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Hot Corrosion Test Facility at the NASA Lewis Special Projects Laboratory

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SPECIAL PROJECTS LABORATORY**

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SUMMARY

The hot corrosion test facility (HCTF) at the NASA Lewis Special Projects Laboratory (SPL) is a high-velocity, pressurized burner rig currently used to evaluate the environmental durability of advanced ceramic materials such as SiC and Si₃N₄. The HCTF uses laboratory service air which is preheated, mixed with jet fuel, and ignited to simulate the conditions of a gas turbine engine. Air, fuel, and water systems are computer-controlled to maintain test conditions which include maximum air flows of 250 kg/hr (550lbm/hr), pressures of 100-600 kPa (1-6 atm), and gas temperatures exceeding 1500°C (2732°F).

The HCTF provides a relatively inexpensive, yet sophisticated means for researchers to study the high-temperature oxidation of advanced materials, and the injection of a salt solution provides the added capability of conducting hot corrosion studies.

INTRODUCTION

Future jet engines will provide more thrust at greater engine efficiency by operating at higher temperatures and using more advanced,

lightweight materials such as SiC and Si₃N₄ for hot-section engine components. The environmental durability of such candidates must be considered and is best evaluated if testing is conducted under realistic conditions, where the materials are subjected to the high temperatures and harsh environments encountered in a gas turbine engine. If operating in a corrosive environments, the high-temperature corrosion of hot-section components then becomes a concern. This process occurs when sodium, either as a fuel impurity or an airborne contaminant, combines with sulfur impurities in the fuel to form sodium sulfate (Na₂SO₄). Molten Na₂SO₄ can condense on hot engine components leading to accelerated oxidation and severe corrosion. Degradation by this salt is termed "hot corrosion."

Hot corrosion has been studied by immersion tests, thin salt film tests, and burner rig studies.¹ Burner rig tests more closely model the harsh, corrosive environments in a gas turbine engine while providing a continuous deposition of salt, opposed to the one-time deposition used in furnace testing. Two examples of previous studies at NASA Lewis involve the effect of hot corrosion on the room temperature four-point bend strength of sintered α -SiC.^{2,3} In those experiments, test variables included 1000°C (1832°F) specimen temperature, 4 atm system pressure, 2 ppm added sodium (as NaCl), and 40 hours of exposure time. A detailed view of the product layer formed on one sample is shown in Fig. 1, where portions of this product were chipped away to examine the interior of the layer. Removing the products by HF dissolution revealed a dramatic pitting attack of the SiC substrate, shown in Fig. 2. A correlation was found between fracture strength and corrosion pit dimensions, and the

strength decreased by as much as 25-35% due to the formation of deep pits in the SiC.

Studies like this make rigs such as the HCTF and other 1 atm, mach 0.3 burner rigs at NASA LeRC very valuable in the development of advanced aerospace materials. The purpose of this report is to promote awareness of the HCTF, provide corporate documentation of both the hardware and software being used, and describe the operation and capabilities of the test facility with emphasis on corrosion testing.

CORROSION TESTING REQUIREMENTS

At this point, it is helpful to discuss both the factors that influence hot corrosion and the significance of the HCTF in such studies. The deposition of Na_2SO_4 and subsequent corrosion is a function of temperature and pressure, therefore a burner rig used to study hot corrosion must satisfy certain requirements. The HCTF's operating range was specifically chosen such that deposition of the salt is predicted to occur on the test specimens.

As stated, hot corrosion occurs when sodium combines with sulfur impurities in the fuel to form Na_2SO_4 . Deposition of Na_2SO_4 occurs in a temperature window bordered by the melting point of the salt (884°C or 1623°F) and the dew point which is pressure dependent. The dew point is the highest temperature at which the condensed phase of the salt can form. A test temperature of 1000°C (1832°F) was targeted because furnace tests⁴⁻⁶ have shown rapid kinetics to occur at this temperature. The dew point was calculated⁷ (see Table I) for various sodium and sulfur combinations (jet fuel is typically 0.05% S) at a test pressure of 100

kPa (1 atm). The dew point ranged between 920-970°C (1688-1778°F) for 0.5-4.0 ppm of Na, respectively. Higher operating pressures will raise the dew point and allow deposition to occur at higher temperatures. As a result, testing at higher pressures will more accurately model conditions in the engine, and since it raises the dew point, test temperatures of 1000°C (1832°F) can be obtained. Given a test pressure of 400 kPa (4 atm), dew points are on the order of 981-1038°C (1798-1900°F), therefore deposition should occur for sodium concentrations above 2.0 ppm, as indicated by Table I.

In summary, the HCTF allows testing at temperatures of 1000°C (1832°F) or above, but more importantly the capability of being pressurized to 4 atm assures Na₂SO₄ deposition.

TEST FACILITY SYSTEMS

The HCTF pictured in Fig. 3 has a number of critical systems which must work together to attain desired test conditions. These systems include the air, fuel, water, and salt systems which are shown schematically in Fig. 4. The combustion process occurs as preheated air is mixed with jet fuel and ignited in the combustor. After ignition, a salt solution is introduced into the gas stream. The hot gases flow downstream passing over the test specimens located in the test section, where temperature and pressure is maintained by automated control. Before exiting, the hot exhaust gases are quenched with cooling water to desired temperature levels.

AIR SYSTEM The HCTF uses 800 kPa (120 psig) pressurized air supplied by the laboratory central air system. The pressurized air is filtered

through a filter assembly and then passes through a venturi flowmeter. The mass flow rate is calculated from the pressures, temperature, and flow coefficients associated with the venturi. Air flow, which is controlled using valve A, can be supplied at rates of 50-250 kg/hr (100-550 lbm/hr), with a typical corrosion test operating at a mass flow rate of 150 kg/hr (325 lbm/hr). The air flow is directed into a preheater which increases the air temperature to 260°C (500°F) prior to entering the combustor. Preheating allows combustion to occur more efficiently, resulting in less soot development and buildup in the combustor.

The rig is pressurized to higher pressures by closing down exhaust valve B. As mentioned, test pressures can be varied between 100-600 kPa (1-6 atm), depending on mass air flow rates. Maximum air flows are available only at lower pressures. As discussed, hot corrosion tests are typically conducted at 4 atm to raise the dew point of Na_2SO_4 above 1000°C (1832°F).

FUEL SYSTEM The HCTF can burn Jet-A, JP-4, or JP-5 jet fuel, as well as diesel fuel. The jet fuels are supplied from a 19,000 liter (5000 gal) underground storage tank while the diesel fuel is supplied from a smaller surface tank. Each storage tank is equipped with a low-pressure fuel pump and 25-micron filter for delivering fuel to the facility. The fuel then passes through a high-pressure pump (1.7 MPa or 250 psig max.) in the test cell before being filtered through a second, 10-micron assembly and injected into the combustor.

The amount of fuel burned depends on the desired test temperature. Fuel flow is controlled with valve C, which schedules the fuel-to-air ratio required to produce the desired temperature. Flow rates, which are

measured with a turbine flowmeter, are relatively low with a maximum of 0.1 l/min (.025 gpm). A fuel nozzle (80°swirl) sprays atomized fuel into the combustor where it is mixed with the combustion air and ignited. The available range of fuel-to-air ratios and resulting gas temperatures are given in Fig. 5, suggesting only minimal heat loss when compared to calculated adiabatic temperatures. As an example, the standard hot corrosion test temperature of 1000°C (1832°F) would require a fuel-to-air ratio of approximately 0.024. This corresponds to a fuel flow near 0.073 l/min (.019 gpm) for the standard mass air flow of 150 kg/hr (325 lbm/hr).

WATER SYSTEM City water (400 kPa or 60 psig) is used to quench the combustion air exiting the test section. The hot gases expelled from the combustor, noted to reach as high as 1500°C (2732°F), must be cooled to protect the exhaust valve from thermal failure. The water pressure is initially boosted using a high-pressure pump (10 MPa or 160 psig max) before being filtered through a 25-micron filter. Water flow rates, also measured with a turbine flowmeter, are regulated with valve D as the cooling water is directed through a spray ring and water jet nozzles located before the exhaust valve. A Chromel-Alumel thermocouple (type K) monitors the exit temperature used to control the water flow. Only a flow of 2.0 l/min (.5 gpm) is required to cool the exhaust below 100°C (200°F).

SALT SYSTEM Salt solutions are injected into the hot gases leaving the combustor with an aspirating probe. The salt solution typically consists of 2-4 ppm NaCl in distilled water and is supplied from a 20 liter teflon tank located in the test cell. Salt flow is controlled with an

adjustable pump, capable of delivering a maximum steady flow of 2.0 l/hr. Current hot corrosion tests operate at a flow near 0.25 l/hr. Salt flow is indicated by a load cell which monitors the weight change of the salt tank. The salt solution is atomized within the aspirator probe and injected into the combustor.

TEST FACILITY CONFIGURATIONS

For discussion purposes, the HCTF has two primary areas of concern, the combustor and the test section (Fig. 6). Maintenance is often required in these areas due to their high-temperature nature and typically involves the replacement of certain components or the installation of test specimens. This section of the report focusses on the configuration of these two areas, discussing both the components and instrumentation which are an integral part of each area.

