16	- .214	- .218	- .219	- .237			- .202	- .240	16
17	.356		.503	.511			.516	.409	17
18	.309		.447	.503			.521	.369	18
19	.313		.398	.458			.490	.265	19
20	.289		.317	.360			.392	.192	20
21	.169		.183	.244			.284	.106	21
22	.177		.168	.201				.055	22
23	.169			.192			.194	.024	23
24	.167		.155	.184			.167	- .004	24
25	.165		.146	.159			.146	.023	25
26	.094		.108	.125			.100	- .028	26

$\alpha = 6$ $\delta = 10$

1	- .052		- .050	- .044			- .045	- .031	1
2	- .039		- .043	- .040			- .034	.000	2
3	- .028		- .049	- .044			- .039	.011	3
4	- .044		- .067	- .065			- .074	- .011	4
5	- .129		- .139	- .122			- .116	- .056	5
6	- .129		- .136.	- .147			- .139	- .110	6
7	- .127		- .142	- .145			- .142	- .158	7
8	- .137		- .135	- .149			- .148		8
9	- .128		- .152	- .172			- .143	- .188	9
10	- .156		- .165	- .181			- .162	- .202	10
11	- .150		- .165	- .188			- .132	- .219	11
12	- .202	- .224	- .303	- .304			- .249	- .304	12
13	- .209	- .248	- .333	- .347			- .332	- .321	13
14	- .192	- .260	- .324	- .354			- .316	- .308	14
15	- .210	- .273	- .299	- .354			- .328	- .342	15
16	- .202	- .233	- .187	- .249			- .294	- .342	16
17	.351		.502	.504			.515	.413	17
18	.304		.443	.499			.520	.363	18
19	.312		.395	.459			.495	.278	19
20	.286		.315	.364			.395	.189	20
21	.160		.184	.240			.287	.103	21
22	.177		.168	.202				.066	22
23	.166			.189			.193	.035	23
24	.161		.153	.182			.163	- .003	24
25	.159		.143	.157			.141	.031	25
26	.085		.107	.122			.103	- .011	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.055		-.054	-.039			-.045	-.031	1
2	-.044		-.049	-.039			-.036	-.006	2
3	-.033		-.050	-.041			-.036	.009	3
4	-.045		-.070	-.065			-.074	-.014	4
5	-.133		-.144	-.121			-.117	-.065	5
6	-.129		-.138	-.146			-.139	-.114	6
7	-.127		-.141	-.145			-.142	-.167	7
8	-.136		-.136	-.149			-.149		8
9	-.130		-.157	-.164			-.141	-.184	9
10	-.160		-.164	-.181			-.161	-.197	10
11	-.152		-.165	-.184			-.124	-.135	11
12	-.209	-.230	-.381	-.378			-.337	-.369	12
13	-.209	-.265	-.408	-.411			-.409	-.369	13
14	-.190	-.280	-.391	-.368			-.408	-.402	14
15	-.213	-.292	-.292	-.352			-.399	-.421	15
16	-.119	-.243	-.344	-.316			-.304	-.414	16
17	.355		.499	.505			.503	.391	17
18	.305		.440	.489			.510	.363	18
19	.309		.388	.456			.485	.265	19
20	.285		.312	.358			.388	.192	20
21	.167		.183	.236			.273	.100	21
22	.170		.165	.198				.055	22
23	.166			.189			.188	.020	23
24	.164		.151	.180			.159	-.009	24
25	.159		.138	.291			.158	.034	25
26	.091		.376	.527			.510	.200	26

$\alpha=6$ $\delta=30$

1	-.051		-.052	-.040			-.043	-.041	1
2	-.043		-.045	-.038			-.033	-.004	2
3	-.030		-.049	-.042			-.039	.013	3
4	-.042		-.066	-.065			-.068	-.016	4
5	-.125		-.134	-.120			-.114	-.054	5
6	-.125		-.136	-.140			-.137	-.105	6
7	-.124		-.138	-.143			-.140	-.143	7
8	-.136		-.133	-.152			-.148		8
9	-.126		-.152	-.163			-.139	-.059	9
10	-.161		-.164	-.179			-.159	-.126	10
11	-.149		-.161	-.185			-.121	-.180	11
12	-.199	-.227	-.411	-.383			-.407	-.437	12
13	-.209	-.263	-.403	-.383			-.421	-.437	13
14	-.192	-.279	-.384	-.363			-.389	-.437	14
15	-.207	-.258	-.352	-.366			-.382	-.428	15
16	-.026	-.237	-.368	-.366			-.376	-.411	16
17	.352		.503	.498			.502	.388	17
18	.305		.442	.495			.511	.356	18
19	.299		.391	.453			.482	.268	19
20	.281		.314	.357			.386	.182	20
21	.166		.181	.232			.274	.098	21
22	.172		.166	.200				.048	22
23	.166			.607			.620	.321	23
24	.162		.464	.634			.658	.297	24
25	.159		.533	.651			.671	.357	25
26	.092		.509	.648			.668	.328	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.122		-.133	-.130			-.136	-.134	1
2	-.108		-.123	-.119			-.121	-.059	2
3	-.091		-.128	-.120			-.117	-.074	3
4	-.112		-.138	-.142			-.149	-.111	4
5	-.182		-.207	-.193			-.185	-.163	5
6	-.176		-.204	-.210			-.207	-.257	6
7	-.179		-.202	-.212			-.209	-.285	7
8	-.193		-.194	-.214			-.217		8
9	-.177		-.204	-.228			-.200	-.302	9
10	-.204		-.214	-.246			-.212	-.305	10
11	-.199		-.214	-.247			-.174	-.297	11
12	-.240	-.249	-.242	-.255			-.197	-.283	12
13	-.240	-.260	-.252	-.282			-.247	-.308	13
14	-.240	-.253	-.262	-.280			-.234	-.298	14
15	-.255	-.254	-.262	-.280			-.243	-.304	15
16	-.229	-.224	-.238	-.280			-.243	-.283	16
17	.481		.721	.780			.824	.630	17
18	.422		.582	.668			.739	.510	18
19	.437		.519	.599			.645	.371	19
20	.397		.439	.475			.502	.260	20
21	.263		.273	.333			.371	.153	21
22	.267		.263	.292				.104	22
23	.264			.284			.272	.061	23
24	.257		.252	.273			.243	.030	24
25	.254		.245	.251			.225	.060	25
26	.175		.198	.212			.174	.006	26

$\alpha = 12$ $\delta = -30$

1	-.204		-.244	-.255			-.264	-.247	1
2	-.159		-.195	-.204			-.221	-.153	2
3	-.145		-.207	-.203			-.200	-.155	3
4	-.164		-.207	-.215			-.221	-.220	4
5	-.225		-.268	-.259			-.248	-.265	5
6	-.221		-.271	-.269			-.273	-.336	6
7	-.228		-.265	-.270			-.272	-.372	7
8	-.237		-.252	-.088			-.109		8
9	-.226		-.084	-.071			-.037	-.362	9
10	-.246		-.054	-.026			-.033	-.339	10
11	-.248		-.055	-.025			-.004	-.239	11
12	-.270	-.174	-.040	.005			.014	-.194	12
13	-.285	-.197	-.040	-.011			.000	-.134	13
14	-.268	-.279	.170	.091			.169	-.059	14
15	-.284	-.343	.248	.198			.348	-.148	15
16	-.108	-.342	.203	.222			.406	-.235	16
17	.617		.902	.971			.998	.754	17
18	.559		.740	.832			.885	.598	18
19	.574		.662	.732			.765	.448	19
20	.522		.528	.565			.605	.337	20
21	.359		.357	.424			.458	.205	21
22	.378		.361	.395				.153	22
23	.355			.392			.363	.120	23
24	.355		.355	.380			.338	.090	24
25	.347		.343	.358			.314	.118	25
26	.258		.291	.308			.262	.068	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.212		-.244	-.254			-.269	-.252	1
2	-.168		-.203	-.208			-.225	-.158	2
3	-.148		-.205	-.205			-.203	-.157	3
4	-.164		-.217	-.216			-.222	-.219	4
5	-.232		-.271	-.262			-.254	-.269	5
6	-.220		-.273	-.276			-.276	-.348	6
7	-.233		-.269	-.272			-.276	-.382	7
8	-.241		-.255	-.269			-.258		8
9	-.224		-.245	-.222			-.230	-.372	9
10	-.247		-.225	-.238			-.133	-.354	10
11	-.249		-.225	-.102			-.026	-.298	11
12	-.269	-.207	-.056	-.059			-.024	-.234	12
13	-.282	-.248	.001	-.039			.004	-.193	13
14	-.265	-.257	.071	.056			.118	-.185	14
15	-.279	-.310	.043	.083			.164	-.247	15
16	-.163	-.339	.009	.091			.164	-.269	16
17	.615		.898	.967			.994	.747	17
18	.556		.739	.829			.880	.606	18
19	.568		.659	.724			.761	.456	19
20	.515		.523	.567			.598	.351	20
21	.359		.356	.418			.458	.213	21
22	.374		.360	.396				.149	22
23	.354			.390			.358	.119	23
24	.351		.354	.376			.332	.086	24
25	.344		.347	.354			.312	.119	25
26	.256		.293	.308			.260	.059	26

α=12 δ=-10

1	-.207		-.240	-.255			-.263	-.258	1
2	-.162		-.205	-.205			-.219	-.158	2
3	-.153		-.205	-.204			-.199	-.160	3
4	-.163		-.218	-.219			-.219	-.227	4
5	-.226		-.268	-.263			-.252	-.279	5
6	-.225		-.273	-.276			-.278	-.361	6
7	-.232		-.269	-.274			-.275	-.384	7
8	-.241		-.257	-.279			-.277		8
9	-.227		-.255	-.282			-.259	-.384	9
10	-.251		-.257	-.300			-.257	-.372	10
11	-.250		-.257	-.286			-.161	-.341	11
12	-.274	-.277	-.160	-.183			-.136	-.280	12
13	-.284	-.268	-.143	-.177			-.124	-.277	13
14	-.275	-.269	-.155	-.172			-.103	-.303	14
15	-.290	-.228	-.167	-.165			-.103	-.333	15
16	-.182	-.305	-.172	-.160			-.103	-.318	16
17	.613		.897	.967			.989	.744	17
18	.559		.735	.826			.885	.600	18
19	.566		.658	.725			.761	.453	19
20	.514		.522	.566			.596	.343	20
21	.358		.356	.419			.456	.203	21
22	.368		.357	.390				.146	22
23	.353			.387			.356	.121	23
24	.353		.353	.375			.330	.083	24
25	.345		.342	.355			.309	.114	25
26	.257		.286	.307			.257	.053	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.186		-.228	-.244			-.256	-.243	1
2	-.156		.270	-.198			-.210	-.141	2
3	-.142		-.193	-.198			-.199	-.153	3
4	-.160		-.206	-.211			-.212	-.214	4
5	-.217		-.261	-.253			-.249	-.263	5
6	-.086		-.270	-.248			-.225	-.329	6
7	-.158		-.228	-.263			-.253	-.362	7
8	-.227		-.251	-.273			-.275		8
9	-.217		-.250	-.193			-.257	-.359	9
10	-.240		-.250	-.295			-.271	-.359	10
11	-.240		-.251	-.306			-.209	-.343	11
12	-.278	-.305	-.284	-.316			-.244	-.357	12
13	-.288	-.310	-.297	-.337			-.295	-.373	13
14	-.275	-.303	-.303	-.337			-.280	-.371	14
15	-.292	-.307	-.302	-.334			-.289	-.371	15
16	-.207	-.194	-.208	-.298			-.287	-.351	16
17	.619		.887	.954			.974	.730	17
18	.548		.722	.808			.848	.580	18
19	.560		.653	.710			.745	.438	19
20	.509		.511	.550			.585	.316	20
21	.354		.349	.409			.439	.177	21
22	.360		.349	.373				.129	22
23	.343			.370			.345	.103	23
24	.345		.344	.356			.318	.071	24
25	.342		.325	.337			.289	.095	25
26	.249		.275	.297			.230	.045	26

$\alpha = 12$ $\delta = 0$

1	-.204		-.234	-.252			-.256	-.260	1
2	-.159		-.196	-.204			-.216	-.162	2
3	-.150		-.206	-.197			-.195	-.162	3
4	-.161		-.212	-.216			-.218	-.224	4
5	-.223		-.270	-.253			-.247	-.280	5
6	-.223		-.266	-.271			-.271	-.348	6
7	-.225		-.262	-.273			-.269	-.383	7
8	-.236		-.249	-.275			-.274		8
9	-.229		-.252	-.290			-.255	-.384	9
10	-.247		-.254	-.299			-.260	-.381	10
11	-.246		-.254	-.302			-.206	-.348	11
12	-.269	-.290	-.282	-.302			-.239	-.341	12
13	-.282	-.300	-.290	-.326			-.292	-.356	13
14	-.267	-.293	-.307	-.326			-.275	-.356	14
15	-.207	-.293	-.300	-.326			-.285	-.371	15
16	-.193	-.184	-.192	-.293			-.285	-.342	16
17	.617		.893	.969			.992	.741	17
18	.559		.739	.824			.878	.593	18
19	.568		.658	.727			.756	.439	19
20	.514		.525	.568			.594	.346	20
21	.355		.354	.421			.455	.204	21
22	.376		.361	.393				.143	22
23	.352			.389			.354	.111	23
24	.353		.354	.375			.332	.076	24
25	.341		.338	.354			.311	.110	25
26	.254		.286	.305			.258	.055	26

TABLE IV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.203		-.242	-.251			-.256	-.248	1
2	-.153		-.199	-.203			-.215	-.149	2
3	-.143		-.204	-.199			-.194	-.148	3
4	-.161		-.215	-.213			-.210	-.207	4
5	-.233		-.273	-.254			-.245	-.263	5
6	-.223		-.273	-.268			-.266	-.341	6
7	-.226		-.273	-.270			-.266	-.371	7
8	-.234		-.249	-.273			-.274		8
9	-.224		-.254	-.285			-.255	-.369	9
10	-.249		-.257	-.297			-.265	-.368	10
11	-.243		-.256	-.303			-.213	-.336	11
12	-.263	-.298	-.349	-.367			-.309	-.396	12
13	-.274	-.326	-.367	-.394			-.373	-.403	13
14	-.268	-.326	-.367	-.408			-.362	-.409	14
15	-.275	-.326	-.274	-.316			-.369	-.411	15
16	-.134	-.250	-.229	-.269			-.272	-.411	16
17	.616		.890	.959			.984	.736	17
18	.558		.733	.822			.872	.595	18
19	.571		.656	.719			.757	.448	19
20	.508		.526	.559			.588	.338	20
21	.360		.355	.415			.454	.204	21
22	.378		.358	.395				.133	22
23	.345			.386			.357	.113	23
24	.347		.351	.370			.322	.079	24
25	.352		.338	.351			.303	.106	25
26	.258		.284	.307			.252	.058	26

α= 12 δ= 20

1	-.203		-.237	-.253			-.254	-.253	1
2	-.156		-.203	-.208			-.211	-.157	2
3	-.143		-.210	-.202			-.195	-.157	3
4	-.157		-.210	-.214			-.217	-.214	4
5	-.229		-.265	-.255			-.247	-.263	5
6	-.222		-.269	-.273			-.270	-.347	6
7	-.226		-.269	-.269			-.270	-.377	7
8	-.236		-.252	-.276			-.272		8
9	-.222		-.252	-.281			-.253	-.363	9
10	-.246		-.252	-.299			-.260	-.336	10
11	-.246		-.252	-.303			-.203	-.287	11
12	-.274	-.298	-.407	-.411			-.387	-.426	12
13	-.282	-.323	-.429	-.392			-.416	-.441	13
14	-.278	-.334	-.376	-.363			-.416	-.443	14
15	-.287	-.318	-.338	-.361			-.377	-.443	15
16	-.110	-.250	-.391	-.348			-.329	-.422	16
17	.619		.891	.955			.984	.729	17
18	.551		.737	.817			.868	.582	18
19	.560		.658	.723			.748	.428	19
20	.510		.517	.554			.592	.332	20
21	.355		.349	.416			.451	.194	21
22	.371		.355	.388				.128	22
23	.350			.379			.353	.105	23
24	.350		.348	.593			.609	.138	24
25	.342		.493	.788			.765	.354	25
26	.257		.702	.850			.838	.428	26

TABLE IV.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.242		-.315	-.321			-.338	-.326	1
2	-.196		-.249	-.256			-.290	-.222	2
3	-.189		-.245	-.250			-.257	-.220	3
4	-.193		-.248	-.263			-.272	-.268	4
5	-.256		-.305	-.298			-.292	-.319	5
6	-.236		-.305	-.303			-.309	-.369	6
7	-.248		-.305	-.303			-.309	-.398	7
8	-.264		-.299	-.312			-.317		8
9	-.252		-.289	-.312			-.302	-.381	9
10	-.280		-.278	-.327			-.302	-.364	10
11	-.280		-.278	-.337			-.245	-.349	11
12	-.293	-.323	-.302	-.336			-.275	-.389	12
13	-.293	-.323	-.321	-.354			-.321	-.408	13
14	-.294	-.323	-.321	-.358			-.302	-.418	14
15	-.308	-.322	-.321	-.358			-.314	-.407	15
16	-.163	-.180	-.170	-.237			-.303	-.389	16
17	.755		1.033	1.070			1.076	.808	17
18	.677		.850	.917			.958	.665	18
19	.709		.753	.804			.828	.501	19
20	.591		.590	.632			.671	.392	20
21	.437		.427	.490			.521	.252	21
22	.484		.475	.506				.212	22
23	.476			.521			.451	.179	23
24	.489		.507	.506			.428	.144	24
25	.473		.476	.481			.409	.175	25
26	.389		.403	.411			.347	.129	26

α=15 δ=0

1	-.257		-.335	-.337			-.367	-.343	1
2	-.216		.096	-.287			-.297	-.230	2
3	-.195		-.259	-.263			-.271	-.233	3
4	-.209		-.271	-.273			-.283	-.285	4
5	-.261		-.316	-.313			-.299	-.334	5
6	-.234		-.325	-.313			-.298	-.383	6
7	-.253		-.314	-.316			-.314	-.412	7
8	-.272		-.308	-.325			-.325		8
9	-.263		-.301	-.311			-.302	-.412	9
10	-.282		-.296	-.335			-.304	-.394	10
11	-.285		-.297	-.344			-.246	-.378	11
12	-.295	-.332	-.317	-.346			-.288	-.409	12
13	-.309	-.343	-.329	-.367			-.321	-.419	13
14	-.307	-.336	-.334	-.371			-.314	-.427	14
15	-.316	-.336	-.327	-.372			-.322	-.422	15
16	-.175	-.188	-.187	-.249			-.309	-.406	16
17	.754		1.022	1.066			1.071	.813	17
18	.671		.849	.918			.957	.654	18
19	.708		.751	.801			.829	.492	19
20	.591		.584	.629			.666	.384	20
21	.427		.418	.485			.518	.240	21
22	.477		.467	.505				.202	22
23	.462			.520			.453	.178	23
24	.483		.505	.501			.427	.140	24
25	.470		.461	.478			.406	.160	25
26	.367		.390	.402			.332	.111	26

TABLE V

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-15 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.773		1.042	1.088			1.074	.858	1
2	.682		.866	.939			.973	.671	2
3	.714		.769	.824			.846	.530	3
4	.614		.618	.658			.679	.377	4
5	.449		.431	.507			.548	.269	5
6	.491		.501	.529			.506	.182	6
7	.495		.503	.544			.485	.168	7
8	.497		.524	.542			.458	.134	8
9	.480		.504	.487			.402	.134	9
10	.659		.700	.686			.446	.134	10
11	.774		.793	.777			.653	.113	11
12	.907		.905	.896			.799	.374	12
13	.888		.880	.869			.778	.374	13
14	.829		.817	.803			.716	.343	14
15	.762		.766	.736			.676	.346	15
16	.639		.657	.652			.600	.314	16
17	-.262		-.334	-.367			-.370	-.355	17
18	-.210		-.274	-.291			-.305	-.227	18
19	-.193		-.263	-.265			-.271	-.248	19
20	-.215		-.266	-.271			-.277	-.277	20
21	-.264		-.322	-.303			-.305	-.340	21
22	-.260		-.322	-.317				-.395	22
23	-.265			-.319			-.317	-.403	23
24	-.267		-.308	-.321			-.323	-.418	24
25	-.270		-.298	-.327			-.311	-.401	25
26	-.297		-.309	-.337			-.301	-.399	26
27								-.399	27

α=-15 δ= 0

1	.775		1.043	1.086			1.072	.875	1
2	.693		.866	.937			.974	.689	2
3	.720		.774	.823			.845	.541	3
4	.617		.620	.655			.677	.387	4
5	.448		.436	.505			.544	.272	5
6	.494		.500	.529			.503	.189	6
7	.484		.501	.544			.483	.186	7
8	.500		.526	.539			.447	.144	8
9	.470		.485	.458			.405	.150	9
10	.396		.406	.420			.347	.142	10
11	.399		.353	.362			.283	.106	11
12	.326		.322	.327			.243	.005	12
13	.301		.295	.291			.212	.002	13
14	.309		.293	.289			.228	.002	14
15	.309		.293	.290			.215	.002	15
16	.293		.295	.280			.206	-.017	16
17	-.261		-.335	-.368			-.374	-.338	17
18	-.206		-.277	-.294			-.305	-.224	18
19	-.193		-.265	-.272			-.278	-.245	19
20	-.212		-.267	-.277			-.278	-.275	20
21	-.265		-.322	-.308			-.310	-.329	21
22	-.258		-.326	-.322				-.380	22
23	-.263			-.324			-.323	-.398	23
24	-.266		-.310	-.328			-.324	-.413	24
25	-.270		-.301	-.332			-.313	-.385	25
26	-.298		-.313	-.340			-.305	-.396	26
27								-.396	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -15$ $\delta = 10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.780		1.046	1.090			1.073	.877	1
2	.685		.870	.939			.975	.692	2
3	.720		.775	.827			.843	.546	3
4	.620		.621	.657			.681	.388	4
5	.456		.441	.506			.552	.287	5
6	.490		.503	.536			.513	.201	6
7	.508		.510	.548			.487	.175	7
8	.503		.535	.543			.449	.129	8
9	.478		.487	.462			.410	.159	9
10	.399		.410	.422			.351	.145	10
11	.398		.356	.365			.284	.105	11
12	.025		.015	.023			-.035	-.181	12
13	.002		-.004	-.007			-.058	-.197	13
14	.007		-.009	-.017			-.047	-.184	14
15	.007		-.007	-.017			-.057	-.185	15
16	-.007		-.007	-.017			-.057	-.205	16
17	-.260		-.329	-.373			-.378	-.351	17
18	-.206		-.277	-.293			-.314	-.222	18
19	-.190		-.266	-.270			-.276	-.252	19
20	-.211		-.266	-.278			-.284	-.272	20
21	-.263		-.319	-.306			-.314	-.319	21
22	-.257		-.325	-.320				-.386	22
23	-.263			-.324			-.323	-.401	23
24	-.267		-.311	-.327			-.328	-.416	24
25	-.266		-.300	-.331			-.316	-.401	25
26	-.297		-.313	-.345			-.312	-.401	26
27								-.401	27

$\alpha = -15$ $\delta = 20$

1	.785		1.050	1.094			1.075	.885	1
2	.696		.873	.943			.975	.695	2
3	.725		.779	.829			.843	.557	3
4	.621		.624	.665			.680	.406	4
5	.459		.442	.513			.553	.289	5
6	.501		.508	.542			.513	.202	6
7	.509		.513	.552			.491	.191	7
8	.504		.538	.543			.447	.138	8
9	.479		.492	.465			.413	.160	9
10	.408		.413	.425			.353	.150	10
11	.410		.359	.368			.287	.112	11
12	-.164		-.178	-.168			-.206	-.311	12
13	-.201		-.195	-.194			-.237	-.338	13
14	-.170		-.201	-.202			-.232	-.321	14
15	-.202		-.200	-.208			-.231	-.322	15
16	-.200		-.200	-.205			-.223	-.323	16
17	-.259		-.331	-.380			-.382	-.343	17
18	-.203		-.275	-.301			-.317	-.222	18
19	-.187		-.264	-.274			-.283	-.242	19
20	-.205		-.265	-.281			-.287	-.274	20
21	-.259		-.319	-.311			-.315	-.327	21
22	-.252		-.321	-.324				-.379	22
23	-.258			-.327			-.327	-.396	23
24	-.263		-.308	-.330			-.337	-.412	24
25	-.267		-.298	-.334			-.325	-.401	25
26	-.293		-.242	-.347			-.263	-.401	26
27								-.401	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-15 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.781		1.048	1.091			1.079	.874	1
2	.686		.871	.944			.981	.686	2
3	.722		.777	.829			.848	.547	3
4	.621		.626	.663			.684	.392	4
5	.447		.438	.512			.556	.282	5
6	.495		.506	.542			.519	.206	6
7	.501		.512	.555			.494	.168	7
8	.503		.539	.544			.452	.144	8
9	.477		.491	.465			.417	.168	9
10	.404		.414	.426			.356	.149	10
11	.413		.357	.373			.293	.118	11
12	-.243		-.254	-.248			-.279	-.351	12
13	-.284		-.271	-.268			-.298	-.376	13
14	-.254		-.286	-.281			-.295	-.350	14
15	-.286		-.286	-.290			-.296	-.360	15
16	-.268		-.272	-.282			-.305	-.356	16
17	-.264		-.333	-.376			-.384	-.359	17
18	-.207		-.277	-.298			-.314	-.234	18
19	-.191		-.264	-.273			-.283	-.259	19
20	-.211		-.265	-.279			-.286	-.280	20
21	-.264		-.320	-.308			-.314	-.348	21
22	-.257		-.323	-.323				-.390	22
23	-.264			-.324			-.328	-.406	23
24	-.267		-.315	-.326			-.335	-.428	24
25	-.268		-.204	-.264			-.319	-.407	25
26	-.125		-.097	-.140			-.120	-.398	26
27								-.399	27

α=-12 δ=-20

1	.606		.865	.942			.946	.772	1
2	.531		.712	.805			.852	.599	2
3	.548		.642	.710			.739	.464	3
4	.500		.522	.556			.576	.314	4
5	.350		.331	.405			.446	.199	5
6	.353		.339	.366			.374	.122	6
7	.394		.491	.647			.424	.081	7
8	.707		.740	.784			.663	.179	8
9	.799		.818	.811			.783	.383	9
10	.845		.858	.906			.847	.441	10
11	.863		.877	.923			.879	.399	11
12	.915		.936	.968			.938	.471	12
13	.972		.968	1.002			.961	.545	13
14	1.038		1.036	1.023			.961	.602	14
15	.963		.964	.951			.880	.535	15
16	.742		.767	.769			.762	.454	16
17	-.191		-.214	-.238			-.244	-.200	17
18	-.144		-.192	-.200			-.205	-.101	18
19	-.137		-.191	-.190			-.187	-.129	19
20	-.161		-.201	-.204			-.206	-.178	20
21	-.219		-.260	-.248			-.245	-.218	21
22	-.213		-.265	-.262				-.293	22
23	-.216			-.268			-.264	-.317	23
24	-.222		-.247	-.271			-.271	-.363	24
25	-.218		-.248	-.277			-.255	-.330	25
26	-.255		-.264	-.288			-.255	-.311	26
27								-.311	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.613		.869	.945			.950	.773	1
2	.538		.717	.806			.858	.598	2
3	.556		.646	.711			.740	.456	3
4	.509		.524	.556			.582	.307	4
5	.354		.337	.410			.445	.207	5
6	.357		.343	.372			.377	.115	6
7	.350		.343	.370			.346	.091	7
8	.337		.343	.364			.317	.053	8
9	.325		.322	.316			.276	.076	9
10	.261		.266	.283			.224	.058	10
11	.330		.245	.273			.197	.033	11
12	.561		.600	.562			.499	.197	12
13	.572		.600	.592			.485	.210	13
14	.592		.600	.583			.478	.182	14
15	.592		.600	.550			.466	.190	15
16	.531		.541	.519			.448	.176	16
17	-.191		-.220	-.241			-.248	-.215	17
18	-.143		-.191	-.198			-.205	-.120	18
19	-.136		-.188	-.191			-.188	-.129	19
20	-.162		-.203	-.202			-.207	-.179	20
21	-.219		-.264	-.246			-.247	-.233	21
22	-.211		-.269	-.263				-.297	22
23	-.218			-.268			-.264	-.324	23
24	-.221		-.252	-.269			-.271	-.365	24
25	-.223		-.252	-.277			-.257	-.338	25
26	-.255		-.267	-.291			-.254	-.355	26
27								-.354	27

α=-12 δ= 0

1	.618		.871	.950			.950	.784	1
2	.524		.720	.810			.857	.600	2
3	.554		.647	.711			.738	.465	3
4	.514		.525	.557			.578	.322	4
5	.358		.339	.409			.443	.216	5
6	.365		.346	.372			.373	.123	6
7	.354		.348	.369			.340	.089	7
8	.342		.347	.365			.308	.064	8
9	.327		.325	.314			.269	.075	9
10	.261		.269	.283			.223	.074	10
11	.276		.230	.243			.181	.033	11
12	.202		.191	.216			.144	-.053	12
13	.184		.179	.185			.120	-.073	13
14	.185		.179	.180			.133	-.060	14
15	.180		.179	.180			.121	-.062	15
16	.180		.180	.173			.116	-.076	16
17	-.187		-.218	-.246			-.259	-.213	17
18	-.141		-.191	-.204			-.215	-.105	18
19	-.133		-.191	-.194			-.197	-.122	19
20	-.155		-.199	-.207			-.213	-.180	20
21	-.213		-.261	-.252			-.255	-.234	21
22	-.209		-.264	-.265				-.312	22
23	-.214			-.273			-.274	-.329	23
24	-.220		-.247	-.275			-.282	-.355	24
25	-.218		-.247	-.280			-.266	-.344	25
26	-.251		-.264	-.294			-.264	-.359	26
27								-.359	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.603		.865	.950			.954	.772	1
2	.520		.712	.808			.860	.592	2
3	.549		.639	.713			.741	.466	3
4	.500		.523	.561			.586	.301	4
5	.347		.335	.410			.447	.199	5
6	.353		.341	.375			.377	.121	6
7	.346		.343	.370			.354	.092	7
8	.333		.348	.369			.320	.062	8
9	.314		.324	.320			.282	.070	9
10	.249		.268	.286			.234	.070	10
11	.263		.227	.248			.189	.025	11
12	-.057		-.058	-.047			-.090	-.222	12
13	-.070		-.072	-.088			-.106	-.233	13
14	-.070		-.089	-.086			-.109	-.218	14
15	-.081		-.089	-.089			-.126	-.219	15
16	-.084		-.089	-.089			-.127	-.218	16
17	-.200		-.219	-.243			-.252	-.217	17
18	-.150		-.198	-.201			-.208	-.117	18
19	-.142		-.194	-.193			-.193	-.141	19
20	-.165		-.205	-.208			-.213	-.180	20
21	-.224		-.264	-.249			-.248	-.245	21
22	-.217		-.267	-.264				-.327	22
23	-.222			-.269			-.267	-.334	23
24	-.226		-.249	-.271			-.276	-.361	24
25	-.227		-.248	-.278			-.264	-.342	25
26	-.261		-.267	-.293			-.260	-.361	26
27								-.360	27

α=-12 δ=20

1	.610		.866	.947			.957	.779	1
2	.526		.716	.807			.864	.609	2
3	.553		.643	.710			.744	.472	3
4	.509		.526	.563			.586	.322	4
5	.350		.336	.408			.449	.211	5
6	.353		.344	.376			.378	.122	6
7	.348		.346	.376			.356	.096	7
8	.338		.346	.372			.321	.068	8
9	.320		.326	.324			.282	.081	9
10	.253		.268	.290			.235	.073	10
11	.270		.227	.252			.192	.038	11
12	-.217		-.215	-.207			-.234	-.322	12
13	-.239		-.234	-.245			-.253	-.350	13
14	-.219		-.249	-.245			-.260	-.301	14
15	-.245		-.249	-.245			-.265	-.303	15
16	-.229		-.249	-.237			-.275	-.296	16
17	-.196		-.218	-.243			-.256	-.223	17
18	-.150		-.194	-.206			-.212	-.115	18
19	-.141		-.194	-.193			-.195	-.134	19
20	-.163		-.204	-.207			-.215	-.186	20
21	-.224		-.264	-.249			-.249	-.243	21
22	-.216		-.268	-.264				-.308	22
23	-.220			-.269			-.271	-.329	23
24	-.226		-.251	-.271			-.278	-.346	24
25	-.225		-.253	-.276			-.263	-.343	25
26	-.258		-.246	-.290			-.209	-.351	26
27								-.351	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.611		.869	.952			.959	.777	1
2	.525		.720	.813			.866	.602	2
3	.552		.642	.715			.746	.469	3
4	.506		.525	.564			.589	.316	4
5	.347		.338	.415			.449	.207	5
6	.353		.346	.374			.379	.126	6
7	.345		.347	.374			.356	.090	7
8	.338		.350	.371			.322	.064	8
9	.320		.326	.324			.286	.080	9
10	.260		.266	.290			.237	.067	10
11	.274		.227	.254			.191	.037	11
12	-.284		-.284	-.275			-.295	-.377	12
13	-.319		-.303	-.293			-.322	-.356	13
14	-.286		-.317	-.302			-.322	-.350	14
15	-.319		-.317	-.323			-.322	-.350	15
16	-.224		-.290	-.309			-.332	-.335	16
17	-.199		-.224	-.249			-.261	-.229	17
18	-.152		-.199	-.208			-.214	-.122	18
19	-.143		-.198	-.195			-.201	-.148	19
20	-.166		-.208	-.209			-.220	-.184	20
21	-.226		-.265	-.252			-.253	-.263	21
22	-.219		-.271	-.263				-.321	22
23	-.224			-.273			-.272	-.342	23
24	-.228		-.253	-.278			-.277	-.366	24
25	-.229		-.216	-.232			-.244	-.355	25
26	-.046		-.015	-.048			-.030	-.363	26
27								-.363	27

α=-9 δ=0

1	.473		.695	.762			.784	.661	1
2	.406		.646	.652			.731	.503	2
3	.418		.511	.589			.628	.392	3
4	.387		.431	.466			.483	.255	4
5	.251		.252	.324			.360	.159	5
6	.377		.250	.281			.294	.080	6
7	.366		.244	.266			.264	.054	7
8	.240		.247	.258			.228	.033	8
9	.230		.227	.234			.193	.035	9
10	.173		.181	.188			.146	.035	10
11	.195		.144	.160			.112	.002	11
12	.142		.125	.145			.094	-.065	12
13	.127		.112	.107			.067	-.083	13
14	.112		.112	.107			.067	-.083	14
15	.113		.113	.107			.057	-.083	15
16	.109		.113	.107			.038	-.090	16
17	-.127		-.131	-.145			-.138	-.079	17
18	-.099		-.132	-.133			-.145	-.014	18
19	-.087		-.127	-.133			-.133	-.042	19
20	-.113		-.140	-.152			-.161	-.089	20
21	-.181		-.207	-.198			-.203	-.144	21
22	-.172		-.210	-.216				-.216	22
23	-.174			-.224			-.221	-.258	23
24	-.182		-.199	-.225			-.231	-.296	24
25	-.185		-.210	-.232			-.220	-.284	25
26	-.223		-.228	-.251			-.218	-.284	26
27								-.282	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.360		.485	.503			.503	.434	1
2	.305		.447	.492			.512	.355	2
3	.309		.397	.456			.485	.302	3
4	.290		.324	.370			.383	.200	4
5	.169		.173	.237			.279	.117	5
6	.173		.531	.448			.241	.042	6
7	.495		.596	.647			.634	.309	7
8	.620		.612	.662			.659	.309	8
9	.641		.632	.679			.665	.350	9
10	.650		.649	.688			.664	.350	10
11	.659		.657	.698			.673	.327	11
12	.686		.678	.742			.695	.322	12
13	.705		.688	.741			.703	.361	13
14	.936		.773	.898			.836	.540	14
15	1.021		.850	.997			.942	.677	15
16	.803		.737	.867			.858	.634	16
17	-.052		-.051	-.049			-.043	-.005	17
18	-.032		-.053	-.050			-.043	.037	18
19	-.028		-.052	-.047			-.046	.035	19
20	-.055		-.067	-.068			-.079	-.009	20
21	-.127		-.137	-.125			-.129	-.038	21
22	-.121		-.143	-.146				-.076	22
23	-.126			-.151			-.149	-.111	23
24	-.129		-.146	-.153			-.157	-.049	24
25	-.131		-.156	-.160			-.150	-.032	25
26	-.173		-.177	-.175			-.164	-.131	26
27								-.131	27

α=-6 δ=-25

1	.361		.488	.505			.505	.429	1
2	.310		.447	.493			.513	.346	2
3	.310		.396	.458			.484	.295	3
4	.291		.321	.370			.384	.196	4
5	.171		.174	.240			.278	.109	5
6	.171		.165	.193			.226	.047	6
7	.170		.428	.439			.186	.016	7
8	.515		.553	.585			.507	.113	8
9	.588		.588	.599			.583	.305	9
10	.613		.604	.626			.596	.321	10
11	.615		.608	.630			.603	.281	11
12	.635		.623	.653			.609	.266	12
13	.676		.637	.670			.642	.306	13
14	.890		.756	.819			.782	.450	14
15	.922		.829	.894			.858	.567	15
16	.726		.709	.777			.776	.519	16
17	-.051		-.046	-.051			-.045	-.006	17
18	-.033		-.049	-.052			-.043	.028	18
19	-.027		-.050	-.049			-.050	.028	19
20	-.056		-.068	-.070			-.080	-.015	20
21	-.126		-.137	-.126			-.129	-.049	21
22	-.118		-.141	-.147				-.081	22
23	-.123			-.153			-.150	-.129	23
24	-.129		-.143	-.155			-.162	-.173	24
25	-.130		-.154	-.165			-.155	-.152	25
26	-.173		-.175	-.177			-.164	-.017	26
27								-.020	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.363		.489	.504			.507	.441	1
2	.302		.447	.494			.513	.358	2
3	.312		.397	.451			.483	.302	3
4	.291		.323	.370			.385	.201	4
5	.172		.173	.241			.278	.118	5
6	.178		.161	.194			.225	.049	6
7	.168		.155	.191			.185	.021	7
8	.159		.158	.180			.154	.014	8
9	.244		.376	.330			.130	.014	9
10	.518		.531	.542			.463	.154	10
11	.541		.545	.556			.508	.234	11
12	.578		.592	.592			.541	.287	12
13	.641		.634	.626			.589	.360	13
14	.771		.773	.762			.698	.399	14
15	.790		.808	.790			.718	.420	15
16	.657		.694	.689			.660	.395	16
17	-.050		-.048	-.055			-.048	.002	17
18	-.032		-.050	-.053			-.047	.039	18
19	-.029		-.052	-.050			-.052	.038	19
20	-.055		-.066	-.074			-.083	-.009	20
21	-.127		-.137	-.126			-.134	-.038	21
22	-.119		-.142	-.148				-.074	22
23	-.123			-.150			-.151	-.113	23
24	-.127		-.143	-.156			-.164	-.166	24
25	-.130		-.155	-.162			-.155	-.136	25
26	-.172		-.176	-.178			-.168	-.174	26
27								-.174	27

α=-6 δ=-10

1	.371		.492	.516			.516	.430	1
2	.319		.455	.503			.517	.351	2
3	.319		.406	.465			.490	.300	3
4	.300		.330	.378			.389	.197	4
5	.176		.183	.247			.280	.111	5
6	.181		.170	.201			.226	.035	6
7	.179		.163	.193			.189	.005	7
8	.170		.166	.182			.155	-.005	8
9	.163		.150	.146			.122	-.005	9
10	.114		.111	.110			.080	-.005	10
11	.155		.079	.093			.058	-.048	11
12	.324		.328	.334			.307	.125	12
13	.333		.351	.345			.296	.159	13
14	.332		.348	.349			.293	.121	14
15	.334		.348	.349			.279	.099	15
16	.333		.348	.343			.274	.075	16
17	-.046		-.038	-.051			-.052	-.017	17
18	-.027		-.045	-.055			-.049	.016	18
19	-.024		-.046	-.050			-.053	.016	19
20	-.047		-.063	-.075			-.085	-.020	20
21	-.120		-.133	-.127			-.136	-.053	21
22	-.112		-.137	-.148				-.094	22
23	-.118			-.154			-.156	-.129	23
24	-.123		-.139	-.156			-.164	-.174	24
25	-.128		-.153	-.166			-.157	-.152	25
26	-.168		-.172	-.181			-.169	-.201	26
27								-.200	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.367		.487	.514			.519	.449	1
2	.315		.449	.496			.519	.365	2
3	.316		.398	.460			.490	.308	3
4	.296		.325	.372			.389	.203	4
5	.171		.173	.242			.278	.122	5
6	.176		.167	.195			.225	.055	6
7	.173		.157	.191			.186	.023	7
8	.162		.159	.180			.156	.014	8
9	.156		.143	.145			.122	.014	9
10	.105		.105	.111			.079	.000	10
11	.119		.073	.089			.055	-.022	11
12	.078		.064	.076			.049	-.070	12
13	.065		.054	.051			.025	-.080	13
14	.047		.054	.057			.015	-.100	14
15	.048		.054	.057			.001	-.086	15
16	.054		.054	.044			.001	-.081	16
17	-.051		-.053	-.053			-.052	-.004	17
18	-.030		-.052	-.052			-.053	.035	18
19	-.028		-.054	-.053			-.058	.031	19
20	-.054		-.070	-.075			-.086	-.009	20
21	-.127		-.141	-.129			-.138	-.053	21
22	-.116		-.142	-.152				-.086	22
23	-.121			-.155			-.157	-.125	23
24	-.129		-.146	-.158			-.164	-.178	24
25	-.131		-.158	-.169			-.159	-.142	25
26	-.173		-.177	-.182			-.169	-.197	26
27								-.196	27

$\alpha = -6$ $\delta = 10$

1	.366		.488	.521			.531	.454	1
2	.310		.450	.501			.527	.360	2
3	.314		.400	.461			.496	.302	3
4	.295		.328	.378			.392	.196	4
5	.168		.177	.245			.284	.112	5
6	.173		.169	.198			.232	.048	6
7	.171		.159	.196			.196	.017	7
8	.162		.162	.187			.163	.000	8
9	.155		.147	.150			.126	.001	9
10	.104		.104	.115			.087	.001	10
11	.121		.075	.095			.063	-.037	11
12	-.143		-.143	-.125			-.160	-.223	12
13	-.163		-.166	-.170			-.179	-.242	13
14	-.158		-.166	-.163			-.185	-.189	14
15	-.162		-.165	-.165			-.186	-.129	15
16	-.162		-.165	-.165			-.195	-.111	16
17	-.053		-.050	-.051			-.050	-.006	17
18	-.034		-.048	-.054			-.050	.022	18
19	-.030		-.052	-.050			-.054	.022	19
20	-.054		-.066	-.074			-.082	-.022	20
21	-.126		-.138	-.126			-.136	-.052	21
22	-.119		-.142	-.149				-.088	22
23	-.124			-.154			-.155	-.132	23
24	-.128		-.142	-.155			-.168	-.179	24
25	-.132		-.153	-.165			-.155	-.154	25
26	-.173		-.175	-.180			-.171	-.196	26
27								-.196	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.362		.490	.520			.535	.466	1
2	.307		.449	.500			.533	.376	2
3	.310		.402	.459			.501	.305	3
4	.288		.325	.377			.399	.201	4
5	.171		.170	.246			.286	.123	5
6	.169		.166	.202			.234	.047	6
7	.168		.157	.197			.199	.027	7
8	.160		.160	.185			.167	.015	8
9	.155		.146	.153			.132	.020	9
10	.102		.105	.117			.092	.004	10
11	.122		.074	.097			.069	- .014	11
12	- .271	- .285	- .274			-	.290	- .335	12
13	- .305	- .302	- .312			-	.313	- .335	13
14	- .282	- .308	- .306			-	.324	- .258	14
15	- .305	- .302	- .302			-	.324	- .197	15
16	- .186	- .306	- .305			-	.324	- .201	16
17	- .058	- .053	- .054			-	.051	- .001	17
18	- .036	- .052	- .057			-	.050	.043	18
19	- .032	- .057	- .053			-	.055	.026	19
20	- .057	- .071	- .078			-	.085	- .014	20
21	- .130	- .139	- .130			-	.137	- .042	21
22	- .122	- .146	- .150					- .094	22
23	- .126		- .155			-	.153	- .133	23
24	- .132	- .146	- .156			-	.164	- .189	24
25	- .135	- .157	- .168			-	.153	- .145	25
26	- .174	- .175	- .180			-	.144	- .199	26
27								- .196	27

$\alpha = -6$ $\delta = 25$

1	.365		.490	.527			.538	.464	1
2	.305		.451	.501			.534	.376	2
3	.312		.399	.464			.498	.313	3
4	.292		.327	.376			.400	.211	4
5	.172		.176	.246			.286	.120	5
6	.172		.166	.202			.234	.051	6
7	.170		.157	.199			.196	.030	7
8	.158		.161	.187			.169	.018	8
9	.158		.146	.155			.132	.018	9
10	.106		.105	.117			.089	.006	10
11	.129		.074	.104			.073	- .018	11
12	- .318	- .328	- .329			-	.327	- .363	12
13	- .349	- .345	- .358			-	.356	- .349	13
14	- .327	- .361	- .356			-	.358	- .256	14
15	- .355	- .361	- .359			-	.361	- .239	15
16	- .190	- .328	- .356			-	.323	- .253	16
17	- .056	- .054	- .053			-	.054	- .004	17
18	- .035	- .054	- .055			-	.054	.026	18
19	- .033	- .056	- .052			-	.058	.025	19
20	- .059	- .073	- .077			-	.086	- .009	20
21	- .128	- .140	- .128			-	.138	- .051	21
22	- .122	- .145	- .150					- .091	22
23	- .127		- .155			-	.158	- .142	23
24	- .131	- .146	- .157			-	.165	- .180	24
25	- .132	- .120	- .141				.019	- .154	25
26	.133	.139	.133				.161	- .206	26
27								- .205	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-3 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.241		.297	.295			.294	.274	1
2	.198		.375	.294			.474	.221	2
3	.210		.279	.301			.284	.192	3
4	.195		.221	.256			.238	.141	4
5	.078		.084	.148			.165	.079	5
6	.164		.074	.111			.128	.037	6
7	.183		.067	.092			.126	.022	7
8	.073		.064	.082			.085	.022	8
9	.066		.049	.075			.057	.018	9
10	.022		.017	.026			.022	.012	10
11	.044	-	.006	.007			.001 -	.002	11
12	.011	-	.017	.001		-	.009 -	.036	12
13 -	.009	-	.018 -	.021		-	.042 -	.060	13
14 -	.030	-	.018 -	.021		-	.042 -	.074	14
15 -	.028	-	.018 -	.021		-	.041 -	.054	15
16 -	.028	-	.018 -	.021		-	.049 -	.042	16
17	.052		.048	.044			.041	.054	17
18	.043		.045	.039			.037	.072	18
19	.045		.047	.046			.046	.072	19
20	.024		.024	.020			.007	.036	20
21 -	.061	-	.059 -	.046		-	.049 -	.002	21
22 -	.053	-	.069 -	.071				.000	22
23 -	.057		-	.076		-	.077 -	.009	23
24 -	.064	-	.082 -	.079		-	.093 -	.038	24
25 -	.064	-	.097 -	.085		-	.090 -	.023	25
26 -	.118	-	.118 -	.119		-	.106 -	.048	26
27							-	.047	27

α=0 δ=-30

1	.139		.153	.152			.150	.148	1
2	.116		.153	.150			.150	.132	2
3	.117		.150	.150			.147	.127	3
4	.098		.112	.124			.108	.092	4
5 -	.002		.000	.043			.043	.051	5
6	.000	-	.002	.012			.017	.033	6
7	.084		.336	.355			.236	.045	7
8	.345		.359	.377			.385	.092	8
9	.378		.366	.386			.393	.317	9
10	.393		.374	.396			.390	.299	10
11	.397		.381	.398			.407	.260	11
12	.440		.420	.437			.417	.225	12
13	.486		.429	.439			.417	.250	13
14	.747		.544	.573			.541	.375	14
15	.872		.662	.715			.663	.466	15
16	.713		.627	.692			.659	.446	16
17	.144		.153	.153			.154	.157	17
18	.115		.151	.153			.162	.143	18
19	.116		.155	.156			.164	.129	19
20	.098		.110	.123			.118	.086	20
21 -	.002		.008	.044			.048	.053	21
22	.008	-	.003	.020				.043	22
23	.001			.013			.016	.039	23
24 -	.006	-	.019	.004			.001	.012	24
25 -	.005	-	.028 -	.017		-	.008	.134	25
26 -	.063	-	.057 -	.044		-	.038	.165	26
27								.164	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.134		.152	.156			.154	.142	1
2	.106		.151	.151			.153	.126	2
3	.118		.148	.154			.151	.124	3
4	.099		.115	.125			.115	.082	4
5	-.001		.001	.043			.045	.047	5
6	-.002		-.001	.014			.021	.033	6
7	.002		-.012	.005			.016	.020	7
8	-.008		-.013	.004			-.001	.029	8
9	.277		.327	.294			.314	.077	9
10	.357		.352	.356			.355	.292	10
11	.365		.356	.366			.372	.285	11
12	.404		.396	.396			.380	.274	12
13	.452		.415	.424			.410	.321	13
14	.630		.561	.589			.587	.372	14
15	.715		.680	.691			.671	.355	15
16	.614		.625	.643			.644	.322	16
17	.143		.152	.154			.154	.149	17
18	.113		.151	.154			.162	.143	18
19	.114		.154	.158			.166	.121	19
20	.100		.110	.126			.120	.080	20
21	-.002		.009	.045			.052	.043	21
22	.004		-.002	.023				.034	22
23	.001			.015			.021	.028	23
24	-.006		-.018	.008			.008	.004	24
25	-.006		-.024	-.011			-.005	.026	25
26	-.063		-.055	-.041			-.032	.015	26
27								.013	27

$\alpha = 0$ $\delta = -20$

1	.137		.154	.154			.153	.135	1
2	.102		.151	.154			.154	.116	2
3	.117		.154	.156			.151	.115	3
4	.098		.115	.128			.116	.080	4
5	-.003		.002	.046			.048	.039	5
6	.000		-.005	.014			.021	.023	6
7	.003		-.012	.008			.016	.015	7
8	-.008		-.011	.003			-.001	.023	8
9	-.001		-.030	-.023			-.017	.015	9
10	.068		.044	.015			-.025	.012	10
11	.252		.269	.272			.287	.062	11
12	.319		.330	.320			.330	.368	12
13	.404		.405	.393			.405	.365	13
14	.492		.513	.502			.506	.272	14
15	.523		.549	.534			.523	.230	15
16	.494		.521	.507			.505	.198	16
17	.140		.152	.153			.153	.146	17
18	.112		.148	.154			.161	.138	18
19	.114		.155	.156			.168	.114	19
20	.102		.112	.125			.122	.086	20
21	-.001		.010	.043			.048	.056	21
22	.006		.000	.019				.038	22
23	.001			.013			.017	.026	23
24	-.006		-.018	.007			.007	.022	24
25	-.005		-.024	-.014			-.008	.015	25
26	-.063		-.056	-.043			-.035	-.009	26
27								-.009	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.134		.154	.158			.156	.140	1
2	.104		.154	.154			.157	.123	2
3	.121		.154	.157			.155	.115	3
4	.099		.120	.128			.117	.080	4
5	-.001		.001	.045			.050	.045	5
6	-.001		-.001	.014			.024	.022	6
7	.004		-.013	.008			.020	.034	7
8	-.009		-.010	.001			.000	.028	8
9	-.006		-.031	-.024		-.018	.015		9
10	-.049		-.057	-.049		-.044	.013		10
11	-.010		-.085	-.067		-.045	-.009		11
12	.135		.134	.121			.129	.142	12
13	.143		.140	.132			.135	.118	13
14	.140		.145	.142			.143	.053	14
15	.142		.149	.148			.147	.034	15
16	.138		.152	.148			.148	.015	16
17	.142		.151	.151			.151	.140	17
18	.112		.151	.152			.158	.135	18
19	.115		.155	.155			.164	.121	19
20	.099		.111	.122			.117	.083	20
21	.000		.011	.043			.047	.039	21
22	.006		-.002	.021				.032	22
23	.001			.013			.016	.023	23
24	-.004		-.020	.006			.004	.025	24
25	-.005		-.027	-.015		-.007		.022	25
26	-.061		-.056	-.044		-.036	-.002		26
27							.000		27

$\alpha=0$ $\delta=0$

1	.137		.153	.156			.153	.145	1
2	.103		.154	.156			.154	.124	2
3	.119		.153	.157			.154	.115	3
4	.100		.119	.134			.117	.091	4
5	-.002		.014	.048			.046	.051	5
6	.001		.000	.016			.022	.036	6
7	.003		-.013	.010			.016	.020	7
8	-.006		-.011	.004		-.001	.027		8
9	-.010		-.030	-.024		-.020	.016		9
10	-.053		-.055	-.050		-.049	.015		10
11	-.033		-.081	-.067		-.057	-.013		11
12	-.066		-.086	-.076		-.080	-.049		12
13	-.074		-.093	-.100		-.096	-.059		13
14	-.085		-.092	-.094		-.094	-.054		14
15	-.088		-.093	-.091		-.091	-.042		15
16	-.091		-.092	-.091		-.097	-.029		16
17	.140		.150	.148			.143	.138	17
18	.114		.146	.148			.153	.141	18
19	.115		.152	.154			.158	.129	19
20	.102		.111	.120			.110	.089	20
21	.002		.010	.039			.043	.044	21
22	.010		-.001	.014				.032	22
23	.003			.008			.012	.027	23
24	-.005		-.020	.001		-.006		.020	24
25	-.004		-.031	-.017		-.011		.016	25
26	-.057		-.057	-.049		-.040	-.005		26
27							-.005		27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.150		.166	.161			.155	.158	1
2	.123		.151	.157			.153	.140	2
3	.128		.161	.162			.155	.134	3
4	.114		.126	.133			.115	.092	4
5	.012		.007	.054			.050	.054	5
6	.005		.012	.020			.017	.029	6
7	- .008		- .005	.014			.012	.016	7
8	- .002		- .002	.010			- .004	.027	8
9	.002		- .024	- .020			- .025	.027	9
10	- .037		- .042	- .046			- .052	.026	10
11	- .022		- .070	- .059			- .054	.000	11
12	- .046		- .059	- .046			- .050	- .028	12
13	- .046		- .078	- .084			- .079	- .042	13
14	- .063		- .068	- .074			- .070	- .033	14
15	- .063		- .068	- .071			- .070	- .024	15
16	- .063		- .068	- .071			- .071	- .015	16
17	.157		.162	.158			.150	.156	17
18	.131		.166	.162			.160	.150	18
19	.128		.167	.164			.162	.136	19
20	.116		.125	.131			.115	.094	20
21	.013		.021	.051			.047	.063	21
22	.025		.013	.025				.045	22
23	.016			.019			.016	.045	23
24	.015		- .004	.012			.000	.028	24
25	.008		- .012	- .008			- .010	.044	25
26	- .049		- .041	- .037			- .038	.012	26
27								.012	27

$\alpha = 0$ $\delta = 10$

1	.134		.155	.158			.158	.132	1
2	.105		.154	.158			.161	.121	2
3	.118		.154	.159			.159	.115	3
4	.100		.119	.131			.118	.071	4
5	- .003		.001	.049			.052	.028	5
6	- .001		.005	.018			.025	.010	6
7	.004		- .008	.012			.023	.009	7
8	- .007		- .008	.008			.006	.039	8
9	- .006		- .030	- .017			- .014	.004	9
10	- .047		- .055	- .043			- .043	.005	10
11	- .029		- .082	- .060			- .044	- .017	11
12	- .222		- .227	- .225			- .221	- .211	12
13	- .252		- .241	- .254			- .243	- .173	13
14	- .236		- .262	- .250			- .243	- .121	14
15	- .254		- .256	- .250			- .243	- .142	15
16	- .189		- .250	- .250			- .255	- .239	16
17	.139		.148	.147			.144	.132	17
18	.111		.147	.147			.154	.132	18
19	.114		.151	.153			.155	.100	19
20	.098		.111	.120			.111	.072	20
21	- .001		.005	.041			.042	.034	21
22	.008		- .003	.016				.021	22
23	.000			.010			.010	.021	23
24	- .005		- .020	.004			- .002	.000	24
25	- .008		- .027	- .016			- .009	.022	25
26	- .062		- .058	- .046			- .040	- .006	26
27								- .002	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.133		.160	.164			.162	.146	1
2	.106		.156	.162			.164	.123	2
3	.119		.156	.163			.165	.115	3
4	.108		.121	.132			.123	.086	4
5	-.002		.001	.048			.056	.037	5
6	.006		.007	.021			.031	.025	6
7	.005		-.008	.015			.024	.013	7
8	-.005		-.006	.010			.008	.029	8
9	.002		-.026	-.014		-	.008	.011	9
10	-.042		-.050	-.040		-	.038	.011	10
11	-.023		-.082	-.053		-	.032	.016	11
12	-.327		-.332	-.325		-	.332	- .294	12
13	-.360		-.349	-.361		-	.360	- .218	13
14	-.333		-.365	-.361		-	.359	- .293	14
15	-.358		-.363	-.361		-	.337	- .391	15
16	-.224		-.223	-.281		-	.234	- .429	16
17	.141		.150	.147			.144	.135	17
18	.111		.147	.147			.154	.135	18
19	.115		.151	.152			.155	.111	19
20	.098		.110	.119			.109	.077	20
21	-.002		.008	.041			.042	.042	21
22	.006		-.004	.015				.025	22
23	.001			.007			.008	.026	23
24	-.001		-.019	.003		-	.003	.010	24
25	-.003		-.027	-.017		-	.014	.021	25
26	.124		.190	.089			.076	.005	26
27								.005	27

$\alpha = 0$ $\delta = 25$

1	.138		.159	.164			.166	.164	1
2	.108		.157	.160			.165	.137	2
3	.120		.154	.164			.164	.131	3
4	.101		.118	.137			.126	.093	4
5	-.001		.003	.052			.057	.054	5
6	.002		.004	.022			.031	.034	6
7	.002		-.010	.014			.028	.020	7
8	-.007		-.008	.010			.009	.042	8
9	.003		-.026	-.015		-	.010	.025	9
10	-.041		-.047	-.039		-	.038	.044	10
11	-.019		-.077	-.052		-	.028	.121	11
12	-.368		-.377	-.371		-	.369	- .299	12
13	-.394		-.388	-.398		-	.394	- .206	13
14	-.360		-.388	-.392		-	.371	- .372	14
15	-.338		-.314	-.327		-	.299	- .446	15
16	-.279		-.287	-.294		-	.289	- .453	16
17	.138		.149	.145			.142	.143	17
18	.111		.144	.146			.150	.143	18
19	.112		.152	.153			.153	.113	19
20	.096		.111	.121			.110	.077	20
21	-.004		.009	.041			.040	.048	21
22	.008		.000	.015				.033	22
23	.002			.008			.009	.029	23
24	-.003		.003	.041		-	.004	.012	24
25	.298		.345	.345			.304	.146	25
26	.356		.363	.365			.368	.294	26
27								.294	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.043		.049	.054			.049	.063	1
2	.044		.039	.049			.050	.077	2
3	.041		.047	.051			.049	.082	3
4	.023		.029	.031			.017	.061	4
5	-.062		-.063	-.039			-.045	.013	5
6	-.065		-.063	-.064			-.067	.007	6
7	-.080		-.068	-.069			-.074	-.013	7
8	-.066		-.076	-.071			-.082	-.039	8
9	-.066		-.095	-.097			-.091	-.038	9
10	-.100		-.106	-.112			-.110	-.038	10
11	-.083		-.134	-.127			-.102	-.067	11
12	-.099		-.106	-.099			-.107	-.089	12
13	-.099		-.122	-.133			-.122	-.106	13
14	-.107		-.118	-.127			-.112	-.117	14
15	-.107		-.114	-.127			-.112	-.136	15
16	-.107		-.114	-.127			-.112	-.136	16
17	.248		.300	.292			.287	.274	17
18	.211		.300	.297			.300	.248	18
19	.209		.280	.300			.293	.203	19
20	.195		.219	.254			.246	.151	20
21	.085		.099	.153			.165	.079	21
22	.091		.086	.111				.056	22
23	.088			.100			.117	.045	23
24	.085		.071	.085			.090	.017	24
25	.081		.063	.074			.076	.035	25
26	.018		.032	.039			.041	.004	26
27								.004	27

$\alpha = 6$ $\delta = -30$

1	-.042		-.040	-.042			-.042	-.026	1
2	-.030		-.040	-.043			-.038	.017	2
3	-.018		-.044	-.043			-.040	.024	3
4	-.046		-.065	-.065			-.069	-.006	4
5	-.118		-.140	-.118			-.117	-.057	5
6	-.115		-.133	-.146			-.138	-.111	6
7	-.115		-.135	-.142			-.139	-.158	7
8	-.126		-.122	.051			-.034	-.184	8
9	.115		.146	.011			.149	-.184	9
10	.195		.181	.153			.163	-.165	10
11	.202		.178	.168			.189	-.005	11
12	.227		.209	.201			.199	.090	12
13	.289		.223	.223			.232	.261	13
14	.499		.379	.377			.394	.164	14
15	.570		.505	.474			.514	.236	15
16	.519		.495	.474			.509	.342	16
17	.373		.505	.544			.567	.458	17
18	.327		.462	.513			.556	.387	18
19	.322		.406	.473			.516	.303	19
20	.296		.328	.378			.417	.217	20
21	.176		.191	.252			.297	.128	21
22	.183		.177	.218				.083	22
23	.177			.208			.208	.057	23
24	.176		.163	.193			.181	.023	24
25	.171		.157	.172			.160	.046	25
26	.099		.121	.136			.125	.011	26
27								.011	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=-25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.043		-.044	-.039			-.042	-.023	1
2	-.036		-.041	-.041			-.041	.015	2
3	-.023		-.046	-.040			-.042	.022	3
4	-.050		-.062	-.062			-.070	-.005	4
5	-.123		-.139	-.118			-.117	-.050	5
6	-.120		-.131	-.142			-.138	-.112	6
7	-.119		-.132	-.144			-.140	-.162	7
8	-.127		-.130	-.146			-.148	-.193	8
9	-.116		-.146	-.162			-.072	-.181	9
10	.127		.129	.115			.141	-.190	10
11	.161		.149	.138			.175	-.193	11
12	.195		.184	.173			.181	.167	12
13	.260		.233	.212			.228	.300	13
14	.426		.389	.359			.392	-.007	14
15	.458		.466	.426			.474	.074	15
16	.440		.441	.416			.452	.182	16
17	.371		.504	.544			.564	.459	17
18	.327		.457	.513			.554	.387	18
19	.320		.407	.470			.517	.300	19
20	.293		.327	.377			.412	.210	20
21	.175		.191	.249			.300	.123	21
22	.183		.177	.214				.073	22
23	.177			.207			.208	.042	23
24	.176		.164	.195			.178	.016	24
25	.168		.154	.173			.162	.046	25
26	.097		.112	.137			.123	.001	26
27								.001	27

$\alpha=6$ $\delta=-20$

1	-.036		-.038	-.038			-.037	-.026	1
2	-.019		-.037	-.040			-.037	.017	2
3	-.016		-.042	-.040			-.038	.018	3
4	-.044		-.057	-.056			-.067	-.004	4
5	-.115		-.137	-.117			-.116	-.053	5
6	-.107		-.129	-.140			-.135	-.112	6
7	-.110		-.135	-.141			-.135	-.160	7
8	-.121		-.129	-.144			-.145	-.192	8
9	-.113		-.148	-.161			-.146	-.183	9
10	-.144		-.161	-.177			-.150	-.197	10
11	.070		.052	.030			.109	-.197	11
12	.133		.139	.116			.167	.071	12
13	.212		.198	.178			.236	.137	13
14	.276		.271	.247			.311	-.112	14
15	.280		.299	.264			.336	-.084	15
16	.283		.299	.275			.317	-.007	16
17	.375		.506	.543			.564	.448	17
18	.331		.462	.517			.554	.381	18
19	.322		.407	.474			.518	.303	19
20	.297		.329	.380			.417	.205	20
21	.178		.194	.255			.301	.121	21
22	.185		.179	.219				.067	22
23	.181			.211			.210	.050	23
24	.178		.165	.196			.181	.006	24
25	.172		.158	.177			.162	.032	25
26	.103		.120	.139			.126	-.001	26
27								-.001	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=6 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.042		-.039	-.036			-.038	-.039	1
2	-.022		-.039	-.039			-.038	.002	2
3	-.022		-.038	-.040			-.040	.021	3
4	-.050		-.060	-.058			-.070	-.011	4
5	-.123		-.141	-.115			-.117	-.053	5
6	-.110		-.130	-.143			-.136	-.112	6
7	-.115		-.134	-.140			-.135	-.164	7
8	-.125		-.129	-.144			-.146	-.198	8
9	-.120		-.148	-.162			-.146	-.189	9
10	-.153		-.162	-.176			-.155	-.204	10
11	-.119		-.189	-.187			-.122	-.220	11
12	-.011		-.023	-.037			.000	-.089	12
13	.006		-.012	-.028			.017	-.082	13
14	.006		-.001	-.020			.027	-.203	14
15	.006		.007	-.015			.046	-.208	15
16	.006		.007	-.012			.046	-.149	16
17	.374		.503	.535			.556	.437	17
18	.329		.459	.509			.545	.365	18
19	.321		.404	.468			.513	.295	19
20	.295		.327	.375			.409	.200	20
21	.176		.192	.250			.302	.111	21
22	.184		.177	.212				.072	22
23	.178			.204			.204	.034	23
24	.173		.163	.192			.175	.015	24
25	.171		.156	.169			.160	.033	25
26	.100		.117	.129			.119	-.011	26
27								-.011	27

α=6 δ=0

1	-.042		-.038	-.034			-.037	-.026	1
2	-.021		-.005	-.038			-.035	.013	2
3	-.019		-.045	-.038			-.042	.024	3
4	-.047		-.056	-.059			-.067	-.009	4
5	-.116		-.137	-.113			-.115	-.057	5
6	-.095		-.130	-.136			-.137	-.116	6
7	-.085		-.131	-.144			-.129	-.151	7
8	-.123		-.130	-.146			-.145	-.183	8
9	-.116		-.150	-.161			-.144	-.175	9
10	-.149		-.162	-.180			-.151	-.188	10
11	-.142		-.185	-.190			-.131	-.208	11
12	-.143		-.168	-.173			-.151	-.200	12
13	-.162		-.183	-.194			-.167	-.225	13
14	-.162		-.183	-.188			-.154	-.219	14
15	-.176		-.166	-.189			-.148	-.178	15
16	-.167		-.170	-.189			-.150	-.198	16
17	.373		.505	.534			.548	.442	17
18	.327		.456	.509			.542	.372	18
19	.321		.405	.465			.511	.289	19
20	.292		.326	.374			.409	.200	20
21	.177		.194	.244			.296	.125	21
22	.183		.178	.210				.072	22
23	.180			.203			.204	.038	23
24	.173		.163	.190			.175	.015	24
25	.170		.152	.169			.158	.033	25
26	.099		.115	.130			.121	-.001	26
27								.000	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.039		-.038	-.037			-.038	-.012	1
2	-.024		-.038	-.035			-.036	.022	2
3	-.021		-.045	-.036			-.038	.038	3
4	-.050		-.061	-.056			-.066	.011	4
5	-.122		-.138	-.111			-.114	-.039	5
6	-.115		-.130	-.137			-.134	-.098	6
7	-.116		-.134	-.138			-.137	-.136	7
8	-.123		-.130	-.141			-.143	-.173	8
9	-.116		-.146	-.151			-.145	-.172	9
10	-.149		-.162	-.174			-.152	-.176	10
11	-.144		-.184	-.186			-.131	-.186	11
12	-.250		-.284	-.283			-.267	-.288	12
13	-.297		-.275	-.316			-.298	-.263	13
14	-.278		-.313	-.309			-.282	-.286	14
15	-.299		-.298	-.309			-.292	-.306	15
16	-.159		-.181	-.247			-.271	-.309	16
17	.370		.504	.529			.541	.440	17
18	.327		.460	.503			.535	.375	18
19	.321		.406	.466			.505	.297	19
20	.294		.326	.373			.405	.215	20
21	.176		.193	.247			.290	.131	21
22	.184		.179	.209				.076	22
23	.178			.200			.197	.050	23
24	.175		.162	.187			.173	.020	24
25	.168		.155	.164			.153	.043	25
26	.096		.118	.129			.115	.005	26
27								.007	27

$\alpha=6$ $\delta=20$

1	-.041		-.040	-.037			-.037	-.017	1
2	-.023		-.038	-.037			-.034	.018	2
3	-.020		-.041	-.037			-.037	.035	3
4	-.049		-.059	-.062			-.066	.001	4
5	-.118		-.138	-.114			-.111	-.045	5
6	-.116		-.132	-.137			-.132	-.089	6
7	-.115		-.133	-.139			-.132	-.142	7
8	-.125		-.131	-.143			-.142	-.176	8
9	-.111		-.147	-.159			-.140	-.164	9
10	-.142		-.159	-.175			-.147	-.176	10
11	-.135		-.186	-.183			-.123	-.129	11
12	-.338		-.364	-.357			-.355	-.347	12
13	-.375		-.364	-.386			-.366	-.335	13
14	-.359		-.375	-.372			-.366	-.383	14
15	-.360		-.304	-.306			-.366	-.383	15
16	-.253		-.282	-.292			-.265	-.383	16
17	.369		.499	.524			.530	.433	17
18	.324		.454	.502			.530	.377	18
19	.319		.400	.460			.498	.292	19
20	.292		.321	.369			.401	.209	20
21	.174		.190	.243			.288	.126	21
22	.184		.174	.208				.077	22
23	.176			.198			.199	.050	23
24	.173		.158	.183			.169	.017	24
25	.350		.497	.482			.159	.039	25
26	.537		.562	.560			.513	.210	26
27								.210	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.043		-.038	-.035			-.035	-.016	1
2	-.023		-.038	-.038			-.035	.024	2
3	-.023		-.040	-.038			-.037	.033	3
4	-.050		-.060	-.059			-.066	-.006	4
5	-.116		-.138	-.114			-.114	-.043	5
6	-.116		-.130	-.141			-.134	-.095	6
7	-.121		-.132	-.140			-.133	-.144	7
8	-.128		-.128	-.141			-.142	-.173	8
9	-.110		-.151	-.153			-.142	-.143	9
10	-.147		-.158	-.174			-.149	-.017	10
11	-.138		-.182	-.184			-.126	-.103	11
12	-.388		-.400	-.407			-.400	-.413	12
13	-.414		-.381	-.397			-.421	-.408	13
14	-.368		-.343	-.355			-.421	-.430	14
15	-.320		-.330	-.343			-.354	-.421	15
16	-.291		-.328	-.343			-.310	-.381	16
17	.367		.499	.522			.529	.430	17
18	.320		.453	.500			.529	.366	18
19	.316		.399	.460			.497	.295	19
20	.290		.321	.367			.404	.203	20
21	.172		.190	.242			.287	.120	21
22	.180		.176	.208				.076	22
23	.290			.523			.260	.044	23
24	.551		.584	.612			.566	.248	24
25	.603		.609	.640			.613	.342	25
26	.622		.623	.652			.628	.339	26
27								.339	27

$\alpha = 9$ $\delta = 0$

1	-.135		-.129	-.133			-.132	-.120	1
2	-.098		-.179	-.130			-.138	-.046	2
3	-.094		-.133	-.124			-.124	-.062	3
4	-.115		-.149	-.142			-.148	-.109	4
5	-.179		-.213	-.188			-.192	-.164	5
6	-.200		-.206	-.216			-.206	-.254	6
7	-.220		-.206	-.211			-.228	-.291	7
8	-.187		-.197	-.213			-.215	-.324	8
9	-.173		-.211	-.242			-.205	-.309	9
10	-.206		-.218	-.245			-.208	-.308	10
11	-.196		-.241	-.254			-.171	-.291	11
12	-.190		-.205	-.225			-.188	-.289	12
13	-.204		-.221	-.245			-.205	-.311	13
14	-.204		-.216	-.242			-.198	-.308	14
15	-.204		-.216	-.242			-.195	-.302	15
16	-.198		-.216	-.242			-.188	-.278	16
17	.499		.721	.792			.837	.647	17
18	.435		.589	.680			.751	.495	18
19	.445		.529	.615			.669	.383	19
20	.400		.450	.485			.519	.274	20
21	.267		.279	.344			.382	.161	21
22	.276		.269	.302				.109	22
23	.264			.293			.283	.081	23
24	.264		.262	.282			.254	.043	24
25	.256		.252	.262			.230	.071	25
26	.182		.204	.219			.192	.033	26
27								.034	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.182		-.200	-.225			-.239	-.215	1
2	-.141		-.182	-.190			-.202	-.117	2
3	-.133		-.184	-.183			-.191	-.126	3
4	-.156		-.192	-.198			-.203	-.183	4
5	-.217		-.259	-.240			-.239	-.234	5
6	-.205		-.254	-.257			-.257	-.317	6
7	-.213		-.251	-.137			-.258	-.344	7
8	-.215		-.084	-.022			-.071	-.344	8
9	-.063		-.021	-.124			-.032	-.344	9
10	.058		.022	.003			-.005	-.324	10
11	.069		.015	.007			.026	-.199	11
12	.107		.060	.037			.035	-.166	12
13	.156		.067	.035			.042	-.066	13
14	.375		.219	.112			.189	-.095	14
15	.448		.350	.179			.346	-.156	15
16	.436		.366	.201			.420	-.234	16
17	.620		.873	.953			.984	.751	17
18	.545		.722	.815			.873	.578	18
19	.562		.650	.729			.758	.458	19
20	.507		.521	.556			.594	.352	20
21	.350		.353	.415			.452	.215	21
22	.364		.357	.388				.161	22
23	.348			.382			.356	.137	23
24	.346		.347	.373			.325	.099	24
25	.338		.334	.350			.305	.120	25
26	.255		.283	.301			.269	.073	26
27								.073	27

