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# RESEARCH MEMORANDUM

ALTITUDE PERFORMANCE EVALUATION  
OF J71-A-11 TURBOJET ENGINE

By James W. Useller and George E. Pappas

Lewis Flight Propulsion Laboratory  
Cleveland, Ohio

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## NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

WASHINGTON

March 30, 1956

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## NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

## ALTITUDE PERFORMANCE EVALUATION OF J71-A-11 TURBOJET ENGINE

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## SUMMARY

An investigation of the altitude performance of the J71-A-11 turbojet engine was conducted in the NACA Lewis altitude wind tunnel. Data were obtained with five exhaust-nozzle areas and with the variable-area exhaust nozzle interlinked with the control system at conditions simulating flight at a Mach number of 0.8 and altitudes of 35,000 and 45,000 feet. Data simulating operation at zero flight Mach number at an altitude of 15,000 feet are also included. Engine component performance data are presented in addition to the over-all engine performance.

## INTRODUCTION

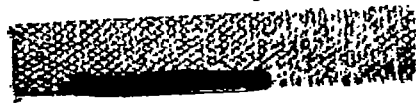
In cooperation with the U. S. Air Force, an altitude performance evaluation of the J71-A-11 turbojet engine was made in the NACA Lewis altitude wind tunnel. A calibration of the Douglas thrust rake was also made to provide a means of measuring thrust during the flight application of the J71 turbojet engine. Data were obtained with five exhaust-nozzle areas and with the engine control system modulating the fuel flow and engine speed.

The engine performance was obtained for a range of engine rotor speeds from 4500 to 6100 rpm at conditions simulating flight at a Mach number of 0.8 at altitudes of 35,000 and 45,000 feet. Performance data were also obtained at zero flight Mach number at an altitude of 15,000 feet. Component performance data are presented in addition to the over-all engine performance.

## APPARATUS AND PROCEDURE

## Engine

The J71-A-11 turbojet engine (fig. 1) has an annular inlet, a 16-stage axial-flow compressor, a cannular-type combustor with 10 cylindrical inner liners, a three-stage turbine, and a variable-area iris-type exhaust nozzle. The engine has a military thrust rating of 9700 pounds



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at 6100 rpm and a turbine-outlet gas temperature of 1150° F at sea-level static conditions.

To facilitate acceleration in the engine-speed range below 85 percent of rated speed, the engine is equipped with two-position compressor-inlet guide vanes and four air-bleed ports at the compressor eighth stage. The guide vanes are closed and the bleed ports open up to 85 percent of rated rotor speed. At higher speeds, the ports are closed and the guide vanes assume the normal open position.

### Instrumentation

Instrumentation for measuring temperatures and pressures was installed at various stations throughout the engine as shown in figure 1(a). The table accompanying the figure indicates the number and type of measurements obtained at each station. Air flow to the engine was measured by a venturi section in the ram pipe ahead of the engine.

Figure 1(b) shows a schematic of the arrangement of the total-pressure and temperature probes in the engine tail pipe. The pressure probes of the Douglas rake were manifolded to indicate an average pressure, while the probes of the more comprehensive survey (station 9) were read individually. The comprehensive pressure survey was made with instrumentation supplied by Arnold Engineering Development Center (AEDC) and was located  $6\frac{1}{4}$  inches downstream of the Douglas rake.

### Installation

The engine was mounted on a wing section that spanned the 20-foot-diameter test section of the altitude wind tunnel. Dry, refrigerated air was supplied from the tunnel make-up air system through a duct to the engine inlet. The inlet-air duct was connected to the engine by means of a frictionless slip-joint which permitted installation drag and thrust to be measured by the tunnel balance scales. The air leakage through the engine-inlet-screen actuator ports was calibrated and included in the values given for engine air flow.

### Procedure

Steady-state performance data were obtained at conditions simulating flight at a Mach number of 0.8 at altitudes of 35,000 and 45,000 feet. Data were also obtained at a simulated altitude of 15,000 feet at zero flight Mach number. For the 35,000- and 45,000-foot flight conditions, the engine was operated with both the variable-area exhaust

nozzle interlinked with the engine control system and with five fixed exhaust-nozzle areas. The five exhaust-nozzle areas were established by limiting the stroke of the variable-area exhaust-nozzle operating mechanism to establish exhaust areas of 100, 104, 109, 114, and 119 percent of rated area. The variable-area exhaust nozzle had an area range from rated to 126 percent of rated exhaust area. Engine speeds from 4500 to 6100 rpm were investigated with each nozzle area. All operation was with the inlet guide vanes and compressor-bleed ports fixed in the normal, high-speed positions.

All performance data were obtained at standard NACA inlet conditions of pressure and temperature corresponding to the indicated flight conditions. In addition, data were obtained at an altitude of 35,000 feet, with the interlinked control system, at inlet-air temperatures of 475°, 450°, and 430° R.

The fuel used throughout this investigation conformed to the specifications of MIL-F-5624a, grade JP-4, and had a lower heating value of 18,700 Btu per pound and a hydrogen-carbon ratio of 0.171.

A list of the symbols used herein is contained in the appendix, and a tabulation of the data obtained is presented in table I.

#### PRESENTATION OF DATA

The over-all engine performance of the J71-A-11 turbojet engine using five exhaust-nozzle areas is presented in figures 2 to 4 at zero flight Mach number at an altitude of 15,000 feet and a flight Mach number of 0.8 at altitudes of 35,000 and 45,000 feet. The specific-fuel-consumption data presented were based on the thrust measured by the balance system. All exhaust-gas temperature data, unless otherwise noted, are based on measurements from the AEDC rake. All engine performance data have been adjusted by the factors  $\delta_a$  and  $\theta_a$  to NACA standard altitude conditions to eliminate small deviations in setting test conditions. Similar engine performance data are shown in figure 5 for the two higher altitudes when the engine fuel flow and exhaust-nozzle area were modulated by the manufacturer's control system. To evaluate the effect of deviation of the engine-inlet-air temperature from NACA standard temperature (440° R) for the indicated flight condition, the engine was operated at inlet-air temperatures of 430°, 440°, 450°, and 475° R. The variation of the net thrust and fuel flow with inlet-air temperature is shown in figure 6.

The performance of the engine components (compressor, combustor, turbine and tail pipe) is presented in figure 7. Data are shown for operation with the five exhaust-nozzle areas and with the variable-area exhaust nozzle. The component performance has been adjusted to sea-level conditions to permit generalization of the data. The deviation of some of the performance variables with the variable-area exhaust nozzle from

the efficiencies obtained with the fixed areas in the low-speed range is due to the fact that at low speeds the nozzle area, when operating on interlinked control, was larger than that of the largest fixed-nozzle setting.

It was anticipated that, when the engine was installed in the flight vehicle, the Douglas thrust rakes installed in the tail pipe would provide an average tail-pipe total pressure that can be used to indicate a function of jet thrust that will be readable during flight operation. To evaluate the average pressure reading indicated by the Douglas rake, a more comprehensive pressure survey was installed as near as practical to the plane of the Douglas rake. The indicated tail-pipe total pressure from the Douglas rake is compared with the average pressure determined from the detailed survey in figure 8. The failure of the data for operation at an altitude of 35,000 feet to coincide with that at 45,000 feet is probably due to a shift in the pressure profile in the tail pipe and/or a shift in the swirl pattern leaving the turbine as the turbine operating conditions are changed with altitude. The tail-pipe total pressure determined by the Douglas rake may be used to determine a jet-thrust parameter as is shown in figure 9. The thrust parameter shown here is based on the balance-system measurements and shows relatively good agreement with the values of the pressure parameter based on the Douglas rake average total pressure. A detailed discussion of the deviation and reliability of the thrust parameter is contained in reference 1.

A calibration of the air leakage through the engine-inlet-screen actuator ports is shown in figure 10. For flight Mach numbers less than 0.4 the leakage flow is into the engine inlet, and for higher Mach numbers the leakage is out of the engine inlet. The engine air-flow data presented include the air leakage and represent the actual air flow to the compressor.

Lewis Flight Propulsion Laboratory  
National Advisory Committee for Aeronautics  
Cleveland, Ohio, October 11, 1955

## APPENDIX - SYMBOLS

A	area, sq ft
$F_{j,a}$	jet thrust from AEDC rake
$F_{j,D}$	jet thrust from Douglas rake
$F_{j,s}$	jet thrust from balance system
$F_{n,D}$	net thrust from Douglas rake
$F_{n,s}$	net thrust from balance system
M	Mach number
N	engine rotor speed, rpm
P	total pressure, lb/sq ft
p	static pressure, lb/sq ft
T	total temperature, °R
$W_a$	air flow, lb/sec
$W_f$	fuel flow, lb/hr
$W_s$	weight flow, lb/sec
$\beta$	correction factor for variation of specific heats,

$$\frac{\gamma^*}{\gamma} \frac{\left(\frac{\gamma + 1}{2}\right)^{\frac{\gamma}{\gamma-1}}}{\left(\frac{\gamma^* + 1}{2}\right)^{\frac{\gamma^*}{\gamma^*-1}}}$$

$\gamma$	ratio of specific heats
$\delta_a$	ratio of total pressure to NACA standard total pressure at indicated flight condition
$\delta_{s2}$	ratio of total pressure to static sea-level pressure, P/2116

- $\eta$  efficiency, percent
- $\theta_a$  ratio of total temperature to NACA standard total temperature at indicated flight condition
- $\theta_{s2}$  ratio of total temperature to static sea-level temperature,  $T/519$

## Subscripts:

- b combustor
- c compressor
- e compressor-inlet screens
- t turbine
- 0 free stream
- 1 engine inlet
- 2 compressor outlet
- 3 combustor inlet
- 4 turbine inlet
- 5 turbine outlet
- 9 exhaust-nozzle inlet

## Superscript:

- \* NACA standard sea-level condition

## REFERENCE

1. Sivo, Joseph N., and Fenn, David B.: A Method of Measuring Jet Thrust of Turbojet Engines in Flight Installations. NACA RM E53J15, 1954.







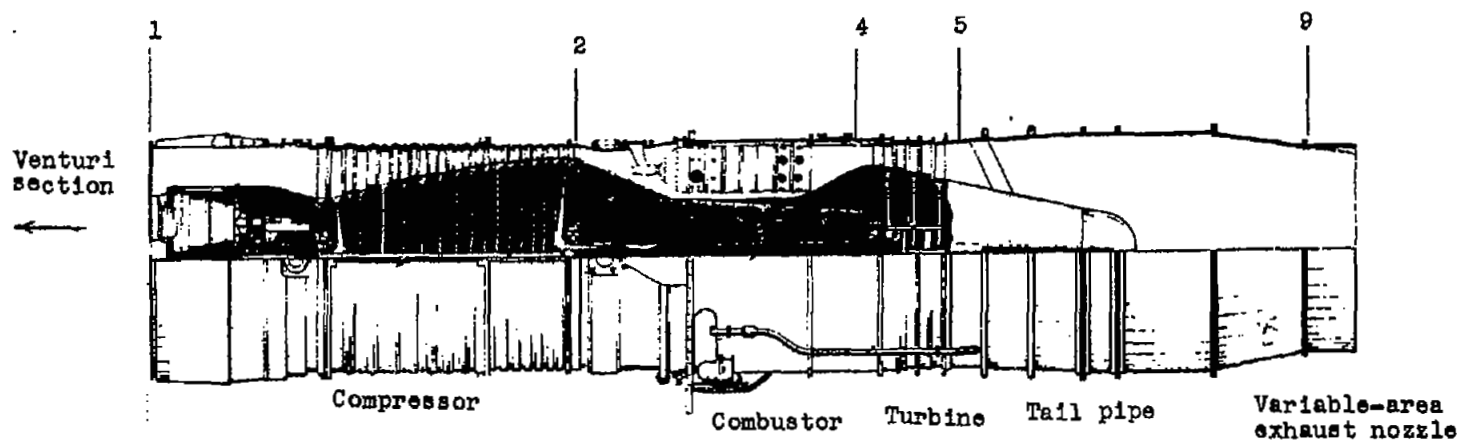






Station	Total pressures	Static pressures	Temperatures
1	8	4	16
2	16	-	16
4	10	-	10
5	15	-	15
9	32	-	20

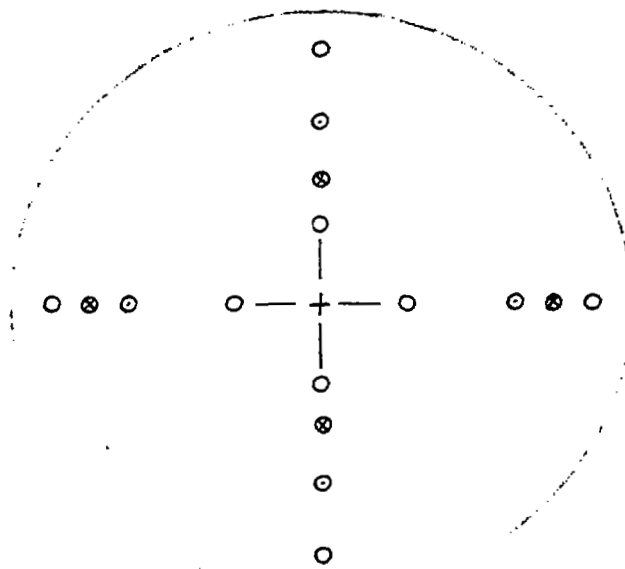
Engine station



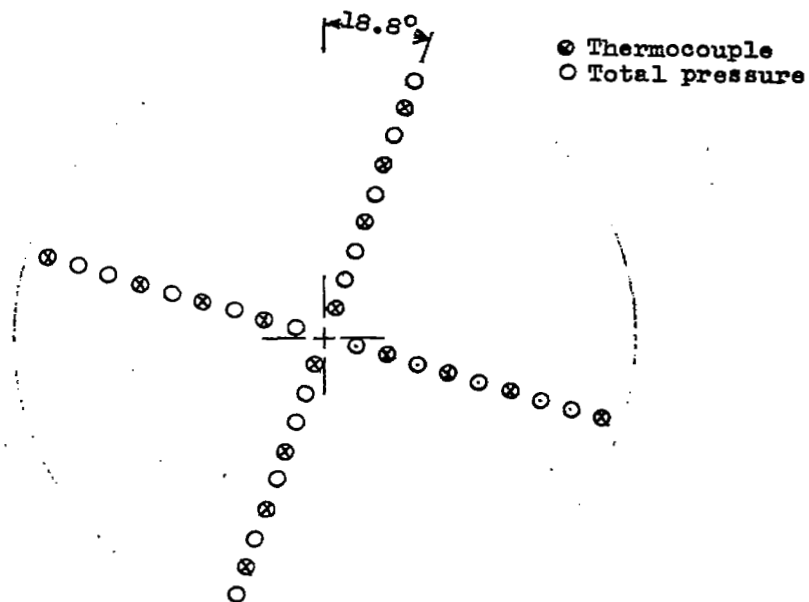
(a) Engine instrumentation stations.