In Fig. 7, preheated air enters the combustor through a 1.9 cm (3/4 in) inlet. Here, a thermocouple (type K) monitors the inlet temperature used to control the preheater. Combustion pressure is also monitored. The air is forced through a swirler and mixed with the atomized fuel in the combustor liner. The fuel is sprayed from a fuel nozzle found in the center of the co-rotating swirler. Gases in the primary zone are ignited with a spark generated from an ignitor which extends through an opening in the liner. The liner, fabricated from Inconel 601 material, is cooled with bypass air flowing down the outside diameter. This cooling air eventually dumps into the secondary zone through perforations in the liner and is added to the combustion process. The salt aspirator and a platinum-platinum/(13%)rhodium

thermocouple (type R) also extend through an opening into the liner. The combustion thermocouple monitors the flame temperature inside the liner and is used to detect a flameout condition.

As the combustor transitions into the test section, the hot gases accelerate through a nozzle and into the flame tube. Gas velocities typically reach 45-60 m/s (150-200 ft/sec) but can exceed 300 m/s (1000 ft/sec). Two test specimens (2.54 cm x 0.64 cm x 0.32 cm) are loaded horizontally through openings in the flame tube. The two specimens are held by a set of lava grips which are positioned by a lava specimen holder clamped to the flame tube. A cross section of this arrangement is shown in Fig. 8. A thermocouple (type R) is positioned on center between the two test specimens to monitor the test temperature and to control fuel flow. A flange on either side can be removed to gain easy access to the test section, which along with the transition section is packed with ceramic fiber insulation to minimize heat losses. A second set of test specimens can be assembled downstream in the test section (see Fig. 6). Here, the thermocouple is for information purposes only and temperatures are reduced approximately 25°C (50°F) due to heat losses.

DATA ACQUISITION AND CONTROL SYSTEM

The HCTF is equipped with an automated data acquisition and control system which is responsible for collecting data and modulating the control valves of the air, fuel, and water supplies. The rig is operated from the control room (Fig. 9), containing both the computer system and control panel. The computer system is integrated with the manual controls which include all the "hard-wired" permissives and

safety interlocks which must be satisfied before computer operation of the control valves is permitted.

The computer interfaces with a data acquisition and control unit to manage data flowing between the test facility and control room. An internal voltmeter collects data from pressure, temperature, and flow sensors. The data is processed by software and displayed as shown in Fig. 10, along with test parameter setpoints and valve positions. As setpoints are changed with the special function keys, control subroutines compare the data with corresponding setpoints and automatically make any necessary corrections to valve positions. Data scanning and setpoint control occurs at 0.5-1.0 Hz. The test parameters available for such closed-loop feedback and control include mass air flow, specimen temperature, and system pressure.

The software was developed internally at NASA LeRC and is listed in Appendix A for documentation purposes. In addition to data acquisition and control, the software also provides automated documentation. Data may be printed out or stored on a hard disk at user-defined intervals. Furthermore, a test log (Fig. 11) is used to store the test conditions and specimen data of individual test runs. These test conditions include a programmable "real-time" clock which adds the capability of unattended operation.

SAFETY FEATURES

The HCTF was designed with safety interlocks which prevent the rig from reaching a potentially unsafe or destructive mode. The HCTF's control logic will initiate a shutdown to safely handle any critical

situation. As mentioned, the computer works together with these "hard-wired" features, requiring that certain permissives are satisfied before computer operation of the control valves is permitted.

The most important parameters monitored are temperature and pressure. As previously mentioned, the HCTF was designed with a preheater which can only be operated if sufficient air flow is indicated by a pressure switch located at the venturi meter. Even as sufficient air flow is present, ignition is permitted only when the preheated air temperature is between assigned low and high limits. Other critical parameters which either must be within limits before ignition or during operation include combustor temperature, exit temperature, and system pressure. The upper and lower limits are given in Table II.

In the event that any critical limits are exceeded, an appropriate meter relay will automatically close the fuel supply solenoid valve and disable computer control of the fuel. Indicator lights in the control panel are used to provide diagnostic information. Therefore, any loss of air flow, mechanical malfunction, or operator control error will result in shutdown of the rig.

Although having a secondary logic priority, the computer will also initiate the shutdown of the facility under certain circumstances. If sensor data is not within software-defined limits, closed loop control of the setpoints is no longer possible. Therefore, the control valve to the fuel is closed, triggering the "hard-wired" shutdown. A diagnostic message is printed to indicate which parameter caused the shutdown.

CONCLUSIONS

The SPL hot corrosion test facility at NASA Lewis is a relatively simple, easy-to-operate resource for providing researchers with valuable information on advanced, high-temperature materials. Low maintenance and fuel costs make the facility attractive economically, and the rig's flexibility makes it useful for both oxidation and corrosion studies. The HCTF has been helpful in numerous programs, evaluating materials for aerospace, automotive, and other applications. Researchers interested in using the HCTF should contact the Facility Manager, Environmental Durability Branch, or the Materials Division.

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REFERENCES

1. N. S. Jacobson, J. L. Smialek, and D. S. Fox, "Molten Salt Corrosion of SiC and Si₃N₄," Handbook of Ceramics and Composites, Vol. 1: Synthesis and Properties (N. P. Cheremisinoff, ed), Marcel Dekker, New York, 99-136 (1990).
2. N. S. Jacobson, C. S. Stearns, and J. L. Smialek, "Burner Rig Corrosion of SiC at 1000°C," Adv. Ceram. Mat., 1 [2] 154-161 (1986).
3. D. S. Fox and J. L. Smialek, "Burner Rig Hot Corrosion of Silicon Carbide and Silicon Nitride," J. Am. Ceram. Soc., 73 [2] 303-311 (1990).
4. N. S. Jacobson and J. L. Smialek, "Hot Corrosion of Sintered SiC at 1000°C," J. Am. Ceram. Soc., 68 [8] 432-39 (1985).
5. J. L. Smialek and N. S. Jacobson, "Mechanism of Strength Degradation for Hot Corrosion of α -SiC," J. Am. Ceram. Soc., 69 [10] 741-752 (1986).
6. N. S. Jacobson, "Kinetics and Mechanism of SiC Molten Salt Corrosion," J. Am. Ceram. Soc., 69 [1] 74-82 (1986).
7. S. Gordon and B. J. McBride, "Computer Program for Calculation of Complex Chemical Equilibrium Compositions, Rocket Performance, Incident and Reflected Shocks, and Chapman-Jouget Detonations," NASA SP-273 (1976).

APPENDIX A

The software listed on the following pages has been included to serve as documentation for the control and operational procedures used in this facility. As seen before, test facilities can experience periods of dormancy due to programmatic or personnel changes. In such a case, this record could prove critical in attempts to renew operations of the facility after any such period.

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10 ! PROGRAM "X1PGM"
20 ! 4.0 ATMOSHERES, HOT CORROSION BURNER RIG
30 ! CELL #1-BLDG. 24
40   OPTION BASE 1
50   MASS STORAGE IS ":CS80,805"
60   PRINTER IS 1
70   SYSTEM PRIORITY 9
80   GOSUB Clearscreen
90   PRINT TABXY(1,5)
100  PRINT "*****"
110  PRINT "      *      *"
120  PRINT "      *   X1PGM - SPL HCTF DATA ACQ.   *"
130  PRINT "      *   LATEST REVISION: 1/93          *"
140  PRINT "      *      *"
150  PRINT "      *   THIS PROGRAM IS THE PROPERTY OF   *"
160  PRINT "      *   THE NASA ENVIROMENTAL DURABILITY  *"
170  PRINT "      *   BRANCH. MAINTENANCE BY UNAUTHOR-  *"
180  PRINT "      *   IZED PERSONNEL IS PROHIBITED.    *"
190  PRINT "      *      *"
200  PRINT "      *   CONTACT: C. ROBINSON X-5547      *"
210  PRINT "*****"
220  WAIT 4
230  DIM Chan_label$(40)[14],Display_format$(40)[5],Sensor$(40)[5]
240  DIM Unit$(40)[5],Disp$(12)[80],L$(10),A$(5),B$(5),Title$(9),Fuel$(6)
250  DIM Ans$(25),Run_time$(11),Target_time$(15),Elap_time$(15)
260  DIM Air_control$(6),Back_control$(6),Fuel_control$(6),Blank$(80)
270  DIM Specimen$(4)[15],Install$(4)[15],Tot_time$(4)[15]
280  DIM Volt(30),Dval(40),K(13),R(13),Hi_lim(40),Low_lim(40)
290  DIM P(7,5),Amt(5),P_prop(5)
300  REAL Vref,Volt_comp,Vt,Temp,Err,Out,Prop,Sp_fraction
310  REAL Ts,Trun,Trun_start,Prev_ts,Tp,Fuel_gal,Target_temp
320  REAL Fuel_sp,Quench_sp,Air_sp,Back_sp,Setpoint
330  REAL Spec_temp_sp,Quench_temp_sp,Air_flow_sp,Back_psi_sp
340  REAL C,F,Tair,Roe,Wair_cf,Mu,Re_cf,Cf
350  INTEGER I,J,N,X,Z,Y,Print_order(15),Ignite_ind,Screen(12,2),Ans,Pid_ind
360  INTEGER Nlines,Nlines_page,Hot_ind,Prt_int,Out_lim_ind,Cntrl_ind,Pid
370  INTEGER Hours,Minutes,Tot_hours,Tot_minutes,Target_minutes
380  INTEGER Airout,Backout,Quenchout,Fuelout
390  Main_menu_keys: !
400  PRINTER IS 1
410  OFF KEY
420  ON KEY 0 LABEL "   RUN RIG   ",10 GOTO Main
430  ON KEY 2 LABEL "   TEST SETUP ",10 GOTO Setup
440  Menu_display: !
450  GOSUB Clearscreen
460  PRINT TABXY(1,5);"
470  PRINT TABXY(1,8);"
480  PRINT TABXY(1,10);"
490  PRINT TABXY(1,12);"
500  Echo: !
510  GOTO Echo
520  !!!!!!!!!!!!!!! TEST SETUP SUBPROGRAM !!!!!!!!!!!!!!!
530  Setup: !
540  Blank$="
      "
550  GOSUB Read_common
560  GOSUB Clearscreen
570  GOSUB Test_info
580  PRINT TABXY(1,18);"ENTER INDEX OF INFORMATION TO BE CHANGED"
590  INPUT "(1=TEST PARAMETERS  2=SPECIMEN DATA  0=EXIT)",N

```