α=12 δ=-25

1	-.178		-.196	-.223			-.244	-.231	1
2	-.136		-.180	-.189			-.202	-.131	2
3	-.131		-.184	-.180			-.189	-.132	3
4	-.153		-.192	-.196			-.206	-.190	4
5	-.213		-.254	-.242			-.239	-.242	5
6	-.206		-.253	-.254			-.255	-.330	6
7	-.206		-.247	-.260			-.256	-.353	7
8	-.215		-.239	-.258			-.265	-.349	8
9	-.206		-.239	-.272			-.242	-.357	9
10	-.054		-.008	-.052			-.031	-.352	10
11	.013		-.001	-.032			.014	-.293	11
12	.068		.032	.005			.018	-.161	12
13	.125		.057	.016			.043	-.090	13
14	.245		.189	.122			.209	-.153	14
15	.270		.260	.181			.281	-.178	15
16	.293		.260	.181			.288	-.267	16
17	.620		.875	.949			.982	.745	17
18	.546		.721	.813			.871	.560	18
19	.561		.648	.723			.756	.442	19
20	.508		.521	.556			.594	.344	20
21	.353		.353	.415			.450	.200	21
22	.365		.355	.386				.148	22
23	.349			.379			.354	.121	23
24	.347		.346	.369			.323	.088	24
25	.341		.337	.348			.305	.111	25
26	.256		.285	.302			.269	.076	26
27								.073	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.174		-.194	-.221			-.242	-.210	1
2	-.130		-.175	-.187			-.198	-.114	2
3	-.128		-.180	-.179			-.185	-.125	3
4	-.145		-.190	-.193			-.204	-.186	4
5	-.199		-.254	-.238			-.239	-.231	5
6	-.193		-.252	-.254			-.255	-.324	6
7	-.202		-.247	-.257			-.255	-.339	7
8	-.210		-.235	-.257			-.263	-.339	8
9	-.201		-.239	-.268			-.253	-.339	9
10	-.229		-.212	-.284			-.226	-.339	10
11	-.049		-.074	-.131			-.029	-.311	11
12	.032		.005	-.033			.000	-.184	12
13	.085		.042	-.015			.029	-.166	13
14	.133		.115	.051			.120	-.220	14
15	.145		.136	.071			.148	-.260	15
16	.145		.142	.084			.148	-.277	16
17	.621		.876	.950			.979	.748	17
18	.545		.718	.810			.866	.575	18
19	.563		.647	.722			.756	.453	19
20	.508		.522	.555			.595	.352	20
21	.355		.356	.412			.450	.210	21
22	.367		.356	.387				.155	22
23	.350			.378			.351	.136	23
24	.350		.347	.366			.323	.092	24
25	.345		.333	.346			.303	.120	25
26	.259		.285	.299			.269	.078	26
27								.079	27

α=12 δ=-10

1	-.177		-.193	-.216			-.228	-.206	1
2	-.133		-.177	-.185			-.192	-.110	2
3	-.130		-.179	-.179			-.184	-.129	3
4	-.150		-.190	-.190			-.199	-.178	4
5	-.210		-.259	-.235			-.237	-.226	5
6	-.208		-.254	-.253			-.252	-.316	6
7	-.206		-.253	-.255			-.251	-.342	7
8	-.217		-.239	-.257			-.259	-.342	8
9	-.206		-.241	-.265			-.250	-.342	9
10	-.233		-.245	-.285			-.250	-.342	10
11	-.206		-.262	-.287			-.169	-.315	11
12	-.082		-.101	-.154			-.109	-.253	12
13	-.076		-.125	-.148			-.092	-.263	13
14	-.077		-.087	-.131			-.077	-.304	14
15	-.076		-.079	-.132			-.070	-.305	15
16	-.072		-.079	-.132			-.070	-.278	16
17	.612		.867	.943			.975	.737	17
18	.536		.710	.805			.864	.562	18
19	.553		.638	.716			.750	.448	19
20	.500		.516	.547			.590	.342	20
21	.346		.348	.407			.446	.209	21
22	.360		.349	.380				.148	22
23	.342			.375			.346	.120	23
24	.340		.342	.363			.318	.085	24
25	.335		.330	.341			.297	.112	25
26	.251		.278	.292			.261	.071	26
27								.071	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.177		-.189	-.210			-.219	-.210	1
2	-.132		-.135	-.179			-.182	-.109	2
3	-.131		-.177	-.176			-.177	-.123	3
4	-.149		-.185	-.189			-.196	-.172	4
5	-.208		-.248	-.235			-.229	-.220	5
6	-.182		-.250	-.240			-.249	-.305	6
7	-.174		-.242	-.252			-.229	-.330	7
8	-.212		-.237	-.252			-.254	-.315	8
9	-.203		-.237	-.251			-.243	-.333	9
10	-.233		-.241	-.282			-.242	-.322	10
11	-.232		-.264	-.289			-.191	-.311	11
12	-.209		-.234	-.260			-.221	-.302	12
13	-.228		-.248	-.284			-.248	-.317	13
14	-.233		-.248	-.277			-.228	-.326	14
15	-.233		-.238	-.277			-.230	-.321	15
16	-.151		-.226	-.276			-.231	-.291	16
17	.608		.862	.937			.964	.730	17
18	.530		.704	.801			.858	.556	18
19	.546		.638	.712			.744	.442	19
20	.495		.514	.546			.584	.339	20
21	.343		.346	.407			.442	.211	21
22	.355		.346	.377				.140	22
23	.341			.370			.342	.122	23
24	.338		.339	.359			.308	.082	24
25	.331		.325	.338			.295	.107	25
26	.250		.272	.292			.258	.070	26
27								.070	27

$\alpha = 12$ $\delta = 10$

1	-.179		-.192	-.218			-.229	-.208	1
2	-.135		-.179	-.185			-.191	-.126	2
3	-.129		-.183	-.177			-.180	-.123	3
4	-.150		-.190	-.188			-.197	-.179	4
5	-.210		-.259	-.239			-.233	-.228	5
6	-.204		-.250	-.254			-.249	-.320	6
7	-.207		-.247	-.255			-.252	-.344	7
8	-.218		-.237	-.257			-.257	-.344	8
9	-.200		-.234	-.241			-.246	-.344	9
10	-.234		-.239	-.282			-.243	-.335	10
11	-.230		-.260	-.289			-.192	-.308	11
12	-.298		-.332	-.341			-.314	-.369	12
13	-.331		-.321	-.368			-.337	-.364	13
14	-.331		-.350	-.366			-.328	-.374	14
15	-.331		-.349	-.366			-.333	-.375	15
16	-.205		-.211	-.243			-.261	-.375	16
17	.620		.872	.947			.977	.746	17
18	.543		.717	.809			.870	.567	18
19	.562		.647	.721			.758	.453	19
20	.505		.519	.551			.593	.350	20
21	.354		.353	.411			.450	.215	21
22	.365		.353	.383				.154	22
23	.349			.377			.349	.126	23
24	.346		.344	.366			.323	.093	24
25	.340		.333	.344			.305	.116	25
26	.254		.281	.295			.269	.076	26
27								.076	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.178		-.193	-.219			-.226	-.223	1
2	-.137		-.180	-.182			-.192	-.121	2
3	-.130		-.183	-.177			-.180	-.126	3
4	-.150		-.190	-.190			-.195	-.183	4
5	-.208		-.254	-.235			-.234	-.238	5
6	-.205		-.252	-.252			-.249	-.321	6
7	-.205		-.248	-.255			-.253	-.350	7
8	-.212		-.239	-.258			-.256	-.349	8
9	-.192		-.240	-.266			-.244	-.335	9
10	-.224		-.239	-.284			-.242	-.300	10
11	-.223		-.266	-.290			-.181	-.254	11
12	-.374		-.400	-.394			-.386	-.420	12
13	-.405		-.392	-.407			-.397	-.420	13
14	-.396		-.353	-.377			-.398	-.430	14
15	-.347		-.333	-.361			-.398	-.422	15
16	-.305		-.320	-.343			-.309	-.409	16
17	.616		.870	.941			.970	.736	17
18	.541		.716	.805			.863	.557	18
19	.556		.644	.715			.747	.441	19
20	.503		.517	.548			.588	.333	20
21	.351		.348	.408			.444	.190	21
22	.363		.354	.378				.143	22
23	.538			.714			.579	.128	23
24	.752		.773	.820			.723	.288	24
25	.819		.846	.888			.824	.438	25
26	.859		.885	.931			.895	.501	26
27								.501	27

α=12 δ=25

1	-.178		-.194	-.220			-.225	-.221	1
2	-.134		-.181	-.186			-.192	-.126	2
3	-.130		-.184	-.180			-.180	-.132	3
4	-.150		-.192	-.192			-.195	-.184	4
5	-.207		-.258	-.238			-.235	-.239	5
6	-.207		-.254	-.255			-.249	-.324	6
7	-.210		-.253	-.253			-.251	-.344	7
8	-.219		-.239	-.254			-.257	-.347	8
9	-.190		-.241	-.262			-.241	-.347	9
10	-.225		-.241	-.280			-.239	-.333	10
11	-.223		-.269	-.288			-.175	-.282	11
12	-.431		-.414	-.407			-.425	-.448	12
13	-.442		-.392	-.393			-.431	-.474	13
14	-.399		-.380	-.376			-.437	-.463	14
15	-.347		-.371	-.375			-.394	-.451	15
16	-.335		-.360	-.375			-.355	-.437	16
17	.616		.868	.941			.968	.724	17
18	.539		.712	.805			.863	.554	18
19	.557		.643	.718			.750	.436	19
20	.501		.515	.546			.586	.338	20
21	.351		.349	.408			.643	.277	21
22	.575		.746	.815				.366	22
23	.866			.944			.860	.470	23
24	.916		.944	1.003			.926	.487	24
25	.958		1.001	1.064			1.001	.591	25
26	.993		1.039	1.112			1.067	.631	26
27								.631	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=15 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.240		-.304	-.339			-.347	-.337	1
2	-.194		-.252	-.274			-.290	-.234	2
3	-.175		-.247	-.251			-.259	-.216	3
4	-.195		-.254	-.258			-.265	-.272	4
5	-.247		-.313	-.294			-.287	-.320	5
6	-.250		-.307	-.303			-.305	-.385	6
7	-.248		-.306	-.158			-.306	-.405	7
8	-.254		-.149	-.081			-.194	-.393	8
9	-.232		-.091	-.127			-.100	-.411	9
10	-.017		-.059	-.068			-.092	-.364	10
11	.000		-.066	-.066			-.052	-.276	11
12	.050		-.026	-.035			-.035	-.209	12
13	.094		-.018	-.035			-.024	-.176	13
14	.294		.134	-.004			.150	-.192	14
15	.370		.254	.057			.314	-.247	15
16	.385		.302	.092			.393	-.305	16
17	.781		1.034	1.080			1.094	.825	17
18	.698		.854	.933			.979	.664	18
19	.714		.758	.825			.854	.525	19
20	.595		.603	.647			.686	.420	20
21	.445		.440	.506			.539	.277	21
22	.487		.491	.524				.231	22
23	.482			.539			.472	.201	23
24	.499		.519	.526			.453	.164	24
25	.486		.488	.499			.436	.192	25
26	.391		.408	.425			.385	.144	26
27								.144	27

α=15 δ=-25

1	-.243		-.301	-.337			-.348	-.331	1
2	-.194		-.252	-.272			-.288	-.233	2
3	-.177		-.247	-.248			-.259	-.217	3
4	-.194		-.252	-.257			-.265	-.278	4
5	-.246		-.309	-.294			-.286	-.335	5
6	-.241		-.302	-.304			-.305	-.391	6
7	-.247		-.306	-.302			-.305	-.404	7
8	-.254		-.295	-.304			-.314	-.392	8
9	-.245		-.270	-.313			-.300	-.404	9
10	-.126		-.072	-.116			-.106	-.383	10
11	-.042		-.073	-.104			-.052	-.332	11
12	.013		-.035	-.062			-.037	-.277	12
13	.072		-.018	-.048			-.016	-.212	13
14	.171		.122	.038			.133	-.239	14
15	.212		.187	.083			.209	-.293	15
16	.239		.211	.100			.228	-.314	16
17	.779		1.028	1.082			1.092	.835	17
18	.694		.853	.934			.978	.662	18
19	.711		.757	.824			.853	.526	19
20	.593		.600	.644			.685	.419	20
21	.442		.437	.499			.539	.278	21
22	.484		.486	.521				.230	22
23	.481			.538			.468	.205	23
24	.500		.516	.523			.450	.162	24
25	.485		.488	.498			.433	.186	25
26	.387		.413	.423			.386	.153	26
27								.153	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=15 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.239		-.300	-.335			-.348	-.336	1
2	-.195		-.250	-.270			-.291	-.237	2
3	-.177		-.244	-.248			-.260	-.221	3
4	-.194		-.252	-.256			-.266	-.278	4
5	-.245		-.308	-.294			-.290	-.326	5
6	-.246		-.304	-.308			-.304	-.391	6
7	-.249		-.310	-.307			-.305	-.421	7
8	-.252		-.296	-.310			-.314	-.402	8
9	-.244		-.286	-.316			-.306	-.404	9
10	-.267		-.263	-.331			-.268	-.393	10
11	-.103		-.126	-.203			-.094	-.357	11
12	-.024		-.060	-.101			-.066	-.282	12
13	.022		-.035	-.090			-.040	-.261	13
14	.061		.039	-.027			.042	-.291	14
15	.082		.065	-.022			.070	-.324	15
16	.087		.074	-.005			.087	-.347	16
17	.777		1.031	1.076			1.087	.822	17
18	.693		.853	.927			.973	.647	18
19	.712		.757	.822			.848	.510	19
20	.595		.603	.642			.678	.403	20
21	.442		.439	.497			.530	.260	21
22	.485		.484	.516				.223	22
23	.482			.534			.465	.187	23
24	.500		.515	.520			.441	.153	24
25	.485		.486	.494			.426	.177	25
26	.386		.410	.422			.379	.140	26
27								.144	27

α=15 δ=-10

1	-.241		-.298	-.331			-.345	-.331	1
2	-.193		-.252	-.272			-.287	-.233	2
3	-.174		-.248	-.245			-.258	-.210	3
4	-.195		-.253	-.254			-.264	-.270	4
5	-.249		-.311	-.294			-.287	-.313	5
6	-.248		-.304	-.306			-.302	-.385	6
7	-.248		-.306	-.306			-.302	-.403	7
8	-.257		-.297	-.304			-.310	-.393	8
9	-.243		-.286	-.314			-.300	-.396	9
10	-.270		-.281	-.329			-.293	-.383	10
11	-.252		-.295	-.330			-.201	-.360	11
12	-.120		-.155	-.206			-.155	-.326	12
13	-.120		-.144	-.195			-.149	-.331	13
14	-.121		-.140	-.192			-.128	-.369	14
15	-.121		-.128	-.192			-.123	-.363	15
16	-.120		-.123	-.192			-.122	-.338	16
17	.773		1.026	1.073			1.085	.827	17
18	.691		.850	.926			.970	.651	18
19	.707		.754	.820			.846	.519	19
20	.593		.600	.641			.677	.413	20
21	.439		.435	.495			.531	.260	21
22	.479		.479	.511				.222	22
23	.478			.528			.462	.188	23
24	.492		.508	.515			.435	.150	24
25	.479		.481	.491			.423	.178	25
26	.383		.409	.417			.375	.131	26
27								.131	27

TABLE V.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.239		-.296	-.326			-.338	-.332	1
2	-.192		-.227	-.269			-.279	-.223	2
3	-.174		-.239	-.244			-.254	-.212	3
4	-.192		-.249	-.253			-.261	-.271	4
5	-.245		-.308	-.289			-.286	-.317	5
6	-.239		-.301	-.299			-.303	-.376	6
7	-.230		-.301	-.306			-.294	-.396	7
8	-.253		-.293	-.305			-.309	-.382	8
9	-.243		-.285	-.306			-.299	-.392	9
10	-.265		-.277	-.329			-.290	-.374	10
11	-.269		-.301	-.333			-.229	-.343	11
12	-.234		-.269	-.306			-.263	-.372	12
13	-.249		-.280	-.321			-.274	-.386	13
14	-.260		-.280	-.321			-.264	-.389	14
15	-.266		-.280	-.321			-.264	-.377	15
16	-.120		-.164	-.259			-.264	-.361	16
17	.772		1.027	1.071			1.082	.828	17
18	.690		.850	.924			.967	.645	18
19	.709		.754	.815			.841	.519	19
20	.592		.599	.638			.676	.404	20
21	.439		.434	.494			.524	.263	21
22	.481		.477	.506				.223	22
23	.477			.522			.456	.197	23
24	.492		.506	.510			.434	.153	24
25	.479		.480	.487			.421	.179	25
26	.383		.406	.412			.373	.142	26
27								.142	27

α=15 δ=10

1	-.239		-.300	-.331			-.340	-.324	1
2	-.186		-.250	-.269			-.287	-.219	2
3	-.172		-.244	-.242			-.257	-.206	3
4	-.192		-.254	-.253			-.263	-.272	4
5	-.248		-.308	-.293			-.291	-.308	5
6	-.239		-.304	-.305			-.303	-.382	6
7	-.242		-.305	-.302			-.304	-.402	7
8	-.253		-.295	-.301			-.310	-.394	8
9	-.232		-.285	-.306			-.298	-.394	9
10	-.261		-.273	-.325			-.290	-.370	10
11	-.264		-.302	-.331			-.221	-.344	11
12	-.336		-.355	-.363			-.342	-.415	12
13	-.352		-.355	-.387			-.357	-.425	13
14	-.347		-.380	-.387			-.355	-.425	14
15	-.357		-.276	-.315			-.357	-.418	15
16	-.225		-.252	-.270			-.260	-.394	16
17	.777		1.029	1.070			1.078	.828	17
18	.692		.853	.925			.968	.658	18
19	.711		.756	.814			.846	.524	19
20	.593		.601	.638			.672	.418	20
21	.441		.436	.496			.523	.269	21
22	.485		.485	.508				.226	22
23	.480			.524			.455	.195	23
24	.496		.508	.511			.434	.151	24
25	.498		.510	.527			.422	.173	25
26	.686		.716	.685			.527	.147	26
27								.142	27

TABLE V.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=15 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.239		-.299	-.334			-.360	-.357	1
2	-.188		-.250	-.270			-.295	-.250	2
3	-.177		-.244	-.246			-.250	-.226	3
4	-.195		-.254	-.249			-.270	-.277	4
5	-.253		-.309	-.292			-.285	-.321	5
6	-.251		-.305	-.303			-.302	-.383	6
7	-.248		-.306	-.305			-.303	-.414	7
8	-.254		-.296	-.302			-.313	-.398	8
9	-.227		-.283	-.305			-.290	-.399	9
10	-.257		-.272	-.327			-.281	-.371	10
11	-.261		-.301	-.333			-.199	-.350	11
12	-.396		-.424	-.421			-.410	-.443	12
13	-.413		-.399	-.410			-.410	-.453	13
14	-.409		-.363	-.393			-.410	-.453	14
15	-.338		-.355	-.381			-.405	-.443	15
16	-.314		-.337	-.357			-.335	-.415	16
17	.767		1.027	1.090			1.134	.858	17
18	.688		.852	.955			1.032	.697	18
19	.708		.757	.875			.927	.570	19
20	.593		.614	.777			.822	.504	20
21	.455		.717	.789			.771	.419	21
22	.805		.836	.862				.414	22
23	.901			.931			.844	.457	23
24	.956		.962	.968			.885	.451	24
25	1.012		1.035	1.023			.944	.543	25
26	1.096		1.114	1.090			1.020	.591	26
27								.591	27

TABLE VI

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.575		.832	.909			.925	.735	1
2	.480		.677	.781			.837	.557	2
3	.500		.615	.685			.722	.413	3
4	.484		.488	.531			.563	.273	4
5	.317		.319	.382			.429	.168	5
6	.322		.314	.365			.374	.078	6
7	.722		.759	.809			.727	.304	7
8	.796		.812	.881			.813	.363	8
9	.837		.865	.938			.893	.471	9
10	.869		.900	.965			.938	.527	10
11	.891		.915	.981			.959	.500	11
12	.898		.949	.995			.970	.519	12
13	.980		.983	1.021			1.000	.614	13
14	1.071		1.052	1.060			1.000	.668	14
15	.977		.992	.971			.908	.578	15
16	.752		.764	.777			.767	.489	16
17	-.206		-.228	-.240			-.245	-.226	17
18	-.157		-.205	-.203			-.196	-.106	18
19	-.150		-.199	-.192			-.184	-.145	19
20	-.176		-.226	-.208			-.209	-.179	20
21	-.239		-.274	-.252			-.247	-.256	21
22	-.234		-.274	-.266				-.318	22
23	-.237			-.272			-.259	-.348	23
24	-.241		-.256	-.272			-.267	-.358	24
25	-.237		-.256	-.282			-.250	-.336	25
26	-.266		-.275	-.296			-.247	-.353	26
27									27
28	-.436		-.438	-.462			-.428	-.446	28
29	-.451		-.469	-.462			-.435	-.466	29
30	-.413		-.457	-.457			-.449	-.467	30
31	-.449		-.387	-.417			-.450	-.479	31
32	-.367		-.374	-.396			-.407	-.470	32

α=-12 δ=-10

1	.578		.836	.918			.927	.738	1
2	.485		.683	.777			.839	.553	2
3	.507		.617	.690			.722	.433	3
4	.491		.497	.539			.559	.281	4
5	.320		.326	.385			.429	.178	5
6	.324		.318	.351			.358	.079	6
7	.322		.313	.348			.325	.059	7
8	.309		.320	.342			.316	.032	8
9	.305		.300	.305			.253	.047	9
10	.277		.292	.290			.202	.034	10
11	.556		.561	.554			.397	-.004	11
12	.649		.687	.690			.602	.290	12
13	.703		.719	.726			.626	.290	13
14	.735		.753	.711			.619	.291	14
15	.699		.719	.659			.586	.291	15
16	.587		.605	.588			.544	.258	16
17	-.198		-.222	-.240			-.253	-.213	17
18	-.148		-.202	-.200			-.198	-.103	18
19	-.145		-.193	-.192			-.184	-.135	19
20	-.168		-.212	-.213			-.211	-.185	20
21	-.229		-.267	-.255			-.253	-.249	21
22	-.225		-.269	-.265				-.312	22
23	-.229			-.275			-.265	-.340	23
24	-.236		-.254	-.271			-.273	-.372	24
25	-.234		-.253	-.283			-.257	-.345	25
26	-.256		-.272	-.297			-.256	-.369	26
27									27
28	-.357		-.355	-.388			-.352	-.417	28
29	-.374		-.377	-.393			-.363	-.403	29
30	-.354		-.384	-.408			-.373	-.412	30
31	-.365		-.384	-.408			-.373	-.427	31
32	-.363		-.384	-.408			-.365	-.418	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.333		.486	.492			.476	.408	1
2	.284		.434	.482			.485	.316	2
3	.297		.386	.434			.467	.275	3
4	.280		.308	.353			.371	.175	4
5	.149		.172	.217			.262	.105	5
6	.542		.584	.629			.603	.231	6
7	.621		.614	.667			.698	.347	7
8	.632		.641	.674			.706	.316	8
9	.645		.654	.691			.708	.365	9
10	.652		.668	.710			.703	.353	10
11	.664		.678	.735			.721	.320	11
12	.656		.694	.762			.725	.304	12
13	.692		.717	.762			.725	.360	13
14	.820		.859	.881			.872	.602	14
15	.902		.960	.979			.993	.748	15
16	.756		.811	.852			.895	.677	16
17	-.057		-.056	-.065			-.049	-.018	17
18	-.033		-.055	-.053			-.039	.028	18
19	-.029		-.059	-.051			-.040	.013	19
20	-.056		-.077	-.077			-.074	-.024	20
21	-.136		-.142	-.133			-.133	-.066	21
22	-.133		-.145	-.151				-.088	22
23	-.133			-.155			-.152	-.037	23
24	-.135		-.151	-.163			-.160	-.097	24
25	-.140		-.160	-.172			-.151	-.078	25
26	-.172		-.184	-.186			-.167	-.208	26
27									27
28	-.428		-.406	-.442			-.451	-.432	28
29	-.406		-.399	-.426			-.456	-.461	29
30	-.387		-.388	-.402			-.456	-.466	30
31	-.381		-.388	-.398			-.422	-.446	31
32	-.355		-.388	-.398			-.389	-.432	32

α=-6 δ=-20

1	.333		.480	.499			.478	.410	1
2	.280		.430	.483			.491	.315	2
3	.295		.382	.439			.475	.286	3
4	.280		.305	.353			.372	.181	4
5	.150		.166	.226			.266	.092	5
6	.150		.143	.179			.215	.040	6
7	.152		.140	.174			.177	-.006	7
8	.153		.264	.352			.156	-.006	8
9	.511		.545	.555			.483	.121	9
10	.570		.574	.578			.540	.261	10
11	.576		.574	.585			.555	.239	11
12	.599		.593	.604			.562	.233	12
13	.656		.621	.626			.600	.306	13
14	.822		.746	.752			.719	.436	14
15	.843		.825	.822			.759	.490	15
16	.679		.688	.702			.687	.447	16
17	-.056		-.053	-.062			-.048	-.009	17
18	-.036		-.053	-.051			-.041	.034	18
19	-.034		-.050	-.050			-.044	.019	19
20	-.062		-.072	-.077			-.079	-.019	20
21	-.134		-.144	-.133			-.132	-.052	21
22	-.131		-.146	-.151				-.089	22
23	-.134			-.153			-.152	-.136	23
24	-.129		-.146	-.157			-.157	-.183	24
25	-.134		-.160	-.165			-.155	-.163	25
26	-.171		-.178	-.180			-.169	-.188	26
27									27
28	-.383		-.392	-.403			-.382	-.369	28
29	-.411		-.407	-.411			-.401	-.398	29
30	-.375		-.420	-.425			-.416	-.432	30
31	-.398		-.420	-.425			-.423	-.427	31
32	-.379		-.388	-.399			-.373	-.427	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.339		.485	.504			.487	.420	1
2	.286		.435	.486			.500	.321	2
3	.302		.384	.447			.482	.277	3
4	.285		.301	.358			.383	.173	4
5	.150		.164	.231			.271	.102	5
6	.155		.148	.184			.222	.024	6
7	.158		.141	.173			.178	- .004	7
8	.144		.147	.172			.155	- .019	8
9	.146		.132	.135			.121	- .016	9
10	.108		.083	.106			.070	- .014	10
11	.218		.078	.096			.070	- .045	11
12	.374		.369	.373			.367	.180	12
13	.379		.411	.402			.347	.209	13
14	.410		.418	.416			.347	.189	14
15	.413		.438	.416			.336	.154	15
16	.398		.393	.377			.323	.121	16
17	- .056		- .055	- .059			- .046	- .014	17
18	- .033		- .050	- .047			- .035	.025	18
19	- .025		- .057	- .047			- .037	.009	19
20	- .058		- .073	- .075			- .075	- .023	20
21	- .133		- .146	- .127			- .129	- .059	21
22	- .130		- .148	- .148				- .095	22
23	- .135			- .150			- .148	- .151	23
24	- .137		- .146	- .152			- .154	- .198	24
25	- .142		- .150	- .158			- .151	- .174	25
26	- .171		- .180	- .180			- .167	- .210	26
27									27
28	- .292		- .300	- .318			- .284	- .315	28
29	- .319		- .309	- .325			- .301	- .276	29
30	- .297		- .319	- .343			- .309	- .295	30
31	- .305		- .319	- .343			- .309	- .336	31
32	- .305		- .319	- .331			- .266	- .357	32

$\alpha = 0$ $\delta = -30$

1	.133		.147	.149			.139	.121	1
2	.096		.150	.143			.144	.103	2
3	.112		.144	.147			.141	.098	3
4	.094		.104	.119			.095	.067	4
5	- .010		- .001	.035			.029	.009	5
6	- .008		.344	.286			.245	.015	6
7	.327		.386	.390			.388	.275	7
8	.379		.395	.401			.396	.275	8
9	.395		.402	.411			.394	.265	9
10	.401		.410	.410			.391	.236	10
11	.413		.414	.410			.418	.202	11
12	.433		.422	.433			.417	.134	12
13	.469		.423	.444			.417	.178	13
14	.775		.494	.606			.538	.343	14
15	.945		.601	.781			.688	.488	15
16	.766		.557	.745			.697	.488	16
17	.132		.141	.133			.143	.126	17
18	.105		.140	.139			.149	.154	18
19	.110		.137	.141			.144	.106	19
20	.092		.107	.110			.109	.069	20
21	- .012		.000	.032			.029	.025	21
22	- .004		- .010	.008				.008	22
23	- .012			- .004			- .001	.068	23
24	- .014		- .031	- .007			- .018	.159	24
25	- .014		- .037	- .030			- .027	.178	25
26	- .061		- .066	- .059			- .052	.095	26
27									27
28	- .428		- .431	- .430			- .431	- .301	28
29	- .432		- .406	- .435			- .444	- .301	29
30	- .377		- .372	- .404			- .427	- .401	30
31	- .363		- .369	- .375			- .396	- .449	31
32	- .339		- .358	- .375			- .369	- .462	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.137		.150	.153			.141	.126	1
2	.103		.155	.150			.147	.108	2
3	.123		.151	.148			.161	.108	3
4	.105		.110	.123			.100	.074	4
5	-.005		.004	.038			.036	.009	5
6	-.004		-.009	.003			.004	.009	6
7	-.002		-.019	-.001			-.001	-.009	7
8	-.016		-.013	-.010			-.015	.019	8
9	.155		.276	.233			.218	-.005	9
10	.330		.340	.340			.322	.246	10
11	.341		.343	.347			.342	.263	11
12	.369		.364	.368			.353	.248	12
13	.421		.391	.402			.386	.304	13
14	.580		.539	.546			.528	.364	14
15	.654		.633	.636			.604	.323	15
16	.573		.567	.596			.571	.272	16
17	.144		.145	.135			.148	.130	17
18	.112		.143	.140			.156	.161	18
19	.113		.143	.143			.148	.107	19
20	.091		.109	.114			.110	.068	20
21	-.003		.006	.030			.035	.026	21
22	-.002		-.001	.004				.006	22
23	-.005			.001			.004	.006	23
24	-.013		-.023	-.008			-.014	-.015	24
25	-.014		-.035	-.027			-.021	.006	25
26	-.057		-.060	-.054			-.049	-.010	26
27									27
28	-.357		-.355	-.355			-.349	-.258	28
29	-.381		-.375	-.378			-.378	-.203	29
30	-.353		-.388	-.387			-.398	-.319	30
31	-.369		-.386	-.387			-.402	-.418	31
32	-.387		-.386	-.387			-.363	-.435	32

$\alpha = 0$ $\delta = -10$

1	.141		.154	.155			.145	.121	1
2	.112		.161	.146			.146	.108	2
3	.124		.154	.152			.143	.107	3
4	.109		.115	.119			.101	.068	4
5	-.001		.006	.037			.033	.005	5
6	-.002		.000	.004			.003	.005	6
7	.002		-.016	-.003			-.005	-.008	7
8	-.008		-.009	-.010			-.017	.005	8
9	-.006		-.032	-.037			-.036	-.013	9
10	-.036		-.056	-.056			-.068	-.013	10
11	.075		-.070	-.065			-.032	-.021	11
12	.200		.185	.183			.189	.176	12
13	.212		.217	.212			.202	.166	13
14	.221		.233	.237			.229	.107	14
15	.236		.257	.238			.229	.073	15
16	.236		.238	.228			.229	.049	16
17	.136		.141	.130			.143	.118	17
18	.113		.142	.134			.146	.149	18
19	.113		.143	.143			.141	.101	19
20	.094		.108	.107			.098	.059	20
21	.001		.004	.032			.025	.011	21
22	.000		-.004	.006				.004	22
23	-.006			-.001			-.004	.005	23
24	-.005		-.025	-.009			-.020	-.014	24
25	-.004		-.035	-.032			-.033	.009	25
26	-.056		-.068	-.062			-.056	-.024	26
27									27
28	-.243		-.239	-.248			-.237	-.208	28
29	-.262		-.266	-.261			-.268	-.180	29
30	-.243		-.262	-.272			-.273	-.142	30
31	-.253		-.260	-.272			-.287	-.163	31
32	-.253		-.260	-.272			-.257	-.219	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.127		.144	.153			.152	.125	1
2	.091		.148	.146			.150	.106	2
3	.115		.143	.149			.151	.106	3
4	.096		.108	.118			.108	.066	4
5	-.014		-.002	.037			.040	.008	5
6	-.016		-.006	.004			.009	.008	6
7	-.010		-.027	-.002			-.005	-.014	7
8	-.020		-.019	-.008			-.012	.001	8
9	-.021		-.043	-.034			-.030	-.014	9
10	-.052		-.063	-.057			-.060	-.013	10
11	-.044		-.095	-.070			-.062	-.029	11
12	-.030		-.073	-.074			-.050	-.045	12
13	-.060		-.067	-.074			-.086	-.059	13
14	-.059		-.067	-.068			-.072	-.053	14
15	-.059		-.067	-.068			-.084	-.047	15
16	-.068		-.073	-.077			-.083	-.042	16
17	.131		.137	.128			.143	.115	17
18	.102		.133	.134			.149	.139	18
19	.105		.136	.140			.144	.087	19
20	.084		.097	.104			.102	.045	20
21	-.014		-.007	.033			.028	.009	21
22	-.010		-.014	.003				.008	22
23	-.010			-.006			-.002	.001	23
24	-.015		-.032	-.009			-.017	-.016	24
25	-.016		-.042	-.031			-.028	.010	25
26	-.072		-.072	-.061			-.052	-.025	26
27									27
28	-.047		-.053	-.068			-.055	-.042	28
29	-.057		-.063	-.068			-.071	-.042	29
30	-.057		-.062	-.073			-.079	-.042	30
31	-.055		-.062	-.063			-.079	-.042	31
32	-.055		-.062	-.062			-.079	-.042	32

$\alpha = 3$ $\delta = 0$

1	.033		.042	.047			.036	.025	1
2	.018		.047	.046			.045	.042	2
3	.034		.038	.041			.039	.052	3
4	.021		.016	.016			-.006	.028	4
5	-.081		-.065	-.059			-.059	-.023	5
6	-.080		-.076	-.078			-.085	-.024	6
7	-.075		-.080	-.089			-.081	-.044	7
8	-.083		-.083	-.092			-.095	-.048	8
9	-.078		-.100	-.111			-.104	-.066	9
10	-.107		-.117	-.128			-.127	-.073	10
11	-.108		-.146	-.140			-.111	-.097	11
12	-.083		-.135	-.140			-.108	-.108	12
13	-.115		-.135	-.140			-.141	-.151	13
14	-.115		-.135	-.140			-.115	-.151	14
15	-.115		-.118	-.140			-.121	-.169	15
16	-.117		-.130	-.140			-.117	-.183	16
17	.235		.297	.276			.297	.252	17
18	.199		.287	.275			.280	.238	18
19	.200		.273	.286			.285	.165	19
20	.178		.204	.234			.233	.110	20
21	.075		.092	.137			.150	.052	21
22	.081		.076	.091				.028	22
23	.074			.087			.105	.006	23
24	.070		.057	.078			.078	-.019	24
25	.068		.047	.055			.065	.008	25
26	.000		.016	.024			.029	-.020	26
27									27
28	.034		.033	.037			-.032	-.045	28
29	.034		.018	.029			-.013	-.044	29
30	.033		.024	.013			-.016	-.054	30
31	.033		.024	.024			-.016	-.059	31
32	.033		.024	.023			-.018	-.050	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.062		-.057	-.056			-.072	-.055	1
2	-.051		-.053	-.054			-.057	-.021	2
3	-.037		-.058	-.056			-.065	-.006	3
4	-.057		-.077	-.080			-.100	-.033	4
5	-.143		-.153	-.136			-.145	-.074	5
6	-.143		-.110	.014			-.151	-.132	6
7	-.040		.159	.156			.152	-.186	7
8	.157		.175	.168			.157	-.118	8
9	.183		.182	.172			.163	-.018	9
10	.200		.183	.175			.171	.013	10
11	.204		.181	.176			.199	.006	11
12	.242		.192	.202			.199	.014	12
13	.287		.193	.200			.226	.151	13
14	.631		.305	.272			.360	.643	14
15	.741		.444	.392			.501	.592	15
16	.622		.444	.410			.530	.505	16
17	.346		.493	.516			.528	.432	17
18	.307		.445	.487			.532	.377	18
19	.304		.391	.447			.495	.276	19
20	.285		.314	.353			.395	.181	20
21	.160		.174	.230			.279	.095	21
22	.172		.161	.194				.052	22
23	.165			.185			.188	.020	23
24	.160		.148	.172			.159	-.008	24
25	.158		.139	.148			.140	.020	25
26	.088		.102	.110			.101	-.004	26
27									27
28	-.402		-.394	-.404			-.404	-.344	28
29	-.422		-.415	-.412			-.416	-.323	29
30	-.415		-.423	-.425			-.428	-.319	30
31	-.415		-.423	-.425			-.423	-.336	31
32	-.384		-.331	-.367			-.344	-.319	32

$\alpha = 6$ $\delta = -20$

1	-.055		-.051	-.054			-.067	-.047	1
2	-.043		-.052	-.055			-.061	-.014	2
3	-.032		-.060	-.059			-.063	-.004	3
4	-.053		-.078	-.083			-.100	-.026	4
5	-.134		-.148	-.137			-.145	-.077	5
6	-.141		-.149	-.163			-.166	-.132	6
7	-.135		-.150	-.169			-.170	-.180	7
8	-.141		-.145	-.171			-.176	-.200	8
9	-.130		-.161	-.190			-.169	-.208	9
10	.037		.091	.069			.104	-.218	10
11	.122		.111	.101			.140	-.234	11
12	.161		.141	.134			.144	.084	12
13	.232		.193	.163			.195	.227	13
14	.357		.329	.290			.345	-.006	14
15	.377		.396	.357			.393	-.004	15
16	.386		.373	.336			.382	.091	16
17	.345		.487	.512			.519	.423	17
18	.306		.441	.487			.525	.384	18
19	.303		.389	.448			.471	.276	19
20	.283		.309	.355			.389	.197	20
21	.164		.175	.232			.268	.112	21
22	.173		.160	.195				.058	22
23	.166			.185			.180	.018	23
24	.162		.144	.170			.155	-.005	24
25	.158		.135	.149			.131	.028	25
26	.088		.098	.111			.094	-.025	26
27									27
28	-.282		-.285	-.290			-.295	-.328	28
29	-.321		-.307	-.309			-.320	-.328	29
30	-.306		-.311	-.321			-.329	-.261	30
31	-.305		-.315	-.321			-.343	-.217	31
32	-.305		-.315	-.321			-.310	-.217	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.065		-.063	-.057			-.062	-.048	1
2	-.055		-.059	-.057			-.053	-.016	2
3	-.040		-.060	-.062			-.057	-.005	3
4	-.061		-.081	-.081			-.095	-.029	4
5	-.149		-.152	-.141			-.140	-.078	5
6	-.146		-.153	-.166			-.158	-.135	6
7	-.141		-.165	-.167			-.162	-.179	7
8	-.151		-.151	-.166			-.167	-.193	8
9	-.143		-.172	-.186			-.163	-.207	9
10	-.172		-.187	-.201			-.181	-.221	10
11	-.125		-.203	-.203			-.114	-.232	11
12	.016		-.006	-.030			.005	-.118	12
13	.021		.014	-.004			.020	-.081	13
14	.039		.026	.000			.044	-.174	14
15	.038		.048	.011			.055	-.231	15
16	.038		.032	.010			.068	-.186	16
17	.340		.488	.510			.519	.415	17
18	.298		.435	.490			.525	.364	18
19	.299		.385	.447			.490	.273	19
20	.278		.304	.351			.387	.181	20
21	.158		.171	.233			.276	.095	21
22	.165		.155	.196				.038	22
23	.158			.186			.185	.013	23
24	.157		.141	.172			.155	-.014	24
25	.153		.135	.149			.136	.020	25
26	.077		.091	.114			.100	-.018	26
27									27
28	-.123		-.111	-.120			-.123	-.212	28
29	-.141		-.145	-.137			-.159	-.234	29
30	-.136		-.137	-.159			-.171	-.203	30
31	-.136		-.137	-.141			-.173	-.161	31
32	-.136		-.140	-.142			-.165	-.136	32

$\alpha=6$ $\delta=0$

1	-.061		-.055	-.056			-.061	-.045	1
2	-.047		-.055	-.057			-.053	-.006	2
3	-.036		-.061	-.056			-.059	.004	3
4	-.054		-.078	-.080			-.092	-.023	4
5	-.143		-.149	-.138			-.138	-.068	5
6	-.140		-.147	-.162			-.161	-.116	6
7	-.132		-.153	-.167			-.162	-.165	7
8	-.144		-.149	-.165			-.171	-.192	8
9	-.141		-.167	-.190			-.168	-.195	9
10	-.167		-.178	-.201			-.183	-.208	10
11	-.158		-.205	-.213			-.150	-.224	11
12	-.139		-.184	-.203			-.151	-.215	12
13	-.170		-.184	-.203			-.179	-.246	13
14	-.168		-.184	-.203			-.164	-.238	14
15	-.168		-.184	-.203			-.165	-.238	15
16	-.168		-.184	-.203			-.154	-.258	16
17	.339		.485	.506			.510	.417	17
18	.303		.441	.486			.515	.374	18
19	.300		.383	.441			.488	.282	19
20	.272		.308	.353			.383	.186	20
21	.157		.172	.228			.268	.105	21
22	.171		.157	.191				.054	22
23	.162			.177			.178	.024	23
24	.152		.143	.167			.150	-.006	24
25	.152		.133	.142			.133	.021	25
26	.080		.095	.109			.099	-.011	26
27									27
28	.117		.127	.122			.102	-.033	28
29	.110		.115	.112			.073	-.039	29
30	.110		.115	.098			.058	-.048	30
31	.110		.115	.108			.052	-.058	31
32	.110		.107	.108			.052	-.057	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.060		-.055	-.054			-.055	-.047	1
2	-.048		-.048	-.051			-.048	-.010	2
3	-.035		-.049	-.055			-.050	.003	3
4	-.064		-.073	-.081			-.090	-.021	4
5	-.138		-.144	-.137			-.136	-.071	5
6	-.139		-.146	-.160			-.158	-.120	6
7	-.134		-.150	-.159			-.160	-.165	7
8	-.141		-.141	-.162			-.165	-.190	8
9	-.131		-.163	-.181			-.161	-.192	9
10	-.154		-.174	-.195			-.178	-.209	10
11	-.149		-.198	-.207			-.136	-.229	11
12	-.263		-.323	-.331			-.285	-.321	12
13	-.338		-.333	-.340			-.330	-.294	13
14	-.309		-.336	-.353			-.325	-.316	14
15	-.316		-.334	-.347			-.315	-.345	15
16	-.333		-.334	-.347			-.329	-.367	16
17	.343		.490	.503			.507	.397	17
18	.304		.438	.491			.514	.363	18
19	.304		.386	.443			.491	.270	19
20	.284		.305	.351			.385	.179	20
21	.162		.176	.231			.269	.092	21
22	.173		.159	.192				.048	22
23	.164			.181			.183	.018	23
24	.160		.144	.174			.151	-.013	24
25	.158		.134	.147			.132	.015	25
26	.089		.095	.109			.092	-.026	26
27									27
28	.408		.420	.401			.410	.229	28
29	.440		.464	.469			.427	.249	29
30	.462		.488	.475			.329	.217	30
31	.480		.489	.475			.403	.193	31
32	.442		.461	.451			.391	.166	32

$\alpha=6$ $\delta=20$

1	-.056		-.057	-.054			-.060	-.044	1
2	-.047		-.054	-.052			-.051	-.004	2
3	-.032		-.056	-.058			-.055	.001	3
4	-.051		-.077	-.081			-.092	-.026	4
5	-.138		-.150	-.141			-.136	-.083	5
6	-.143		-.148	-.157			-.161	-.117	6
7	-.133		-.151	-.164			-.161	-.163	7
8	-.140		-.147	-.166			-.170	-.188	8
9	-.133		-.166	-.174			-.163	-.188	9
10	-.158		-.172	-.197			-.177	-.149	10
11	-.152		-.201	-.206			-.137	-.066	11
12	-.349		-.404	-.408			-.384	-.389	12
13	-.418		-.423	-.425			-.418	-.399	13
14	-.399		-.427	-.432			-.418	-.431	14
15	-.399		-.425	-.432			-.410	-.430	15
16	-.334		-.330	-.374			-.410	-.430	16
17	.342		.485	.498			.494	.393	17
18	.304		.432	.480			.502	.347	18
19	.301		.381	.436			.480	.262	19
20	.279		.301	.344			.376	.179	20
21	.160		.166	.226			.261	.093	21
22	.169		.154	.190				.045	22
23	.160			.178			.171	.016	23
24	.386		.489	.511			.226	-.009	24
25	.549		.568	.575			.531	.266	25
26	.586		.583	.596			.570	.297	26
27									27
28	.610		.611	.609			.585	.248	28
29	.653		.619	.653			.639	.296	29
30	.820		.733	.803			.747	.465	30
31	.856		.809	.868			.814	.532	31
32	.672		.685	.732			.719	.483	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.054		-.052	-.051			-.054	-.040	1
2	-.043		-.051	-.048			-.049	.003	2
3	-.032		-.058	-.050			-.057	.003	3
4	-.054		-.074	-.075			-.090	-.023	4
5	-.137		-.148	-.136			-.139	-.057	5
6	-.148		-.147	-.161			-.163	-.096	6
7	-.136		-.150	-.159			-.161	-.038	7
8	-.148		-.144	-.165			-.169	-.082	8
9	-.129		-.161	-.174			-.160	-.117	9
10	-.160		-.172	-.201			-.179	-.200	10
11	-.152		-.199	-.201			-.132	-.234	11
12	-.375		-.415	-.447			-.445	-.462	12
13	-.421		-.403	-.438			-.470	-.475	13
14	-.382		-.386	-.413			-.464	-.475	14
15	-.379		-.382	-.402			-.418	-.465	15
16	-.367		-.382	-.397			-.399	-.441	16
17	.341		.490	.492			.494	.404	17
18	.308		.479	.479			.501	.363	18
19	.303		.388	.436			.477	.270	19
20	.283		.309	.345			.377	.181	20
21	.162		.180	.245			.264	.097	21
22	.590		.606	.662				.362	22
23	.645			.684			.738	.397	23
24	.659		.672	.699			.748	.374	24
25	.677		.689	.712			.749	.404	25
26	.686		.693	.736			.749	.377	26
27									27
28	.711		.735	.784			.776	.307	28
29	.727		.748	.810			.791	.358	29
30	.825		.908	.940			.945	.617	30
31	.892		.998	1.004			1.082	.782	31
32	.740		.856	.877			.954	.711	32

$\alpha=9$ $\delta=0$

1	-.159		-.145	-.144			-.154	-.131	1
2	-.135		-.140	-.135			-.139	-.062	2
3	-.119		-.148	-.137			-.137	-.078	3
4	-.137		-.163	-.158			-.166	-.113	4
5	-.214		-.229	-.209			-.209	-.169	5
6	-.209		-.224	-.227			-.226	-.260	6
7	-.209		-.224	-.235			-.224	-.296	7
8	-.217		-.211	-.235			-.236	-.309	8
9	-.206		-.228	-.246			-.222	-.309	9
10	-.233		-.234	-.262			-.231	-.309	10
11	-.227		-.264	-.268			-.190	-.309	11
12	-.180		-.228	-.256			-.202	-.287	12
13	-.214		-.228	-.256			-.233	-.310	13
14	-.214		-.228	-.256			-.217	-.310	14
15	-.214		-.228	-.256			-.217	-.319	15
16	-.214		-.228	-.256			-.217	-.319	16
17	.453		.698	.775			.819	.624	17
18	.410		.566	.658			.737	.496	18
19	.409		.500	.589			.639	.367	19
20	.377		.429	.467			.499	.258	20
21	.242		.259	.325			.361	.140	21
22	.255		.248	.284				.091	22
23	.242			.271			.262	.059	23
24	.243		.236	.262			.236	.032	24
25	.235		.227	.237			.214	.066	25
26	.155		.181	.200			.172	.010	26
27									27
28	.213		.221	.213			.169	-.016	28
29	.199		.207	.200			.139	-.025	29
30	.199		.209	.184			.129	-.033	30
31	.199		.200	.198			.129	-.029	31
32	.199		.200	.186			.121	-.032	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.207		-.220	-.235			-.261	-.262	1
2	-.157		-.198	-.203			-.220	-.168	2
3	-.151		-.199	-.199			-.206	-.171	3
4	-.171		-.210	-.213			-.226	-.224	4
5	-.236		-.272	-.260			-.262	-.280	5
6	-.232		-.271	-.241			-.282	-.365	6
7	-.233		-.026	-.014			-.044	-.398	7
8	-.144		-.014	.000			-.030	-.386	8
9	.034		-.011	.004			-.029	-.399	9
10	.054		.004	.008			-.030	-.232	10
11	.056		-.003	.005			-.003	-.199	11
12	.096		.011	.011			-.001	-.203	12
13	.125		.011	.011			-.011	-.179	13
14	.444		.156	.049			.129	-.048	14
15	.530		.304	.122			.295	-.139	15
16	.480		.328	.147			.378	-.194	16
17	.600		.871	.948			.980	.718	17
18	.532		.711	.809			.873	.580	18
19	.546		.634	.711			.744	.422	19
20	.496		.510	.551			.591	.316	20
21	.341		.346	.415			.446	.179	21
22	.359		.346	.378				.125	22
23	.338			.371			.343	.107	23
24	.336		.338	.361			.316	.066	24
25	.328		.328	.340			.295	.106	25
26	.244		.277	.293			.256	.043	26
27									27
28	-.355		-.349	-.359			-.377	-.386	28
29	-.387		-.374	-.374			-.381	-.387	29
30	-.370		-.377	-.383			-.401	-.387	30
31	-.386		-.386	-.383			-.401	-.384	31
32	-.368		-.386	-.383			-.378	-.384	32

α=12 δ=-20

1	-.203		-.221	-.242			-.277	-.252	1
2	-.165		-.200	-.209			-.228	-.158	2
3	-.149		-.204	-.203			-.215	-.159	3
4	-.170		-.215	-.219			-.234	-.223	4
5	-.234		-.272	-.266			-.271	-.272	5
6	-.234		-.275	-.279			-.290	-.364	6
7	-.238		-.267	-.283			-.291	-.394	7
8	-.241		-.258	-.297			-.297	-.382	8
9	-.230		-.260	-.305			-.278	-.383	9
10	-.191		-.087	-.175			-.103	-.383	10
11	-.043		-.041	-.086			-.028	-.347	11
12	.043		-.013	-.039			-.015	-.232	12
13	.084		.024	-.013			-.018	-.163	13
14	.175		.134	.057			.144	-.202	14
15	.183		.184	.123			.185	-.262	15
16	.194		.173	.113			.185	-.301	16
17	.598		.868	.937			.966	.719	17
18	.535		.705	.797			.859	.571	18
19	.542		.633	.703			.735	.423	19
20	.495		.502	.535			.579	.320	20
21	.337		.334	.395			.432	.178	21
22	.357		.339	.365				.130	22
23	.332			.358			.328	.105	23
24	.333		.330	.344			.303	.072	24
25	.325		.321	.329			.279	.101	25
26	.236		.263	.276			.247	.059	26
27									27
28	-.221		-.221	-.229			-.241	-.324	28
29	-.248		-.247	-.238			-.258	-.338	29
30	-.236		-.247	-.253			-.277	-.309	30
31	-.236		-.247	-.253			-.265	-.304	31
32	-.236		-.247	-.253			-.265	-.304	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.207		-.223	-.234			-.254	-.246	1
2	-.168		-.201	-.201			-.213	-.155	2
3	-.154		-.203	-.198			-.201	-.155	3
4	-.165		-.213	-.211			-.223	-.213	4
5	-.240		-.271	-.257			-.254	-.268	5
6	-.233		-.270	-.272			-.273	-.363	6
7	-.234		-.263	-.276			-.278	-.374	7
8	-.240		-.252	-.276			-.284	-.374	8
9	-.232		-.258	-.293			-.266	-.374	9
10	-.253		-.261	-.305			-.267	-.374	10
11	-.219		-.272	-.303			-.174	-.374	11
12	-.077		-.131	-.169			-.117	-.287	12
13	-.091		-.108	-.163			-.115	-.277	13
14	-.083		-.092	-.149			-.083	-.320	14
15	-.077		-.077	-.150			-.084	-.345	15
16	-.077		-.088	-.150			-.079	-.340	16
17	.588		.859	.932			.968	.717	17
18	.526		.700	.800			.860	.573	18
19	.531		.627	.703			.736	.423	19
20	.490		.503	.537			.586	.320	20
21	.335		.333	.401			.433	.186	21
22	.352		.338	.371				.127	22
23	.330			.361			.333	.100	23
24	.328		.328	.349			.307	.062	24
25	.320		.317	.329			.285	.102	25
26	.231		.265	.281			.246	.042	26
27									27
28	-.018		-.019	-.023			-.055	-.192	28
29	-.044		-.033	-.042			-.078	-.207	29
30	-.040		-.033	-.055			-.086	-.217	30
31	-.026		-.039	-.047			-.086	-.213	31
32	-.029		-.039	-.048			-.086	-.204	32

$\alpha = 12$ $\delta = 0$

1	-.215		-.224	-.233			-.256	-.238	1
2	-.174		-.198	-.198			-.212	-.144	2
3	-.163		-.203	-.193			-.195	-.144	3
4	-.174		-.218	-.208			-.221	-.200	4
5	-.255		-.277	-.259			-.251	-.258	5
6	-.242		-.273	-.269			-.272	-.335	6
7	-.239		-.269	-.282			-.273	-.367	7
8	-.254		-.259	-.278			-.278	-.359	8
9	-.241		-.262	-.297			-.262	-.369	9
10	-.261		-.266	-.309			-.265	-.369	10
11	-.261		-.294	-.311			-.217	-.358	11
12	-.214		-.277	-.312			-.252	-.354	12
13	-.261		-.276	-.311			-.285	-.374	13
14	-.261		-.276	-.310			-.270	-.373	14
15	-.261		-.275	-.310			-.270	-.391	15
16	-.261		-.275	-.310			-.270	-.377	16
17	.578		.854	.929			.967	.725	17
18	.519		.695	.796			.860	.571	18
19	.516		.621	.699			.737	.430	19
20	.482		.496	.535			.580	.321	20
21	.323		.331	.398			.430	.190	21
22	.341		.335	.367				.126	22
23	.321			.357			.337	.101	23
24	.321		.327	.337			.310	.067	24
25	.316		.313	.319			.285	.100	25
26	.227		.258	.275			.251	.053	26
27									27
28	.300		.316	.305			.249	.020	28
29	.289		.301	.300			.223	.020	29
30	.296		.301	.272			.217	.010	30
31	.299		.301	.286			.208	.008	31
32	.299		.292	.273			.202	.008	32

TABLE VI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.209		-.222	-.233			-.244	-.238	1
2	-.170		-.197	-.196			-.208	-.154	2
3	-.155		-.203	-.191			-.192	-.154	3
4	-.175		-.216	-.213			-.217	-.218	4
5	-.244		-.268	-.254			-.252	-.263	5
6	-.238		-.274	-.268			-.269	-.354	6
7	-.239		-.270	-.276			-.269	-.372	7
8	-.242		-.254	-.273			-.274	-.372	8
9	-.225		-.256	-.282			-.257	-.372	9
10	-.252		-.256	-.302			-.260	-.372	10
11	-.245		-.281	-.309			-.203	-.334	11
12	-.305		-.386	-.402			-.354	-.399	12
13	-.386		-.401	-.415			-.392	-.399	13
14	-.370		-.407	-.423			-.392	-.430	14
15	-.382		-.407	-.423			-.392	-.430	15
16	-.357		-.358	-.377			-.394	-.422	16
17	.587		.862	.936			.969	.712	17
18	.529		.700	.797			.859	.566	18
19	.532		.630	.703			.740	.422	19
20	.491		.508	.540			.582	.316	20
21	.331		.339	.401			.435	.180	21
22	.351		.340	.366				.125	22
23	.329			.361			.338	.093	23
24	.327		.331	.349			.308	.062	24
25	.330		.374	.367			.285	.100	25
26	.650		.686	.682			.552	.060	26
27									27
28	.761		.777	.786			.699	.320	28
29	.804		.814	.839			.751	.358	29
30	.833		.852	.833			.750	.418	30
31	.786		.794	.759			.708	.389	31
32	.640		.651	.641			.625	.355	32

α=12 δ=20

1	-.207		-.221	-.230			-.244	-.244	1
2	-.172		-.198	-.196			-.206	-.156	2
3	-.159		-.203	-.191			-.194	-.155	3
4	-.173		-.216	-.212			-.216	-.207	4
5	-.244		-.270	-.255			-.248	-.261	5
6	-.238		-.275	-.268			-.268	-.349	6
7	-.241		-.264	-.275			-.269	-.364	7
8	-.245		-.253	-.273			-.271	-.364	8
9	-.227		-.259	-.276			-.249	-.363	9
10	-.254		-.256	-.301			-.260	-.363	10
11	-.246		-.282	-.305			-.192	-.292	11
12	-.355		-.449	-.454			-.431	-.444	12
13	-.451		-.461	-.481			-.455	-.474	13
14	-.436		-.426	-.450			-.465	-.480	14
15	-.447		-.392	-.417			-.460	-.480	15
16	-.352		-.377	-.397			-.410	-.474	16
17	.588		.855	.932			.964	.718	17
18	.525		.704	.797			.858	.573	18
19	.531		.627	.703			.735	.411	19
20	.485		.498	.535			.578	.309	20
21	.329		.337	.398			.434	.171	21
22	.352		.602	.723				.295	22
23	.810			.891			.821	.423	23
24	.867		.890	.953			.884	.440	24
25	.911		.941	1.020			.963	.543	25
26	.949		.980	1.061			1.025	.586	26
27									27
28	.997		1.018	1.089			1.057	.621	28
29	1.052		1.055	1.126			1.091	.687	29
30	1.105		1.105	1.104			1.041	.669	30
31	1.003		1.008	.975			.931	.588	31
32	.771		.788	.799			.804	.518	32

TABLE VI.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 5.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 15$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .278		- .350	- .385			- .408	- .391	1
2	- .223		- .286	- .305			- .332	- .263	2
3	- .211		- .279	- .278			- .292	- .263	3
4	- .221		- .284	- .289			- .302	- .319	4
5	- .284		- .334	- .325			- .328	- .367	5
6	- .268		- .340	- .338			- .341	- .410	6
7	- .278		- .336	- .341			- .338	- .440	7
8	- .288		- .323	- .339			- .346	- .420	8
9	- .272		- .311	- .345			- .332	- .438	9
10	- .296		- .304	- .361			- .326	- .417	10
11	- .294		- .329	- .361			- .262	- .393	11
12	- .237		- .316	- .358			- .297	- .412	12
13	- .297		- .315	- .358			- .326	- .435	13
14	- .291		- .315	- .358			- .310	- .446	14
15	- .291		- .315	- .358			- .323	- .440	15
16	- .291		- .315	- .358			- .316	- .427	16
17	.790		1.050	1.089			1.095	.819	17
18	.716		.865	.936			.975	.653	18
19	.719		.766	.818			.846	.508	19
20	.601		.607	.646			.687	.399	20
21	.453		.449	.509			.561	.253	21
22	.513		.515	.552				.222	22
23	.497			.557			.479	.194	23
24	.516		.542	.534			.456	.156	24
25	.502		.499	.506			.436	.185	25
26	.393		.416	.422			.363	.132	26
27									27
28	.436		.436	.421			.341	.092	28
29	.421		.421	.408			.316	.089	29
30	.433		.421	.375			.323	.086	30
31	.433		.421	.396			.323	.077	31
32	.416		.404	.370			.310	.066	32

TABLE VII

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = -12$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.600		.859	.932			.949	.729	1
2	.508		.703	.793			.856	.555	2
3	.522		.634	.702			.741	.423	3
4	.511		.517	.552			.580	.280	4
5	.342		.342	.397			.449	.166	5
6	.344		.336	.367			.373	.086	6
7	.345		.335	.370			.345	.059	7
8	.331		.342	.364			.334	.031	8
9	.404		.499	.446			.301	.039	9
10	.684		.720	.727			.622	.207	10
11	.737		.720	.776			.681	.271	11
12			.777	.788			.678	.345	12
13	.802		.821	.828			.722	.403	13
14	.843		.859	.848			.769	.446	14
15	.794		.812	.784			.722	.411	15
16	.639		.664	.661			.632	.387	16
17	-.188		-.217	-.233		-.235	-.234		17
18	-.113		-.194	-.192		-.184	-.117		18
19	-.137		-.191	-.178		-.176	-.154		19
20	-.158		-.204	-.198		-.199	-.195		20
21	-.219		-.263	-.239		-.237	-.257		21
22	-.212		-.265	-.252			-.326		22
23	-.216			-.257		-.251	-.347		23
24	-.219		-.247	-.259		-.257	-.365		24
25	-.217		-.247	-.267		-.246	-.351		25
26	-.243		-.267	-.278		-.242	-.370		26
28	-.347		-.360	-.382		-.345	-.367		28
29			-.367	-.377		-.351	-.355		29
30	-.331		-.373	-.396		-.356	-.413		30
31			-.372	-.398		-.356	-.433		31
32	-.367		-.370	-.398		-.352	-.426		32

$\alpha = -12$ $\delta = 20$

1	.618		.886	.968			.970	.756	1
2	.526		.727	.822			.877	.580	2
3	.548		.660	.727			.755	.442	3
4	.530		.532	.570			.599	.296	4
5	.364		.357	.423			.463	.187	5
6	.360		.357	.390			.393	.099	6
7	.359		.356	.392			.363	.074	7
8	.342		.359	.382			.340	.045	8
9	.333		.335	.351			.302	.059	9
10	.275		.277	.301			.241	.051	10
11	.303		.277	.278			.209	.019	11
12			-.211	-.215		-.230	-.337		12
13	-.227		-.230	-.229		-.266	-.336		13
14	-.199		-.236	-.229		-.264	-.302		14
15	-.212		-.227	-.235		-.259	-.291		15
16	-.227		-.235	-.235		-.265	-.291		16
17	-.193		-.226	-.248		-.263	-.252		17
18	-.135		-.199	-.207		-.210	-.140		18
19	-.142		-.191	-.192		-.196	-.177		19
20	-.161		-.204	-.207		-.210	-.207		20
21	-.223		-.262	-.247		-.249	-.281		21
22	-.218		-.267	-.264			-.345		22
23	-.222			-.269		-.266	-.368		23
24	-.226		-.247	-.271		-.275	-.387		24
25	-.226		-.059	-.050		-.097	-.368		25
26	-.010		-.004	-.025		-.012	-.385		26
28	.051		-.005	-.031		-.010	-.170		28
29			.027	-.010		.024	-.107		29
30	.264		.175	.086		.192	-.177		30
31			.265	.152		.299	-.236		31
32	.311		.264	.152		.310	-.291		32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.349		.487	.489			.478	.403	1
2	.292		.432	.484			.482	.292	2
3	.298		.379	.444			.471	.262	3
4	.295		.312	.359			.374	.169	4
5	.162		.178	.234			.269	.090	5
6	.166		.291	.516			.227	.024	6
7	.591		.572	.634			.633	.294	7
8	.620		.582	.652			.659	.292	8
9	.634		.604	.661			.673	.338	9
10	.642		.647	.670			.674	.333	10
11	.648		.647	.684			.681	.306	11
12			.678	.687			.674	.336	12
13	.651		.709	.691			.681	.373	13
14	.783		.869	.772			.818	.581	14
15	.866		.958	.848			.911	.681	15
16	.703		.793	.747			.827	.658	16
17	-.038		-.044	-.049			-.038	-.022	17
18	.041		-.041	-.042			-.032	.024	18
19	-.028		-.043	-.040			-.036	.011	19
20	-.049		-.060	-.069			-.068	-.027	20
21	-.121		-.136	-.124			-.118	-.060	21
22	-.117		-.138	-.142				-.085	22
23	-.122			-.146			-.140	-.119	23
24	-.125		-.139	-.148			-.149	-.034	24
25	-.125		-.149	-.155			-.142	-.027	25
26	-.162		-.170	-.171			-.158	-.137	26
28	-.416		-.426	-.440			-.421	-.457	28
29			-.438	-.428			-.432	-.448	29
30	-.417		-.448	-.452			-.446	-.443	30
31			-.450	-.457			-.445	-.428	31
32	-.432		-.441	-.421			-.422	-.432	32

α=-6 δ=-20

1	.342		.487	.497			.482	.401	1
2	.290		.431	.483			.485	.295	2
3	.297		.379	.441			.473	.261	3
4	.292		.308	.357			.374	.166	4
5	.160		.177	.230			.273	.089	5
6	.160		.158	.187			.224	.021	6
7	.183		.399	.511			.204	-.007	7
8	.527		.546	.588			.541	.186	8
9	.579		.565	.605			.603	.296	9
10	.604		.592	.617			.616	.309	10
11	.609		.591	.624			.622	.282	11
12			.612	.629			.612	.295	12
13	.652		.636	.639			.629	.335	13
14	.846		.766	.759			.763	.470	14
15	.882		.847	.839			.829	.555	15
16	.703		.711	.733			.746	.536	16
17	-.044		-.045	-.056			-.038	-.021	17
18	-.013		-.046	-.041			-.029	.024	18
19	-.022		-.044	-.039			-.033	.007	19
20	-.051		-.060	-.066			-.068	-.029	20
21	-.122		-.136	-.122			-.115	-.065	21
22	-.123		-.137	-.143				-.089	22
23	-.123			-.146			-.136	-.127	23
24	-.130		-.141	-.145			-.144	-.164	24
25	-.129		-.149	-.155			-.141	-.132	25
26	-.162		-.177	-.170			-.151	-.041	26
28	-.385		-.395	-.412			-.338	-.435	28
29			-.408	-.408			-.402	-.427	29
30	-.361		-.420	-.428			-.415	-.431	30
31			-.418	-.427			-.415	-.410	31
32	-.411		-.417	-.426			-.408	-.421	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-6$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.349		.491	.505			.489	.402	1
2	.289		.431	.490			.495	.300	2
3	.303		.384	.450			.477	.262	3
4	.297		.315	.365			.382	.162	4
5	.164		.178	.236			.278	.090	5
6	.162		.164	.195			.226	.019	6
7	.165		.155	.185			.189 -	.001	7
8	.154		.160	.178			.163 -	.011	8
9	.160		.139	.183			.126 -	.011	9
10	.125		.101	.111			.082 -	.016	10
11	.348		.101	.339			.303 -	.037	11
12			.473	.475			.413	.285	12
13	.497		.540	.533			.463	.323	13
14	.547		.583	.586			.502	.292	14
15	.563		.588	.572			.490	.255	15
16	.512		.531	.521			.460	.241	16
17 -	.037		- .042	- .050			- .036	- .022	17
18 -	.016		- .040	- .039			- .028	.021	18
19 -	.021		- .037	- .037			- .031	.012	19
20 -	.044		- .057	- .066			- .063	- .025	20
21 -	.119		- .130	- .118			- .120	- .064	21
22 -	.116		- .132	- .136				- .091	22
23 -	.118			- .139			- .136	- .129	23
24 -	.122		- .133	- .141			- .144	- .164	24
25 -	.122		- .143	- .150			- .139	- .147	25
26 -	.160		- .173	- .165			- .150	- .186	26
28 -	.277		- .292	- .307			- .281	- .292	28
29			- .301	- .309			- .284	- .235	29
30 -	.260		- .304	- .316			- .284	- .287	30
31			- .304	- .315			- .285	- .333	31
32 -	.296		- .304	- .317			- .279	- .361	32

$\alpha=-6$ $\delta=0$

1	.351		.495	.505			.494	.408	1
2	.293		.438	.494			.504	.309	2
3	.306		.388	.454			.485	.271	3
4	.297		.317	.364			.390	.169	4
5	.167		.179	.238			.283	.092	5
6	.166		.166	.195			.234	.024	6
7	.167		.154	.191			.190 -	.005	7
8	.152		.164	.184			.164 -	.011	8
9	.151		.143	.149			.134 -	.016	9
10	.108		.105	.115			.092 -	.016	10
11	.134		.105	.105			.068 -	.044	11
12			.101	.147			.141 -	.005	12
13	.145		.145	.151			.116	.014	13
14	.134		.154	.155			.107 -	.001	14
15	.139		.154	.149			.099 -	.019	15
16	.137		.145	.134			.085 -	.017	16
17 -	.038		- .041	- .048			- .035	- .024	17
18 -	.019		- .040	- .041			- .029	.017	18
19 -	.019		- .039	- .037			- .032	.006	19
20 -	.046		- .055	- .061			- .062	- .032	20
21 -	.119		- .129	- .119			- .113	- .069	21
22 -	.116		- .135	- .137				- .102	22
23 -	.119			- .139			- .135	- .140	23
24 -	.121		- .136	- .143			- .143	- .176	24
25 -	.119		- .142	- .149			- .137	- .155	25
26 -	.162		- .170	- .164			- .148	- .195	26
28 -	.112		- .135	- .156			- .121	- .196	28
29			- .127	- .146			- .111	- .186	29
30 -	.115		- .127	- .146			- .110	- .267	30
31			- .125	- .146			- .105	- .234	31
32 -	.117		- .127	- .146			- .100	- .244	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=0 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.143		.160	.164			.157	.102	1
2	.106		.159	.159			.155	.092	2
3	.120		.154	.160			.147	.089	3
4	.111		.124	.130			.103	.049	4
5	.012		.015	.052			.043	.006	5
6	.058		.354	.380			.354	.010	6
7	.373		.376	.420			.419	.272	7
8	.393		.379	.431			.427	.276	8
9	.412		.395	.402			.428	.271	9
10	.425		.418	.436			.421	.230	10
11	.433		.414	.454			.440	.189	11
12			.427	.441			.437	.202	12
13	.473		.441	.436			.420	.205	13
14	.729		.561	.543			.530	.372	14
15	.868		.684	.683			.654	.537	15
16	.717		.642	.668			.666	.577	16
17	.151		.163	.150			.163	.126	17
18	.125		.163	.161			.168	.155	18
19	.131		.166	.166			.162	.105	19
20	.113		.126	.136			.131	.064	20
21	.016		.022	.056			.049	.016	21
22	.022		.011	.028				.004	22
23	.014			.020			.018	.102	23
24	.005		- .012	.012			.006	.175	24
25	.004		- .013	- .007		-	.009	.172	25
26	- .038		- .041	- .036		-	.037	.075	26
28	- .422		- .428	- .431		-	.412	- .290	28
29			- .436	- .417		-	.430	- .279	29
30	- .401		- .446	- .443		-	.440	- .357	30
31			- .450	- .446		-	.407	- .408	31
32	- .430		- .396	- .390		-	.358	- .420	32