Figure 1.- Schematic diagram of J71-A-11 turbojet engine with instrumentation stations and details.

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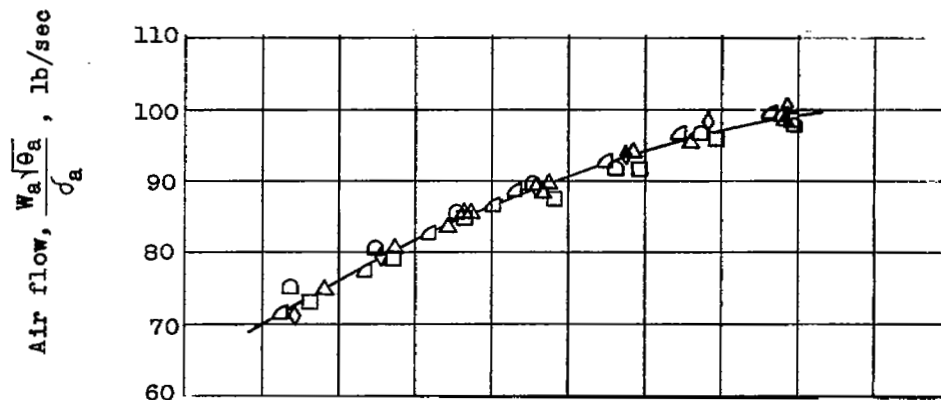
Douglas thrust rake



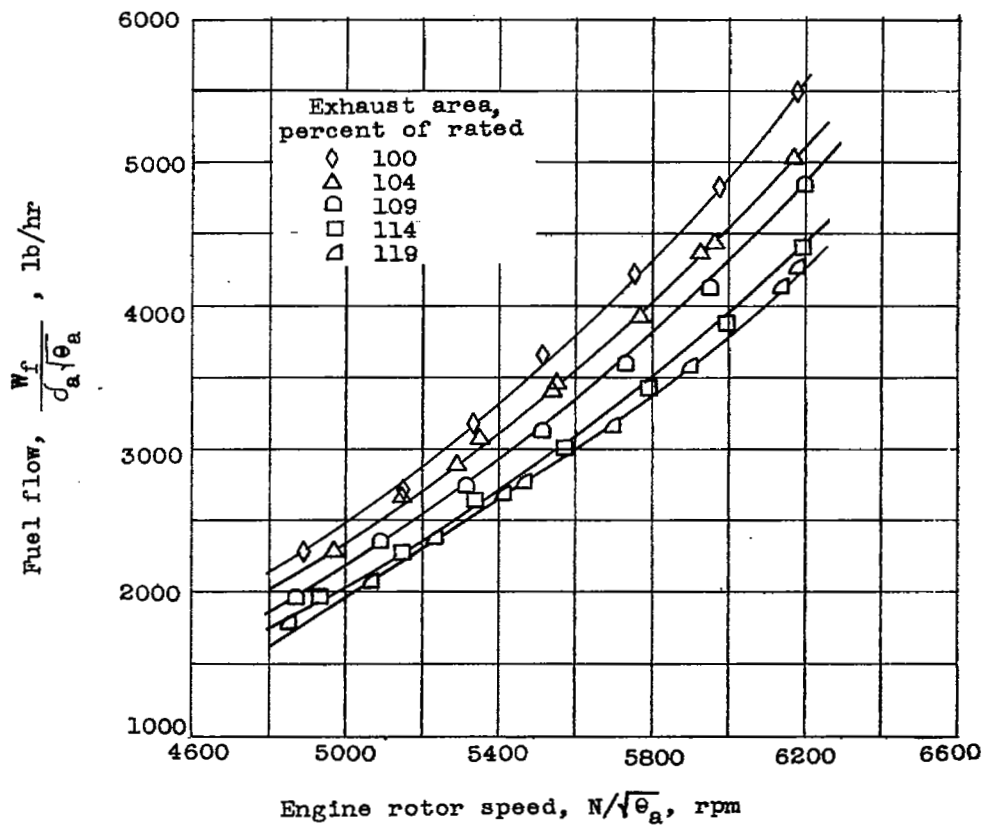
Comprehensive survey at station 9.

(b) Tail-pipe instrumentation details.

Figure 1. - Concluded. Schematic diagram of J71-A-11 turbojet engine.

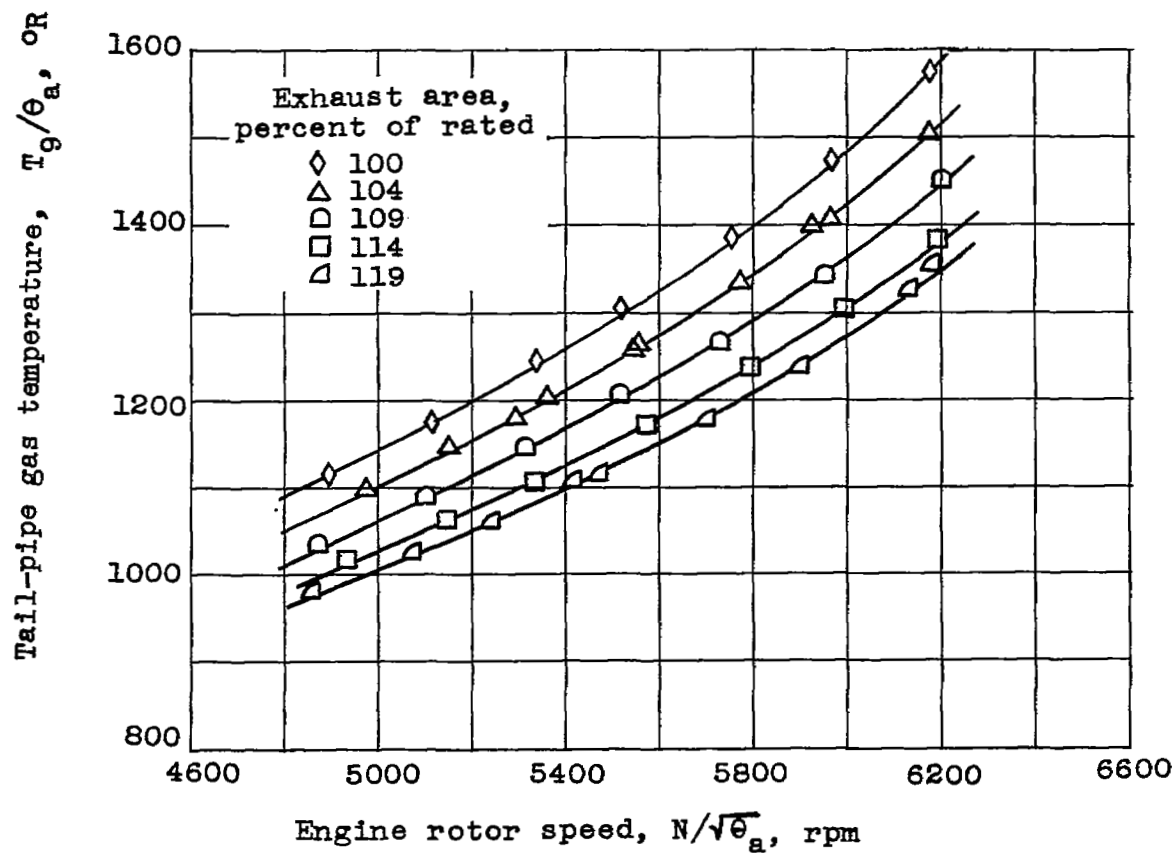


(a) Engine air flow.



(b) Engine fuel flow.

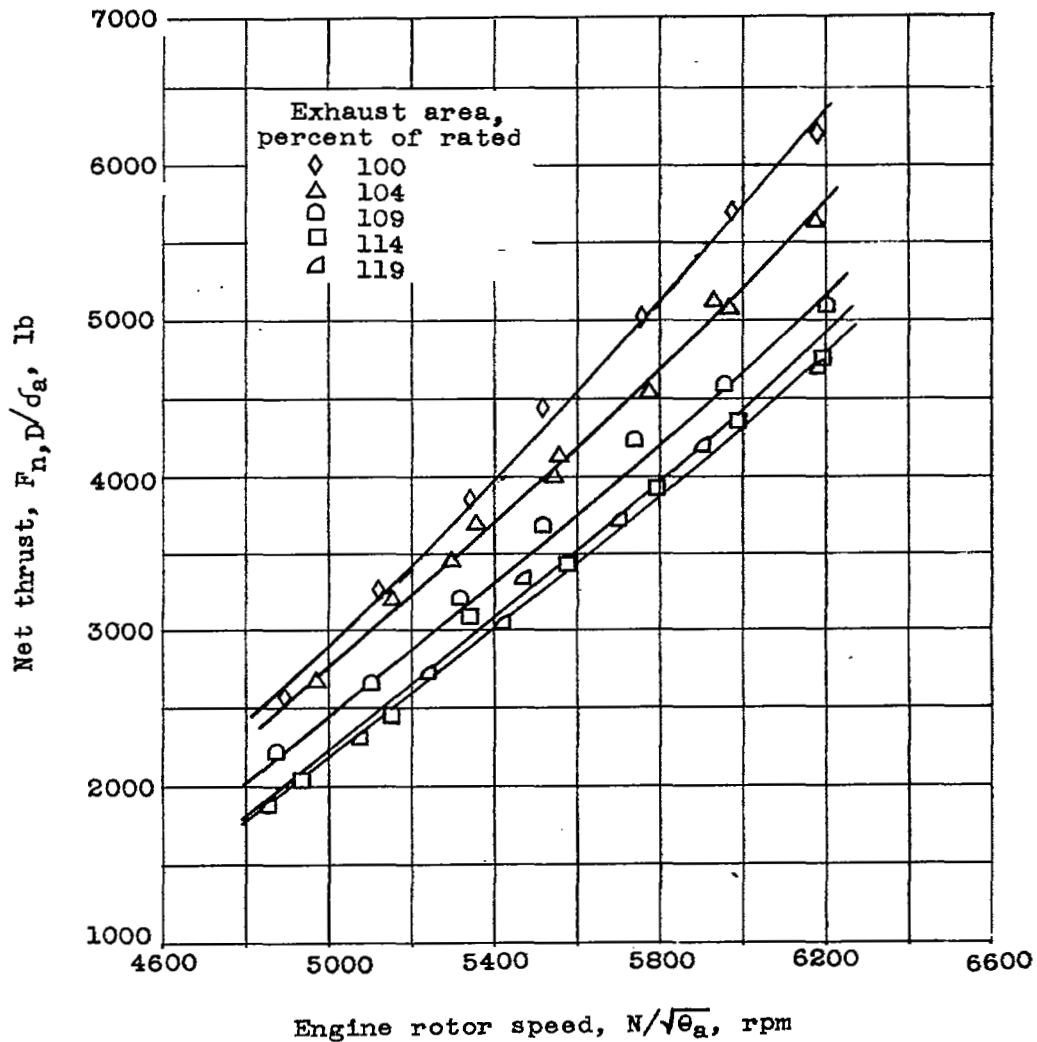
Figure 2.- Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 15,000 feet; flight Mach number, 0.



(c) Tail-pipe gas temperature.

Figure 2. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 15,000 feet; flight Mach number, 0.