```

600     SELECT N
610     CASE 1
620         PRINT TABXY(1,18);Blank$
630         INPUT "ENTER INDEX FOR TYPE OF TEST (1=OXIDATION 2=CORROSION)",I
640         IF I=1 THEN Title$="OXIDATION"
650         IF I=2 THEN Title$="CORROSION"
660         INPUT "ENTER INDEX FOR FUEL TYPE (1=JET A 2=DIESEL)",I
670         IF I=1 THEN Fuel$="JET A "
680         IF I=2 THEN Fuel$="DIESEL"
690         INPUT "ENTER TARGET TEMP IN DEG F",Target_temp
700         LINPUT "ENTER TEST DURATION (xxHRS,xxMIN)",Target_time$
710         LINPUT "ENTER TIME ELAPSED (xxHRS,xxMIN)",Elap_time$
720         GOTO 560
730     CASE 2
740         PRINT TABXY(1,18);Blank$
750         INPUT "ENTER POSITION NO. OF SPECIMEN TO BE CHANGED",I
760         GOSUB Spec_change
770         GOTO 560
780     CASE 0
790         GOSUB Write_common
800         GOTO Main_menu_keys
810     CASE ELSE
820         BEEP
830         GOTO 580
840     END SELECT
850 Spec_change: !
860     LINPUT "ENTER 8 CHARACTER PART NO. OR -1=NO CHANGE -2=EMPTY",Ans$
870     IF Ans$="-2" THEN
880         Specimen$(I)="EMPTY"
890         Install$(I)=" "
900         Tot_time$(I)="0 HRS,0 MIN"
910         GOTO 1050
920     END IF
930     IF Ans$="-1" THEN
940         GOTO 980
950     ELSE
960         Specimen$(I)=Ans$
970     END IF
980     LINPUT "ENTER DATE INSTALLED (DD MMM YYYY) OR -1=NO CHANGE",Ans$
990     IF Ans$="-1" THEN
1000         GOTO 1040
1010     ELSE
1020         Install$(I)=Ans$
1030     END IF
1040     LINPUT "ENTER TEST TIME TO DATE (xxHRS,xxMIN)",Tot_time$(I)
1050     RETURN
1060 Test_info: !
1070     PRINT "SPL HOT CORROSION TEST FACILITY - CURRENT TEST SETUP"
1080     PRINT
1090     PRINT "TEST TYPE: "&Title$
1100     PRINT "FUEL TYPE: "&Fuel$
1110     PRINT "TARGET TEMP IN DEG F: "&VAL$(Target_temp)
1120     PRINT "CURRENT TEST TIME REQUEST: "&Target_time$
1130     PRINT "                TIME ELAPSED: "&Elap_time$
1140     PRINT
1150     PRINT
1160     PRINT "                POSITION #1                POSITION #2                POSITION #3
1170     PRINT "                POSITION #4"
1180     PRINT USING 1210;"SPEC NAME: ",Specimen$(1),Specimen$(2),Specimen$(3),Spe

```



```

cimen$(4)
1190 PRINT USING 1220;"INSTALLED: ",Install$(1),Install$(2),Install$(3),Instal
1$(4)
1200 PRINT USING 1220;"TEST TIME: ",Tot_time$(1),Tot_time$(2),Tot_time$(3),Tot
_time$(4)
1210 IMAGE 11A,4X,8A,10X,11A,7X,11A,7X,11A
1220 IMAGE 11A,4X,11A,7X,11A,7X,11A,7X,11A
1230 RETURN
1240 !!!!!!!!!!!!!!!!!!!!!!! MAIN SUBPROGRAM !!!!!!!!!!!!!!!!!!!!!!!
1250 Main: !
1260 CLEAR 705
1270 GOSUB Read_coef
1280 GOSUB Read_label_lim
1290 GOSUB Read_common
1300 GOSUB Read_pid_val
1310 GOSUB Screen_setup
1320 GOSUB Build_string
1330 RESTORE 1370
1340 FOR I=1 TO 12
1350 READ Print_order(I)
1360 NEXT I
1370 DATA 24,23,31,32,25,26,2,8,6,7,11,29
1380 Reset: !
1390 LINPUT "ENTER TODAY'S DATE AND TIME (DD MMM YYYY HH:MM:SS)",Ans$
1400 SET TIMEDATE DATE(Ans$[1,11])+TIME(Ans$[13,20])
1410 PRINTER IS 701
1420 PRINT CHR$(12)
1430 Nlines=0
1440 GOSUB Print_header_1
1450 PRINTER IS 1
1460 Init_variables: !
1470 Target_minutes=VAL(Target_time$[1,2])*60+VAL(Target_time$[7,8])-VAL(Elap_
time$[1,2])*60-VAL(Elap_time$[7,8])
1480 Prt_int=300
1490 Fuel_sp=0.
1500 Quench_sp=50.
1510 Air_sp=50.
1520 Back_sp=50.
1530 GOSUB Air_out
1540 GOSUB Back_out
1550 GOSUB Quench_out
1560 Spec_temp_sp=-999.
1570 Air_flow_sp=-99.9
1580 Quench_temp_sp=200.
1590 Back_psi_sp=-99.9
1600 Fuel_control$="OPEN"
1610 Air_control$="OPEN"
1620 Back_control$="OPEN"
1630 Blank$="
"
1640 Hours=0
1650 Minutes=0
1660 Tot_hours=0
1670 Tot_minutes=0
1680 Hot_ind=2
1690 Ignite_ind=2
1700 Out_lim_ind=0
1710 Trun=0.
1720 Run_time$="0 HRS,0 MIN"
1730 Nlines_page=60

```

```

1740 Fuel_gal=0.
1750 MAT Volt= (0.)
1760 MAT Dval= (0.)
1770 Soft keys: !
1780 GOSUB Clearscreen
1790 ON KEY 0 LABEL " SHUT_DOWN ",10 GOTO Shutdown
1800 ON KEY 1 LABEL " START_FUEL ",10 GOSUB Start_fuel
1810 ON KEY 2 LABEL " % AIR VALVE",10 GOTO Air_out_sp
1820 ON KEY 3 LABEL " % BACK VALVE",10 GOTO Back_out_sp
1830 ON KEY 4 LABEL " % H2O VALVE",10 GOTO Quench_out_sp
1840 ON KEY 5 LABEL "SET INTERVALS",10 GOTO Set_prt_int
1850 ON KEY 6 LABEL " ",10 GOSUB Invalid
1860 ON KEY 7 LABEL " SET PID ",10 GOTO Pid_parm
1870 ON KEY 8 LABEL " SET CONTROL ",10 GOTO Control_setup
1880 ON KEY 9 LABEL " PRINT DUMP ",10 GOSUB Print_data
1890 Init_scanner: !
1900 OUTPUT 705;"AFOAL29AC0VT4VN30VA0VS1VD5SD0AE1"
1910 OUTPUT 705;"VT3"
1920 Tp=TIMEDATE
1930 Ts=TIMEDATE
1940 !!!!!!!!!!!!!!!!!!!!!!! MAIN PROGRAM LOOP !!!!!!!!!!!!!!!!!!!!!!!
1950 Scan: !
1960 Prev_ts=Ts
1970 Ts=TIMEDATE
1980 OUTPUT 705;"VS"
1990 SYSTEM PRIORITY 15
2000 FOR I=1 TO 30
2010 ENTER 705 USING "#,K";Volt(I)
2020 NEXT I
2030 SYSTEM PRIORITY 9
2040 OUTPUT 705;"VT3"
2050 GOSUB Convert
2060 GOSUB Calculate
2070 GOSUB Check
2080 GOSUB Control
2090 GOSUB Status
2100 GOSUB Display
2110 IF Prt_int=-3 THEN GOTO 2160
2120 IF Ts-Tp>Prt_int THEN
2130 Tp=Ts
2140 GOSUB Print_data
2150 END IF
2160 GOSUB Fuel_count
2170 GOTO Scan
2180 !!!!!!!!!!!!!!!!!!!!!!! PRIMARY SUBROUTINES !!!!!!!!!!!!!!!!!!!!!!!
2190 Convert: !
2200! HP 3497 ANALOG INPUT CHANNELS/SLOT #0
2210 Vref=Volt(20)
2220 FOR I=1 TO 4 ! CHAN A0-A3
2230 GOSUB Type_k
2240 NEXT I
2250 FOR I=5 TO 8 ! CHAN A4-A7
2260 GOSUB Type_r
2270 NEXT I
2280 I=11 ! CHAN B0
2290 GOSUB Type_k
2300! HP 3497 ANALOG INPUT CHANNELS/SLOT #1
2310 Dval(21)=6.689*Volt(21)*1000-.428 ! CHAN A0 - VENTURI PSI
2320 Dval(22)=.318*Volt(22)*1000-.010 ! CHAN A1 - VENTURI DP
2330 ! CHAN A2 - FUEL FLOW