α=0 δ=-25

1	.139		.160	.165			.160	.110	1
2	.106		.163	.163			.156	.097	2
3	.126		.155	.160			.145	.097	3
4	.112		.114	.134			.104	.054	4
5	.004		.017	.047			.046	.016	5
6	.006		.006	.012			.012	.007	6
7	.042		.332	.349			.309	.005	7
8	.336		.357	.379			.391	.242	8
9	.369		.367	.400			.392	.281	9
10	.396		.385	.405			.401	.262	10
11	.396		.384	.404			.408	.237	11
12			.385	.400			.396	.227	12
13	.456		.403	.408			.390	.247	13
14	.717		.515	.543			.535	.363	14
15	.813		.631	.682			.659	.423	15
16	.666		.588	.654			.652	.445	16
17	.158		.175	.154			.167	.127	17
18	.125		.160	.160			.173	.164	18
19	.127		.168	.162			.163	.112	19
20	.103		.123	.134			.126	.069	20
21	.014		.022	.056			.048	.015	21
22	.012		.012	.030				.005	22
23	.011			.019			.020	- .001	23
24	.008		- .011	.013			.005	- .011	24
25	- .001		- .016	- .006		-	.012	.110	25
26	- .032		- .044	- .031		-	.036	.129	26
28	- .382		- .387	- .386		-	.371	- .197	28
29			- .401	- .392		-	.402	- .205	29
30	- .350		- .408	- .411		-	.417	- .338	30
31			- .408	- .412		-	.417	- .398	31
32	- .415		- .403	- .415		-	.408	- .422	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.143		.165	.166			.153	.117	1
2	.106		.160	.160			.161	.102	2
3	.121		.151	.161			.150	.096	3
4	.109		.117	.119			.108	.060	4
5	.000		.013	.047			.054	.011	5
6	.009		.005	.012			.016	.005	6
7	.008		- .003	.008			.014	- .007	7
8	- .004		.002	.008		-	.001	.009	8
9	.252		.320	.327			.318	.091	9
10	.350		.355	.361			.357	.265	10
11	.363		.356	.351			.365	.261	11
12			.371	.367			.357	.264	12
13	.406		.402	.400			.388	.312	13
14	.587		.555	.548			.536	.372	14
15	.668		.653	.643			.623	.342	15
16	.570		.595	.597			.605	.327	16
17	.152		.163	.153			.163	.134	17
18	.125		.160	.158			.163	.164	18
19	.126		.162	.160			.165	.102	19
20	.108		.119	.130			.124	.057	20
21	.012		.014	.050			.056	.019	21
22	.012		.006	.025				.007	22
23	.012			.013			.021	.004	23
24	.012		- .007	.012			.005	.004	24
25	.007		- .013	- .011		-	.009	.010	25
26	- .043		- .048	- .039		-	.032	.009	26
28	- .327		- .336	- .333		-	.315	- .194	28
29			- .352	- .337		-	.348	- .162	29
30	- .297		- .352	- .358		-	.353	- .254	30
31			- .358	- .360		-	.357	- .373	31
32	- .347		- .360	- .361		-	.353	- .422	32

$\alpha = 0$ $\delta = -10$

1	.124		.154	.161			.154	.117	1
2	.093		.156	.164			.159	.096	2
3	.107		.146	.164			.153	.091	3
4	.098		.115	.138			.110	.057	4
5	- .003		.008	.045			.045	.011	5
6	- .002		.002	.013			.017	.000	6
7	- .001		- .006	.009			.015	- .012	7
8	- .012		- .006	.008			.000	- .001	8
9	- .003		- .026	.004		-	.018	- .015	9
10	- .037		- .047	- .046		-	.053	- .014	10
11	.137		- .047	- .025			.064	- .016	11
12			.215	.220			.222	.235	12
13	.254		.275	.272			.272	.230	13
14	.275		.307	.311			.304	.170	14
15	.282		.317	.313			.309	.137	15
16	.287		.306	.301			.305	.127	16
17	.143		.161	.150			.157	.125	17
18	.110		.157	.158			.165	.157	18
19	.116		.161	.160			.165	.099	19
20	.104		.118	.125			.119	.052	20
21	.002		.013	.047			.046	.009	21
22	.006		.010	.025				.002	22
23	.005			.013			.016	- .005	23
24	.000		- .008	.012			.006	- .015	24
25	- .001		- .023	- .008		-	.009	.002	25
26	- .055		- .048	- .044		-	.043	- .026	26
28	- .202		- .207	- .207		-	.190	- .167	28
29			- .217	- .211		-	.214	- .122	29
30	- .199		- .220	- .219		-	.215	- .094	30
31			- .217	- .220		-	.220	- .115	31
32	- .217		- .222	- .216		-	.226	- .132	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.134		.156	.164			.159	.117	1
2	.096		.158	.161			.165	.105	2
3	.111		.149	.160			.160	.096	3
4	.100		.116	.133			.117	.056	4
5	-.004		.012	.048			.053	.011	5
6	-.002		.006	.012			.020	.000	6
7	.004	- .005	.013				.019	- .009	7
8	-.013	- .005	.010				.004	- .004	8
9	-.012	- .023	- .018			-	.012	- .017	9
10	-.046	- .051	- .043			-	.042	- .015	10
11	-.026	- .050	- .059			-	.050	- .036	11
12		- .035	- .012				.004	.036	12
13	.000	- .007	- .005			-	.007	.026	13
14	-.011	- .006	.000				.001	.015	14
15	-.005	.000	- .001				.000	.016	15
16	-.010	- .005	- .004			-	.001	.015	16
17	.143		.158	.147			.161	.117	17
18	.114		.154	.160			.166	.152	18
19	.111		.159	.160			.163	.095	19
20	.094		.112	.125			.117	.051	20
21	.003		.012	.049			.051	.015	21
22	.002		.007	.025				.004	22
23	.009			.014			.015	.000	23
24	.003	- .012		.015			.001	- .009	24
25	.000	- .022	- .006			-	.011	.000	25
26	-.057	- .051	- .039			-	.039	- .022	26
28	-.004	- .015	- .005				.004	.019	28
29		- .012	- .004				.000	.017	29
30	-.017	- .005	- .007			-	.006	.014	30
31		- .006	- .006			-	.002	.016	31
32	-.015	- .012	- .011			-	.004	.014	32

$\alpha = 0$ $\delta = 10$

1	.140		.161	.172			.155	.129	1
2	.107		.167	.170			.169	.111	2
3	.129		.164	.170			.160	.102	3
4	.112		.126	.142			.114	.067	4
5	.005		.018	.055			.055	.017	5
6	.015		.011	.015			.025	.010	6
7	.013	- .005		.010			.019	- .001	7
8	-.008	- .003		.011			.004	.004	8
9	.003	- .015	- .020			-	.018	- .010	9
10	-.030	- .039	- .042			-	.043	- .011	10
11	-.019	- .039	- .055			-	.050	- .019	11
12		- .210	- .207			-	.195	- .165	12
13	-.190	- .219	- .220			-	.219	- .134	13
14	-.196	- .220	- .220			-	.212	- .105	14
15	-.200	- .212	- .215			-	.216	- .122	15
16	-.205	- .216	- .217			-	.221	- .137	16
17	.151		.168	.140			.157	.115	17
18	.127		.154	.150			.158	.150	18
19	.122		.161	.152			.160	.104	19
20	.105		.117	.122			.116	.066	20
21	.007		.018	.044			.044	.021	21
22	.015		.014	.023				.009	22
23	.014			.010			.009	.002	23
24	.009	- .011		.005		-	.007	- .009	24
25	.004	- .013	- .016			-	.014	.016	25
26	-.048	- .049	- .042			-	.042	- .010	26
28	.244		.225	.217			.252	.229	28
29			.272	.279			.284	.216	29
30	.274		.305	.311			.305	.166	30
31			.316	.313			.312	.145	31
32	.286		.306	.301			.310	.125	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.133		.153	.173			.160	.126	1
2	.100		.155	.165			.165	.106	2
3	.108		.152	.167			.161	.100	3
4	.093		.118	.138			.118	.061	4
5	.000		.007	.049			.055	.014	5
6	-.005		.003	.013			.022	.001	6
7	-.001	-.009		.012			.023	-.010	7
8	-.012	-.008		.008			.004	-.001	8
9	-.010	-.021	-.011			-.011	-.010		9
10	-.043	-.042	-.042			-.038	.031		10
11	-.024	-.042	-.052			-.049	.079		11
12		-.347	-.347			-.335	-.219		12
13	-.333	-.362	-.360			-.367	-.165		13
14	-.333	-.366	-.366			-.370	-.266		14
15	-.336	-.362	-.368			-.368	-.400		15
16	-.365	-.367	-.365			-.375	-.421		16
17	.137		.150	.134			.150	.107	17
18	.106		.150	.148			.157	.145	18
19	.118		.153	.151			.149	.087	19
20	.095		.111	.117			.106	.046	20
21	-.004		.000	.040			.038	.006	21
22	.002		.002	.013				.000	22
23	.001			.007			.006	-.005	23
24	-.005	-.013		.030		-.005	-.016		24
25	.295	.343		.337			.337	.159	25
26	.347	.362		.366			.373	.270	26
28	.367	.358		.373			.362	.250	28
29		.386		.418			.406	.292	29
30	.593	.513		.587			.565	.383	30
31		.617		.681			.654	.368	31
32	.570	.566		.623			.622	.340	32

$\alpha = 0$ $\delta = 25$

1	.141		.164	.168			.160	.129	1
2	.108		.169	.164			.166	.111	2
3	.128		.160	.164			.159	.099	3
4	.114		.118	.142			.114	.061	4
5	.002		.014	.051			.049	.019	5
6	.006		.003	.011			.022	.004	6
7	.010	-.001		.010			.012	-.007	7
8	-.002	-.002		.000		-.004	.039		8
9	.003	-.020	-.021			-.015	.151		9
10	-.038	-.044	-.046			-.045	.126		10
11	-.022	-.044	-.058			-.054	.039		11
12		-.385	-.396			-.385	-.245		12
13	-.368	-.407	-.411			-.412	-.224		13
14	-.368	-.418	-.418			-.416	-.350		14
15	-.396	-.413	-.416			-.422	-.415		15
16	-.422	-.411	-.418			-.412	-.433		16
17	.144		.151	.137			.140	.111	17
18	.116		.156	.145			.151	.150	18
19	.121		.158	.142			.144	.094	19
20	.099		.114	.113			.108	.051	20
21	.007		.011	.037			.037	.015	21
22	.007	-.002		.007				.004	22
23	.166			.333			.366	.184	23
24	.344		.377	.365			.383	.259	24
25	.376		.393	.381			.391	.277	25
26	.403		.393	.398			.390	.251	26
28	.398		.393	.405			.391	.195	28
29			.402	.440			.403	.214	29
30	.718		.495	.641			.521	.358	30
31			.601	.809			.651	.448	31
32	.674		.553	.736			.629	.461	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=6 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.054		-.052	-.042			-.055	-.057	1
2	-.042		-.049	-.045			-.036	-.010	2
3	-.033		-.048	-.045			-.042	-.006	3
4	-.042		-.066	-.065			-.081	-.035	4
5	-.132		-.148	-.125			-.125	-.087	5
6	-.133		.065	.137			-.004	-.145	6
7	.132		.188	.197			.190	-.069	7
8	.172		.186	.206			.184	-.050	8
9	.201		.189	.203			.188	.011	9
10	.214		.197	.209			.203	.056	10
11	.217		.197	.211			.230	.040	11
12			.201	.206			.214	.074	12
13	.274		.200	.206			.262	.249	13
14	.618		.292	.269			.431	.678	14
15	.757		.431	.377			.572	.586	15
16	.626		.440	.400			.587	.502	16
17	.342		.491	.516			.516	.405	17
18	.297		.439	.496			.526	.358	18
19	.307		.396	.450			.509	.261	19
20	.281		.317	.371			.398	.182	20
21	.166		.180	.243			.278	.094	21
22	.177		.165	.203				.045	22
23	.165			.193			.197	.014	23
24	.164		.154	.185			.171	-.009	24
25	.163		.141	.157			.149	.011	25
26	.092		.099	.121			.104	.040	26
28	-.387		-.385	-.391			-.380	-.322	28
29			-.400	-.382			-.397	-.279	29
30	-.351		-.411	-.403			-.415	-.294	30
31			-.410	-.406			-.413	-.302	31
32	-.410		-.410	-.406			-.401	-.290	32

α=6 δ=-25

1	-.042		-.044	-.041			-.053	-.047	1
2	-.037		-.038	-.039			-.043	-.014	2
3	-.025		-.042	-.045			-.043	-.007	3
4	-.039		-.070	-.073			-.080	-.032	4
5	-.121		-.134	-.126			-.129	-.082	5
6	-.132		-.135	-.130			-.138	-.140	6
7	-.100		-.113	.087			.022	-.184	7
8	-.111		.143	.163			.170	-.195	8
9	.157		.167	.180			.185	-.197	9
10	.197		.174	.183			.189	.007	10
11	.209		.190	.184			.211	.034	11
12			.177	.180			.190	.024	12
13	.277		.190	.181			.186	.189	13
14	.525		.327	.267			.306	.355	14
15	.597		.471	.376			.436	.355	15
16	.528		.467	.383			.447	.438	16
17	.355		.494	.509			.524	.403	17
18	.311		.449	.494			.522	.357	18
19	.310		.393	.454			.505	.261	19
20	.283		.315	.359			.398	.175	20
21	.170		.177	.234			.284	.097	21
22	.180		.168	.197				.047	22
23	.166			.189			.189	.016	23
24	.165		.151	.175			.163	-.015	24
25	.163		.140	.149			.146	.015	25
26	.102		.105	.120			.104	-.022	26
28	-.330		-.330	-.337			-.327	-.336	28
29			-.347	-.338			-.358	-.301	29
30	-.302		-.353	-.356			-.367	-.241	30
31			-.351	-.356			-.368	-.231	31
32	-.350		-.357	-.357			-.375	-.229	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.040		-.036	-.041			-.054	-.046	1
2	-.019		-.036	-.041			-.036	-.011	2
3	-.017		-.038	-.040			-.045	-.004	3
4	-.040		-.059	-.058			-.079	-.032	4
5	-.127		-.132	-.114			-.128	-.084	5
6	-.118		-.130	-.139			-.147	-.136	6
7	-.117		-.135	-.154			-.142	-.185	7
8	-.118		-.127	-.150			-.154	-.206	8
9	-.101		-.127	.038			.107	-.204	9
10	.140		.153	.135			.160	-.214	10
11	.170		.157	.141			.175	-.135	11
12			.165	.140			.154	.131	12
13	.224		.226	.180			.184	.267	13
14	.380		.381	.311			.338	.051	14
15	.440		.446	.386			.423	.100	15
16	.420		.426	.373			.416	.240	16
17	.359		.506	.509			.515	.403	17
18	.317		.460	.497			.521	.361	18
19	.322		.397	.455			.505	.267	19
20	.287		.315	.359			.392	.174	20
21	.171		.186	.238			.283	.094	21
22	.182		.168	.201				.047	22
23	.168			.191			.190	.012	23
24	.171		.154	.180			.168	-.007	24
25	.163		.141	.160			.142	.016	25
26	.097		.107	.122			.101	-.020	26
28	-.276		-.275	-.277			-.264	-.318	28
29			-.292	-.281			-.301	-.292	29
30	-.251		-.291	-.282			-.306	-.219	30
31			-.292	-.290			-.309	-.164	31
32	-.291		-.297	-.297			-.316	-.164	32

$\alpha = 6$ $\delta = -10$

1	-.050		-.043	-.038			-.055	-.046	1
2	-.047		-.041	-.034			-.037	.000	2
3	-.028		-.032	-.040			-.042	-.004	3
4	-.057		-.062	-.062			-.083	-.029	4
5	-.133		-.131	-.119			-.124	-.082	5
6	-.132		-.139	-.147			-.146	-.135	6
7	-.127		-.141	-.148			-.143	-.176	7
8	-.133		-.136	-.150			-.155	-.206	8
9	-.126		-.156	-.162			-.152	-.200	9
10	-.153		-.167	-.185			-.162	-.212	10
11	-.012		-.166	-.161			-.047	-.231	11
12			.042	.026			.061	-.010	12
13	.092		.099	.066			.111	.044	13
14	.106		.125	.097			.152	-.162	14
15	.116		.134	.105			.165	-.185	15
16	.124		.134	.107			.161	-.116	16
17	.348		.496	.505			.512	.395	17
18	.308		.439	.489			.517	.357	18
19	.308		.384	.446			.499	.261	19
20	.280		.308	.355			.395	.176	20
21	.161		.180	.238			.286	.085	21
22	.171		.169	.195				.042	22
23	.165			.184			.191	.012	23
24	.159		.151	.166			.166	-.012	24
25	.155		.137	.160			.147	.007	25
26	.087		.103	.128			.102	-.027	26
28	-.107		-.111	-.109			-.117	-.194	28
29			-.115	-.107			-.140	-.205	29
30	-.100		-.115	-.115			-.149	-.182	30
31			-.116	-.119			-.159	-.149	31
32	-.114		-.121	-.121			-.159	-.119	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.051		-.047	-.038			-.050	-.047	1
2	-.045		-.045	-.037			-.041	-.017	2
3	-.034		-.050	-.041			-.046	-.009	3
4	-.044		-.072	-.055			-.085	-.030	4
5	-.131		-.136	-.122			-.126	-.084	5
6	-.134		-.138	-.145			-.146	-.140	6
7	-.130		-.146	-.154			-.148	-.176	7
8	-.142		-.133	-.153			-.160	-.206	8
9	-.130		-.154	-.167			-.158	-.204	9
10	-.158		-.171	-.185			-.172	-.215	10
11	-.150		-.171	-.198			-.154	-.235	11
12			-.145	-.156			-.124	-.180	12
13	-.116		-.130	-.149			-.119	-.175	13
14	-.112		-.126	-.142			-.105	-.239	14
15	-.109		-.119	-.144			-.097	-.244	15
16	-.117		-.126	-.144			-.095	-.256	16
17	.346		.486	.498			.504	.375	17
18	.309		.440	.477			.506	.345	18
19	.302		.387	.434			.496	.255	19
20	.274		.309	.350			.380	.175	20
21	.158		.179	.228			.274	.091	21
22	.169		.163	.190				.040	22
23	.161			.180			.185	.006	23
24	.160		.144	.160			.159	-.014	24
25	.153		.135	.146			.130	.006	25
26	.084		.096	.112			.095	-.037	26
28	.124		.126	.129			.111	-.006	28
29			.127	.139			.102	-.007	29
30	.109		.126	.132			.090	-.024	30
31			.125	.126			.080	-.036	31
32	.115		.119	.116			.080	-.034	32

$\alpha = 6$ $\delta = 10$

1	-.043		-.036	-.032			-.037	-.045	1
2	-.027		-.043	-.037			-.027	-.014	2
3	-.020		-.043	-.035			-.030	-.005	3
4	-.036		-.060	-.056			-.067	-.031	4
5	-.123		-.130	-.114			-.113	-.081	5
6	-.124		-.128	-.144			-.133	-.130	6
7	-.122		-.140	-.137			-.133	-.167	7
8	-.120		-.129	-.137			-.139	-.201	8
9	-.122		-.151	-.153			-.136	-.196	9
10	-.147		-.164	-.174			-.153	-.210	10
11	-.140		-.164	-.184			-.142	-.221	11
12			-.295	-.309			-.274	-.289	12
13	-.284		-.306	-.323			-.296	-.271	13
14	-.281		-.307	-.321			-.290	-.309	14
15	-.287		-.305	-.322			-.285	-.346	15
16	-.299		-.304	-.323			-.289	-.377	16
17	.348		.490	.505			.507	.370	17
18	.318		.443	.505			.511	.335	18
19	.310		.390	.450			.501	.250	19
20	.281		.311	.363			.395	.162	20
21	.165		.181	.244			.279	.081	21
22	.177		.166	.206				.036	22
23	.174			.190			.193	.005	23
24	.165		.150	.189			.163	-.022	24
25	.161		.138	.160			.143	-.001	25
26	.096		.098	.119			.100	-.032	26
28	.440		.440	.466			.432	.271	28
29			.496	.523			.455	.294	29
30	.517		.548	.560			.462	.254	30
31			.552	.546			.453	.217	31
32	.481		.495	.496			.441	.202	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.048		-.040	-.032			-.040	-.045	1
2	-.041		-.041	-.034			-.033	-.006	2
3	-.033		-.046	-.035			-.039	-.005	3
4	-.048		-.069	-.056			-.077	-.027	4
5	-.121		-.136	-.124			-.117	-.082	5
6	-.133		-.136	-.145			-.142	-.127	6
7	-.123		-.132	-.146			-.141	-.172	7
8	-.135		-.130	-.149			-.152	-.199	8
9	-.129		-.146	-.161			-.144	-.152	9
10	-.151		-.163	-.185			-.162	-.060	10
11	-.141		-.163	-.191			-.148	-.149	11
12			-.398	-.410			-.381	-.426	12
13	-.378		-.411	-.420			-.408	-.418	13
14	-.378		-.421	-.425			-.412	-.435	14
15	-.402		-.417	-.426			-.410	-.423	15
16	-.425		-.420	-.432			-.411	-.426	16
17	.343		.485	.493			.497	.370	17
18	.308		.438	.473			.497	.330	18
19	.305		.388	.432			.481	.250	19
20	.282		.311	.352			.376	.167	20
21	.166		.180	.232			.263	.087	21
22	.173		.159	.195				.037	22
23	.252			.483			.285	.020	23
24	.538		.575	.581			.559	.232	24
25	.579		.604	.611			.608	.307	25
26	.608		.615	.628			.622	.300	26
28	.600		.605	.634			.617	.274	28
29			.616	.679			.632	.299	29
30	.827		.716	.863			.771	.472	30
31			.797	.916			.846	.565	31
32	.689		.676	.767			.758	.522	32

$\alpha=6$ $\delta=25$

1	-.048		-.038	-.037			-.044	-.057	1
2	-.045		-.035	-.034			-.034	-.014	2
3	-.024		-.041	-.033			-.038	-.001	3
4	-.038		-.069	-.054			-.078	-.026	4
5	-.125		-.129	-.116			-.122	-.079	5
6	-.123		-.132	-.142			-.144	-.122	6
7	-.121		-.138	-.147			-.144	-.125	7
8	-.122		-.127	-.145			-.151	-.055	8
9	-.123		-.147	-.159			-.138	-.107	9
10	-.146		-.157	-.185			-.156	-.181	10
11	-.139		-.156	-.188			-.150	-.239	11
12			-.436	-.445			-.423	-.456	12
13	-.417		-.450	-.456			-.447	-.447	13
14	-.405		-.460	-.463			-.452	-.458	14
15	-.443		-.460	-.466			-.448	-.436	15
16	-.386		-.402	-.442			-.447	-.438	16
17	.349		.485	.493			.484	.367	17
18	.311		.439	.484			.499	.331	18
19	.307		.381	.441			.480	.247	19
20	.281		.309	.350			.383	.162	20
21	.160		.182	.235			.266	.080	21
22	.192		.539	.513				.034	22
23	.601			.645			.654	.325	23
24	.622		.628	.663			.677	.301	24
25	.635		.646	.678			.682	.351	25
26	.647		.654	.689			.684	.323	26
28	.636		.652	.696			.673	.302	28
29			.654	.714			.689	.331	29
30	.842		.743	.873			.832	.570	30
31			.824	.964			.927	.693	31
32	.741		.708	.824			.846	.641	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.209		-.215	-.234			-.257	-.276	1
2	-.161		-.196	-.193			-.216	-.176	2
3	-.151		-.196	-.189			-.199	-.182	3
4	-.178		-.209	-.208			-.221	-.244	4
5	-.231		-.260	-.255			-.253	-.297	5
6	-.224		-.137	-.012			-.206	-.381	6
7	-.225		-.013	.003			-.028	-.401	7
8	-.015		-.012	.007			-.017	-.386	8
9	.026		-.011	.000			-.020	-.372	9
10	.052		.012	.015			-.026	-.227	10
11	.055		.015	.015			.012	-.240	11
12			.006	.009			.000	-.245	12
13	.121		.000	.005			-.017	-.177	13
14	.503		.132	.047			.105	.059	14
15	.596		.269	.115			.286	-.105	15
16	.518		.307	.145			.385	-.131	16
17	.581		.884	.955			.975	.709	17
18	.525		.718	.821			.872	.558	18
19	.557		.649	.717			.746	.417	19
20	.505		.522	.556			.591	.310	20
21	.355		.353	.417			.443	.175	21
22	.365		.352	.383				.115	22
23	.346			.377			.346	.090	23
24	.348		.348	.359			.323	.074	24
25	.339		.332	.336			.302	.085	25
26	.254		.270	.295			.243	.039	26
28	-.351		-.346	-.351			-.343	-.413	28
29			-.360	-.347			-.370	-.382	29
30	-.316		-.363	-.365			-.380	-.383	30
31			-.367	-.366			-.381	-.391	31
32	-.365		-.370	-.371			-.385	-.393	32

α=12 δ=-25

1	-.193		-.218	-.234			-.270	-.260	1
2	-.153		-.187	-.201			-.217	-.167	2
3	-.144		-.193	-.194			-.199	-.177	3
4	-.163		-.207	-.209			-.219	-.234	4
5	-.229		-.256	-.251			-.252	-.290	5
6	-.223		-.269	-.240			-.264	-.372	6
7	-.222		-.231	-.138			-.249	-.387	7
8	-.226		-.096	-.018			-.071	-.383	8
9	-.151		.000	-.012			-.025	-.387	9
10	.045		.020	-.005			-.020	-.350	10
11	.058		.020	-.010			.003	-.232	11
12			.002	-.007			-.010	-.187	12
13	.111		.016	-.009			.000	-.091	13
14	.325		.177	.057			.175	-.106	14
15	.391		.306	.135			.330	-.204	15
16	.381		.312	.155			.383	-.257	16
17	.586		.876	.959			.981	.713	17
18	.537		.727	.813			.873	.570	18
19	.561		.650	.716			.754	.426	19
20	.511		.517	.554			.597	.315	20
21	.358		.355	.409			.448	.177	21
22	.368		.354	.377				.121	22
23	.350			.378			.352	.096	23
24	.351		.344	.368			.323	.064	24
25	.345		.334	.341			.298	.089	25
26	.253		.282	.294			.242	.037	26
28	-.275		-.271	-.272			-.266	-.366	28
29			-.285	-.279			-.307	-.347	29
30	-.249		-.287	-.290			-.312	-.333	30
31			-.290	-.290			-.316	-.331	31
32	-.287		-.296	-.295			-.323	-.327	32

TABLE VII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.196		-.206	-.233			-.252	-.270	1
2	-.160		-.196	-.200			-.215	-.174	2
3	-.154		-.200	-.194			-.195	-.176	3
4	-.167		-.204	-.207			-.217	-.235	4
5	-.232		-.262	-.265			-.249	-.290	5
6	-.225		-.262	-.269			-.271	-.372	6
7	-.227		-.256	-.265			-.264	-.393	7
8	-.232		-.245	-.270			-.277	-.390	8
9	-.216		-.234	-.191			-.215	-.393	9
10	-.063		-.010	-.048			-.036	-.386	10
11	.008		-.010	-.036			-.002	-.331	11
12			-.014	-.040			-.036	-.194	12
13	.082		.029	-.020			.022	-.117	13
14	.212		.169	.081			.180	-.182	14
15	.235		.240	.141			.259	-.236	15
16	.264		.232	.140			.261	-.307	16
17	.582		.878	.958			.985	.714	17
18	.539		.728	.823			.870	.567	18
19	.561		.649	.721			.752	.418	19
20	.509		.524	.561			.603	.311	20
21	.353		.349	.416			.446	.180	21
22	.370		.353	.385				.115	22
23	.352			.381			.351	.096	23
24	.347		.343	.370			.325	.064	24
25	.337		.338	.347			.302	.089	25
26	.250		.280	.300			.253	.037	26
28	-.210		-.207	-.206			-.220	±.325	28
29			-.217	-.209			-.249	-.337	29
30	-.192		-.219	-.220			-.252	-.306	30
31			-.222	-.225			-.256	-.300	31
32	-.214		-.225	-.226			-.260	-.292	32

α=12 δ=-10

1	-.197		-.220	-.227			-.257	-.262	1
2	-.157		-.193	-.190			-.215	-.167	2
3	-.152		-.198	-.191			-.193	-.175	3
4	-.160		-.211	-.209			-.221	-.232	4
5	-.238		-.265	-.252			-.255	-.286	5
6	-.223		-.263	-.265			-.276	-.367	6
7	-.224		-.258	-.269			-.272	-.391	7
8	-.229		-.246	-.273			-.277	-.387	8
9	-.227		-.249	-.278			-.264	-.391	9
10	-.248		-.248	-.297			-.263	-.387	10
11	-.146		-.247	-.279			-.131	±.370	11
12			-.099	-.144			-.102	-.255	12
13	-.040		-.060	-.117			-.065	-.237	13
14	-.026		-.029	-.094			-.019	-.287	14
15	-.020		-.019	-.089			-.010	-.332	15
16	-.022		-.021	-.084			-.014	-.346	16
17	.587		.879	.952			.979	.712	17
18	.541		.727	.815			.863	.566	18
19	.558		.638	.720			.749	.420	19
20	.499		.519	.556			.592	.316	20
21	.355		.357	.416			.442	.177	21
22	.365		.354	.379				.116	22
23	.352			.376			.348	.092	23
24	.345		.345	.357			.324	.061	24
25	.330		.336	.343			.294	.087	25
26	.245		.277	.290			.248	.035	26
28	-.004		.000	.004			-.017	-.172	28
29			-.001	.004			-.041	-.181	29
30	-.007		-.007	.000			-.045	-.190	30
31			-.007	-.009			-.055	-.187	31
32	-.005		-.010	-.016			-.061	-.191	32

TABLE VII.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 6.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.187		.215	.234			.248	.254	1
2	.157		.192	.197			.214	.160	2
3	.142		.196	.193			.196	.171	3
4	.154		.206	.209			.216	.230	4
5	.228		.259	.252			.249	.286	5
6	.225		.266	.264			.274	.373	6
7	.222		.260	.268			.267	.352	7
8	.229		.248	.271			.282	.391	8
9	.220		.253	.280			.260	.392	9
10	.239		.258	.295			.259	.393	10
11	.237		.258	.304			.221	.380	11
12			.242	.276			.234	.342	12
13	.211		.232	.270			.227	.332	13
14	.209		.230	.266			.214	.356	14
15	.210		.222	.266			.206	.385	15
16	.214		.224	.266			.215	.391	16
17	.592		.877	.952			.973	.708	17
18	.546		.712	.808			.871	.565	18
19	.560		.646	.712			.749	.411	19
20	.505		.513	.551			.590	.304	20
21	.350		.347	.407			.444	.169	21
22	.363		.350	.382				.111	22
23	.348			.378			.344	.082	23
24	.346		.345	.360			.316	.054	24
25	.338		.334	.342			.297	.077	25
26	.251		.282	.287			.252	.026	26
28	.284		.295	.307			.262	.022	28
29			.295	.305			.239	.019	29
30	.276		.292	.299			.225	.009	30
31			.292	.281			.211	.005	31
32	.280		.269	.269			.202	.004	32

α=12 δ=10

1	.194		.210	.233			.237	.251	1
2	.155		.194	.197			.204	.159	2
3	.145		.199	.189			.184	.165	3
4	.157		.207	.206			.204	.226	4
5	.232		.264	.250			.240	.276	5
6	.225		.264	.266			.260	.362	6
7	.226		.262	.263			.259	.385	7
8	.231		.250	.267			.266	.386	8
9	.221		.250	.274			.245	.387	9
10	.242		.249	.289			.252	.378	10
11	.239		.248	.301			.221	.325	11
12			.361	.387			.343	.373	12
13	.341		.373	.400			.365	.370	13
14	.342		.380	.406			.361	.426	14
15	.365		.375	.405			.362	.437	15
16	.370		.376	.402			.361	.433	16
17	.583		.872	.949			.977	.707	17
18	.540		.710	.809			.871	.558	18
19	.550		.642	.717			.750	.411	19
20	.501		.511	.552			.596	.305	20
21	.347		.348	.410			.448	.165	21
22	.362		.346	.381				.110	22
23	.344			.375			.350	.085	23
24	.340		.341	.361			.321	.051	24
25	.419		.561	.551			.332	.081	25
26	.703		.739	.752			.664	.215	26
28	.771		.781	.808			.726	.370	28
29			.818	.854			.777	.406	29
30	.844		.857	.851			.777	.441	30
31			.797	.779			.713	.392	31
32	.633		.647	.649			.636	.353	32

TABLE VIII

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=-12\ \delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.593		.862	.936			.944	.754	1
2	.510		.705	.799			.851	.577	2
3	.542		.638	.705			.736	.447	3
4	.509		.519	.554			.572	.300	4
5	.340		.344	.403			.441	.198	5
6	.341		.339	.367			.372	.100	6
7	.335		.337	.367			.340	.066	7
8	.327		.341	.352			.307	.044	8
9	.308		.316	.311			.278	.044	9
10	.251		.259	.279			.226	.044	10
11	.260		.212	.240			.178	.018	11
12	.767		.784	.783			.627	.313	12
13	.741		.764	.744			.595	.317	13
14	.707		.727	.684			.572	.259	14
15	.664		.676	.646			.547	.249	15
16	.592		.586	.566			.516	.224	16
17	-.189		-.215	-.237		-.240	-.217		17
18	-.142		-.191	-.198		-.187	-.104		18
19	-.139		-.188	-.185		-.187	-.138		19
20	-.161		-.201	-.206		-.206	-.190		20
21	-.219		-.261	-.247		-.243	-.245		21
22	-.212		-.261	-.260			-.309		22
23	-.220			-.268		-.260	-.332		23
24	-.222		-.246	-.269		-.262	-.367		24
25	-.224		-.247	-.273		-.251	-.338		25
26	-.255		-.263	-.281		-.247	-.364		26

$\alpha=-12\ \delta=0$

1	.596		.861	.942			.945	.755	1
2	.510		.706	.804			.851	.583	2
3	.545		.641	.709			.738	.452	3
4	.514		.521	.555			.573	.302	4
5	.345		.342	.404			.442	.200	5
6	.349		.342	.369			.374	.105	6
7	.346		.338	.367			.343	.069	7
8	.329		.343	.353			.309	.050	8
9	.311		.320	.312			.278	.051	9
10	.255		.262	.280			.229	.053	10
11	.261		.217	.243			.182	.023	11
12	.217		.209	.225			.140	-.034	12
13	.209		.208	.197			.141	-.023	13
14	.197		.208	.197			.128	-.036	14
15	.198		.197	.192			.128	-.045	15
16	.198		.197	.179			.106	-.063	16
17	-.188		-.213	-.242		-.243	-.224		17
18	-.143		-.191	-.200		-.200	-.098		18
19	-.135		-.186	-.188		-.188	-.131		19
20	-.158		-.199	-.205		-.205	-.179		20
21	-.219		-.258	-.250		-.245	-.252		21
22	-.211		-.262	-.269			-.308		22
23	-.216			-.269		-.263	-.337		23
24	-.221		-.244	-.270		-.269	-.354		24
25	-.221		-.245	-.277		-.254	-.348		25
26	-.254		-.262	-.291		-.254	-.361		26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.596		.865	.944			.950	.757	1
2	.510		.708	.801			.859	.576	2
3	.543		.639	.710			.742	.448	3
4	.513		.521	.557			.578	.305	4
5	.341		.344	.404			.448	.202	5
6	.344		.344	.371			.379	.108	6
7	.342		.339	.370			.348	.074	7
8	.328		.343	.357			.315	.045	8
9	.311		.320	.316			.282	.045	9
10	.254		.262	.284			.233	.045	10
11	.262		.218	.247			.186	.023	11
12 -	.059	-	.068	- .064		-	.119	- .227	12
13 -	.084	-	.084	- .085		-	.119	- .223	13
14 -	.080	-	.089	- .091		-	.124	- .229	14
15 -	.090	-	.089	- .091		-	.134	- .228	15
16 -	.090	-	.089	- .106		-	.141	- .228	16
17 -	.192	-	.220	- .241		-	.248	- .224	17
18 -	.147	-	.195	- .201		-	.201	- .115	18
19 -	.139	-	.192	- .188		-	.192	- .144	19
20 -	.162	-	.204	- .204		-	.209	- .187	20
21 -	.221	-	.263	- .247		-	.248	- .249	21
22 -	.214	-	.268	- .264				- .324	22
23 -	.219			- .268		-	.264	- .341	23
24 -	.223	-	.249	- .268		-	.272	- .372	24
25 -	.224	-	.250	- .276		-	.255	- .349	25
26 -	.256	-	.269	- .291		-	.252	- .363	26

α=-12 δ=20

1	.606		.875	.956			.957	.761	1
2	.518		.719	.811			.866	.592	2
3	.555		.649	.717			.751	.464	3
4	.521		.528	.563			.586	.314	4
5	.347		.352	.413			.455	.209	5
6	.351		.349	.381			.387	.109	6
7	.347		.345	.377			.355	.081	7
8	.338		.347	.362			.324	.060	8
9	.320		.325	.325			.291	.060	9
10	.262		.268	.288			.236	.060	10
11	.266		.224	.250			.191	.025	11
12 -	.240	-	.255	- .247		-	.279	- .357	12
13 -	.274	-	.265	- .272		-	.288	- .341	13
14 -	.259	-	.287	- .278		-	.290	- .332	14
15 -	.273	-	.279	- .283		-	.302	- .332	15
16 -	.268	-	.279	- .277		-	.310	- .313	16
17 -	.193	-	.228	- .254		-	.258	- .235	17
18 -	.148	-	.198	- .207		-	.210	- .121	18
19 -	.144	-	.197	- .195		-	.195	- .157	19
20 -	.164	-	.207	- .213		-	.212	- .202	20
21 -	.221	-	.268	- .254		-	.254	- .263	21
22 -	.217	-	.271	- .269				- .323	22
23 -	.223			- .275		-	.272	- .342	23
24 -	.224	-	.251	- .274		-	.275	- .381	24
25 -	.224	-	.248	- .283		-	.261	- .354	25
26 -	.192	-	.086	- .086		-	.050	- .354	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-12 δ=30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.612		.881	.962			.964	.775	1
2	.522		.725	.816			.872	.596	2
3	.561		.652	.722			.757	.459	3
4	.525		.529	.566			.588	.314	4
5	.353		.353	.417			.458	.214	5
6	.357		.353	.386			.389	.116	6
7	.351		.351	.383			.361	.085	7
8	.337		.353	.371			.327	.063	8
9	.323		.331	.330			.297	.063	9
10	.266		.274	.294			.241	.063	10
11	.271		.229	.255			.195	.033	11
12	-.336		-.361	-.364			-.373	-.408	12
13	-.381		-.371	-.379			-.384	-.392	13
14	-.361		-.384	-.389			-.387	-.391	14
15	-.379		-.384	-.391			-.407	-.382	15
16	-.243		-.376	-.376			-.387	-.352	16
17	-.195		-.227	-.254			-.263	-.232	17
18	-.149		-.196	-.215			-.215	-.120	18
19	-.143		-.195	-.197			-.201	-.150	19
20	-.164		-.207	-.212			-.219	-.188	20
21	-.222		-.265	-.255			-.258	-.265	21
22	-.215		-.270	-.269				-.327	22
23	-.220			-.012			-.050	-.348	23
24	-.220		-.012	-.002			-.028	-.379	24
25	.023		-.002	.000			-.015	-.356	25
26	.054		.007	.009			-.003	-.194	26

α=-6 δ=-10

1	.347		.500	.514			.488	.418	1
2	.297		.435	.493			.490	.307	2
3	.299		.383	.449			.476	.272	3
4	.297		.309	.360			.382	.179	4
5	.157		.177	.232			.273	.106	5
6	.164		.158	.189			.225	.036	6
7	.160		.145	.180			.185	-.009	7
8	.150		.156	.172			.158	-.009	8
9	.143		.136	.136			.127	-.015	9
10	.099		.098	.106			.087	-.015	10
11	.113		.061	.082			.059	-.043	11
12	.413		.416	.401			.346	.174	12
13	.403		.409	.401			.343	.209	13
14	.388		.404	.401			.338	.170	14
15	.389		.404	.401			.324	.136	15
16	.371		.393	.384			.316	.109	16
17	-.044		-.045	-.054			-.037	-.010	17
18	-.026		-.044	-.043			-.021	.030	18
19	-.019		-.044	-.042			-.039	.016	19
20	-.049		-.060	-.068			-.068	-.028	20
21	-.122		-.135	-.127			-.122	-.051	21
22	-.118		-.138	-.145				-.081	22
23	-.122			-.144			-.142	-.140	23
24	-.123		-.140	-.146			-.148	-.190	24
25	-.126		-.152	-.157			-.144	-.169	25
26	-.169		-.173	-.174			-.155	-.199	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.348		.505	.516			.491	.442	1
2	.295		.440	.496			.494	.314	2
3	.302		.387	.450			.480	.283	3
4	.296		.316	.361			.380	.180	4
5	.159		.176	.234			.275	.098	5
6	.165		.161	.191			.227	.024	6
7	.163		.151	.186			.187	.001	7
8	.151		.158	.171			.154	-.008	8
9	.147		.139	.142			.130	-.008	9
10	.102		.103	.107			.088	-.008	10
11	.115		.065	.084			.062	-.028	11
12	.068		.059	.079			.019	-.028	12
13	.060		.040	.040			.014	-.060	13
14	.026		.040	.040			.000	-.080	14
15	.030		.040	.040		-.003	-.086	15	
16	.033		.040	.034		-.011	-.080	16	
17	-.039	-.043	-.055			-.040	-.008	17	
18	-.022	-.045	-.046			-.032	.039	18	
19	-.018	-.045	-.043			-.039	.011	19	
20	-.050	-.058	-.068			-.069	-.021	20	
21	-.120	-.133	-.124			-.120	-.059	21	
22	-.115	-.137	-.144				-.083	22	
23	-.119		-.146			-.143	-.148	23	
24	-.123	-.139	-.147			-.149	-.185	24	
25	-.124	-.151	-.159			-.143	-.179	25	
26	-.169	-.173	-.172			-.155	-.202	26	

α=-6 δ=10

1	.347		.505	.519			.499	.439	1
2	.291		.443	.502			.506	.332	2
3	.300		.386	.454			.487	.285	3
4	.298		.315	.365			.387	.195	4
5	.154		.179	.237			.280	.101	5
6	.163		.164	.193			.231	.029	6
7	.163		.151	.189			.193	-.003	7
8	.151		.158	.176			.160	-.003	8
9	.147		.139	.144			.134	-.013	9
10	.101		.102	.110			.091	-.013	10
11	.118		.065	.087			.065	-.034	11
12	-.163	-.173	-.163			-.198	-.222	12	
13	-.185	-.203	-.202			-.218	-.247	13	
14	-.177	-.197	-.202			-.218	-.230	14	
15	-.190	-.197	-.202			-.223	-.154	15	
16	-.198	-.205	-.202			-.235	-.116	16	
17	-.049	-.050	-.058			-.044	-.009	17	
18	-.030	-.050	-.050			-.038	.024	18	
19	-.023	-.049	-.046			-.042	.008	19	
20	-.056	-.064	-.072			-.074	-.028	20	
21	-.126	-.137	-.127			-.126	-.050	21	
22	-.118	-.141	-.147				-.091	22	
23	-.123		-.150			-.149	-.151	23	
24	-.126	-.142	-.151			-.152	-.197	24	
25	-.129	-.153	-.161			-.147	-.182	25	
26	-.171	-.176	-.174			-.158	-.212	26	

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.356		.511	.528			.513	.459	1
2	.296		.450	.513			.526	.347	2
3	.309		.393	.462			.499	.297	3
4	.303		.323	.371			.391	.190	4
5	.166		.186	.244			.288	.108	5
6	.171		.169	.199			.236	.035	6
7	.168		.157	.196			.198	.008	7
8	.161		.161	.182			.165	.008	8
9	.155		.145	.153			.138	-.009	9
10	.109		.109	.117			.094	-.009	10
11	.133		.073	.095			.077	-.024	11
12	-.285		-.313	-.309			-.317	-.329	12
13	-.331		-.333	-.336			-.341	-.344	13
14	-.319		-.348	-.336			-.348	-.257	14
15	-.338		-.342	-.336			-.351	-.210	15
16	-.207		-.316	-.346			-.368	-.223	16
17	-.047		-.051	-.059			-.049	-.014	17
18	-.029		-.049	-.053			-.042	.031	18
19	-.024		-.050	-.049			.050	.015	19
20	-.054		-.065	-.077			-.079	-.021	20
21	-.124		-.138	-.131			-.132	-.058	21
22	-.118		-.142	-.151				-.093	22
23	-.125			-.151			-.152	-.164	23
24	-.127		-.142	-.153			-.159	-.200	24
25	-.128		-.151	-.162			-.153	-.190	25
26	-.084		-.022	-.153			-.140	-.213	26

α=-6 δ=30

1	.355		.515	.534			.523	.463	1
2	.299		.451	.520			.536	.361	2
3	.309		.395	.467			.508	.304	3
4	.306		.325	.373			.398	.204	4
5	.168		.185	.246			.291	.113	5
6	.173		.169	.202			.240	.036	6
7	.169		.158	.200			.200	-.001	7
8	.158		.160	.184			.169	-.001	8
9	.160		.147	.159			.141	-.001	9
10	.111		.112	.119			.097	-.001	10
11	.169		.075	.101			.107	.045	11
12	-.387		-.406	-.396			-.399	-.391	12
13	-.413		-.417	-.421			-.422	-.384	13
14	-.406		-.411	-.429			-.422	-.322	14
15	-.371		-.316	-.373			-.341	-.349	15
16	-.293		-.307	-.298			-.323	-.336	16
17	-.052		-.056	-.065			-.051	-.013	17
18	-.035		-.057	-.058			-.045	.038	18
19	-.028		-.056	-.053			-.051	.010	19
20	-.061		-.069	-.080			-.086	-.031	20
21	-.130		-.139	-.132			-.138	-.054	21
22	-.122		-.145	-.152				-.103	22
23	-.127			-.123			.004	-.162	23
24	.132		.180	.140			.129	-.220	24
25	.172		.183	.143			.144	-.025	25
26	.194		.188	.146			.149	.043	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=-30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.138		.153	.161			.153	.114	1
2	.098		.155	.158			.157	.100	2
3	.117		.149	.159			.148	.093	3
4	.107		.114	.127			.105	.063	4
5	.002		.007	.041			.042	.015	5
6	.004		.005	.010			.015	.001	6
7	.183		.341	.343			.215	-.014	7
8	.348		.358	.370			.364	.086	8
9	.372		.368	.323			.370	.264	9
10	.385		.372	.387			.356	.283	10
11	.374		.373	.382			.356	.268	11
12	.391		.379	.386			.334	.233	12
13	.475		.413	.423			.397	.284	13
14	.774		.557	.615			.631	.483	14
15	.915		.707	.794			.818	.546	15
16	.736		.666	.754			.786	.508	16
17	.145		.158	.143			.162	.128	17
18	.118		.160	.155			.168	.160	18
19	.119		.159	.154			.162	.106	19
20	.100		.120	.123			.125	.061	20
21	.003		.014	.044			.053	.021	21
22	.009		.007	.022				.006	22
23	.006			.013			.021	.001	23
24	.000		-.011	.008			.008	-.015	24
25	-.002		-.020	-.014			-.010	.038	25
26	-.058		-.051	-.039			-.027	.202	26

$\alpha=0$ $\delta=-20$

1	.139		.154	.161			.158	.116	1
2	.102		.157	.158			.161	.101	2
3	.117		.149	.158			.150	.091	3
4	.105		.116	.125			.109	.060	4
5	.001		.009	.042			.046	.010	5
6	.004		.005	.011			.019	.003	6
7	.020		-.012	.009			.015	-.013	7
8	-.009		-.008	.002			-.007	.000	8
9	.000		-.026	.082			-.018	-.015	9
10	.026		-.046	-.048			-.044	-.015	10
11	.183		.112	.061			.073	.009	11
12	.318		.424	.352			.359	.179	12
13	.464		.535	.486			.477	.268	13
14	.586		.650	.627			.586	.333	14
15	.612		.675	.647			.603	.289	15
16	.563		.597	.581			.568	.248	16
17	.146		.155	.144			.163	.124	17
18	.119		.153	.155			.169	.148	18
19	.121		.156	.157			.160	.094	19
20	.102		.117	.126			.130	.051	20
21	.004		.014	.045				.011	21
22	.009		.004	.025				.005	22
23	.005			.015			.024	.000	23
24	.000		-.013	.011			.006	-.019	24
25	.000		-.022	-.013			-.010	.011	25
26	-.059		-.050	-.040			-.033	-.034	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=0 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.138		.156	.164			.162	.126	1
2	.103		.158	.160			.164	.116	2
3	.119		.150	.162			.156	.099	3
4	.108		.117	.129			.111	.073	4
5	.000		.010	.046			.049	.026	5
6	.002		.004	.013			.021	.018	6
7	.004		-.014	.010			.014	.001	7
8	-.009		-.007	.003			-.004	.001	8
9	-.007		-.025	-.015			-.017	-.010	9
10	-.042		-.050	-.048			-.044	-.003	10
11	-.018		-.080	-.065			-.037	-.019	11
12	.151		.149	.128			.124	.130	12
13	.177		.170	.148			.146	.120	13
14	.159		.180	.168			.162	.084	14
15	.173		.185	.177			.174	.053	15
16	.164		.177	.167			.172	.024	16
17	.145		.154	.146			.160	.135	17
18	.117		.157	.153			.168	.162	18
19	.118		.154	.156			.158	.104	19
20	.099		.116	.123			.124	.056	20
21	.003		.012	.042			.049	.024	21
22	.009		.005	.023				.018	22
23	.004			.016			.021	.010	23
24	.001		-.014	.008			.007	-.003	24
25	-.003		-.024	-.012			-.008	-.020	25
26	-.060		-.053	-.040			-.037	-.018	26

α=0 δ=0

1	.143		.160	.168			.165	.135	1
2	.104		.162	.163			.169	.114	2
3	.123		.153	.164			.160	.103	3
4	.112		.119	.132			.116	.069	4
5	.008		.011	.045			.050	.020	5
6	.008		.009	.013			.023	.016	6
7	.007		-.006	.012			.018	.005	7
8	-.006		-.003	.005			-.001	.005	8
9	-.004		-.021	-.021			-.014	-.005	9
10	-.040		-.045	-.047			-.043	-.005	10
11	-.026		-.079	-.065			-.043	-.018	11
12	-.083		-.090	-.085			-.089	-.071	12
13	-.083		-.106	-.118			-.111	-.065	13
14	-.100		-.104	-.110			-.101	-.046	14
15	-.100		-.104	-.104			-.109	-.041	15
16	-.100		-.104	-.104			-.109	-.034	16
17	.148		.155	.143			.157	.126	17
18	.120		.153	.156			.166	.154	18
19	.121		.153	.154			.155	.105	19
20	.103		.116	.121			.119	.063	20
21	.004		.013	.043			.045	.030	21
22	.011		.005	.021				.013	22
23	.007			.014			.018	.011	23
24	.003		-.014	.011			.002	-.005	24
25	.000		-.023	-.012			-.011	.020	25
26	-.057		-.056	-.040			-.038	-.015	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=0 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.141		.160	.169			.169	.139	1
2	.105		.163	.164			.170	.121	2
3	.121		.154	.167			.159	.108	3
4	.106		.118	.134			.116	.073	4
5	.008		.013	.046			.053	.021	5
6	.007		.007	.016			.025	.016	6
7	.007		- .010	.012			.022	- .009	7
8	- .005		- .004	.006			.002	.010	8
9	- .001		- .025	- .020			- .014	- .006	9
10	- .041		- .043	- .047			- .039	.000	10
11	- .014		- .077	- .064			- .037	- .015	11
12	- .254		- .264	- .260			- .267	- .253	12
13	- .270		- .288	- .289			- .290	- .212	13
14	- .270		- .288	- .289			- .287	- .149	14
15	- .287		- .288	- .287			- .287	- .173	15
16	- .205		- .288	- .287			- .293	- .310	16
17	.145		.151	.140			.148	.130	17
18	.118		.152	.148			.158	.146	18
19	.119		.152	.150			.149	.104	19
20	.101		.114	.117			.115	.068	20
21	.005		.011	.039			.039	.028	21
22	.009		.003	.018				.019	22
23	.005			.013			.012	.015	23
24	.001		- .016	.006			.001	- .005	24
25	- .001		- .026	- .015			- .014	.013	25
26	- .059		- .057	- .044			- .044	- .019	26

α=0 δ=20

1	.139		.159	.169			.169	.146	1
2	.101		.160	.164			.171	.128	2
3	.119		.152	.167			.164	.109	3
4	.107		.117	.133			.119	.078	4
5	.001		.009	.046			.058	.029	5
6	.002		.006	.014			.028	.018	6
7	.004		- .013	.013			.026	.000	7
8	- .007		- .005	.006			.007	.013	8
9	.000		- .024	- .018			- .009	- .001	9
10	- .040		- .045	- .045			- .038	.000	10
11	.117		.066	.085			.087	.010	11
12	- .354		- .366	- .363			- .372	- .319	12
13	- .374		- .389	- .383			- .393	- .238	13
14	- .374		- .404	- .397			- .393	- .321	14
15	- .394		- .402	- .408			- .393	- .439	15
16	- .244		- .245	- .263			- .260	- .456	16
17	.139		.150	.137			.149	.129	17
18	.114		.147	.145			.156	.148	18
19	.117		.147	.148			.146	.109	19
20	.094		.112	.115			.112	.060	20
21	.000		.011	.039			.035	.026	21
22	.005		.001	.016				.018	22
23	.002			.010			.011	.018	23
24	- .004		- .016	.005			- .005	.001	24
25	- .004		- .027	- .020			- .014	.028	25
26	.064		- .047	- .045			- .043	- .010	26
								.010	27

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=30$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.141		.163	.174			.170	.143	1
2	.104		.164	.169			.174	.128	2
3	.122		.157	.171			.165	.116	3
4	.114		.121	.138			.118	.081	4
5	.006		.013	.048			.059	.026	5
6	.004		.011	.021			.030	.024	6
7	.005		-.008	.013			.026	.003	7
8	-.003		-.004	.006			.007	.014	8
9	.005		-.019	-.013			-.006	.038	9
10	-.040		-.039	-.041			-.029	.248	10
11	.165		.194	.235			.274	.264	11
12	-.408		-.437	-.429			-.433	-.319	12
13	-.423		-.423	-.446			-.441	-.249	13
14	-.348		-.358	-.424			-.367	-.399	14
15	-.327		-.334	-.358			-.327	-.437	15
16	-.310		-.331	-.331			-.327	-.449	16
17	.143		.154	.139			.146	.125	17
18	.117		.149	.145			.155	.148	18
19	.123		.151	.146			.147	.106	19
20	.099		.113	.115			.110	.069	20
21	.000		.012	.037			.033	.030	21
22	.010		.004	.016				.021	22
23	.262			.352			.353	.011	23
24	.355		.383	.366			.399	.075	24
25	.380		.394	.370			.400	.284	25
26	.386		.392	.366			.386	.317	26

$\alpha=6$ $\delta=-30$

1	-.053		-.048	-.043			-.052	-.045	1
2	-.044		-.047	-.041			-.044	-.005	2
3	-.029		-.054	-.047			-.049	.011	3
4	-.050		-.045	-.064			-.082	-.018	4
5	-.139		-.144	-.126			-.129	-.070	5
6	-.130		-.141	-.149			-.145	-.129	6
7	-.115		.119	.152			-.112	-.174	7
8	.101		.163	.172			-.169	-.208	8
9	.160		.171	.104			-.171	-.174	9
10	.188		.183	.189			-.173	-.020	10
11	.183		.181	.193			.202	.036	11
12	.219		.208	.218			.215	.025	12
13	.299		.208	.210			.252	.141	13
14	.613		.334	.284			.412	.431	14
15	.700		.478	.388			.532	.406	15
16	.607		.485	.409			.541	.446	16
17	.351		.502	.522			.527	.431	17
18	.313		.445	.501			.527	.374	18
19	.316		.395	.455			.497	.275	19
20	.286		.320	.364			.395	.193	20
21	.166		.185	.243			.285	.108	21
22	.172		.171	.206				.065	22
23	.165			.198			.198	.030	23
24	.163		.155	.185			.170	.001	24
25	.161		.145	.162			.145	.036	25
26	.088		.109	.126			.117	-.008	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=-20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.051		-.046	-.043			-.051	-.054	1
2	-.039		-.043	-.041			-.042	-.016	2
3	-.026		-.051	-.047			-.046	.003	3
4	-.044		-.062	-.070			-.081	-.025	4
5	-.127		-.141	-.128			-.125	-.076	5
6	-.121		-.139	-.149			-.145	-.139	6
7	-.120		-.137	-.149			-.138	-.185	7
8	-.128		-.135	-.157			-.158	-.212	8
9	-.120		-.152	-.054			-.148	-.212	9
10	-.105		-.145	-.065			-.098	-.212	10
11	.066		.086	.080			.125	-.174	11
12	.119		.148	.110			.143	-.043	12
13	.208		.218	.140			.200	-.001	13
14	.316		.312	.250			.321	-.114	14
15	.334		.349	.295			.366	-.075	15
16	.334		.336	.287			.352	-.023	16
17	.354		.502	.520			.525	.418	17
18	.319		.450	.499			.533	.366	18
19	.321		.396	.455			.497	.272	19
20	.288		.318	.363			.403	.185	20
21	.168		.185	.244			.288	.100	21
22	.177		.168	.204				.051	22
23	.170			.196			.198	.021	23
24	.166		.154	.185			.175	-.013	24
25	.163		.144	.162			.153	.030	25
26	.092		.107	.127			.117	-.019	26

$\alpha=6$ $\delta=-10$

1	-.049		-.045	-.039			-.046	-.039	1
2	-.040		-.043	-.039			-.040	-.001	2
3	-.027		-.049	-.044			-.044	.013	3
4	-.047		-.065	-.065			-.081	-.010	4
5	-.129		-.144	-.126			-.122	-.066	5
6	-.123		-.139	-.148			-.142	-.119	6
7	-.124		-.141	-.149			-.144	-.172	7
8	-.131		-.138	-.155			-.154	-.197	8
9	-.125		-.152	-.143			-.152	-.197	9
10	-.157		-.165	-.186			-.159	-.208	10
11	-.087		-.181	-.177			-.094	-.223	11
12	-.009		-.010	-.033			-.003	-.130	12
13	.009		-.003	-.026			.014	-.109	13
14	.008		.008	-.008			.035	-.232	14
15	.023		.026	-.005			.056	-.121	15
16	.023		.026	-.005			.056	-.151	16
17	.355		.500	.518			.519	.423	17
18	.316		.449	.498			.527	.373	18
19	.318		.394	.455			.497	.275	19
20	.289		.318	.362			.397	.188	20
21	.166		.183	.243			.287	.108	21
22	.176		.170	.206				.058	22
23	.170			.196			.197	.030	23
24	.164		.152	.184			.169	-.001	24
25	.162		.145	.161			.150	.034	25
26	.090		.106	.124			.115	-.009	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.047		-.045	-.038			-.042	-.035	1
2	-.039		-.040	-.038			-.036	-.003	2
3	-.028		-.046	-.044			-.039	.019	3
4	-.044		-.063	-.064			-.075	-.011	4
5	-.126		-.138	-.120			-.119	-.071	5
6	-.120		-.139	-.144			-.140	-.113	6
7	-.120		-.141	-.146			-.143	-.172	7
8	-.129		-.135	-.151			-.148	-.189	8
9	-.124		-.153	-.162			-.147	-.189	9
10	-.158		-.165	-.184			-.154	-.200	10
11	-.129		-.191	-.191			-.116	-.222	11
12	-.182		-.197	-.203			-.179	-.249	12
13	-.189		-.217	-.225			-.199	-.235	13
14	-.199		-.217	-.227			-.189	-.235	14
15	-.199		-.200	-.227			-.189	-.197	15
16	-.199		-.203	-.227			-.182	-.233	16
17	.357		.500	.514			.516	.414	17
18	.317		.447	.497			.525	.364	18
19	.320		.394	.455			.492	.275	19
20	.290		.320	.363			.394	.180	20
21	.169		.185	.241			.288	.099	21
22	.174		.169	.204				.053	22
23	.170			.196			.196	.025	23
24	.167		.154	.183			.170	-.006	24
25	.162		.146	.164			.148	.033	25
26	.090		.107	.124			.115	-.009	26

$\alpha=6$ $\delta=10$

1	-.053		-.048	-.043			-.044	-.040	1
2	-.045		-.047	-.041			-.037	-.004	2
3	-.031		-.053	-.048			-.042	.013	3
4	-.053		-.071	-.066			-.077	-.029	4
5	-.132		-.144	-.126			-.121	-.078	5
6	-.132		-.142	-.151			-.142	-.118	6
7	-.129		-.145	-.150			-.144	-.157	7
8	-.137		-.142	-.155			-.152	-.189	8
9	-.134		-.157	-.169			-.150	-.189	9
10	-.165		-.171	-.190			-.159	-.199	10
11	-.129		-.192	-.187			-.114	-.220	11
12	-.313		-.321	-.324			-.302	-.334	12
13	-.331		-.346	-.354			-.337	-.275	13
14	-.331		-.357	-.363			-.337	-.331	14
15	-.341		-.352	-.363			-.337	-.361	15
16	-.193		-.195	-.225			-.284	-.351	16
17	.347		.496	.506			.508	.409	17
18	.311		.439	.491			.513	.354	18
19	.312		.390	.450			.487	.272	19
20	.283		.313	.356			.392	.187	20
21	.161		.178	.238			.279	.105	21
22	.169		.162	.200				.056	22
23	.164			.191			.191	.021	23
24	.158		.149	.176			.164	-.011	24
25	.157		.141	.155			.143	.025	25
26	.085		.101	.117			.109	-.011	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.046		-.045	-.041			-.037	-.033	1
2	-.040		-.042	-.039			-.033	.001	2
3	-.028		-.049	-.045			-.036	.015	3
4	-.046		-.068	-.063			-.072	-.014	4
5	-.127		-.141	-.122			-.115	-.070	5
6	-.126		-.138	-.147			-.135	-.108	6
7	-.127		-.143	-.146			-.138	-.151	7
8	-.133		-.136	-.151			-.146	-.183	8
9	-.118		-.153	-.162			-.143	-.183	9
10	-.156		-.163	-.118			-.128	-.185	10
11	.045		.065	.079			.121	-.111	11
12	-.386		-.416	-.412			-.409	-.399	12
13	-.413		-.416	-.417			-.421	-.408	13
14	-.394		-.441	-.438			-.421	-.423	14
15	-.414		-.392	-.437			-.413	-.411	15
16	-.290		-.299	-.314			-.307	-.404	16
17	.351		.496	.507			.508	.403	17
18	.314		.438	.490			.512	.346	18
19	.315		.390	.450			.487	.270	19
20	.286		.313	.357			.390	.189	20
21	.163		.179	.239			.285	.103	21
22	.172		.163	.200				.056	22
23	.167			.193			.192	.021	23
24	.164		.150	.179			.161	-.004	24
25	.173		.310	.160			.142	.024	25
26	.470		.496	.303			.170	-.009	26

$\alpha = 12$ $\delta = -30$

1	-.209		-.228	-.257			-.272	-.269	1
2	-.167		-.204	-.213			-.229	-.168	2
3	-.149		-.204	-.203			-.207	-.169	3
4	-.164		-.197	-.221			-.230	-.228	4
5	-.228		-.273	-.262			-.262	-.280	5
6	-.221		-.274	-.277			-.278	-.359	6
7	-.221		-.062	-.020			-.069	-.388	7
8	-.236		-.030	-.010			-.038	-.376	8
9	.004		-.016	-.047			-.028	-.376	9
10	.044		-.001	-.002			-.020	-.185	10
11	.051		-.007	-.002			.005	-.157	11
12	.083		.019	.020			.008	-.223	12
13	.134		.019	.020			-.006	-.203	13
14	.423		.146	.048			.124	-.111	14
15	.512		.270	.099			.270	-.194	15
16	.472		.308	.114			.346	-.175	16
17	.638		.900	.972			.995	.744	17
18	.556		.740	.830			.885	.586	18
19	.601		.662	.729			.758	.443	19
20	.514		.529	.562			.600	.334	20
21	.361		.358	.421			.458	.202	21
22	.374		.360	.396				.140	22
23	.353			.389			.360	.118	23
24	.353		.356	.376			.333	.080	24
25	.346		.344	.358			.310	.123	25
26	.256		.290	.303			.285	.071	26

TABLE VIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.206		-.225	-.253			-.265	-.262	1
2	-.168		-.201	-.210			-.222	-.167	2
3	-.149		-.203	-.202			-.203	-.167	3
4	-.169		-.208	-.218			-.225	-.219	4
5	-.231		-.272	-.262			-.259	-.284	5
6	-.223		-.273	-.274			-.275	-.352	6
7	-.227		-.261	-.276			-.267	-.384	7
8	-.234		-.259	-.279			-.281	-.367	8
9	-.223		-.256	-.194			-.265	-.381	9
10	-.202		-.082	-.094			-.065	-.332	10
11	-.036		-.039	-.066			-.009	-.199	11
12	.016		-.006	-.040			-.019	-.255	12
13	.049		.018	-.019			-.001	-.255	13
14	.136		.109	.023			.079	-.233	14
15	.158		.141	.056			.133	-.259	15
16	.170		.141	.056			.143	-.333	16
17	.638		.899	.970			.996	.740	17
18	.556		.740	.832			.885	.586	18
19	.600		.663	.726			.761	.444	19
20	.516		.530	.562			.606	.337	20
21	.358		.360	.421			.458	.198	21
22	.372		.361	.397				.148	22
23	.353			.391			.361	.116	23
24	.354		.359	.376			.334	.080	24
25	.347		.345	.357			.313	.125	25
26	.257		.288	.304			.287	.068	26

α=12 δ=-10

1	-.205		-.226	-.251			-.264	-.264	1
2	-.167		-.202	-.208			-.221	-.162	2
3	-.150		-.205	-.202			-.200	-.162	3
4	-.170		-.211	-.217			-.222	-.233	4
5	-.228		-.273	-.262			-.256	-.284	5
6	-.223		-.273	-.277			-.273	-.357	6
7	-.227		-.270	-.278			-.273	-.384	7
8	-.231		-.258	-.280			-.281	-.377	8
9	-.228		-.258	-.264			-.268	-.386	9
10	-.251		-.258	-.302			-.259	-.354	10
11	-.142		-.195	-.192			-.068	-.237	11
12	-.106		-.135	-.158			-.151	-.310	12
13	-.108		-.135	-.168			-.144	-.328	13
14	-.108		-.123	-.168			-.119	-.353	14
15	-.108		-.110	-.168			-.106	-.329	15
16	-.108		-.106	-.162			-.099	-.329	16
17	.638		.897	.969			.995	.754	17
18	.557		.738	.827			.882	.588	18
19	.595		.662	.727			.762	.457	19
20	.514		.530	.560			.601	.343	20
21	.355		.357	.420			.458	.207	21
22	.375		.358	.396				.141	22
23	.355			.391			.363	.116	23
24	.353		.356	.375			.339	.083	24
25	.347		.343	.356			.311	.119	25
26	.257		.287	.303			.287	.066	26

TABLE VIII.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4

WITH 0.20-INCH HINGE-LINE GAP.