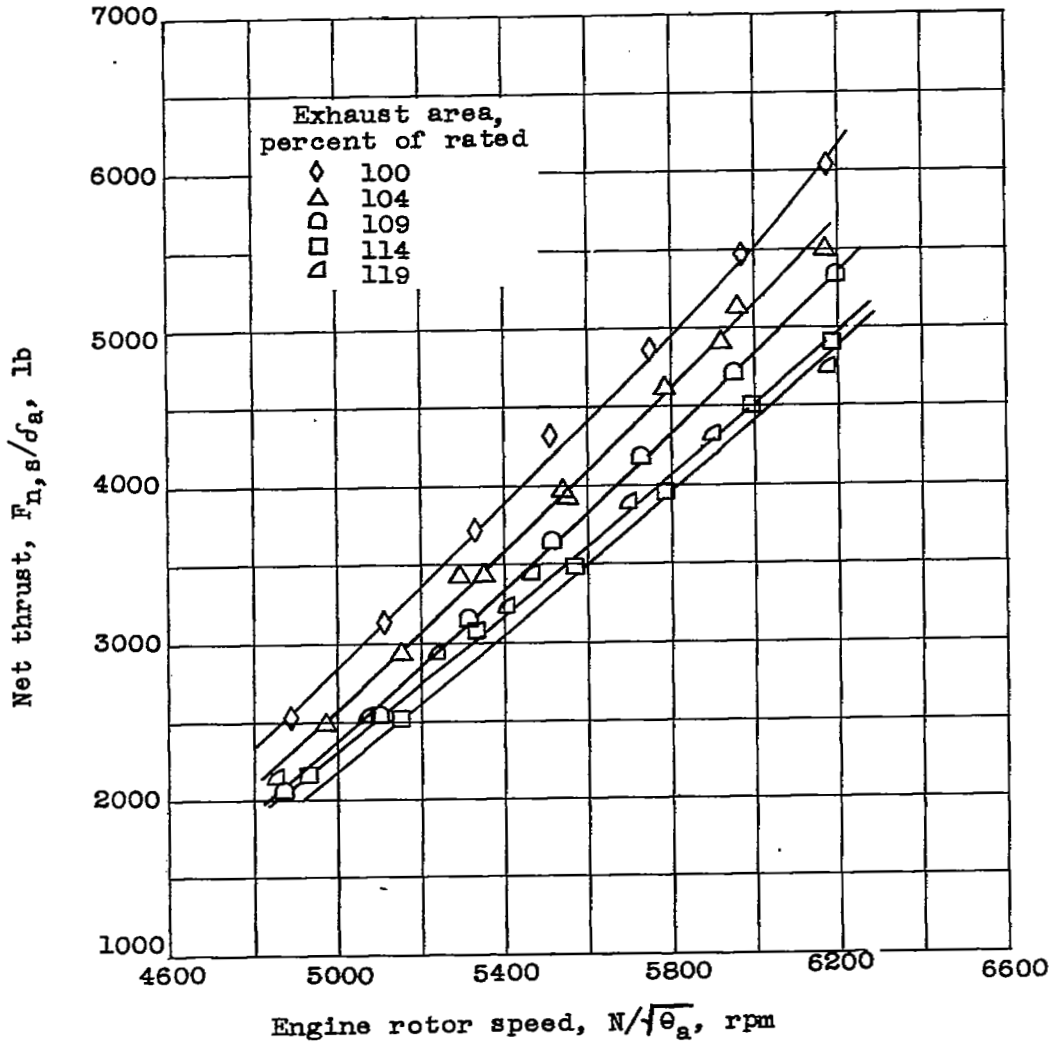




(d) Net thrust from Douglas rake.

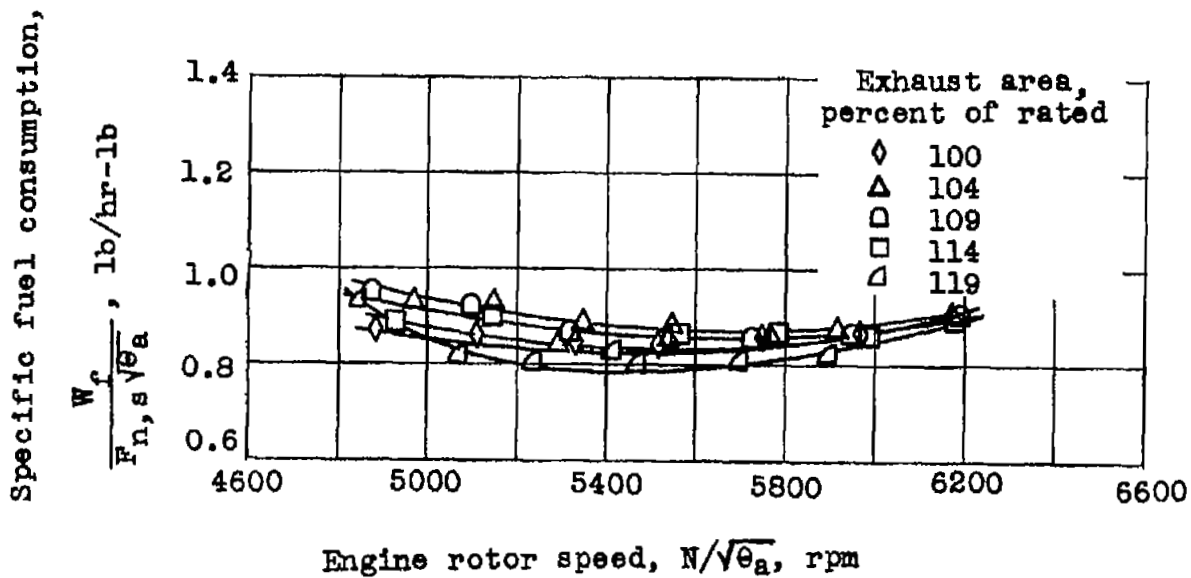
Figure 2. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 15,000 feet; flight Mach number 0.

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(e) Net thrust measured by balance system.

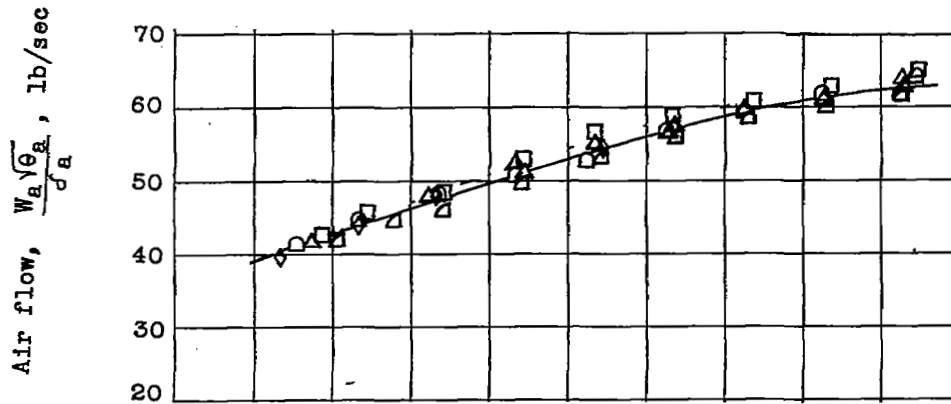
Figure 2. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 15,000 feet; flight Mach number, 0.



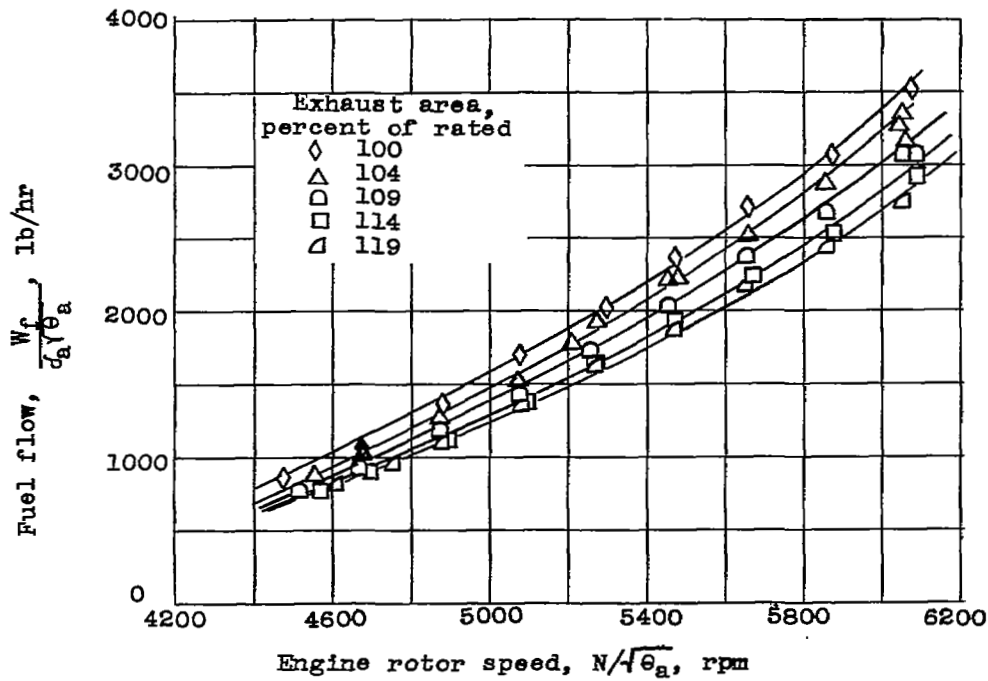
(f) Specific fuel consumption.

Figure 2. - Concluded. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 15,000 feet; flight Mach number, 0.

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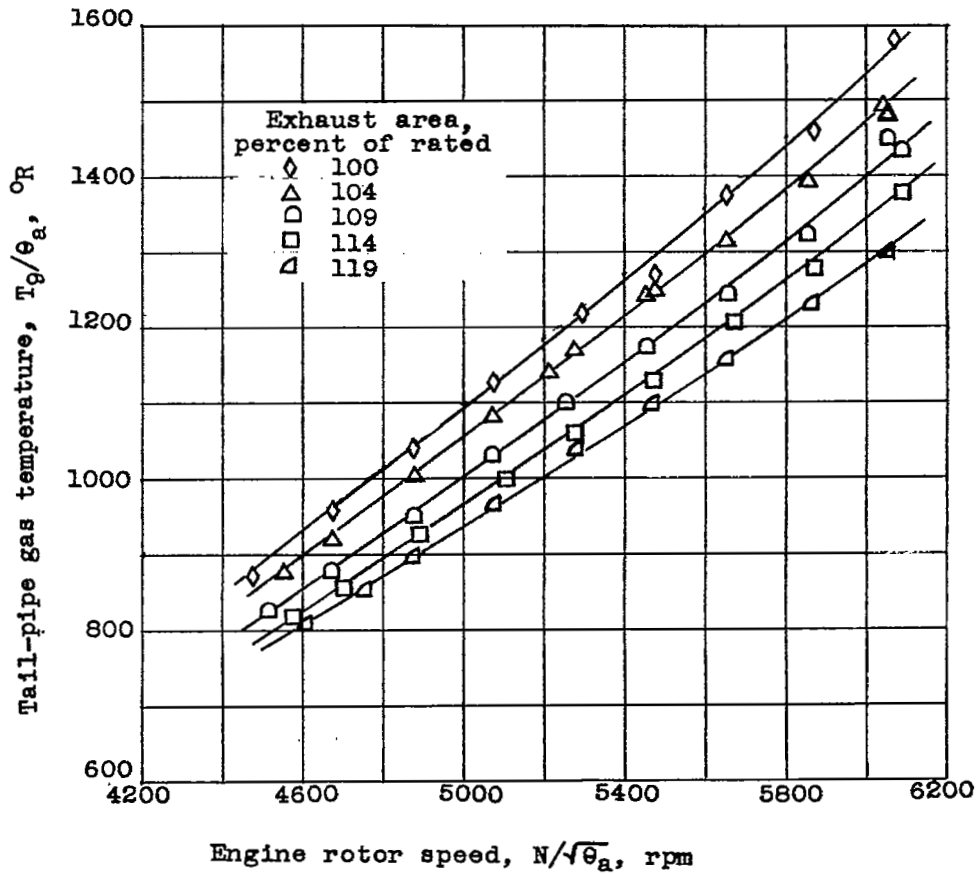


(a) Engine air flow.



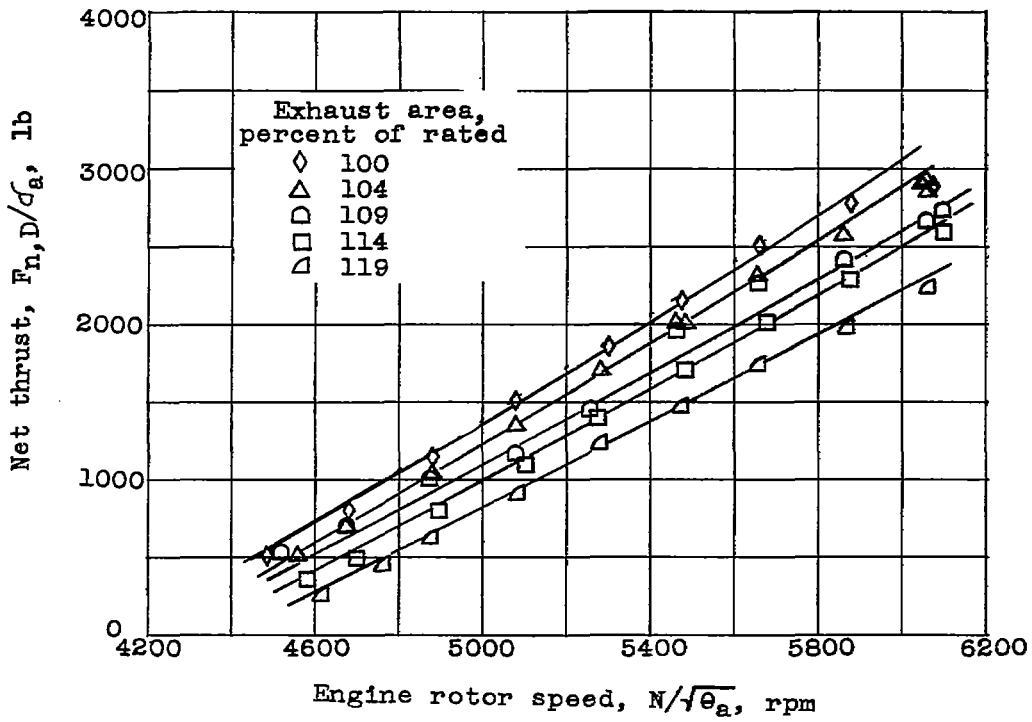
(b) Engine fuel flow.