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2340   Dval(23)=Volt(23)*160                                ! DC to Hz (800 HZ)
2350   ! IF Dval(23)<10 THEN ! MUST ZERO CALCULATED VALUE TO Y-INTERCEPT
2360   !       Dval(23)=0.
2370   !       GOTO 2400
2380   !   END IF
2390   Dval(23)=(9.13E-9*Dval(23)^2+4.41E-5*Dval(23)+.0090356)*60    ! Hz to GPH
2400   Dval(24)=16.378*Volt(24)*1000-4.569                        ! CHAN A3 - FUEL PRESS
2410   Dval(25)=(3.614*Volt(25)*1000-.148)+14.7                  ! CHAN A4 - COMB PRESS
2420   Dval(26)=(4.007*Volt(26)*1000+.008)+14.7                  ! CHAN A5 - TEST PRESS
2430   Dval(27)=7.975*Volt(27)*1000-1.412                        ! CHAN A6 - H2O PRESS
2440                                           ! CHAN A7 - H2O FLOW
2450   Dval(28)=Volt(28)*320                                      ! DC to Hz (1600 HZ)
2460   Dval(28)=.000517*Dval(28)+.003                            ! Hz to GPM
2470   Dval(29)=Volt(29)                                          ! CHAN A8 - LOAD CELL
2480   RETURN
2490   Type k: !
2500   Volt_comp=K(1)+Vref*(K(2)+Vref*K(3))
2510   Vt=Volt_comp+Volt(I)
2520   Temp=K(8)+Vt*(K(9)+Vt*(K(10)+Vt*(K(11)+Vt*(K(12)+Vt*(K(13))))))
2530   Temp=K(4)+Vt*(K(5)+Vt*(K(6)+Vt*(K(7)+Vt*Temp)))
2540   Dval(I)=Temp*1.8+32
2550   RETURN
2560   Type r: !
2570   Volt_comp=R(1)+Vref*(R(2)+Vref*R(3))
2580   Vt=Volt_comp+Volt(I)
2590   Vt=Vt*1.E+6
2600   Temp=R(8)+Vt*(R(9)+Vt*(R(10)+Vt*(R(11)+Vt*(R(12)+Vt*(R(13))))))
2610   Temp=R(4)+Vt*(R(5)+Vt*(R(6)+Vt*(R(7)+Vt*Temp)))
2620   Dval(I)=Temp*1.8+32
2630   RETURN
2640   Check: !
2650   FOR Z=1 TO 11
2660       IF Dval(Z)<0. THEN Dval(Z)=0.
2670       IF Dval(Z)>9999. THEN Dval(Z)=9999.
2680   NEXT Z
2690   FOR Z=21 TO 32
2700       IF Dval(Z)<0. THEN Dval(Z)=0.
2710       SELECT Display_format$(Z)
2720       CASE "DDD.D"
2730           IF Dval(Z)>999.9 THEN Dval(Z)=999.9
2740       CASE "DD.DD"
2750           IF Dval(Z)>99.99 THEN Dval(Z)=99.99
2760       CASE "D.DDD"
2770           IF Dval(Z)>9.999 THEN Dval(Z)=9.999
2780       END SELECT
2790   NEXT Z
2800   RETURN
2810   Limits: !
2820   IF Dval(J)<Low_lim(J) OR Dval(J)>Hi_lim(J) THEN
2830       GOSUB Print_data
2840       PRINTER IS 701
2850       X=2
2860       GOSUB Turn_page
2870       PRINT USING "8A,2X,14A,34A";TIME$(TIMEDATE),Chan_label$(J)," DATA HAS E
XCEEDED A HI/LOW LIMIT!"
2880       PRINT
2890       Nlines=Nlines+2
2900       PRINTER IS 1
2910       Out_lim_ind=Out_lim_ind+1
2920       IF Out_lim_ind>4 THEN

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2930     PRINTER IS 701
2940     X=3
2950     GOSUB Turn_page
2960     PRINT USING "8A,2X,21A";TIME$(TIMEDATE),"5 CLOSED LOOP ERRORS!"
2970     GOSUB End_sequence
2980     GOTO Restart
2990     ELSE
3000     GOTO Restart
3010     END IF
3020     END IF
3030     RETURN
3040 Calculate: !
3050 ! COMB AIR MASS FLOW RATE
3060 C=1-(Dval(22)/(Dval(21)+14.7))
3070 Tair=Dval(1)+459.7
3080 Mu=32.1741*(2.270E-8*(Tair^1.5/(Tair+198.6)))
3090 Roe=144*Dval(21)/(53.35*Tair)
3100 IF C=1 OR Mu=0. OR Roe<0. OR Dval(22)<0. THEN
3110     Dval(31)=0.
3120     GOTO 3230
3130     END IF
3140 F=(C^1.42857*3.5*((1-C^.28571)/(1-C))*(.79241/(1-.20759*C^1.42857)))^.5
3150 Wair_cf=.52502*F*.675^2*(Roe*Dval(22))^.5
3160 Re_cf=(48*Wair_cf/(3.14*.675*Mu))/100000
3170 IF Re_cf>1.73 THEN
3180     Cf=1.07594+.0021752*Re_cf
3190     ELSE
3200     Cf=1.12381-.05719*Re_cf+.017205*Re_cf^2
3210     END IF
3220 Dval(31)=3600*Cf*Wair_cf
3230 ! FUEL/AIR RATIO
3240 IF Dval(31)=0. THEN
3250     Dval(32)=0.
3260     ELSE
3270     Dval(32)=Dval(23)*6.74/Dval(31)
3280     END IF
3290 ! SETPOINTS
3300 Dval(33)=Air_flow_sp
3310 Dval(34)=Spec_temp_sp
3320 Dval(35)=Back_psi_sp
3330 Dval(36)=Quench_temp_sp
3340 Dval(37)=Air_sp
3350 Dval(38)=Fuel_sp
3360 Dval(39)=Back_sp
3370 Dval(40)=Quench_sp
3380     RETURN
3390 Fuel_count: !
3400 IF Ignite_ind=0 THEN GOTO 3440
3410 IF Dval(23)<0 THEN Dval(23)=0.
3420 IF Dval(23)>Hi_lim(23) THEN Dval(23)=0.
3430 Fuel_gal=Fuel_gal+Dval(23)*(Ts-Prev_ts)/3600
3440     RETURN
3450 Status: !
3460 IF Dval(6)>Target_temp-50. AND Ignite_ind=1 THEN
3470     SELECT Hot_ind
3480     CASE 0
3490         Hot_ind=1
3500         Trun_start=TIMEDATE
3510         GOSUB Print_data
3520     CASE 1

```

```

3530      Trun=Trun+(TIMEDATE-Trun_start)
3540      Trun_start=TIMEDATE
3550      Minutes=Trun DIV 60
3560      Hours=Minutes DIV 60
3570      Minutes=Minutes MOD 60
3580      Run_time$[1,2]=VAL$(Hours)
3590      Run_time$[7,8]=VAL$(Minutes)
3600      IF Trun DIV 60=Target_minutes THEN
3610          PRINTER IS 701
3620          X=3
3630          GOSUB Turn_page
3640          PRINT USING "8A,2X,15A";TIME$(TIMEDATE),"TEST COMPLETED!"
3650          GOSUB End_sequence
3660      END IF
3670      CASE 2
3680          PRINTER IS 701
3690          X=3
3700          GOSUB Turn_page
3710          PRINT USING "8A,2X,14A";TIME$(TIMEDATE),"STATUS ERRORS!"
3720          GOSUB End_sequence
3730      END SELECT
3740  ELSE
3750      IF Dval(8)>500 THEN
3760          SELECT Ignite_ind
3770          CASE 0
3780              Ignite_ind=1
3790              Hot_ind=0
3800              Quench_sp=95.
3810              GOSUB Quench_out
3820              PRINTER IS 701
3830              X=3
3840              GOSUB Turn_page
3850              PRINT USING "8A,2X,21A";TIME$(TIMEDATE),"RIG HAS BEEN IGNITED!"
3860              PRINT USING "10X,31A";"NEW H2O VALVE SETPOINT IS 95 %."
3870              PRINT
3880              Nlines=Nlines+3
3890              GOSUB Print_data
3900              PRINTER IS 1
3910          CASE 1
3920              IF Hot_ind=1 THEN
3930                  Hot_ind=0
3940                  GOSUB Print_data
3950              END IF
3960          CASE ELSE
3970              GOTO 4110
3980          END SELECT
3990      ELSE
4000          IF Ignite_ind=1 THEN
4010              PRINTER IS 701
4020              X=3
4030              GOSUB Turn_page
4040              PRINT USING "8A,2X,18A";TIME$(TIMEDATE),"FLAMEOUT DETECTED!"
4050              GOSUB End_sequence
4060          ELSE
4070              GOTO 4110
4080          END IF
4090      END IF
4100  END IF
4110  RETURN
4120 Display:  !

```