$M = 1.61$; $R = 3.6 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.209		-.227	-.251			-.261	-.260	1
2	-.171		-.202	-.207			-.219	-.164	2
3	-.151		-.204	-.204			-.199	-.160	3
4	-.170		-.214	-.216			-.222	-.224	4
5	-.231		-.273	-.264			-.252	-.273	5
6	-.232		-.274	-.277			-.272	-.362	6
7	-.231		-.273	-.275			-.273	-.389	7
8	-.232		-.259	-.276			-.280	-.382	8
9	-.232		-.259	-.279			-.269	-.382	9
10	-.254		-.260	-.303			-.265	-.367	10
11	-.195		-.241	-.245			-.089	-.270	11
12	-.250		-.268	-.282			-.259	-.383	12
13	-.267		-.282	-.307			-.280	-.371	13
14	-.267		-.290	-.316			-.280	-.382	14
15	-.273		-.290	-.317			-.279	-.372	15
16	-.153		-.155	-.203			-.269	-.326	16
17	.635		.892	.966			.989	.737	17
18	.553		.734	.826			.878	.592	18
19	.589		.659	.727			.754	.449	19
20	.510		.526	.560			.600	.332	20
21	.356		.356	.420			.453	.202	21
22	.369		.356	.395				.141	22
23	.350			.387			.357	.106	23
24	.350		.351	.373			.331	.070	24
25	.342		.339	.354			.307	.109	25
26	.254		.285	.303			.279	.059	26

α=12 δ=10

1	-.204		-.224	-.246			-.258	-.255	1
2	-.168		-.200	-.206			-.217	-.164	2
3	-.151		-.204	-.201			-.198	-.164	3
4	-.169		-.212	-.217			-.221	-.217	4
5	-.233		-.273	-.261			-.251	-.275	5
6	-.224		-.273	-.274			-.273	-.352	6
7	-.229		-.270	-.274			-.272	-.386	7
8	-.236		-.259	-.277			-.279	-.379	8
9	-.227		-.257	-.284			-.267	-.386	9
10	-.252		-.260	-.300			-.260	-.374	10
11	-.120		-.152	-.149			-.070	-.265	11
12	-.366		-.373	-.377			-.369	-.429	12
13	-.379		-.391	-.401			-.387	-.416	13
14	-.379		-.409	-.423			-.389	-.434	14
15	-.367		-.280	-.302			-.389	-.434	15
16	-.234		-.248	-.269			-.265	-.409	16
17	.634		.892	.961			.985	.734	17
18	.555		.733	.821			.874	.580	18
19	.587		.658	.724			.755	.442	19
20	.510		.525	.559			.596	.331	20
21	.353		.355	.416			.451	.190	21
22	.370		.356	.389				.131	22
23	.351			.384			.353	.109	23
24	.351		.351	.371			.324	.065	24
25	.342		.338	.353			.300	.109	25
26	.252		.283	.300			.273	.054	26

TABLE IX

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-12 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.582		.893	.960			.958	.771	1
2	.513		.703	.819			.865	.571	2
3	.570		.654	.720			.757	.472	3
4	.517		.523	.559			.650	.346	4
5	.380		.350	.475			.646	.283	5
6	.553		.789	.789			.671	.313	6
7	.433		.880	.933			.806	.390	7
8	.950		.977	.996			.903	.370	8
9	1.000		1.019	.739			.987	.516	9
10	1.044		1.072	1.104			1.053	.595	10
11	1.057		1.068	1.120			1.106	.595	11
12	1.062		1.092	1.144			1.094	.645	12
13	1.141		1.114	1.171			1.097	.710	13
14	1.144		1.127	1.138			1.064	.658	14
15	1.048		1.037	1.009			.955	.582	15
16	.809		.809	.812			.771	.496	16
17	-.179		-.209	-.241			-.236	-.225	17
18	-.118		-.190	-.205			-.148	-.110	18
19	-.133		-.188	-.200			-.196	-.148	19
20	-.158		-.198	-.219			-.211	-.189	20
21	-.219		-.257	-.249			-.249	-.241	21
22	-.207		-.253	-.255				-.302	22
23	-.211			-.262			-.249	-.310	23
24	-.217		-.241	-.260			-.257	-.346	24
25	-.217		-.234	-.266			-.249	-.313	25
26	-.230		-.257	-.264			-.247	-.318	26

α=-12 δ=-20

1	.578		.880	.960			.964	.754	1
2	.506		.722	.814			.869	.579	2
3	.549		.650	.722			.755	.444	3
4	.509		.519	.557			.587	.307	4
5	.363		.346	.403			.452	.192	5
6	.376		.365	.401			.405	.104	6
7	.525		.684	.743			.635	.107	7
8	.764		.806	.833			.732	.285	8
9	.840		.867	.895			.836	.431	9
10	.890		.922	.958			.903	.502	10
11	.914		.920	.983			.968	.505	11
12	.963		.952	1.001			.966	.554	12
13	1.018		.990	1.031			.971	.625	13
14	1.045		1.048	1.015			.949	.603	14
15	.952		.960	.919			.859	.529	15
16	.732		.749	.749			.730	.472	16
17	-.186		-.232	-.253			-.247	-.252	17
18	-.148		-.203	-.207			-.179	-.115	18
19	-.143		-.200	-.203			-.192	-.145	19
20	-.179		-.215	-.215			-.215	-.203	20
21	-.238		-.270	-.251			-.251	-.255	21
22	-.228		-.272	-.257				-.321	22
23	-.228			-.266			-.255	-.332	23
24	-.230		-.251	-.264			-.264	-.351	24
25	-.234		-.247	-.268			-.257	-.315	25
26	-.260		-.268	-.283			-.251	-.313	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-12 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.570		.876	.964			.964	.752	1
2	.502		.720	.821			.869	.568	2
3	.553		.654	.728			.757	.442	3
4	.513		.528	.561			.587	.307	4
5	.359		.348	.411			.460	.200	5
6	.359		.363	.384			.388	.112	6
7	.462		.361	.382			.371	.069	7
8	.342		.361	.380			.329	.066	8
9	.323		.344	.506			.310	.069	9
10	.281		.319	.306			.262	.096	10
11	.380		.384	.329			.323	.055	11
12	.634		.645	.617			.524	.236	12
13	.636		.645	.617			.521	.225	13
14	.642		.645	.617			.521	.214	14
15	.642		.645	.617			.496	.203	15
16	.560		.532				.455	.181	16
17	-.196		-.232	-.247			-.253	-.241	17
18	-.148		-.205	-.203			-.190	-.121	18
19	-.154		-.192	-.194			-.190	-.148	19
20	-.171		-.205	-.211			-.207	-.197	20
21	-.222		-.268	-.251			-.236	-.255	21
22	-.224		-.264	-.255				-.321	22
23	-.224			-.268			-.253	-.343	23
24	-.226		-.245	-.264			-.255	-.376	24
25	-.224		-.243	-.270			-.253	-.315	25
26	-.257		-.262	-.283			-.247	-.321	26

α=-12 δ=0

1	.584		.888	.956			.958	.757	1
2	.498		.724	.821			.878	.579	2
3	.565		.646	.715			.762	.436	3
4	.511		.530	.559			.589	.307	4
5	.367		.344	.405			.462	.195	5
6	.363		.361	.388			.386	.104	6
7	.407		.357	.382			.363	.063	7
8	.335		.359	.384			.329	.052	8
9	.325		.323	.357			.306	.052	9
10	.274		.295	.295			.243	.052	10
11	.270		.238	.255			.247	.003	11
12	.266		.214	.236			.170	-.003	12
13	.214		.233	.200			.145	-.022	13
14	.200		.217	.187			.154	-.022	14
15	.200		.217	.189			.134	-.027	15
16	.200		.217	.184			.110	-.049	16
17	-.192		-.224	-.247			-.247	-.266	17
18	-.148		-.207	-.205			-.203	-.140	18
19	-.143		-.200	-.192			-.198	-.167	19
20	-.165		-.209	-.215			-.234	-.222	20
21	-.224		-.268	-.249			-.255	-.274	21
22	-.215		-.264	-.255				-.337	22
23	-.219			-.262			-.253	-.340	23
24	-.219		-.247	-.266			-.264	-.373	24
25	-.222		-.249	-.272			-.260	-.359	25
26	-.255		-.268	-.279			-.257	-.354	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.580		.884	.964			.960	.752	1
2	.511		.734	.825			.871	.557	2
3	.568		.656	.728			.764	.425	3
4	.519		.528	.555			.595	.302	4
5	.371		.359	.409			.462	.192	5
6	.373		.361	.386			.386	.112	6
7	.384		.357	.384			.363	.060	7
8	.340		.367	.382			.331	.047	8
9	.329		.325	.342			.302	.049	9
10	.281		.295	.287			.249	.052	10
11	.268		.234	.247			.255	.022	11
12 -	.016	-	.049	- .038		-	.074	- .189	12
13 -	.055	-	.049	- .069		-	.096	- .203	13
14 -	.055	-	.071	- .074		-	.096	- .200	14
15 -	.058	-	.066	- .085		-	.110	- .200	15
16 -	.058	-	.069	- .077		-	.129	- .208	16
17 -	.184	-	.222	- .257		-	.249	- .252	17
18 -	.150	-	.203	- .213		-	.200	- .140	18
19 -	.150	-	.196	- .196		-	.192	- .181	19
20 -	.165	-	.209	- .215		-	.211	- .217	20
21 -	.224	-	.270	- .253		-	.245	- .277	21
22 -	.213	-	.264	- .257				- .337	22
23 -	.217			- .266		-	.253	- .337	23
24 -	.222	-	.245	- .264		-	.262	- .387	24
25 -	.226	-	.245	- .270		-	.257	- .337	25
26 -	.253	-	.272	- .283		-	.241	- .359	26

α=-12 δ=20

1	.591		.893	.964			.964	.771	1
2	.523		.736	.829			.874	.562	2
3	.578		.650	.732			.753	.444	3
4	.521		.532	.565			.595	.307	4
5	.376		.363	.414			.454	.192	5
6	.373		.373	.386			.380	.101	6
7	.371		.357	.382			.363	.069	7
8	.338		.367	.382			.323	.052	8
9	.338		.329	.338			.295	.052	9
10	.287		.298	.293			.241	.066	10
11	.283		.236	.247			.247	.027	11
12 -	.170	-	.211	- .203		-	.217	- .310	12
13 -	.236	-	.211	- .228		-	.239	- .324	13
14 -	.222	-	.228	- .236		-	.241	- .294	14
15 -	.236	-	.241	- .247		-	.255	- .310	15
16 -	.184	-	.236	- .241		-	.250	- .299	16
17 -	.179	-	.228	- .260		-	.249	- .258	17
18 -	.137	-	.194	- .205		-	.203	- .132	18
19 -	.133	-	.196	- .196		-	.200	- .162	19
20 -	.160	-	.209	- .215		-	.219	- .206	20
21 -	.224	-	.274	- .253		-	.257	- .266	21
22 -	.213	-	.264	- .260				- .321	22
23 -	.213			- .266		-	.257	- .343	23
24 -	.222	-	.247	- .262		-	.260	- .381	24
25 -	.222	-	.243	- .272		-	.251	- .340	25
26 -	.245	-	.257	- .287		-	.213	- .357	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-12 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.589		.888	.968			.973	.774	1
2	.519		.734	.825			.878	.562	2
3	.572		.650	.730			.764	.458	3
4	.523		.525	.563			.591	.304	4
5	.367		.352	.416			.456	.192	5
6	.363		.371	.390			.390	.099	6
7	.359		.354	.388			.367	.052	7
8	.340		.365	.382			.333	.038	8
9	.331		.329	.338			.306	.058	9
10	.279		.300	.295			.247	.049	10
11	.279		.238	.251			.255	.016	11
12	-.266		-.285	-.277			-.315	-.368	12
13	-.302		-.288	-.310			-.332	-.368	13
14	-.304		-.326	-.315			-.332	-.357	14
15	-.310		-.321	-.332			-.332	-.348	15
16	-.219		-.283	-.294			-.329	-.326	16
17	-.196		-.213	-.253			-.245	-.247	17
18	-.148		-.192	-.200			-.205	-.132	18
19	-.152		-.196	-.194			-.198	-.156	19
20	-.167		-.209	-.209			-.222	-.222	20
21	-.226		-.264	-.249			-.255	-.261	21
22	-.213		-.264	-.257				-.340	22
23	-.219			-.268			-.245	-.343	23
24	-.219		-.245	-.260			-.238	-.376	24
25	-.224		-.230	-.257			-.179	-.343	25
26	-.053		-.004	-.074			-.106	-.348	26

α=-6 δ=-25

1	.327		.492	.513			.487	.420	1
2	.260		.253	.487			.502	.285	2
3	.308		.380	.456			.483	.261	3
4	.285		.245	.354			.382	.170	4
5	.167		.158	.234			.283	.080	5
6	.146		.162	.181			.194	.011	6
7	-.055		.416	.441			.209	-.027	7
8	.487		.563	.593			.546	-.038	8
9	.563		.572	.298			.612	.228	9
10	.599		.601	.627			.625	.280	10
11	.603		.591	.637			.688	.283	11
12	.592		.612	.636			.617	.299	12
13	.708		.573	.623			.623	.354	13
14	.946		.686	.763			.686	.557	14
15	.902		.763	.853			.763	.595	15
16	.691		.642	.749			.691	.496	16
17	-.030		-.036	-.036			-.013	.000	17
18	.017		-.040	-.027			.169	.027	18
19	-.023		-.040	-.025			-.023	.008	19
20	-.053		-.055	-.055			-.046	-.049	20
21	-.122		-.129	-.103			-.114	-.066	21
22	-.116		-.139	-.120				-.093	22
23	-.116			-.131			-.114	-.118	23
24	-.124		-.131	-.129			-.116	-.170	24
25	-.122		-.137	-.137			-.114	-.107	25
26	-.150		-.167	-.137			-.131	-.060	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.327		.490	.511			.496	.436	1
2	.262		.388	.492			.506	.315	2
3	.300		.384	.454			.479	.283	3
4	.272		.300	.367			.380	.165	4
5	.156		.173	.230			.268	.101	5
6	.169		.156	.192			.217	.038	6
7	.013		.184	.184			.192	-.016	7
8	.152		.165	.175			.179	-.030	8
9	.228		.399	.382			.186	.011	9
10	.513		.555	.546			.498	.165	10
11	.534		.549	.557			.582	.225	11
12	.579		.587	.573			.557	.274	12
13	.623		.609	.625			.573	.354	13
14	.768		.738	.721			.699	.403	14
15	.757		.776	.757			.694	.400	15
16	.601		.647	.653			.631	.373	16
17	-.030		-.038	-.049			-.032	-.008	17
18	-.019		-.044	-.038			.038	.030	18
19	-.025		-.038	-.042			-.036	.011	19
20	-.057		-.057	-.057			-.055	-.036	20
21	-.131		-.129	-.122			-.122	-.052	21
22	-.118		-.135	-.141				-.080	22
23	-.116			-.148			-.131	-.107	23
24	-.127		-.127	-.137			-.141	-.159	24
25	-.122		-.139	-.148			-.135	-.132	25
26	-.160		-.167	-.160			-.148	-.123	26

α=-6 δ=-10

1	.344		.498	.506			.492	.414	1
2	.266		.430	.498			.506	.310	2
3	.304		.382	.449			.492	.269	3
4	.285		.325	.367			.378	.184	4
5	.167		.181	.238			.285	.091	5
6	.173		.173	.190			.230	.014	6
7	.097		.156	.177			.190	-.025	7
8	.156		.169	.181			.158	-.027	8
9	.143		.152	.188			.148	-.022	9
10	.106		.137	.112			.099	-.019	10
11	.143		.116	.118			.154	-.025	11
12	.343		.326	.326			.304	.165	12
13	.343		.348	.326			.288	.162	13
14	.343		.340	.351			.288	.134	14
15	.343		.340	.340			.274	.110	15
16	.318		.340	.337			.263	.080	16
17	-.027		-.042	-.046			-.040	-.022	17
18	-.025		-.042	-.040			-.008	.036	18
19	-.019		-.046	-.040			-.034	.008	19
20	-.051		-.057	-.059			-.061	-.047	20
21	-.124		-.141	-.118			-.122	-.071	21
22	-.110		-.135	-.131				-.091	22
23	-.110			-.135			-.129	-.132	23
24	-.120		-.131	-.135			-.141	-.187	24
25	-.112		-.139	-.143			-.135	-.137	25
26	-.158		-.169	-.158			-.143	-.176	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

$\alpha=-6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.333		.485	.515			.494	.414	1
2	.260		.441	.492			.513	.307	2
3	.302		.376	.454			.487	.266	3
4	.281		.314	.357			.384	.167	4
5	.165		.184	.243			.283	.069	5
6	.171		.162	.198			.226	.027	6
7	.129		.150	.186			.192	-.027	7
8	.160		.165	.181			.158	-.036	8
9	.139		.146	.152			.141	-.030	9
10	.106		.127	.097			.089	-.025	10
11	.112		.070	.074			.129	-.049	11
12	.091		.033	.077			.038	-.044	12
13	.058		.052	.041			.016	-.060	13
14	.033		.036	.033			.011	-.082	14
15	.033		.047	.030			.005	-.088	15
16	.022		.041	.025			-.005	-.093	16
17	-.038		-.038	-.051			-.023	-.027	17
18	-.027		-.040	-.036			-.019	-.019	18
19	-.027		-.036	-.042			-.040	-.003	19
20	-.053		-.055	-.070			-.076	-.055	20
21	-.122		-.127	-.114			-.120	-.071	21
22	-.120		-.133	-.131				-.101	22
23	-.116			-.143			-.131	-.137	23
24	-.129		-.127	-.139			-.141	-.195	24
25	-.127		-.139	-.148			-.135	-.126	25
26	-.169		-.169	-.169			-.146	-.197	26

$\alpha=-6$ $\delta=10$

1	.335		.500	.506			.490	.422	1
2	.262		.441	.485			.511	.304	2
3	.314		.388	.460			.483	.255	3
4	.287		.312	.363			.380	.151	4
5	.165		.186	.236			.264	.074	5
6	.165		.165	.194			.222	.027	6
7	.150		.148	.184			.186	-.038	7
8	.148		.162	.177			.152	-.038	8
9	.148		.148	.135			.135	-.030	9
10	.106		.127	.106			.087	-.022	10
11	.101		.065	.078			.127	-.052	11
12	-.145		-.151	-.148			-.176	-.208	12
13	-.181		-.165	-.178			-.211	-.230	13
14	-.181		-.187	-.187			-.195	-.203	14
15	-.181		-.192	-.187			-.217	-.162	15
16	-.181		-.192	-.189			-.230	-.134	16
17	-.034		-.040	-.053			-.034	-.025	17
18	-.025		-.042	-.046			-.030	-.011	18
19	-.021		-.042	-.040			-.038	-.008	19
20	-.049		-.053	-.065			-.076	-.060	20
21	-.122		-.141	-.127			-.120	-.080	21
22	-.114		-.137	-.135				-.118	22
23	-.118			-.141			-.127	-.137	23
24	-.122		-.133	-.148			-.135	-.200	24
25	-.133		-.141	-.150			-.141	-.143	25
26	-.165		-.171	-.167			-.133	-.184	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.338		.498	.502			.500	.444	1
2	.268		.443	.494			.511	.315	2
3	.302		.384	.456			.490	.288	3
4	.268		.323	.354			.388	.181	4
5	.165		.184	.232			.289	.091	5
6	.171		.160	.192			.234	.033	6
7	.158		.148	.181			.194	-.025	7
8	.154		.165	.175			.158	-.016	8
9	.146		.148	.141			.135	-.019	9
10	.099		.131	.097			.089	-.019	10
11	.108		.070	.084			.135	-.044	11
12	-.263		-.288	-.274			-.294	-.324	12
13	-.302		-.285	-.313			-.324	-.321	13
14	-.299		-.324	-.313			-.324	-.252	14
15	-.313		-.307	-.318			-.335	-.217	15
16	-.189		-.285	-.285			-.313	-.222	16
17	-.038		-.042	-.059			-.030	-.016	17
18	-.030		-.046	-.042			-.023	.016	18
19	-.023		-.042	-.044			-.036	.003	19
20	-.049		-.061	-.072			-.072	-.047	20
21	-.120		-.133	-.122			-.122	-.071	21
22	-.108		-.137	-.148				-.096	22
23	-.120			-.139			-.141	-.132	23
24	-.120		-.135	-.141			-.137	-.197	24
25	-.122		-.146	-.150			-.116	-.137	25
26	-.160		-.158	-.171			-.055	-.132	26

α=-6 δ=25

1	.335		.496	.517			.511	.420	1
2	.274		.445	.502			.519	.310	2
3	.304		.380	.462			.492	.283	3
4	.279		.325	.371			.395	.167	4
5	.165		.181	.234			.289	.074	5
6	.169		.171	.194			.230	.019	6
7	.169		.150	.181			.198	-.030	7
8	.156		.169	.179			.173	-.014	8
9	.156		.148	.135			.150	-.014	9
10	.106		.133	.108			.093	-.016	10
11	.118		.074	.095			.158	-.041	11
12	-.326		-.348	-.335			-.332	-.381	12
13	-.365		-.343	-.368			-.379	-.357	13
14	-.362		-.368	-.365			-.354	-.277	14
15	-.354		-.340	-.343			-.346	-.280	15
16	-.228		-.263	-.288			-.315	-.296	16
17	-.032		-.042	-.061			-.023	-.008	17
18	-.023		-.046	-.046			-.019	.027	18
19	-.019		-.042	-.044			-.032	-.005	19
20	-.046		-.053	-.063			-.061	-.047	20
21	-.118		-.139	-.118			-.120	-.066	21
22	-.114		-.141	-.129				-.093	22
23	-.118			-.139			-.087	-.118	23
24	-.122		-.137	-.139			-.036	-.184	24
25	-.122		.078	.032			.049	-.137	25
26	.162		.171	.158			.129	-.082	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=0 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.148		.167	.179			.171	.156	1
2	.095		.169	.173			.173	.126	2
3	.122		.160	.169			.171	.123	3
4	.097		.116	.141			.120	.091	4
5	.006		.021	.044			.061	.047	5
6	.011		.017	.023			.027	.022	6
7	.025		-.015	.023			.057	.016	7
8	-.006		-.002	.021			.072	.044	8
9	.253		.357	.335			.217	.071	9
10	.371		.397	.371			.359	.200	10
11	.382		.376	.384			.430	.241	11
12	.395		.395	.395			.373	.272	12
13	.447		.425	.439			.436	.381	13
14	.625		.573	.614			.617	.400	14
15	.699		.653	.691			.675	.381	15
16	.603		.595	.647			.625	.340	16
17	.165		.181	.158			.186	.148	17
18	.127		.162	.165			.188	.154	18
19	.127		.158	.169			.173	.118	19
20	.116		.127	.139			.133	.063	20
21	.013		.004	.055			.059	.036	21
22	.013		.013	.038				.033	22
23	.015			.027			.040	.027	23
24	.008		-.006	.025			.023	.000	24
25	.008		-.013	.004			.002	.027	25
26	-.049		-.038	-.017			-.015	.055	26

α=0 δ=-20

1	.152		.173	.171			.160	.134	1
2	.097		.167	.160			.162	.121	2
3	.122		.156	.160			.152	.110	3
4	.099		.131	.127			.114	.063	4
5	-.002		.008	.049			.046	.022	5
6	.017		.021	.011			.019	.000	6
7	.032		-.013	.019			.019	-.022	7
8	-.002		-.004	.013			.000	.005	8
9	.008		-.006	.099			.034	.005	9
10	.097		.179	.042			.087	.027	10
11	.270		.289	.293			.257	.077	11
12	.299		.324	.329			.277	.162	12
13	.379		.392	.392			.376	.252	13
14	.480		.505	.494			.516	.318	14
15	.513		.516	.521			.510	.255	15
16	.472		.480	.477			.491	.197	16
17	.162		.175	.156			.169	.137	17
18	.118		.167	.152			.171	.126	18
19	.124		.160	.160			.158	.091	19
20	.114		.131	.124			.116	.030	20
21	.008		.013	.044			.038	.025	21
22	.017		.013	.030				.014	22
23	.008			.025			.019	.008	23
24	.008		-.006	.013			-.002	-.027	24
25	.006		-.011	-.008			-.008	.022	25
26	-.046		-.049	-.040			-.034	.008	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

$\alpha = 0$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.150		.169	.173			.169	.156	1
2	.082		.160	.160			.171	.126	2
3	.108		.148	.162			.165	.118	3
4	.095		.112	.133			.122	.074	4
5	.008		.006	.051			.059	.019	5
6	.004		.011	.021			.032	.014	6
7	.019		- .011	.017			.025	- .022	7
8	- .004		- .006	.013			.004	- .003	8
9	- .002		- .023	.000		-	.008	- .019	9
10	- .044		- .015	- .044		-	.042	- .011	10
11	- .004		- .059	- .057			.087	- .003	11
12	.148		.137	.129			.082	.071	12
13	.145		.151	.129			.134	.134	13
14	.140		.156	.143			.156	.088	14
15	.151		.156	.143			.151	.052	15
16	.148		.159	.143			.151	.016	16
17	.162		.171	.152			.177	.154	17
18	.112		.156	.156			.184	.143	18
19	.124		.158	.169			.165	.093	19
20	.099		.124	.129			.118	.052	20
21	.008		.011	.055			.046	.027	21
22	.006		.000	.036				.014	22
23	.013			.023			.025	.016	23
24	.008		- .013	.017			.008	- .003	24
25	.002		- .023	- .002		-	.002	.019	25
26	- .051		- .057	- .034		-	.025	- .008	26

$\alpha = 0$ $\delta = 0$

1	.133		.165	.177			.169	.151	1
2	.084		.160	.158			.177	.134	2
3	.116		.158	.165			.169	.123	3
4	.095		.120	.129			.122	.080	4
5	.002		.011	.042			.057	.041	5
6	.015		.011	.019			.034	.025	6
7	.015		- .017	.019			.027	- .019	7
8	- .008		- .004	.019		-	.002	.008	8
9	- .006		- .030	- .008		-	.013	- .011	9
10	- .040		- .025	- .044		-	.042	- .003	10
11	- .032		- .074	- .059			.049	- .014	11
12	- .055		- .069	- .080		-	.069	- .038	12
13	- .060		- .074	- .085		-	.088	- .052	13
14	- .082		- .074	- .088		-	.096	- .041	14
15	- .088		- .074	- .099		-	.101	- .044	15
16	- .082		- .074	- .099		-	.096	- .036	16
17	.152		.167	.156			.175	.148	17
18	.118		.160	.160			.184	.137	18
19	.116		.148	.162			.169	.099	19
20	.106		.114	.137			.120	.055	20
21	.002		.011	.057			.051	.033	21
22	.013		.006	.034				.033	22
23	.008			.025			.032	.033	23
24	.011		- .017	.019			.004	.000	24
25	.002		- .017	- .008		-	.002	.041	25
26	- .055		- .051	- .034		-	.021	.008	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=0 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.154		.165	.179			.171	.151	1
2	.089		.169	.167			.175	.118	2
3	.124		.150	.165			.169	.112	3
4	.101		.129	.135			.122	.071	4
5	.011		.011	.040			.068	.022	5
6	.006		.015	.023			.030	.011	6
7	.017	- .013	.021				.032	- .025	7
8	.002	- .002	.013				.004	- .008	8
9 -	.002	- .023	- .011			-	.004	- .022	9
10 -	.040	- .002	- .038			-	.040	- .008	10
11 -	.038	- .065	- .055				.046	- .016	11
12 -	.211	- .239	- .233			-	.241	- .206	12
13 -	.258	- .239	- .252			-	.258	- .167	13
14 -	.252	- .266	- .261			-	.277	- .132	14
15 -	.252	- .258	- .266			-	.263	- .159	15
16 -	.170	- .263	- .263			-	.266	- .241	16
17	.152		.175	.156			.173	.129	17
18	.118		.160	.158			.175	.132	18
19	.120		.156	.152			.158	.088	19
20	.116		.129	.120			.120	.025	20
21 -	.002		.013	.042			.046	.011	21
22	.006		.006	.019				.000	22
23	.008			.023			.025	.000	23
24	.004	- .013		.013			.002	- .008	24
25	.006	- .023	- .008			-	.002	- .005	25
26 -	.057	- .057	- .034			-	.019	- .014	26

α=0 δ=20

1	.154		.173	.171			.179	.151	1
2	.089		.169	.167			.177	.132	2
3	.118		.162	.169			.160	.112	3
4	.089		.114	.137			.124	.082	4
5	.006		.011	.055			.070	.027	5
6	.008		.013	.021			.036	.019	6
7	.013	- .004	.023				.027	- .019	7
8	.002	- .004	.011				.004	.011	8
9	.004	- .025	- .006			-	.004	- .003	9
10 -	.038	- .008	- .044			-	.042	.022	10
11 -	.027	- .063	- .055				.053	.014	11
12 -	.296	- .337	- .324			-	.324	- .288	12
13 -	.340	- .343	- .373			-	.370	- .225	13
14 -	.354	- .370	- .376			-	.348	- .283	14
15 -	.354	- .335	- .351			-	.326	- .359	15
16 -	.222	- .236	- .269			-	.266	- .381	16
17	.156		.169	.137			.169	.137	17
18	.112		.148	.156			.177	.143	18
19	.118		.156	.160			.162	.110	19
20	.108		.112	.124			.124	.049	20
21	.006		.006	.049			.044	.019	21
22	.006		.000	.030				.030	22
23	.008			.021			.027	.036	23
24	.004	- .015		.015			.008	- .008	24
25	.002	- .017	- .006				.030	.025	25
26	.162		.230	.141			.135	.058	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

$\alpha=0$ $\delta=25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.148		.177	.173			.171	.151	1
2	.101		.171	.173			.175	.126	2
3	.127		.160	.171			.171	.112	3
4	.093		.129	.131			.120	.082	4
5	-.008		.017	.042			.068	.027	5
6	.006		.017	.017			.030	.022	6
7	.017		-.008	.019			.030	-.019	7
8	-.008		.000	.019			.011	.005	8
9	.000		-.019	-.006			-.002	-.014	9
10	-.036		-.006	-.042			-.034	.022	10
11	-.032		-.061	-.051			.068	.022	11
12	-.337		-.387	-.362			-.373	-.326	12
13	-.376		-.379	-.406			-.398	-.252	13
14	-.346		-.337	-.379			-.368	-.340	14
15	-.302		-.302	-.343			-.318	-.390	15
16	-.274		-.299	-.302			-.315	-.411	16
17	.156		.171	.158			.165	.129	17
18	.118		.156	.160			.160	.129	18
19	.124		.158	.156			.156	.085	19
20	.110		.127	.131			.114	.052	20
21	.011		.008	.053			.046	.025	21
22	.013		.004	.027				.011	22
23	.006			.015			.051	.016	23
24	.008		.127	.171			.074	.016	24
25	.306		.348	.346			.279	.085	25
26	.388		.361	.363			.384	.291	26

$\alpha=3$ $\delta=0$

1	.070		.057	.076			.072	.066	1
2	.021		.317	.061			.106	.049	2
3	.042		.068	.053			.061	.071	3
4	.017		.124	.036			.025	.044	4
5	-.059		-.055	-.046			-.019	.003	5
6	.006		-.057	-.021			-.006	-.014	6
7	.194		-.051	-.059			-.023	-.041	7
8	-.063		-.070	-.068			-.072	-.036	8
9	-.072		-.080	.027			-.078	-.049	9
10	-.099		-.068	-.110			-.093	-.038	10
11	-.091		-.122	-.118			.017	-.069	11
12	-.099		-.143	-.140			-.121	-.096	12
13	-.121		-.143	-.154			-.151	-.115	13
14	-.126		-.145	-.154			-.134	-.126	14
15	-.143		-.145	-.154			-.134	-.143	15
16	-.143		-.145	-.154			-.137	-.151	16
17	.253		.310	.289			.306	.252	17
18	.177		.287	.285			.198	.214	18
19	.203		.270	.291			.287	.137	19
20	.190		.213	.251			.243	.088	20
21	.074		.087	.148			.156	.038	21
22	.087		.072	.114				.022	22
23	.084			.101			.120	.011	23
24	.076		.065	.089			.093	-.041	24
25	.078		.046	.074			.072	.011	25
26	.006		.023	.036			.036	-.008	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=6 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.030		-.027	-.021			-.015	-.016	1
2	-.042		.046	-.019			-.004	.000	2
3	-.030		-.030	-.034			-.023	.005	3
4	-.049		-.019	-.055			-.059	-.025	4
5	-.135		-.114	-.124			-.099	-.071	5
6	-.089		-.122	-.110			-.097	-.110	6
7	-.019		-.114	-.129			-.072	-.173	7
8	-.127		-.127	-.133			-.068	-.162	8
9	-.122		-.057	-.042			.027	-.178	9
10	.146		.179	.137			.099	-.099	10
11	.171		.152	.156			.217	-.126	11
12	.165		.189	.165			.156	-.165	12
13	.250		.225	.230			.176	.340	13
14	.400		.379	.354			.315	.030	14
15	.475		.458	.414			.417	.118	15
16	.431		.417	.403			.400	.230	16
17	.354		.509	.509			.530	.409	17
18	.285		.437	.496			.483	.359	18
19	.319		.388	.449			.487	.250	19
20	.291		.314	.367			.403	.167	20
21	.156		.184	.243			.281	.082	21
22	.173		.167	.209				.060	22
23	.173			.203			.203	.016	23
24	.167		.158	.194			.186	.005	24
25	.158		.160	.179			.179	.052	25
26	.112		.116	.156			.141	.011	26

α=6 δ=-20

1	-.040		-.034	-.038			-.032	.005	1
2	-.044		.006	-.025			-.019	.000	2
3	-.023		-.038	-.034			-.032	.003	3
4	-.051		-.042	-.068			-.059	-.008	4
5	-.133		-.122	-.118			-.106	-.044	5
6	-.110		-.120	-.127			-.124	-.093	6
7	-.036		-.129	-.148			-.108	-.148	7
8	-.120		-.129	-.143			-.116	-.159	8
9	-.122		-.127	-.089			-.076	-.173	9
10	-.133		-.061	-.095			-.040	-.110	10
11	.084		.091	.023			.122	-.115	11
12	.129		.154	.093			.069	-.134	12
13	.222		.222	.184			.145	.033	13
14	.269		.285	.263			.302	-.041	14
15	.294		.310	.283			.340	-.047	15
16	.294		.285	.288			.315	.016	16
17	.357		.511	.500			.528	.439	17
18	.300		.437	.492			.525	.368	18
19	.310		.388	.456			.483	.263	19
20	.287		.319	.359			.397	.184	20
21	.165		.184	.249			.270	.112	21
22	.165		.160	.194				.074	22
23	.169			.196			.200	.049	23
24	.162		.160	.184			.167	.008	24
25	.160		.154	.175			.150	.044	25
26	.093		.106	.124			.116	.005	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

$\alpha=6$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.040		-.030	-.034			-.025	-.033	1
2	-.053		-.019	-.040			-.023	-.011	2
3	-.027		-.040	-.044			-.030	.011	3
4	-.040		-.051	-.063			-.063	-.011	4
5	-.124		-.127	-.116			-.106	-.063	5
6	-.120		-.120	-.137			-.131	-.107	6
7	-.059		-.129	-.154			-.131	-.159	7
8	-.127		-.127	-.143			-.139	-.178	8
9	-.124		-.143	-.141			-.137	-.187	9
10	-.154		-.110	-.177			-.129	-.178	10
11	-.116		-.148	-.150			.004	-.176	11
12	.005		-.022	-.041			-.096	-.148	12
13	.014		.016	-.033			-.052	-.080	13
14	.014		.014	-.008			.052	-.189	14
15	.011		.011	-.005			.052	-.192	15
16	.011		.011	.000			.049	-.129	16
17	.348		.506	.504			.532	.422	17
18	.304		.433	.492			.530	.362	18
19	.314		.373	.449			.492	.269	19
20	.289		.304	.359			.384	.176	20
21	.160		.173	.236			.281	.099	21
22	.171		.160	.207				.071	22
23	.177			.190			.194	.047	23
24	.167		.160	.186			.167	-.005	24
25	.160		.154	.169			.150	.038	25
26	.099		.099	.116			.116	-.005	26

$\alpha=6$ $\delta=0$

1	-.044		-.032	-.030			-.030	-.047	1
2	-.044		-.025	-.027			-.025	-.003	2
3	-.025		-.040	-.034			-.030	.008	3
4	-.046		-.057	-.055			-.063	-.016	4
5	-.118		-.131	-.112			-.112	-.069	5
6	-.114		-.122	-.131			-.131	-.115	6
7	-.089		-.139	-.148			-.133	-.165	7
8	-.124		-.122	-.146			-.137	-.173	8
9	-.127		-.143	-.150			-.139	-.184	9
10	-.154		-.116	-.177			-.148	-.197	10
11	-.152		-.177	-.179			-.023	-.192	11
12	-.143		-.181	-.197			-.159	-.195	12
13	-.167		-.181	-.211			-.181	-.211	13
14	-.167		-.181	-.211			-.178	-.239	14
15	-.167		-.184	-.211			-.178	-.214	15
16	-.167		-.184	-.211			-.178	-.203	16
17	.359		.506	.500			.519	.400	17
18	.304		.439	.487			.523	.337	18
19	.314		.386	.441			.485	.247	19
20	.287		.321	.357			.399	.165	20
21	.169		.186	.234			.279	.091	21
22	.177		.167	.200				.047	22
23	.171			.192			.198	.016	23
24	.160		.160	.184			.173	-.005	24
25	.156		.160	.160			.150	.022	25
26	.087		.114	.122			.116	-.008	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=6 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.036		-.030	-.025			-.027	-.033	1
2	-.049		-.040	-.032			-.025	.011	2
3	-.021		-.038	-.036			-.025	.030	3
4	-.051		-.057	-.057			-.059	-.008	4
5	-.118		-.124	-.114			-.108	-.052	5
6	-.106		-.118	-.135			-.135	-.088	6
7	-.091		-.135	-.141			-.129	-.170	7
8	-.120		-.122	-.146			-.150	-.178	8
9	-.120		-.146	-.160			-.143	-.184	9
10	-.160		-.110	-.184			-.154	-.187	10
11	-.152		-.175	-.184			-.025	-.165	11
12	-.252		-.291	-.299			-.272	-.307	12
13	-.304		-.296	-.321			-.299	-.283	13
14	-.299		-.321	-.340			-.302	-.315	14
15	-.315		-.318	-.332			-.307	-.321	15
16	-.170		-.219	-.283			-.285	-.326	16
17	.354		.509	[illegible]			.519	.406	17
18	.300		.443	.492			.525	.351	18
19	.321		.390	.449			.481	.269	19
20	.289		.317	.361			.392	.184	20
21	.165		.186	.241			.283	.101	21
22	.171		.162	.205				.055	22
23	.165			.188			.198	.038	23
24	.162		.154	.186			.162	-.022	24
25	.160		.156	.162			.139	.038	25
26	.101		.114	.122			.116	-.005	26

α=6 δ=20

1	-.030		-.030	-.034			-.032	-.025	1
2	-.042		-.038	-.036			-.034	-.005	2
3	-.030		-.044	-.038			-.038	.014	3
4	-.049		-.070	-.065			-.072	-.022	4
5	-.122		-.129	-.112			-.118	-.058	5
6	-.112		-.120	-.137			-.139	-.104	6
7	-.099		-.133	-.143			-.139	-.162	7
8	-.129		-.127	-.141			-.148	-.167	8
9	-.114		-.148	-.152			-.150	-.176	9
10	-.150		-.114	-.181			-.162	-.151	10
11	-.148		-.179	-.177			-.036	-.112	11
12	-.332		-.370	-.368			-.359	-.346	12
13	-.373		-.370	-.395			-.390	-.318	13
14	-.376		-.362	-.373			-.387	-.370	14
15	-.313		-.324	-.332			-.381	-.381	15
16	-.272		-.294	-.304			-.299	-.384	16
17	.359		.504	.494			.506	.411	17
18	.304		.437	.483			.513	.337	18
19	.319		.388	.443			.475	.263	19
20	.293		.317	.354			.390	.181	20
21	.165		.181	.241			.270	.099	21
22	.173		.165	.196				.063	22
23	.165			.188			.186	.030	23
24	.165		.158	.181			.162	.000	24
25	.325		.460	.452			.173	.025	25
26	.513		.551	.538			.504	.178	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=6 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.030		-.025	-.032			-.021	-.049	1
2	-.042		-.025	-.034			-.019	-.011	2
3	-.023		-.038	-.032			-.023	.003	3
4	-.049		-.057	-.055			-.061	-.014	4
5	-.120		-.127	-.118			-.099	-.060	5
6	-.110		-.122	-.133			-.124	-.110	6
7	-.099		-.133	-.143			-.124	-.170	7
8	-.127		-.124	-.143			-.146	-.181	8
9	-.118		-.148	-.150			-.137	-.140	9
10	-.150		-.116	-.181			-.150	-.071	10
11	-.143		-.179	-.219			-.023	-.121	11
12	-.368		-.384	-.411			-.392	-.384	12
13	-.400		-.370	-.403			-.417	-.373	13
14	-.373		-.337	-.368			-.403	-.409	14
15	-.337		-.340	-.354			-.351	-.414	15
16	-.324		-.337	-.346			-.326	-.403	16
17	.363		.509	.494			.517	.387	17
18	.312		.441	.490			.521	.343	18
19	.321		.388	.454			.487	.255	19
20	.293		.321	.357			.405	.176	20
21	.165		.186	.241			.289	.091	21
22	.175		.167	.203				.060	22
23	.272			.536			.380	.036	23
24	.549		.578	.616			.599	.137	24
25	.597		.606	.627			.637	.294	25
26	.612		.618	.639			.652	.337	26

α=9 δ=0

1	-.091		-.106	-.101			-.103	-.099	1
2	-.110		-.097	-.099			-.061	-.044	2
3	-.084		-.093	-.095			-.093	-.033	3
4	-.108		-.038	-.127			-.131	-.082	4
5	-.177		-.173	-.175			-.152	-.126	5
6	-.118		-.175	-.148			-.139	-.184	6
7	.091		-.160	-.188			-.152	-.233	7
8	-.167		-.181	-.205			-.186	-.181	8
9	-.165		-.184	-.114			-.188	-.233	9
10	-.203		-.148	-.222			-.192	-.219	10
11	-.198		-.205	-.230			-.055	-.222	11
12	-.159		-.228	-.236			-.219	-.250	12
13	-.195		-.219	-.258			-.219	-.263	13
14	-.228		-.225	-.247			-.219	-.263	14
15	-.225		-.233	-.250			-.222	-.263	15
16	-.178		-.233	-.252			-.222	-.263	16
17	.464		.709	.766			.817	.603	17
18	.390		.574	.641			.601	.486	18
19	.428		.513	.582			.629	.354	19
20	.386		.443	.460			.492	.252	20
21	.251		.270	.321			.361	.140	21
22	.268		.251	.285				.093	22
23	.255			.272			.268	.063	23
24	.253		.266	.262			.238	.016	24
25	.249		.243	.243			.211	.063	25
26	.173		.192	.192			.177	.027	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=12 δ=-25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.156		-.181	-.200			-.203	-.230	1
2	-.160		-.097	-.173			-.156	-.143	2
3	-.124		-.162	-.171			-.162	-.134	3
4	-.150		-.133	-.188			-.188	-.181	4
5	-.196		-.228	-.232			-.205	-.222	5
6	-.181		-.224	-.215			-.203	-.280	6
7	-.116		-.217	-.236			-.211	-.313	7
8	-.205		-.232	-.238			-.238	-.274	8
9	-.203		-.217	-.217			-.186	-.302	9
10	-.030		-.002	-.065			-.091	-.269	10
11	.023		-.004	-.034			.093	-.269	11
12	.000		.047	.008			.016	-.261	12
13	.101		.066	.014			.049	-.159	13
14	.233		.214	.145			.211	-.203	14
15	.269		.263	.187			.283	-.244	15
16	.266		.258	.184			.269	-.291	16
17	.606		.884	.954			.990	.710	17
18	.540		.732	.814			.846	.573	18
19	.584		.652	.722			.749	.428	19
20	.515		.525	.559			.595	.304	20
21	.361		.354	.416			.447	.187	21
22	.378		.365	.392				.145	22
23	.357			.388			.361	.115	23
24	.357		.357	.380			.329	.055	24
25	.346		.346	.361			.308	.107	25
26	.268		.285	.306			.279	.066	26

α=12 δ=-20

1	-.186		-.207	-.228			-.228	-.207	1
2	-.167		-.131	-.190			-.186	-.102	2
3	-.148		-.188	-.188			-.181	-.105	3
4	-.162		-.179	-.211			-.203	-.208	4
5	-.215		-.249	-.245			-.230	-.200	5
6	-.207		-.236	-.245			-.230	-.307	6
7	-.137		-.241	-.253			-.232	-.308	7
8	-.222		-.241	-.253			-.253	-.304	8
9	-.222		-.234	-.241			-.224	-.306	9
10	-.217		-.135	-.222			-.175	-.308	10
11	-.042		-.055	-.112			.057	-.303	11
12	.030		-.019	-.055			-.008	-.201	12
13	.047		.047	-.025			.030	-.108	13
14	.099		.115	.044			.121	-.209	14
15	.134		.123	.049			.121	-.205	15
16	.112		.121	.049			.126	-.208	16
17	.580		.884	.947			.994	.705	17
18	.538		.722	.808			.882	.501	18
19	.580		.644	.722			.753	.401	19
20	.509		.519	.553			.595	.203	20
21	.354		.350	.420			.441	.107	21
22	.361		.359	.392				.101	22
23	.340			.388			.352	.101	23
24	.342		.350	.376			.329	.000	24
25	.348		.340	.359			.306	.102	25
26	.255		.285	.304			.270	.005	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=12 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.200		-.217	-.238			-.245	-.269	1
2	-.190		-.173	-.200			-.207	-.148	2
3	-.150		-.200	-.192			-.196	-.145	3
4	-.175		-.205	-.215			-.217	-.208	4
5	-.230		-.268	-.260			-.245	-.255	5
6	-.230		-.251	-.266			-.255	-.346	6
7	-.171		-.255	-.268			-.255	-.362	7
8	-.245		-.253	-.262			-.272	-.329	8
9	-.236		-.255	-.262			-.253	-.359	9
10	-.249		-.190	-.295			-.249	-.337	10
11	-.211		-.236	-.264			-.061	-.315	11
12	-.096		-.129	-.165			-.145	-.307	12
13	-.096		-.093	-.165			-.118	-.288	13
14	-.107		-.110	-.165			-.085	-.318	14
15	-.107		-.093	-.165			-.085	-.324	15
16	-.107		-.096	-.165			-.085	-.291	16
17	.587		.874	.950			.983	.724	17
18	.538		.709	.817			.865	.573	18
19	.568		.644	.717			.736	.420	19
20	.506		.511	.546			.587	.307	20
21	.344		.346	.403			.435	.189	21
22	.371		.359	.386				.143	22
23	.340			.380			.348	.112	23
24	.346		.344	.369			.312	.063	24
25	.333		.333	.352			.295	.107	25
26	.249		.283	.287			.260	.049	26

α=12 δ=0

1	-.188		-.217	-.228			-.245	-.252	1
2	-.179		-.177	-.198			-.198	-.159	2
3	-.154		-.194	-.184			-.190	-.154	3
4	-.162		-.200	-.213			-.217	-.203	4
5	-.222		-.264	-.247			-.243	-.274	5
6	-.215		-.243	-.260			-.260	-.354	6
7	-.186		-.255	-.266			-.255	-.368	7
8	-.232		-.245	-.264			-.274	-.332	8
9	-.226		-.249	-.266			-.257	-.365	9
10	-.245		-.188	-.298			-.260	-.332	10
11	-.247		-.262	-.293			-.084	-.324	11
12	-.214		-.241	-.288			-.252	-.332	12
13	-.236		-.244	-.288			-.272	-.335	13
14	-.247		-.266	-.288			-.247	-.348	14
15	-.239		-.272	-.291			-.247	-.343	15
16	-.159		-.247	-.291			-.247	.395	16
17	.599		.878	.943			.975	.716	17
18	.544		.715	.810			.869	.565	18
19	.559		.641	.713			.739	.420	19
20	.500		.523	.542			.576	.310	20
21	.354		.346	.403			.449	.189	21
22	.361		.357	.378				.137	22
23	.344			.371			.350	.115	23
24	.348		.348	.367			.317	.115	24
25	.335		.340	.344			.287	.104	25
26	.255		.279	.298			.262	.052	26

TABLE IX.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.186		-.211	-.232			-.241	-.230	1
2	-.179		-.177	-.198			-.194	-.148	2
3	-.150		-.198	-.192			-.190	-.121	3
4	-.169		-.205	-.209			-.207	-.178	4
5	-.224		-.268	-.257			-.236	-.230	5
6	-.217		-.245	-.262			-.255	-.332	6
7	-.184		-.257	-.264			-.253	-.354	7
8	-.226		-.245	-.257			-.264	-.321	8
9	-.213		-.245	-.272			-.251	-.348	9
10	-.249		-.192	-.285			-.253	-.318	10
11	-.241		-.266	-.298			-.089	-.296	11
12	-.294		-.337	-.357			-.337	-.370	12
13	-.337		-.337	-.365			-.354	-.365	13
14	-.337		-.348	-.379			-.337	-.384	14
15	-.332		-.337	-.370			-.348	-.392	15
16	-.200		-.222	-.272			-.315	-.376	16
17	.582		.880	.941			.983	.752	17
18	.536		.711	.808			.878	.587	18
19	.565		.648	.713			.751	.431	19
20	.500		.515	.553			.597	.321	20
21	.340		.338	.409			.447	.200	21
22	.369		.357	.382				.148	22
23	.327			.378			.348	.126	23
24	.338		.346	.369			.312	.071	24
25	.329		.319	.350			.302	.129	25
26	.249		.283	.304			.270	.058	26

α=12 δ=20

1	-.196		-.211	-.226			-.241	-.236	1
2	-.173		-.173	-.192			-.196	-.121	2
3	-.154		-.188	-.186			-.179	-.129	3
4	-.171		-.211	-.211			-.209	-.181	4
5	-.222		-.266	-.249			-.241	-.241	5
6	-.213		-.249	-.266			-.262	-.332	6
7	-.192		-.260	-.260			-.257	-.362	7
8	-.234		-.241	-.255			-.268	-.321	8
9	-.203		-.243	-.268			-.255	-.354	9
10	-.253		-.192	-.287			-.257	-.304	10
11	-.230		-.274	-.289			-.072	-.294	11
12	-.370		-.398	-.395			-.390	-.428	12
13	-.406		-.384	-.409			-.414	-.409	13
14	-.392		-.368	-.376			-.417	-.425	14
15	-.335		-.346	-.359			-.403	-.422	15
16	-.310		-.343	-.359			-.346	-.406	16
17	.601		.867	.937			.979	.721	17
18	.538		.726	.819			.874	.565	18
19	.568		.648	.715			.747	.433	19
20	.509		.509	.549			.589	.318	20
21	.346		.338	.409			.430	.197	21
22	.365		.354	.384				.137	22
23	.644			.772			.652	.222	23
24	.789		.814	.859			.747	.310	24
25	.833		.874	.924			.840	.439	25
26	.861		.897	.962			.920	.549	26

TABLE IX.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 1.7 \times 10^6$.

α=12 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.194		-.211	-.234			-.236	-.250	1
2	-.186		-.181	-.205			-.205	-.167	2
3	-.152		-.196	-.188			-.188	-.143	3
4	-.173		-.205	-.209			-.213	-.200	4
5	-.232		-.257	-.251			-.245	-.274	5
6	-.219		-.249	-.260			-.255	-.354	6
7	-.209		-.257	-.260			-.255	-.381	7
8	-.230		-.249	-.264			-.264	-.340	8
9	-.226		-.249	-.270			-.253	-.373	9
10	-.249		-.200	-.289			-.251	-.332	10
11	-.236		-.283	-.291			-.063	-.315	11
12	-.406		-.398	-.403			-.420	-.455	12
13	-.425		-.400	-.409			-.447	-.453	13
14	-.403		-.373	-.398			-.444	-.453	14
15	-.357		-.365	-.395			-.417	-.447	15
16	-.351		-.365	-.395			-.362	-.444	16
17	.582		.869	.943			.977	.716	17
18	.540		.713	.810			.871	.560	18
19	.565		.639	.722			.743	.431	19
20	.498		.517	.546			.669	.329	20
21	.344		.346	.555			.677	.280	21
22	.671		.798	.846				.368	22
23	.888			.960			.874	.458	23
24	.945		.977	1.019			.935	.455	24
25	.979		1.019	1.080			1.006	.549	25
26	1.021		1.047	1.120			1.082	.617	26

α=15 δ=0

1	-.215		-.276	-.285			-.289	-.313	1
2	-.217		-.051	-.243			-.219	-.241	2
3	-.171		-.211	-.234			-.234	-.217	3
4	-.205		-.154	-.245			-.243	-.269	4
5	-.238		-.276	-.274			-.257	-.302	5
6	-.198		-.270	-.245			-.236	-.343	6
7	.008		-.255	-.285			-.251	-.376	7
8	-.243		-.274	-.293			-.285	-.335	8
9	-.241		-.264	-.215			-.276	-.370	9
10	-.266		-.211	-.302			-.279	-.335	10
11	-.264		-.283	-.308			-.103	-.348	11
12	-.266		-.310	-.340			-.294	-.368	12
13	-.294		-.302	-.351			-.315	-.368	13
14	-.294		-.324	-.351			-.296	-.370	14
15	-.291		-.313	-.351			-.294	-.370	15
16	-.148		-.217	-.299			-.291	-.370	16
17	.766		1.055	1.087			1.093	.790	17
18	.684		.863	.937			.935	.620	18
19	.739		.772	.833			.846	.483	19
20	.631		.620	.660			.684	.365	20
21	.481		.466	.521			.563	.233	21
22	.528		.521	.561				.211	22
23	.517			.561			.481	.189	23
24	.532		.555	.542			.460	.134	24
25	.513		.502	.504			.437	.167	25
26	.395		.416	.420			.388	.132	26

TABLE X

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

α=-12 δ=-5

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.606		.872	.946			.946	.759	1
2	.531		.725	.815			.849	.574	2
3	.550		.652	.721			.739	.445	3
4	.514		.521	.557			.571	.292	4
5	.358		.350	.406			.440	.183	5
6	.351		.343	.375			.373	.090	6
7	.309		.343	.369			.342	.070	7
8	.334		.352	.359			.307	.035	8
9	.322		.320	.313			.286	.059	9
10	.270		.258	.276			.221	.042	10
11	.274		.215	.241			.166	.014	11
12	.335		.336	.322			.271	.047	12
13	.325		.331	.335			.262	.041	13
14	.326		.330	.324			.253	.042	14
15	.323		.326	.324			.245	.032	15
16	.321		.326	.305			.235	.020	16
17	-.208		-.236	-.261			-.276	-.246	17
18	-.150		-.202	-.216			-.219	-.140	18
19	-.150		-.204	-.203			-.206	-.166	19
20	-.173		-.217	-.224			-.231	-.194	20
21	-.229		-.272	-.265			-.263	-.269	21
22	-.226		-.276	-.281				-.335	22
23	-.229			-.285			-.290	-.357	23
24	-.232		-.261	-.286			-.291	-.376	24
25	-.232		-.262	-.297			-.279	-.362	25
26	-.269		-.279	-.310			-.278	-.387	26

α=-12 δ=0

1	.610		.874	.956			.960	.758	1
2	.529		.730	.819			.864	.579	2
3	.552		.655	.726			.750	.453	3
4	.514		.521	.565			.586	.305	4
5	.358		.357	.413			.453	.188	5
6	.356		.347	.383			.386	.102	6
7	.344		.348	.380			.355	.074	7
8	.333		.354	.368			.317	.046	8
9	.321		.320	.326			.300	.058	9
10	.269		.263	.283			.236	.050	10
11	.275		.225	.251			.179	.017	11
12	.138		.160	.172			.119	-.067	12
13	.155		.142	.156			.103	-.082	13
14	.158		.146	.148			.096	-.081	14
15	.149		.150	.146			.088	-.080	15
16	.148		.151	.133			.080	-.091	16
17	-.207		-.235	-.259			-.268	-.247	17
18	-.151		-.200	-.211			-.223	-.145	18
19	-.151		-.203	-.199			-.198	-.166	19
20	-.175		-.214	-.218			-.221	-.195	20
21	-.232		-.269	-.259			-.257	-.279	21
22	-.228		-.276	-.276				-.344	22
23	-.229			-.278			-.278	-.368	23
24	-.232		-.259	-.281			-.283	-.388	24
25	-.234		-.259	-.288			-.269	-.365	25
26	-.264		-.276	-.302			-.263	-.388	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

α=-12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.609		.876	.958			.958	.760	1
2	.534		.731	.821			.861	.586	2
3	.554		.656	.728			.748	.460	3
4	.518		.526	.566			.583	.306	4
5	.363		.357	.413			.451	.187	5
6	.362		.352	.386			.383	.104	6
7	.348		.353	.375			.351	.074	7
8	.338		.356	.366			.318	.044	8
9	.326		.321	.321			.294	.064	9
10	.274		.264	.283			.231	.054	10
11	.278		.225	.245			.179	.023	11
12 -	.072	- .092	- .078			-	.127 -	.230	12
13 -	.110	- .105	- .106			-	.143 -	.252	13
14 -	.103	- .117	- .114			-	.140 -	.239	14
15 -	.114	- .114	- .119			-	.152 -	.240	15
16 -	.114	- .114	- .122			-	.164 -	.244	16
17 -	.204	- .229	- .258			-	.273 -	.253	17
18 -	.141	- .195	- .211			-	.222 -	.137	18
19 -	.143	- .197	- .201			-	.201 -	.158	19
20 -	.171	- .212	- .218			-	.223 -	.198	20
21 -	.225	- .264	- .261			-	.259 -	.269	21
22 -	.218	- .271	- .278				-	.334	22
23 -	.224		- .279			-	.279 -	.361	23
24 -	.226	- .254	- .280			-	.283 -	.381	24
25 -	.226	- .256	- .289			-	.271 -	.359	25
26 -	.260	- .273	- .305			-	.273 -	.384	26

α=-12 δ=20

1	.615		.884	.968			.971	.767	1
2	.538		.736	.832			.874	.586	2
3	.561		.661	.733			.760	.460	3
4	.526		.533	.576			.596	.307	4
5	.367		.364	.423			.459	.191	5
6	.363		.357	.391			.393	.106	6
7	.356		.361	.386			.364	.085	7
8	.347		.364	.378			.330	.054	8
9	.331		.331	.331			.310	.069	9
10	.280		.276	.296			.243	.058	10
11	.290		.235	.261			.195	.028	11
12 -	.218	- .238	- .231			-	.252 -	.327	12
13 -	.274	- .248	- .254			-	.270 -	.340	13
14 -	.240	- .261	- .258			-	.275 -	.302	14
15 -	.272	- .266	- .266			-	.282 -	.298	15
16 -	.261	- .262	- .265			-	.285 -	.296	16
17 -	.194	- .222	- .256			-	.269 -	.249	17
18 -	.138	- .192	- .203			-	.214 -	.146	18
19 -	.138	- .191	- .191			-	.195 -	.166	19
20 -	.163	- .213	- .212			-	.218 -	.200	20
21 -	.218	- .261	- .253			-	.254 -	.269	21
22 -	.213	- .265	- .264				-	.334	22
23 -	.216		- .273			-	.273 -	.357	23
24 -	.223	- .248	- .273			-	.278 -	.375	24
25 -	.223	- .250	- .282			-	.263 -	.365	25
26 -	.253	- .244	- .294			-	.190 -	.382	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

α=-6 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.359		.504	.505			.505	.433	1
2	.308		.449	.498			.515	.335	2
3	.303		.399	.463			.488	.291	3
4	.294		.318	.374			.391	.181	4
5	.168		.188	.239			.284	.106	5
6	.160		.167	.194			.230	.037	6
7	.023		.156	.193			.193	.011	7
8	.158		.163	.183			.161	-.005	8
9	.154		.139	.148			.151	.000	9
10	.114		.099	.116			.088	-.005	10
11	.149		.070	.095			.055	-.029	11
12	.307		.322	.299			.300	.076	12
13	.326		.329	.335			.292	.157	13
14	.339		.346	.344			.279	.131	14
15	.335		.347	.343			.277	.112	15
16	.328		.344	.334			.267	.080	16
17	-.048		-.044	-.048			-.038	-.019	17
18	-.022		-.033	-.033			.065	.043	18
19	-.020		-.046	-.039			-.024	.023	19
20	-.050		-.059	-.059			-.061	-.010	20
21	-.123		-.131	-.121			-.111	-.050	21
22	-.118		-.135	-.141				-.084	22
23	-.119			-.141			-.139	-.136	23
24	-.124		-.140	-.145			-.144	-.171	24
25	-.124		-.150	-.149			-.139	-.149	25
26	-.168		-.173	-.168			-.153	-.184	26

α=-6 δ=0

1	.353		.499	.504			.507	.435	1
2	.301		.443	.497			.511	.337	2
3	.298		.395	.458			.485	.286	3
4	.286		.314	.368			.386	.181	4
5	.160		.183	.235			.279	.100	5
6	.162		.160	.193			.227	.033	6
7	.100		.150	.183			.187	.000	7
8	.152		.158	.176			.159	-.004	8
9	.145		.135	.141			.144	-.003	9
10	.106		.094	.104			.083	-.015	10
11	.120		.062	.083			.047	-.037	11
12	.024		.007	.025			-.011	-.101	12
13	.015		.003	-.001			-.023	-.109	13
14	-.001		.003	.002			-.032	-.119	14
15	.000		.002	.007			-.041	-.110	15
16	-.002		.002	-.005			-.050	-.102	16
17	-.060		-.057	-.061			-.052	-.032	17
18	-.034		-.046	-.049			-.039	.028	18
19	-.031		-.049	-.049			-.043	.007	19
20	-.063		-.071	-.073			-.079	-.021	20
21	-.131		-.140	-.129			-.126	-.064	21
22	-.124		-.144	-.153				-.106	22
23	-.129			-.155			-.154	-.153	23
24	-.133		-.149	-.158			-.161	-.187	24
25	-.138		-.161	-.170			-.153	-.164	25
26	-.178		-.183	-.184			-.167	-.203	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

α=-6 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.351		.495	.498			.511	.437	1
2	.294		.437	.492			.514	.342	2
3	.289		.387	.453			.484	.292	3
4	.281		.307	.363			.380	.176	4
5	.153		.176	.228			.276	.097	5
6	.157		.150	.184			.222	.032	6
7	.130		.143	.180			.180	-.002	7
8	.144		.154	.167			.150	-.011	8
9	.138		.122	.137			.137	-.006	9
10	.099		.082	.097			.076	-.015	10
11	.114		.053	.078			.038	-.044	11
12	-.152		-.164	-.158			-.179	-.242	12
13	-.186		-.185	-.191			-.197	-.261	13
14	-.178		-.196	-.183			-.205	-.214	14
15	-.188		-.196	-.191			-.213	-.162	15
16	-.188		-.192	-.192			-.224	-.132	16
17	-.072		-.073	-.075			-.066	-.045	17
18	-.044		-.058	-.061			-.062	-.019	18
19	-.043		-.066	-.063			-.056	-.001	19
20	-.074		-.084	-.093			-.093	-.032	20
21	-.144		-.158	-.144			-.145	-.077	21
22	-.139		-.158	-.171				-.118	22
23	-.143			-.169			-.170	-.161	23
24	-.146		-.164	-.173			-.177	-.204	24
25	-.147		-.175	-.180			-.174	-.167	25
26	-.192		-.199	-.197			-.184	-.212	26

α=-6 δ=20

1	.369		.514	.526			.547	.467	1
2	.313		.452	.514			.544	.356	2
3	.309		.409	.472			.506	.293	3
4	.303		.331	.381			.404	.190	4
5	.171		.188	.245			.295	.105	5
6	.172		.171	.199			.237	.037	6
7	.166		.160	.200			.199	.006	7
8	.160		.168	.186			.169	-.001	8
9	.157		.144	.155			.155	.002	9
10	.118		.103	.121			.096	-.012	10
11	.134		.073	.108			.059	-.029	11
12	-.280		-.294	-.286			-.298	-.339	12
13	-.326		-.309	-.319			-.318	-.347	13
14	-.300		-.322	-.318			-.323	-.266	14
15	-.325		-.322	-.318			-.333	-.209	15
16	-.211		-.322	-.328			-.335	-.201	16
17	-.061		-.064	-.068			-.058	-.035	17
18	-.031		-.049	-.054			-.051	.024	18
19	-.029		-.059	-.055			-.049	.004	19
20	-.066		-.076	-.080			-.084	-.031	20
21	-.133		-.145	-.134			-.139	-.073	21
22	-.124		-.148	-.156				-.126	22
23	-.131			-.159			-.161	-.177	23
24	-.132		-.148	-.159			-.164	-.211	24
25	-.132		-.164	-.171			-.157	-.183	25
26	-.174		-.183	-.185			-.126	-.218	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 0$ $\delta = -15$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.143		.155	.156			.151	.128	1
2	.112		.158	.164			.160	.110	2
3	.119		.164	.165			.154	.113	3
4	.108		.120	.133			.108	.073	4
5	.007		.014	.048			.044	.032	5
6	.006		.005	.017			.019	.024	6
7	.008	- .005	.012				.014	.011	7
8 -	.008	- .003	.001			- .003	.012		8
9	.002	- .021	- .023			- .008	.004		9
10 -	.036	- .049	- .048			- .048	.000		10
11	.108	- .055	- .036			- .008	- .008		11
12	.214	.235	.200				.217	.187	12
13	.263	.278	.261				.266	.203	13
14	.286	.304	.292				.291	.149	14
15	.292	.312	.304				.296	.122	15
16	.292	.312	.296				.298	.094	16
17	.138	.162	.149				.158	.135	17
18	.124	.167	.169				.178	.168	18
19	.122	.160	.162				.170	.116	19
20	.103	.118	.129				.126	.071	20
21	.007	.019	.046				.054	.037	21
22	.012	.010	.024					.024	22
23	.009		.019				.020	.014	23
24	.004	- .009	.014				.006	.005	24
25	.003	- .019	- .007			- .006	.021		25
26 -	.054	- .051	- .038			- .038	- .003		26

$\alpha = 0$ $\delta = -10$

1	.137		.149	.156			.151	.122	1
2	.103		.149	.161			.159	.106	2
3	.111		.159	.163			.157	.109	3
4	.099		.116	.127			.112	.065	4
5 -	.003		.010	.044			.046	.024	5
6 -	.001	- .001	.014				.018	.010	6
7 -	.002	- .011	.007				.015	.001	7
8 -	.009	- .006	.000			- .001	.001		8
9 -	.009	- .028	- .028			- .009	- .006		9
10 -	.044	- .056	- .054			- .048	- .011		10
11 -	.014	- .078	- .068			- .065	- .032		11
12	.106	.098	.082				.097	.101	12
13	.117	.113	.102				.106	.109	13
14	.117	.119	.114				.114	.054	14
15	.117	.127	.123				.118	.032	15
16	.117	.127	.123				.117	.007	16
17	.133	.158	.143				.154	.130	17
18	.117	.159	.161				.177	.160	18
19	.113	.154	.158				.169	.109	19
20	.094	.113	.123				.124	.067	20
21	.001	.014	.043				.053	.027	21
22	.006	.003	.019					.014	22
23	.003		.011				.017	.006	23
24 -	.002	- .015	.008				.006	- .001	24
25 -	.003	- .026	- .011			- .007	.016		25
26 -	.060	- .054	- .041			- .038	- .014		26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.131		.145	.151			.152	.118	1
2	.096		.144	.158			.159	.099	2
3	.108		.153	.158			.157	.101	3
4	.093		.108	.126			.111	.058	4
5	- .006		.003	.039			.047	.012	5
6	- .009	- .008		.008			.016	.006	6
7	- .011	- .018		.003			.014	- .003	7
8	- .018	- .014	- .004			- .005	- .003		8
9	- .020	- .034	- .031			- .011	- .019		9
10	- .049	- .066	- .058			- .050	- .024		10
11	- .036	- .090	- .073			- .072	- .041		11
12	- .093	- .103	- .094			- .102	- .057		12
13	- .099	- .117	- .123			- .110	- .067		13
14	- .106	- .117	- .117			- .119	- .055		14
15	- .113	- .113	- .111			- .119	- .056		15
16	- .115	- .113	- .111			- .120	- .055		16
17	.123		.150	.136			.147	.112	17
18	.110		.152	.156			.172	.146	18
19	.104		.146	.151			.161	.097	19
20	.088		.106	.116			.118	.050	20
21	- .009		.007	.036			.045	.016	21
22	- .002	- .004		.010				.006	22
23	- .004			.006			.010	- .005	23
24	- .009	- .024		.003		- .003	- .011		24
25	- .009	- .034	- .019			- .014		.004	25
26	- .068	- .065	- .050			- .042	- .030		26

$\alpha = 0$ $\delta = 10$

1	.128		.149	.158			.163	.132	1
2	.098		.151	.164			.172	.110	2
3	.109		.157	.165			.168	.112	3
4	.094		.114	.131			.121	.067	4
5	- .009		.007	.056			.057	.024	5
6	- .009	- .002		.019			.026	.011	6
7	- .005	- .013		.012			.025	.002	7
8	- .019	- .010		.004			.005	.007	8
9	- .016	- .031	- .019			- .001	- .006		9
10	- .049	- .059	- .051			- .042	- .011		10
11	- .033	- .081	- .063			- .062	- .024		11
12	- .239	- .246	- .239			- .240	- .233		12
13	- .261	- .266	- .270			- .259	- .192		13
14	- .251	- .273	- .272			- .262	- .127		14
15	- .263	- .270	- .272			- .270	- .150		15
16	- .244	- .272	- .272			- .274	- .237		16
17	.125		.151	.139			.149	.119	17
18	.110		.154	.157			.174	.153	18
19	.106		.149	.154			.163	.105	19
20	.091		.107	.119			.119	.062	20
21	- .006		.008	.039			.045	.028	21
22	.002	- .001		.016				.009	22
23	- .003			.011			.014	.004	23
24	- .009	- .021		.008			.000	- .002	24
25	- .009	- .030	- .013			- .013		.013	25
26	- .066	- .061	- .043			- .039	- .015		26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 0$ $\delta = 15$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.134		.153	.159			.163	.132	1
2	.104		.151	.163			.172	.115	2
3	.113		.161	.169			.169	.112	3
4	.096		.113	.133			.123	.067	4
5	-.006		.008	.051			.059	.024	5
6	-.004		.001	.017			.030	.011	6
7	-.002	-.012		.016			.026	.001	7
8	-.014	-.006		.004			.006	.005	8
9	-.008	-.026	-.016			-.001	-.004		9
10	-.046	-.054	-.048			-.041	-.014		10
11	-.025	-.080	-.056			-.056	-.013		11
12	-.307	-.313	-.308			-.305	-.292		12
13	-.328	-.333	-.337			-.328	-.231		13
14	-.314	-.343	-.339			-.333	-.192		14
15	-.330	-.337	-.339			-.337	-.283		15
16	-.200	-.279	-.256			-.335	-.411		16
17	.126		.151	.137			.146	.110	17
18	.109		.154	.156			.167	.149	18
19	.109		.146	.153			.157	.103	19
20	.091		.109	.117			.116	.063	20
21	-.006		.009	.041			.044	.028	21
22	.001	-.001		.014				.015	22
23	-.003			.010			.011	.007	23
24	-.003	-.020		.007		-.001	-.003		24
25	-.009	-.032	-.014			-.013	-.014		25
26	-.065	-.060	-.046			-.041	-.011		26

$\alpha = 6$ $\delta = -20$

1	-.068	-.056	-.049			-.047	-.052		1
2	-.051	-.029	-.041			-.040	-.004		2
3	-.043	-.050	-.043			-.044	.007		3
4	-.061	-.064	-.067			-.075	-.024		4
5	-.135	-.149	-.122			-.121	-.078		5
6	-.131	-.149	-.148			-.137	-.143		6
7	-.089	-.153	-.147			-.140	-.184		7
8	-.142	-.141	-.154			-.151	-.221		8
9	-.133	-.156	-.160			-.141	-.209		9
10	-.165	-.177	-.186			-.148	-.223		10
11	.037	.046	.024			.096	-.233		11
12	.097	.104	.067			.119	.103		12
13	.197	.176	.119			.182	-.123		13
14	.254	.248	.208			.271	-.110		14
15	.263	.274	.238			.304	-.044		15
16	.268	.280	.245			.304	.334		16
17	.355	.516	.527			.564	.422		17
18	.313	.452	.522			.566	.373		18
19	.306	.396	.474			.526	.287		19
20	.282	.324	.380			.421	.204		20
21	.163	.191	.251			.306	.102		21
22	.171	.173	.213				.062		22
23	.169		.207			.212	.029		23
24	.163	.160	.195			.184	.005		24
25	.161	.148	.175			.167	.034		25
26	.090	.114	.138			.128	-.012		26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 6$ $\delta = -10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.076		-.064	-.056			-.055	-.054	1
2	-.061		-.056	-.049			-.048	-.002	2
3	-.051		-.061	-.047			-.050	.008	3
4	-.066		-.078	-.071			-.080	-.021	4
5	-.146		-.151	-.129			-.124	-.072	5
6	-.141		-.156	-.156			-.145	-.136	6
7	-.121		-.154	-.151			-.151	-.184	7
8	-.151		-.148	-.162			-.158	-.216	8
9	-.143		-.168	-.174			-.149	-.205	9
10	-.174		-.186	-.194			-.166	-.224	10
11	-.133		-.203	-.201			-.152	-.232	11
12	-.023		-.037	-.064			-.030	-.124	12
13	-.007		-.021	-.050			-.007	-.110	13
14	-.007		-.008	-.038			.012	-.206	14
15	-.007		-.004	-.032			.024	-.243	15
16	-.007		-.004	-.024			.030	-.187	16
17	.347		.510	.515			.550	.420	17
18	.305		.447	.513			.555	.373	18
19	.298		.393	.464			.512	.282	19
20	.275		.316	.370			.408	.198	20
21	.156		.185	.244			.293	.102	21
22	.164		.167	.203				.054	22
23	.160			.199			.198	.034	23
24	.155		.151	.186			.174	.011	24
25	.153		.143	.163			.156	.029	25
26	.081		.108	.127			.117	-.014	26

$\alpha = 6$ $\delta = 0$

1	-.078		-.071	-.061			-.063	-.058	1
2	-.064		-.066	-.056			-.055	-.021	2
3	-.052		-.066	-.055			-.059	-.007	3
4	-.071		-.085	-.078			-.090	-.040	4
5	-.149		-.163	-.140			-.141	-.089	5
6	-.146		-.164	-.164			-.154	-.149	6
7	-.140		-.166	-.164			-.156	-.197	7
8	-.156		-.153	-.170			-.169	-.228	8
9	-.155		-.171	-.186			-.160	-.218	9
10	-.178		-.189	-.204			-.176	-.231	10
11	-.165		-.213	-.213			-.176	-.248	11
12	-.190		-.208	-.216			-.200	-.233	12
13	-.201		-.218	-.241			-.207	-.259	13
14	-.202		-.222	-.235			-.197	-.243	14
15	-.214		-.218	-.235			-.192	-.207	15
16	-.209		-.222	-.235			-.188	-.231	16
17	.343		.503	.506			.534	.401	17
18	.299		.439	.504			.536	.357	18
19	.291		.386	.453			.500	.279	19
20	.269		.308	.359			.398	.187	20
21	.150		.177	.231			.283	.083	21
22	.157		.159	.197				.045	22
23	.154			.186			.189	.013	23
24	.151		.146	.178			.165	-.008	24
25	.147		.134	.155			.143	.018	25
26	.074		.098	.114			.108	-.032	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 6$ $\delta = 10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.062		-.049	-.041			-.044	-.040	1
2	-.039		-.043	-.035			-.035	-.005	2
3	-.031		-.045	-.036			-.038	.014	3
4	-.054		-.068	-.058			-.068	-.012	4
5	-.130		-.139	-.118			-.116	-.063	5
6	-.123		-.143	-.141			-.133	-.121	6
7	-.119		-.148	-.144			-.138	-.170	7
8	-.136		-.134	-.151			-.147	-.201	8
9	-.126		-.154	-.166			-.138	-.194	9
10	-.158		-.170	-.188			-.152	-.202	10
11	-.141		-.192	-.192			-.153	-.216	11
12	-.296		-.313	-.319			-.296	-.318	12
13	-.322		-.329	-.348			-.325	-.274	13
14	-.313		-.341	-.348			-.323	-.300	14
15	-.337		-.343	-.348			-.322	-.332	15
16	-.190		-.206	-.240			-.296	-.332	16
17	.358		.514	.512			.536	.411	17
18	.315		.450	.513			.538	.365	18
19	.309		.396	.463			.505	.279	19
20	.288		.320	.369			.405	.198	20
21	.168		.190	.243			.292	.102	21
22	.173		.174	.206				.055	22
23	.169			.197			.196	.022	23
24	.169		.158	.185			.173	.002	24
25	.165		.147	.168			.154	.028	25
26	.094		.111	.126			.115	-.011	26

$\alpha = 12$ $\delta = -25$

1	-.225		-.244	-.269			-.284	-.283	1
2	-.181		-.194	-.222			-.241	-.186	2
3	-.167		-.218	-.211			-.223	-.187	3
4	-.178		-.226	-.228			-.243	-.253	4
5	-.241		-.289	-.272			-.280	-.305	5
6	-.237		-.288	-.288			-.288	-.390	6
7	-.203		-.289	-.293			-.296	-.409	7
8	-.248		-.272	-.292			-.302	-.404	8
9	-.237		-.269	-.258			-.279	-.406	9
10	-.120		-.061	-.102			-.079	-.408	10
11	-.026		-.044	-.079			-.048	-.362	11
12	.015		-.023	-.054			-.047	-.228	12
13	.073		.010	-.045			-.008	-.166	13
14	.202		.142	.055			.154	-.199	14
15	.227		.205	.118			.231	-.261	15
16	.247		.218	.126			.241	-.308	16
17	.628		.891	.964			.989	.733	17
18	.550		.738	.828			.878	.559	18
19	.555		.658	.726			.764	.443	19
20	.504		.519	.556			.598	.325	20
21	.350		.350	.414			.449	.188	21
22	.361		.355	.388				.129	22
23	.344			.379			.353	.109	23
24	.346		.348	.368			.324	.080	24
25	.339		.337	.348			.306	.105	25
26	.251		.281	.297			.267	.043	26

TABLE X.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.208		-.223	-.248			-.269	-.267	1
2	-.168		-.189	-.205			-.224	-.171	2
3	-.149		-.199	-.194			-.204	-.166	3
4	-.161		-.221	-.213			-.221	-.226	4
5	-.229		-.271	-.257			-.258	-.280	5
6	-.224		-.272	-.271			-.269	-.358	6
7	-.197		-.270	-.273			-.277	-.379	7
8	-.234		-.256	-.277			-.281	-.383	8
9	-.222		-.256	-.269			-.266	-.388	9
10	-.247		-.253	-.290			-.238	-.388	10
11	-.069		-.086	-.142			-.069	-.357	11
12	-.003		-.037	-.083			-.054	-.222	12
13	.045		.003	-.059			-.006	-.205	13
14	.091		.072	.002			.077	-.235	14
15	.103		.099	.021			.105	-.286	15
16	.114		.106	.032			.114	-.291	16
17	.634		.899	.971			.994	.740	17
18	.564		.745	.834			.887	.572	18
19	.563		.665	.733			.768	.454	19
20	.514		.526	.561			.607	.343	20
21	.364		.364	.422			.463	.201	21
22	.373		.362	.397				.145	22
23	.358			.393			.364	.119	23
24	.358		.358	.377			.334	.092	24
25	.351		.343	.361			.311	.119	25
26	.264		.289	.308			.276	.064	26

α=12 δ=-10

1	-.214		-.233	-.253			-.268	-.273	1
2	-.177		-.205	-.213			-.226	-.175	2
3	-.158		-.206	-.198			-.204	-.171	3
4	-.173		-.221	-.219			-.226	-.230	4
5	-.238		-.277	-.263			-.263	-.285	5
6	-.233		-.280	-.282			-.276	-.363	6
7	-.220		-.282	-.278			-.280	-.383	7
8	-.243		-.264	-.281			-.285	-.393	8
9	-.231		-.268	-.290			-.269	-.389	9
10	-.257		-.273	-.307			-.270	-.391	10
11	-.231		-.284	-.311			-.223	-.383	11
12	-.113		-.146	-.195			-.152	-.289	12
13	-.113		-.136	-.189			-.136	-.295	13
14	-.118		-.131	-.177			-.118	-.334	14
15	-.114		-.123	-.175			-.109	-.345	15
16	-.112		-.123	-.175			-.102	-.317	16
17	.629		.893	.966			.991	.736	17
18	.552		.739	.831			.881	.571	18
19	.556		.659	.729			.764	.443	19
20	.508		.521	.561			.606	.330	20
21	.356		.357	.418			.456	.201	21
22	.366		.358	.390				.141	22
23	.349			.386			.359	.117	23
24	.350		.351	.370			.328	.084	24
25	.338		.338	.354			.311	.108	25
26	.254		.285	.301			.272	.058	26

TABLE X.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 1.61$; $R = 5.6 \times 10^6$.