Figure 3. - Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 35,000 feet; flight Mach number, 0.8.



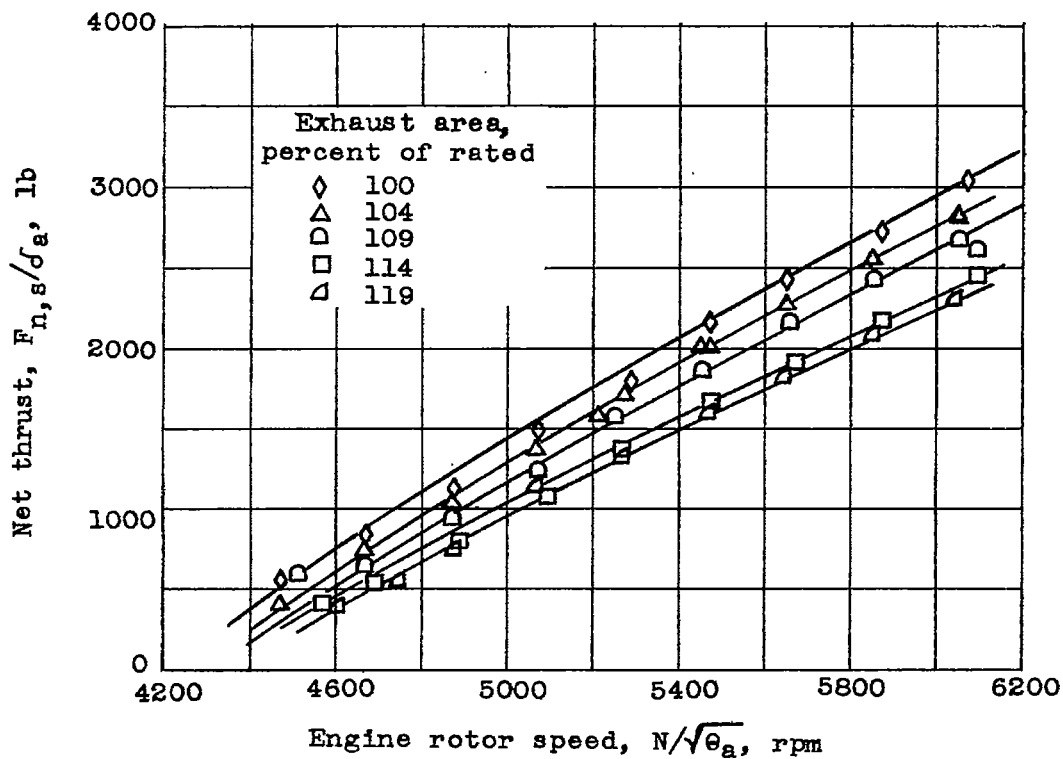
(c) Tail-pipe gas temperature.

Figure 3. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 35,000 feet; flight Mach number, 0.8.



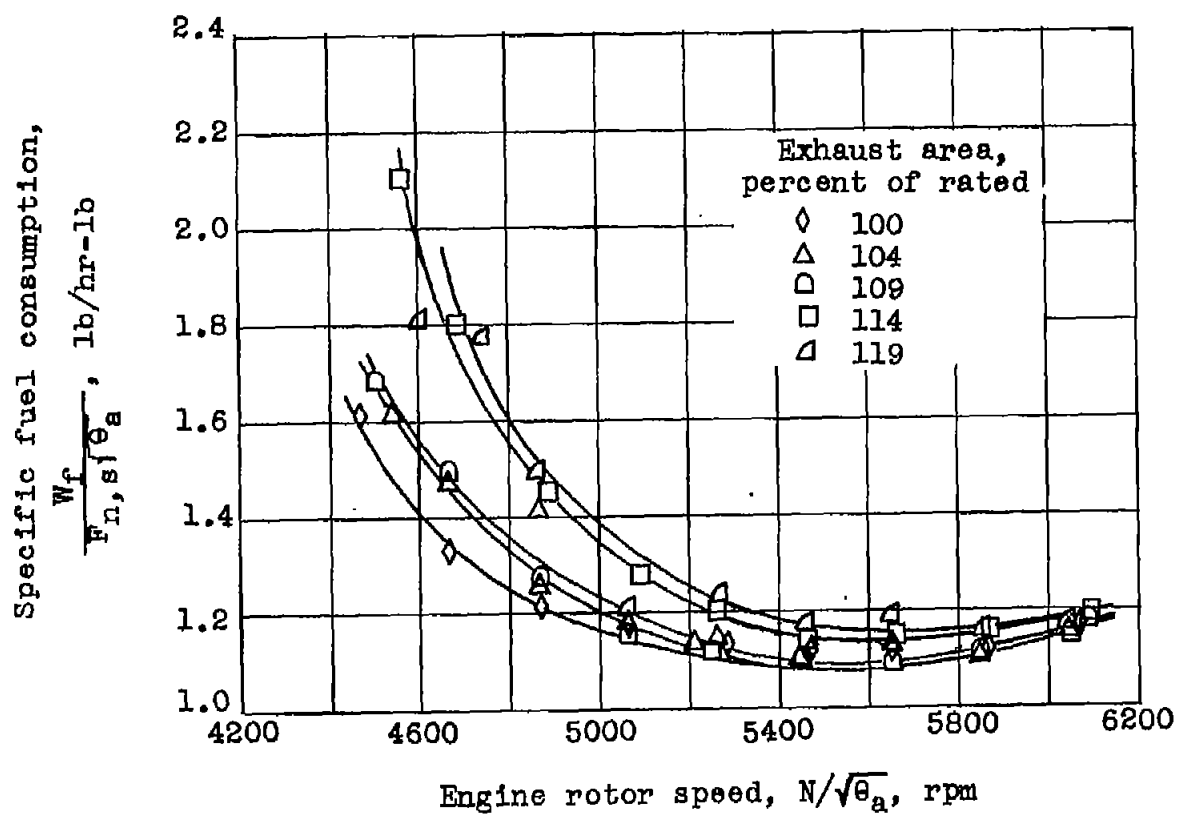
(d) Net thrust from Douglas rake.

Figure 3. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 35,000 feet; flight Mach number, 0.8.



(e) Net thrust measured by balance system.

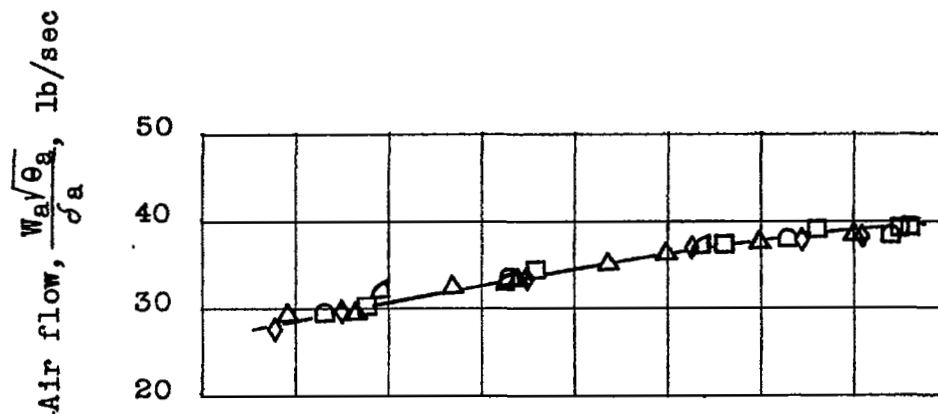
Figure 3. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 35,000 feet; flight Mach number, 0.8.



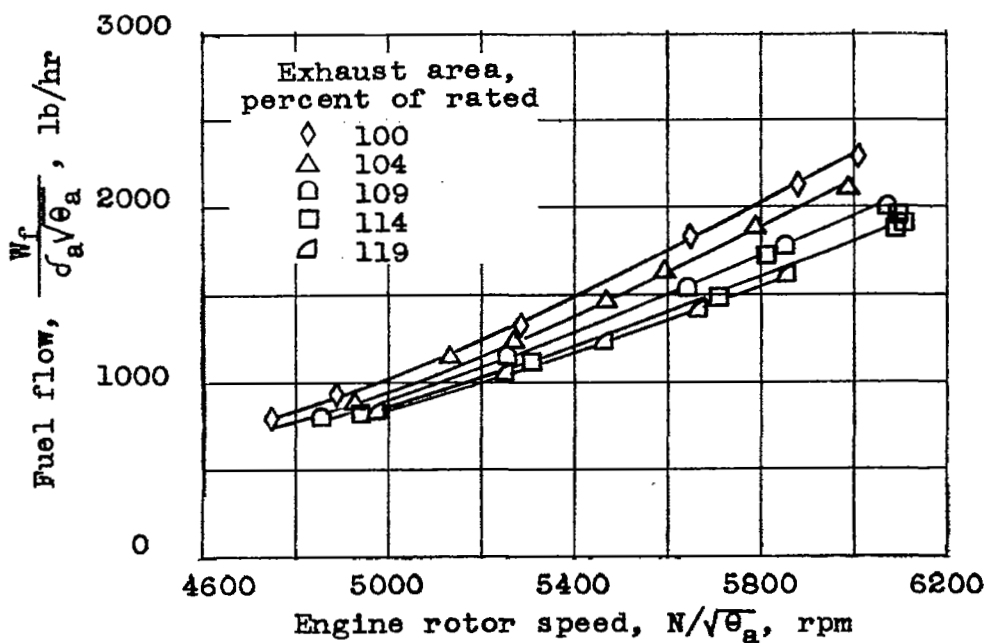
(f) Specific fuel consumption.

Figure 3. - Concluded. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 35,000 feet; flight Mach number, 0.8.



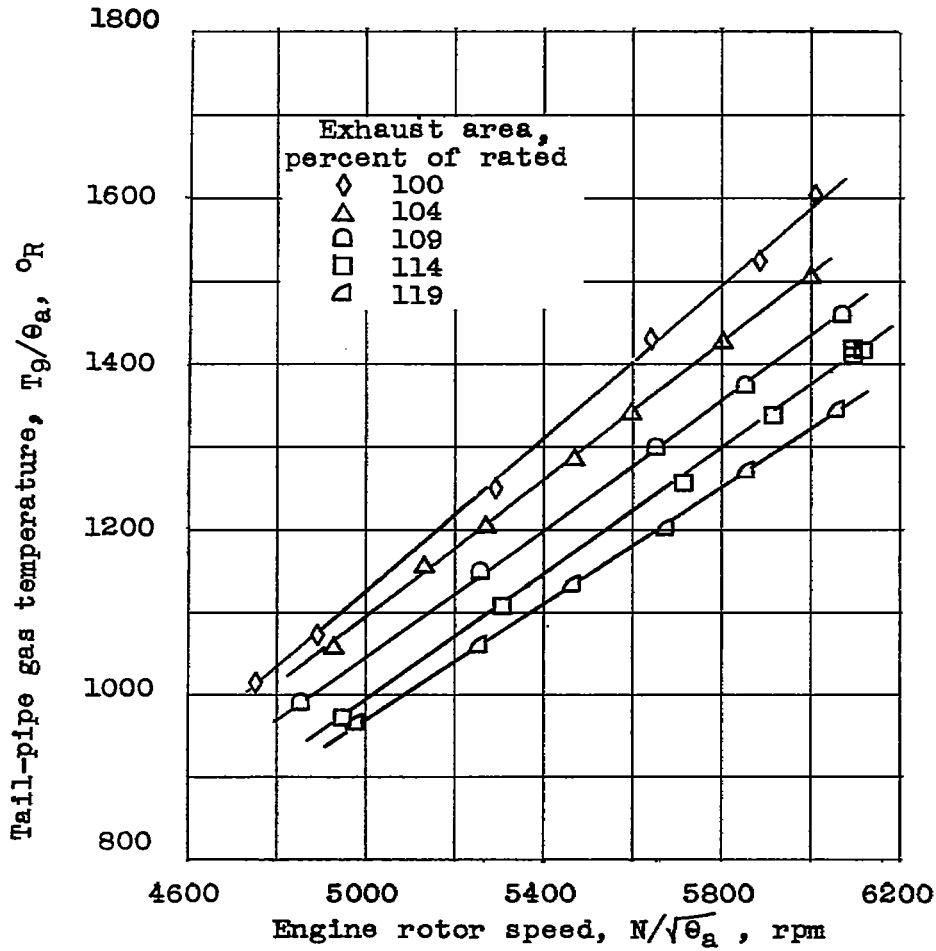


(a) Engine air flow



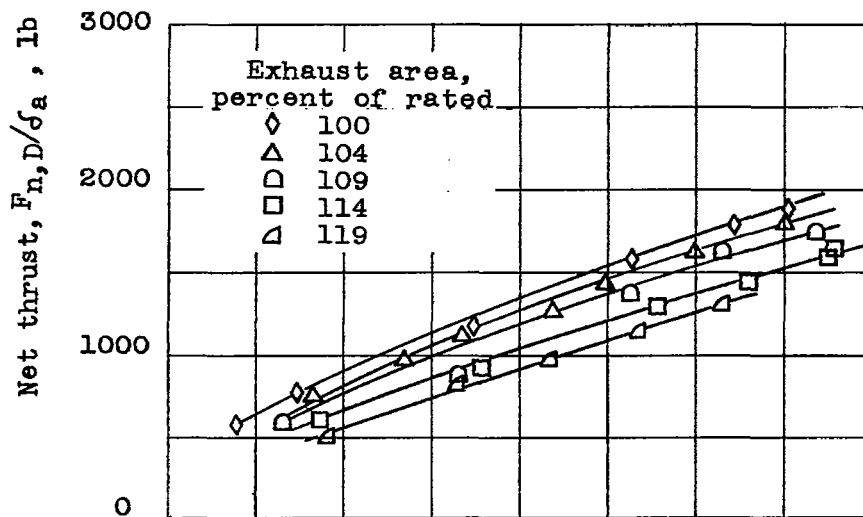
(b) Engine fuel flow.