```

4130 GOSUB Build_string
4140 PRINT TABXY(26,1);"SPL HOT CORROSION TEST FACILITY"
4150 PRINT TABXY(1,2);Blank$
4160 PRINT " ***** RIG PARAMETERS *****"
4170 FOR I=1 TO 8
4180 PRINT Disp$(I)
4190 NEXT I
4200 PRINT TABXY(1,12);Blank$
4210 PRINT " ***** CONTROL SECTION *****"
4220 FOR I=9 TO 12
4230 PRINT Disp$(I)
4240 NEXT I
4250 PRINT TABXY(1,18);Blank$
4260 DISP USING "8A,5X,6A,DD.DD";TIME$(TIMEDATE),"CYCLE=",Ts-Prev_ts
4270 OUTPUT 705;"AO4,0,"&VAL$(INT(Dval(32)*2000))
4280 RETURN
4290 !!!!!!!!!!!!!!!!!!!!!!! CLOSED LOOP CONTROL !!!!!!!!!!!!!!!!!!!!!!!
4300 Control: !
4310 IF Fuel_control$="TEMP" THEN
4320 J=6
4330 GOSUB Limits
4340 GOSUB Control_loop
4350 GOSUB Fuel_out
4360 END IF
4370 IF Air_control$="FLOW" THEN
4380 J=31
4390 GOSUB Limits
4400 GOSUB Control_loop
4410 GOSUB Air_out
4420 END IF
4430 IF Back_control$="PRESS" THEN
4440 J=26
4450 GOSUB Limits
4460 GOSUB Control_loop
4470 GOSUB Back_out
4480 END IF
4490 RETURN
4500 Control loop: !
4510 SELECT J
4520 CASE 6 ! SPEC TEMP
4530 Err=Dval(34)-Dval(6)
4540 Pid=1
4550 Sp_fraction=Fuel_sp/100
4560 GOSUB Pid
4570 IF Out<Low_lim(38)/100. THEN
4580 Out=Low_lim(38)/100.
4590 END IF
4600 Fuel_sp=Out*100
4610 IF Fuel_sp>Hi_lim(38) THEN Fuel_sp=Hi_lim(38)
4620 CASE 31 ! AIR MASS FLOW
4630 Err=Dval(33)-Dval(31)
4640 Pid=2
4650 Sp_fraction=Air_sp/100
4660 GOSUB Pid
4670 IF Out<Low_lim(37)/100. THEN
4680 Out=Low_lim(37)/100.
4690 END IF
4700 Air_sp=Out*100
4710 IF Air_sp>Hi_lim(37) THEN Air_sp=Hi_lim(37)
4720 CASE 26 ! TEST PRESS

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4730     Err=Dval(35)-Dval(26)
4740     Pid=3
4750     Sp_fraction=Back_sp/100
4760     GOSUB Pid
4770     Out=Sp_fraction+(Sp_fraction-Out)
4780     IF Out<Low_lim(39)/100 THEN
4790         Out=Low_lim(39)/100
4800     END IF
4810     Back_sp=Out*100
4820     IF Back_sp>Hi_lim(39) THEN Back_sp=Hi_lim(39)
4830 END SELECT
4840 RETURN
4850 Pid: !
4860 IF Err<=-P(3,Pid) THEN
4870     Prop=(Err+P(3,Pid))*P(4,Pid)-P(3,Pid)*P(2,Pid)
4880 ELSE
4890     IF Err<P(3,Pid) THEN
4900         Prop=Err*P(2,Pid)
4910     ELSE
4920         Prop=(Err-P(3,Pid))*P(5,Pid)+P(3,Pid)*P(2,Pid)
4930     END IF
4940 END IF
4950 Amt(Pid)=Sp_fraction+Prop*(Ts-Prev_ts)*P(7,Pid)
4960 IF Amt(Pid)>P(1,Pid) THEN Amt(Pid)=P(1,Pid)
4970 IF Amt(Pid)<-P(1,Pid) THEN Amt(Pid)=-P(1,Pid)
4980 Out=Prop+Amt(Pid)+((Prop-P_prop(Pid))/(Ts-Prev_ts))*P(6,Pid)
4990 IF Out>1 THEN Out=1.
5000 P_prop(Pid)=Prop
5010 RETURN
5020 !!!!!!!!!!!!!!!!!!!!!!!!!!!!! P.I.D. VALUES !!!!!!!!!!!!!!!!!!!!!!!!!!!!!
5030 Pid_parm: !
5040 GOSUB Clearscreen
5050 PRINT
5060 PRINT
5070 PRINT "CURRENT CLOSED LOOP PARAMETERS"
5080 PRINT
5090 PRINT "1. SPECIMEN TEMP CONTROL OF FUEL VALVE"
5100 PRINT "2. MASS AIR FLOW CONTROL OF AIR VALVE"
5110 PRINT "3. SYSTEM PRESS CONTROL OF BACK PSI VALVE"
5120 INPUT "ENTER INDEX OF PARAMETER (0 TO QUIT)",Index
5130 IF Index=0 THEN GOTO Restart
5140 SELECT Index
5150 CASE 1 ! SPECIMEN TEMP
5160     Pid_ind=1
5170     GOSUB Pid_val_input
5180 CASE 2 ! AIR FLOW
5190     Pid_ind=2
5200     GOSUB Pid_val_input
5210 CASE 3 ! SYSTEM PRESS
5220     Pid_ind=3
5230     GOSUB Pid_val_input
5240 END SELECT
5250 GOTO Restart
5260 Pid_val_input: !
5270 GOSUB Clearscreen
5280 PRINT
5290 PRINT
5300 SELECT Pid_ind
5310 CASE 1
5320     PRINT TABXY(3,1);"SPECIMEN TEMPERATURE ";

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5330 CASE 2
5340 PRINT TABXY(3,1);"MASS AIR FLOW ";
5350 CASE 3
5360 PRINT TABXY(3,1);"SYSTEM PRESSURE ";
5370 END SELECT
5380 PRINT "CONTROL LOOP PARAMETERS"
5390 PRINT
5400 PRINT "1) RESET LIMIT=";P(1,Pid_ind)
5410 PRINT "2) MID-BAND GAIN=";P(2,Pid_ind)
5420 PRINT "3) 1/2 MID-BAND WIDTH=";P(3,Pid_ind)
5430 PRINT "4) LOW BAND GAIN=";P(4,Pid_ind)
5440 PRINT "5) HI BAND GAIN=";P(5,Pid_ind)
5450 PRINT "6) RATE CONSTANT=";P(6,Pid_ind)
5460 PRINT "7) RESET CONSTANT=";P(7,Pid_ind)
5470 PRINT
5480 PRINT TABXY(1,18);"ENTER INDEX OF PARAMETER TO BE CHANGED"
5490 INPUT "(0 TO QUIT, OR -1 TO RECALL LAST STORED SET)",Index
5500 IF Index>0 THEN
5510 INPUT "ENTER NEW VALUE",P(Index,Pid_ind)
5520 GOTO Pid_val_input
5530 END IF
5540 IF Index=-1 THEN
5550 GOSUB Read_pid_val
5560 GOTO Pid_val_input
5570 ELSE
5580 PRINT TABXY(1,18);Blank$
5590 END IF
5600 GOSUB Write_pid_val
5610 RETURN
5620 !!!!!!!!!!!!!!!!!!!!!!!!!!!!! PRINT SECTION !!!!!!!!!!!!!!!!!!!!!!!!!!!!!
5630 Print_header_2: !
5640 PRINT USING "#,9X"
5650 FOR Z=1 TO 12
5660 PRINT USING "#,X,DD,XXX";Z
5670 NEXT Z
5680 PRINT
5690 PRINT USING "#,2X,4A,2X";"TIME"
5700 FOR Z=1 TO 12
5710 PRINT USING "#,X,5A";Sensor$(Print_order(Z))
5720 NEXT Z
5730 PRINT
5740 PRINT USING "#,9X"
5750 FOR Z=1 TO 12
5760 PRINT USING "#,5A,X";Unit$(Print_order(Z))
5770 NEXT Z
5780 PRINT
5790 PRINT
5800 Nlines=Nlines+4
5810 RETURN
5820 Print_header_1: !
5830 PRINT DATE$(TIMEDATE)
5840 PRINT
5850 GOSUB Test_info
5860 PRINT
5870 PRINT
5880 PRINT "* THESE ARE THE PARAMETERS TO BE PRINTED OUT"
5890 FOR I=1 TO 12
5900 PRINT USING "5X,2D,A,2X,16A";I,".",Chan_label$(Print_order(I))
5910 NEXT I
5920 PRINT

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5930 Nlines=Nlines+32
5940 GOSUB Print_header_2
5950 RETURN
5960 Print_data: !
5970 PRINTER IS 701
5980 GOSUB Check
5990 X=2
6000 GOSUB Turn_page
6010 PRINT USING "8A,X,#";TIME$(TIMEDATE)
6020 FOR Z=1 TO 12
6030 PRINT USING Display_format$(Print_order(Z))&","X,#";Dval(Print_order(Z))
6040 NEXT Z
6050 PRINT
6060 PRINT
6070 Nlines=Nlines+2
6080 PRINTER IS 1
6090 RETURN
6100 Turn_page: !
6110 IF Nlines+X>Nlines_page THEN
6120 PRINT CHR$(12)
6130 Nlines=0
6140 GOSUB Print_header_2
6150 END IF
6160 RETURN
6170 !!!!!!!!!!!!!!!!!!!!!!!!!!!!! SETPOINT SECTION !!!!!!!!!!!!!!!!!!!!!!!!!!!!!
6180 Cooldown: !
6190 Ignite_ind=2 ! RIG CANNOT RE-IGNITE THUS ELIMINATING ERRONEOUS MESSAGES
6200 Hot_ind=2 ! DUE TO TC DRIFT
6210 Prt_int=-3
6220 Quench_sp=50.
6230 GOSUB Quench_out
6240 Fuel_control$="OPEN"
6250 Spec_temp_sp=-999.
6260 Fuel_sp=0.
6270 GOSUB Fuel_out
6280 ON KEY 1 LABEL " RIG RESTART ",10 GOTO Rig_restart
6290 Back_control$="OPEN"
6300 Back_psi_sp=-99.9
6310 Back_sp=50.
6320 GOSUB Back_out
6330 ON KEY 3 LABEL " % BACK VALVE",10 GOTO Back_out_sp
6340 Air_control$="OPEN"
6350 Air_flow_sp=-99.9
6360 Air_sp=60.
6370 GOSUB Air_out
6380 ON KEY 2 LABEL " % AIR VALVE",10 GOTO Air_out_sp
6390 ON KEY 0 LABEL " PROGRAM END ",10 GOTO Pgm_stop
6400 PRINTER IS 701
6410 X=5
6420 GOSUB Turn_page
6430 PRINT USING "10X,25A,3D.D,23A";"NEW AIR VALVE SETPOINT IS",Air_sp,"% IN O
PEN LOOP CONTROL!"
6440 PRINT USING "10X,26A,3D.D,23A";"NEW FUEL VALVE SETPOINT IS",Fuel_sp,"% IN
OPEN LOOP CONTROL!"
6450 PRINT USING "10X,27A,3D.D,23A";"NEW BACK VALVE SETPOINT IS ",Back_sp,"% I
N OPEN LOOP CONTROL!"
6460 PRINT USING "10X,25A,3D.D,23A";"NEW H2O VALVE SETPOINT IS",Quench_sp,"% I
N OPEN LOOP CONTROL!"
6470 PRINT
6480 Nlines=Nlines+5