$\alpha = 12$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.229		-.243	-.261			-.273	-.276	1
2	-.189		-.217	-.218			-.231	-.179	2
3	-.171		-.220	-.206			-.210	-.179	3
4	-.184		-.232	-.226			-.229	-.238	4
5	-.249		-.289	-.270			-.266	-.293	5
6	-.246		-.290	-.289			-.279	-.378	6
7	-.243		-.291	-.286			-.283	-.399	7
8	-.253		-.273	-.292			-.289	-.408	8
9	-.245		-.272	-.300			-.274	-.399	9
10	-.272		-.281	-.317			-.273	-.412	10
11	-.264		-.303	-.324			-.252	-.389	11
12	-.244		-.284	-.309			-.273	-.345	12
13	-.270		-.284	-.328			-.286	-.356	13
14	-.279		-.294	-.324			-.273	-.369	14
15	-.280		-.293	-.325			-.276	-.370	15
16	-.199		-.264	-.322			-.274	-.339	16
17	.618		.884	.961			.983	.724	17
18	.540		.730	.824			.874	.556	18
19	.544		.650	.723			.759	.435	19
20	.498		.513	.552			.594	.321	20
21	.344		.348	.411			.447	.183	21
22	.354		.351	.381				.127	22
23	.337			.379			.353	.103	23
24	.337		.344	.366			.322	.071	24
25	.333		.331	.347			.304	.101	25
26	.241		.276	.293			.267	.034	26

TABLE XI

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = -15$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.583		.806	.860			.871	.783	1
2	.509		.710	.800			.827	.615	2
3	.526		.647	.728			.769	.513	3
4	.519		.564	.614			.649	.379	4
5	.397		.419	.482			.534	.288	5
6	.390		.394	.442			.477	.188	6
7	.380		.392	.422			.443	.167	7
8	.373		.398	.418			.425		8
9	.362		.361	.383			.361	.144	9
10	.313		.318	.361			.317	.150	10
11	.354			.331			.302	.127	11
12	.229	.228	.307	.286	.302	.298	.318	.090	12
13	.230	.243	.255	.255	.293	.288	.266	.097	13
14	.227	.237	.243	.266	.265	.262	.251	.064	14
15	.224	.227	.253	.266	.248	.247	.247	.066	15
16	.219	.222	.243	.270	.246	.238	.227	.045	16
17	- .169	-	.168	- .169		-	.163	- .140	17
18	- .137	-	.173	- .171		-	.153	- .107	18
19	- .142	-	.175	- .169		-	.168	- .137	19
20	- .153	-	.180	- .182		-	.177	- .171	20
21	- .194	-	.214	- .207		-	.204	- .210	21
22	- .182	-	.221	- .215				- .250	22
23	- .196			- .216		-	.211	- .261	23
24	- .192	-	.221	- .218		-	.210	- .275	24
25	- .191	-	.215	- .217		-	.212	- .255	25
26	- .199	-	.222	- .203		-	.216	- .252	26

$\alpha = -12$ $\delta = -30$

1	.474		.609	.610			.608	.549	1
2	.406		.564	.564			.556	.432	2
3	.396		.520	.571			.576	.376	3
4	.403		.449	.508			.512	.294	4
5	.288		.320	.387			.426	.213	5
6	.287		.297	.344			.388	.144	6
7	.279		.277	.378			.373	.112	7
8	.270		.289	.719			.351		8
9	.268		.631	.731			.312	.099	9
10	.213		.629	.760			.297	.103	10
11	.246			.754			.334	.083	11
12	.153	.404	.603	.784	.649	.454	.354	.048	12
13	.157	.397	.673	.773	.647	.500	.339	.080	13
14	.169	.154	1.029	1.021	.925	.253	.323	.017	14
15	.232	.043	1.043	1.227	1.003	.139	.293	.023	15
16	.289	.019	.885	1.104	.887	.081	.278	.004	16
17	- .141	-	.143	- .130		-	.121	- .115	17
18	- .117	-	.140	- .133		-	.120	- .079	18
19	- .117	-	.143	- .135		-	.126	- .092	19
20	- .126	-	.144	- .148		-	.141	- .118	20
21	- .175	-	.188	- .174		-	.169	- .160	21
22	- .157	-	.194	- .188				- .228	22
23	- .166			- .189		-	.179	- .241	23
24	- .172	-	.198	- .185		-	.180	- .261	24
25	- .170	-	.197	- .196		-	.187	- .242	25
26	- .188	-	.210	- .197		-	.189	- .242	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.470		.619	.619			.617	.560	1
2	.405		.563	.561			.556	.437	2
3	.398		.524	.574			.575	.383	3
4	.408		.452	.509			.510	.294	4
5	.286		.314	.393			.432	.220	5
6	.296		.299	.349			.390	.150	6
7	.281		.280	.327			.376	.121	7
8	.272		.297	.320			.353		8
9	.266		.270	.350			.314	.103	9
10	.211		.250	.578			.263	.108	10
11	.251			.658			.252	.090	11
12	.164	.340	.620	.685	.622	.440	.255	.052	12
13	.164	.302	.738	.768	.681	.354	.200	.059	13
14	.159	.209	.741	.931	.718	.293	.179	.020	14
15	.153	.038	.685	.941	.672	.132	.214	.025	15
16	.168	.041	.634	.853	.614	.069	.238	.008	16
17	-.142		-.134	-.129			-.121	-.111	17
18	-.116		-.145	-.132			-.124	-.071	18
19	-.116		-.135	-.131			-.121	-.085	19
20	-.121		-.143	-.144			-.143	-.111	20
21	-.164		-.182	-.176			-.173	-.153	21
22	-.176		-.190	-.182				-.220	22
23	-.162			-.186			-.177	-.236	23
24	-.167		-.192	-.183			-.180	-.260	24
25	-.170		-.192	-.199			-.192	-.237	25
26	-.195		-.209	-.197			-.192	-.236	26

α =-12 δ =-10

1	.473		.616	.617			.610	.555	1
2	.408		.564	.569			.562	.430	2
3	.396		.533	.578			.579	.377	3
4	.404		.457	.515			.508	.293	4
5	.287		.317	.396			.435	.216	5
6	.296		.302	.352			.391	.143	6
7	.284		.289	.328			.376	.115	7
8	.271		.294	.321			.356		8
9	.265		.271	.291			.311	.101	9
10	.217		.231	.273			.263	.106	10
11	.252			.258			.250	.081	11
12	.154	.210	.503	.447	.428	.276	.248	.053	12
13	.159	.244	.463	.503	.472	.292	.197	.060	13
14	.153	.239	.400	.517	.407	.274	.169	.020	14
15	.146	.113	.373	.522	.372	.186	.173	.025	15
16	.145	.041	.344	.504	.334	.113	.164	.008	16
17	-.137		-.136	-.137			-.119	-.117	17
18	-.110		-.128	-.131			-.126	-.078	18
19	-.117		-.132	-.130			-.129	-.092	19
20	-.127		-.146	-.140			-.139	-.120	20
21	-.166		-.184	-.173			-.165	-.162	21
22	-.161		-.188	-.187				-.228	22
23	-.166			-.189			-.173	-.243	23
24	-.168		-.189	-.182			-.183	-.262	24
25	-.171		-.186	-.194			-.185	-.248	25
26	-.194		-.207	-.200			-.188	-.246	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.470		.619	.626			.616	.556	1
2	.402		.564	.566			.562	.435	2
3	.397		.533	.580			.583	.384	3
4	.404		.464	.517			.515	.292	4
5	.287		.328	.402			.440	.220	5
6	.293		.308	.355			.396	.153	6
7	.284		.299	.326			.381	.120	7
8	.270		.303	.325			.359		8
9	.267		.277	.295			.320	.104	9
10	.210		.250	.276			.270	.111	10
11	.252			.245			.254	.087	11
12	.163	.155	.215	.204	.220	.223	.253	.050	12
13	.163	.162	.165	.169	.215	.224	.201	.056	13
14	.159	.162	.160	.176	.201	.201	.172	.018	14
15	.154	.154	.162	.168	.186	.191	.177	.022	15
16	.150	.146	.160	.177	.178	.174	.159	.004	16
17	-.138		-.127	-.136			-.118	-.111	17
18	-.119		-.133	-.129			-.114	-.076	18
19	-.115		-.132	-.132			-.117	-.088	19
20	-.119		-.140	-.142			-.136	-.118	20
21	-.156		-.175	-.172			-.159	-.160	21
22	-.159		-.184	-.179				-.225	22
23	-.157			-.185			-.175	-.241	23
24	-.169		-.184	-.183			-.171	-.258	24
25	-.163		-.187	-.194			-.180	-.241	25
26	-.183		-.200	-.195			-.184	-.239	26

α=-12 δ=10

1	.476		.616	.627			.615	.559	1
2	.408		.563	.570			.564	.434	2
3	.399		.530	.577			.583	.383	3
4	.408		.452	.514			.522	.290	4
5	.284		.325	.396			.438	.220	5
6	.296		.297	.354			.397	.145	6
7	.283		.290	.326			.378	.118	7
8	.272		.297	.320			.353		8
9	.264		.274	.291			.316	.101	9
10	.219		.236	.271			.272	.104	10
11	.251			.250			.253	.088	11
12	.160	.151	-.001	.013	.038	.215	.251	.050	12
13	.160	.111	-.038	-.036	.027	.199	.199	.056	13
14	.154	.080	-.010	-.029	.034	.127	.171	.018	14
15	.151	.055	-.017	-.042	-.013	.108	.173	.022	15
16	.145	.036	-.051	-.038	-.066	.084	.154	.005	16
17	-.143		-.133	-.141			-.121	-.120	17
18	-.113		-.141	-.136			-.127	-.076	18
19	-.115		-.134	-.132			-.127	-.093	19
20	-.119		-.145	-.147			-.142	-.121	20
21	-.163		-.186	-.181			-.168	-.164	21
22	-.156		-.191	-.178				-.229	22
23	-.163			-.190			-.179	-.244	23
24	-.176		-.191	-.183			-.181	-.265	24
25	-.168		-.189	-.195			-.187	-.246	25
26	-.183		-.206	-.192			-.190	-.243	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.474		.614	.624			.607	.558	1
2	.405		.568	.569			.562	.430	2
3	.395		.528	.573			.579	.382	3
4	.407		.455	.515			.516	.292	4
5	.284		.320	.396			.434	.219	5
6	.295		.301	.356			.390	.149	6
7	.277		.289	.329			.375	.118	7
8	.266		.297	.321			.353		8
9	.265		.272	.289			.309	.102	9
10	.212		.237	.270			.261	.108	10
11	.250			.250			.248	.087	11
12	.159	.160	- .132	- .112	- .109	.228	.255	.051	12
13	.160	.102	- .167	- .165	- .111	.191	.197	.059	13
14	.154	.061	- .149	- .163	- .121	.103	.174	.014	14
15	.150	.029	- .159	- .167	- .158	.075	.174	.018	15
16	.144	.015	- .176	- .173	- .163	.059	.158	.006	16
17	- .140		- .135	- .139		-	.134	- .116	17
18	- .120		- .142	- .136		-	.132	- .078	18
19	- .116		- .139	- .136		-	.133	- .092	19
20	- .130		- .143	- .145		-	.142	- .125	20
21	- .170		- .185	- .180		-	.175	- .160	21
22	- .157		- .189	- .186				- .229	22
23	- .166			- .192		-	.183	- .246	23
24	- .175		- .192	- .188		-	.185	- .262	24
25	- .171		- .191	- .198		-	.190	- .244	25
26	- .191		- .202	- .204		-	.195	- .244	26

α=-12 δ=30

1	.477		.619	.623			.613	.560	1
2	.407		.570	.572			.563	.424	2
3	.397		.533	.583			.580	.377	3
4	.403		.460	.520			.515	.289	4
5	.290		.331	.405			.433	.218	5
6	.282		.306	.352			.396	.149	6
7	.279		.293	.331			.374	.112	7
8	.266		.300	.322			.351		8
9	.269		.277	.294			.312	.099	9
10	.224		.240	.267			.266	.104	10
11	.249			.250			.249	.081	11
12	.154	.168	- .218	- .210	- .196	.224	.251	.052	12
13	.158	.099	- .243	- .241	- .199	.191	.195	.057	13
14	.150	.061	- .236	- .243	- .210	.104	.172	.020	14
15	.148	.025	- .238	- .247	- .230	.074	.173	.024	15
16	.143	.013	- .248	- .238	- .229	.059	.154	.006	16
17	- .139		- .134	- .139		-	.130	- .120	17
18	- .120		- .141	- .131		-	.129	- .084	18
19	- .117		- .134	- .126		-	.130	- .098	19
20	- .124		- .141	- .139		-	.145	- .125	20
21	- .168		- .183	- .174		-	.176	- .168	21
22	- .158		- .191	- .185				- .233	22
23	- .166			- .188		-	.182	- .250	23
24	- .169		- .189	- .185		-	.190	- .269	24
25	- .168		- .196	- .195		-	.189	- .250	25
26	- .184		- .049	- .054		-	.200	- .246	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-9 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.367		.396	.414			.408	.393	1
2	.292		.409	.409			.411	.307	2
3	.301		.398	.403			.412	.269	3
4	.303		.352	.376			.365	.204	4
5	.201		.224	.288			.295	.140	5
6	.185		.205	.254			.261	.083	6
7	.191		.199	.239			.254	.051	7
8	.179		.196	.228			.242		8
9	.186		.177	.201			.216	.045	9
10	.136		.152	.183			.172	.046	10
11	.167			.161			.169	.031	11
12	.089	.084	.137	.135	.148	.144	.177	- .009	12
13	.092	.085	.092	.098	.139	.148	.129	.005	13
14	.085	.083	.084	.102	.131	.127	.108	- .031	14
15	.085	.075	.092	.095	.115	.118	.107	- .028	15
16	.076	.078	.087	.103	.108	.109	.095	- .036	16
17	- .089	-	- .089	- .087		-	.082	- .067	17
18	- .066	-	- .090	- .086		-	.074	- .036	18
19	- .078	-	- .087	- .081		-	.081	- .037	19
20	- .087	-	- .095	- .101		-	.103	- .066	20
21	- .144	-	- .146	- .130		-	.131	- .085	21
22	- .124	-	- .152	- .146			-	.129	22
23	- .132	-		- .149		-	.142	- .167	23
24	- .136	-	- .152	- .151		-	.146	- .195	24
25	- .130	-	- .157	- .153		-	.151	- .168	25
26	- .154	-	- .165	- .130		-	.163	- .188	26

α=-6 δ=-30

1	.270		.275	.284			.286	.266	1
2	.203		.293	.284			.288	.201	2
3	.214		.282	.286			.292	.182	3
4	.222		.258	.257			.248	.132	4
5	.117		.152	.187			.190	.081	5
6	.121		.125	.157			.161	.038	6
7	.117		.118	.156			.162	.008	7
8	.106		.126	.307			.147		8
9	.104		.304	.502			.138	.001	9
10	.067		.428	.525			.096	.003	10
11	.091		.428	.522			.098	- .009	11
12	.025	.205	.409	.549	.438	.248	.101	- .037	12
13	.031	.214	.484	.538	.440	.264	.061	- .023	13
14	.029	.001	.812	.794	.743	.099	.125	- .056	14
15	.032	- .087	.844	1.015	.819	- .008	.120	- .055	15
16	.064	- .103	.764	.974	.752	- .051	.098	- .053	16
17	- .047	-	- .029	- .027		-	.026	- .024	17
18	- .013	-	- .034	- .032		-	.022	.000	18
19	- .027	-	- .025	- .027		-	.030	- .004	19
20	- .041	-	- .049	- .044		-	.044	- .027	20
21	- .097	-	- .099	- .082		-	.081	- .045	21
22	- .090	-	- .104	- .101			-	.051	22
23	- .095	-		- .100		-	.095	- .070	23
24	- .097	-	- .104	- .106		-	.102	- .106	24
25	- .096	-	- .115	- .110		-	.109	- .083	25
26	- .122	-	- .129	- .117		-	.117	- .116	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.276		.277	.292			.286	.274	1
2	.214		.300	.284			.289	.205	2
3	.231		.290	.288			.290	.186	3
4	.232		.264	.266			.251	.137	4
5	.130		.151	.187			.189	.085	5
6	.133		.128	.167			.167	.039	6
7	.123		.119	.162			.157	.008	7
8	.113		.125	.157			.148		8
9	.119		.107	.165			.137	.006	9
10	.075		.100	.134			.096	.004	10
11	.096		.100	.401			.095	-.005	11
12	.027	.145	.412	.448	.387	.224	.099	-.038	12
13	.033	.104	.546	.570	.480	.159	.052	-.023	13
14	.031	.056	.537	.689	.519	.112	.042	-.055	14
15	.020	-.079	.493	.707	.474	-.013	.047	-.053	15
16	.018	-.098	.456	.677	.432	-.053	.048	-.052	16
17	-.025		-.019	-.029			-.024	-.022	17
18	-.016		-.035	-.023			-.022	.001	18
19	-.026		-.023	-.020			-.026	-.003	19
20	-.041		-.041	-.036			-.048	-.027	20
21	-.096		-.092	-.084			-.088	-.042	21
22	-.091		-.099	-.098				-.051	22
23	-.095			-.102			-.097	-.071	23
24	-.095		-.100	-.103			-.106	-.108	24
25	-.095		-.111	-.110			-.108	-.084	25
26	-.120		-.125	-.126			-.120	-.118	26

α=-6 δ=-10

1	.258		.272	.281			.283	.275	1
2	.201		.282	.274			.292	.207	2
3	.219		.284	.282			.298	.185	3
4	.216		.256	.256			.256	.136	4
5	.110		.142	.182			.197	.080	5
6	.110		.117	.157			.165	.041	6
7	.110		.110	.152			.166	.004	7
8	.106		.118	.153			.148		8
9	.103		.098	.131			.139	.006	9
10	.066		.080	.115			.097	.003	10
11	.090		.080	.099			.107	-.008	11
12	.027	.052	.295	.250	.216	.084	.099	-.034	12
13	.032	.083	.280	.299	.281	.122	.053	-.022	13
14	.029	.079	.228	.309	.242	.109	.036	-.051	14
15	.015	-.009	.206	.304	.216	.057	.041	-.050	15
16	.017	-.065	.186	.311	.182	-.004	.033	-.050	16
17	-.043		-.039	-.035			-.030	-.024	17
18	-.028		-.039	-.028			-.021	.001	18
19	-.031		-.032	-.023			-.023	-.005	19
20	-.048		-.053	-.048			-.039	-.028	20
21	-.099		-.103	-.081			-.080	-.046	21
22	-.095		-.112	-.095				-.051	22
23	-.096			-.102			-.095	-.071	23
24	-.098		-.114	-.098			-.106	-.109	24
25	-.102		-.119	-.111			-.113	-.085	25
26	-.127		-.139	-.122			-.128	-.125	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.272		.275	.294			.272	.267	1
2	.218		.288	.277			.289	.209	2
3	.226		.284	.289			.289	.185	3
4	.226		.266	.265			.252	.132	4
5	.123		.154	.192			.195	.076	5
6	.130		.132	.155			.163	.037	6
7	.125		.122	.155			.158	.006	7
8	.110		.131	.151			.147		8
9	.118		.104	.130			.136	.003	9
10	.072		.089	.113			.099	.003	10
11	.094			.096			.106	- .009	11
12	.025	.031	.061	.065	.071	.069	.099	- .029	12
13	.032	.031	.024	.031	.071	.078	.052	- .022	13
14	.029	.031	.019	.034	.064	.062	.037	- .047	14
15	.018	.023	.023	.031	.056	.059	.039	- .048	15
16	.013	.023	.022	.029	.050	.052	.028	- .047	16
17	- .032	-	- .031	- .037		-	.025	- .027	17
18	- .029	-	- .041	- .033		-	.025	- .001	18
19	- .032	-	- .029	- .027		-	.027	- .008	19
20	- .042	-	- .049	- .043		-	.047	- .032	20
21	- .081	-	- .095	- .086		-	.086	- .046	21
22	- .088	-	- .109	- .105				- .056	22
23	- .086			- .100		-	.099	- .076	23
24	- .095	-	- .114	- .105		-	.106	- .116	24
25	- .094	-	- .112	- .117		-	.103	- .088	25
26	- .120	-	- .133	- .124		-	.123	- .125	26

α=-6 δ=10

1	.270		.283	.293			.279	.281	1
2	.215		.300	.280			.290	.213	2
3	.225		.294	.294			.291	.195	3
4	.234		.265	.261			.247	.146	4
5	.123		.149	.191			.194	.092	5
6	.130		.133	.164			.161	.050	6
7	.125		.117	.154			.155	.018	7
8	.117		.134	.153			.146		8
9	.117		.112	.129			.135	.011	9
10	.075		.084	.115			.096	.010	10
11	.098			.093			.096	.001	11
12	.033	.029	- .085	- .065	- .059	.074	.104	- .033	12
13	.042	- .004	- .117	- .117	- .076	.062	.059	- .022	13
14	.038	- .027	- .107	- .116	- .071	.009	.043	- .050	14
15	.027	- .046	- .101	- .118	- .089	.000	.047	- .047	15
16	.023	- .053	- .108	- .123	- .101	- .011	.037	- .048	16
17	- .026	-	- .030	- .041		-	.026	- .019	17
18	- .017	-	- .041	- .037		-	.032	.008	18
19	- .022	-	- .029	- .028		-	.037	.003	19
20	- .036	-	- .048	- .045		-	.048	- .019	20
21	- .095	-	- .098	- .083		-	.087	- .038	21
22	- .085	-	- .108	- .103				- .046	22
23	- .093			- .105		-	.102	- .066	23
24	- .091	-	- .107	- .107		-	.108	- .106	24
25	- .093	-	- .113	- .118		-	.110	- .081	25
26	- .118	-	- .132	- .131		-	.121	- .116	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.269		.274	.294			.287	.281	1
2	.201		.292	.280			.297	.216	2
3	.220		.294	.294			.295	.193	3
4	.224		.256	.264			.255	.141	4
5	.122		.155	.198			.199	.089	5
6	.122		.131	.162			.166	.047	6
7	.117		.115	.157			.158	.013	7
8	.106		.130	.153			.149		8
9	.109		.110	.129			.138	.013	9
10	.065		.089	.114			.099	.009	10
11	.092			.094			.104	- .005	11
12	.032	.036	- .183	- .167	- .164	.074	.103	- .031	12
13	.038	- .008	- .211	- .210	- .179	.062	.059	- .018	13
14	.033	- .038	- .209	- .215	- .173	- .001	.047	- .048	14
15	.023	- .061	- .199	- .218	- .188	- .020	.048	- .047	15
16	.022	- .066	- .209	- .218	- .209	- .028	.038	- .047	16
17	- .043		- .038	- .039			- .026	- .023	17
18	- .024		- .031	- .027			- .027	.003	18
19	- .029		- .027	- .037			- .028	- .001	19
20	- .045		- .047	- .049			- .039	- .025	20
21	- .101		- .103	- .086			- .082	- .041	21
22	- .086		- .106	- .110				- .048	22
23	- .097			- .100			- .094	- .071	23
24	- .102		- .110	- .111			- .101	- .109	24
25	- .098		- .113	- .116			- .113	- .085	25
26	- .131		- .129	- .135			- .123	- .121	26

α=-6 δ=30

1	.275		.282	.294			.283	.280	1
2	.214		.304	.283			.296	.215	2
3	.229		.298	.299			.298	.193	3
4	.225		.266	.265			.259	.145	4
5	.132		.157	.197			.192	.092	5
6	.127		.128	.167			.167	.043	6
7	.121		.131	.159			.162	.008	7
8	.114		.135	.153			.150		8
9	.116		.116	.134			.138	.011	9
10	.072		.077	.116			.104	.010	10
11	.092			.089			.101	- .003	11
12	.033	.041	- .238	- .227	- .225	.074	.108	- .027	12
13	.041	- .011	- .258	- .258	- .237	.060	.061	- .019	13
14	.037	- .039	- .256	- .260	- .229	- .006	.046	- .048	14
15	.028	- .065	- .251	- .257	- .252	- .023	.048	- .046	15
16	.023	- .067	- .233	- .237	- .264	- .032	.038	- .046	16
17	- .031		- .031	- .033			- .031	- .023	17
18	- .021		- .039	- .034			- .024	.005	18
19	- .025		- .028	- .027			- .032	.001	19
20	- .041		- .042	- .048			- .052	- .024	20
21	- .096		- .098	- .087			- .083	- .042	21
22	- .084		- .104	- .105				- .050	22
23	- .088			- .109			- .101	- .073	23
24	- .093		- .107	- .109			- .116	- .111	24
25	- .091		- .113	- .063			- .110	- .084	25
26	- .119		.078	.108			- .126	- .117	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-3 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.189		.191	.201			.192	.192	1
2	.140		.198	.197			.199	.144	2
3	.159		.203	.195			.198	.135	3
4	.164		.184	.178			.167	.093	4
5	.074		.098	.114			.118	.046	5
6	.064		.072	.084			.087	.023	6
7	.065		.061	.083			.084	.000	7
8	.061		.064	.082			.077		8
9	.058		.044	.061			.071	.000	9
10	.026		.035	.053			.030 -	.003	10
11	.038		.034	.035			.051 -	.014	11
12 -	.014	- .020	.011	.018	- .001	.001	.043 -	.036	12
13 -	.010	- .025	- .020	- .017	- .005	.009	.003 -	.029	13
14 -	.009	- .027	- .029	- .013	- .001	- .008	- .010 -	.057	14
15 -	.024	- .032	- .024	- .014	- .008	- .011	- .009 -	.051	15
16 -	.027	- .031	- .024	- .015	- .018	- .010	- .017 -	.052	16
17	.038		.035	.028			.036	.034	17
18	.039		.034	.029			.048	.048	18
19	.032		.038	.033			.032	.038	19
20	.014		.017	.015			.011	.009	20
21 -	.050		- .043	- .030			- .031 -	.010	21
22 -	.048		- .056	- .047			-	.009	22
23 -	.046		-	- .057			- .045 -	.010	23
24 -	.053		- .056	- .059			- .053 -	.028	24
25 -	.050		- .064	- .061			- .060 -	.011	25
26 -	.080		- .084	- .070			- .078 -	.029	26

α=0 δ=-30

1	.098		.100	.106			.105	.099	1
2	.067		.096	.104			.106	.070	2
3	.075		.109	.102			.107	.078	3
4	.079		.096	.087			.078	.052	4
5	.006		.015	.026			.042	.017	5
6	.004		.009	.005			.011	.006	6
7 -	.002		- .006	.009			.010 -	.008	7
8 -	.007		- .005	.002			- .003		8
9 -	.008		- .007	.259			- .006 -	.008	9
10 -	.034		.245	.300			- .025 -	.009	10
11 -	.032		.245	.305			- .010 -	.020	11
12 -	.064	.048	.240	.322	.235	.094	- .028 -	.025	12
13 -	.071	.070	.319	.339	.257	.061	- .062 -	.027	13
14 -	.064	- .097	.610	.610	.531 -	.034	- .067 -	.033	14
15 -	.075	- .156	.627	.788	.577 -	.112	- .032 -	.031	15
16 -	.065	- .154	.574	.778	.543 -	.131	- .037 -	.032	16
17	.107		.112	.107			.111	.097	17
18	.087		.112	.100			.109	.097	18
19	.088		.113	.106			.105	.074	19
20	.065		.095	.090			.084	.042	20
21	.001		.021	.037			.034	.011	21
22	.008		.004	.010				.005	22
23	.005			.009			.017	.003	23
24 -	.003		.003	.012			.012 -	.010	24
25 -	.004		- .012	- .008			.004	.004	25
26 -	.041		- .031	- .015			- .010 -	.003	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=0 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.116		.107	.120			.103	.103	1
2	.083		.106	.110			.105	.078	2
3	.094		.117	.101			.101	.084	3
4	.098		.104	.089			.072	.057	4
5	.025		.013	.025			.038	.019	5
6	.023		.005	.004			.006	.013	6
7	.018		-.007	-.009			.003	-.003	7
8	.009		.004	.002			-.010		8
9	.011		-.010	.032			-.010	-.003	9
10	-.021		-.013	.002			-.034	.000	10
11	-.012		-.013	.141			-.016	-.010	11
12	-.055	.008	.234	.243	.179	.053	-.031	-.018	12
13	-.056	-.014	.348	.357	.283	.019	-.061	-.028	13
14	-.055	-.046	.347	.441	.311	-.023	-.069	-.032	14
15	-.072	-.146	.309	.454	.282	-.099	-.065	-.024	15
16	-.072	-.136	.281	.449	.255	-.122	-.070	-.025	16
17	.118		.111	.099			.104	.102	17
18	.096		.108	.108			.104	.107	18
19	.096		.109	.106			.101	.081	19
20	.076		.094	.084			.080	.047	20
21	.017		.019	.024			.025	.019	21
22	.016		.005	.008				.014	22
23	.017			.011			.013	.011	23
24	.009		.005	-.001			-.004	.000	24
25	.010		-.007	-.013			-.011	.015	25
26	-.030		-.033	-.025			-.023	.006	26

α=0 δ=-10

1	.112		.105	.114			.103	.099	1
2	.089		.102	.107			.099	.076	2
3	.090		.109	.104			.101	.075	3
4	.086		.100	.090			.071	.057	4
5	.005		.018	.026			.032	.017	5
6	.002		.010	.010			.010	.009	6
7	.001		-.005	.005			.003	-.006	7
8	.001		.002	.003			-.009		8
9	.001		-.012	-.014			-.009	-.008	9
10	-.020		-.030	-.019			-.032	-.005	10
11	-.022		-.029	-.037			-.016	-.015	11
12	-.057	-.058	.117	.072	.036	-.051	-.031	-.024	12
13	-.062	-.038	.131	.131	.098	-.028	-.061	-.032	13
14	-.057	-.033	.092	.146	.079	-.034	-.071	-.037	14
15	-.076	-.094	.075	.145	.064	-.060	-.071	-.033	15
16	-.076	-.105	.060	.150	.042	-.083	-.076	-.033	16
17	.117		.107	.093			.106	.099	17
18	.094		.111	.104			.105	.097	18
19	.080		.113	.102			.102	.074	19
20	.072		.097	.078			.079	.043	20
21	.003		.019	.029			.024	.014	21
22	.004		.001	.011				.006	22
23	.004			.004			.010	.005	23
24	.003		.001	.006			.001	-.008	24
25	.002		-.016	-.011			-.007	.010	25
26	-.030		-.033	-.025			-.021	-.001	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.114		.105	.114			.099	.098	1
2	.078		.103	.111			.101	.072	2
3	.085		.115	.106			.103	.078	3
4	.094		.099	.092			.074	.053	4
5	.021		.021	.033			.040	.017	5
6	.014		.009	.005			.012	.006	6
7	.004		-.003	-.001			.011	-.010	7
8	-.003		-.004	.006			-.004		8
9	-.003		-.014	-.010			-.005	-.010	9
10	-.021		-.025	-.019			-.031	-.008	10
11	-.016		-.026	-.027			-.013	-.018	11
12	-.064	-.074	-.051	-.038	-.052	-.056	-.032	-.032	12
13	-.064	-.076	-.062	-.069	-.062	-.050	-.064	-.031	13
14	-.061	-.072	-.072	-.066	-.062	-.061	-.075	-.037	14
15	-.076	-.081	-.072	-.065	-.069	-.069	-.070	-.036	15
16	-.080	-.078	-.074	-.067	-.067	-.071	-.076	-.037	16
17	.109		.116	.089			.096	.094	17
18	.098		.111	.097			.103	.097	18
19	.087		.109	.097			.103	.072	19
20	.071		.085	.081			.078	.038	20
21	.006		.022	.027			.028	.014	21
22	.011		.004	.009				.006	22
23	.016			.006			.014	.004	23
24	.011		.004	.002			.001	-.009	24
25	-.001		-.006	-.007			-.005	.006	25
26	-.034		-.025	-.021			-.022	-.005	26

$\alpha = 0$ $\delta = 10$

1	.104		.106	.120			.110	.098	1
2	.072		.105	.110			.106	.071	2
3	.089		.110	.103			.114	.072	3
4	.087		.098	.096			.084	.044	4
5	.009		.017	.034			.043	.010	5
6	.017		.002	.000			.019	.004	6
7	.010		-.011	.008			.017	-.013	7
8	.004		-.007	.006			.003		8
9	.000		-.022	-.008			-.004	-.010	9
10	-.022		-.027	-.016			-.021	-.006	10
11	-.018		-.027	-.027			-.011	-.018	11
12	-.064	-.069	-.164	-.154	-.154	-.057	-.032	-.024	12
13	-.064	-.095	-.188	-.194	-.167	-.057	-.065	-.028	13
14	-.061	-.113	-.187	-.194	-.165	-.097	-.075	-.033	14
15	-.076	-.125	-.175	-.194	-.149	-.104	-.072	-.028	15
16	-.079	-.114	-.165	-.197	-.170	-.102	-.079	-.033	16
17	.108		.116	.094			.109	.089	17
18	.096		.108	.106			.108	.093	18
19	.094		.107	.109			.105	.065	19
20	.074		.092	.092			.086	.039	20
21	.001		.011	.033			.034	.011	21
22	.015		-.002	.016				.005	22
23	.018			.008			.017	.001	23
24	.005		.001	.009			.004	-.010	24
25	.003		-.014	-.003			-.001	.008	25
26	-.034		-.033	-.017			-.014	-.004	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=0 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.099		.102	.115			.094	.102	1
2	.066		.103	.107			.099	.072	2
3	.087		.113	.101			.103	.075	3
4	.082		.095	.089			.075	.055	4
5	-.004		.016	.029			.032	.017	5
6	.012		.002	.010			.008	.008	6
7	.010		-.004	.001			.005	-.008	7
8	-.003		-.004	-.001			-.010		8
9	-.008		-.011	-.018			-.010	-.006	9
10	-.031		-.023	-.027			-.033	-.006	10
11	-.023		-.023	-.038			-.017	-.014	11
12	-.060	-.071	-.231	-.220	-.221	-.050	-.031	-.020	12
13	-.062	-.100	-.248	-.254	-.228	-.058	-.064	-.025	13
14	-.056	-.122	-.249	-.257	-.225	-.103	-.071	-.033	14
15	-.072	-.132	-.225	-.252	-.229	-.116	-.067	-.029	15
16	-.078	-.127	-.224	-.207	-.257	-.113	-.075	-.029	16
17	.110		.108	.090			.098	.100	17
18	.090		.104	.090			.102	.094	18
19	.088		.106	.101			.100	.075	19
20	.069		.089	.075			.075	.041	20
21	.000		.018	.023			.018	.013	21
22	.003		.004	.005				.010	22
23	.011			.002			.005	.008	23
24	.006		-.001	.001			-.009	-.006	24
25	.000		-.011	-.014			-.012	-.011	25
26	-.029		-.040	-.030			-.028	-.001	26

α=0 δ=30

1	.116		.104	.115			.106	.102	1
2	.064		.106	.113			.103	.072	2
3	.080		.108	.106			.106	.078	3
4	.081		.097	.096			.073	.056	4
5	.018		.021	.030			.031	.014	5
6	.010		.013	.011			.004	.009	6
7	-.007		-.011	.001			.011	-.010	7
8	-.007		-.004	.002			-.008		8
9	-.006		-.008	-.015			-.010	-.009	9
10	-.023		-.024	-.027			-.033	-.005	10
11	-.023		-.024	-.039			-.017	-.015	11
12	-.065	-.076	-.266	-.263	-.255	-.050	-.031	-.024	12
13	-.066	-.105	-.273	-.282	-.263	-.058	-.064	-.028	13
14	-.060	-.123	-.264	-.275	-.245	-.105	-.072	-.034	14
15	-.074	-.132	-.247	-.264	-.273	-.116	-.071	-.031	15
16	-.080	-.126	-.245	-.245	-.283	-.117	-.075	-.033	16
17	.109		.112	.090			.097	.097	17
18	.091		.110	.088			.094	.090	18
19	.082		.103	.100			.093	.072	19
20	.065		.092	.074			.069	.039	20
21	.008		.021	.023			.022	.013	21
22	.008		.003	.004				.006	22
23	.008			-.006			.008	.004	23
24	.001		.003	.002			-.010	-.009	24
25	.000		.054	.272			-.015	.009	25
26	-.030		.244	.295			-.028	-.004	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.038		.027	.040			.038	.038	1
2	.018		.030	.039			.051	.038	2
3	.022		.049	.041			.048	.047	3
4	.029		.032	.026			.021	.028	4
5	-.037		-.035	-.021			-.012	-.001	5
6	-.034		-.048	-.047			-.031	-.005	6
7	-.041		-.062	-.054			-.040	-.025	7
8	-.050		-.055	-.050			-.051		8
9	-.058		-.065	-.056			-.053	-.019	9
10	-.072		-.074	-.069			-.073	-.022	10
11	-.076		-.074	-.078			-.041	-.039	11
12	-.093	-.108	-.085	-.084	-.098	-.092	-.076	-.047	12
13	-.095	-.111	-.100	-.109	-.105	-.088	-.099	-.055	13
14	-.093	-.105	-.111	-.111	-.103	-.100	-.103	-.072	14
15	-.103	-.112	-.108	-.111	-.105	-.100	-.099	-.097	15
16	-.107	-.111	-.111	-.108	-.109	-.102	-.104	-.111	16
17	.193		.208	.180			.194	.175	17
18	.146		.201	.186			.197	.158	18
19	.153		.199	.194			.196	.125	19
20	.138		.173	.165			.172	.086	20
21	.064		.088	.106			.112	.048	21
22	.065		.065	.091				.029	22
23	.066			.078			.092	.017	23
24	.065		.064	.077			.077	.000	24
25	.060		.040	.064			.068	.019	25
26	.013		.021	.046			.046	.003	26

$\alpha = 6$ $\delta = -30$

1	-.028		-.043	-.025			-.018	-.028	1
2	-.038		-.029	-.024			-.021	-.008	2
3	-.030		-.034	-.021			-.020	.001	3
4	-.033		-.035	-.041			-.048	-.011	4
5	-.092		-.106	-.083			-.070	-.042	5
6	-.098		-.106	-.102			-.093	-.058	6
7	-.090		-.115	-.093			-.090	-.097	7
8	-.100		-.108	-.089			-.106		8
9	-.101		-.097	-.057			-.107	-.116	9
10	-.121		.090	.123			-.123	-.126	10
11	-.122		.090	.130			-.078	-.145	11
12	-.128	-.064	.100	.151	.094	-.025	-.122	-.161	12
13	-.132	-.057	.177	.189	.122	-.070	-.142	-.151	13
14	-.131	-.158	.416	.447	.344	-.127	-.136	-.161	14
15	-.140	-.194	.423	.543	.361	-.168	-.130	-.183	15
16	-.139	-.183	.391	.553	.332	-.177	-.123	-.169	16
17	.269		.285	.286			.285	.263	17
18	.216		.296	.284			.293	.233	18
19	.214		.286	.295			.293	.182	19
20	.207		.260	.262			.258	.137	20
21	.119		.153	.189			.191	.079	21
22	.121		.131	.168				.053	22
23	.126			.159			.169	.032	23
24	.120		.118	.159			.159	.010	24
25	.122		.100	.144			.147	.034	25
26	.067		.074	.114			.120	.011	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.021		-.032	-.015			-.016	-.018	1
2	-.021		-.017	-.024			-.018	-.003	2
3	-.011		-.013	-.024			-.012	.008	3
4	-.017		-.027	-.035			-.045	-.003	4
5	-.078		-.095	-.069			-.071	-.037	5
6	-.073		-.091	-.089			-.096	-.050	6
7	-.086		-.102	-.101			-.093	-.093	7
8	-.087		-.100	-.096			-.102		8
9	-.089		-.105	-.108			-.101	-.111	9
10	-.104		-.096	-.113			-.125	-.119	10
11	-.112		-.096	-.048			-.076	-.137	11
12	-.125	-.095	.093	.072	.019	-.074	-.121	-.167	12
13	-.127	-.109	.182	.168	.100	-.089	-.137	-.151	13
14	-.125	-.130	.188	.235	.135	-.118	-.139	-.160	14
15	-.137	-.169	.156	.238	.114	-.141	-.135	-.179	15
16	-.139	-.169	.133	.238	.090	-.158	-.133	-.169	16
17	.290		.296	.285			.294	.268	17
18	.229		.309	.288			.299	.239	18
19	.231		.294	.299			.292	.186	19
20	.219		.263	.262			.259	.139	20
21	.129		.154	.191			.188	.085	21
22	.131		.136	.169				.062	22
23	.137			.161			.167	.041	23
24	.126		.137	.158			.152	.014	24
25	.130		.118	.140			.146	.038	25
26	.077		.084	.115			.118	.014	26

α=6 δ=-10

1	-.021		-.024	-.019			-.023	-.019	1
2	-.021		-.024	-.020			-.021	-.006	2
3	-.017		-.020	-.021			-.012	.006	3
4	-.030		-.023	-.036			-.041	-.005	4
5	-.084		-.092	-.075			-.074	-.037	5
6	-.078		-.098	-.095			-.091	-.053	6
7	-.083		-.102	-.095			-.101	-.092	7
8	-.091		-.092	-.105			-.108		8
9	-.091		-.109	-.112			-.104	-.109	9
10	-.107		-.099	-.121			-.127	-.119	10
11	-.109		-.099	-.127			-.082	-.140	11
12	-.127	-.136	-.013	-.055	-.090	-.130	-.123	-.165	12
13	-.135	-.123	.003	-.014	-.037	-.118	-.145	-.154	13
14	-.131	-.125	-.019	.003	-.043	-.118	-.146	-.161	14
15	-.140	-.128	-.032	.004	-.052	-.123	-.140	-.183	15
16	-.145	-.149	-.046	.005	-.060	-.125	-.141	-.174	16
17	.285		.296	.282			.287	.263	17
18	.228		.302	.280			.293	.233	18
19	.227		.294	.294			.294	.183	19
20	.220		.265	.258			.253	.136	20
21	.128		.157	.190			.190	.083	21
22	.126		.130	.164				.057	22
23	.135			.157			.168	.036	23
24	.129		.130	.158			.153	.009	24
25	.131		.115	.138			.146	.033	25
26	.070		.087	.109			.119	.011	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.022		-.028	-.013			-.018	.020	1
2	-.024		-.021	-.024			-.018	-.010	2
3	-.019		-.018	-.025			-.010	.005	3
4	-.021		-.027	-.037			-.036	-.004	4
5	-.080		-.088	-.076			-.070	-.038	5
6	-.081		-.094	-.089			-.085	-.056	6
7	-.093		-.104	-.089			-.085	-.092	7
8	-.093		-.096	-.091			-.098		8
9	-.090		-.109	-.106			-.099	-.111	9
10	-.107		-.103	-.110			-.117	-.117	10
11	-.110		-.102	-.121			-.077	-.140	11
12	-.126	-.144	-.111	-.126	-.141	-.139	-.125	-.163	12
13	-.132	-.146	-.136	-.145	-.142	-.132	-.144	-.151	13
14	-.131	-.141	-.144	-.141	-.144	-.139	-.145	-.159	14
15	-.141	-.150	-.141	-.144	-.144	-.141	-.140	-.180	15
16	-.142	-.144	-.145	-.144	-.145	-.139	-.141	-.170	16
17	.287		.296	.277			.285	.258	17
18	.224		.306	.292			.296	.234	18
19	.231		.291	.301			.294	.183	19
20	.217		.264	.262			.257	.139	20
21	.127		.162	.190			.187	.079	21
22	.130		.138	.174				.057	22
23	.134			.165			.173	.036	23
24	.123		.134	.159			.161	.010	24
25	.124		.109	.142			.149	.032	25
26	.071		.076	.120			.121	.011	26

$\alpha=6$ $\delta=10$

1	-.026		-.035	-.016			-.017	-.023	1
2	-.026		-.026	-.027			-.026	-.010	2
3	-.022		-.022	-.027			-.022	.001	3
4	-.022		-.039	-.040			-.042	-.010	4
5	-.084		-.087	-.076			-.075	-.044	5
6	-.083		-.097	-.093			-.093	-.058	6
7	-.095		-.110	-.100			-.094	-.097	7
8	-.100		-.096	-.100			-.105		8
9	-.106		-.116	-.107			-.099	-.113	9
10	-.116		-.110	-.118			-.122	-.121	10
11	-.115		-.110	-.130			-.081	-.142	11
12	-.133	-.142	-.200	-.200	-.205	-.135	-.125	-.161	12
13	-.135	-.161	-.222	-.230	-.210	-.140	-.146	-.150	13
14	-.133	-.174	-.221	-.230	-.216	-.163	-.145	-.155	14
15	-.144	-.179	-.214	-.233	-.196	-.170	-.141	-.178	15
16	-.145	-.156	-.164	-.174	-.229	-.167	-.140	-.169	16
17	.283		.292	.279			.289	.261	17
18	.213		.303	.281			.287	.230	18
19	.221		.290	.293			.286	.174	19
20	.211		.261	.259			.248	.136	20
21	.117		.154	.184			.178	.078	21
22	.123		.132	.164				.053	22
23	.131			.155			.166	.032	23
24	.125		.132	.153			.150	.008	24
25	.117		.110	.139			.141	.024	25
26	.067		.078	.110			.114	.005	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.025		-.031	-.020			-.013	-.023	1
2	-.032		-.026	-.021			-.026	-.015	2
3	-.013		-.021	-.023			-.017	.003	3
4	-.021		-.028	-.034			-.049	-.011	4
5	-.076		-.087	-.074			-.073	-.044	5
6	-.086		-.095	-.092			-.096	-.056	6
7	-.087		-.104	-.097			-.098	-.095	7
8	-.092		-.096	-.103			-.104		8
9	-.088		-.106	-.108			-.103	-.114	9
10	-.102		-.103	-.120			-.120	-.119	10
11	-.109		-.103	-.127			-.082	-.142	11
12	-.132	-.147	-.253	-.249	-.249	-.135	-.125	-.163	12
13	-.137	-.169	-.269	-.273	-.252	-.139	-.145	-.153	13
14	-.133	-.180	-.241	-.250	-.247	-.174	-.149	-.155	14
15	-.142	-.182	-.221	-.239	-.268	-.182	-.141	-.180	15
16	-.146	-.151	-.217	-.221	-.285	-.173	-.145	-.170	16
17	.285		.298	.276			.282	.257	17
18	.227		.304	.279			.293	.225	18
19	.228		.292	.289			.294	.178	19
20	.213		.260	.251			.245	.136	20
21	.127		.151	.180			.184	.076	21
22	.130		.133	.160				.053	22
23	.134			.154			.165	.029	23
24	.128		.133	.155			.154	.004	24
25	.124		.112	.137			.144	.025	25
26	.067		.082	.114			.115	.006	26

α=6 δ=30

1	-.020		-.028	-.022			-.014	-.023	1
2	-.034		-.027	-.026			-.019	-.009	2
3	-.020		-.021	-.027			-.014	.001	3
4	-.028		-.031	-.043			-.039	-.010	4
5	-.090		-.102	-.088			-.070	-.042	5
6	-.081		-.105	-.101			-.092	-.056	6
7	-.089		-.110	-.099			-.090	-.093	7
8	-.092		-.106	-.098			-.104		8
9	-.091		-.111	-.112			-.098	-.109	9
10	-.111		-.109	-.114			-.116	-.118	10
11	-.106		-.109	-.129			-.076	-.142	11
12	-.132	-.145	-.269	-.263	-.280	-.137	-.125	-.160	12
13	-.137	-.170	-.272	-.271	-.278	-.141	-.145	-.147	13
14	-.135	-.183	-.249	-.257	-.266	-.178	-.145	-.151	14
15	-.142	-.180	-.241	-.257	-.305	-.186	-.141	-.178	15
16	-.146	-.153	-.248	-.250	-.310	-.178	-.142	-.170	16
17	.281		.290	.274			.284	.258	17
18	.221		.296	.280			.287	.226	18
19	.226		.286	.289			.287	.177	19
20	.213		.256	.255			.251	.133	20
21	.124		.149	.185			.186	.072	21
22	.128		.130	.167				.053	22
23	.128			.157			.160	.029	23
24	.122		.118	.336			.150	.005	24
25	.124		.361	.506			.143	.025	25
26	.060		.426	.523			.113	.006	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.069		-.075	-.065			-.068	-.066	1
2	-.068		-.069	-.069			-.072	-.047	2
3	-.058		-.064	-.070			-.074	-.034	3
4	-.062		-.070	-.086			-.096	-.051	4
5	-.119		-.132	-.122			-.119	-.084	5
6	-.106		-.131	-.138			-.134	-.141	6
7	-.113		-.136	-.139			-.128	-.186	7
8	-.123		-.137	-.139			-.146		8
9	-.126		-.140	-.150			-.141	-.192	9
10	-.134		-.130	-.156			-.158	-.190	10
11	-.142			-.166			-.115	-.194	11
12	-.155	-.171	-.152	-.164	-.178	-.168	-.155	-.192	12
13	-.162	-.176	-.171	-.185	-.178	-.164	-.172	-.190	13
14	-.161	-.172	-.176	-.183	-.176	-.172	-.169	-.195	14
15	-.168	-.177	-.178	-.181	-.178	-.176	-.162	-.201	15
16	-.169	-.172	-.177	-.182	-.182	-.176	-.163	-.197	16
17	.391		.426	.386			.406	.371	17
18	.310		.429	.399			.408	.324	18
19	.316		.409	.410			.405	.255	19
20	.311		.354	.374			.361	.203	20
21	.199		.230	.286			.291	.138	21
22	.207		.211	.257				.101	22
23	.207			.239			.258	.078	23
24	.199		.204	.227			.243	.045	24
25	.201		.174	.205			.231	.073	25
26	.138		.156	.178			.194	.047	26

$\alpha = 12$ $\delta = -30$

1	-.113		-.127	-.112			-.122	-.118	1
2	-.110		-.122	-.118			-.122	-.097	2
3	-.101		-.120	-.118			-.117	-.083	3
4	-.103		-.124	-.131			-.135	-.110	4
5	-.152		-.172	-.162			-.157	-.159	5
6	-.146		-.172	-.172			-.172	-.229	6
7	-.157		-.178	-.173			-.170	-.259	7
8	-.165		-.176	-.170			-.180		8
9	-.158		-.184	-.181			-.176	-.256	9
10	-.165		-.044	-.042			-.192	-.248	10
11	-.176			-.004			-.136	-.241	11
12	-.191	-.130	-.020	.010	-.024	-.118	-.199	-.234	12
13	-.194	-.139	.028	.068	.004	-.161	-.210	-.232	13
14	-.192	-.191	.238	.270	.185	-.178	-.205	-.240	14
15	-.204	-.229	.261	.319	.192	-.203	-.199	-.241	15
16	-.181	-.223	.234	.330	.171	-.210	-.196	-.232	16
17	.484		.610	.558			.573	.506	17
18	.397		.567	.561			.557	.426	18
19	.407		.521	.563			.561	.348	19
20	.401		.446	.504			.508	.290	20
21	.278		.314	.389			.420	.209	21
22	.286		.305	.346				.161	22
23	.294			.325			.371	.134	23
24	.279		.284	.314			.355	.104	24
25	.275		.261	.289			.329	.134	25
26	.209		.233	.257			.291	.104	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.126		-.140	-.123			-.124	-.108	1
2	-.122		-.127	-.129			-.123	-.087	2
3	-.104		-.132	-.128			-.123	-.078	3
4	-.104		-.137	-.138			-.142	-.104	4
5	-.158		-.184	-.168			-.159	-.145	5
6	-.153		-.175	-.181			-.177	-.223	6
7	-.167		-.190	-.183			-.176	-.247	7
8	-.172		-.188	-.179			-.181		8
9	-.165		-.194	-.187			-.180	-.245	9
10	-.175		-.172	-.195			-.197	-.242	10
11	-.185			-.168			-.136	-.234	11
12	-.180	-.162	-.043	-.051	-.094	-.175	-.189	-.229	12
13	-.186	-.166	.024	.014	-.032	-.166	-.203	-.228	13
14	-.183	-.176	.052	.065	.005	-.178	-.196	-.233	14
15	-.192	-.191	.036	.071	-.006	-.169	-.190	-.234	15
16	-.183	-.219	.019	.080	-.019	-.182	-.189	-.224	16
17	.475		.599	.553			.565	.512	17
18	.393		.558	.553			.545	.428	18
19	.403		.515	.564			.551	.350	19
20	.393		.431	.504			.494	.294	20
21	.270		.305	.384			.411	.210	21
22	.278		.296	.339				.167	22
23	.278			.322			.365	.143	23
24	.270		.273	.305			.340	.106	24
25	.270		.252	.285			.314	.135	25
26	.202		.220	.256			.270	.108	26

α=12 δ=-10

1	-.124		-.131	-.121			-.114	-.111	1
2	-.115		-.123	-.123			-.117	-.089	2
3	-.103		-.124	-.121			-.116	-.080	3
4	-.106		-.128	-.133			-.130	-.106	4
5	-.158		-.172	-.165			-.152	-.147	5
6	-.155		-.173	-.175			-.168	-.223	6
7	-.161		-.184	-.176			-.168	-.250	7
8	-.167		-.181	-.176			-.176		8
9	-.166		-.185	-.183			-.177	-.247	9
10	-.170		-.169	-.188			-.190	-.241	10
11	-.180			-.194			-.130	-.236	11
12	-.182	-.192	-.113	-.134	-.155	-.199	-.187	-.234	12
13	-.187	-.183	-.104	-.124	-.143	-.192	-.201	-.233	13
14	-.187	-.183	-.116	-.111	-.141	-.187	-.194	-.240	14
15	-.194	-.158	-.121	-.116	-.147	-.183	-.186	-.237	15
16	-.186	-.204	-.126	-.106	-.136	-.168	-.189	-.233	16
17	.479		.604	.561			.572	.508	17
18	.394		.559	.558			.559	.429	18
19	.411		.519	.571			.554	.350	19
20	.403		.442	.506			.503	.294	20
21	.279		.311	.388			.418	.211	21
22	.286		.295	.347				.167	22
23	.281			.325			.370	.141	23
24	.279		.277	.315			.354	.108	24
25	.277		.257	.291			.323	.139	25
26	.207		.221	.256			.280	.110	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.115		-.123	-.117			-.108	-.110	1
2	-.114		-.117	-.113			-.115	-.089	2
3	-.102		-.115	-.120			-.117	-.076	3
4	-.098		-.120	-.128			-.131	-.099	4
5	-.150		-.168	-.154			-.155	-.141	5
6	-.144		-.168	-.166			-.171	-.215	6
7	-.150		-.176	-.172			-.165	-.240	7
8	-.160		-.174	-.176			-.173		8
9	-.157		-.176	-.179			-.177	-.238	9
10	-.167		-.156	-.187			-.188	-.231	10
11	-.177			-.195			-.130	-.227	11
12	-.180	-.196	-.183	-.196	-.210	-.203	-.189	-.227	12
13	-.182	-.201	-.197	-.213	-.209	-.197	-.205	-.222	13
14	-.185	-.199	-.201	-.214	-.205	-.203	-.195	-.231	14
15	-.194	-.206	-.201	-.211	-.210	-.208	-.191	-.232	15
16	-.185	-.183	-.189	-.204	-.213	-.208	-.190	-.224	16
17	.485		.613	.561			.565	.508	17
18	.407		.568	.561			.549	.426	18
19	.411		.529	.568			.555	.349	19
20	.405		.451	.497			.504	.290	20
21	.284		.319	.392			.418	.211	21
22	.289		.301	.345				.166	22
23	.289			.320			.368	.139	23
24	.284		.287	.310			.343	.106	24
25	.279		.262	.288			.321	.136	25
26	.211		.228	.257			.270	.108	26

α=12 δ=10

1	-.125		-.127	-.116			-.117	-.115	1
2	-.114		-.125	-.124			-.119	-.093	2
3	-.106		-.131	-.116			-.114	-.083	3
4	-.103		-.128	-.130			-.135	-.104	4
5	-.154		-.175	-.166			-.160	-.147	5
6	-.153		-.172	-.172			-.172	-.224	6
7	-.161		-.185	-.178			-.172	-.251	7
8	-.171		-.182	-.180			-.178		8
9	-.161		-.186	-.193			-.180	-.250	9
10	-.170		-.158	-.173			-.191	-.245	10
11	-.179			-.180			-.136	-.233	11
12	-.183	-.196	-.236	-.233	-.236	-.192	-.195	-.233	12
13	-.189	-.211	-.247	-.251	-.236	-.199	-.206	-.228	13
14	-.187	-.220	-.214	-.241	-.241	-.213	-.199	-.243	14
15	-.195	-.204	-.199	-.208	-.227	-.222	-.194	-.240	15
16	-.183	-.191	-.180	-.185	-.245	-.218	-.194	-.236	16
17	.480		.606	.553			.570	.506	17
18	.397		.562	.553			.546	.428	18
19	.403		.521	.564			.555	.347	19
20	.400		.443	.498			.505	.292	20
21	.275		.311	.383			.416	.210	21
22	.284		.294	.342				.163	22
23	.280			.320			.368	.139	23
24	.276		.280	.309			.347	.107	24
25	.270		.255	.287			.312	.139	25
26	.201		.234	.257			.278	.110	26

TABLE XI.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.133		-.139	-.123			-.113	-.113	1
2	-.124		-.136	-.129			-.122	-.094	2
3	-.115		-.137	-.124			-.116	-.082	3
4	-.112		-.139	-.136			-.137	-.102	4
5	-.164		-.187	-.167			-.154	-.150	5
6	-.167		-.183	-.182			-.170	-.223	6
7	-.173		-.192	-.180			-.173	-.255	7
8	-.172		-.185	-.174			-.175		8
9	-.173		-.193	-.187			-.179	-.250	9
10	-.187		-.165	-.191			-.190	-.243	10
11	-.192			-.197			-.136	-.229	11
12	-.187	-.200	-.268	-.270	-.269	-.206	-.195	-.229	12
13	-.192	-.219	-.268	-.282	-.273	-.206	-.210	-.229	13
14	-.190	-.228	-.232	-.254	-.248	-.225	-.201	-.245	14
15	-.200	-.209	-.238	-.228	-.270	-.231	-.197	-.243	15
16	-.171	-.186	-.245	-.211	-.289	-.219	-.195	-.236	16
17	.474		.597	.548			.567	.502	17
18	.390		.555	.556			.549	.422	18
19	.393		.518	.559			.555	.345	19
20	.391		.440	.504			.503	.288	20
21	.269		.308	.382			.417	.208	21
22	.279		.293	.338				.161	22
23	.274			.318			.371	.132	23
24	.268		.276	.307			.349	.104	24
25	.266		.255	.286			.319	.130	25
26	.199		.257	.590			.276	.104	26

α=12 δ=30

1	-.127		-.131	-.113			-.122	-.116	1
2	-.110		-.121	-.123			-.123	-.087	2
3	-.104		-.124	-.127			-.118	-.079	3
4	-.108		-.130	-.135			-.139	-.104	4
5	-.165		-.172	-.171			-.158	-.147	5
6	-.159		-.179	-.178			-.173	-.220	6
7	-.161		-.187	-.181			-.174	-.251	7
8	-.169		-.179	-.178			-.179		8
9	-.165		-.186	-.185			-.182	-.251	9
10	-.177		-.160	-.191			-.194	-.245	10
11	-.185			-.200			-.133	-.229	11
12	-.185	-.199	-.255	-.259	-.266	-.200	-.190	-.223	12
13	-.187	-.218	-.255	-.264	-.269	-.199	-.208	-.222	13
14	-.187	-.222	-.256	-.254	-.271	-.223	-.200	-.238	14
15	-.191	-.208	-.270	-.250	-.292	-.223	-.194	-.241	15
16	-.103	-.185	-.266	-.241	-.287	-.201	-.182	-.233	16
17	.477		.595	.550			.563	.507	17
18	.396		.557	.553			.547	.427	18
19	.401		.516	.563			.551	.349	19
20	.400		.440	.496			.501	.289	20
21	.273		.313	.379			.410	.209	21
22	.279		.298	.335				.164	22
23	.281			.539			.366	.136	23
24	.271		.290	.720			.344	.108	24
25	.267		.636	.746			.321	.135	25
26	.202		.640	.746			.344	.108	26

TABLE XI.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 2.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.158		-.163	-.148			-.159	-.134	1
2	-.158		-.163	-.152			-.169	-.108	2
3	-.139		-.160	-.154			-.157	-.115	3
4	-.145		-.166	-.165			-.177	-.161	4
5	-.193		-.201	-.197			-.195	-.201	5
6	-.175		-.199	-.200			-.204	-.250	6
7	-.193		-.208	-.211			-.206	-.268	7
8	-.196		-.207	-.210			-.216		8
9	-.190		-.213	-.217			-.215	-.259	9
10	-.200		-.181	-.222			-.221	-.248	10
11	-.202			-.227			-.153	-.243	11
12	-.200	-.219	-.211	-.220	-.233	-.228	-.213	-.243	12
13	-.205	-.223	-.225	-.236	-.233	-.224	-.227	-.246	13
14	-.203	-.220	-.223	-.234	-.232	-.228	-.214	-.262	14
15	-.211	-.227	-.222	-.234	-.234	-.231	-.208	-.256	15
16	-.162	-.148	-.148	-.187	-.222	-.213	-.203	-.254	16
17	.585		.769	.790			.812	.705	17
18	.495		.695	.743			.782	.589	18
19	.507		.626	.694			.731	.487	19
20	.494		.534	.590			.633	.395	20
21	.365		.395	.458			.511	.283	21
22	.370		.381	.418				.223	22
23	.371			.402			.428	.191	23
24	.361		.362	.394			.405	.161	24
25	.359		.344	.376			.382	.192	25
26	.279		.307	.336			.332	.162	26

TABLE XII

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.565		.772	.824			.827	.758	1
2	.507		.691	.764			.799	.616	2
3	.516		.633	.712			.754	.513	3
4	.514		.558	.611			.634	.389	4
5	.381		.420	.482			.528	.300	5
6	.380		.389	.437			.475	.196	6
7	.378		.382	.421			.438	.178	7
8	.371		.387	.412			.421		8
9	.361		.362	.378			.371	.163	9
10	.299		.317	.355			.322	.160	10
11	.339		.316	.335			.298	.132	11
12	.241	.215	.287	.307			.369	.083	12
13	.241	.242	.248	.257			.246	.079	13
14	.241	.234	.252	.264			.232	.070	14
15	.236	.223	.250	.262			.216	.060	15
16	.233	.211	.236	.264			.204	.055	16
17	-.155		-.152	-.156		-.151	-.120		17
18	-.128		-.154	-.154		-.148	-.090		18
19	-.130		-.162	-.156		-.153	-.119		19
20	-.139		-.164	-.165		-.169	-.147		20
21	-.176		-.199	-.192		-.191	-.188		21
22	-.173		-.204	-.201			-.230		22
23	-.178			-.206		-.201	-.238		23
24	-.183		-.202	-.205		-.203	-.250		24
25	-.181		-.205	-.201		-.186	-.230		25
26	-.191		-.206	-.186		-.189	-.220		26

α=-12 δ=-30

1	.471		.585	.582			.568	.511	1
2	.416		.550	.551			.535	.406	2
3	.402		.526	.552			.544	.349	3
4	.402		.452	.502			.492	.269	4
5	.292		.322	.389			.413	.201	5
6	.295		.303	.346			.381	.133	6
7	.289		.294	.668			.753	.320	7
8	.278		.407	.738			.782		8
9	.275		.650	.760			.791	.424	9
10	.221		.638	.774			.785	.422	10
11	.254		.638	.779			.792	.397	11
12	.160	.419	.413	.814			.774	.402	12
13	.160	.347	.634	.800			.790	.449	13
14	.225	.123	.988	1.043			.946	.639	14
15	.275	.029	1.041	1.256			1.114	.844	15
16	.298	-.005	.872	1.148			1.080	.863	16
17	-.115		-.118	-.122		-.114	-.109		17
18	-.099		-.116	-.117		-.116	-.072		18
19	-.098		-.118	-.119		-.113	-.087		19
20	-.103		-.123	-.133		-.131	-.114		20
21	-.148		-.165	-.160		-.156	-.145		21
22	-.141		-.170	-.171			-.209		22
23	-.150			-.175		-.171	-.223		23
24	-.153		-.170	-.175		-.173	-.228		24
25	-.150		-.174	-.180		-.178	-.207		25
26	-.167		-.185	-.190		-.185	-.192		26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.475		.588	.584			.570	.507	1
2	.415		.552	.552			.537	.403	2
3	.404		.529	.552			.545	.347	3
4	.406		.454	.502			.492	.269	4
5	.293		.326	.389			.414	.195	5
6	.296		.305	.343			.376	.132	6
7	.289		.288	.325			.364	.096	7
8	.279		.291	.312			.342		8
9	.278		.267	.283			.304	.093	9
10	.222		.258	.637			.592	.186	10
11	.255		.256	.670			.678	.292	11
12	.148	.334	.580	.685			.676	.305	12
13	.154	.282	.704	.721			.737	.413	13
14	.154	.195	.750	.895			.895	.550	14
15	.138	.037	.686	.963			.933	.598	15
16	.152	.033	.620	.884			.873	.591	16
17 -	.111		- .121	- .126		- .115	- .114		17
18 -	.096		- .118	- .120		- .119	- .076		18
19 -	.097		- .122	- .123		- .115	- .087		19
20 -	.101		- .127	- .133		- .132	- .113		20
21 -	.147		- .170	- .163		- .158	- .154		21
22 -	.138		- .174	- .174			- .214		22
23 -	.148			- .178		- .172	- .233		23
24 -	.150		- .175	- .177		- .174	- .259		24
25 -	.149		- .179	- .182		- .177	- .232		25
26 -	.164		- .190	- .191		- .187	- .198		26

α=-12 δ=-10

1	.473		.589	.587			.574	.521	1
2	.417		.554	.553			.540	.411	2
3	.407		.529	.552			.549	.355	3
4	.412		.456	.505			.493	.275	4
5	.295		.326	.391			.416	.204	5
6	.297		.306	.349			.373	.136	6
7	.299		.290	.330			.363	.109	7
8	.279		.291	.317			.343		8
9	.279		.270	.283			.309	.099	9
10	.223		.240	.265			.253	.101	10
11	.250		.240	.259			.241	.068	11
12	.159	.198	.483	.381			.434	.069	12
13	.159	.244	.470	.512			.518	.288	13
14	.161	.233	.415	.529			.507	.292	14
15	.143	.110	.381	.534			.492	.261	15
16	.145	.041	.340	.527			.476	.257	16
17 -	.110		- .116	- .122		- .116	- .106		17
18 -	.093		- .113	- .118		- .119	- .067		18
19 -	.093		- .116	- .119		- .120	- .079		19
20 -	.099		- .121	- .133		- .134	- .106		20
21 -	.144		- .163	- .161		- .158	- .147		21
22 -	.136		- .166	- .171			- .209		22
23 -	.145			- .175		- .173	- .228		23
24 -	.148		- .166	- .174		- .174	- .246		24
25 -	.147		- .170	- .180		- .178	- .229		25
26 -	.164		- .184	- .188		- .186	- .212		26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.472		.591	.593			.578	.535	1
2	.417		.554	.554			.543	.411	2
3	.407		.529	.555			.551	.366	3
4	.408		.458	.508			.493	.279	4
5	.294		.325	.396			.418	.212	5
6	.292		.305	.351			.375	.148	6
7	.289		.289	.330			.366	.115	7
8	.280		.293	.320			.345		8
9	.280		.271	.284			.308	.110	9
10	.223		.239	.265			.254	.113	10
11	.250		.240	.251			.237	.088	11
12	.161	.137	.192	.216			.297	.044	12
13	.165	.157	.165	.170			.173	.024	13
14	.164	.151	.164	.173			.159	.010	14
15	.150	.141	.163	.168			.148	.001	15
16	.147	.137	.150	.172			.131	-.004	16
17	-.109		-.112	-.119			-.112	-.090	17
18	-.082		-.108	-.115			-.106	-.054	18
19	-.095		-.113	-.114			-.112	-.065	19
20	-.099		-.117	-.129			-.130	-.091	20
21	-.143		-.161	-.157			-.155	-.133	21
22	-.135		-.164	-.165				-.187	22
23	-.145			-.170			-.170	-.202	23
24	-.147		-.164	-.171			-.169	-.223	24
25	-.145		-.165	-.174			-.172	-.202	25
26	-.158		-.177	-.180			-.182	-.207	26

α=-12 δ=10

1	.467		.584	.588			.575	.530	1
2	.411		.550	.551			.544	.424	2
3	.402		.524	.551			.553	.370	3
4	.405		.452	.503			.493	.294	4
5	.289		.322	.390			.420	.212	5
6	.290		.303	.346			.378	.147	6
7	.287		.286	.330			.369	.119	7
8	.275		.290	.317			.350		8
9	.275		.267	.287			.312	.111	9
10	.215		.236	.266			.256	.114	10
11	.244		.236	.251			.239	.087	11
12	.168	.146	.022	.037			.131	-.076	12
13	.170	.114	-.020	-.018			-.006	-.102	13
14	.170	.084	.005	-.012			-.023	-.113	14
15	.157	.063	.005	-.024			-.028	-.118	15
16	.148	.036	-.038	-.018			-.038	-.119	16
17	-.115		-.123	-.123			-.119	-.104	17
18	-.099		-.118	-.120			-.120	-.063	18
19	-.099		-.124	-.123			-.117	-.074	19
20	-.105		-.128	-.137			-.137	-.108	20
21	-.149		-.169	-.164			-.161	-.143	21
22	-.141		-.175	-.174				-.206	22
23	-.150			-.178			-.175	-.228	23
24	-.152		-.175	-.178			-.178	-.236	24
25	-.151		-.179	-.185			-.178	-.224	25
26	-.167		-.190	-.192			-.189	-.209	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.466		.580	.584			.581	.522	1
2	.409		.546	.546			.545	.416	2
3	.398		.521	.547			.554	.351	3
4	.403		.448	.502			.495	.275	4
5	.286		.316	.387			.418	.204	5
6	.288		.298	.344			.380	.134	6
7	.282		.283	.326			.370	.096	7
8	.271		.286	.314			.345		8
9	.271		.262	.283			.311	.099	9
10	.215		.232	.263			.256	.101	10
11	.240		.232	.248			.241	.076	11
12	.159	.150	- .115	- .102		-	.032	- .164	12
13	.161	.106	- .154	- .148		-	.132	- .187	13
14	.161	.065	- .132	- .150		-	.145	- .193	14
15	.146	.032	- .141	- .147		-	.154	- .197	15
16	.143	.019	- .163	- .159		-	.160	- .195	16
17 -	.122		- .126	- .132		-	.121	- .114	17
18 -	.105		- .125	- .127		-	.124	- .077	18
19 -	.104		- .130	- .127		-	.120	- .083	19
20 -	.111		- .135	- .138		-	.137	- .118	20
21 -	.156		- .177	- .167		-	.164	- .157	21
22 -	.147		- .182	- .179				- .218	22
23 -	.156			- .181		-	.177	- .238	23
24 -	.159		- .182	- .181		-	.180	- .256	24
25 -	.158		- .187	- .185		-	.182	- .236	25
26 -	.174		- .196	- .194		-	.190	- .221	26