Figure 4.- Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 45,000 feet; flight Mach number, 0.8.

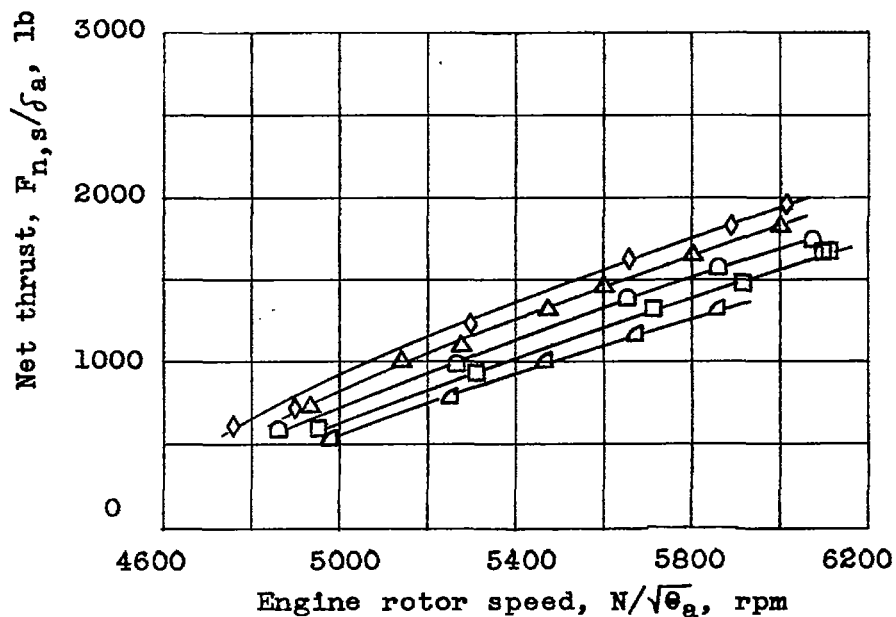


(c) Tail-pipe gas temperature.

Figure 4. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 45,000 feet; flight Mach number, 0.8.



(d) Net thrust from Douglas rake.



(e) Net thrust measured by balance system.

Figure 4. - Continued. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 45,000 feet; flight Mach number, 0.8.

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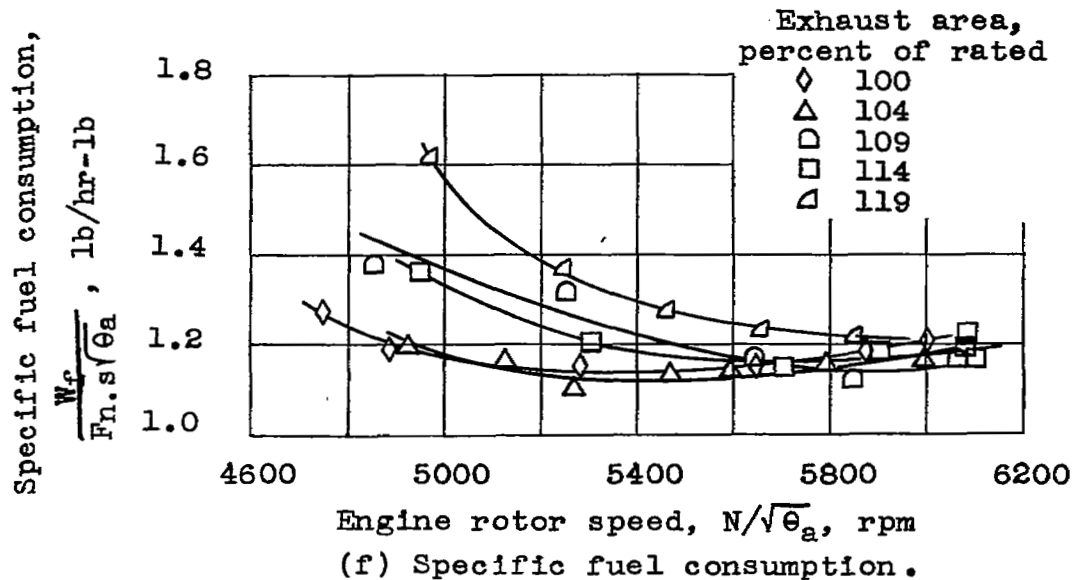
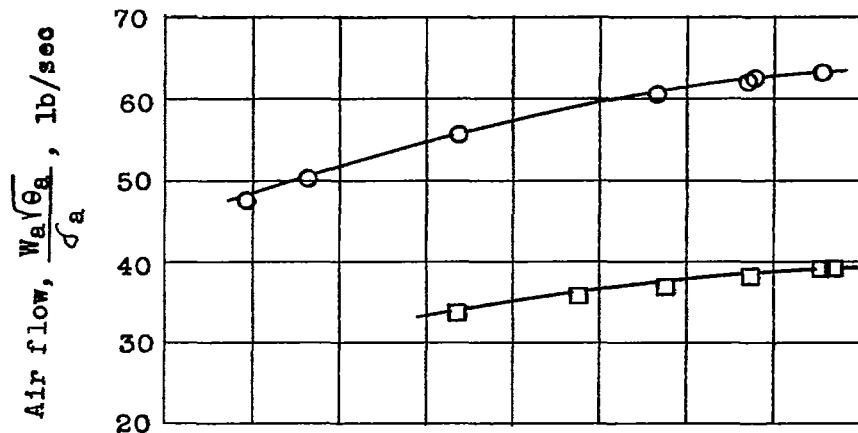
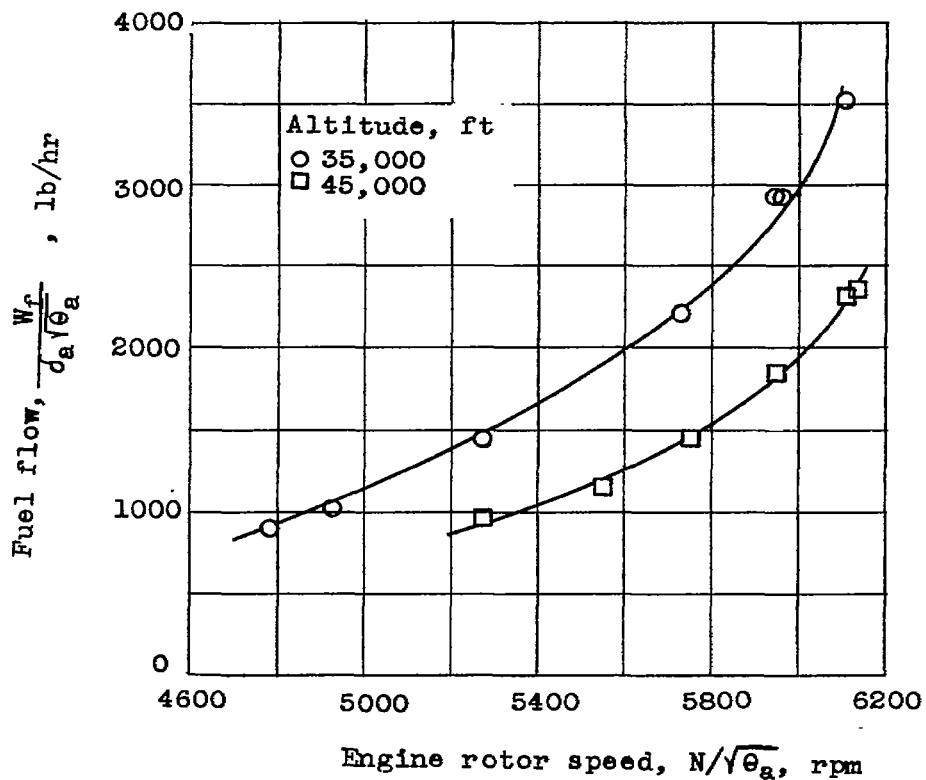


Figure 4.-Concluded. Performance of J71-A-11 turbojet engine with fixed-area exhaust nozzles. Altitude, 45,000 feet; flight Mach number, 0.8.

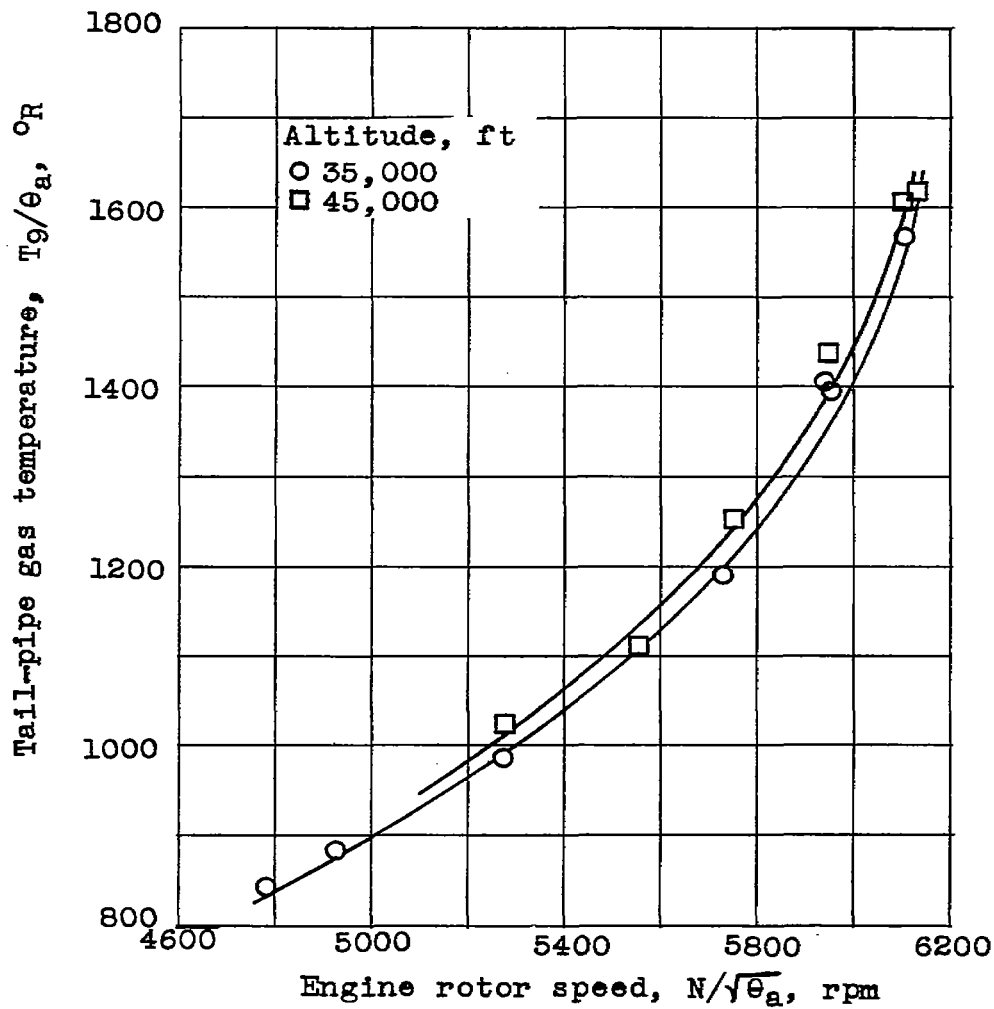


(a) Engine air flow.