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```

6490  PRINTER IS 1
6500  RETURN
6510  Quench_out_sp:  !
6520  PRINT TABXY(1,18);Blank$
6530  PRINT TABXY(1,18);"PRESENT %OUTPUT OF H2O VALVE IS ";DROUND(Quench_sp,4);
"%."
6540  INPUT "ENTER NEW %OUTPUT OF H2O VALVE",Quench_sp
6550  Setpoint=Quench_sp
6560  J=40
6570  GOSUB Confirm_sp
6580  GOSUB Quench_out
6590  PRINT USING "8A,2X,25A,3D.D,23A";TIME$(TIMEDATE),"NEW H2O VALVE SETPOINT
IS",Quench_sp,"% IN OPEN LOOP CONTROL!"
6600  PRINT
6610  PRINTER IS 1
6620  GOTO Restart
6630  Quench_out:  !
6640  Quenchout=INT(Quench_sp*100)
6650  OUTPUT 705;"AO3,1,"&VAL$(Quenchout)
6660  RETURN
6670  Air_out_sp:  !
6680  PRINT TABXY(1,18);Blank$
6690  PRINT TABXY(1,18);"PRESENT %OUTPUT OF AIR VALVE IS ";DROUND(Air_sp,4);"%."
"
6700  INPUT "ENTER NEW %OUTPUT OF AIR VALVE",Air_sp
6710  Setpoint=Air_sp
6720  J=37
6730  GOSUB Confirm_sp
6740  Air_control$="OPEN"
6750  Air_flow_sp=-99.9
6760  GOSUB Air_out
6770  PRINT USING "8A,2X,25A,3D.D,23A";TIME$(TIMEDATE),"NEW AIR VALVE SETPOINT
IS",Air_sp,"% IN OPEN LOOP CONTROL!"
6780  PRINT
6790  PRINTER IS 1
6800  GOTO Restart
6810  Air_flow_sp:  !
6820  PRINT TABXY(1,18);Blank$
6830  PRINT TABXY(1,18);"PRESENT AIR FLOW SETPOINT IS ";Air_flow_sp;" LBM/HR."
6840  INPUT "ENTER NEW AIR FLOW SETPOINT VALUE",Air_flow_sp
6850  Setpoint=Air_flow_sp
6860  J=33
6870  GOSUB Confirm_sp
6880  Air_control$="FLOW"
6890  PRINT USING "8A,2X,25A,3D.D,31A";TIME$(TIMEDATE),"NEW AIR FLOW SETPOINT I
S ",Air_flow_sp," LBM/HR IN CLOSED LOOP CONTROL!"
6900  PRINT
6910  PRINTER IS 1
6920  GOTO Restart
6930  Air_out:  !
6940  Airout=INT(Air_sp*100)
6950  OUTPUT 705;"AO2,0,"&VAL$(Airout)
6960  RETURN
6970  Back_out_sp:  !
6980  PRINT TABXY(1,18);Blank$
6990  PRINT TABXY(1,18);"PRESENT %OUTPUT OF BACK PSI VALVE IS ";DROUND(Back_sp,
4);"%."
7000  INPUT "ENTER NEW %OUTPUT OF BACK PSI VALVE",Back_sp
7010  Setpoint=Back_sp
7020  J=39

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7030  GOSUB Confirm_sp
7040  Back_control$="OPEN"
7050  Back_psi_sp=-99.9
7060  GOSUB Back_out
7070  PRINT USING "8A,2X,30A,3D.D,23A";TIME$(TIMEDATE),"NEW BACK PSI VALVE SETP
OINT IS",Back_sp,"% IN OPEN LOOP CONTROL!"
7080  PRINT
7090  PRINTER IS 1
7100  GOTO Restart
7110  Back_psi_sp: !
7120  PRINT TABXY(1,18);Blank$
7130  PRINT TABXY(1,18);"PRESENT SYSTEM PRESS SETPOINT IS ";Back_psi_sp;" PSIA.
"
7140  INPUT "ENTER NEW SYSTEM PRESS SETPOINT VALUE",Back_psi_sp
7150  Setpoint=Back_psi_sp
7160  J=35
7170  GOSUB Confirm_sp
7180  Back_control$="PRESS"
7190  PRINT USING "8A,2X,29A,3D.D,29A";TIME$(TIMEDATE),"NEW SYSTEM PRESS SETPOI
NT IS ",Back_psi_sp," PSIA IN CLOSED LOOP CONTROL!"
7200  PRINT
7210  PRINTER IS 1
7220  GOTO Restart
7230  Back_out: !
7240  Backout=INT((100-Back_sp)*100)          ! NORMALLY OPEN (20mA FOR 0%=CLOSE)
7250  OUTPUT 705;"AO3,0,"&VAL$(Backout)
7260  RETURN
7270  Start_fuel: !
7280  Ignite_ind=0
7290  Fuel_sp=15.
7300  GOSUB Fuel_out
7310  ON KEY 1 LABEL " % FUEL VALVE",10 GOTO Fuel_out_sp
7320  PRINTER IS 701
7330  X=3
7340  GOSUB Turn_page
7350  PRINT USING "8A,2X,54A";TIME$(TIMEDATE),"RIG IS READY FOR IGNITION. CURRE
NT VALVE SETTINGS ARE:"
7360  PRINT USING 7370;"AIR=",Air_sp,"%","FUEL=",Fuel_sp,"%","BACK=",Back_sp,"%
","H2O=",Quench_sp,"%"
7370  IMAGE 10X,4A,3D.D,A,5X,5A,3D.D,A,5X,5A,3D.D,A,5X,4A,3D.D,A
7380  PRINT
7390  Nlines=Nlines+3
7400  GOSUB Print_data
7410  PRINTER IS 1
7420  RETURN
7430  Fuel_out_sp: !
7440  PRINT TABXY(1,18);Blank$
7450  PRINT TABXY(1,18);"PRESENT %OUTPUT OF FUEL VALVE IS ";DROUND(Fuel_sp,4);"
%."
7460  INPUT "ENTER NEW %OUTPUT OF FUEL VALVE",Fuel_sp
7470  Setpoint=Fuel_sp
7480  J=38
7490  GOSUB Confirm_sp
7500  Fuel_control$="OPEN"
7510  Spec_temp_sp=-999.
7520  GOSUB Fuel_out
7530  PRINT USING "8A,2X,26A,3D.D,23A";TIME$(TIMEDATE),"NEW FUEL VALVE SETPOINT
IS",Fuel_sp,"% IN OPEN LOOP CONTROL!"
7540  PRINT
7550  PRINTER IS 1

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7560 GOTO Restart
7570 Spec_temp_sp: !
7580 PRINT TABXY(1,18);Blank$
7590 PRINT TABXY(1,18);"PRESENT SPEC. TEMP SETPOINT IS ";Spec_temp_sp;" DEG F.
"
7600 INPUT "ENTER NEW SPEC. TEMP SETPOINT VALUE",Spec_temp_sp
7610 Setpoint=Spec_temp_sp
7620 J=34
7630 GOSUB Confirm_sp
7640 Fuel_control$="TEMP"
7650 PRINT USING "8A,2X,27A,4D,26A";TIME$(TIMEDATE),"NEW FLAME TEMP SETPOINT I
S ",Spec_temp_sp," F IN CLOSED LOOP CONTROL!"
7660 PRINT
7670 PRINTER IS 1
7680 GOTO Restart
7690 Fuel_out: !
7700 Fuelout=INT(Fuel_sp*100)
7710 OUTPUT 705;"AO2,1,"&VAL$(Fuelout)
7720 RETURN
7730 Confirm_sp: !
7740 IF Setpoint>Hi_lim(J) THEN Setpoint=Hi_lim(J)
7750 IF Setpoint<Low_lim(J) THEN Setpoint=Low_lim(J)
7760 PRINT TABXY(1,18);Blank$
7770 PRINTER IS 701
7780 X=2
7790 GOSUB Turn_page
7800 Nlines=Nlines+2
7810 RETURN
7820 !!!!!!!!!!!!!!!!!!!!!!!!!!!!! MISC SUBROUTINES !!!!!!!!!!!!!!!!!!!!!!!!!!!!!
7830 Read_pid_val: !
7840 ASSIGN @Pid TO "PID_PARM"
7850 ENTER @Pid;P(*)
7860 ASSIGN @Pid TO *
7870 RETURN
7880 Write_pid_val: !
7890 ASSIGN @Pid TO "PID_PARM"
7900 OUTPUT @Pid;P(*)
7910 ASSIGN @Pid TO *
7920 RETURN
7930 Read_common: !
7940 ASSIGN @Path_1 TO "TEST_LOG"
7950 ENTER @Path_1;Title$,Fuel$,Target_temp,Target_time$,Elap_time$
7960 ENTER @Path_1;Specimen$(*),Install$(*),Tot_time$(*)
7970 ASSIGN @Path_1 TO *
7980 RETURN
7990 Write_common: !
8000 ASSIGN @Path_1 TO "TEST_LOG"
8010 OUTPUT @Path_1;Title$,Fuel$,Target_temp,Target_time$,Elap_time$
8020 OUTPUT @Path_1;Specimen$(*),Install$(*),Tot_time$(*)
8030 ASSIGN @Path_1 TO *
8040 RETURN
8050 Set_prt_int: !
8060 INPUT "ENTER NEW PRINT INTERVAL IN SECONDS (-1=15min, -2=30min, OR -3=OFF
)",Prt_int
8070 IF Prt_int=-1 THEN Prt_int=900
8080 IF Prt_int=-2 THEN Prt_int=1800
8090 GOTO Restart
8100 Spec_update: !
8110 FOR I=1 TO 4
8120 IF Specimen$(I)="EMPTY" THEN GOTO 8180

```