α=-12 δ=30

1	.479		.599	.606			.595	.534	1
2	.424		.562	.564			.555	.419	2
3	.411		.536	.565			.565	.362	3
4	.413		.462	.517			.507	.280	4
5	.296		.334	.402			.430	.206	5
6	.300		.311	.357			.390	.142	6
7	.295		.296	.337			.376	.114	7
8	.283		.297	.324			.356		8
9	.284		.277	.292			.320	.109	9
10	.227		.245	.274			.263	.111	10
11	.258		.245	.261			.247	.078	11
12	.160	.156	- .202	- .196		-	.159	- .228	12
13	.168	.100	- .230	- .227		-	.221	- .244	13
14	.161	.058	- .219	- .230		-	.228	- .241	14
15	.148	.026	- .219	- .232		-	.228	- .246	15
16	.146	.012	- .238	- .221		-	.221	- .230	16
17 -	.110		- .114	- .123		-	.118	- .109	17
18 -	.096		- .115	- .118		-	.122	- .072	18
19 -	.095		- .120	- .122		-	.116	- .082	19
20 -	.100		- .123	- .134		-	.134	- .120	20
21 -	.146		- .165	- .161		-	.162	- .155	21
22 -	.138		- .170	- .170				- .220	22
23 -	.145			- .175		-	.173	- .234	23
24 -	.147		- .169	- .175		-	.176	- .248	24
25 -	.148		- .171	- .131		-	.034	- .232	25
26 -	.164		- .027	- .024			.020	- .205	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-9 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.374		.402	.415			.404	.366	1
2	.317		.410	.408			.402	.291	2
3	.313		.406	.402			.401	.253	3
4	.309		.360	.376			.355	.195	4
5	.210		.237	.293			.295	.132	5
6	.206		.217	.259			.259	.076	6
7	.201		.205	.244			.253	.041	7
8	.198		.208	.237			.242		8
9	.198		.185	.205			.226	.041	9
10	.144		.163	.188			.177	.041	10
11	.169		.163	.174			.167	.024	11
12	.084	.082	.122	.152			.228	.001	12
13	.090	.095	.095	.097			.113	-.018	13
14	.086	.092	.091	.108			.101	-.029	14
15	.081	.084	.093	.102			.096	-.035	15
16	.078	.084	.078	.111			.084	-.028	16
17	-.066		-.070	-.076		-.071	-.064		17
18	-.041		-.067	-.071		-.065	-.029		18
19	-.055		-.068	-.070		-.073	-.032		19
20	-.064		-.077	-.086		-.088	-.061		20
21	-.114		-.125	-.118		-.115	-.083		21
22	-.102		-.131	-.131			-.122		22
23	-.112			-.136		-.135	-.164		23
24	-.115		-.129	-.135		-.128	-.183		24
25	-.114		-.131	-.134		-.124	-.156		25
26	-.133		-.144	-.133		-.139	-.182		26

α=-6 δ=-30

1	.275		.286	.292			.286	.279	1
2	.232		.295	.288			.290	.207	2
3	.231		.295	.291			.289	.184	3
4	.232		.268	.262			.253	.142	4
5	.138		.162	.192			.191	.077	5
6	.137		.138	.166			.164	.038	6
7	.129		.129	.166			.372	.018	7
8	.124		.137	.443			.509		8
9	.124		.406	.492			.530	.291	9
10	.078		.443	.530			.526	.296	10
11	.105		.442	.539			.540	.271	11
12	.041	.224	.268	.557			.522	.243	12
13	.046	.198	.468	.580			.530	.288	13
14	.044	.004	.805	.867			.678	.470	14
15	.059	-.082	.856	1.092			.838	.637	15
16	.091	-.097	.750	1.047			.850	.644	16
17	-.014		-.017	-.019		-.014	-.003		17
18	-.006		-.015	-.010		-.015	.019		18
19	-.008		-.015	-.015		-.016	.010		19
20	-.024		-.027	-.032		-.032	-.017		20
21	-.076		-.085	-.071		-.072	-.029		21
22	-.075		-.092	-.084			-.029		22
23	-.077			-.087		-.085	-.050		23
24	-.080		-.090	-.091		-.089	-.082		24
25	-.079		-.098	-.099		-.095	-.005		25
26	-.103		-.114	-.113		-.107	.029		26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.279		.287	.292			.284	.285	1
2	.233		.300	.288			.287	.216	2
3	.234		.298	.289			.286	.198	3
4	.231		.270	.262			.249	.147	4
5	.137		.164	.192			.189	.101	5
6	.141		.142	.165			.162	.052	6
7	.135		.132	.163			.157	.027	7
8	.124		.139	.154			.144		8
9	.126		.114	.132			.137	.032	9
10	.084		.099	.136			.120	.024	10
11	.104		.099	.418			.395	.045	11
12	.047	.160	.396	.458			.424	.187	12
13	.052	.109	.543	.561			.534	.352	13
14	.049	.063	.564	.700			.672	.462	14
15	.037	-.069	.508	.726			.689	.417	15
16	.036	-.095	.458	.716			.673	.393	16
17	-.010		-.016	-.024			-.016	.004	17
18	-.001		-.013	-.019			-.019	.029	18
19	-.004		-.013	-.019			-.020	.022	19
20	-.020		-.028	-.035			-.036	-.003	20
21	-.073		-.085	-.077			-.076	-.022	21
22	-.069		-.090	-.089				-.028	22
23	-.072			-.092			-.089	-.044	23
24	-.076		-.089	-.094			-.094	-.078	24
25	-.076		-.097	-.104			-.101	-.051	25
26	-.101		-.114	-.115			-.110	-.088	26

α=-6 δ=-10

1	.281		.289	.299			.289	.273	1
2	.230		.302	.293			.295	.207	2
3	.234		.298	.294			.294	.192	3
4	.233		.274	.271			.255	.142	4
5	.139		.165	.197			.196	.081	5
6	.139		.144	.171			.166	.044	6
7	.134		.133	.164			.163	.017	7
8	.127		.139	.158			.149		8
9	.127		.112	.133			.139	.017	9
10	.082		.099	.123			.101	.013	10
11	.099		.099	.107			.102	-.001	11
12	.042	.044	.283	.193			.211	-.038	12
13	.041	.086	.293	.316			.308	.175	13
14	.038	.077	.247	.324			.310	.170	14
15	.028	-.010	.221	.321			.302	.146	15
16	.029	-.065	.193	.324			.296	.131	16
17	-.009		-.012	-.020			-.014	-.013	17
18	-.002		-.010	-.017			-.014	.017	18
19	-.006		-.010	-.017			-.016	.008	19
20	-.019		-.024	-.033			-.033	-.018	20
21	-.073		-.080	-.073			-.072	-.035	21
22	-.070		-.088	-.086				-.037	22
23	-.074			-.088			-.085	-.050	23
24	-.077		-.086	-.091			-.092	-.091	24
25	-.075		-.093	-.100			-.094	-.070	25
26	-.103		-.109	-.112			-.108	-.101	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.276		.283	.295			.286	.276	1
2	.225		.297	.286			.293	.207	2
3	.230		.294	.288			.291	.189	3
4	.228		.269	.267			.250	.137	4
5	.134		.160	.191			.191	.088	5
6	.127		.138	.166			.164	.045	6
7	.125		.127	.161			.160	.022	7
8	.119		.133	.153			.147		8
9	.120		.108	.129			.136	.013	9
10	.079		.096	.118			.098	.010	10
11	.098		.096	.101			.099 -	.001	11
12	.040	.024	.054	.081			.148 -	.033	12
13	.045	.031	.029	.036			.040 -	.044	13
14	.038	.029	.031	.041			.031 -	.050	14
15	.029	.022	.032	.035			.031 -	.051	15
16	.024	.017	.022	.033			.020 -	.050	16
17 -	.015		- .016	- .025			- .017 -	.005	17
18	.006		- .014	- .020			- .003	.013	18
19 -	.009		- .014	- .018			- .018	.009	19
20 -	.022		- .028	- .035			- .034 -	.017	20
21 -	.077		- .085	- .074			- .071 -	.031	21
22 -	.073		- .092	- .088			-	.036	22
23 -	.075		-	- .092			- .087 -	.055	23
24 -	.080		- .091	- .092			- .091 -	.091	24
25 -	.078		- .097	- .101			- .095 -	.065	25
26 -	.101		- .114	- .109			- .110 -	.106	26

α=-6 δ=10

1	.280		.290	.302			.294	.273	1
2	.230		.304	.293			.301	.209	2
3	.237		.298	.295			.298	.187	3
4	.233		.276	.273			.257	.138	4
5	.140		.165	.198			.199	.087	5
6	.140		.146	.176			.170	.046	6
7	.135		.133	.165			.174	.037	7
8	.126		.140	.164			.159		8
9	.126		.120	.152			.149	.022	9
10	.086		.105	.128			.113	.020	10
11	.104		.105	.114			.109	.003	11
12	.042	.027	- .073	- .056			.009 -	.120	12
13	.045	- .001	- .106	- .106			- .099 -	.148	13
14	.040	- .024	- .091	- .104			- .109 -	.143	14
15	.027	- .044	- .091	- .104			- .114 -	.109	15
16	.024	- .055	- .100	- .109			- .118 -	.079	16
17 -	.009		- .013	- .023			- .015 -	.017	17
18 -	.002		- .013	- .018			- .016	.009	18
19 -	.006		- .014	- .017			- .019	.004	19
20 -	.020		- .025	- .034			- .035 -	.015	20
21 -	.073		- .081	- .074			- .072 -	.032	21
22 -	.069		- .089	- .086			-	.044	22
23 -	.074			- .090			- .088 -	.064	23
24 -	.077		- .087	- .092			- .091 -	.104	24
25 -	.077		- .095	- .101			- .098 -	.070	25
26 -	.102		- .111	- .114			- .111 -	.105	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.286		.293	.305			.296	.287	1
2	.234		.307	.296			.301	.223	2
3	.240		.303	.296			.301	.198	3
4	.242		.279	.276			.260	.155	4
5	.145		.168	.201			.203	.102	5
6	.145		.151	.177			.172	.059	6
7	.143		.137	.170			.171	.029	7
8	.131		.146	.166			.161		8
9	.134		.121	.143			.150	.028	9
10	.088		.105	.129			.110	.027	10
11	.105		.104	.116			.110	.012	11
12	.047	.033	- .161	- .150		-	.108	- .189	12
13	.047	- .003	- .196	- .187		-	.186	- .205	13
14	.049	- .040	- .187	- .193		-	.191	- .196	14
15	.035	- .058	- .178	- .195		-	.200	- .150	15
16	.035	- .060	- .193	- .197		-	.197	- .147	16
17	- .010		- .014	- .024		-	.020	- .010	17
18	- .002		- .014	- .019		-	.019	.018	18
19	- .006		- .013	- .018		-	.018	.009	19
20	- .016		- .027	- .034		-	.037	- .014	20
21	- .072		- .082	- .077		-	.073	- .027	21
22	- .069		- .089	- .088				- .037	22
23	- .071			- .091		-	.091	- .056	23
24	- .074		- .087	- .092		-	.095	- .097	24
25	- .076		- .095	- .101		-	.101	- .070	25
26	- .099		- .111	- .114		-	.111	- .108	26

α=-6 δ=30

1	.287		.297	.311			.305	.278	1
2	.244		.313	.306			.308	.211	2
3	.241		.310	.306			.308	.186	3
4	.240		.283	.281			.269	.140	4
5	.146		.174	.207			.209	.088	5
6	.148		.153	.182			.182	.041	6
7	.140		.141	.179			.178	.020	7
8	.135		.148	.171			.165		8
9	.136		.126	.148			.157	.017	9
10	.094		.109	.132			.114	.019	10
11	.113		.109	.120			.118	.005	11
12	.037	.035	- .229	- .224		-	.192	- .242	12
13	.044	- .003	- .256	- .247		-	.243	- .250	13
14	.041	- .037	- .244	- .247		-	.234	- .205	14
15	.032	- .058	- .224	- .243		-	.225	- .227	15
16	.027	- .064	- .215	- .216		-	.216	- .244	16
17	- .010		- .009	- .022		-	.019	- .028	17
18	- .003		- .013	- .019		-	.020	.005	18
19	- .005		- .012	- .019		-	.017	.001	19
20	- .017		- .025	- .033		-	.037	- .023	20
21	- .070		- .083	- .075		-	.074	- .040	21
22	- .067		- .089	- .087				- .047	22
23	- .071			- .091		-	.092	- .076	23
24	- .074		- .088	- .091			.023	- .115	24
25	- .073		- .068	.088			.118	- .078	25
26	- .099		.101	.100			.157	- .113	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-3 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.191		.194	.204			.198	.183	1
2	.165		.202	.180			.200	.134	2
3	.161		.205	.198			.201	.124	3
4	.164		.184	.182			.167	.093	4
5	.079		.090	.109			.117	.047	5
6	.019		.078	.080			.087	.022	6
7	.048		.059	.088			.077	- .001	7
8	.062		.072	.085			.068		8
9	.066		.051	.052			.068	- .004	9
10	.032		.042	.055			.035	- .005	10
11	.043		.042	.044			.045	- .012	11
12 -	.006	- .019	.005	.029			.087	- .036	12
13 -	.004	- .018	- .014	- .015		-	.015	- .045	13
14 -	.003	- .019	- .020	- .005		-	.017	- .063	14
15 -	.019	- .019	- .015	- .008		-	.020	- .058	15
16 -	.020	- .023	- .019	- .018		-	.028	- .044	16
17	.054		.050	.047			.051	.051	17
18	.103		.054	.050			.155	.065	18
19	.044		.052	.054			.049	.046	19
20	.032		.037	.033			.032	.023	20
21 -	.030		- .029	- .015		-	.009	.008	21
22 -	.026		- .038	- .031				.006	22
23 -	.028			- .036		-	.028	.001	23
24 -	.031		- .039	- .037		-	.028	- .010	24
25 -	.027		- .045	- .042		-	.035	.005	25
26 -	.049		- .067	- .044		-	.053	- .017	26

α=0 δ=-30

1	.101		.105	.123			.104	.103	1
2	.088		.115	.119			.111	.080	2
3	.081		.117	.107			.114	.085	3
4	.080		.102	.096			.085	.060	4
5	.006		.027	.038			.039	.024	5
6	.009		.013	.014			.021	.018	6
7	.001		- .002	.019			.014	.001	7
8 -	.001		.005	.019			.193		8
9 -	.003		.032	.299			.312	.231	9
10 -	.031		.257	.329			.318	.248	10
11 -	.025			.329			.334	.231	11
12 -	.052	.065	.169	.353			.331	.194	12
13 -	.056	.064	.311	.380			.334	.227	13
14 -	.050	- .092	.619	.648			.543	.429	14
15 -	.064	- .144	.645	.812			.716	.499	15
16 -	.051	- .140	.581	.812			.734	.482	16
17	.108		.118	.104			.112	.104	17
18	.092		.112	.109			.113	.103	18
19	.082		.112	.118			.117	.078	19
20	.071		.088	.094			.088	.051	20
21	.002		.020	.036			.038	.017	21
22	.011		.011	.018				.015	22
23	.007			.018			.017	.013	23
24	.001		- .004	.017			.015	.000	24
25	.004		- .012	.007			.009	.017	25
26 -	.035		- .033	- .015		-	.013	.047	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=0 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.117		.116	.124			.109	.107	1
2	.088		.123	.124			.116	.082	2
3	.100		.125	.112			.116	.084	3
4	.094		.108	.100			.087	.057	4
5	.019		.036	.046			.045	.023	5
6	.022		.022	.020			.021	.018	6
7	.019		.010	.022			.014	.000	7
8	.014		.015	.018			.002		8
9	.015		.004	.007			.012	.006	9
10 -	.017		- .004	- .004			.014	.010	10
11 -	.012			.177			.182	.009	11
12 -	.050	.011	.215	.237			.220	.159	12
13 -	.057	- .010	.355	.348			.331	.327	13
14 -	.052	- .045	.358	.446			.428	.322	14
15 -	.071	- .141	.317	.460			.434	.261	15
16 -	.070	- .135	.278	.460			.428	.237	16
17	.123		.126	.116			.121	.104	17
18	.102		.122	.109			.118	.101	18
19	.092		.123	.121			.114	.079	19
20	.082		.097	.096			.096	.047	20
21	.013		.024	.037			.036	.019	21
22	.022		.016	.020				.013	22
23	.016			.017			.016	.011	23
24	.013		.007	.018			.014 -	.001	24
25	.013		- .004	.002			.002	.014	25
26 -	.025		- .025	- .013			- .014	.001	26

α=0 δ=-10

1	.108		.110	.125			.116	.108	1
2	.094		.117	.118			.118	.084	2
3	.090		.123	.113			.119	.088	3
4	.090		.107	.099			.086	.061	4
5	.015		.031	.042			.048	.025	5
6	.019		.016	.015			.024	.020	6
7	.010		.006	.022			.019	.004	7
8	.005		.011	.017			.010		8
9	.006		- .001	.004			.003	.008	9
10 -	.023		- .020	- .006			- .018	.011	10
11 -	.012			- .021			.001 -	.001	11
12 -	.050	- .059	.104	.043			.037 -	.001	12
13 -	.054	- .029	.135	.136			.126	.144	13
14 -	.050	- .034	.106	.150			.132	.097	14
15 -	.065	- .085	.085	.152			.135	.060	15
16 -	.068	- .106	.064	.150			.131	.048	16
17	.111		.123	.110			.122	.110	17
18	.095		.118	.114			.115	.104	18
19	.090		.116	.119			.119	.082	19
20	.079		.094	.096			.097	.050	20
21	.006		.026	.039			.041	.019	21
22	.014		- .001	.020				.015	22
23	.013			.015			.020	.017	23
24	.006		- .001	.016			.012	.001	24
25	.008		- .012	.004			.006	.020	25
26 -	.026		- .033	- .014			- .013	.003	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.122		.121	.128			.119	.110	1
2	.096		.126	.123			.124	.087	2
3	.106		.130	.119			.123	.088	3
4	.099		.111	.105			.092	.066	4
5	.024		.042	.053			.051	.029	5
6	.025		.021	.026			.026	.019	6
7	.019		.009	.022			.022	.001	7
8	.010		.015	.017			.014		8
9	.012		.001	.003			.010	.006	9
10	-.017		-.009	-.007		-.017	-.009		10
11	-.008			-.018			-.001	-.003	11
12	-.050	-.070	-.042	-.032			-.024	-.023	12
13	-.055	-.066	-.062	-.061		-.064	-.034		13
14	-.050	-.065	-.066	-.057		-.068	-.033		14
15	-.061	-.070	-.062	-.060		-.070	-.033		15
16	-.069	-.068	-.068	-.065		-.074	-.025		16
17	.121		.127	.095			.120	.104	17
18	.106		.121	.114			.123	.102	18
19	.100		.123	.114			.115	.080	19
20	.084		.100	.095			.094	.047	20
21	.012		.028	.040			.040	.019	21
22	.024		.014	.023				.013	22
23	.025			.018			.024	.014	23
24	.017		.007	.020			.019	.003	24
25	.018		.002	.006			.013	.019	25
26	-.019		-.030	-.012		-.006		.003	26

$\alpha=0$ $\delta=10$

1	.113		.109	.122			.119	.120	1
2	.096		.121	.121			.119	.092	2
3	.093		.123	.112			.122	.097	3
4	.087		.107	.101			.089	.074	4
5	.014		.033	.044			.046	.038	5
6	.019		.019	.022			.024	.029	6
7	.009		.007	.021			.021	.011	7
8	-.001		.012	.018			.011		8
9	.008		-.004	-.002			.012	.015	9
10	-.024		-.012	-.010		-.015	.017		10
11	-.020			-.019		-.001	.006		11
12	-.045	-.069	-.147	-.138		-.093	-.125		12
13	-.048	-.088	-.178	-.177		-.180	-.154		13
14	-.045	-.106	-.172	-.186		-.183	-.111		14
15	-.057	-.117	-.163	-.185		-.190	-.116		15
16	-.062	-.104	-.152	-.187		-.195	-.173		16
17	.112		.127	.104			.115	.112	17
18	.099		.117	.110			.115	.111	18
19	.094		.117	.119			.114	.087	19
20	.074		.097	.097			.091	.052	20
21	.010		.028	.039			.037	.025	21
22	.015		.012	.018				.022	22
23	.010			.017			.016	.022	23
24	.011		.006	.017			.010	.010	24
25	.007		-.006	.003			.004	.023	25
26	-.028		-.032	-.014		-.019		.009	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=0 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.118		.115	.129			.117	.118	1
2	.099		.123	.123			.119	.096	2
3	.102		.126	.115			.118	.098	3
4	.095		.109	.102			.090	.075	4
5	.020		.039	.041			.048	.033	5
6	.015		.020	.021			.017	.028	6
7	.020		.007	.020			.020	.010	7
8	.013		.014	.017			.005		8
9	.014		-.002	-.001			.012	.013	9
10 -	.011		-.010	-.011		-	.022	.018	10
11 -	.006			-.019			.002	.019	11
12 -	.045	- .068	- .215	- .206		-	.180	- .201	12
13 -	.048	- .094	- .240	- .238		-	.237	- .195	13
14 -	.043	- .117	- .238	- .245		-	.233	- .191	14
15 -	.060	- .127	- .210	- .233		-	.217	- .248	15
16 -	.059	- .120	- .208	- .191		-	.197	- .270	16
17	.120		.120	.102			.102	.106	17
18	.102		.121	.110			.110	.107	18
19	.096		.119	.114			.103	.083	19
20	.084		.093	.092			.082	.056	20
21	.017		.026	.031			.031	.024	21
22	.016		.012	.012				.020	22
23	.022			.005			.012	.023	23
24	.013		.007	.012			.003	.008	24
25	.013		-.004	-.002		-	.008	.024	25
26 -	.023		- .025	- .020		-	.024	.011	26

α=0 δ=30

1	.120		.111	.127			.116	.120	1
2	.101		.118	.123			.123	.090	2
3	.106		.125	.115			.119	.094	3
4	.098		.110	.098			.089	.071	4
5	.025		.036	.043			.048	.029	5
6	.021		.021	.023			.019	.023	6
7	.020		.006	.022			.015	.008	7
8	.014		.013	.018		-	.001		8
9	.015		.002	.002			.006	.011	9
10 -	.018		- .010	- .010		-	.023	.098	10
11 -	.011			- .021			.001	.116	11
12 -	.048	- .068	- .260	- .255		-	.237	- .237	12
13 -	.052	- .097	- .259	- .262		-	.246	- .187	13
14 -	.047	- .116	- .250	- .254		-	.240	- .254	14
15 -	.060	- .125	- .231	- .241		-	.232	- .282	15
16 -	.066	- .118	- .231	- .236		-	.236	- .283	16
17	.119		.121	.100			.107	.099	17
18	.103		.118	.104			.108	.102	18
19	.096		.121	.112			.108	.078	19
20	.077		.099	.087			.083	.050	20
21	.015		.026	.030			.028	.022	21
22	.018		.009	.014				.014	22
23	.018			.007			.015	.033	23
24	.011		.005	.130			.282	.055	24
25	.007		.174	.307			.298	.214	25
26 -	.028		.264	.326			.312	.262	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=3$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.030		.029	.034			.033	.041	1
2	.013		.026	.031			.029	.037	2
3	.023		.034	.026			.034	.049	3
4	.020		.019	.014			.010	.031	4
5	-.051		-.046	-.034			-.027	.000	5
6	-.046		-.056	-.053			-.049	-.004	6
7	-.048		-.062	-.055			-.052	-.019	7
8	-.056		-.059	-.057			-.060		8
9	-.059		-.070	-.069			-.065	-.019	9
10	-.078		-.070	-.076			-.083	-.019	10
11	-.074		-.070	-.081			-.051	-.035	11
12	-.099	-.123	-.088	-.090			-.111	-.047	12
13	-.101	-.120	-.108	-.113			-.110	-.076	13
14	-.099	-.116	-.106	-.108			-.113	-.081	14
15	-.106	-.122	-.110	-.109			-.118	-.109	15
16	-.109	-.118	-.114	-.113			-.118	-.124	16
17	.186		.190	.181			.186	.178	17
18	.150		.195	.184			.189	.160	18
19	.143		.191	.194			.186	.127	19
20	.133		.162	.164			.157	.088	20
21	.053		.071	.099			.104	.046	21
22	.058		.060	.080				.028	22
23	.058			.074			.079	.019	23
24	.048		.050	.072			.070	.001	24
25	.048		.039	.057			.059	.022	25
26	.004		.011	.034			.037	.000	26

$\alpha=6$ $\delta=-30$

1	-.032		-.033	-.029			-.033	-.023	1
2	-.025		-.032	-.033			-.033	-.006	2
3	-.027		-.027	-.033			-.032	.004	3
4	-.023		-.040	-.043			-.056	-.012	4
5	-.087		-.099	-.087			-.086	-.041	5
6	-.085		-.103	-.104			-.103	-.059	6
7	-.099		-.113	-.101			-.087	-.097	7
8	-.096		-.106	-.091			-.086		8
9	-.097		-.095	-.090			-.098	-.105	9
10	-.113		.062	.114			.131	-.105	10
11	-.111		.062	.129			.161	-.091	11
12	-.118	-.055	.099	.157			.163	-.014	12
13	-.122	-.069	.183	.180			.165	.590	13
14	-.122	-.151	.388	.388			.323	.170	14
15	-.129	-.187	.384	.481			.440	.332	15
16	-.129	-.177	.344	.497			.453	.378	16
17	.293		.300	.293			.300	.282	17
18	.237		.319	.297			.304	.251	18
19	.235		.299	.305			.301	.193	19
20	.221		.270	.268			.266	.151	20
21	.133		.160	.198			.198	.095	21
22	.136		.141	.175				.069	22
23	.136			.167			.170	.045	23
24	.130		.131	.161			.164	.013	24
25	.127		.115	.144			.154	.044	25
26	.073		.087	.119			.123	.022	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.028		-.035	-.030			-.032	-.050	1
2	-.024		-.033	-.034			-.034	-.036	2
3	-.024		-.029	-.034			-.031	-.024	3
4	-.024		-.040	-.047			-.052	-.040	4
5	-.087		-.099	-.090			-.085	-.069	5
6	-.086		-.099	-.106			-.103	-.086	6
7	-.093		-.111	-.105			-.105	-.125	7
8	-.095		-.107	-.104			-.113		8
9	-.095		-.114	-.118			-.113	-.141	9
10	-.110		-.109	-.123			-.130	-.148	10
11	-.109		-.109	-.010			.041	-.154	11
12	-.142	-.099	.052	.063			.069	-.065	12
13	-.147	-.113	.156	.142			.138	-.224	13
14	-.147	-.136	.183	.223			.234	-.018	14
15	-.154	-.175	.154	.233			.250	.049	15
16	-.155	-.179	.118	.241			.257	.108	16
17	.294		.304	.289			.297	.255	17
18	.241		.315	.295			.301	.224	18
19	.233		.297	.304			.298	.172	19
20	.222		.268	.270			.261	.124	20
21	.132		.161	.194			.191	.069	21
22	.135		.138	.171				.052	22
23	.137			.164			.169	.026	23
24	.130		.131	.158			.162	-.006	24
25	.129		.114	.144			.151	.022	25
26	.073		.085	.113			.123	-.004	26

α=6 δ=-10

1	-.032		-.033	-.028			-.030	-.041	1
2	-.030		-.033	-.033			-.033	-.027	2
3	-.023		-.031	-.035			-.031	-.015	3
4	-.024		-.040	-.046			-.052	-.029	4
5	-.087		-.101	-.091			-.086	-.063	5
6	-.083		-.099	-.106			-.102	-.079	6
7	-.089		-.112	-.103			-.104	-.110	7
8	-.094		-.107	-.105			-.112		8
9	-.094		-.114	-.115			-.116	-.131	9
10	-.111		-.107	-.123			-.129	-.137	10
11	-.108		-.107	-.128			-.076	-.154	11
12	-.137	-.137	-.047	-.063			-.059	-.110	12
13	-.142	-.118	-.004	-.017			-.015	-.013	13
14	-.142	-.123	-.019	.003			.012	-.109	14
15	-.150	-.123	-.033	.004			.014	-.113	15
16	-.152	-.146	-.052	.000			.019	-.093	16
17	.291		.301	.291			.295	.264	17
18	.234		.314	.296			.299	.230	18
19	.233		.295	.303			.296	.177	19
20	.219		.267	.267			.259	.132	20
21	.130		.158	.196			.194	.074	21
22	.134		.139	.169				.054	22
23	.135			.165			.166	.028	23
24	.128		.130	.158			.158	.004	24
25	.128		.110	.139			.150	.027	25
26	.073		.084	.115			.118	.003	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .032		- .035	- .033			- .033	- .023	1
2	- .022		- .034	- .033			- .031	- .012	2
3	- .026		- .032	- .038			- .031	- .001	3
4	- .024		- .040	- .051			- .051	- .006	4
5	- .087		- .103	- .093			- .086	- .037	5
6	- .082		- .103	- .104			- .102	- .054	6
7	- .091		- .111	- .107			- .103	- .092	7
8	- .095		- .108	- .107			- .110		8
9	- .095		- .115	- .118			- .116	- .105	9
10	- .114		- .107	- .123			- .125	- .114	10
11	- .109		- .108	- .129			- .085	- .134	11
12	- .127	- .146	- .128	- .133			- .101	- .133	12
13	- .129	- .146	- .142	- .155			- .150	- .152	13
14	- .129	- .141	- .142	- .148			- .148	- .178	14
15	- .141	- .143	- .142	- .150			- .146	- .174	15
16	- .141	- .143	- .145	- .150			- .147	- .168	16
17	.286		.296	.287			.292	.278	17
18	.233		.308	.295			.296	.244	18
19	.231		.293	.301			.295	.188	19
20	.217		.263	.266			.259	.146	20
21	.129		.155	.192			.191	.090	21
22	.134		.135	.169				.067	22
23	.133			.163			.164	.041	23
24	.128		.127	.156			.154	.017	24
25	.124		.106	.139			.145	.038	25
26	.072		.079	.111			.119	.018	26

α=6 δ=10

1	- .027		- .030	- .022			- .023	- .023	1
2	- .023		- .027	- .028			- .029	- .009	2
3	- .021		- .024	- .028			- .025	- .003	3
4	- .016		- .034	- .042			- .047	- .014	4
5	- .082		- .094	- .082			- .081	- .044	5
6	- .084		- .097	- .100			- .100	- .058	6
7	- .088		- .103	- .099			- .099	- .095	7
8	- .093		- .101	- .097			- .105		8
9	- .091		- .109	- .111			- .100	- .111	9
10	- .107		- .093	- .109			- .110	- .119	10
11	- .106		- .094	- .112			- .071	- .133	11
12	- .124	- .147	- .195	- .189			- .155	- .184	12
13	- .128	- .157	- .212	- .214			- .207	- .187	13
14	- .129	- .170	- .207	- .215			- .209	- .206	14
15	- .140	- .178	- .201	- .216			- .215	- .212	15
16	- .140	- .151	- .160	- .172			- .197	- .220	16
17	.296		.305	.295			.293	.274	17
18	.238		.317	.295			.298	.239	18
19	.239		.303	.303			.296	.189	19
20	.224		.271	.270			.263	.145	20
21	.134		.164	.198			.192	.084	21
22	.139		.145	.174				.067	22
23	.139			.166			.166	.038	23
24	.132		.136	.162			.160	.015	24
25	.129		.116	.145			.150	.037	25
26	.078		.090	.116			.118	.017	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 6$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.022		-.025	-.017			-.024	-.017	1
2	-.022		-.024	-.022			-.024	-.003	2
3	-.019		-.018	-.020			-.023	.006	3
4	-.015		-.029	-.036			-.044	-.010	4
5	-.077		-.090	-.077			-.076	-.040	5
6	-.076		-.090	-.095			-.097	-.047	6
7	-.085		-.100	-.098			-.098	-.087	7
8	-.085		-.097	-.099			-.104		8
9	-.087		-.102	-.109			-.099	-.109	9
10	-.104		-.096	-.115			-.122	-.108	10
11	-.102		-.097	-.119			-.075	-.091	11
12	-.120	-.151	-.239	-.238			-.216	-.237	12
13	-.127	-.168	-.255	-.261			-.260	-.243	13
14	-.128	-.183	-.230	-.233			-.243	-.265	14
15	-.138	-.179	-.210	-.220			-.227	-.266	15
16	-.134	-.154	-.209	-.210			-.218	-.264	16
17	.297		.308	.291			.295	.275	17
18	.245		.322	.295			.300	.239	18
19	.242		.303	.304			.296	.186	19
20	.226		.273	.267			.261	.150	20
21	.138		.165	.197			.198	.092	21
22	.144		.146	.174				.064	22
23	.145			.164			.167	.045	23
24	.140		.139	.160			.164	.022	24
25	.135		.118	.146			.150	.040	25
26	.083		.092	.120			.122	.014	26

$\alpha = 6$ $\delta = 30$

1	-.025		-.032	-.023			-.027	.001	1
2	-.017		-.028	-.030			-.028	.015	2
3	-.022		-.023	-.029			-.027	.022	3
4	-.018		-.033	-.040			-.050	.006	4
5	-.081		-.094	-.084			-.081	-.019	5
6	-.079		-.097	-.100			-.098	-.031	6
7	-.088		-.104	-.103			-.100	-.068	7
8	-.091		-.101	-.103			-.107		8
9	-.091		-.108	-.114			-.101	-.046	9
10	-.110		-.102	-.121			-.126	.040	10
11	-.108		-.103	-.123			-.079	-.061	11
12	-.110	-.155	-.244	-.248			-.255	-.274	12
13	-.114	-.178	-.241	-.253			-.256	-.274	13
14	-.114	-.189	-.232	-.238			-.248	-.280	14
15	-.122	-.179	-.225	-.236			-.243	-.278	15
16	-.123	-.157	-.232	-.230			-.248	-.273	16
17	.292		.301	.285			.287	.291	17
18	.237		.313	.292			.293	.260	18
19	.235		.298	.298			.294	.206	19
20	.221		.268	.262			.253	.164	20
21	.131		.159	.193			.186	.102	21
22	.137		.138	.168				.081	22
23	.138			.183			.459	.059	23
24	.131		.132	.503			.536	.136	24
25	.129		.430	.539			.548	.335	25
26	.076		.448	.548			.549	.344	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.075		-.065	-.077			-.073	-.054	1
2	-.061		-.079	-.074			-.075	-.029	2
3	-.064		-.074	-.082			-.076	-.017	3
4	-.062		-.080	-.096			-.095	-.031	4
5	-.122		-.133	-.128			-.121	-.059	5
6	-.107		-.138	-.137			-.135	-.118	6
7	-.114		-.144	-.139			-.135	-.159	7
8	-.128		-.145	-.140			-.143		8
9	-.126		-.145	-.147			-.147	-.159	9
10	-.140		-.133	-.155			-.158	-.151	10
11	-.141		-.133	-.159			-.102	-.151	11
12	-.141	-.177	-.155	-.159			-.136	-.193	12
13	-.150	-.178	-.164	-.179			-.178	-.205	13
14	-.147	-.177	-.173	-.178			-.168	-.207	14
15	-.155	-.177	-.169	-.175			-.170	-.224	15
16	-.159	-.174	-.168	-.175			-.169	-.219	16
17	.389		.417	.402			.409	.390	17
18	.319		.427	.410			.409	.342	18
19	.313		.409	.418			.406	.271	19
20	.300		.354	.382			.368	.221	20
21	.201		.231	.293			.296	.152	21
22	.206		.212	.260				.120	22
23	.207			.243			.261	.097	23
24	.201		.204	.235			.253	.068	24
25	.196		.182	.218			.240	.095	25
26	.137		.153	.187			.201	.068	26

$\alpha = 12$ $\delta = -30$

1	-.123		-.127	-.113			-.120	-.097	1
2	-.101		-.122	-.122			-.123	-.081	2
3	-.104		-.122	-.121			-.122	-.068	3
4	-.099		-.126	-.134			-.141	-.097	4
5	-.154		-.173	-.164			-.164	-.140	5
6	-.146		-.171	-.177			-.178	-.216	6
7	-.158		-.181	-.179			-.179	-.241	7
8	-.160		-.179	-.177			-.185		8
9	-.157		-.183	-.175			-.034	-.239	9
10	-.169		-.038	-.014			-.005	-.228	10
11	-.170		-.038	.009			.050	-.191	11
12	-.172	-.123	.003	.040			.041	-.133	12
13	-.178	-.146	.032	.040			.033	-.038	13
14	-.175	-.189	.239	.210			.170	-.070	14
15	-.182	-.225	.266	.300			.292	-.164	15
16	-.166	-.219	.233	.330			.326	-.188	16
17	.479		.588	.547			.559	.516	17
18	.398		.552	.548			.546	.439	18
19	.401		.518	.554			.545	.355	19
20	.382		.440	.497			.495	.301	20
21	.278		.308	.381			.413	.219	21
22	.281		.295	.338				.169	22
23	.281			.319			.363	.143	23
24	.275		.279	.309			.343	.114	24
25	.269		.259	.290			.315	.145	25
26	.204		.223	.255			.271	.110	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.116		-.121	-.113			-.118	-.091	1
2	-.095		-.117	-.118			-.121	-.069	2
3	-.097		-.118	-.120			-.119	-.055	3
4	-.094		-.123	-.132			-.142	-.086	4
5	-.146		-.167	-.163			-.162	-.128	5
6	-.139		-.166	-.173			-.176	-.201	6
7	-.147		-.178	-.178			-.177	-.233	7
8	-.155		-.176	-.175			-.182		8
9	-.152		-.179	-.184			-.184	-.224	9
10	-.164		-.157	-.191			-.193	-.220	10
11	-.164		-.157	-.157			-.060	-.197	11
12	-.163	-.161	-.049	-.042			-.031	-.169	12
13	-.169	-.169	.028	.014			.008	-.125	13
14	-.170	-.182	.060	.065			.092	-.152	14
15	-.177	-.198	.045	.076			.105	-.189	15
16	-.172	-.220	.024	.081			.114	-.216	16
17	.483		.592	.549			.558	.518	17
18	.403		.558	.551			.543	.443	18
19	.404		.518	.554			.537	.361	19
20	.389		.442	.495			.493	.301	20
21	.282		.310	.383			.407	.225	21
22	.286		.296	.338				.180	22
23	.287			.322			.364	.152	23
24	.280		.281	.312			.345	.123	24
25	.275		.258	.289			.315	.152	25
26	.209		.224	.254			.269	.118	26

α=12 δ=-10

1	-.119		-.122	-.115			-.113	-.102	1
2	-.099		-.119	-.120			-.118	-.073	2
3	-.099		-.117	-.120			-.117	-.063	3
4	-.095		-.121	-.132			-.137	-.091	4
5	-.150		-.166	-.164			-.160	-.133	5
6	-.141		-.167	-.172			-.173	-.206	6
7	-.154		-.176	-.175			-.172	-.230	7
8	-.158		-.176	-.174			-.180		8
9	-.156		-.178	-.183			-.181	-.228	9
10	-.167		-.157	-.188			-.192	-.225	10
11	-.167		-.157	-.192			-.115	-.206	11
12	-.170	-.198	-.129	-.132			-.114	-.200	12
13	-.175	-.184	-.101	-.120			-.105	-.196	13
14	-.175	-.183	-.109	-.110			-.084	-.223	14
15	-.186	-.160	-.115	-.109			-.081	-.233	15
16	-.175	-.201	-.124	-.100			-.077	-.207	16
17	.477		.588	.545			.553	.512	17
18	.400		.554	.548			.542	.438	18
19	.402		.515	.552			.538	.351	19
20	.384		.438	.494			.490	.300	20
21	.279		.309	.380			.406	.215	21
22	.284		.294	.337				.170	22
23	.284			.321			.361	.148	23
24	.278		.276	.310			.340	.114	24
25	.271		.255	.288			.314	.143	25
26	.205		.222	.254			.268	.111	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.115		-.121	-.113			-.115	-.111	1
2	-.097		-.117	-.113			-.117	-.095	2
3	-.099		-.114	-.120			-.116	-.079	3
4	-.094		-.119	-.133			-.134	-.105	4
5	-.149		-.165	-.162			-.157	-.145	5
6	-.135		-.165	-.170			-.171	-.212	6
7	-.146		-.172	-.172			-.168	-.236	7
8	-.157		-.175	-.172			-.177		8
9	-.153		-.176	-.178			-.179	-.237	9
10	-.166		-.157	-.185			-.187	-.227	10
11	-.168		-.159	-.189			-.123	-.212	11
12	-.183	-.192	-.197	-.193			-.163	-.216	12
13	-.188	-.197	-.201	-.211			-.206	-.234	13
14	-.188	-.193	-.201	-.211			-.191	-.236	14
15	-.193	-.193	-.201	-.211			-.192	-.242	15
16	-.187	-.186	-.198	-.205			-.193	-.232	16
17	.481		.588	.545			.552	.497	17
18	.400		.558	.546			.539	.420	18
19	.403		.516	.554			.537	.339	19
20	.384		.436	.495			.491	.279	20
21	.278		.308	.381			.405	.201	21
22	.284		.295	.335				.159	22
23	.286			.320			.361	.128	23
24	.279		.278	.308			.341	.100	24
25	.272		.255	.286			.312	.132	25
26	.207		.223	.253			.267	.099	26

α=12 δ=10

1	-.117		-.120	-.110			-.114	-.099	1
2	-.098		-.116	-.118			-.118	-.072	2
3	-.096		-.117	-.117			-.116	-.058	3
4	-.093		-.120	-.129			-.133	-.079	4
5	-.146		-.164	-.161			-.158	-.127	5
6	-.138		-.163	-.171			-.174	-.201	6
7	-.150		-.175	-.174			-.172	-.234	7
8	-.154		-.173	-.172			-.179		8
9	-.150		-.176	-.179			-.163	-.242	9
10	-.164		-.143	-.169			-.166	-.223	10
11	-.164		-.143	-.173			-.112	-.192	11
12	-.168	-.201	-.221	-.219			-.195	-.238	12
13	-.175	-.212	-.238	-.243			-.233	-.241	13
14	-.177	-.220	-.210	-.221			-.224	-.248	14
15	-.182	-.214	-.184	-.193			-.220	-.260	15
16	-.173	-.186	-.169	-.183			-.187	-.259	16
17	.482		.586	.543			.549	.502	17
18	.400		.555	.546			.540	.433	18
19	.403		.516	.551			.535	.353	19
20	.386		.439	.492			.490	.300	20
21	.280		.306	.378			.402	.219	21
22	.285		.295	.335				.172	22
23	.285			.314			.359	.143	23
24	.278		.279	.308			.340	.116	24
25	.274		.257	.285			.310	.140	25
26	.207		.221	.252			.266	.110	26

TABLE XII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.115		-.121	-.114			-.112	-.099	1
2	-.096		-.119	-.120			-.116	-.072	2
3	-.097		-.118	-.120			-.114	-.060	3
4	-.094		-.123	-.132			-.132	-.088	4
5	-.147		-.169	-.164			-.156	-.131	5
6	-.140		-.169	-.173			-.171	-.202	6
7	-.147		-.179	-.176			-.170	-.232	7
8	-.152		-.178	-.175			-.177		8
9	-.152		-.181	-.182			-.169	-.230	9
10	-.164		-.160	-.185			-.186	-.205	10
11	-.165		-.160	-.187			-.117	-.174	11
12	-.169	-.196	-.253	-.261			-.247	-.260	12
13	-.175	-.210	-.250	-.260			-.262	-.262	13
14	-.172	-.218	-.234	-.238			-.244	-.264	14
15	-.180	-.198	-.239	-.221			-.243	-.259	15
16	-.154	-.173	-.244	-.212			-.225	-.252	16
17	.483		.583	.538			.546	.506	17
18	.401		.556	.545			.534	.433	18
19	.404		.516	.546			.534	.349	19
20	.387		.438	.490			.488	.294	20
21	.282		.305	.376			.403	.219	21
22	.286		.292	.333				.170	22
23	.286			.314			.357	.145	23
24	.278		.276	.306			.341	.119	24
25	.272		.255	.289			.312	.145	25
26	.208		.396	.657			.645	.251	26

α=12 δ=30

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.118		-.121	-.110			-.114	-.111	1
2	-.098		-.118	-.117			-.117	-.088	2
3	-.098		-.116	-.117			-.117	-.073	3
4	-.095		-.121	-.131			-.136	-.095	4
5	-.150		-.165	-.160			-.160	-.138	5
6	-.143		-.165	-.171			-.172	-.220	6
7	-.153		-.175	-.175			-.173	-.237	7
8	-.158		-.174	-.175			-.180		8
9	-.153		-.178	-.183			-.171	-.230	9
10	-.167		-.158	-.187			-.191	-.196	10
11	-.167		-.158	-.188			-.113	-.182	11
12	-.175	-.200	-.268	-.252			-.268	-.282	12
13	-.179	-.216	-.264	-.251			-.276	-.283	13
14	-.180	-.220	-.256	-.241			-.257	-.280	14
15	-.188	-.206	-.271	-.241			-.248	-.275	15
16	-.104	-.182	-.268	-.238			-.246	-.271	16
17	.481		.586	.537			.540	.493	17
18	.399		.555	.542			.530	.420	18
19	.402		.517	.544			.530	.337	19
20	.385		.440	.490			.484	.284	20
21	.280		.311	.378			.399	.209	21
22	.284		.295	.331				.159	22
23	.284			.716			.773	.384	23
24	.276		.514	.760			.791	.398	24
25	.272		.652	.773			.798	.453	25
26	.205		.634	.772			.794	.445	26

TABLE XII.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 3.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .156		- .163	- .151			- .154	- .143	1
2	- .137		- .158	- .153			- .156	- .123	2
3	- .134		- .153	- .157			- .158	- .124	3
4	- .136		- .160	- .168			- .173	- .175	4
5	- .177		- .196	- .196			- .189	- .205	5
6	- .164		- .196	- .199			- .202	- .251	6
7	- .173		- .204	- .206			- .201	- .269	7
8	- .184		- .207	- .207			- .209		8
9	- .180		- .208	- .210			- .207	- .256	9
10	- .191		- .181	- .216			- .216	- .238	10
11	- .192		- .180	- .220			- .137	- .229	11
12	- .205	- .218	- .221	- .221			- .200	- .252	12
13	- .212	- .220	- .229	- .242			- .233	- .261	13
14	- .211	- .223	- .225	- .238			- .215	- .273	14
15	- .214	- .221	- .228	- .242			- .218	- .270	15
16	- .173	- .154	- .151	- .191			- .207	- .261	16
17	.585		.773	.797			.817	.698	17
18	.493		.695	.750			.788	.576	18
19	.514		.622	.697			.734	.479	19
20	.486		.539	.588			.633	.384	20
21	.371		.399	.462			.508	.271	21
22	.379		.378	.422				.214	22
23	.378			.407			.432	.186	23
24	.368		.365	.397			.409	.155	24
25	.362		.347	.376			.378	.186	25
26	.288		.313	.337			.332	.142	26

TABLE XIII

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.549		.744	.784			.794	.717	1
2	.467		.653	.731			.773	.591	2
3	.487		.602	.686			.739	.498	3
4	.485		.529	.591			.616	.368	4
5	.360		.392	.455			.518	.282	5
6	.361		.362	.419			.465	.181	6
7	.350		.357	.402			.429	.151	7
8	.336		.359	.396			.406		8
9	.343		.334	.364			.362	.142	9
10	.282		.295	.336			.306	.142	10
11	.313		.295	.323			.298	.108	11
12	.220		.199	.209			.206	.044	12
13	.197		.190	.191			.188	.026	13
14	.177		.190	.209			.190	.026	14
15	.190		.195	.205			.178	.026	15
16	.168		.179	.208			.163	.012	16
17	-.173		-.169	-.165			-.150	-.142	17
18	-.145		-.177	-.166			-.149	-.105	18
19	-.145		-.174	-.164			-.154	-.131	19
20	-.153		-.178	-.175			-.166	-.158	20
21	-.193		-.216	-.205			-.196	-.195	21
22	-.189		-.223	-.208				-.252	22
23	-.194			-.212			-.203	-.264	23
24	-.201		-.218	-.207			-.205	-.282	24
25	-.197		-.208	-.200			-.198	-.250	25
26	-.194		-.225	-.202			-.199	-.257	26

α=-12 δ=-30

1	.462		.572	.563			.537	.525	1
2	.377		.542	.549			.523	.423	2
3	.386		.516	.553			.541	.368	3
4	.388		.447	.502			.482	.296	4
5	.276		.311	.384			.408	.219	5
6	.282		.294	.342			.368	.158	6
7	.493		.545	.703			.557	.127	7
8	.675		.665	.741			.730		8
9	.696		.703	.729			.756	.414	9
10	.703		.717	.767			.758	.437	10
11	.715		.717	.783			.762	.410	11
12	.735		.755	.794			.772	.396	12
13	.749		.769	.794			.792	.418	13
14	.911		.922	.926			.995	.602	14
15	1.061		1.066	1.075			1.135	.765	15
16	.968		.985	1.016			1.086	.761	16
17	-.127		-.124	-.128			-.118	-.090	17
18	-.109		-.128	-.123			-.122	-.050	18
19	-.106		-.135	-.126			-.122	-.067	19
20	-.113		-.136	-.139			-.142	-.095	20
21	-.154		-.178	-.172			-.168	-.129	21
22	-.149		-.186	-.167				-.199	22
23	-.160			-.184			-.176	-.214	23
24	-.163		-.175	-.183			-.182	-.240	24
25	-.163		-.182	-.186			-.188	-.214	25
26	-.175		-.196	-.199			-.192	-.209	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.454		.560	.549			.539	.516	1
2	.377		.537	.533			.528	.414	2
3	.382		.509	.539			.550	.354	3
4	.305		.436	.483			.493	.291	4
5	.266		.298	.372			.416	.210	5
6	.282		.284	.328			.373	.145	6
7	.270		.269	.319			.366	.105	7
8	.253		.271	.301			.344		8
9	.257		.244	.277			.309	.109	9
10	.214		.217	.264			.256	.105	10
11	.460		.215	.567			.565	.088	11
12	.591		.619	.635			.638	.337	12
13	.708		.705	.722			.719	.421	13
14	.784		.802	.826			.792	.460	14
15	.803		.822	.845			.779	.474	15
16	.767		.779	.802			.756	.453	16
17	-.135		-.138	-.140			-.115	-.106	17
18	-.111		-.148	-.131			-.120	-.059	18
19	-.107		-.143	-.132			-.115	-.077	19
20	-.118		-.147	-.146			-.130	-.106	20
21	-.167		-.185	-.177			-.164	-.143	21
22	-.165		-.193	-.181				-.202	22
23	-.167			-.186			-.174	-.232	23
24	-.170		-.190	-.181			-.180	-.260	24
25	-.166		-.193	-.192			-.188	-.241	25
26	-.184		-.206	-.197			-.192	-.241	26

α=-12 δ=-10

1	.454		.563	.558			.541	.535	1
2	.370		.540	.542			.532	.420	2
3	.387		.513	.548			.547	.371	3
4	.380		.436	.495			.488	.302	4
5	.268		.302	.382			.415	.216	5
6	.268		.287	.335			.372	.152	6
7	.269		.270	.312			.363	.122	7
8	.257		.280	.302			.337		8
9	.259		.253	.275			.297	.114	9
10	.202		.221	.253			.242	.114	10
11	.241		.221	.244			.239	.085	11
12	.407		.402	.383			.427	.200	12
13	.407		.402	.421			.428	.200	13
14	.398		.409	.423			.414	.192	14
15	.398		.412	.427			.391	.192	15
16	.388		.401	.427			.380	.178	16
17	-.133		-.136	-.136			-.120	-.100	17
18	-.108		-.138	-.128			-.121	-.055	18
19	-.107		-.132	-.134			-.122	-.077	19
20	-.119		-.140	-.151			-.134	-.102	20
21	-.167		-.183	-.170			-.164	-.132	21
22	-.161		-.189	-.178				-.196	22
23	-.166			-.183			-.179	-.227	23
24	-.167		-.186	-.185			-.177	-.242	24
25	-.168		-.189	-.196			-.182	-.209	25
26	-.182		-.204	-.208			-.193	-.234	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.441		.556	.557			.532	.521	1
2	.369		.534	.538			.526	.416	2
3	.380		.499	.540			.543	.364	3
4	.378		.433	.492			.485	.293	4
5	.264		.293	.377			.404	.216	5
6	.267		.284	.331			.368	.141	6
7	.266		.269	.317			.357	.104	7
8	.250		.272	.296			.331		8
9	.251		.244	.272			.296	.097	9
10	.194		.211	.250			.239	.105	10
11	.230		.211	.232			.237	.076	11
12	.177		.163	.172			.177	.022	12
13	.159		.142	.158			.164	.006	13
14	.127		.142	.165			.155	-.005	14
15	.140		.150	.156			.142	.005	15
16	.132		.135	.161			.132	-.012	16
17	-.136		-.138	-.134			-.123	-.105	17
18	-.102		-.137	-.134			-.119	-.069	18
19	-.114		-.141	-.130			-.134	-.077	19
20	-.126		-.143	-.151			-.139	-.111	20
21	-.167		-.184	-.181			-.168	-.145	21
22	-.166		-.194	-.180				-.208	22
23	-.168			-.188			-.177	-.225	23
24	-.177		-.193	-.190			-.188	-.247	24
25	-.173		-.192	-.198			-.188	-.218	25
26	-.183		-.208	-.199			-.191	-.236	26

α=-12 δ=10

1	.454		.568	.562			.535	.524	1
2	.368		.541	.548			.529	.410	2
3	.390		.516	.550			.546	.357	3
4	.393		.439	.501			.492	.287	4
5	.275		.304	.383			.406	.218	5
6	.279		.293	.339			.365	.141	6
7	.268		.281	.308			.354	.113	7
8	.256		.284	.300			.335		8
9	.257		.256	.271			.300	.096	9
10	.207		.226	.243			.245	.105	10
11	.239		.226	.234			.238	.081	11
12	-.014		-.014	-.004			-.013	-.101	12
13	-.032		-.044	-.035			-.033	-.120	13
14	-.050		-.055	-.026			-.033	-.132	14
15	-.044		-.047	-.041			-.042	-.132	15
16	-.050		-.047	-.037			-.060	-.132	16
17	-.125		-.139	-.147			-.138	-.108	17
18	-.108		-.135	-.138			-.136	-.070	18
19	-.111		-.130	-.140			-.140	-.092	19
20	-.118		-.137	-.151			-.152	-.119	20
21	-.159		-.185	-.182			-.180	-.150	21
22	-.153		-.190	-.188				-.220	22
23	-.169			-.196			-.192	-.237	23
24	-.169		-.183	-.190			-.194	-.260	24
25	-.166		-.190	-.202			-.196	-.233	25
26	-.186		-.203	-.203			-.205	-.255	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.463		.577	.573			.551	.525	1
2	.383		.549	.558			.533	.414	2
3	.393		.517	.557			.552	.360	3
4	.395		.441	.507			.489	.282	4
5	.285		.306	.391			.410	.215	5
6	.279		.295	.345			.366	.147	6
7	.273		.281	.310			.361	.113	7
8	.261		.282	.300			.342		8
9	.260		.260	.276			.300	.100	9
10	.202		.230	.250			.249	.108	10
11	.237		.230	.237			.236	.077	11
12	-.131		-.123	-.109			-.123	-.174	12
13	-.149		-.154	-.146			-.150	-.191	13
14	-.149		-.163	-.145			-.150	-.191	14
15	-.167		-.163	-.158			-.160	-.191	15
16	-.161		-.163	-.158			-.160	-.191	16
17	-.136		-.130	-.143			-.132	-.109	17
18	-.110		-.131	-.139			-.131	-.067	18
19	-.113		-.132	-.144			-.137	-.086	19
20	-.126		-.136	-.157			-.153	-.117	20
21	-.166		-.180	-.189			-.186	-.146	21
22	-.161		-.183	-.195				-.219	22
23	-.169			-.198			-.194	-.246	23
24	-.169		-.181	-.200			-.201	-.266	24
25	-.169		-.186	-.204			-.203	-.240	25
26	-.183		-.205	-.205			-.210	-.251	26

α=-12 δ=30

1	.464		.584	.573			.558	.537	1
2	.378		.546	.560			.552	.423	2
3	.393		.520	.559			.564	.374	3
4	.392		.441	.499			.503	.301	4
5	.276		.306	.384			.427	.225	5
6	.284		.287	.332			.373	.163	6
7	.270		.275	.323			.375	.118	7
8	.258		.278	.310			.348		8
9	.258		.250	.282			.308	.106	9
10	.202		.219	.257			.254	.106	10
11	.236		.219	.249			.246	.095	11
12	-.215		-.206	-.192			-.211	-.240	12
13	-.237		-.236	-.229			-.229	-.240	13
14	-.234		-.245	-.231			-.242	-.240	14
15	-.237		-.237	-.233			-.242	-.240	15
16	-.197		-.219	-.228			-.232	-.237	16
17	-.137		-.133	-.139			-.130	-.111	17
18	-.121		-.138	-.141			-.129	-.074	18
19	-.123		-.146	-.141			-.135	-.108	19
20	-.125		-.148	-.153			-.146	-.115	20
21	-.170		-.187	-.178			-.173	-.159	21
22	-.171		-.195	-.189				-.224	22
23	-.175			-.184			-.192	-.246	23
24	-.179		-.198	-.167			-.189	-.264	24
25	-.178		-.053	-.113			-.114	-.240	25
26	-.030		-.014	-.067			-.052	-.240	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=-9$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.362		.387	.409			.390	.383	1
2	.288		.408	.397			.395	.292	2
3	.303		.396	.397			.407	.252	3
4	.301		.350	.370			.356	.192	4
5	.194		.224	.284			.291	.132	5
6	.192		.205	.246			.260	.072	6
7	.189		.193	.241			.253	.037	7
8	.182		.197	.226			.235		8
9	.183		.171	.193			.212	.040	9
10	.189		.148	.179			.178	.040	10
11	.163		.148	.169			.172	.018	11
12	.072		.065	.069			.078 -	.042	12
13	.059		.044	.053			.060 -	.051	13
14	.029		.044	.051			.060 -	.064	14
15	.046		.050	.058			.050 -	.058	15
16	.033		.044	.058			.038 -	.064	16
17 -	.098		- .095	- .096			- .087 -	.076	17
18 -	.060		- .098	- .095			- .083 -	.044	18
19 -	.080		- .100	- .094			- .087 -	.050	19
20 -	.090		- .103	- .109			- .101 -	.077	20
21 -	.140		- .149	- .140			- .128 -	.099	21
22 -	.130		- .154	- .154			-	.140	22
23 -	.138			- .159			- .144 -	.170	23
24 -	.137		- .154	- .159			- .147 -	.202	24
25 -	.137		- .152	- .158			- .146 -	.169	25
26 -	.151		- .165	- .157			- .156 -	.205	26

$\alpha=-6$ $\delta=-30$

1	.264		.267	.284			.269	.274	1
2	.197		.276	.279			.266	.213	2
3	.222		.275	.280			.271	.190	3
4	.214		.251	.251			.233	.133	4
5	.109		.134	.180			.181	.085	5
6	.111		.123	.152			.153	.051	6
7	.105		.108	.151			.145	.017	7
8	.105		.122	.178			.152		8
9	.414		.454	.474			.482	.205	9
10	.463		.487	.513			.492	.287	10
11	.474		.485	.520			.500	.256	11
12	.510		.514	.542			.502	.242	12
13	.555		.543	.556			.533	.283	13
14	.797		.731	.748			.737	.474	14
15	.917		.895	.907			.863	.567	15
16	.854		.854	.897			.865	.544	16
17 -	.034		- .032	- .042			- .027 -	.014	17
18 -	.030		- .037	- .037			- .032 -	.006	18
19 -	.031		- .036	- .038			- .033 -	.006	19
20 -	.050		- .050	- .052			- .052 -	.022	20
21 -	.101		- .103	- .090			- .093 -	.037	21
22 -	.098		- .117	- .103			-	.050	22
23 -	.099			- .115			- .103 -	.068	23
24 -	.110		- .107	- .111			- .109 -	.109	24
25 -	.103		- .115	- .122			- .115 -	.077	25
26 -	.133		- .130	- .132			- .125 -	.012	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.269		.265	.278			.274	.277	1
2	.207		.282	.272			.266	.209	2
3	.227		.281	.272			.279	.181	3
4	.226		.253	.255			.237	.141	4
5	.126		.144	.183			.183	.077	5
6	.128		.127	.151			.156	.044	6
7	.118		.114	.148			.151	.003	7
8	.111		.130	.140			.138		8
9	.110		.101	.119			.125	.008	9
10	.072		.084	.103			.088	.008	10
11	.223		.084	.182			.227	- .006	11
12	.421		.406	.391			.427	.211	12
13	.488		.485	.498			.506	.348	13
14	.509		.533	.553			.542	.324	14
15	.520		.550	.560			.538	.306	15
16	.519		.550	.564			.523	.275	16
17	- .029		- .033	- .040		- .028	- .017		17
18	- .020		- .034	- .034		- .038	.006		18
19	- .031		- .034	- .035		- .039	.004		19
20	- .040		- .051	- .054		- .059	- .018		20
21	- .092		- .099	- .091		- .097	- .037		21
22	- .094		- .108	- .105			- .049		22
23	- .093			- .112		- .106	- .073		23
24	- .100		- .115	- .113		- .117	- .104		24
25	- .103		- .118	- .123		- .110	- .094		25
26	- .125		- .134	- .132		- .125	- .115		26

$\alpha = -6$ $\delta = -10$

1	.254		.272	.285			.270	.263	1
2	.196		.281	.274			.267	.197	2
3	.214		.277	.274			.271	.177	3
4	.217		.258	.254			.233	.127	4
5	.114		.141	.184			.183	.083	5
6	.118		.130	.155			.152	.032	6
7	.109		.115	.150			.146	.005	7
8	.102		.130	.140			.136		8
9	.104		.099	.113			.119	.000	9
10	.055		.079	.100			.088	.000	10
11	.082		.079	.087			.095	- .019	11
12	.202		.205	.202			.229	.085	12
13	.220		.211	.227			.229	.105	13
14	.201		.211	.233			.228	.086	14
15	.209		.224	.233			.219	.083	15
16	.195		.213	.233			.206	.070	16
17	- .039		- .033	- .040		- .037	- .032		17
18	- .024		- .037	- .039		- .036	.005		18
19	- .030		- .031	- .039		- .038	.004		19
20	- .045		- .048	- .057		- .059	- .028		20
21	- .093		- .102	- .096		- .099	- .041		21
22	- .097		- .105	- .105			- .055		22
23	- .103			- .107		- .103	- .091		23
24	- .106		- .105	- .103		- .114	- .129		24
25	- .104		- .113	- .118		- .124	- .091		25
26	- .126		- .129	- .130		- .128	- .127		26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = -6$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.256		.263	.282			.270	.274	1
2	.203		.282	.273			.273	.202	2
3	.217		.281	.278			.283	.183	3
4	.214		.257	.252			.240	.136	4
5	.121		.145	.178			.185	.088	5
6	.115		.122	.156			.155	.042	6
7	.105		.115	.151			.152	.010	7
8	.099		.121	.138			.134		8
9	.105		.099	.123			.128	.005	9
10	.057		.082	.101			.087	.004	10
11	.086		.081	.094			.099 -	.006	11
12	.036		.019	.032			.037 -	.044	12
13	.026		.010	.013			.020 -	.054	13
14	.004		.010	.023			.024 -	.074	14
15	.013		.010	.023			.018 -	.063	15
16	.004		.010	.023			.006 -	.064	16
17 -	.032		- .033	- .045			- .029 -	.019	17
18 -	.014		- .032	- .032			- .020	.006	18
19 -	.026		- .028	- .035			- .034	.004	19
20 -	.040		- .042	- .056			- .049 -	.017	20
21 -	.093		- .097	- .088			- .091 -	.032	21
22 -	.092		- .106	- .101			-	.044	22
23 -	.099			- .111			- .099 -	.076	23
24 -	.102		- .102	- .110			- .107 -	.104	24
25 -	.099		- .109	- .116			- .107 -	.081	25
26 -	.126		- .129	- .131			- .121 -	.117	26

$\alpha = -6$ $\delta = 10$

1	.263		.266	.292			.279	.275	1
2	.206		.282	.281			.281	.209	2
3	.225		.281	.284			.287	.186	3
4	.226		.258	.254			.245	.137	4
5	.117		.144	.177			.191	.081	5
6	.119		.123	.164			.162	.041	6
7	.118		.116	.156			.155	.008	7
8	.110		.127	.149			.139		8
9	.114		.101	.135			.135	.010	9
10	.063		.083	.109			.104	.010	10
11	.091		.083	.099			.106 -	.005	11
12 -	.097		- .097	- .083			- .095 -	.141	12
13 -	.126		- .123	- .127			- .126 -	.156	13
14 -	.126		- .140	- .122			- .124 -	.140	14
15 -	.126		- .131	- .126			- .135 -	.106	15
16 -	.132		- .131	- .136			- .135 -	.085	16
17 -	.035		- .041	- .040			- .025 -	.029	17
18 -	.021		- .040	- .037			- .031	.004	18
19 -	.032		- .035	- .035			- .033 -	.012	19
20 -	.043		- .050	- .050			- .052 -	.026	20
21 -	.099		- .105	- .088			- .089 -	.045	21
22 -	.096		- .109	- .098			-	.056	22
23 -	.098			- .103			- .102 -	.086	23
24 -	.103		- .101	- .107			- .110 -	.108	24
25 -	.101		- .111	- .120			- .115 -	.092	25
26 -	.124		- .127	- .129			- .121 -	.119	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.266		.273	.285			.285	.273	1
2	.207		.292	.284			.289	.202	2
3	.217		.288	.284			.295	.181	3
4	.224		.262	.264			.246	.136	4
5	.125		.147	.187			.194	.085	5
6	.125		.134	.160			.166	.036	6
7	.119		.120	.164			.159	-.003	7
8	.112		.130	.152			.143		8
9	.121		.105	.131			.140	.005	9
10	.073		.084	.116			.099	.005	10
11	.092		.084	.104			.107	-.010	11
12	-.181	-.182	-.167			-.179	-.201		12
13	-.208	-.214	-.210			-.205	-.210		13
14	-.208	-.222	-.209			-.205	-.177		14
15	-.218	-.222	-.211			-.219	-.155		15
16	-.164	-.216	-.211			-.205	-.163		16
17	-.032	-.033	-.039			-.032	-.036		17
18	-.031	-.036	-.044			-.040	-.004		18
19	-.031	-.033	-.039			-.038	-.014		19
20	-.046	-.050	-.062			-.056	-.032		20
21	-.092	-.100	-.089			-.087	-.047		21
22	-.094	-.111	-.106				-.056		22
23	-.098		-.108			-.103	-.087		23
24	-.099	-.108	-.108			-.114	-.122		24
25	-.098	-.111	-.123			-.117	-.104		25
26	-.122	-.130	-.132			-.129	-.136		26

α=-6 δ=30

1	.260		.269	.294			.283	.288	1
2	.202		.285	.286			.282	.216	2
3	.213		.283	.284			.286	.183	3
4	.218		.258	.260			.248	.137	4
5	.114		.145	.188			.188	.087	5
6	.112		.122	.165			.161	.049	6
7	.107		.112	.153			.162	.006	7
8	.102		.121	.151			.147		8
9	.107		.098	.129			.128	.013	9
10	.056		.081	.103			.102	.014	10
11	.085		.081	.104			.103	-.008	11
12	-.242	-.237	-.229			-.245	-.260		12
13	-.255	-.259	-.255			-.265	-.260		13
14	-.246	-.250	-.250			-.249	-.222		14
15	-.229	-.238	-.250			-.240	-.250		15
16	-.201	-.227	-.232			-.229	-.260		16
17	-.045	-.050	-.052			-.041	-.032		17
18	-.039	-.056	-.044			-.034	-.001		18
19	-.043	-.049	-.044			-.044	-.009		19
20	-.054	-.057	-.059			-.063	-.037		20
21	-.101	-.114	-.102			-.100	-.053		21
22	-.105	-.120	-.121				-.067		22
23	-.105		-.123			-.112	-.092		23
24	-.107	-.074	-.066			-.046	-.126		24
25	.048	.111	.072			.100	-.096		25
26	.095	.134	.070			.133	-.124		26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = -3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.167		.164	.186			.184	.188	1
2	.128		.174	.175			.190	.140	2
3	.138		.183	.188			.195	.124	3
4	.139		.164	.164			.153	.079	4
5	.051		.076	.095			.112	.047	5
6	.015		.054	.074			.086	.023	6
7	.043		.040	.081			.076 -	.009	7
8	.038		.054	.076			.065		8
9	.040		.027	.053			.055 -	.003	9
10	.003		.023	.047			.031 -	.003	10
11	.015		.021	.033			.040 -	.010	11
12 -	.026	- .036	- .038			-	.042 -	.058	12
13 -	.038	- .050	- .056			-	.055 -	.073	13
14 -	.046	- .053	- .047			-	.055 -	.087	14
15 -	.046	- .051	- .047			-	.047 -	.060	15
16 -	.055	- .054	- .051			-	.064 -	.050	16
17	.031		.030	.038			.034	.044	17
18	.050		.030	.040			.080	.055	18
19	.026		.032	.040			.041	.044	19
20	.010		.016	.021			.017	.013	20
21 -	.049	- .047	- .032			-	.028	.001	21
22 -	.049	- .058	- .041				-	.004	22
23 -	.049		- .045			-	.047 -	.012	23
24 -	.057	- .057	- .046			-	.049 -	.022	24
25 -	.055	- .068	- .053			-	.051 -	.005	25
26 -	.082	- .090	- .066			-	.072 -	.024	26

$\alpha = 0$ $\delta = -30$

1	.077	.086	.097			.099	.097	1
2	.059	.086	.096			.099	.077	2
3	.061	.097	.096			.101	.077	3
4	.050	.078	.075			.074	.059	4
5	- .017	.006	.022			.036	.023	5
6	- .016	- .013	.003			.011	.013	6
7	- .015	- .025	.003			.010	.003	7
8	- .031	- .014	.084			.016		8
9	.228	.270	.186			.278	.153	9
10	.272	.294	.315			.297	.189	10
11	.278	.294	.318			.328	.168	11
12	.332	.327	.332			.330	.166	12
13	.215	.357	.358			.354	.270	13
14	.630	.555	.546			.581	.510	14
15	.742	.711	.705			.721	.487	15
16	.724	.711	.728			.746	.439	16
17	.083	.099	.094			.107	.107	17
18	.066	.093	.098			.107	.101	18
19	.064	.093	.101			.115	.082	19
20	.049	.075	.078			.082	.055	20
21	- .018	.008	.025			.040	.028	21
22	- .015	- .008	.008			.027	.023	22
23	- .022	- .014	.002			.015	.019	23
24	- .023	- .018	.004			.008	.005	24
25	- .023	- .029	- .004			.004	.014	25
26	- .053	- .046	- .022			- .015	.029	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=-25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.081		.084	.098			.100	.101	1
2	.061		.084	.096			.103	.073	2
3	.066		.091	.096			.105	.073	3
4	.061		.074	.075			.076	.054	4
5	-.013		.004	.024			.033	.018	5
6	-.015		-.010	.003			.016	.012	6
7	-.021		-.021	.007			.010	.001	7
8	-.024		-.015	.006			.003		8
9	-.020		-.014	.055			.014	.014	9
10	-.022		-.010	-.001			.007	.022	10
11	.182		-.007	.226			.254	.031	11
12	.256		.274	.279			.270	.279	12
13	.349		.367	.364			.357	.340	13
14	.477		.487	.499			.480	.341	14
15	.480		.514	.529			.513	.307	15
16	.501		.529	.527			.513	.262	16
17	.082		.095	.097			.109	.098	17
18	.066		.092	.098			.110	.098	18
19	.067		.089	.102			.113	.075	19
20	.053		.073	.079			.085	.043	20
21	-.021		.000	.027			.038	.023	21
22	-.016		-.010	.005			.025	.018	22
23	-.019		-.013	.007			.016	.017	23
24	-.024		-.014	.007			.010	.003	24
25	-.022		-.027	-.008			.006	.022	25
26	-.055		-.049	-.025			-.014	.003	26