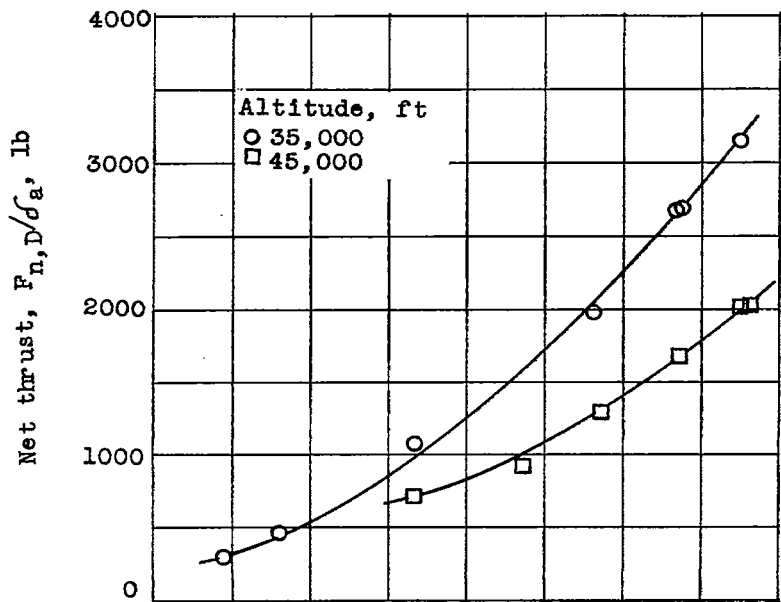
(b) Engine fuel flow.

Figure 5.- Simulated flight performance of J71-A-11 turbojet engine using interlinked control system and variable-area exhaust nozzle. Flight Mach number, 0.8.

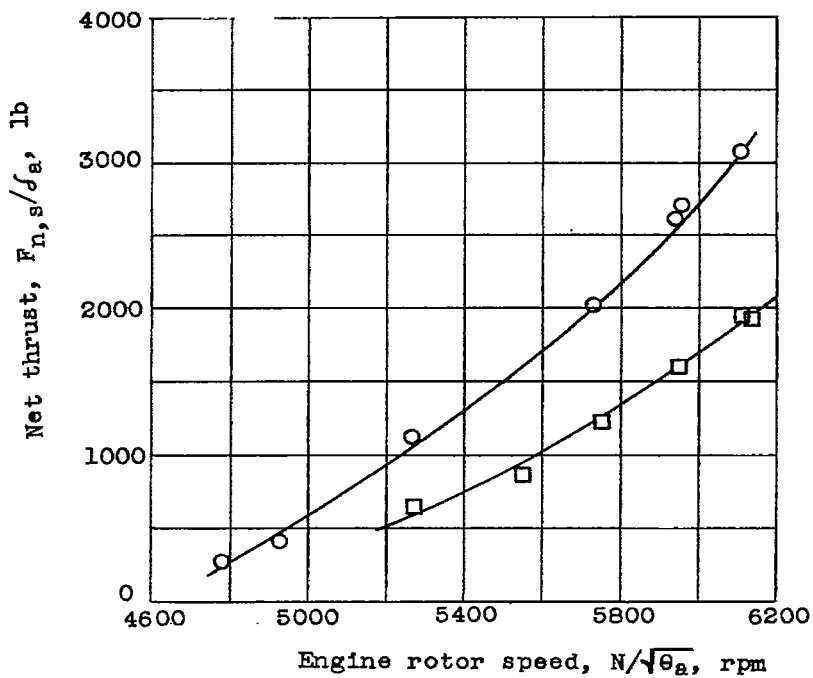


(c) Tail-pipe gas temperature.

Figure 5. - Continued. Simulated flight performance of J71-A-11 turbojet engine using interlinked control system and variable-area exhaust nozzle. Flight Mach number, 0.8.

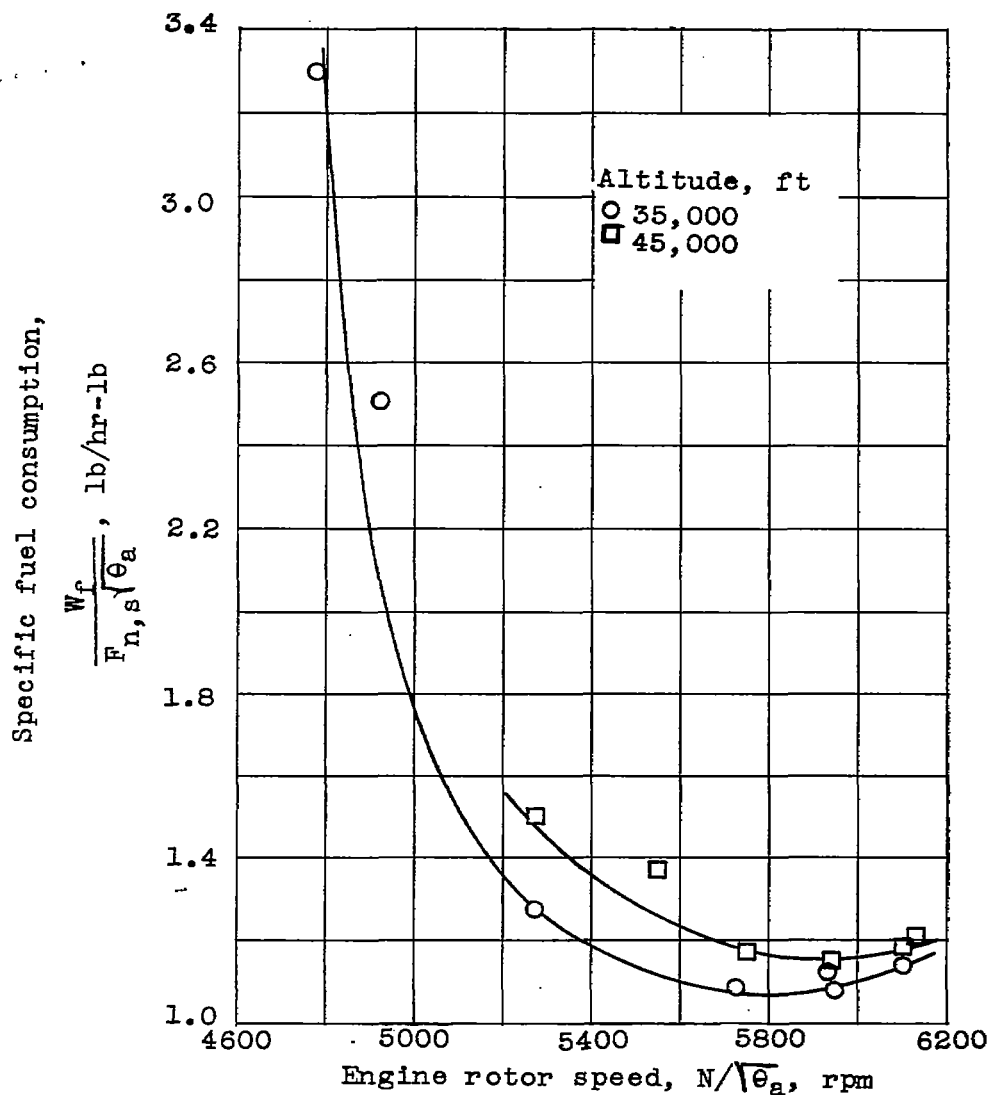


(d) Net thrust from Douglas rake.



(e) Net thrust measured by balance system.

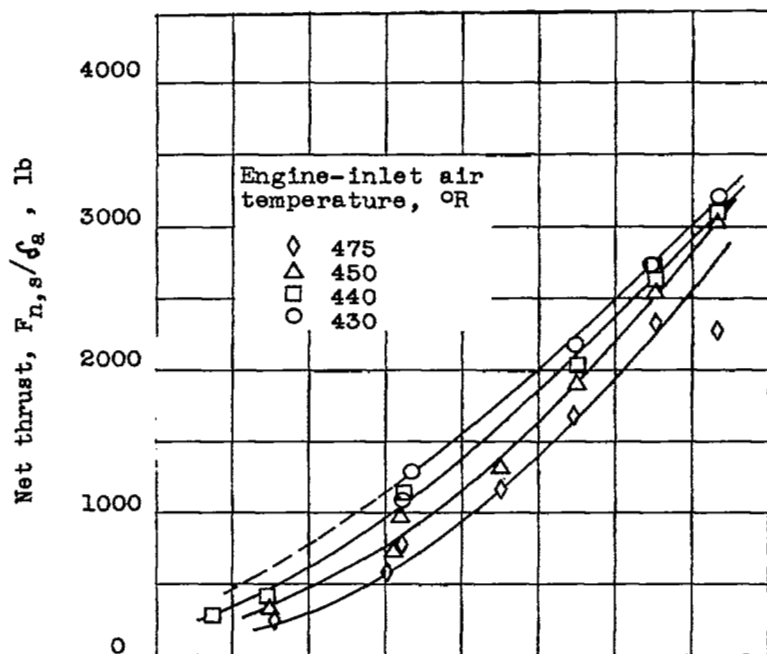
Figure 5. - Continued. Simulated flight performance of J71-A-11 turbojet engine using interlinked control system and variable-area exhaust nozzle. Flight Mach number, 0.8.



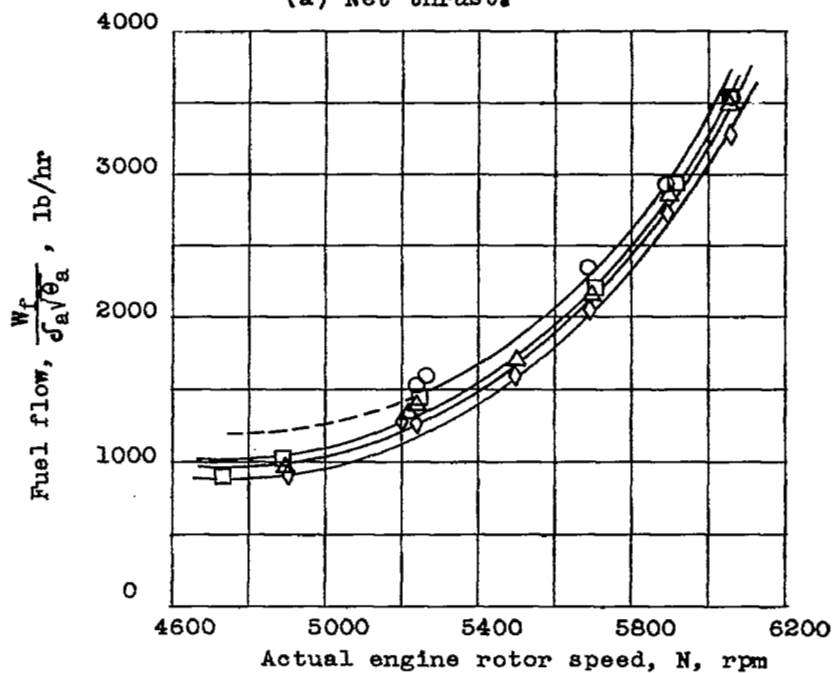
(f) Specific fuel consumption.

Figure 5. - Concluded. Simulated flight performance of J71-A-11 turbojet engine using interlinked control system and variable-area exhaust nozzle. Flight Mach number, 0.8.



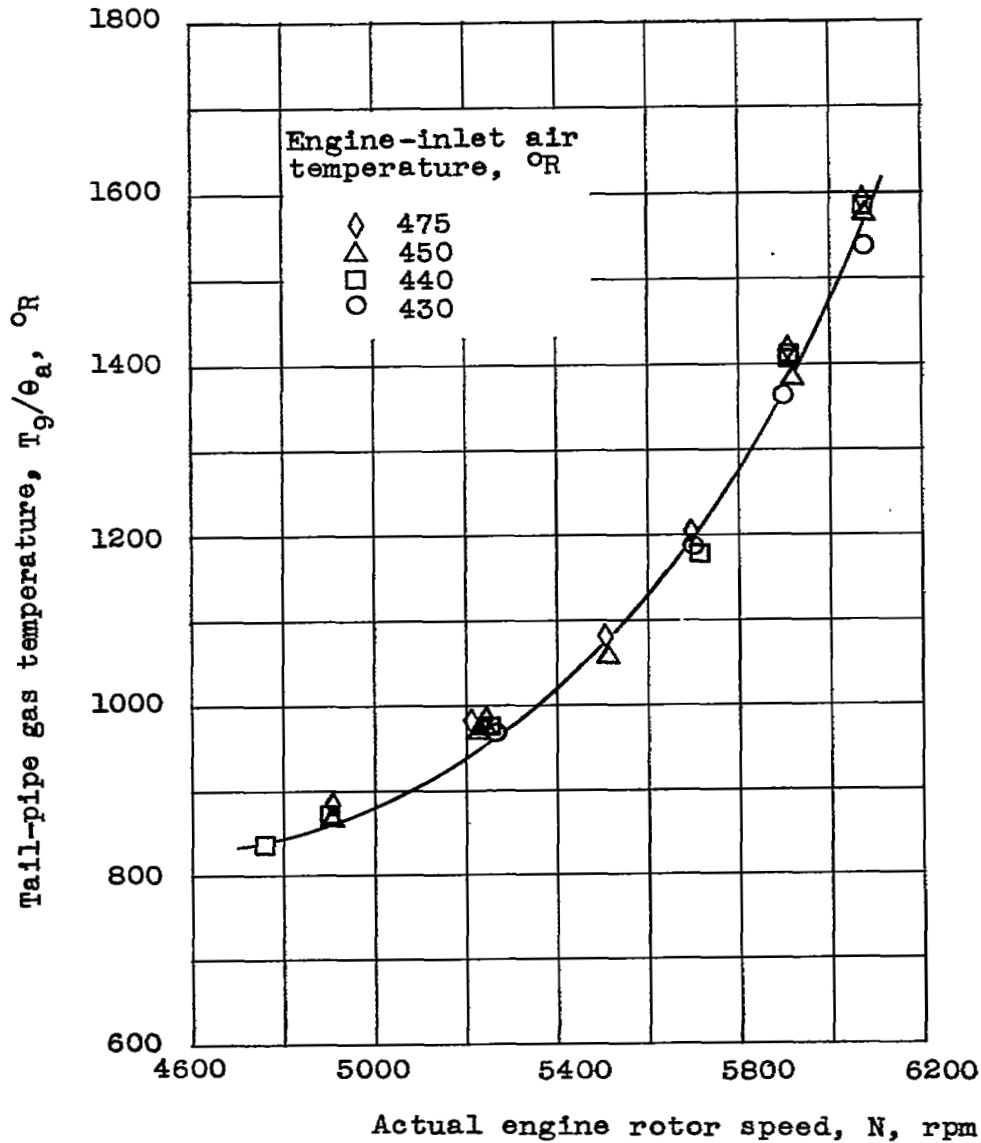


(a) Net thrust.