```

8130     Minutes=(VAL(Tot_time$(I)[1,2])+VAL(Run_time$[1,2]))*60+VAL(Tot_time$(I)
) [7,8])+VAL(Run_time$[7,8])
8140     Hours=Minutes DIV 60
8150     Minutes=Minutes MOD 60
8160     Tot_time$(I)[1,2]=VAL$(Hours)
8170     Tot_time$(I)[7,8]=VAL$(Minutes)
8180     NEXT I
8190     Minutes=(VAL(Elap_time$[1,2])+VAL(Run_time$[1,2]))*60+VAL(Elap_time$[7,8]
)+VAL(Run_time$[7,8])
8200     Hours=Minutes DIV 60
8210     Minutes=Minutes MOD 60
8220     Elap_time$[1,2]=VAL$(Hours)
8230     Elap_time$[7,8]=VAL$(Minutes)
8240     RETURN
8250 Summary: !
8260     PRINTER IS 701
8270     PRINT CHR$(12)
8280     PRINT
8290     PRINT
8300     PRINT "* * * * * RUN SUMMARY * * * * *"
* * * * *
8310     PRINT "                SPL HOT CORROSION TEST FACILITY"
8320     PRINT
8330     PRINT DATE$(TIMEDATE)
8340     PRINT "CURRENT TEST: "&Title$
8350     PRINT "FUEL TYPE: "&Fuel$
8360     PRINT "TARGET TEMP IN DEG F: "&VAL$(Target_temp)
8370     PRINT "TOTAL TIME REQUESTED: "&Target_time$
8380     PRINT "        TIME COMPLETED: "&Elap_time$
8390     PRINT
8400     PRINT USING "12A,11A";"TODAYS RUN: ",Run_time$
8410     PRINT USING "12A,3D.D,8A";"FUEL USAGE: ",Fuel_gal," GALLONS"
8420     PRINT
8430     PRINT "AS OF TODAYS RUN:"
8440     PRINT
8450     GOSUB 1160
8460     PRINT
8470     PRINT "COMMENTS:"
8480     PRINTER IS 1
8490     RETURN
8500     !!!!!!!!!!!!!!!!!!!!! VALVE CONTROL SETUP !!!!!!!!!!!!!!!!!!!!!
8510 Control_setup: !
8520     GOSUB Clearscreen
8530     PRINT
8540     PRINT "CURRENT VALVE CONTROL OPTIONS:"
8550     PRINT
8560     PRINT
8570     PRINT "1) FUEL- MANUAL CONTROL OF VALVE OUTPUT"
8580     PRINT "2) FUEL- CLOSED LOOP WITH SPECIMEN TEMP"
8590     PRINT
8600     PRINT "3) AIR- MANUAL CONTROL OF VALVE OUTPUT"
8610     PRINT "4) AIR- CLOSED LOOP WITH AIR FLOW RATE"
8620     PRINT
8630     PRINT "5) BACK PSI- MANUAL CNTRL OF VALVE OUTPUT"
8640     PRINT "6) BACK PSI- CLOSED LOOP W/ SYSTEM PRESS"
8650     PRINT
8660     PRINT "7) WATER- MANUAL CONTROL OF VALVE OUTPUT"
8670     PRINT "8) WATER- CLOSED LOOP WITH EXIT AIR TEMP"
8680     PRINT
8690     PRINT "ENTER (0) TO RETURN"

```

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8700 INPUT "ENTER YOUR CHOICE",Cntrl_ind
8710 SELECT Cntrl_ind
8720 CASE 0
8730 GOTO Restart
8740 CASE 1
8750 IF Ignite_ind=2 THEN
8760 BEEP
8770 DISP "FUEL CONTROL CURRENTLY NOT AVAILABLE"
8780 WAIT 1
8790 GOTO Control_setup
8800 END IF
8810 ON KEY 1 LABEL " % FUEL VALVE",10 GOTO Fuel_out_sp
8820 GOTO Fuel_out_sp
8830 CASE 2
8840 IF Ignite_ind=2 THEN
8850 BEEP
8860 DISP "FUEL CONTROL CURRENTLY NOT AVAILABLE"
8870 WAIT 1
8880 GOTO Control_setup
8890 END IF
8900 ON KEY 1 LABEL " SPEC_TEMP_SP",10 GOTO Spec_temp_sp
8910 GOTO Spec_temp_sp
8920 CASE 3
8930 ON KEY 2 LABEL " % AIR VALVE",10 GOTO Air_out_sp
8940 GOTO Air_out_sp
8950 CASE 4
8960 ON KEY 2 LABEL "AIR_FLOW_SP ",10 GOTO Air_flow_sp
8970 GOTO Air_flow_sp
8980 CASE 7
8990 GOTO Quench_out_sp
9000 CASE 8
9010 BEEP
9020 DISP "OPTION CURRENTLY NOT PROGRAMMED"
9030 WAIT 1
9040 GOTO Control_setup
9050 CASE 5
9060 ON KEY 3 LABEL " % BACK VALVE",10 GOTO Back_out_sp
9070 GOTO Back_out_sp
9080 CASE 6
9090 ON KEY 3 LABEL " SYS_PSI_SP ",10 GOTO Back_psi_sp
9100 GOTO Back_psi_sp
9110 CASE ELSE
9120 GOTO Control_setup
9130 END SELECT
9140 !!!!!!!!!!!!!!!!!!!!!!! SETUP STRINGS & ARRAYS !!!!!!!!!!!!!!!!!!!!!!!
9150 Build_string: !
9160 L$=" "
9170 FOR I=1 TO 12
9180 N=Screen(I,1)
9190 J=Screen(I,2)
9200 OUTPUT A$ USING Display_format$(N)&" ,#";Dval(N)
9210 OUTPUT B$ USING Display_format$(J)&" ,#";Dval(J)
9220 Disp$(I)=Chan_label$(N)[1,14]&L$[1,10]&A$[1,5]&L$[1,3]&Unit$(N)[1,5]&L$
[1,6]&Chan_label$(J)[1,14]&L$[1,10]&B$[1,5]&L$[1,3]&Unit$(J)[1,5]
9230 NEXT I
9240 RETURN
9250 Read_coef: !
9260 RESTORE 9300
9270 FOR I=1 TO 13
9280 READ K(I)