$\alpha=0$ $\delta=-20$

1	.083		.085	.101			.095	.095	1
2	.067		.096	.097			.097	.074	2
3	.070		.095	.098			.101	.074	3
4	.066		.083	.076			.071	.049	4
5	-.012		.007	.026			.030	.017	5
6	-.010		-.007	.003			.008	.006	6
7	-.014		-.022	.005			.006	-.009	7
8	-.022		-.014	.001			-.002		8
9	-.017		-.026	.000			-.011	.000	9
10	-.039		-.025	-.027			-.025	.009	10
11	.103		-.025	.043			.102	.008	11
12	.240		.237	.219			.229	.201	12
13	.330		.297	.309			.286	.260	13
14	.322		.335	.356			.338	.231	14
15	.332		.345	.356			.340	.205	15
16	.331		.352	.356			.340	.168	16
17	.085		.101	.089			.101	.100	17
18	.070		.094	.095			.103	.095	18
19	.065		.096	.099			.101	.074	19
20	.057		.067	.074			.073	.045	20
21	-.017		.001	.023			.032	.013	21
22	-.015		-.011	.004			.019	.003	22
23	-.017		-.012	.002			.008	.003	23
24	-.019		-.014	.000			-.002	-.006	24
25	-.018		-.024	-.011			-.008	.018	25
26	-.053		-.051	-.030			-.025	-.004	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.095		.092	.103			.096	.111	1
2	.069		.098	.103			.097	.081	2
3	.085		.104	.104			.100	.081	3
4	.075		.086	.078			.069	.061	4
5	.002		.020	.030			.028	.018	5
6	-.001		.000	.007			.004	.018	6
7	-.003		-.013	.005			-.002	.000	7
8	-.013		-.005	.001			-.011		8
9	-.007		-.015	-.014			-.014	-.004	9
10	-.040		-.026	-.028			-.036	-.001	10
11	-.025		-.026	-.030			-.006	-.012	11
12	.073		.079	.079			.069	.064	12
13	.196		.079	.078			.069	.077	13
14	.074		.079	.096			.082	.050	14
15	.074		.078	.082			.072	.026	15
16	.074		.079	.084			.073	.009	16
17	.099		.111	.090			.095	.102	17
18	.078		.101	.091			.096	.091	18
19	.077		.098	.094			.093	.081	19
20	.065		.078	.071			.064	.047	20
21	-.005		.008	.015			.025	.022	21
22	-.003		-.004	-.002			.011	.015	22
23	-.005		-.004	.000			-.002	.014	23
24	-.012		-.007	-.003			-.013	-.001	24
25	-.013		-.020	-.015			-.010	.023	25
26	-.049		-.045	-.035			-.030	-.004	26

$\alpha=0$ $\delta=0$

1	.095		.100	.105			.096	.107	1
2	.070		.100	.106			.100	.078	2
3	.082		.104	.106			.101	.078	3
4	.073		.093	.080			.073	.059	4
5	.000		.014	.027			.030	.010	5
6	-.001		.000	.009			.008	.006	6
7	-.004		-.011	.006			.001	-.004	7
8	-.008		-.008	.004			-.007		8
9	-.008		-.017	-.012			-.018	-.005	9
10	-.039		-.027	-.025			-.039	.000	10
11	-.033		-.027	-.040			-.012	-.014	11
12	-.046		-.043	-.031			-.046	-.035	12
13	.055		-.073	-.068			-.068	-.035	13
14	-.066		-.073	-.047			-.068	-.035	14
15	-.072		-.073	-.065			-.070	-.035	15
16	-.072		-.073	-.070			-.084	-.035	16
17	.097		.104	.086			.092	.096	17
18	.085		.099	.091			.092	.096	18
19	.078		.098	.093			.095	.074	19
20	.060		.081	.077			.061	.036	20
21	-.006		.009	.020			.029	.020	21
22	-.002		-.008	.001			.013	.010	22
23	-.008		-.008	.002			.000	.009	23
24	-.006		-.010	-.002			-.010	-.008	24
25	-.012		-.020	-.016			-.015	.013	25
26	-.047		-.047	-.034			-.030	-.004	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 0$ $\delta = 10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.089		.090	.105			.104	.109	1
2	.072		.091	.106			.108	.083	2
3	.074		.101	.104			.106	.081	3
4	.064		.090	.082			.080	.060	4
5	-.007		.014	.030			.036	.013	5
6	-.007		-.008	.006			.011	.008	6
7	-.008		-.018	.010			.010	-.003	7
8	-.020		-.016	.005			.000		8
9	-.017		-.025	-.013			-.004	-.006	9
10	-.045		-.035	-.024			-.030	.004	10
11	-.038		-.035	-.030			-.001	-.006	11
12	-.153		-.147	-.139			-.155	-.134	12
13	-.059		-.178	-.178			-.176	-.134	13
14	-.164		-.188	-.178			-.189	-.102	14
15	-.176		-.188	-.188			-.187	-.116	15
16	-.160		-.188	-.187			-.198	-.184	16
17	.083		.100	.092			.097	.093	17
18	.073		.090	.093			.096	.093	18
19	.065		.093	.092			.099	.066	19
20	.051		.073	.078			.072	.031	20
21	-.018		.005	.016			.024	.009	21
22	-.012		-.013	.003			.012	.009	22
23	-.016		-.012	.001			.004	.009	23
24	-.021		-.019	-.004			-.006	-.003	24
25	-.022		-.030	-.013			-.010	.014	25
26	-.055		-.051	-.031			-.027	-.001	26

$\alpha = 0$ $\delta = 20$

1	.080		.087	.104			.109	.102	1
2	.060		.090	.104			.111	.077	2
3	.064		.093	.104			.111	.077	3
4	.056		.083	.081			.082	.061	4
5	-.014		.011	.028			.042	.013	5
6	-.018		-.005	.004			.020	.003	6
7	-.018		-.016	.012			.016	-.009	7
8	-.027		-.014	.010			.007		8
9	-.021		-.027	-.010			-.002	-.009	9
10	-.048		-.034	-.021			-.021	.000	10
11	-.042		-.034	-.032			.009	.000	11
12	-.219		-.216	-.202			-.217	-.198	12
13	-.134		-.234	-.240			-.248	-.175	13
14	-.226		-.249	-.240			-.235	-.203	14
15	-.240		-.238	-.229			-.219	-.235	15
16	-.173		-.189	-.201			-.205	-.256	16
17	.081		.092	.089			.100	.088	17
18	.067		.090	.095			.100	.088	18
19	.063		.090	.097			.101	.077	19
20	.046		.073	.072			.076	.043	20
21	-.024		-.006	.020			.027	.006	21
22	-.018		-.014	.005			.013	.008	22
23	-.021		-.016	-.001			.006	.008	23
24	-.023		-.019	.001			.001	-.006	24
25	-.025		-.029	-.008			-.004	.008	25
26	-.053		-.055	-.030			-.024	-.006	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=0$ $\delta=25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.080		.085	.105			.112	.098	1
2	.060		.090	.106			.112	.072	2
3	.061		.096	.103			.112	.072	3
4	.057		.081	.082			.084	.051	4
5	-.016		.009	.029			.042	.010	5
6	-.023		-.007	.004			.018	.004	6
7	-.021		-.019	.010			.016	-.014	7
8	-.030		-.014	.008			.006		8
9	-.028		-.027	-.006			.003	-.005	9
10	-.050		-.033	-.018			-.021	.001	10
11	-.040		-.033	-.029			.010	.020	11
12	-.247		-.248	-.240			-.249	-.202	12
13	-.173		-.267	-.263			-.265	-.171	13
14	-.240		-.249	-.256			-.247	-.248	14
15	-.230		-.237	-.235			-.237	-.267	15
16	-.211		-.223	-.224			-.223	-.277	16
17	.080		.091	.089			.102	.078	17
18	.062		.088	.094			.100	.078	18
19	.063		.090	.095			.103	.061	19
20	.045		.071	.076			.071	.032	20
21	-.023		-.003	.020			.030	.014	21
22	-.018		-.021	.001			.019	.003	22
23	-.021		-.018	.003			.008	.003	23
24	-.025		-.020	-.001			.001	-.014	24
25	-.026		-.031	-.007			-.007	.003	25
26	.156		.233	.224			.241	.038	26

$\alpha=0$ $\delta=30$

1	.097		.096	.109			.111	.118	1
2	.081		.103	.108			.108	.096	2
3	.079		.108	.109			.111	.087	3
4	.072		.093	.088			.085	.064	4
5	.001		.017	.032			.038	.027	5
6	.002		-.002	.010			.018	.014	6
7	-.007		-.005	.013			.012	-.004	7
8	-.012		-.003	.011			.003		8
9	-.007		-.017	-.011			-.003	.017	9
10	-.032		-.020	-.019			-.025	.116	10
11	-.030		-.020	-.025			.003	.100	11
12	-.256		-.256	-.257			-.263	-.203	12
13	-.199		-.256	-.272			-.263	-.176	13
14	-.235		-.240	-.247			-.252	-.270	14
15	-.224		-.234	-.243			-.247	-.285	15
16	-.225		-.234	-.244			-.247	-.285	16
17	.088		.098	.092			.095	.090	17
18	.078		.096	.091			.097	.092	18
19	.074		.096	.090			.098	.074	19
20	.060		.076	.076			.069	.041	20
21	-.012		.008	.020			.024	.013	21
22	-.003		-.005	.001			.017	.013	22
23	-.006		.126	.062			.007	.018	23
24	.226		.257	.299			.266	.027	24
25	.266		.300	.317			.311	.226	25
26	.293		.305	.330			.325	.251	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 3$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.020		.012	.022			.029	.029	1
2	-.007		.019	.018			.021	.023	2
3	.016		.019	.014			.032	.029	3
4	.015		.005	-.003			-.007	.015	4
5	-.054		-.049	-.054			-.032	-.015	5
6	-.054		-.067	-.069			-.061	-.015	6
7	-.064		-.080	-.047			-.060	-.040	7
8	-.064		-.068	-.058			-.069		8
9	-.071		-.084	-.070			-.079	-.037	9
10	-.095		-.083	-.076			-.091	-.037	10
11	-.086		-.036	-.086			-.051	-.058	11
12	-.099		-.108	-.104			-.113	-.077	12
13	-.106		-.123	-.127			-.128	-.081	13
14	-.126		-.123	-.123			-.120	-.100	14
15	-.124		-.118	-.115			-.122	-.122	15
16	-.118		-.123	-.120			-.127	-.138	16
17	.164		.174	.175			.165	.169	17
18	.131		.175	.175			.170	.146	18
19	.138		.169	.184			.170	.109	19
20	.128		.147	.158			.137	.076	20
21	.037		.065	.101			.096	.027	21
22	.044		.043	.073				.009	22
23	.044			.073			.066	.008	23
24	.037		.037	.062			.050	-.015	24
25	.037		.019	.054			.050	.009	25
26	-.004		.003	.029			.029	-.018	26

$\alpha = 6$ $\delta = -30$

1	-.043		-.048	-.033			-.042	-.037	1
2	-.042		-.048	-.050			-.042	-.020	2
3	-.032		-.040	-.050			-.042	-.014	3
4	-.038		-.051	-.065			-.070	-.027	4
5	-.099		-.112	-.101			-.099	-.056	5
6	-.099		-.112	-.117			-.116	-.076	6
7	-.103		-.121	-.112			-.116	-.110	7
8	-.106		-.121	-.112			-.126		8
9	-.106		-.130	-.119			-.123	-.132	9
10	.063		.086	.071			.083	-.146	10
11	.093		.086	.099			.136	-.136	11
12	.136		.127	.128			.131	.122	12
13	.332		.187	.168			.168	.237	13
14	.396		.382	.350			.348	.046	14
15	.404		.445	.425			.429	.261	15
16	.421		.459	.442			.443	.327	16
17	.270		.282	.265			.276	.279	17
18	.213		.291	.277			.279	.238	18
19	.222		.273	.277			.278	.191	19
20	.197		.244	.243			.241	.122	20
21	.115		.144	.177			.186	.076	21
22	.121		.113	.153				.055	22
23	.115			.145			.146	.022	23
24	.109		.120	.142			.144	.009	24
25	.109		.095	.125			.134	.031	25
26	.057		.069	.103			.098	.000	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=-20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.040		-.044	-.031			-.039	-.033	1
2	-.040		-.044	-.042			-.042	-.023	2
3	-.037		-.033	-.042			-.039	-.010	3
4	-.037		-.043	-.061			-.060	-.024	4
5	-.106		-.103	-.099			-.096	-.050	5
6	-.104		-.104	-.113			-.120	-.065	6
7	-.104		-.117	-.106			-.114	-.106	7
8	-.104		-.106	-.111			-.122		8
9	-.109		-.122	-.125			-.124	-.132	9
10	-.120		-.111	-.130			-.138	-.138	10
11	-.034		-.112	-.114			-.043	-.152	11
12	.079		.064	.041			.053	-.060	12
13	.147		.127	.095			.115	.070	13
14	.151		.154	.147			.164	-.091	14
15	.154		.161	.151			.174	.005	15
16	.152		.164	.159			.182	.044	16
17	.267		.279	.271			.271	.257	17
18	.212		.291	.271			.274	.227	18
19	.213		.283	.279			.274	.173	19
20	.198		.244	.247			.236	.128	20
21	.113		.145	.174			.178	.069	21
22	.113		.121	.152				.047	22
23	.113			.142			.148	.031	23
24	.113		.120	.137			.139	.005	24
25	.106		.095	.120			.125	.033	25
26	.055		.068	.097			.099	-.010	26

$\alpha=6$ $\delta=-10$

1	-.033		-.034	-.025			-.032	-.020	1
2	-.033		-.035	-.036			-.038	-.013	2
3	-.027		-.035	-.036			-.033	.006	3
4	-.027		-.043	-.051			-.056	-.006	4
5	-.037		-.104	-.093			-.089	-.037	5
6	-.087		-.104	-.105			-.107	-.059	6
7	-.099		-.113	-.101			-.110	-.091	7
8	-.099		-.109	-.108			-.118		8
9	-.098		-.117	-.114			-.125	-.113	9
10	-.116		-.109	-.125			-.132	-.119	10
11	-.112		-.109	-.131			-.085	-.136	11
12	-.038		-.047	-.072			-.072	-.122	12
13	-.029		-.047	-.060			-.051	-.091	13
14	-.040		-.047	-.050			-.036	-.142	14
15	-.033		-.042	-.041			-.036	-.111	15
16	-.033		-.043	-.041			-.036	-.119	16
17	.271		.276	.269			.271	.269	17
18	.219		.283	.269			.276	.227	18
19	.219		.272	.279			.267	.192	19
20	.205		.246	.250			.237	.145	20
21	.110		.143	.172			.167	.086	21
22	.110		.122	.142				.059	22
23	.118			.143			.149	.035	23
24	.106		.116	.144			.131	.013	24
25	.106		.095	.125			.129	.026	25
26	.050		.065	.098			.100	.006	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.042		-.045	-.034			-.029	-.028	1
2	-.037		-.045	-.034			-.029	-.022	2
3	-.035		-.034	-.038			-.039	-.012	3
4	-.035		-.050	-.057			-.047	-.024	4
5	-.091		-.104	-.099			-.078	-.053	5
6	-.088		-.115	-.108			-.099	-.064	6
7	-.099		-.114	-.110			-.094	-.102	7
8	-.107		-.114	-.115			-.100		8
9	-.107		-.125	-.125			-.105	-.117	9
10	-.130		-.116	-.133			-.119	-.122	10
11	-.122		-.116	-.142			-.076	-.142	11
12	-.135		-.140	-.143			-.141	-.169	12
13	-.146		-.160	-.161			-.159	-.172	13
14	-.152		-.160	-.161			-.152	-.161	14
15	-.152		-.152	-.159			-.146	-.182	15
16	-.159		-.161	-.156			-.147	-.173	16
17	.263		.274	.261			.283	.261	17
18	.204		.281	.267			.282	.225	18
19	.208		.267	.274			.286	.173	19
20	.199		.238	.238			.252	.129	20
21	.107		.139	.171			.189	.076	21
22	.110		.111	.145				.047	22
23	.110			.146			.164	.027	23
24	.110		.114	.139			.150	-.004	24
25	.103		.085	.129			.143	.018	25
26	.050		.065	.096			.122	-.004	26

$\alpha=6$ $\delta=10$

1	-.041		-.046	-.039			-.038	-.040	1
2	-.042		-.047	-.047			-.043	-.027	2
3	-.035		-.039	-.049			-.042	-.010	3
4	-.036		-.052	-.068			-.057	-.029	4
5	-.107		-.120	-.094			-.084	-.053	5
6	-.106		-.113	-.111			-.114	-.072	6
7	-.106		-.125	-.113			-.113	-.100	7
8	-.106		-.117	-.114			-.121		8
9	-.107		-.125	-.129			-.122	-.124	9
10	-.127		-.098	-.107			-.116	-.129	10
11	-.111		-.099	-.109			-.065	-.147	11
12	-.192		-.177	-.154			-.187	-.190	12
13	-.187		-.208	-.205			-.206	-.167	13
14	-.179		-.211	-.186			-.208	-.196	14
15	-.205		-.211	-.209			-.208	-.202	15
16	-.146		-.167	-.182			-.197	-.214	16
17	.271		.280	.268			.264	.259	17
18	.221		.287	.268			.268	.218	18
19	.210		.274	.291			.268	.175	19
20	.196		.238	.258			.231	.126	20
21	.114		.137	.174			.167	.076	21
22	.119		.111	.151				.049	22
23	.110			.145			.141	.033	23
24	.110		.114	.140			.127	-.001	24
25	.103		.096	.123			.116	.033	25
26	.057		.067	.098			.090	-.004	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha=6$ $\delta=20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.043		-.048	-.027			-.035	-.035	1
2	.043		-.048	-.035			-.035	-.027	2
3	.037		-.033	-.036			-.035	-.018	3
4	.035		-.055	-.050			-.062	-.028	4
5	.098		-.112	-.087			-.092	-.056	5
6	.098		-.112	-.107			-.112	-.073	6
7	.103		-.121	-.111			-.112	-.101	7
8	.103		-.118	-.111			-.122		8
9	.103		-.124	-.122			-.126	-.131	9
10	.120		-.111	-.138			-.142	-.137	10
11	.120		-.111	-.132			-.088	-.119	11
12	.251		-.246	-.238			-.250	-.255	12
13	.263		-.265	-.269			-.263	-.237	13
14	.246		-.246	-.257			-.257	-.257	14
15	.232		-.238	-.240			-.243	-.264	15
16	.204		-.223	-.224			-.234	-.269	16
17	.270		.277	.262			.263	.245	17
18	.220		.296	.268			.269	.219	18
19	.217		.277	.277			.269	.169	19
20	.201		.248	.246			.236	.122	20
21	.113		.138	.177			.175	.061	21
22	.118		.122	.153				.040	22
23	.118			.144			.145	.010	23
24	.110		.112	.136			.133	-.008	24
25	.110		.099	.123			.121	.022	25
26	.065		.071	.098			.101	-.003	26

$\alpha=6$ $\delta=30$

1	-.043		-.043	-.034			-.040	-.037	1
2	-.033		-.040	-.046			-.044	-.031	2
3	-.034		-.041	-.045			-.041	-.024	3
4	-.034		-.052	-.052			-.061	-.024	4
5	-.099		-.113	-.098			-.092	-.060	5
6	-.099		-.113	-.115			-.116	-.072	6
7	-.103		-.121	-.112			-.116	-.108	7
8	-.114		-.115	-.115			-.122		8
9	-.105		-.129	-.122			-.128	-.049	9
10	-.126		-.115	-.132			-.139	-.032	10
11	-.121		-.115	-.135			-.086	-.104	11
12	-.270		-.266	-.263			-.266	-.296	12
13	-.270		-.268	-.273			-.273	-.284	13
14	-.260		-.259	-.255			-.263	-.291	14
15	-.251		-.256	-.256			-.263	-.284	15
16	-.252		-.256	-.250			-.263	-.277	16
17	.272		.276	.260			.259	.247	17
18	.216		.283	.271			.263	.213	18
19	.216		.277	.274			.263	.169	19
20	.204		.242	.238			.230	.118	20
21	.109		.141	.173			.170	.068	21
22	.114		.120	.147				.036	22
23	.319			.393			.356	.050	23
24	.466		.479	.513			.494	.206	24
25	.481		.498	.525			.512	.290	25
26	.488		.505	.531			.516	.287	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.093		-.098	-.086			-.083	-.086	1
2	-.084		-.090	-.081			-.086	-.061	2
3	-.081		-.085	-.092			-.088	-.055	3
4	-.079		-.089	-.101			-.107	-.068	4
5	-.138		-.140	-.138			-.132	-.106	5
6	-.117		-.148	-.144			-.150	-.150	6
7	-.131		-.155	-.152			-.145	-.193	7
8	-.143		-.160	-.152			-.158		8
9	-.144		-.157	-.157			-.158	-.192	9
10	-.156		-.143	-.166			-.167	-.178	10
11	-.156		-.143	-.171			-.109	-.199	11
12	-.177		-.184	-.196			-.188	-.218	12
13	-.197		-.199	-.205			-.206	-.222	13
14	-.195		-.199	-.205			-.200	-.219	14
15	-.195		-.199	-.206			-.193	-.231	15
16	-.184		-.199	-.206			-.193	-.231	16
17	.378		.424	.399			.406	.382	17
18	.314		.424	.397			.406	.329	18
19	.311		.411	.413			.405	.261	19
20	.300		.349	.375			.368	.204	20
21	.199		.228	.296			.294	.133	21
22	.197		.207	.258				.100	22
23	.203			.246			.262	.068	23
24	.191		.200	.234			.252	.047	24
25	.195		.178	.215			.236	.069	25
26	.131		.145	.186			.198	.044	26

$\alpha = 12$ $\delta = -30$

1	-.154		-.162	-.148			-.150	-.124	1
2	-.140		-.155	-.151			-.149	-.101	2
3	-.137		-.162	-.147			-.149	-.090	3
4	-.137		-.162	-.161			-.166	-.118	4
5	-.182		-.205	-.188			-.187	-.168	5
6	-.183		-.207	-.200			-.198	-.240	6
7	-.188		-.215	-.210			-.198	-.266	7
8	-.192		-.211	-.207			-.209		8
9	-.194		-.214	-.216			-.210	-.260	9
10	-.075		-.022	-.065			-.060	-.243	10
11	-.017		-.022	-.029			-.013	-.220	11
12	.037		.017	.010			.003	-.159	12
13	.088		.042	.042			.031	-.069	13
14	.236		.206	.195			.208	-.159	14
15	.236		.277	.240			.287	-.193	15
16	.260		.288	.260			.325	-.224	16
17	.475		.613	.571			.571	.528	17
18	.402		.559	.573			.567	.452	18
19	.393		.514	.573			.566	.371	19
20	.381		.438	.500			.518	.320	20
21	.267		.304	.392			.428	.231	21
22	.274		.296	.345				.179	22
23	.268			.326			.368	.152	23
24	.264		.270	.317			.345	.118	24
25	.262		.250	.291			.320	.154	25
26	.198		.221	.258			.268	.109	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.156		-.156	-.142			-.143	-.114	1
2	-.137		-.148	-.152			-.143	-.097	2
3	-.134		-.151	-.152			-.145	-.088	3
4	-.131		-.151	-.159			-.159	-.113	4
5	-.181		-.196	-.187			-.177	-.163	5
6	-.171		-.196	-.203			-.199	-.232	6
7	-.189		-.208	-.193			-.199	-.250	7
8	-.187		-.206	-.194			-.206		8
9	-.190		-.209	-.207			-.208	-.252	9
10	-.200		-.196	-.213			-.216	-.241	10
11	-.119		-.192	-.186			-.094	-.228	11
12	-.004		-.042	-.059			-.056	-.188	12
13	.024		.004	-.010			-.006	-.163	13
14	.033		.047	.015			.038	-.200	14
15	.049		.065	.024			.061	-.225	15
16	.050		.058	.037			.077	-.227	16
17	.481		.621	.571			.573	.528	17
18	.405		.565	.571			.560	.446	18
19	.400		.525	.571			.568	.377	19
20	.387		.442	.510			.519	.315	20
21	.273		.312	.368			.424	.232	21
22	.286		.293	.342				.179	22
23	.274			.326			.367	.154	23
24	.273		.276	.310			.350	.128	24
25	.266		.253	.296			.320	.146	25
26	.196		.219	.262			.271	.114	26

$\alpha = 12$ $\delta = -10$

1	-.153		-.150	-.139			-.147	-.126	1
2	-.139		-.149	-.148			-.144	-.100	2
3	-.127		-.154	-.151			-.148	-.099	3
4	-.136		-.153	-.164			-.163	-.129	4
5	-.175		-.200	-.191			-.180	-.169	5
6	-.174		-.203	-.203			-.197	-.231	6
7	-.186		-.212	-.201			-.199	-.255	7
8	-.182		-.209	-.205			-.211		8
9	-.183		-.212	-.209			-.202	-.263	9
10	-.194		-.189	-.214			-.215	-.246	10
11	-.201		-.189	-.217			-.136	-.231	11
12	-.104		-.129	-.158			-.143	-.214	12
13	-.101		-.120	-.143			-.135	-.215	13
14	-.114		-.113	-.140			-.110	-.243	14
15	-.104		-.106	-.127			-.099	-.243	15
16	-.104		-.119	-.123			-.091	-.220	16
17	.472		.618	.559			.561	.519	17
18	.403		.565	.559			.559	.441	18
19	.393		.517	.562			.557	.363	19
20	.387		.437	.499			.504	.305	20
21	.273		.310	.379			.419	.215	21
22	.273		.291	.333				.172	22
23	.273			.321			.363	.140	23
24	.266		.277	.310			.343	.111	24
25	.266		.256	.289			.307	.147	25
26	.196		.223	.252			.269	.108	26

TABLE XIII.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.149		-.154	-.138			-.139	-.132	1
2	-.139		-.148	-.137			-.137	-.108	2
3	-.126		-.148	-.147			-.141	-.094	3
4	-.123		-.151	-.154			-.164	-.123	4
5	-.176		-.192	-.184			-.177	-.167	5
6	-.160		-.196	-.190			-.190	-.225	6
7	-.176		-.203	-.196			-.188	-.255	7
8	-.183		-.200	-.193			-.196		8
9	-.182		-.208	-.197			-.194	-.247	9
10	-.193		-.178	-.212			-.209	-.240	10
11	-.202		-.178	-.214			-.140	-.233	11
12	-.190		-.204	-.214			-.204	-.241	12
13	-.197		-.214	-.225			-.220	-.241	13
14	-.197		-.214	-.225			-.211	-.252	14
15	-.210		-.214	-.222			-.206	-.252	15
16	-.204		-.205	-.219			-.206	-.247	16
17	.481		.610	.564			.567	.519	17
18	.400		.565	.567			.559	.445	18
19	.393		.517	.569			.558	.365	19
20	.381		.440	.505			.513	.301	20
21	.275		.310	.384			.418	.223	21
22	.275		.291	.336				.167	22
23	.273			.325			.361	.137	23
24	.271		.275	.311			.341	.105	24
25	.267		.256	.289			.319	.142	25
26	.198		.225	.258			.269	.104	26

α=12 δ=10

1	-.151		-.152	-.139			-.135	-.135	1
2	-.139		-.150	-.144			-.140	-.106	2
3	-.129		-.152	-.148			-.147	-.095	3
4	-.130		-.148	-.161			-.158	-.127	4
5	-.174		-.197	-.190			-.179	-.173	5
6	-.166		-.194	-.199			-.197	-.237	6
7	-.181		-.210	-.199			-.203	-.266	7
8	-.186		-.200	-.196			-.207		8
9	-.180		-.211	-.210			-.211	-.266	9
10	-.190		-.179	-.203			-.214	-.247	10
11	-.197		-.179	-.210			-.133	-.228	11
12	-.233		-.240	-.233			-.238	-.265	12
13	-.250		-.260	-.268			-.266	-.256	13
14	-.250		-.270	-.252			-.257	-.273	14
15	-.259		-.242	-.232			-.257	-.284	15
16	-.182		-.197	-.202			-.215	-.277	16
17	.480		.609	.556			.558	.515	17
18	.409		.564	.563			.556	.434	18
19	.399		.516	.565			.554	.357	19
20	.387		.445	.503			.506	.305	20
21	.278		.313	.382			.418	.215	21
22	.281		.293	.339				.163	22
23	.275			.319			.363	.149	23
24	.274		.277	.309			.346	.109	24
25	.270		.251	.286			.312	.146	25
26	.196		.219	.256			.273	.097	26

TABLE XIII.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 3.6 \times 10^6$.

$\alpha = 12$ $\delta = 20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .164		- .157	- .143			- .145	- .129	1
2	- .145		- .151	- .143			- .146	- .100	2
3	- .133		- .154	- .148			- .145	- .087	3
4	- .137		- .161	- .162			- .161	- .115	4
5	- .192		- .201	- .201			- .179	- .154	5
6	- .175		- .199	- .201			- .193	- .229	6
7	- .190		- .215	- .192			- .200	- .260	7
8	- .189		- .203	- .202			- .203		8
9	- .187		- .212	- .208			- .200	- .260	9
10	- .198		- .193	- .211			- .215	- .233	10
11	- .199		- .193	- .218			- .142	- .211	11
12	- .261		- .263	- .263			- .264	- .283	12
13	- .270		- .263	- .273			- .286	- .283	13
14	- .240		- .242	- .256			- .278	- .296	14
15	- .231		- .237	- .251			- .263	- .288	15
16	- .227		- .237	- .242			- .249	- .283	16
17	.470		.607	.565			.566	.518	17
18	.395		.556	.560			.552	.442	18
19	.388		.517	.569			.552	.364	19
20	.377		.438	.498			.501	.310	20
21	.275		.301	.385			.413	.223	21
22	.273		.285	.340				.179	22
23	.265			.321			.363	.143	23
24	.262		.271	.306			.339	.109	24
25	.259		.253	.280			.315	.146	25
26	.361		.540	.584			.474	.102	26

$\alpha = 12$ $\delta = 30$

1	- .153		- .156	- .134			- .144	- .124	1
2	- .137		- .148	- .141			- .144	- .106	2
3	- .132		- .152	- .147			- .141	- .094	3
4	- .131		- .157	- .163			- .160	- .122	4
5	- .183		- .198	- .196			- .179	- .163	5
6	- .182		- .191	- .199			- .199	- .236	6
7	- .180		- .207	- .202			- .190	- .260	7
8	- .186		- .204	- .200			- .203		8
9	- .184		- .210	- .206			- .200	- .257	9
10	- .193		- .187	- .213			- .212	- .220	10
11	- .194		- .186	- .214			- .123	- .200	11
12	- .286		- .268	- .273			- .295	- .307	12
13	- .279		- .268	- .283			- .295	- .307	13
14	- .264		- .268	- .263			- .287	- .301	14
15	- .255		- .268	- .264			- .270	- .296	15
16	- .255		- .268	- .265			- .274	- .296	16
17	.476		.613	.556			.559	.509	17
18	.406		.560	.560			.553	.430	18
19	.396		.515	.561			.551	.364	19
20	.384		.436	.493			.506	.296	20
21	.273		.305	.375			.415	.219	21
22	.276		.289	.336				.159	22
23	.681			.740			.757	.364	23
24	.707		.699	.770			.787	.377	24
25	.708		.733	.789			.800	.443	25
26	.706		.741	.789			.801	.443	26

TABLE XIV

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.627		.857	.898			.893	.837	1
2	.469		.759	.849			.889	.667	2
3	.544		.686	.798			.830	.563	3
4	.559		.591	.664			.698	.437	4
5	.398		.432	.527			.569	.333	5
6	.413		.410	.469			.515	.226	6
7	.400		.388	.434			.481	.164	7
8	.393		.388	.430			.456		8
9	.364		.364	.408			.403	.164	9
10	.317		.352	.369			.325	.164	10
11	.349		.352	.347			.381	.142	11
12	.289		.248	.292			.255	.075	12
13	.245		.245	.258			.245	.050	13
14	.230		.248	.258			.255	.047	14
15	.245		.248	.255			.242	.047	15
16	.230		.242	.255			.217	.013	16
17	-.210		-.198	-.203			-.190	-.154	17
18	-.166		-.203	-.210			-.195	-.107	18
19	-.188		-.205	-.210			-.205	-.142	19
20	-.200		-.210	-.222			-.225	-.173	20
21	-.222		-.259	-.251			-.251	-.208	21
22	-.232		-.256	-.247				-.233	22
23	-.244			-.259			-.254	-.252	23
24	-.244		-.251	-.264			-.259	-.296	24
25	-.244		-.249	-.271			-.266	-.242	25
26	-.244		-.269	-.273			-.264	-.248	26

α=-12 δ=-30

1	.498		.642	.627			.627	.613	1
2	.413		.603	.603			.605	.509	2
3	.422		.564	.618			.610	.428	3
4	.422		.491	.552			.542	.330	4
5	.286		.327	.427			.459	.261	5
6	.288		.312	.391			.398	.192	6
7	.378		.508	.723			.618	.123	7
8	.715		.715	.810			.796		8
9	.737		.735	.747			.862	.418	9
10	.762		.820	.837			.859	.472	10
11	.769		.810	.852			.945	.465	11
12	.865		.874	.912			.925	.478	12
13	.896		.928	.912			.925	.513	13
14	1.157		1.085	1.063			1.066	.689	14
15	1.289		1.211	1.230			1.211	.843	15
16	1.186		1.135	1.157			1.161	.821	16
17	-.168		-.176	-.168			-.144	-.101	17
18	-.161		-.183	-.181			-.159	-.079	18
19	-.154		-.195	-.183			-.188	-.101	19
20	-.161		-.190	-.195			-.190	-.120	20
21	-.195		-.225	-.225			-.227	-.173	21
22	-.222		-.247	-.227				-.242	22
23	-.229			-.234			-.227	-.255	23
24	-.227		-.222	-.239			-.237	-.299	24
25	-.229		-.237	-.254			-.239	-.242	25
26	-.232		-.271	-.266			-.249	-.236	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.503		.625	.637			.615	.594	1
2	.386		.588	.588			.613	.491	2
3	.425		.547	.600			.605	.399	3
4	.398		.466	.527			.542	.321	4
5	.303		.330	.410			.454	.252	5
6	.300		.303	.371			.410	.176	6
7	.281		.271	.334			.403	.113	7
8	.273		.278	.330			.371		8
9	.264		.242	.305			.332	.126	9
10	.207		.276	.286			.290	.126	10
11	.530		.276	.608			.676	.126	11
12	.711		.723	.742			.761	.421	12
13	.824		.815	.846			.846	.497	13
14	.887		.890	.953			.921	.541	14
15	.909		.928	.975			.906	.538	15
16	.865		.862	.881			.833	.491	16
17	-.168		-.168	-.183			-.154	-.132	17
18	-.171		-.198	-.181			-.164	-.082	18
19	-.161		-.210	-.178			-.195	-.120	19
20	-.173		-.203	-.193			-.188	-.170	20
21	-.222		-.237	-.222			-.220	-.195	21
22	-.232		-.251	-.239				-.248	22
23	-.242			-.239			-.242	-.252	23
24	-.244		-.244	-.242			-.249	-.299	24
25	-.237		-.269	-.256			-.249	-.255	25
26	-.247		-.283	-.276			-.244	-.236	26

α=-12 δ=-10

1	.525		.627	.640			.632	.616	1
2	.391		.603	.600			.622	.500	2
3	.425		.557	.610			.622	.428	3
4	.425		.478	.539			.564	.340	4
5	.283		.325	.417			.476	.277	5
6	.290		.317	.371			.437	.145	6
7	.293		.276	.339			.420	.120	7
8	.276		.288	.347			.400		8
9	.276		.259	.315			.361	.120	9
10	.215		.254	.290			.288	.120	10
11	.217		.254	.266			.354	.097	11
12	.462		.437	.453			.487	.217	12
13	.437		.437	.481			.481	.217	13
14	.431		.453	.478			.462	.192	14
15	.428		.450	.491			.459	.195	15
16	.421		.450	.472			.425	.179	16
17	-.168		-.168	-.183			-.146	-.126	17
18	-.159		-.178	-.164			-.144	-.088	18
19	-.156		-.190	-.166			-.173	-.110	19
20	-.154		-.195	-.168			-.181	-.148	20
21	-.215		-.234	-.203			-.220	-.179	21
22	-.212		-.242	-.220				-.239	22
23	-.212			-.220			-.220	-.255	23
24	-.225		-.249	-.237			-.242	-.286	24
25	-.227		-.249	-.244			-.237	-.245	25
26	-.244		-.271	-.239			-.237	-.245	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.549		.652	.642			.632	.579	1
2	.427		.622	.635			.630	.478	2
3	.449		.586	.630			.627	.434	3
4	.459		.515	.564			.561	.321	4
5	.317		.347	.439			.474	.236	5
6	.330		.330	.405			.413	.173	6
7	.337		.312	.366			.425	.113	7
8	.295		.325	.349			.393		8
9	.298		.286	.322			.359	.113	9
10	.237		.290	.295			.305	.113	10
11	.251		.290	.276			.356	.097	11
12	.201		.189	.214			.204	.047	12
13	.189		.170	.192			.204	.031	13
14	.145		.170	.204			.201	.019	14
15	.170		.170	.192			.176	.019	15
16	.164		.170	.211			.154	.003	16
17	-.146		-.149	-.164		- .154	-.145		17
18	-.139		-.161	-.173		- .154	-.110		18
19	-.134		-.166	-.164		- .176	-.135		19
20	-.151		-.164	-.176		- .188	-.167		20
21	-.198		-.212	-.207		- .227	-.201		21
22	-.200		-.222	-.229			-.267		22
23	-.215			-.234		- .229	-.267		23
24	-.212		-.210	-.239		- .229	-.302		24
25	-.217		-.227	-.249		- .229	-.258		25
26	-.229		-.244	-.249		- .229	-.258		26

α=-12 δ=10

1	.530		.652	.640			.630	.607	1
2	.417		.622	.618			.620	.503	2
3	.452		.581	.620			.618	.399	3
4	.454		.513	.559			.544	.343	4
5	.317		.342	.437			.459	.277	5
6	.315		.332	.393			.417	.157	6
7	.339		.342	.383			.442	.110	7
8	.315		.322	.356			.415		8
9	.300		.310	.427			.376	.173	9
10	.244		.315	.325			.332	.211	10
11	.256		.315	.308			.378	.151	11
12	.044		.088	.170			.053	-.009	12
13	.057		.009	.031			.022	-.009	13
14	.038		.009	.075			.019	-.028	14
15	.006		.009	.025			.019	-.028	15
16	.063		.035	.025		- .003	-.063		16
17	-.161		-.164	-.188		- .161	-.101		17
18	-.142		-.178	-.186		- .146	-.072		18
19	-.149		-.195	-.166		- .178	-.091		19
20	-.156		-.183	-.178		- .171	-.157		20
21	-.188		-.225	-.220		- .217	-.192		21
22	-.205		-.239	-.227			-.239		22
23	-.210			-.229		- .234	-.261		23
24	-.212		-.225	-.237		- .229	-.292		24
25	-.215		-.247	-.247		- .242	-.261		25
26	-.227		-.254	-.251		- .237	-.245		26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.500		.635	.613			.630	.616	1
2	.391		.610	.600			.613	.491	2
3	.427		.559	.608			.613	.447	3
4	.434		.486	.539			.552	.343	4
5	.293		.315	.410			.469	.258	5
6	.303		.312	.361			.420	.179	6
7	.298		.288	.352			.408	.145	7
8	.276		.295	.330			.364		8
9	.269		.261	.303			.337	.135	9
10	.198		.264	.276			.269	.135	10
11	.220		.266	.242			.337	.120	11
12	-.091		-.085	-.063			-.091	-.151	12
13	-.097		-.129	-.116			-.120	-.170	13
14	-.123		-.129	-.120			-.120	-.182	14
15	-.145		-.129	-.138			-.142	-.192	15
16	-.113		-.120	-.120			-.142	-.182	16
17	-.173		-.195	-.207			-.156	-.104	17
18	-.156		-.193	-.188			-.166	-.082	18
19	-.164		-.186	-.176			-.195	-.094	19
20	-.161		-.198	-.188			-.200	-.123	20
21	-.210		-.244	-.222			-.237	-.154	21
22	-.220		-.244	-.239				-.245	22
23	-.217			-.227			-.237	-.245	23
24	-.220		-.217	-.210			-.225	-.283	24
25	-.232		-.237	-.217			-.227	-.255	25
26	-.247		-.254	-.227			-.225	-.230	26

α=-12 δ=30

1	.493		.640	.625			.605	.604	1
2	.381		.593	.598			.613	.484	2
3	.410		.564	.613			.622	.434	3
4	.439		.474	.552			.552	.318	4
5	.303		.320	.427			.469	.239	5
6	.290		.303	.381			.415	.179	6
7	.298		.288	.349			.413	.113	7
8	.283		.305	.334			.386		8
9	.276		.261	.310			.356	.113	9
10	.210		.251	.278			.293	.113	10
11	.217		.251	.266			.339	.091	11
12	-.198		-.189	-.157			-.189	-.217	12
13	-.198		-.220	-.201			-.223	-.217	13
14	-.230		-.220	-.198			-.223	-.217	14
15	-.223		-.208	-.217			-.223	-.211	15
16	-.170		-.204	-.201			-.223	-.214	16
17	-.173		-.159	-.173			-.144	-.120	17
18	-.142		-.183	-.176			-.154	-.101	18
19	-.161		-.188	-.183			-.176	-.123	19
20	-.173		-.195	-.193			-.159	-.142	20
21	-.215		-.227	-.195			-.195	-.189	21
22	-.227		-.227	-.195				-.248	22
23	-.217			-.183			-.176	-.270	23
24	-.220		-.198	-.181			-.178	-.286	24
25	-.193		-.188	-.188			-.171	-.258	25
26	-.159		-.161	-.171			-.146	-.233	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha = -9$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.400		.427	.456			.449	.434	1
2	.276		.442	.444			.452	.371	2
3	.315		.434	.434			.459	.324	3
4	.320		.386	.393			.393	.220	4
5	.186		.217	.293			.339	.170	5
6	.220		.207	.266			.290	.126	6
7	.222		.200	.251			.286	.060	7
8	.193		.205	.242			.276		8
9	.183		.178	.229			.254	.060	9
10	.134		.188	.207			.205	.082	10
11	.144		.188	.183			.283	.041	11
12	.101		.075	.094			.091	- .035	12
13	.066		.060	.066			.072	- .050	13
14	.047		.057	.063			.072	- .072	14
15	.069		.057	.060			.050	- .072	15
16	.041		.057	.057			.038	- .072	16
17	- .124		- .115	- .134		-	.112	- .079	17
18	- .117		- .142	- .139		-	.124	- .041	18
19	- .105		- .142	- .127		-	.144	- .072	19
20	- .115		- .154	- .142		-	.134	- .120	20
21	- .178		- .195	- .181		-	.186	- .145	21
22	- .195		- .200	- .181				- .195	22
23	- .183			- .193		-	.186	- .220	23
24	- .198		- .205	- .190		-	.198	- .270	24
25	- .200		- .210	- .203		-	.200	- .226	25
26	- .203		- .232	- .205		-	.198	- .230	26

$\alpha = -6$ $\delta = -30$

1	.293		.300	.339			.317	.330	1
2	.210		.308	.315			.300	.248	2
3	.220		.300	.305			.305	.204	3
4	.225		.254	.264			.261	.135	4
5	.132		.156	.200			.193	.107	5
6	.122		.149	.168			.166	.044	6
7	.134		.107	.166			.168	.013	7
8	.120		.120	.173			.156		8
9	.342		.371	.334			.456	.044	9
10	.456		.471	.503			.510	.138	10
11	.537		.471	.554			.642	.170	11
12	.610		.582	.616			.623	.248	12
13	.720		.654	.629			.654	.425	13
14	1.010		.890	.871			.871	.755	14
15	1.035		1.035	1.041			1.019	.730	15
16	.956		.984	.997			.972	.654	16
17	- .032		- .041	- .083		-	.054	- .019	17
18	- .041		- .068	- .081		-	.049	- .028	18
19	- .059		- .063	- .063		-	.059	- .006	19
20	- .071		- .068	- .088		-	.081	- .047	20
21	- .124		- .129	- .124		-	.129	- .069	21
22	- .139		- .156	- .134				- .047	22
23	- .134			- .149		-	.129	- .085	23
24	- .154		- .127	- .139		-	.149	- .132	24
25	- .137		- .156	- .173		-	.151	- .082	25
26	- .171		- .176	- .176		-	.168	- .085	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-6 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.303		.288	.312			.305	.330	1
2	.183		.300	.303			.310	.245	2
3	.229		.308	.298			.310	.208	3
4	.203		.269	.261			.264	.138	4
5	.105		.137	.195			.212	.088	5
6	.105		.127	.156			.178	.028	6
7	.115		.110	.171			.181	- .009	7
8	.103		.129	.166			.144		8
9	.110		.090	.137			.146	.006	9
10	.051		.127	.117			.088	.028	10
11	.149		.127	.149			.290	.013	11
12	.487		.447	.462			.503	.138	12
13	.566		.544	.572			.582	.349	13
14	.585		.582	.629			.642	.384	14
15	.601		.626	.638			.620	.343	15
16	.569		.588	.638			.579	.299	16
17	- .032	- .041	~	.066		-	.059	- .025	17
18	- .059	- .073	~	.063		-	.073	.000	18
19	- .068	- .066	~	.046		-	.059	- .019	19
20	- .071	- .068	~	.073		-	.066	- .050	20
21	- .122	- .134	~	.124		-	.137	- .053	21
22	- .139	- .137	~	.134				- .053	22
23	- .149		~	.149		-	.142	- .075	23
24	- .154	- .139	~	.149		-	.176	- .182	24
25	- .146	- .168	~	.168		-	.171	- .107	25
26	- .181	- .178	~	.178		-	.181	- .126	26

α=-6 δ=-10

1	.305		.305	.342			.303	.340	1
2	.195		.320	.330			.315	.255	2
3	.237		.317	.334			.327	.220	3
4	.232		.293	.278			.266	.164	4
5	.132		.156	.198			.210	.094	5
6	.132		.166	.190			.178	.072	6
7	.142		.127	.161			.186	.031	7
8	.124		.146	.159			.156		8
9	.120		.115	.132			.149	.013	9
10	.061		.139	.110			.112	.044	10
11	.085		.137	.095			.210	.013	11
12	.264		.239	.252			.264	.075	12
13	.264		.239	.252			.264	.116	13
14	.230		.248	.264			.264	.097	14
15	.270		.264	.264			.239	.094	15
16	.236		.252	.264			.220	.075	16
17	- .054	- .041	~	.071		-	.046	- .041	17
18	- .066	- .051	~	.071		-	.078	.003	18
19	- .051	- .049	~	.063		-	.081	- .031	19
20	- .063	- .054	~	.081		-	.071	- .044	20
21	- .124	- .112	~	.122		-	.132	- .050	21
22	- .124	- .129	~	.137				- .050	22
23	- .129		~	.144		-	.154	- .088	23
24	- .134	- .124	~	.146		-	.161	- .182	24
25	- .129	- .159	~	.168		-	.178	- .113	25
26	- .166	- .178	~	.163		-	.176	- .151	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha=-6$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta. 8	
1	.312		.293	.339			.344	.343	1
2	.195		.325	.342			.337	.280	2
3	.227		.332	.317			.317	.252	3
4	.232		.303	.271			.293	.182	4
5	.129		.154	.200			.225	.116	5
6	.173		.144	.195			.190	.082	6
7	.161		.139	.190			.200	.047	7
8	.124		.137	.183			.188		8
9	.127		.112	.176			.161	.041	9
10	.063		.134	.134			.124	.041	10
11	.098		.134	.120			.227	.031	11
12	.066		.050	.072			.066	- .044	12
13	.038		.025	.019			.028	- .063	13
14	.013		.025	.044			.038	- .101	14
15	.047		.044	.044			.038	- .101	15
16	.016		.019	.044			.019	- .079	16
17	- .066	-	.063	- .081		-	.059	- .038	17
18	- .081	-	.093	- .066		-	.088	- .006	18
19	- .059	-	.090	- .059		-	.068	- .041	19
20	- .083	-	.078	- .081		-	.088	- .069	20
21	- .142	-	.144	- .124		-	.139	- .088	21
22	- .159	-	.159	- .137				- .088	22
23	- .142			- .144		-	.144	- .126	23
24	- .139	-	.159	- .139		-	.164	- .189	24
25	- .156	-	.176	- .176		-	.186	- .132	25
26	- .186	-	.183	- .171		-	.188	- .170	26

$\alpha=-6$ $\delta=10$

1	.308		.303	.332			.300	.333	1
2	.200		.312	.317			.308	.264	2
3	.234		.310	.327			.305	.230	3
4	.227		.278	.273			.261	.157	4
5	.115		.151	.203			.205	.116	5
6	.144		.137	.171			.171	.072	6
7	.132		.115	.161			.173	.028	7
8	.112		.129	.151			.154		8
9	.122		.122	.181			.168	.028	9
10	.073		.149	.139			.137	.060	10
11	.098		.149	.124			.227	.035	11
12	- .069	-	.057	.019		-	.053	- .132	12
13	- .063	-	.101	- .091		-	.094	- .123	13
14	- .063	-	.101	- .038		-	.075	- .104	14
15	- .104	-	.101	- .097		-	.101	- .104	15
16	- .053	-	.101	- .094		-	.101	- .104	16
17	- .061	-	.056	- .081		-	.046	- .006	17
18	- .029	-	.061	- .066		-	.061	.016	18
19	- .061	-	.061	- .059		-	.066	- .006	19
20	- .061	-	.073	- .088		-	.083	- .041	20
21	- .127	-	.132	- .144		-	.127	- .044	21
22	- .132	-	.134	- .134				- .044	22
23	- .134			- .139		-	.127	- .069	23
24	- .134	-	.132	- .142		-	.142	- .123	24
25	- .127	-	.144	- .151		-	.132	- .075	25
26	- .159	-	.171	- .168		-	.132	- .116	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=-6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.295		.288	.322			.342	.296	1
2	.176		.312	.308			.325	.220	2
3	.215		.310	.322			.320	.189	3
4	.200		.276	.266			.264	.138	4
5	.110		.151	.193			.210	.063	5
6	.122		.122	.164			.181	.019	6
7	.120		.110	.166			.178	-.028	7
8	.105		.124	.161			.159		8
9	.107		.098	.146			.161	-.025	9
10	.051		.112	.112			.105	-.006	10
11	.068		.112	.105			.227	-.031	11
12	-.182	-.182	-.148		-.176		-.226		12
13	-.186	-.226	-.217		-.223		-.217		13
14	-.211	-.226	-.208		-.220		-.201		14
15	-.211	-.211	-.220		-.220		-.182		15
16	-.186	-.214	-.211		-.208		-.182		16
17	-.063	-.049	-.066		-.041		-.053		17
18	-.051	-.066	-.063		-.032		-.009		18
19	-.056	-.066	-.056		-.061		-.038		19
20	-.076	-.076	-.083		-.081		-.082		20
21	-.146	-.122	-.115		-.129		-.082		21
22	-.139	-.139	-.139				-.060		22
23	-.127		-.117		-.105		-.104		23
24	-.144	-.139	-.117		-.095		-.142		24
25	-.139	-.149	-.122		-.105		-.091		25
26	-.173	-.159	-.120		-.095		-.151		26

α=-6 δ=30

1	.298		.300	.310			.317	.315	1
2	.200		.317	.308			.312	.230	2
3	.229		.315	.322			.308	.211	3
4	.225		.278	.273			.259	.132	4
5	.127		.154	.205			.198	.069	5
6	.129		.122	.176			.178	.041	6
7	.134		.115	.159			.171	-.003	7
8	.124		.124	.151			.154		8
9	.120		.088	.127			.146	-.003	9
10	.073		.117	.105			.098	.022	10
11	.083		.117	.112			.217	.022	11
12	-.267	-.264	-.233		-.258		-.267		12
13	-.252	-.286	-.280		-.280		-.245		13
14	-.252	-.274	-.258		-.258		-.248		14
15	-.255	-.261	-.274		-.261		-.248		15
16	-.233	-.261	-.258		-.261		-.277		16
17	-.029	-.032	-.073		-.068		-.028		17
18	-.061	-.054	-.076		-.073		.006		18
19	-.054	-.063	-.059		-.083		-.022		19
20	-.063	-.071	-.081		-.098		-.053		20
21	-.117	-.134	-.107		-.107		-.038		21
22	-.124	-.105	-.093				-.038		22
23	-.122		-.085		-.076		-.038		23
24	-.071	-.066	-.073		-.068		-.069		24
25	-.007	-.027	-.024		-.046		-.038		25
26	.034	.037	-.020		-.002		-.035		26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha=-3$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.188		.195	.207			.212	.208	1
2	.105		.210	.229			.212	.164	2
3	.151		.210	.195			.210	.142	3
4	.127		.195	.156			.171	.075	4
5	.056		.098	.093			.117	.038	5
6	.073		.056	.103			.083	.000	6
7	.059		.034	.068			.090	-.022	7
8	.044		.054	.056			.068		8
9	.034		.039	.054			.044	-.019	9
10	-.002		.066	.034			.029	-.003	10
11	-.012		.066	.029			.171	-.028	11
12	-.041	-.053	-.050			-.035	-.079		12
13	-.060	-.085	-.069			-.072	-.094		13
14	-.079	-.085	-.069			-.072	-.094		14
15	-.053	-.085	-.069			-.072	-.094		15
16	-.088	-.085	-.053			-.097	-.088		16
17	.007		.032	-.005			.022	.003	17
18	-.024		.007	.000			.002	.019	18
19	.010		.005	.005			.000	-.006	19
20	-.015	-.007	-.024			-.007	-.041		20
21	-.098	-.083	-.073			-.061	-.041		21
22	-.088	-.090	-.085				-.041		22
23	-.107		-.098			-.083	-.031		23
24	-.085	-.081	-.107			-.088	-.066		24
25	-.076	-.081	-.083			-.090	-.019		25
26	-.110	-.110	-.085			-.098	-.041		26

$\alpha=0$ $\delta=-30$

1	.104		.102	.112			.114	.101	1
2	.039		.109	.107			.114	.073	2
3	.080		.104	.097			.109	.069	3
4	.058		.092	.075			.070	.041	4
5	-.015		.002	.010			.024	-.028	5
6	-.019	-.002	-.005				.034	.009	6
7	-.017	-.029	-.007				.041	-.006	7
8	-.017	-.005	.032				.051		8
9	.209	.180	.109				.124	-.006	9
10	.328	.267	.313				.199	.066	10
11	.352	.267	.350				.379	.092	11
12	.404	.363	.392				.325	.120	12
13	.512	.480	.426				.411	.243	13
14	.777	.755	.651				.660	.578	14
15	.885	.869	.828				.790	.610	15
16	.812	.834	.843				.774	.509	16
17	.112	.109	.102				.117	.101	17
18	.085	.109	.107				.122	.088	18
19	.075	.104	.107				.104	.057	19
20	.058	.080	.078				.080	.013	20
21	-.015	-.007	.022				.017	-.016	21
22	-.010	-.012	.002					-.003	22
23	-.012		-.005			-.002		.003	23
24	-.015	-.022	-.005			-.010		-.032	24
25	-.019	-.034	-.015			-.022		.022	25
26	-.056	-.063	-.036			-.039		-.019	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=0 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.117		.100	.117			.112	.098	1
2	.051		.112	.107			.119	.060	2
3	.075		.104	.102			.112	.082	3
4	.070		.085	.080			.073	.035	4
5	-.005		.012	.012			.029	-.016	5
6	-.012		.000	-.002		-.005	.006		6
7	-.017	-.022	-.005			.000	-.069		7
8	-.015	-.019	-.002			-.017			8
9	-.017	-.029	-.012			.000	-.003		9
10	-.015	.012	-.032			-.007	.003		10
11	.063	.005	-.019			.177	.006		11
12	.234	.205	.246			.028	.000		12
13	.278	.325	.325			.148	.035		13
14	.303	.363	.370			.240	.140		14
15	.366	.379	.392			.385	.190		15
16	.319	.366	.395			.360	.139		16
17	.117	.112	.104			.117	.101		17
18	.087	.102	.109			.119	.085		18
19	.085	.102	.112			.107	.057		19
20	.063	.083	.078			.083	.009		20
21	-.015	.002	.017			.017	-.013		21
22	-.005	-.012	.000				-.003		22
23	-.007		-.005			.002	-.013		23
24	-.007	-.019	-.002			.000	-.057		24
25	-.017	-.034	-.015			-.015	-.022		25
26	-.058	-.061	-.036			-.032	-.054		26

α=0 δ=-10

1	.095		.092	.117			.102	.095	1
2	.039		.107	.109			.114	.063	2
3	.070		.104	.100			.107	.057	3
4	.070		.085	.075			.070	.032	4
5	-.007		.000	.012			.024	-.022	5
6	-.010		.000	-.005		-.010	-.016		6
7	-.017	-.024	-.010			-.007	-.063		7
8	-.017	-.024	-.007			-.019			8
9	-.027	-.036	-.015			-.032	-.016		9
10	-.019	.012	-.039			-.058	-.032		10
11	-.044	.012	-.053			.134	-.022		11
12	.057	.038	.057			.009	-.016		12
13	.063	.073	.079			.047	.028		13
14	.044	.079	.092			.076	.028		14
15	.085	.085	.092			.079	.006		15
16	.059	.069	.098			.063	-.016		16
17	.107	.109	.097			.109	.095		17
18	.080	.100	.102			.112	.079		18
19	.075	.097	.107			.100	.047		19
20	.058	.080	.068			.075	.003		20
21	-.015	.000	.010			.012	-.016		21
22	-.012	-.015	-.002				-.006		22
23	-.010		-.012			-.010	-.009		23
24	-.017	-.022	-.012			-.010	-.054		24
25	-.017	-.034	-.022			-.029	-.013		25
26	-.063	-.063	-.046			-.046	-.054		26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=0 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.109		.102	.119			.117	.117	1
2	.049		.107	.112			.119	.079	2
3	.080		.109	.097			.112	.104	3
4	.061		.085	.078			.080	.066	4
5	-.010		.007	.017			.024	.003	5
6	-.012		.000	.000		-.005		.013	6
7	-.010	-.019	-.010			-.002	-.038		7
8	-.010	-.019	-.005			-.012			8
9	-.015	-.027	-.010			-.022	.028		9
10	-.024	.012	-.029			-.044	-.006		10
11	-.046	.012	-.041			.122	-.035		11
12	-.069	-.069	-.066			-.076	-.095		12
13	-.069	-.098	-.098			-.104	-.069		13
14	-.104	-.101	-.082			-.092	-.066		14
15	-.082	-.095	-.095			-.101	-.054		15
16	-.111	-.101	-.088			-.107	-.060		16
17	.109		.117	.104			.122	.104	17
18	.090		.100	.119			.119	.107	18
19	.075		.104	.104			.119	.076	19
20	.058		.080	.078			.083	.028	20
21	-.015		.000	.015			.017	.003	21
22	-.010	-.010	-.005					.019	22
23	-.007			.000			.007	.003	23
24	-.012	-.017	-.002				.000	-.025	24
25	-.015	-.032	-.015			-.024		.035	25
26	-.061	-.058	-.034			-.041	-.028		26

α=0 δ=10

1	.102		.104	.117			.114	.098	1
2	.051		.112	.117			.117	.054	2
3	.080		.102	.102			.109	.054	3
4	.068		.090	.080			.080	.025	4
5	-.015		.007	.022			.027	-.032	5
6	-.005		.002	.002			.007	-.013	6
7	-.015	-.019	-.002				.012	-.063	7
8	-.015	-.017	.000			-.010			8
9	-.010	.000	.068			-.002	-.009		9
10	-.012	.046	.007			-.010	-.019		10
11	-.022	.049	-.005			.139	-.035		11
12	-.161	-.060	-.136			-.139	-.139		12
13	-.085	-.174	-.174			-.164	-.120		13
14	-.076	-.167	-.123			-.139	-.085		14
15	-.174	-.177	-.167			-.145	-.114		15
16	-.111	-.174	-.161			-.152	-.171		16
17	.114		.117	.095			.117	.088	17
18	.080		.107	.104			.119	.092	18
19	.078		.109	.107			.107	.044	19
20	.063		.085	.075			.083	-.003	20
21	-.015		.000	.015			.019	-.022	21
22	-.007	-.010	.000					-.019	22
23	-.010		-.007			-.002	-.009		23
24	-.017	-.015	-.007			-.002	-.054		24
25	-.017	-.027	-.022			-.022	-.013		25
26	-.058	-.058	-.036			-.007	-.047		26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha=0$ $\delta=20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.117		.107	.122			.117	.111	1
2	.053		.114	.117			.119	.082	2
3	.085		.107	.104			.114	.073	3
4	.073		.090	.075			.080	.047	4
5 -	.012		.010	.022			.034	.003	5
6 -	.005		.005	.005		- .002		.006	6
7 -	.015	- .015	- .005				.007	- .051	7
8 -	.012	- .012	- .002			- .005			8
9 -	.019	- .027	.024			- .019		- .006	9
10 -	.010	.022	- .024			- .039		- .019	10
11 -	.039	.022	- .034			.126		- .006	11
12 -	.240	- .199	- .221			- .221		- .215	12
13 -	.193	- .253	- .262			- .256		- .177	13
14 -	.227	- .278	- .231			- .224		- .215	14
15 -	.265	- .256	- .259			- .227		- .234	15
16 -	.183	- .231	- .224			- .240		- .278	16
17	.122	.112	.095			.114		.104	17
18	.087	.109	.107			.119		.092	18
19	.078	.107	.109			.107		.060	19
20	.068	.090	.080			.083		.028	20
21 -	.010	.007	.019			.029		.006	21
22 -	.002	- .007	.007					.003	22
23 -	.002	-	.002			.017		.003	23
24 -	.010	- .015	.002			.029		- .032	24
25 -	.007	- .027	.007			.032		.035	25
26 -	.044	- .044	.002			.041		.000	26

$\alpha=0$ $\delta=30$

1	.117		.109	.124			.117	.136	1
2	.061		.112	.117			.122	.085	2
3	.083		.107	.102			.119	.101	3
4	.070		.092	.085			.083	.076	4
5 -	.007		.007	.019			.034	.009	5
6	.002		.007	.002			.000	.028	6
7 -	.005	- .015	- .005				.005	- .025	7
8 -	.007	- .019	.000			- .012			8
9 -	.010	- .027	.005			- .019		.000	9
10 -	.005	.015	- .029			- .041		.028	10
11 -	.039	.015	- .041			.139		.044	11
12 -	.272	- .240	- .259			- .281		- .262	12
13 -	.221	- .284	- .291			- .294		- .215	13
14 -	.262	- .269	- .265			- .253		- .269	14
15 -	.269	- .259	- .284			- .275		- .294	15
16 -	.221	- .246	- .262			- .284		- .313	16
17	.114	.112	.104			.117		.107	17
18	.085	.104	.109			.122		.126	18
19	.080	.102	.107			.107		.085	19
20	.070	.085	.083			.087		.032	20
21 -	.007	.005	.017			.034		.006	21
22 -	.010	- .010	.036					.016	22
23 -	.007		.046			.080		.057	23
24 -	.012	.070	.119			.119		.009	24
25	.231	.236	.185			.177		.066	25
26	.275	.321	.265			.253		.139	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha=3$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.041		.029	.049			.039	.057	1
2	-.007		.039	.049			.051	.063	2
3	.022		.046	.032			.034	.057	3
4	.007		.044	.007			.005	.038	4
5	-.063	-.046	-.046			-.034	-.013		5
6	-.044	-.056	-.044			-.061	.013		6
7	-.051	-.070	-.075			-.056	-.038		7
8	-.070	-.073	-.070			-.075			8
9	-.070	-.075	-.039			-.090	-.006		9
10	-.068	-.015	-.095			-.102	-.019		10
11	-.092	-.015	-.102			.095	-.035		11
12	-.098	-.117	-.114			-.126	-.123		12
13	-.114	-.123	-.136			-.148	-.101		13
14	-.114	-.133	-.126			-.117	-.126		14
15	-.104	-.120	-.133			-.120	-.133		15
16	-.120	-.139	-.123			-.111	-.158		16
17	.207	.207	.182			.202	.196		17
18	.139	.194	.194			.185	.174		18
19	.158	.194	.187			.192	.130		19
20	.139	.175	.163			.156	.092		20
21	.053	.073	.090			.102	.047		21
22	.056	.051	.073				.025		22
23	.044		.063			.070	.032		23
24	.041	.051	.070			.068	-.016		24
25	.049	.041	.056			.051	.051		25
26	.015	.010	.039			.034	-.028		26

$\alpha=6$ $\delta=-30$

1	-.044	-.053	-.041			-.046	-.054		1
2	-.078	-.053	-.044			-.044	-.025		2
3	-.044	-.051	-.051			-.053	-.009		3
4	-.066	-.051	-.066			-.078	-.035		4
5	-.129	-.136	-.122			-.087	-.057		5
6	-.126	-.124	-.117			-.087	-.066		6
7	-.129	-.136	-.114			-.073	-.148		7
8	-.134	-.114	-.095			-.078			8
9	-.134	-.085	-.090			-.066	-.107		9
10	-.005	.053	-.015			-.051	-.111		10
11	.114	.053	.007			.163	-.079		11
12	.171	.066	.085			.032	.256		12
13	.322	.148	.101			.057	.493		13
14	.433	.382	.332			.287	.262		14
15	.474	.502	.468			.411	.401		15
16	.505	.524	.505			.452	.338		16
17	.316	.318	.304			.323	.303		17
18	.236	.318	.309			.321	.253		18
19	.238	.309	.304			.316	.193		19
20	.219	.282	.272			.272	.161		20
21	.122	.151	.190			.204	.088		21
22	.124	.131	.170				.060		22
23	.124		.160			.168	.032		23
24	.117	.126	.158			.160	-.028		24
25	.119	.107	.141			.146	.041		25
26	.063	.075	.109			.117	-.076		26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

$\alpha = 6$ $\delta = -20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.036		-.044	-.034			-.034	-.041	1
2	-.063		-.044	-.041			-.029	-.006	2
3	-.034		-.036	-.046			-.036	-.016	3
4	-.056		-.039	-.075			-.066	-.025	4
5	-.124		-.129	-.117			-.097	-.069	5
6	-.109		-.118	-.126			-.126	-.079	6
7	-.114		-.134	-.143			-.097	-.152	7
8	-.129		-.134	-.124			-.097		8
9	-.126		-.129	-.104			-.085	-.092	9
10	-.114		-.032	-.104			-.090	-.155	10
11	-.075		-.032	-.107			-.117	-.145	11
12	.073		-.069	-.082			-.057	-.120	12
13	.123		.057	-.069			-.079	.022	13
14	.145		.186	.161			.044	-.148	14
15	.180		.190	.212			.177	-.044	15
16	.161		.183	.202			.196	.022	16
17	.321		.323	.309			.328	.297	17
18	.243		.333	.311			.330	.256	18
19	.243		.316	.313			.318	.196	19
20	.226		.292	.277			.284	.126	20
21	.131		.160	.204			.211	.082	21
22	.129		.139	.180				.057	22
23	.131			.173			.177	.038	23
24	.126		.131	.170			.175	-.026	24
25	.124		.112	.151			.153	.038	25
26	.073		.087	.122			.126	-.073	26

$\alpha = 6$ $\delta = -10$

1	-.053		-.051	-.046			-.036	-.041	1
2	-.078		-.046	-.039			-.027	-.009	2
3	-.053		-.039	-.046			-.041	.025	3
4	-.070		-.032	-.070			-.073	-.003	4
5	-.124		-.126	-.117			-.100	-.051	5
6	-.114		-.112	-.124			-.126	-.041	6
7	-.112		-.129	-.134			-.119	-.117	7
8	-.131		-.134	-.136			-.131		8
9	-.129		-.143	-.107			-.124	-.047	9
10	-.126		-.050	-.134			-.124	-.120	10
11	-.148		-.056	-.134			-.100	-.123	11
12	-.032		-.123	-.114			-.107	-.171	12
13	-.041		-.062	-.114			-.117	-.139	13
14	-.066		-.047	-.095			-.082	-.199	14
15	-.019		-.032	-.069			-.066	-.167	15
16	-.047		-.054	-.035			-.095	-.136	16
17	.311		.323	.304			.328	.329	17
18	.228		.323	.311			.328	.281	18
19	.233		.316	.311			.321	.221	19
20	.224		.279	.275			.282	.155	20
21	.124		.153	.199			.204	.111	21
22	.126		.134	.180				.082	22
23	.124			.173			.175	.051	23
24	.122		.131	.170			.173	.003	24
25	.124		.107	.151			.148	.060	25
26	.063		.076	.114			.124	-.057	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=6 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.036		-.044	-.034			-.027	-.038	1
2	-.078		-.041	-.027			-.007	-.003	2
3	-.046		-.029	-.044			-.039	.009	3
4	-.070		-.007	-.073			-.061	.003	4
5	-.124		-.114	-.117			-.087	-.041	5
6	-.100		-.109	-.114			-.117	-.051	6
7	-.107		-.122	-.126			-.107	-.111	7
8	-.136		-.136	-.126			-.126		8
9	-.143		-.139	-.083			-.136	-.028	9
10	-.131		-.061	-.151			-.151	-.088	10
11	-.148		-.061	-.151			-.066	-.114	11
12	-.133		-.139	-.152			-.155	-.215	12
13	-.126		-.161	-.174			-.174	-.196	13
14	-.142		-.161	-.158			-.142	-.193	14
15	-.148		-.161	-.174			-.145	-.193	15
16	-.158		-.167	-.142			-.155	-.196	16
17	.309		.311	.306			.323	.306	17
18	.209		.316	.309			.309	.259	18
19	.226		.304	.311			.309	.202	19
20	.214		.272	.275			.270	.136	20
21	.119		.148	.194			.194	.095	21
22	.122		.124	.173				.069	22
23	.124			.163			.165	.044	23
24	.114		.119	.165			.160	-.009	24
25	.112		.102	.143			.134	.057	25
26	.049		.070	.109			.107	-.057	26

α=6 δ=10

1	-.053		-.061	-.051			-.046	-.003	1
2	-.075		-.058	-.046			-.046	.013	2
3	-.051		-.046	-.053			-.053	.022	3
4	-.066		-.053	-.073			-.080	.006	4
5	-.131		-.131	-.122			-.100	-.038	5
6	-.119		-.117	-.126			-.126	-.044	6
7	-.129		-.134	-.139			-.114	-.114	7
8	-.131		-.131	-.134			-.131		8
9	-.134		-.129	-.102			-.134	-.069	9
10	-.119		-.039	-.131			-.131	-.104	10
11	-.122		-.039	-.129			-.068	-.092	11
12	-.101		-.114	-.177			-.183	-.177	12
13	-.073		-.190	-.202			-.212	-.133	13
14	-.095		-.183	-.139			-.161	-.161	14
15	-.174		-.183	-.171			-.158	-.174	15
16	-.101		-.164	-.164			-.177	-.183	16
17	.309		.318	.304			.311	.322	17
18	.231		.316	.309			.318	.278	18
19	.228		.304	.306			.304	.218	19
20	.221		.282	.267			.267	.148	20
21	.124		.153	.190			.190	.107	21
22	.122		.131	.168				.069	22
23	.122			.160			.163	.054	23
24	.119		.129	.153			.151	-.003	24
25	.109		.104	.141			.141	.073	25
26	.056		.070	.107			.109	-.044	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=6 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.046		-.051	-.036			-.041	-.025	1
2	-.070		-.051	-.041			-.041	-.016	2
3	-.046		-.041	-.044			-.051	.013	3
4	-.058		-.053	-.063			-.078	-.009	4
5	-.124		-.134	-.109			-.104	-.044	5
6	-.114		-.114	-.124			-.134	-.051	6
7	-.126		-.141	-.141			-.119	-.107	7
8	-.126		-.131	-.139			-.139		8
9	-.112		-.131	-.114			-.143	-.088	9
10	-.117		-.056	-.151			-.153	-.120	10
11	-.143		-.056	-.156			.068	-.092	11
12	-.246		-.208	-.250			-.253	-.253	12
13	-.190		-.272	-.275			-.291	-.224	13
14	-.218		-.246	-.227			-.234	-.256	14
15	-.237		-.240	-.272			-.253	-.259	15
16	-.196		-.218	-.234			-.256	-.269	16
17	.323		.323	.306			.321	.313	17
18	.236		.328	.309			.321	.278	18
19	.233		.311	.309			.306	.208	19
20	.224		.267	.272			.267	.155	20
21	.124		.158	.199			.199	.101	21
22	.134		.139	.175				.066	22
23	.126			.163			.170	.047	23
24	.124		.134	.163			.170	-.003	24
25	.126		.114	.146			.190	.069	25
26	.070		.090	.117			.194	-.051	26