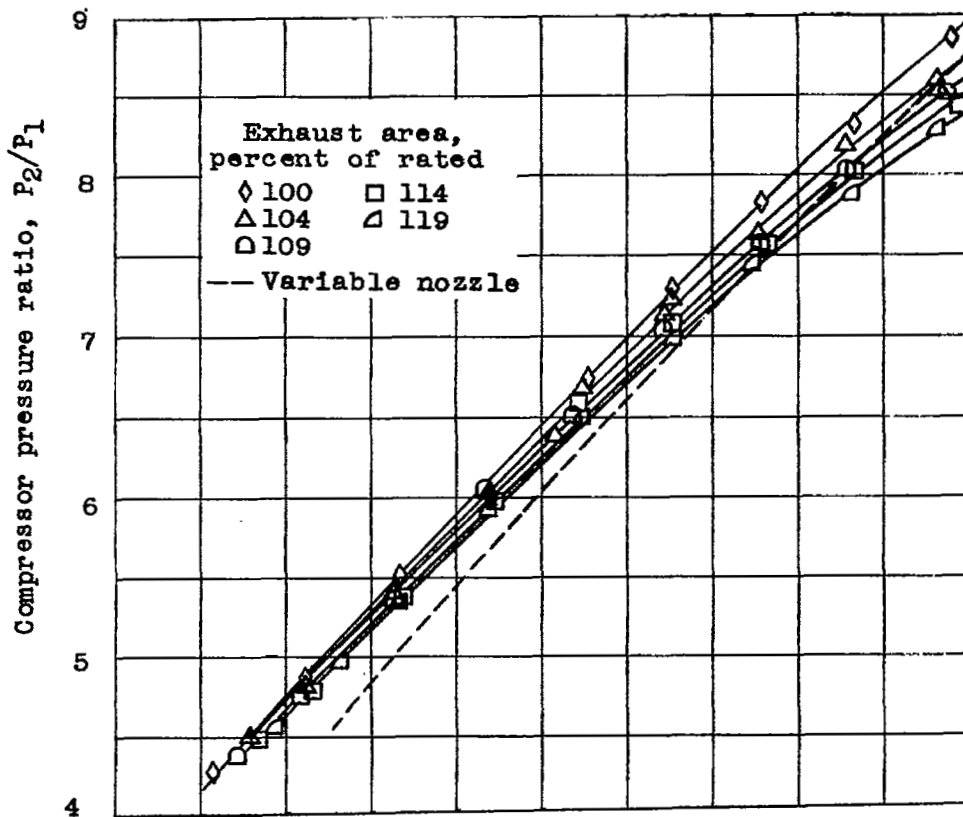
(b) Engine fuel flow.

Figure 6. - Effect of engine-inlet temperature on altitude performance of J71-A-11 turbojet engine. Variable-area exhaust nozzle interlinked with engine control system. Altitude, 35,000 feet; flight Mach number, 0.8.

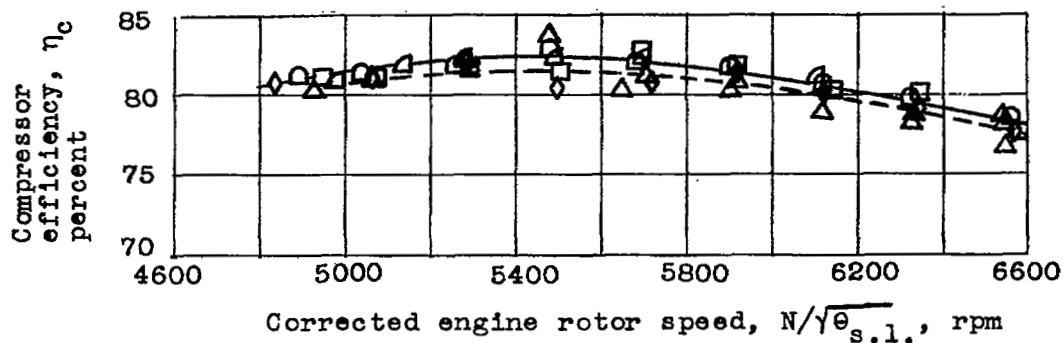


(c) Tail-pipe gas temperature.

Figure 6. - Concluded, Effect of engine-inlet temperature on altitude performance of J71-A-11 turbojet engine. Variable-area exhaust nozzle interlinked with engine control system. Altitude, 35,000 feet; flight Mach number, 0.8.



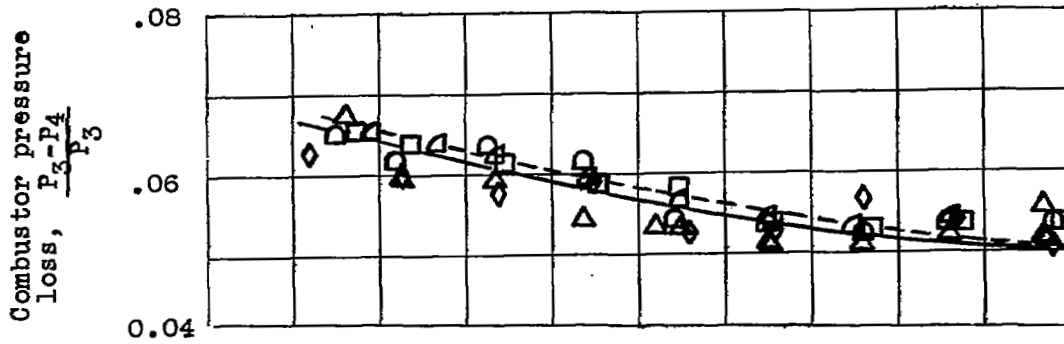
(a) Compressor pressure ratio.



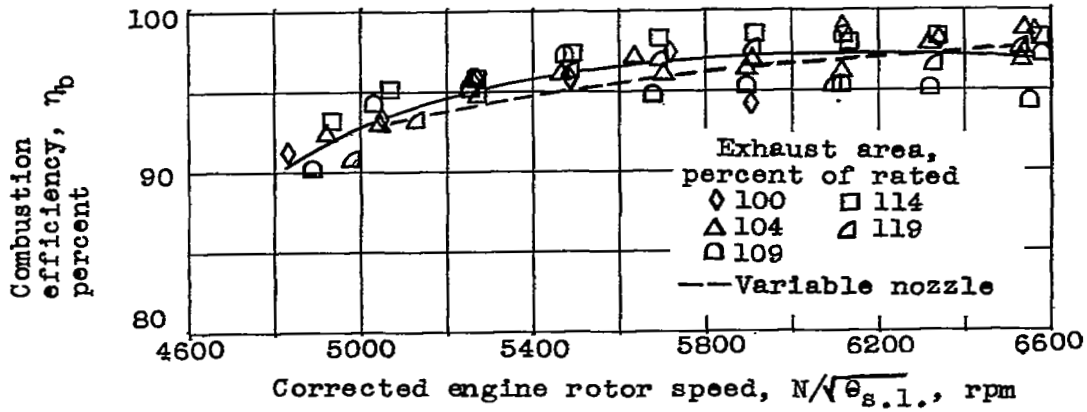
(b) Compressor efficiency.

Figure 7.- Component performance of J71-A-11 turbojet engine operating at an altitude of 35,000 feet and a flight Mach number of 0.8.

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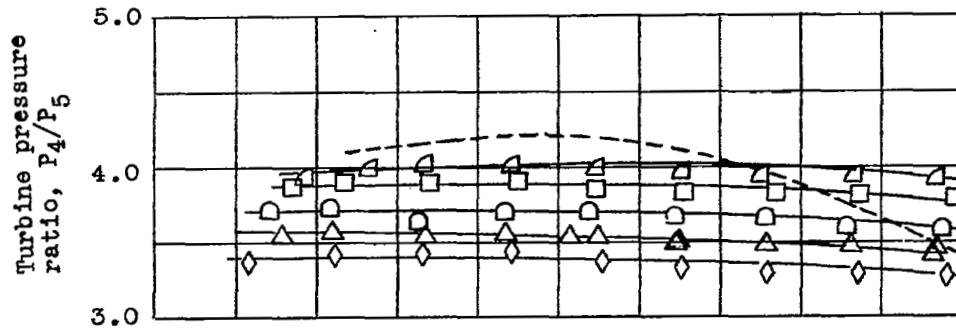


(c) Combustor pressure loss.

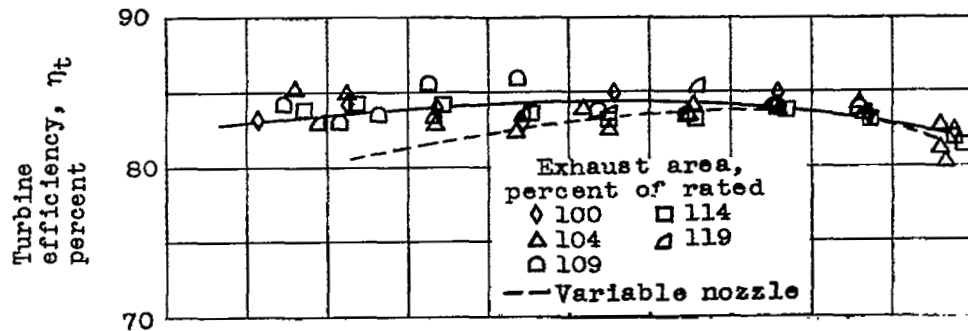


(d) Combustion efficiency.

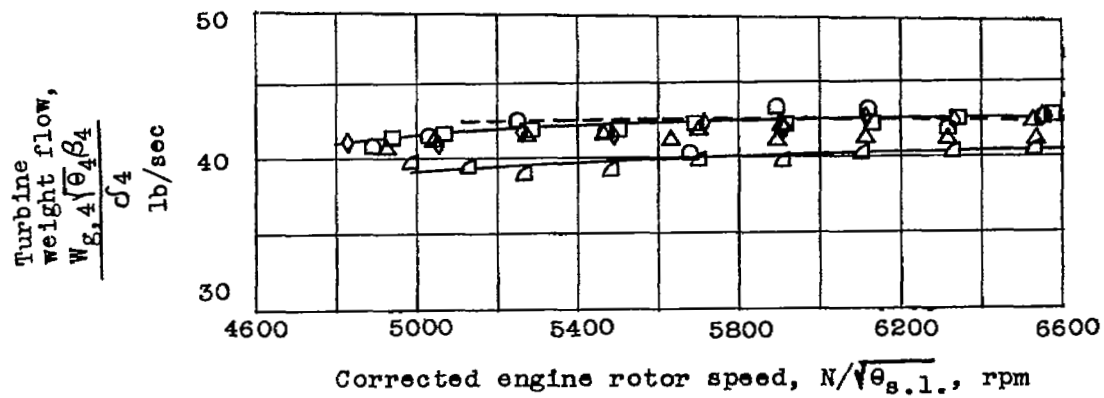
Figure 7. - Continued. Component performance of J71-A-11 turbojet engine operating at an altitude of 35,000 feet and a flight Mach number of 0.8.



(e) Turbine pressure ratio.