α=6 δ=30

1	-.041		-.053	-.053			-.044	-.022	1
2	-.075		-.056	-.053			-.044	-.009	2
3	-.046		-.046	-.058			-.051	.000	3
4	-.063		-.061	-.080			-.075	-.013	4
5	-.136		-.134	-.126			-.109	-.060	5
6	-.131		-.117	-.139			-.129	-.063	6
7	-.131		-.141	-.146			-.129	-.142	7
8	-.134		-.141	-.141			-.134		8
9	-.134		-.146	-.126			-.151	-.104	9
10	-.126		-.063	-.163			-.165	-.054	10
11	-.151		-.063	-.160			.061	-.098	11
12	-.281		-.246	-.291			-.284	-.297	12
13	-.246		-.297	-.297			-.306	-.281	13
14	-.265		-.278	-.278			-.284	-.300	14
15	-.259		-.272	-.297			-.281	-.297	15
16	-.253		-.278	-.275			-.303	-.310	16
17	.304		.313	.301			.316	.313	17
18	.231		.313	.301			.316	.265	18
19	.231		.301	.306			.299	.199	19
20	.211		.275	.272			.262	.130	20
21	.122		.148	.192			.192	.085	21
22	.124		.124	.170				.063	22
23	.141			.527			.255	.038	23
24	.435		.525	.627			.362	.006	24
25	.484		.513	.627			.564	.303	25
26	.491		.539	.625			.637	.376	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=9 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.095		-.114	-.095			-.102	-.104	1
2	-.129		-.104	-.092			-.090	-.057	2
3	-.097		-.095	-.107			-.102	-.047	3
4	-.102		-.095	-.126			-.124	-.069	4
5	-.163		-.170	-.168			-.156	-.120	5
6	-.151		-.160	-.165			-.180	-.145	6
7	-.160		-.175	-.192			-.173	-.215	7
8	-.180		-.185	-.190			-.180		8
9	-.170		-.182	-.158			-.192	-.145	9
10	-.168		-.090	-.204			-.202	-.183	10
11	-.190		-.090	-.209			.039	-.183	11
12	-.218		-.256	-.262			-.256	-.294	12
13	-.253		-.269	-.291			-.287	-.275	13
14	-.250		-.265	-.275			-.243	-.310	14
15	-.234		-.265	-.269			-.227	-.300	15
16	-.215		-.234	-.253			-.250	-.284	16
17	.416		.450	.423			.445	.414	17
18	.309		.445	.420			.430	.347	18
19	.318		.425	.425			.430	.278	19
20	.309		.369	.391			.379	.186	20
21	.197		.231	.294			.292	.120	21
22	.207		.209	.267				.079	22
23	.199			.245			.260	.082	23
24	.194		.204	.238			.250	.013	24
25	.199		.190	.226			.238	.114	25
26	.139		.148	.194			.207	-.006	26

α=12 δ=-30

1	-.168		-.173	-.160			-.168	-.155	1
2	-.175		-.168	-.165			-.168	-.133	2
3	-.141		-.165	-.168			-.173	-.111	3
4	-.170		-.173	-.190			-.194	-.148	4
5	-.211		-.236	-.219			-.207	-.218	5
6	-.197		-.194	-.202			-.197	-.278	6
7	-.211		-.214	-.202			-.185	-.329	7
8	-.211		-.209	-.192			-.199		8
9	-.214		-.180	-.194			-.187	-.227	9
10	-.170		-.041	-.194			-.187	-.281	10
11	-.012		-.041	-.190			.051	-.253	11
12	.032		-.107	-.152			-.164	-.253	12
13	.005		-.051	-.148			-.164	-.196	13
14	.202		.123	.092			.073	-.167	14
15	.250		.240	.231			.262	-.240	15
16	.275		.291	.275			.319	-.253	16
17	.535		.651	.610			.622	.550	17
18	.428		.608	.605			.610	.464	18
19	.433		.571	.600			.593	.354	19
20	.413		.481	.539			.542	.281	20
21	.301		.326	.411			.447	.208	21
22	.306		.309	.365				.174	22
23	.296			.335			.386	.139	23
24	.294		.299	.328			.369	.063	24
25	.284		.282	.309			.335	.142	25
26	.216		.238	.265			.289	.016	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.170		-.173	-.160			-.153	-.180	1
2	-.177		-.175	-.168			-.151	-.142	2
3	-.146		-.168	-.168			-.158	-.120	3
4	-.165		-.165	-.185			-.180	-.136	4
5	-.209		-.233	-.216			-.204	-.212	5
6	-.194		-.207	-.228			-.224	-.275	6
7	-.214		-.233	-.216			-.194	-.322	7
8	-.221		-.228	-.202			-.199		8
9	-.216		-.221	-.190			-.187	-.218	9
10	-.219		-.097	-.202			-.190	-.297	10
11	-.168		-.097	-.202			.051	-.246	11
12	-.057		-.193	-.186			-.177	-.272	12
13	-.025		-.133	-.196			-.193	-.246	13
14	-.013		.032	-.123			-.126	-.234	14
15	.035		.060	.000			.013	-.272	15
16	.009		.038	.025			.063	-.272	16
17	.530		.651	.612			.634	.550	17
18	.423		.608	.600			.617	.461	18
19	.433		.564	.612			.612	.366	19
20	.403		.474	.554			.556	.284	20
21	.299		.318	.418			.454	.190	21
22	.304		.306	.369				.174	22
23	.299			.345			.401	.133	23
24	.289		.296	.335			.386	.066	24
25	.287		.277	.316			.357	.167	25
26	.211		.233	.277			.309	.013	26

α=12 δ=-10

1	-.163		-.175	-.160			-.160	-.152	1
2	-.177		-.170	-.160			-.146	-.130	2
3	-.141		-.160	-.175			-.160	-.095	3
4	-.170		-.158	-.190			-.185	-.136	4
5	-.214		-.226	-.224			-.204	-.193	5
6	-.197		-.204	-.221			-.233	-.256	6
7	-.202		-.228	-.241			-.219	-.303	7
8	-.221		-.233	-.238			-.228		8
9	-.219		-.231	-.199			-.221	-.205	9
10	-.216		-.112	-.236			-.228	-.262	10
11	-.226		-.112	-.241			.027	-.246	11
12	-.155		-.231	-.227			-.212	-.272	12
13	-.161		-.202	-.221			-.224	-.269	13
14	-.171		-.180	-.202			-.196	-.300	14
15	-.142		-.161	-.193			-.174	-.275	15
16	-.167		-.155	-.167			-.167	-.272	16
17	.522		.639	.595			.612	.562	17
18	.416		.595	.590			.605	.480	18
19	.425		.559	.600			.593	.379	19
20	.408		.469	.542			.535	.297	20
21	.292		.316	.411			.435	.205	21
22	.296		.299	.362				.174	22
23	.292			.340			.391	.139	23
24	.284		.292	.318			.369	.069	24
25	.279		.265	.301			.333	.183	25
26	.204		.228	.265			.289	.022	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.139		-.158	-.136			-.143	-.142	1
2	-.163		-.146	-.134			-.119	-.095	2
3	-.139		-.134	-.148			-.143	-.079	3
4	-.156		-.129	-.168			-.163	-.098	4
5	-.199		-.209	-.202			-.180	-.155	5
6	-.170		-.190	-.202			-.211	-.208	6
7	-.187		-.207	-.216			-.197	-.275	7
8	-.216		-.216	-.219			-.209		8
9	-.207		-.214	-.177			-.214	-.171	9
10	-.211		-.109	-.231			-.224	-.231	10
11	-.224		-.112	-.233			.027	-.224	11
12	-.224		-.237	-.246			-.246	-.281	12
13	-.227		-.256	-.275			-.272	-.262	13
14	-.227		-.250	-.259			-.231	-.294	14
15	-.237		-.250	-.243			-.224	-.278	15
16	-.224		-.224	-.221			-.224	-.284	16
17	.510		.634	.593			.610	.534	17
18	.377		.595	.590			.569	.449	18
19	.416		.556	.590			.590	.366	19
20	.401		.469	.537			.525	.275	20
21	.279		.316	.403			.433	.190	21
22	.287		.294	.357				.148	22
23	.289			.330			.377	.133	23
24	.282		.284	.321			.357	.063	24
25	.270		.267	.299			.326	.139	25
26	.192		.221	.255			.277	.006	26

α=12 δ=10

1	-.173		-.180	-.173			-.170	-.130	1
2	-.192		-.180	-.175			-.165	-.101	2
3	-.151		-.173	-.177			-.170	-.092	3
4	-.168		-.180	-.192			-.192	-.136	4
5	-.216		-.241	-.231			-.207	-.196	5
6	-.209		-.211	-.221			-.216	-.256	6
7	-.221		-.226	-.228			-.207	-.297	7
8	-.224		-.238	-.221			-.214		8
9	-.219		-.224	-.197			-.211	-.221	9
10	-.214		-.104	-.224			-.219	-.256	10
11	-.185		-.100	-.226			.027	-.234	11
12	-.208		-.183	-.237			-.243	-.297	12
13	-.139		-.227	-.237			-.265	-.246	13
14	-.133		-.199	-.164			-.199	-.243	14
15	-.202		-.180	-.193			-.180	-.275	15
16	-.120		-.161	-.174			-.158	-.297	16
17	.516		.642	.605			.620	.575	17
18	.420		.603	.603			.615	.493	18
19	.430		.556	.600			.598	.392	19
20	.408		.476	.549			.542	.303	20
21	.287		.316	.408			.437	.221	21
22	.296		.301	.362				.190	22
23	.294			.335			.391	.148	23
24	.289		.292	.328			.369	.079	24
25	.275		.272	.309			.340	.186	25
26	.211		.228	.265			.294	.025	26

TABLE XIV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.168		-.173	-.165			-.153		1
2	-.175		-.173	-.160			-.153		2
3	-.143		-.166	-.170			-.160		3
4	-.175		-.182	-.182			-.182		4
5	-.211		-.236	-.219			-.204		5
6	-.204		-.202	-.224			-.224		6
7	-.221		-.238	-.228			-.214		7
8	-.221		-.236	-.226			-.224		8
9	-.219		-.220	-.202			-.221		9
10	-.214		-.114	-.233			-.228		10
11	-.216		-.114	-.231			.029		11
17	.522		.642	.612			.627		17
18	.420		.603	.603			.617		18
19	.428		.564	.612			.608		19
20	.408		.476	.549			.544		20
21	.292		.316	.418			.445		21
22	.301		.304	.374					22
23	.294			.345			.401		23
24	.264		.292	.333			.382		24
25	.287		.275	.311			.350		25
26	.447		.642	.659			.530		26

α=12 δ=30

1	-.173		-.175	-.168			-.160	-.114	1
2	-.180		-.168	-.168			-.165	-.117	2
3	-.158		-.170	-.170			-.163	-.095	3
4	-.170		-.177	-.185			-.185	-.085	4
5	-.216		-.233	-.219			-.214	-.107	5
6	-.207		-.202	-.231			-.236	-.180	6
7	-.219		-.231	-.238			-.221	-.243	7
8	-.221		-.236	-.231			-.231		8
9	-.214		-.236	-.216			-.238	.044	9
10	-.214		-.117	-.248			-.243	-.224	10
11	-.228		-.117	-.248			.024	-.224	11
12	-.269		-.276	-.316			-.316	-.354	12
13	-.209		-.310	-.310			-.341	-.332	13
14	-.231		-.291	-.297			-.319	-.332	14
15	-.276		-.287	-.310			-.306	-.329	15
16	-.276		-.284	-.291			-.322	-.338	16
17	.527		.646	.610			.622	.565	17
18	.423		.605	.603			.610	.477	18
19	.428		.564	.608			.598	.401	19
20	.408		.479	.542			.539	.322	20
21	.292		.321	.413			.442	.237	21
22	.304		.309	.367				.199	22
23	.673			.643			.520	.145	23
24	.758		.790	.892			.826	.243	24
25	.753		.797	.894			.933	.458	25
26	.780		.831	.911			1.013	.543	26

TABLE XIV.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 1.7 \times 10^6$.

α=15 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.187		.197	.180			.187	.183	1
2	.194		.187	.182			.180	.133	2
3	.177		.187	.185			.194	.152	3
4	.190		.187	.204			.214	.177	4
5	.236		.241	.236			.231	.231	5
6	.216		.211	.241			.253	.287	6
7	.228		.243	.258			.243	.335	7
8	.241		.258	.260			.250		8
9	.241		.250	.233			.250	.256	9
10	.238		.136	.267			.258	.281	10
11	.253		.136	.267			.012	.253	11
12	.269		.284	.294			.291	.322	12
13	.272		.297	.316			.319	.319	13
14	.281		.294	.281			.278	.319	14
15	.269		.287	.284			.275	.319	15
16	.259		.240	.259			.262	.322	16
17	.646		.860	.697			.948	.774	17
18	.518		.770	.838			.855	.644	18
19	.549		.693	.780			.833	.515	19
20	.535		.590	.659			.702	.392	20
21	.403		.430	.505			.564	.291	21
22	.413		.401	.457				.231	22
23	.401			.452			.479	.193	23
24	.396		.411	.445			.464	.158	24
25	.403		.401	.428			.445	.269	25
26	.345		.343	.403			.396	.136	26

TABLE XV

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=-12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.467		.566	.555			.528	.510	1
2	.391		.541	.539			.516	.403	2
3	.393		.515	.544			.531	.349	3
4	.393		.412	.495			.475	.276	4
5	.275		.308	.375			.394	.202	5
6	.276		.291	.329			.356	.137	6
7	.270		.266	.308			.343	.103	7
8	.262		.271	.292			.327		8
9	.264		.252	.266			.290	.099	9
10	.218		.219	.246			.233	.091	10
11	.448		.218	.546			.530	.075	11
12	.589		.603	.625			.635	.338	12
13	.546		.701	.716			.715	.411	13
14	.770		.782	.809			.779	.446	14
15	.785		.808	.829			.770	.459	15
16	.748		.773	.791			.744	.437	16
17	-.134		-.137	-.146			-.140	-.118	17
18	-.110		-.136	-.145			-.140	-.075	18
19	-.114		-.138	-.142			-.142	-.082	19
20	-.125		-.147	-.160			-.158	-.106	20
21	-.171		-.189	-.189			-.186	-.154	21
22	-.161		-.190	-.198				-.206	22
23	-.168			-.197			-.197	-.247	23
24	-.173		-.192	-.200			-.202	-.265	24
25	-.169		-.197	-.203			-.204	-.234	25
26	-.184		-.207	-.214			-.214	-.247	26

α=-12 δ=-10

1	.459		.565	.555			.528	.517	1
2	.383		.537	.543			.526	.413	2
3	.390		.513	.544			.531	.364	3
4	.386		.429	.491			.481	.285	4
5	.273		.308	.380			.398	.206	5
6	.274		.290	.324			.360	.142	6
7	.269		.270	.309			.346	.109	7
8	.257		.270	.299			.329		8
9	.259		.252	.267			.289	.105	9
10	.203		.217	.246			.234	.105	10
11	.241		.216	.237			.222	.074	11
12	.389		.397	.377			.418	.185	12
13	.467		.397	.416			.418	.195	13
14	.394		.402	.419			.405	.192	14
15	.395		.402	.419			.393	.186	15
16	.380		.390	.419			.372	.162	16
17	-.136		-.136	-.145			-.140	-.110	17
18	-.119		-.139	-.138			-.139	-.072	18
19	-.117		-.139	-.141			-.141	-.081	19
20	-.126		-.147	-.154			-.155	-.103	20
21	-.171		-.189	-.186			-.181	-.145	21
22	-.166		-.194	-.197				-.214	22
23	-.171			-.197			-.198	-.239	23
24	-.169		-.192	-.200			-.201	-.255	24
25	-.169		-.197	-.207			-.202	-.240	25
26	-.187		-.211	-.214			-.211	-.250	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=-12$ $\delta=0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.463		.564	.556			.537	.517	1
2	.387		.539	.543			.533	.415	2
3	.392		.510	.543			.539	.366	3
4	.392		.437	.493			.491	.285	4
5	.275		.307	.376			.408	.208	5
6	.276		.292	.328			.368	.142	6
7	.271		.268	.312			.354	.114	7
8	.260		.268	.302			.337		8
9	.259		.248	.272			.296	.101	9
10	.204		.217	.249			.240	.100	10
11	.239		.217	.239			.226	.080	11
12	.173		.159	.173			.167	.015	12
13	.248		.139	.155			.155	- .002	13
14	.132		.134	.164			.153	- .011	14
15	.137		.140	.148			.138	- .005	15
16	.125		.134	.149			.127	- .015	16
17	- .136		- .141	- .143		-	.137	- .106	17
18	- .117		- .140	- .143		-	.137	- .066	18
19	- .114		- .142	- .140		-	.139	- .076	19
20	- .123		- .149	- .153		-	.151	- .100	20
21	- .168		- .191	- .179		-	.176	- .143	21
22	- .161		- .199	- .190				- .213	22
23	- .167			- .193		-	.190	- .238	23
24	- .175		- .195	- .199		-	.195	- .251	24
25	- .170		- .198	- .200		-	.197	- .237	25
26	- .189		- .213	- .210		-	.207	- .253	26

$\alpha=-12$ $\delta=10$

1	.452		.568	.559			.544	.516	1
2	.380		.539	.544			.535	.413	2
3	.385		.510	.544			.549	.363	3
4	.379		.435	.495			.493	.277	4
5	.265		.305	.377			.411	.204	5
6	.268		.284	.328			.372	.138	6
7	.261		.269	.318			.357	.110	7
8	.251		.267	.302			.336		8
9	.251		.243	.268			.298	.093	9
10	.196		.211	.252			.241	.097	10
11	.231		.211	.237			.230	.072	11
12	- .011		- .021	- .007		-	.013	- .107	12
13	.062		- .054	- .039		-	.028	- .124	13
14	- .057		- .054	- .023		-	.039	- .135	14
15	- .057		- .054	- .048		-	.050	- .135	15
16	- .057		- .054	- .043		-	.060	- .147	16
17	- .145		- .145	- .146		-	.140	- .122	17
18	- .127		- .143	- .143		-	.140	- .077	18
19	- .123		- .145	- .141		-	.139	- .088	19
20	- .132		- .152	- .152		-	.153	- .113	20
21	- .176		- .196	- .184		-	.181	- .159	21
22	- .171		- .203	- .197				- .223	22
23	- .177			- .195		-	.193	- .243	23
24	- .178		- .198	- .197		-	.199	- .270	24
25	- .178		- .205	- .204		-	.201	- .245	25
26	- .194		- .213	- .210		-	.207	- .256	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=-12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.454		.576	.568			.559	.534	1
2	.372		.543	.552			.552	.424	2
3	.384		.516	.555			.562	.374	3
4	.383		.436	.502			.509	.295	4
5	.264		.308	.384			.421	.212	5
6	.268		.288	.336			.381	.144	6
7	.265		.271	.324			.366	.115	7
8	.250		.272	.308			.347		8
9	.252		.247	.277			.308	.099	9
10	.197		.216	.259			.251	.100	10
11	.234		.217	.249			.239	.077	11
12	-.138		-.140	-.122		-.139	-.191		12
13	-.069		-.167	-.164		-.159	-.213		13
14	-.163		-.176	-.164		-.170	-.210		14
15	-.183		-.176	-.171		-.174	-.210		15
16	-.176		-.176	-.181		-.179	-.210		16
17	-.150		-.149	-.145		-.134	-.115		17
18	-.132		-.146	-.143		-.135	-.081		18
19	-.130		-.148	-.139		-.137	-.094		19
20	-.133		-.153	-.153		-.154	-.118		20
21	-.181		-.197	-.179		-.180	-.154		21
22	-.174		-.201	-.194			-.222		22
23	-.181			-.193		-.193	-.244		23
24	-.184		-.199	-.196		-.195	-.266		24
25	-.184		-.202	-.201		-.197	-.241		25
26	-.199		-.214	-.209		-.206	-.253		26

α=-12 δ=25

1	.448		.579	.573			.565	.537	1
2	.369		.540	.557			.557	.426	2
3	.379		.511	.560			.569	.374	3
4	.376		.435	.503			.514	.294	4
5	.264		.303	.384			.426	.215	5
6	.264		.284	.336			.384	.145	6
7	.260		.268	.319			.372	.118	7
8	.248		.271	.308			.349		8
9	.251		.247	.276			.312	.106	9
10	.190		.209	.256			.255	.105	10
11	.227		.210	.244			.241	.081	11
12	-.195		-.192	-.183		-.192	-.235		12
13	-.142		-.219	-.214		-.208	-.250		13
14	-.212		-.229	-.214		-.218	-.238		14
15	-.229		-.229	-.223		-.225	-.241		15
16	-.201		-.227	-.229		-.225	-.238		16
17	-.160		-.156	-.149		-.143	-.127		17
18	-.139		-.151	-.144		-.139	-.083		18
19	-.134		-.156	-.144		-.141	-.099		19
20	-.141		-.157	-.159		-.154	-.118		20
21	-.186		-.204	-.186		-.179	-.169		21
22	-.181		-.205	-.198			-.235		22
23	-.190			-.200		-.192	-.251		23
24	-.188		-.202	-.201		-.198	-.268		24
25	-.187		-.212	-.205		-.198	-.255		25
26	-.194		-.069	-.202		-.117	-.268		26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=-6$ $\delta=-25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.269		.276	.280			.267	.258	1
2	.214		.288	.284			.268	.191	2
3	.221		.284	.280			.280	.168	3
4	.221		.248	.252			.238	.125	4
5	.123		.146	.181			.177	.077	5
6	.125		.127	.150			.149	.034	6
7	.120		.120	.152			.146	.010	7
8	.110		.125	.141			.132		8
9	.117		.097	.118			.121	.000	9
10	.097		.199	.267			.302	-.004	10
11	.356		.199	.433			.419	.099	11
12	.403		.444	.470			.442	.239	12
13	.302		.544	.565			.525	.354	13
14	.692		.700	.717			.670	.452	14
15	.711		.742	.758			.714	.425	15
16	.711		.731	.745			.706	.407	16
17	-.034		-.037	-.043			-.040	-.026	17
18	-.029		-.036	-.040			-.041	-.001	18
19	-.031		-.034	-.039			-.040	-.005	19
20	-.043		-.050	-.055			-.057	-.025	20
21	-.096		-.106	-.097			-.097	-.045	21
22	-.093		-.113	-.109				-.060	22
23	-.101			-.114			-.116	-.088	23
24	-.101		-.108	-.117			-.121	-.122	24
25	-.099		-.119	-.125			-.122	-.104	25
26	-.124		-.136	-.135			-.134	-.144	26

$\alpha=-6$ $\delta=-20$

1	.263		.272	.282			.272	.265	1
2	.220		.289	.282			.280	.204	2
3	.217		.282	.277			.241	.179	3
4	.218		.252	.256			.177	.127	4
5	.122		.145	.181			.151	.077	5
6	.117		.129	.153			.147	.035	6
7	.117		.117	.153			.129	.013	7
8	.109		.121	.144			.121		8
9	.112		.093	.121			.098	.004	9
10	.078		.081	.112			.098	.004	10
11	.190		.082	.188			.204	-.002	11
12	.409		.400	.387			.419	.184	12
13	.470		.488	.496			.501	.336	13
14	.509		.525	.550			.532	.317	14
15	.517		.544	.557			.532	.297	15
16	.507		.541	.557			.512	.271	16
17	-.038		-.034	-.040			-.036	-.031	17
18	-.028		-.036	-.042			-.038	.002	18
19	-.033		-.033	-.038			-.038	-.001	19
20	-.045		-.052	-.053			-.061	-.025	20
21	-.099		-.105	-.097			-.099	-.036	21
22	-.096		-.111	-.112				-.053	22
23	-.101			-.116			-.113	-.097	23
24	-.103		-.109	-.113			-.119	-.122	24
25	-.105		-.117	-.137			-.120	-.108	25
26	-.125		-.132	-.136			-.135	-.132	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=-6$ $\delta=-10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.258		.269	.282			.271	.277	1
2	.213		.288	.281			.282	.209	2
3	.217		.281	.276			.281	.193	3
4	.217		.256	.259			.242	.146	4
5	.113		.146	.181			.185	.089	5
6	.117		.125	.159			.156	.052	6
7	.116		.117	.154			.152	.021	7
8	.105		.120	.144			.139		8
9	.106		.094	.120			.125	.015	9
10	.066		.079	.108			.095	.015	10
11	.087		.075	.095			.088	.000	11
12	.214		.202	.206			.220	.061	12
13	.318		.202	.220			.209	.091	13
14	.208		.209	.230			.209	.081	14
15	.214		.213	.219			.215	.070	15
16	.195		.209	.220			.196	.056	16
17	-.044	-	.037	- .042		-	.031	- .024	17
18	-.033	-	.040	- .039		-	.033	.011	18
19	-.035	-	.035	- .034		-	.040	.007	19
20	-.047	-	.050	- .049		-	.052	- .017	20
21	-.100	-	.105	- .097		-	.096	- .034	21
22	-.098	-	.114	- .110				- .047	22
23	-.103			- .112		-	.109	- .078	23
24	-.106	-	.109	- .113		-	.111	- .111	24
25	-.106	-	.117	- .121		-	.115	- .102	25
26	-.129	-	.135	- .133		-	.129	- .128	26

$\alpha=-6$ $\delta=0$

1	.253		.266	.284			.274	.275	1
2	.209		.284	.283			.277	.209	2
3	.213		.277	.278			.285	.182	3
4	.211		.254	.255			.244	.137	4
5	.116		.144	.181			.185	.086	5
6	.112		.124	.158			.157	.039	6
7	.114		.117	.157			.151	.015	7
8	.101		.118	.141			.139		8
9	.105		.091	.118			.128	.006	9
10	.061		.078	.109			097	.006	10
11	.084		.074	.093			094	- .006	11
12	.027		.032	.040			.034	- .049	12
13	.110		.010	.015			.017	- .060	13
14	.003		.003	.027			.017	- .072	14
15	.013		.009	.021			.017	- .072	15
16	.005		.009	.010			.003	- .067	16
17	-.043	-	.044	- .044		-	.035	- .029	17
18	-.038	-	.045	- .041		-	.038	.003	18
19	-.036	-	.039	- .038		-	.035	.002	19
20	-.050	-	.053	- .052		-	.054	- .017	20
21	-.105	-	.112	- .096		-	.094	- .037	21
22	-.105	-	.115	- .108				- .053	22
23	-.107			- .113		-	.110	- .084	23
24	-.111	-	.114	- .113		-	.117	- .121	24
25	-.113	-	.121	- .121		-	.117	- .106	25
26	-.131	-	.137	- .134		-	.129	- .134	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=-6 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.209		.272	.287			.280	.274	1
2	.217		.291	.286			.281	.206	2
3	.217		.284	.282			.294	.184	3
4	.117		.258	.262			.249	.136	4
5	.116		.148	.183			.193	.083	5
6	.115		.130	.159			.160	.043	6
7	.105		.117	.159			.151	.017	7
8	.105		.121	.146			.145		8
9	.062		.099	.124			.133	.008	9
10	.064		.081	.110			.101	.005	10
11	.087		.077	.096			.094	-.003	11
12	-.105	-	.105	-.098		-	.102	-.152	12
13	-.035	-	.137	-.128		-	.122	-.171	13
14	-.128	-	.145	-.127		-	.128	-.155	14
15	-.149	-	.140	-.131		-	.134	-.116	15
16	-.143	-	.140	-.143		-	.141	-.102	16
17	-.042	-	.039	-.046		-	.038	-.037	17
18	-.038	-	.043	-.042		-	.038	-.001	18
19	-.038	-	.037	-.038		-	.037	-.007	19
20	-.052	-	.054	-.057		-	.055	-.023	20
21	-.106	-	.109	-.098		-	.095	-.040	21
22	-.103	-	.117	-.113				-.056	22
23	-.104			-.115		-	.110	-.094	23
24	-.106	-	.114	-.117		-	.117	-.133	24
25	-.109	-	.122	-.121		-	.119	-.111	25
26	-.134	-	.136	-.133		-	.132	-.145	26

α=-6 δ=20

1	.267		.270	.288			.285	.291	1
2	.217		.287	.280			.284	.226	2
3	.220		.288	.280			.294	.201	3
4	.217		.256	.258			.250	.155	4
5	.119		.142	.180			.196	.092	5
6	.117		.125	.159			.163	.045	6
7	.115		.117	.160			.156	.016	7
8	.107		.121	.149			.147		8
9	.107		.093	.130			.133	.011	9
10	.065		.072	.112			.102	.011	10
11	.088		.072	.101			.097	-.004	11
12	-.186	-	.197	-.186		-	.195	-.223	12
13	-.130	-	.220	-.218		-	.219	-.234	13
14	-.208	-	.230	-.218		-	.224	-.188	14
15	-.223	-	.230	-.230		-	.228	-.172	15
16	-.186	-	.230	-.229		-	.225	-.180	16
17	-.050	-	.053	-.054		-	.047	-.030	17
18	-.046	-	.054	-.049		-	.050	.003	18
19	-.043	-	.050	-.046		-	.045	-.004	19
20	-.053	-	.064	-.062		-	.063	-.022	20
21	-.108	-	.119	-.104		-	.105	-.039	21
22	-.106	-	.127	-.121				-.057	22
23	-.112			-.123		-	.120	-.093	23
24	-.114	-	.123	-.125		-	.125	-.136	24
25	-.113	-	.127	-.132		-	.128	-.107	25
26	-.136	-	.143	-.143		-	.137	-.140	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=−6 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.280		.285	.294			.285	.274	1
2	.225		.297	.292			.285	.211	2
3	.233		.296	.290			.295	.191	3
4	.228		.267	.266			.253	.131	4
5	.128		.154	.192			.193	.078	5
6	.128		.136	.163			.163	.033	6
7	.125		.126	.164			.159	.000	7
8	.116		.129	.155			.143		8
9	.117		.106	.131			.132	.004	9
10	.079		.084	.112			.097	.004	10
11	.099		.084	.103			.093	−.008	11
12	−.233	−.235	−.224			−.230	−.247		12
13	−.198	−.253	−.250			−.250	−.247		13
14	−.252	−.267	−.258			−.254	−.192		14
15	−.263	−.267	−.260			−.250	−.220		15
16	−.164	−.224	−.230			−.216	−.240		16
17	−.040	−.053	−.056			−.054	−.035		17
18	−.030	−.046	−.054			−.054	−.008		18
19	−.035	−.043	−.050			−.054	−.018		19
20	−.050	−.061	−.064			−.073	−.035		20
21	−.101	−.112	−.107			−.107	−.057		21
22	−.096	−.118	−.121				−.075		22
23	−.103		−.121			−.125	−.107		23
24	−.104	−.119	−.125			−.135	−.132		24
25	−.108	−.124	−.132			−.137	−.124		25
26	.021	.064	.026			.056	−.154		26

α=0 δ=−25

1	.089		.086	.093			.086	.076	1
2	.077		.088	.093			.088	.057	2
3	.072		.097	.089			.091	.060	3
4	.068		.078	.070			.062	.037	4
5	−.010		−.008	.017			−.021	−.003	5
6	−.009	−.010	−.005			−.002	−.006		6
7	−.013	−.019	−.003			−.006	−.016		7
8	−.018	−.017	−.007			−.016			8
9	−.017	−.032	−.024			−.021	−.016		9
10	−.029	−.042	−.034			−.039	−.012		10
11	.173	−.044	.197			.212	−.017		11
12	.216	.217	.183			.208	.169		12
13	.274	.284	.282			.275	.222		13
14	.301	.319	.336			.316	.202		14
15	.307	.327	.336			.320	.169		15
16	.306	.328	.335			.319	.142		16
17	.097	.101	.086			.096	.079		17
18	.078	.097	.093			.098	.083		18
19	.074	.093	.097			.101	.063		19
20	.058	.075	.076			.074	.032		20
21	−.013	.005	.017			.034	.005		21
22	−.007	−.008	−.001				−.002		22
23	−.009		−.003			.002	−.008		23
24	−.015	−.015	−.005			−.004	−.022		24
25	−.016	−.025	−.017			−.009	−.008		25
26	−.049	−.047	−.034			−.030	−.023		26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=0$ $\delta=-20$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.089		.084	.093			.089	.063	1
2	.070		.089	.094			.092	.046	2
3	.071		.095	.093			.093	.046	3
4	.066		.078	.078			.065	.022	4
5	-.010		.006	.018			.022	-.013	5
6	-.010		-.009	-.001			-.002	-.023	6
7	-.012		-.020	-.001			-.004	-.028	7
8	-.019		-.016	-.002			-.014		8
9	-.020		-.031	-.021			-.018	-.029	9
10	-.041		-.043	-.033			-.042	-.028	10
11	.094		-.044	-.004			.045	-.028	11
12	.208		.210	.183			.208	.168	12
13	.270		.278	.279			.276	.221	13
14	.295		.311	.330			.318	.195	14
15	.299		.324	.336			.320	.168	15
16	.295		.327	.334			.315	.138	16
17	.096		.100	.089			.098	.074	17
18	.078		.098	.096			.100	.070	18
19	.074		.095	.100			.103	.053	19
20	.059		.078	.078			.076	.025	20
21	-.014		.005	.022			.026	-.005	21
22	-.007		-.007	.002				-.013	22
23	-.008			-.002			.002	-.018	23
24	-.015		-.014	-.002			-.002	-.025	24
25	-.018		-.026	-.013			-.010	-.016	25
26	-.050		-.050	-.034			-.030	-.030	26

$\alpha=0$ $\delta=-10$

1	.090		.087	.096			.093	.081	1
2	.075		.092	.097			.093	.057	2
3	.074		.099	.094			.095	.060	3
4	.070		.082	.079			.068	.037	4
5	-.010		.010	.021			.025	.002	5
6	-.006		-.006	.002			.000	-.006	6
7	-.007		-.016	.000			-.001	-.015	7
8	-.016		-.012	-.002			-.013		8
9	-.014		-.028	-.019			-.019	-.018	9
10	-.044		-.042	-.032			-.038	-.019	10
11	-.030		-.041	-.037			-.026	-.026	11
12	.051		.048	.037			.052	.044	12
13	.134		.054	.056			.053	.064	13
14	.054		.057	.069			.060	.027	14
15	.059		.060	.065			.062	.006	15
16	.053		.060	.065			.059	-.009	16
17	.100		.104	.089			.097	.082	17
18	.080		.100	.094			.098	.080	18
19	.077		.097	.098			.098	.061	19
20	.061		.080	.076			.074	.035	20
21	-.010		.007	.019			.026	.002	21
22	-.005		-.005	.002				-.006	22
23	-.008			-.002			.003	-.009	23
24	-.012		-.014	-.002			-.005	-.016	24
25	-.014		-.022	-.014			-.009	-.003	25
26	-.050		-.048	-.033			-.028	-.020	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha = 0$ $\delta = 0$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.093		.088	.098			.093	.082	1
2	.077		.093	.097			.096	.061	2
3	.074		.099	.094			.098	.060	3
4	.068		.082	.078			.070	.038	4
5	-.008		.011	.021			.027	.000	5
6	-.006	-.004		.001			.001	-.006	6
7	-.007	-.015		.000			.001	-.019	7
8	-.014	-.013	-.002			-.011			8
9	-.017	-.028	-.019			-.017	-.021		9
10	-.043	-.038	-.031			-.038	-.018		10
11	-.033	-.038	-.037			-.027	-.024		11
12	-.080	-.087	-.082			-.083	-.060		12
13	.002	-.103	-.102			-.099	-.063		13
14	-.099	-.111	-.093			-.100	-.048		14
15	-.106	-.106	-.099			-.104	-.051		15
16	-.106	-.106	-.101			-.108	-.052		16
17	.097		.102	.090			.094	.079	17
18	.080		.099	.093			.099	.076	18
19	.078		.097	.098			.099	.059	19
20	.060		.079	.076			.074	.030	20
21	-.010		.006	.021			.026	.003	21
22	-.004	-.006		.002				-.006	22
23	-.006		-.001				-.002	-.008	23
24	-.011	-.014	-.001			-.002	-.011	-.018	24
25	-.014	-.022	-.012			-.011	-.006	-.006	25
26	-.052	-.045	-.032			-.030	-.023	-.023	26

$\alpha = 0$ $\delta = 10$

1	.094		.090	.101			.096	.076	1
2	.077		.093	.099			.097	.057	2
3	.076		.102	.096			.100	.062	3
4	.071		.084	.078			.073	.036	4
5	-.006		.013	.022			.029	-.008	5
6	-.004	-.003		.003			.006	-.010	6
7	-.004	-.014		.003			.005	-.022	7
8	-.013	-.010		.001		-.009			8
9	-.011	-.026	-.016			-.013	-.022		9
10	-.039	-.038	-.028			-.038	-.023		10
11	-.030	-.038	-.035			-.023	-.030		11
12	-.183	-.172	-.177			-.177	-.165		12
13	-.114	-.208	-.203			-.200	-.155		13
14	-.197	-.213	-.202			-.202	-.120		14
15	-.212	-.212	-.209			-.209	-.141		15
16	-.193	-.215	-.209			-.213	-.219		16
17	.099		.101	.089			.094	.077	17
18	.081		.101	.091			.096	.070	18
19	.077		.095	.097			.098	.055	19
20	.062		.079	.076			.073	.022	20
21	-.009		.006	.020			.026	-.003	21
22	-.004	-.005		.001				-.010	22
23	-.006		-.002				-.002	-.009	23
24	-.010	-.013	-.005			-.003	-.003	-.018	24
25	-.013	-.022	-.014			-.010	-.010	-.010	25
26	-.050	-.047	-.034			-.031	-.031	-.021	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=0 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	.093		.090	.100			.098	.092	1
2	.076		.093	.101			.098	.065	2
3	.077		.101	.097			.101	.069	3
4	.070		.084	.082			.072	.040	4
5	-.005		.012	.023			.031	.007	5
6	-.005	-.004		.003			.006	-.003	6
7	-.006	-.014		.005			.005	-.013	7
8	-.012	-.011		.002		-.008			8
9	-.012	-.027	-.015			-.012	-.012		9
10	-.038	-.038	-.027			-.034	-.010		10
11	-.030	-.038	-.033			-.019	-.007		11
12	-.239	-.233	-.235			-.238	-.221		12
13	-.179	-.258	-.263			-.261	-.192		13
14	-.249	-.272	-.265			-.262	-.227		14
15	-.267	-.269	-.262			-.244	-.273		15
16	-.195	-.217	-.215			-.223	-.297		16
17	.097		.099	.088			.093	.082	17
18	.080		.100	.093			.094	.084	18
19	.076		.095	.096			.097	.062	19
20	.060		.077	.074			.070	.031	20
21	-.011		.005	.018			.026	.005	21
22	-.005	-.006		.000				-.001	22
23	-.008			-.003		-.001		-.003	23
24	-.013	-.014		-.004		-.006		-.018	24
25	-.014	-.026		-.014		-.012		-.003	25
26	-.042	-.046		-.032		-.030		-.019	26

α=0 δ=25

1	.093		.089	.100			.099	.093	1
2	.078		.093	.101			.098	.078	2
3	.074		.101	.097			.101	.076	3
4	.069		.083	.080			.074	.054	4
5	-.006		.013	.021			.030	.006	5
6	-.006	-.003		.005			.007	.003	6
7	-.010	-.014		.002			.004	-.008	7
8	-.017	-.012		.001		-.006			8
9	-.011	-.026	-.016			-.010	-.002		9
10	-.037	-.038	-.028			-.032	-.001		10
11	-.030	-.038	-.033			-.020	.022		11
12	-.262	-.253	-.252			-.255	-.228		12
13	-.207	-.282	-.281			-.273	-.176		13
14	-.244	-.257	-.267			-.251	-.281		14
15	-.230	-.238	-.243			-.235	-.302		15
16	-.221	-.227	-.233			-.234	-.308		16
17	.094		.096	.087			.092	.085	17
18	.078		.097	.093			.093	.084	18
19	.075		.093	.093			.097	.070	19
20	.058		.075	.073			.069	.042	20
21	-.012		.003	.016			.022	.012	21
22	-.008	-.009		.002				.004	22
23	-.008			-.006		-.002		-.001	23
24	-.014	-.016		-.006		-.008		-.011	24
25	-.015	-.026		-.016		-.013		-.010	25
26	.189	.234		.248			.242	.057	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=6$ $\delta=-25$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.039		-.046	-.036			-.042	-.047	1
2	-.033		-.046	-.042			-.040	-.025	2
3	-.034		-.035	-.042			-.041	-.015	3
4	-.036		-.045	-.054			-.063	-.036	4
5	-.101		-.108	-.099			-.094	-.060	5
6	-.094		-.113	-.114			-.113	-.083	6
7	-.099		-.117	-.114			-.113	-.124	7
8	-.105		-.114	-.117			-.122		8
9	-.104		-.123	-.128			-.125	-.147	9
10	-.121		-.123	-.137			-.135	-.158	10
11	.050		-.123	.036			.075	-.168	11
12	.090		.088	.075			.084	-.039	12
13	.097		.176	.155			.154	.110	13
14	.245		.273	.257			.265	-.074	14
15	.253		.292	.271			.292	.090	15
16	.267		.290	.276			.307	.174	16
17	.272		.284	.268			.277	.256	17
18	.220		.295	.275			.284	.222	18
19	.216		.280	.280			.284	.169	19
20	.200		.248	.248			.248	.128	20
21	.109		.141	.177			.183	.065	21
22	.117		.120	.153				.040	22
23	.113			.147			.151	.011	23
24	.108		.114	.142			.147	-.007	24
25	.105		.094	.129			.137	.016	25
26	.055		.069	.101			.105	-.008	26

$\alpha=6$ $\delta=-20$

1	-.040		-.046	-.037			-.039	-.045	1
2	-.030		-.046	-.043			-.041	-.034	2
3	-.032		-.036	-.042			-.039	-.022	3
4	-.034		-.049	-.056			-.061	-.044	4
5	-.100		-.109	-.099			-.092	-.074	5
6	-.097		-.114	-.114			-.111	-.095	6
7	-.105		-.120	-.113			-.113	-.126	7
8	-.107		-.116	-.116			-.121		8
9	-.105		-.125	-.129			-.125	-.153	9
10	-.125		-.125	-.133			-.137	-.165	10
11	-.027		-.125	-.102			-.035	-.181	11
12	.060		.061	.031			.031	-.077	12
13	.131		.114	.090			.097	.030	13
14	.135		.146	.135			.141	-.112	14
15	.137		.153	.142			.161	-.018	15
16	.135		.156	.140			.170	.024	16
17	.271		.284	.269			.278	.245	17
18	.219		.296	.278			.285	.213	18
19	.217		.280	.283			.286	.160	19
20	.201		.248	.251			.251	.121	20
21	.113		.141	.179			.189	.057	21
22	.119		.121	.155				.031	22
23	.116			.149			.154	.005	23
24	.109		.113	.145			.149	-.013	24
25	.108		.094	.128			.137	.010	25
26	.055		.067	.101			.106	-.022	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=6 δ=-10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.040		-.044	-.030			-.038	-.038	1
2	-.030		-.043	-.038			-.039	-.027	2
3	-.030		-.034	-.038			-.037	-.016	3
4	-.034		-.047	-.050			-.060	-.024	4
5	-.098		-.106	-.094			-.092	-.055	5
6	-.094		-.110	-.110			-.109	-.079	6
7	-.102		-.117	-.112			-.112	-.116	7
8	-.103		-.114	-.115			-.119		8
9	-.105		-.121	-.126			-.124	-.147	9
10	-.122		-.121	-.135			-.137	-.156	10
11	-.115		-.121	-.134			-.095	-.169	11
12	-.043		-.048	-.064			-.067	-.137	12
13	.042		-.042	-.053			-.051	-.102	13
14	-.051		-.042	-.039			-.039	-.157	14
15	-.039		-.040	-.042			-.034	-.112	15
16	-.038		-.040	-.050			-.030	-.125	16
17	.273		.284	.269			.274	.256	17
18	.220		.297	.277			.282	.221	18
19	.220		.281	.284			.285	.167	19
20	.204		.251	.248			.247	.130	20
21	.113		.145	.177			.184	.070	21
22	.121		.125	.154				.045	22
23	.117			.148			.152	.024	23
24	.112		.117	.142			.146	.000	24
25	.109		.098	.128			.135	.021	25
26	.054		.071	.102			.104	-.005	26

α=6 δ=0

1	-.042		-.044	-.030			-.036	-.043	1
2	-.030		-.042	-.039			-.038	-.029	2
3	-.031		-.033	-.036			-.035	-.016	3
4	-.034		-.046	-.052			-.058	-.027	4
5	-.098		-.108	-.091			-.089	-.058	5
6	-.096		-.109	-.108			-.106	-.079	6
7	-.101		-.115	-.112			-.108	-.114	7
8	-.105		-.113	-.114			-.117		8
9	-.104		-.121	-.126			-.120	-.136	9
10	-.124		-.121	-.133			-.135	-.154	10
11	-.121		-.121	-.138			-.104	-.171	11
12	-.140		-.141	-.152			-.149	-.186	12
13	-.070		-.159	-.169			-.162	-.186	13
14	-.152		-.166	-.158			-.156	-.179	14
15	-.159		-.166	-.165			-.156	-.196	15
16	-.159		-.166	-.170			-.158	-.186	16
17	.272		.282	.268			.275	.253	17
18	.220		.296	.276			.284	.220	18
19	.220		.281	.281			.286	.169	19
20	.200		.250	.249			.247	.132	20
21	.113		.143	.177			.186	.069	21
22	.120		.124	.153				.043	22
23	.117			.148			.152	.018	23
24	.112		.117	.144			.145	-.004	24
25	.108		.097	.129			.135	.017	25
26	.055		.072	.102			.105	-.013	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

$\alpha=6$ $\delta=10$

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.039		-.042	-.030			-.035	-.035	1
2	-.030		-.042	-.038			-.036	-.022	2
3	-.030		-.033	-.037			-.034	-.006	3
4	-.032		-.046	-.048			-.056	-.028	4
5	-.096		-.107	-.093			-.088	-.053	5
6	-.095		-.109	-.109			-.105	-.070	6
7	-.104		-.117	-.103			-.108	-.108	7
8	-.102		-.113	-.112			-.116		8
9	-.101		-.121	-.125			-.119	-.136	9
10	-.121		-.121	-.132			-.133	-.144	10
11	-.119		-.121	-.137			-.104	-.163	11
12	-.222		-.217	-.219			-.217	-.237	12
13	-.153		-.240	-.244			-.239	-.214	13
14	-.226		-.252	-.240			-.243	-.235	14
15	-.245		-.246	-.250			-.244	-.253	15
16	-.176		-.186	-.199			-.234	-.258	16
17	.272		.284	.267			.273	.254	17
18	.219		.294	.275			.281	.217	18
19	.220		.280	.281			.284	.172	19
20	.202		.250	.248			.247	.131	20
21	.114		.144	.177			.185	.070	21
22	.121		.122	.153				.036	22
23	.117			.147			.150	.018	23
24	.111		.116	.141			.144	.000	24
25	.109		.096	.128			.134	.020	25
26	.057		.070	.101			.105	-.011	26

$\alpha=6$ $\delta=20$

1	-.043		-.044	-.033			-.034	-.028	1
2	-.032		-.043	-.039			-.036	-.019	2
3	-.035		-.034	-.038			-.034	-.004	3
4	-.037		-.048	-.052			-.054	-.018	4
5	-.101		-.105	-.095			-.087	-.048	5
6	-.099		-.111	-.111			-.105	-.069	6
7	-.105		-.117	-.111			-.108	-.104	7
8	-.107		-.115	-.111			-.115		8
9	-.105		-.123	-.124			-.117	-.126	9
10	-.124		-.122	-.130			-.129	-.141	10
11	-.120		-.121	-.135			-.101	-.131	11
12	-.263		-.257	-.263			-.263	-.266	12
13	-.211		-.281	-.284			-.283	-.253	13
14	-.264		-.256	-.267			-.277	-.274	14
15	-.235		-.244	-.250			-.253	-.282	15
16	-.217		-.231	-.239			-.242	-.285	16
17	.268		.281	.264			.269	.255	17
18	.217		.293	.273			.278	.216	18
19	.217		.276	.278			.281	.175	19
20	.199		.248	.244			.244	.138	20
21	.109		.140	.176			.185	.076	21
22	.116		.120	.151				.048	22
23	.114			.145			.148	.023	23
24	.109		.114	.141			.143	.003	24
25	.106		.094	.126			.133	.020	25
26	.066		.069	.100			.102	-.006	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=6 δ=25

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.024		-.043	-.035			-.033	-.033	1
2	-.029		-.043	-.042			-.034	-.021	2
3	-.032		-.037	-.041			-.034	-.006	3
4	-.038		-.049	-.054			-.055	-.017	4
5	-.102		-.109	-.096			-.089	-.050	5
6	-.099		-.113	-.112			-.106	-.070	6
7	-.105		-.118	-.112			-.107	-.104	7
8	-.108		-.114	-.113			-.115		8
9	-.107		-.122	-.123			-.118	-.136	9
10	-.123		-.121	-.131			-.131	-.124	10
11	-.121		-.121	-.135			-.102	-.038	11
12	-.288		-.280	-.284			-.283	-.292	12
13	-.239		-.280	-.290			-.296	-.286	13
14	-.266		-.264	-.266			-.275	-.302	14
15	-.246		-.254	-.258			-.262	-.300	15
16	-.242		-.254	-.258			-.262	-.300	16
17	.267		.278	.264			.267	.251	17
18	.216		.289	.273			.276	.217	18
19	.215		.276	.276			.276	.173	19
20	.199		.247	.246			.240	.132	20
21	.110		.136	.175			.179	.075	21
22	.116		.119	.150				.039	22
23	.112			.145			.145	.020	23
24	.109		.113	.141			.141	.003	24
25	.216		.395	.429			.362	.021	25
26	.442		.464	.491			.489	.252	26

α=12 δ=-25

1	-.132		-.141	-.128			-.130	-.126	1
2	-.111		-.135	-.128			-.125	-.095	2
3	-.114		-.132	-.134			-.133	-.091	3
4	-.115		-.127	-.143			-.149	-.111	4
5	-.169		-.181	-.175			-.169	-.153	5
6	-.150		-.186	-.181			-.184	-.225	6
7	-.162		-.188	-.187			-.181	-.247	7
8	-.173		-.190	-.189			-.188		8
9	-.170		-.191	-.193			-.192	-.252	9
10	-.180		-.179	-.201			-.197	-.242	10
11	-.051		-.179	-.088			-.034	-.231	11
12	.004		-.020	-.027			-.022	-.172	12
13	-.079		.035	.021			.025	-.130	13
14	.114		.117	.089			.124	-.187	14
15	.120		.139	.114			.154	-.216	15
16	.135		.148	.124			.170	-.241	16
17	.466		.581	.535			.542	.488	17
18	.389		.549	.546			.542	.432	18
19	.389		.511	.543			.539	.342	19
20	.373		.431	.488			.495	.280	20
21	.268		.300	.372			.411	.196	21
22	.272		.283	.328				.153	22
23	.266			.310			.356	.124	23
24	.262		.266	.301			.337	.097	24
25	.258		.244	.281			.314	.117	25
26	.193		.215	.246			.269	.088	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

$M = 2.01$; $R = 4.5 \times 10^6$.

α=12 δ=-20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.137		-.144	-.131			-.135	-.120	1
2	-.114		-.137	-.135			-.135	-.090	2
3	-.117		-.137	-.137			-.136	-.087	3
4	-.113		-.137	-.146			-.154	-.110	4
5	-.170		-.185	-.177			-.177	-.148	5
6	-.155		-.188	-.188			-.189	-.222	6
7	-.168		-.195	-.194			-.189	-.250	7
8	-.173		-.194	-.192			-.197		8
9	-.170		-.196	-.199			-.198	-.258	9
10	-.184		-.185	-.207			-.206	-.243	10
11	-.104		-.184	-.161			-.092	-.230	11
12	-.012		-.038	-.059			-.059	-.180	12
13	.010		-.005	-.027			-.017	-.147	13
14	.024		.031	.008			.034	-.193	14
15	.042		.043	.016			.051	-.221	15
16	.035		.043	.020			.059	-.238	16
17	.467		.579	.531			.539	.497	17
18	.390		.547	.543			.539	.435	18
19	.389		.508	.543			.534	.354	19
20	.373		.429	.487			.491	.294	20
21	.267		.299	.371			.400	.213	21
22	.272		.283	.326				.161	22
23	.266			.309			.353	.131	23
24	.262		.264	.297			.336	.100	24
25	.257		.245	.279			.310	.124	25
26	.190		.215	.241			.265	.092	26

α=12 δ=-10

1	-.137		-.144	-.133			-.135	-.124	1
2	-.112		-.141	-.139			-.135	-.095	2
3	-.115		-.137	-.139			-.135	-.088	3
4	-.113		-.141	-.146			-.153	-.114	4
5	-.168		-.186	-.177			-.174	-.160	5
6	-.158		-.189	-.191			-.185	-.238	6
7	-.170		-.195	-.193			-.189	-.262	7
8	-.173		-.194	-.192			-.192		8
9	-.172		-.199	-.202			-.197	-.266	9
10	-.183		-.185	-.205			-.205	-.256	10
11	-.183		-.186	-.204			-.149	-.245	11
12	-.112		-.130	-.144			-.149	-.214	12
13	-.057		-.130	-.144			-.136	-.206	13
14	-.118		-.126	-.134			-.119	-.233	14
15	-.120		-.119	-.134			-.111	-.242	15
16	-.115		-.119	-.134			-.107	-.222	16
17	.465		.580	.532			.541	.492	17
18	.391		.543	.543			.539	.429	18
19	.387		.508	.545			.535	.347	19
20	.372		.431	.487			.491	.289	20
21	.265		.300	.373			.403	.204	21
22	.269		.283	.324				.158	22
23	.265			.312			.354	.125	23
24	.260		.264	.300			.332	.105	24
25	.255		.241	.280			.308	.128	25
26	.189		.212	.244			.266	.090	26

TABLE XV.- Continued

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

M = 2.01; R = 4.5 × 10⁶.

α=12 δ=0

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.128		-.137	-.129			-.133	-.122	1
2	-.109		-.132	-.135			-.137	-.099	2
3	-.102		-.132	-.135			-.138	-.087	3
4	-.105		-.135	-.145			-.155	-.111	4
5	-.160		-.181	-.173			-.181	-.158	5
6	-.151		-.181	-.190			-.189	-.235	6
7	-.156		-.191	-.190			-.193	-.254	7
8	-.165		-.188	-.189			-.196		8
9	-.161		-.194	-.203			-.203	-.263	9
10	-.173		-.181	-.205			-.212	-.254	10
11	-.177		-.181	-.209			-.158	-.236	11
12	-.180		-.193	-.199			-.201	-.233	12
13	-.126		-.207	-.213			-.213	-.233	13
14	-.193		-.207	-.207			-.201	-.249	14
15	-.207		-.207	-.218			-.201	-.249	15
16	-.193		-.199	-.208			-.201	-.236	16
17	.474		.581	.527			.527	.496	17
18	.396		.547	.536			.530	.434	18
19	.393		.512	.541			.522	.347	19
20	.380		.432	.483			.479	.289	20
21	.273		.300	.365			.396	.208	21
22	.276		.285	.322				.160	22
23	.272			.306			.345	.125	23
24	.265		.252	.294			.325	.098	24
25	.260		.269	.276			.301	.118	25
26	.190		.241	.240			.257	.090	26

α=12 δ=10

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	-.130		-.140	-.131			-.140	-.126	1
2	-.118		-.136	-.137			-.140	-.100	2
3	-.108		-.135	-.137			-.140	-.084	3
4	-.111		-.139	-.147			-.161	-.107	4
5	-.161		-.186	-.180			-.186	-.148	5
6	-.153		-.189	-.193			-.198	-.228	6
7	-.162		-.193	-.198			-.199	-.258	7
8	-.169		-.191	-.196			-.201		8
9	-.165		-.194	-.205			-.206	-.255	9
10	-.179		-.181	-.210			-.214	-.252	10
11	-.177		-.181	-.213			-.166	-.227	11
12	-.245		-.247	-.249			-.251	-.264	12
13	-.214		-.261	-.270			-.269	-.260	13
14	-.252		-.271	-.270			-.269	-.277	14
15	-.262		-.225	-.241			-.269	-.277	15
16	-.193		-.202	-.213			-.210	-.269	16
17	.470		.580	.523			.519	.488	17
18	.394		.539	.533			.524	.425	18
19	.391		.508	.533			.518	.339	19
20	.373		.431	.479			.474	.282	20
21	.268		.299	.364			.388	.199	21
22	.272		.280	.316				.151	22
23	.268			.300			.336	.121	23
24	.261		.264	.290			.318	.099	24
25	.259		.240	.268			.293	.122	25
26	.196		.213	.229			.250	.085	26

TABLE XV.- Concluded

SURFACE PRESSURE COEFFICIENTS FOR CONFIGURATION 4.

M = 2.01; R = 4.5 × 10⁶.

α=12 δ=20

Orif	Sta 1	Sta 2	Sta 3	Sta 4	Sta 5	Sta 6	Sta 7	Sta 8	
1	- .136		- .142	- .129			- .139	- .115	1
2	- .115		- .139	- .138			- .142	- .090	2
3	- .109		- .136	- .136			- .137	- .083	3
4	- .106		- .137	- .145			- .156	- .104	4
5	- .161		- .182	- .181			- .179	- .144	5
6	- .156		- .187	- .195			- .192	- .219	6
7	- .166		- .193	- .194			- .194	- .249	7
8	- .172		- .192	- .190			- .196		8
9	- .165		- .197	- .198			- .200	- .255	9
10	- .177		- .181	- .210			- .211	- .240	10
11	- .177		- .181	- .206			- .157	- .199	11
12	- .277		- .275	- .277			- .280	- .291	12
13	- .239		- .271	- .284			- .298	- .291	13
14	- .251		- .256	- .264			- .281	- .301	14
15	- .240		- .248	- .251			- .266	- .293	15
16	- .236		- .242	- .247			- .252	- .283	16
17	.467		.575	.520			.515	.488	17
18	.393		.543	.535			.519	.431	18
19	.388		.507	.531			.517	.342	19
20	.371		.428	.479			.473	.288	20
21	.267		.293	.364			.387	.206	21
22	.272		.280	.316				.154	22
23	.267			.300			.337	.133	23
24	.264		.260	.291			.318	.105	24
25	.257		.238	.269			.295	.121	25
26	.519		.586	.634			.581	.108	26

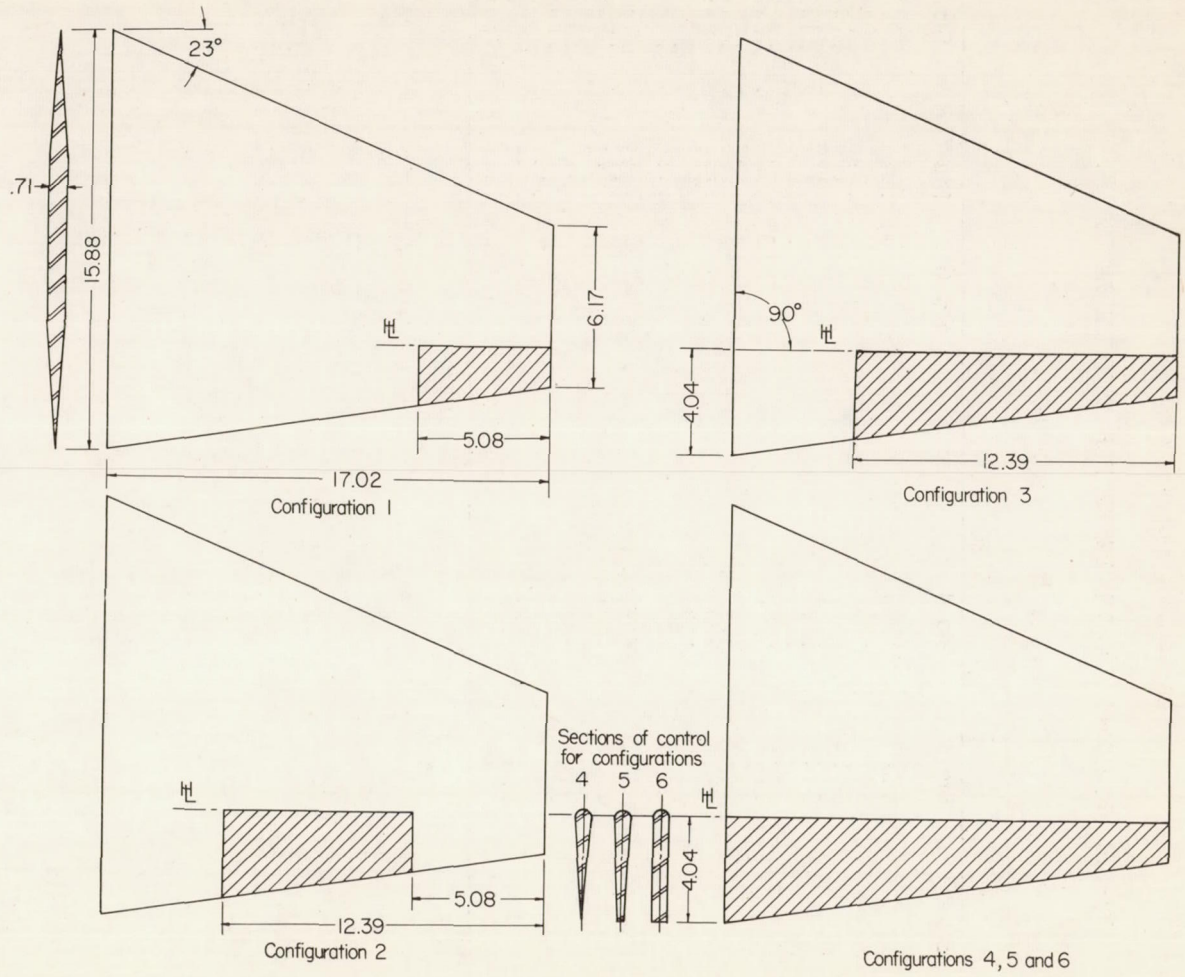
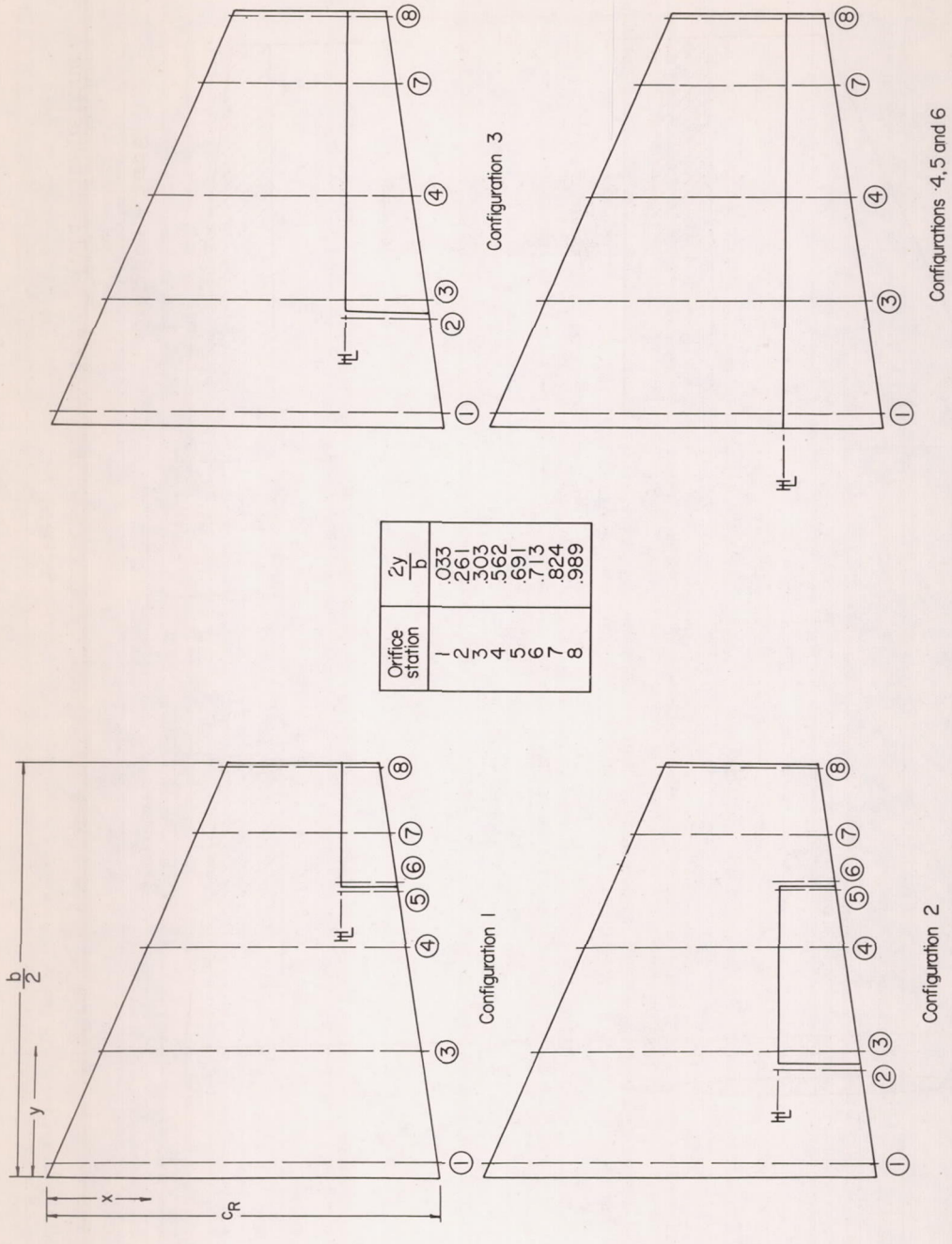


Figure 1.- Sketches of model configurations tested. (All dimensions in inches.)



Orifice station	2y/b
1	.033
2	.261
3	.303
4	.562
5	.691
6	.713
7	.824
8	.989

Figure 2.- Locations of orifice stations.

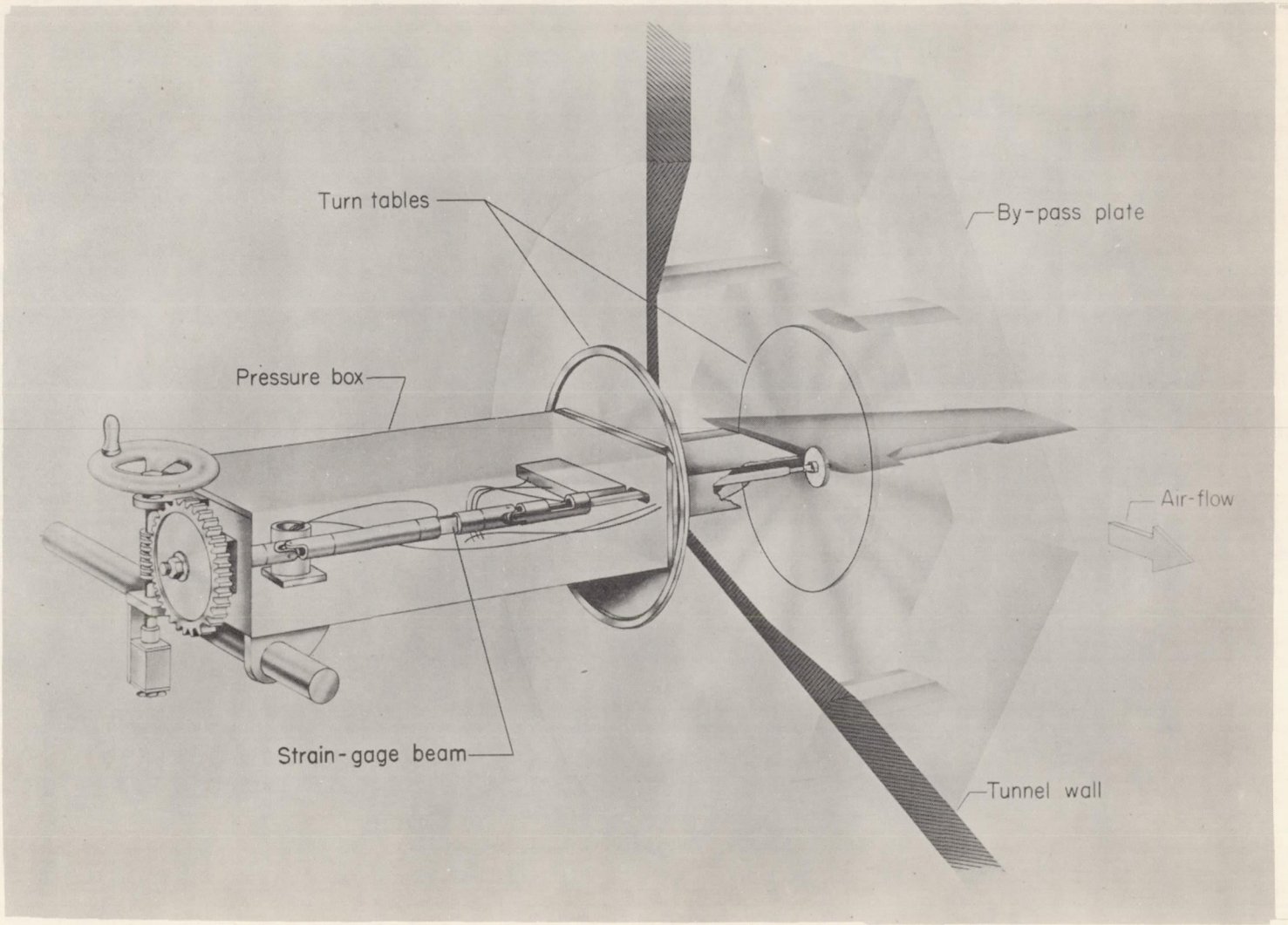
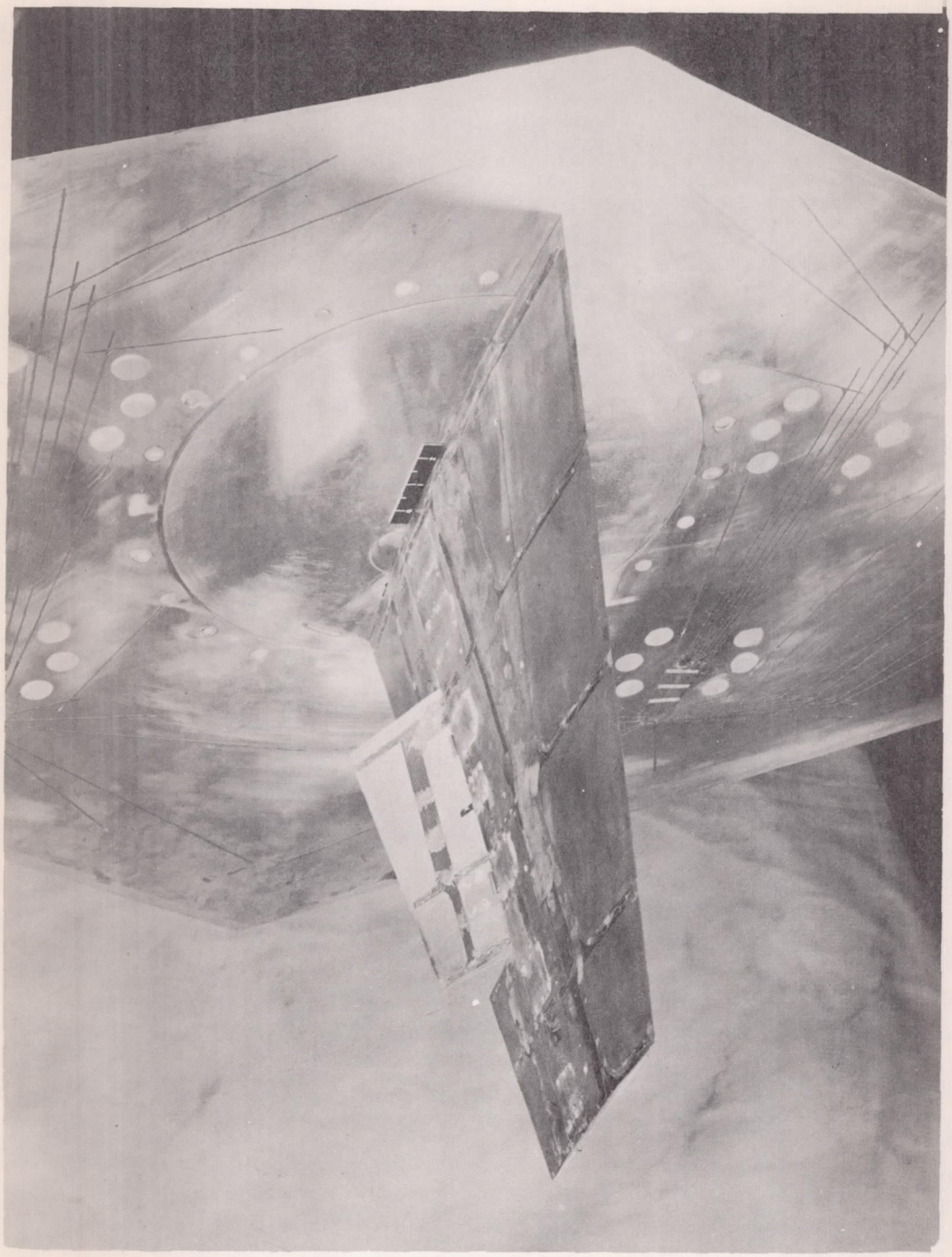


Figure 3.- Sketch of test setup.

L-83645



L-79384

Figure 4.- Photograph of model configuration 2 mounted on the bypass plate.

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