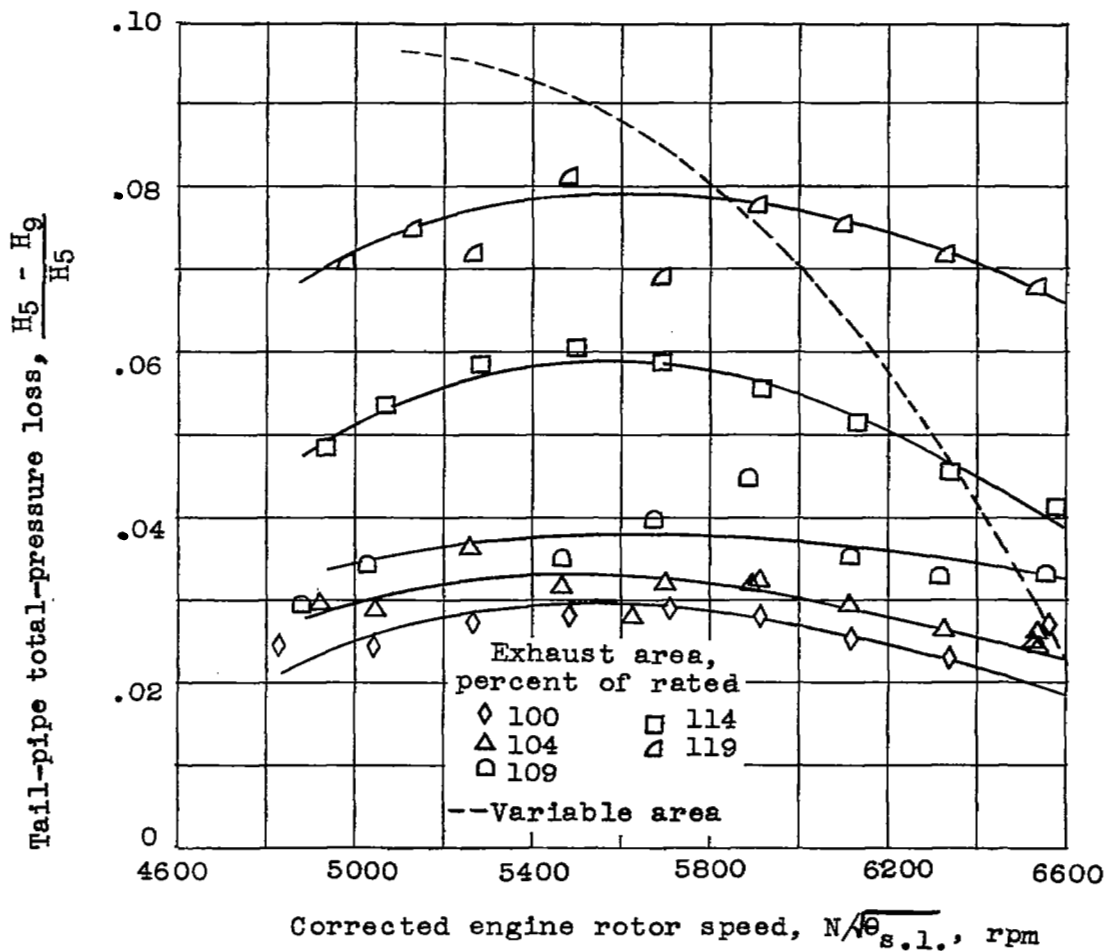


(f) Turbine efficiency.



(g) Turbine weight flow.

Figure 7. - Continued. Component performance of J71-A-11 turbojet engine operating at an altitude of 35,000 feet and a flight Mach number of 0.8.



(h) Tail-pipe total-pressure loss.

Figure 7. - Concluded. Component performance of J71-A-11 turbojet engine operating at an altitude of 35,000 feet and a flight Mach number of 0.8.

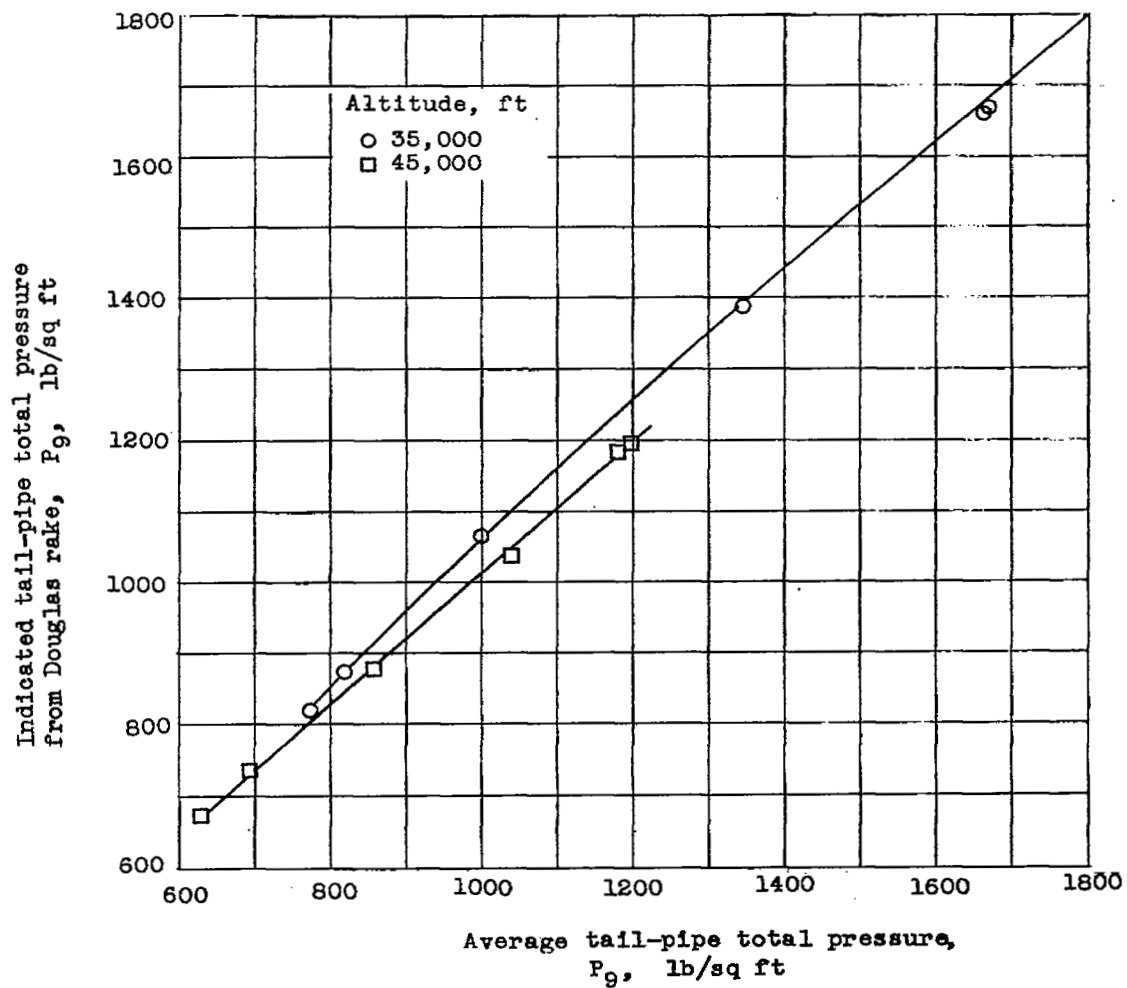


Figure 8. J71-A-11 turbojet engine tail-pipe total pressure indicated from Douglas rake compared with average of comprehensive pressure survey. Operation at a flight Mach number of 0.8.

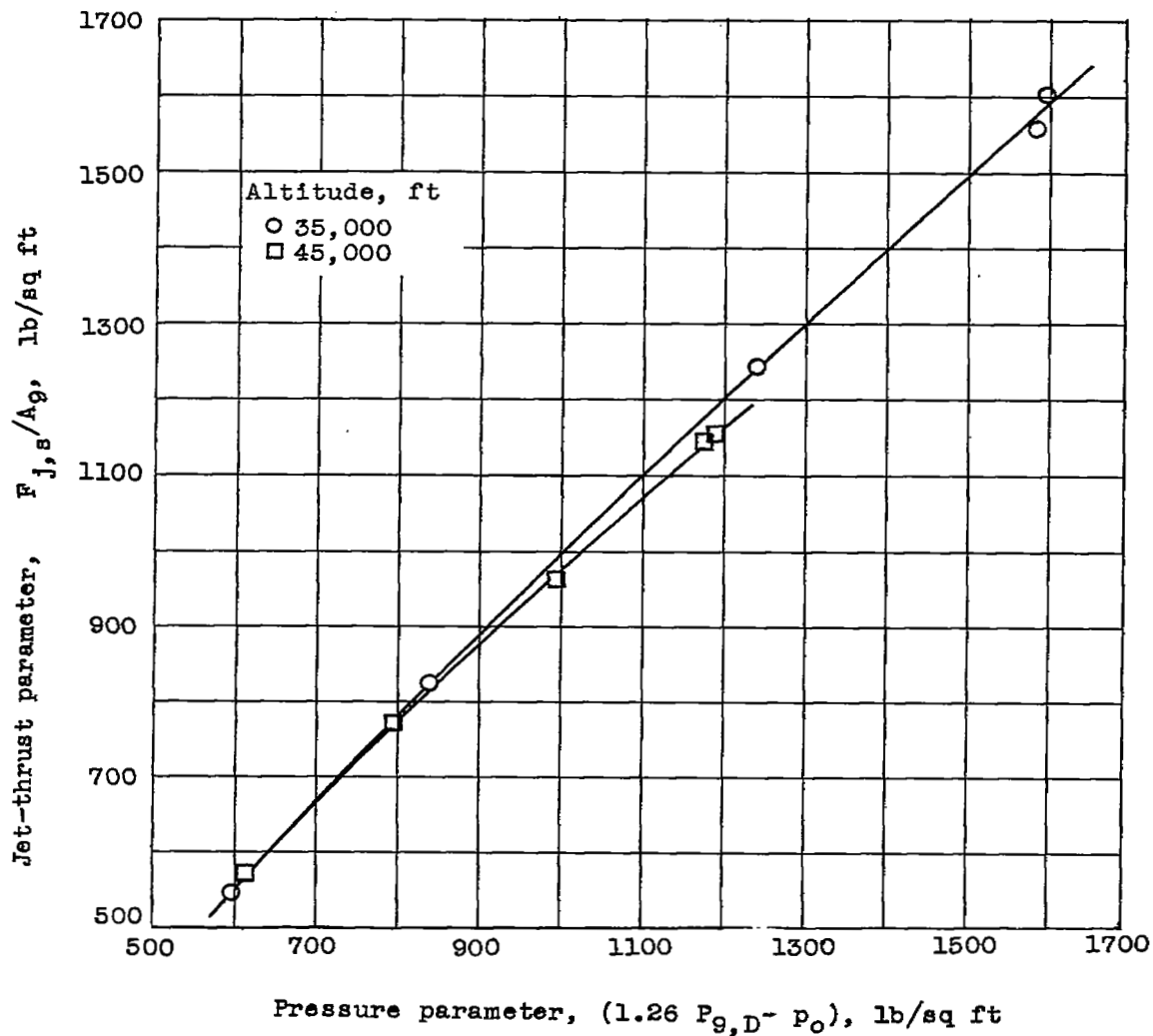


Figure 9. Jet thrust per unit exhaust-nozzle area as a function of Douglas rake indicated tail-pipe total pressure and altitude pressure. Flight Mach number, 0.8.



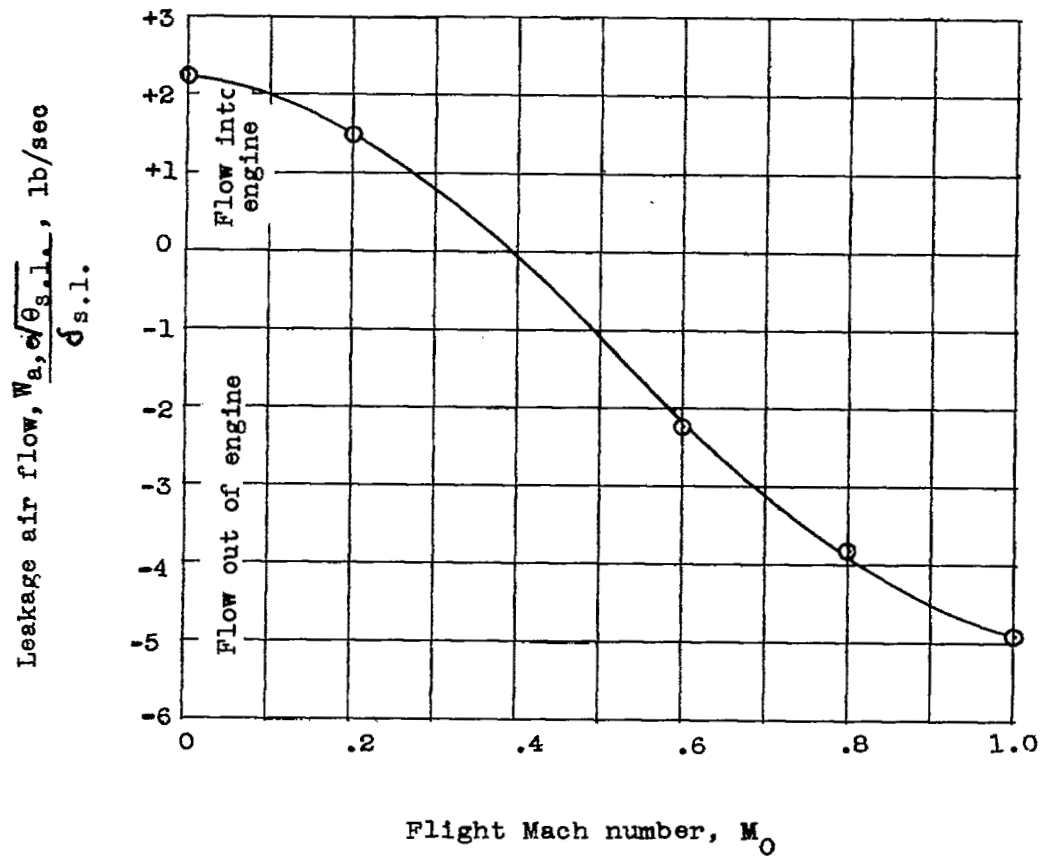


Figure 10. Calibration of air leakage at inlet-screen actuator holes. Corrected engine speed, 6100 rpm.

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