```

```

9290 NEXT I
9300 DATA -8.16774E-7,3.964E-4,1.6E-8
9310 DATA -5.1E-2,2.48503E4,-3.82662E5,9.9661057E7,-1.0820624E10
9320 DATA 6.0392855E11,-1.9109E13,3.4782347E14,-3.3991028E15,1.3828514E16
9330 FOR I=1 TO 13
9340 READ R(I)
9350 NEXT I
9360 DATA -2.11284E-7,5.334E-5,1.2E-8,4.8343651E1
9370 DATA 1.109827E-1,-2.435389E-6,4.5164488E-11,1.8172612E-16,0,0,0,0,0
9380 RETURN
9390 Read_label_lim: !
9400 RESTORE 9450
9410 FOR I=1 TO 40
9420 READ Chan_label$(I),Unit$(I),Display_format$(I),Sensor$(I)
9430 READ Hi_lim(I),Low_lim(I)
9440 NEXT I
9450 DATA "INLET AIR TEMP","DEG F","DDDD.,","AS112",500,0 ! SLOT #0
9460 DATA "PREHEATER-WEST","DEG F","DDDD.,","TP1 ",650,250
9470 DATA "EXIT TEMP ","DEG F","DDDD.,","TP130",400,0
9480 DATA "PREHEATER- API","DEG F","DDDD.,","K-4 ",650,250
9490 DATA "COMBUSTOR TEMP","DEG F","DDDD.,","TP136",2200,500 ! R
9500 DATA "SPEC. TEMP #1 ","DEG F","DDDD.,","TP100",2500,500 ! R
9510 DATA "SPEC. TEMP #2 ","DEG F","DDDD.,","TP2 ",2500,0 ! R
9520 DATA "COMB TEMP- API","DEG F","DDDD.,","R-4 ",2500,500 ! R
9530 DATA "SPARE TYPE R","DEG F","DDDD.,","R-5 ",3200,0 ! R
9540 DATA "SPARE TYPE R","DEG F","DDDD.,","R-6 ",3200,0 ! R
9550 DATA "EXIT TEMP- API","DEG F","DDDD.,","K-5 ",400,0
9560 DATA " ","","DDDD.,"," ",3200,0
9570 DATA " ","","DDDD.,"," ",3200,0
9580 DATA " ","","DDDD.,"," ",3200,0
9590 DATA " ","","DDDD.,"," ",3200,0
9600 DATA " ","","DDDD.,"," ",3200,0
9610 DATA " ","","DDDD.,"," ",3200,0
9620 DATA " ","","DDDD.,"," ",3200,0
9630 DATA " ","","DDDD.,"," ",3200,0
9640 DATA "TC REF. VOLT ","","DDDD.,"," REF ",3200,0
9650 DATA "INLET PRESSURE","PSIA ","DDD.D","AS114",200,0 ! SLOT #1
9660 DATA "VENTURI DP ","PSID ","DD.DD","AS116",5,0
9670 DATA "FUEL FLOW RATE","GPH ","DD.DD","FC105",6,.6
9680 DATA "FUEL PRESSURE","PSIG ","DDD.D","FC107",500,0
9690 DATA "COMB PRESSURE","PSIA ","DDD.D","TP137",120,0
9700 DATA "SYS. PRESSURE","PSIA ","DDD.D","TP104",120,0
9710 DATA "H2O PRESSURE","PSIG ","DDD.D","WD107",200,0
9720 DATA "H2O FLOW RATE","GPM ","DD.DD","WD112",.75,.02
9730 DATA "SALT LOAD CELL","VOLT ","D.DDD","SALT ",10,0
9740 DATA " ","","DDD.D"," ",100,0
9750 DATA "AIR FLOW RATE","LB/HR","DDD.D","Mair",800,50 ! CALCULATED
9760 DATA "F/A RATIO ","","D.DDD"," F/A ",.2,0
9770 DATA "AIR FLOW SP","LB/HR","DDD.D","SP #1",800,50
9780 DATA "SPEC. TEMP SP","DEG F","DDDD.,","SP #2",3000,100
9790 DATA "SYSTEM PSI SP","PSIA ","DDD.D","SP #3",120,0
9800 DATA "EXIT TEMP SP","DEG F","DDDD.,","SP #4",350,0
9810 DATA "% AIR VALVE "," " % ","DDD.D","AS111",100,0
9820 DATA "% FUEL VALVE "," " % ","DDD.D","FC104",100,0
9830 DATA "% BACK VALVE "," " % ","DDD.D","TP113",100,0
9840 DATA "% H2O VALVE "," " % ","DDD.D","WD109",100,0
9850 RETURN
9860 Screen_setup: !
9870 RESTORE 9930
9880 FOR I=1 TO 12

```

```

9890     FOR J=1 TO 2
9900         READ Screen(I,J)
9910     NEXT J
9920     NEXT I
9930     DATA 21,22,31,1,24,2,23,8,32,6,25,7,26,11,27,28,33,37,34,38,35,39,36,40
9940     RETURN
9950     !!!!!!!!!!!!!!!!!!!!!!! UTILITY SUBROUTINES !!!!!!!!!!!!!!!!!!!!!!!
9960 End sequence: !
9970     PRINT USING "10X,28A";"SHUTDOWN SEQUENCE INITIATED."
9980     PRINT
9990     Nlines=Nlines+3
10000    PRINTER IS 1
10010    GOSUB Cooldown
10020    GOSUB Print_data
10030    GOSUB Spec_update
10040    GOSUB Write_common
10050    GOSUB Summary
10060    RETURN
10070 Restart: !
10080    GOSUB Fuel_count
10090    OUTPUT 705;"VS1"
10100    OUTPUT 705;"VT3"
10110    GOTO Scan
10120 Rig_restart: !
10130    PRINTER IS 701
10140    PRINT CHR$(12)
10150    Nlines=0
10160    GOSUB Print_header_1
10170    PRINTER IS 1
10180    GOTO Init_variables
10190 Clearscreen: !
10200    OUTPUT 2 USING "#,B";255,75
10210    RETURN
10220 Invalid: !
10230    BEEP
10240    DISP Blank$
10250    DISP "NOT VALID KEY"
10260    WAIT .5
10270    RETURN
10280 Shutdown: !
10290    BEEP
10300    LINPUT "DO YOU REALLY WISH TO SHUTDOWN?(Y/N)",Ans$
10310    IF Ans$="Y" THEN
10320        PRINTER IS 701
10330        X=3
10340        GOSUB Turn_page
10350        PRINT USING "8A,2X,17A";TIME$(TIMEDATE),"OPERATOR REQUEST!"
10360        GOSUB End_sequence
10370        GOTO Restart
10380    ELSE
10390        GOTO Restart
10400    END IF
10410 Pgm_stop: !
10420    BEEP
10430    GOSUB Clearscreen
10440    PRINT "THIS WILL RETURN YOU TO THE MAIN MENU."
10450    PRINT
10460    PRINT "RIG SHOULD BE COOLED DOWN BEFORE PROCEEDING!"
10470    LINPUT "DO YOU WISH TO CONTINUE? (Y/N)",Ans$
10480    IF Ans$="Y" THEN

```



```

10490   Air_sp=0.
10500   GOSUB Air_out
10510   Back_sp=100.
10520   GOSUB Back_out
10530   Quench_sp=0.
10540   GOSUB Quench_out
10550   DISP "PROGRAM ENDS"
10560   BEEP 500,3
10570   GOTO Main_menu_keys
10580   ELSE
10590   GOTO Restart
10600   END IF
10610   STOP
10620   END

```

Table I. - Dew Point of Na₂SO₄ for Given Sodium Concentrations

<u>Na (ppm)</u>	<u>1 atm Dew Pt.</u>	<u>4 atm Dew Pt.</u>
0.5	920°C (1688°F)	981°C (1798°F)
1.0	938°C (1720°F)	1001°C (1834°F)
2.0	954°C (1749°F)	1020°C (1868°F)
4.0	970°C (1778°F)	1038°C (1900°F)

Table II. - Safety Upper/Lower Limits on Critical Parameters

<u>Parameter</u>	<u>Upper limit</u>	<u>Lower limit</u>
Preheated temperature	370°C (700°F)	120°C (250°F)
Combustor temperature	1400°C (2550°F)	420°C (800°F)
Exhaust temperature	200°C (400°F)	none
System pressure	600 kPa	none

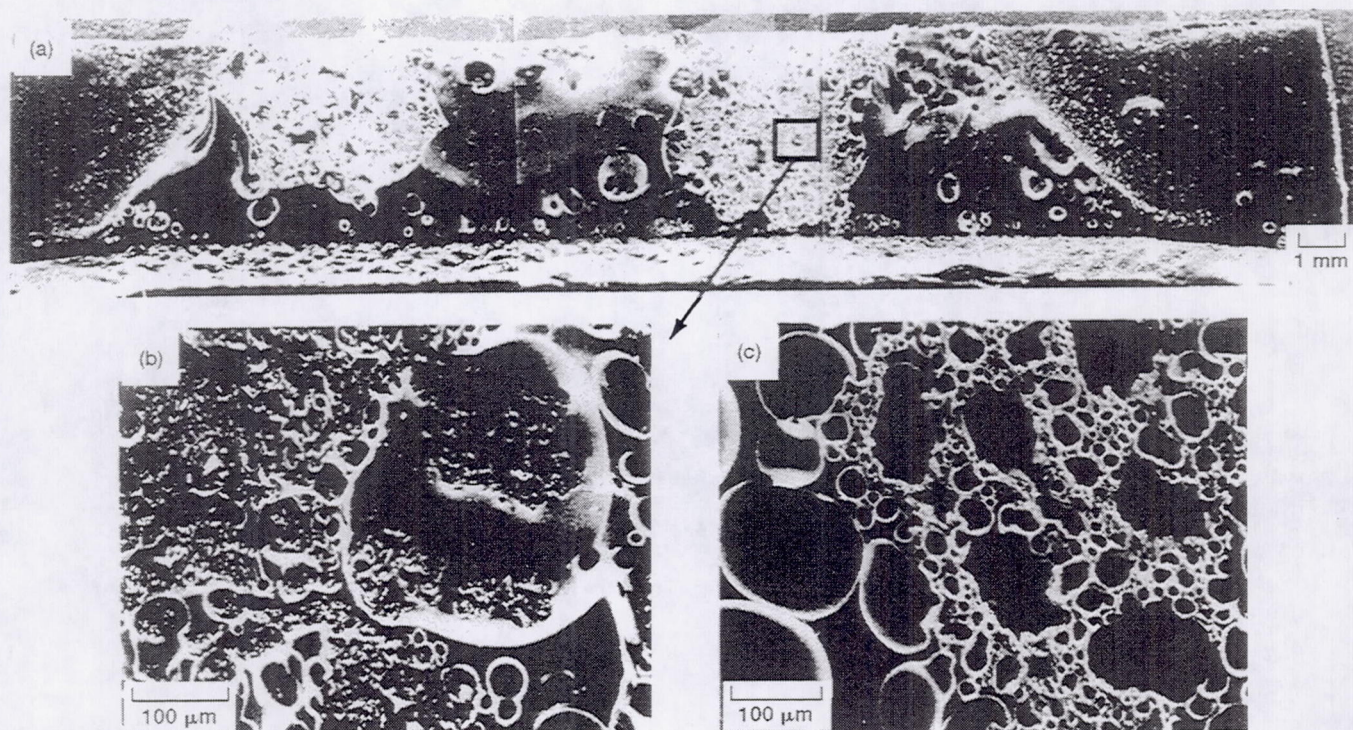


Figure 1.—SEM views of glassy products on SiC burner rig sample; (a) the entire sample (bar = 1 mm), (b) an enlargement of products near surface (bar = 100 μm); and (c) the underside of a spalled section (bar = 100 μm).

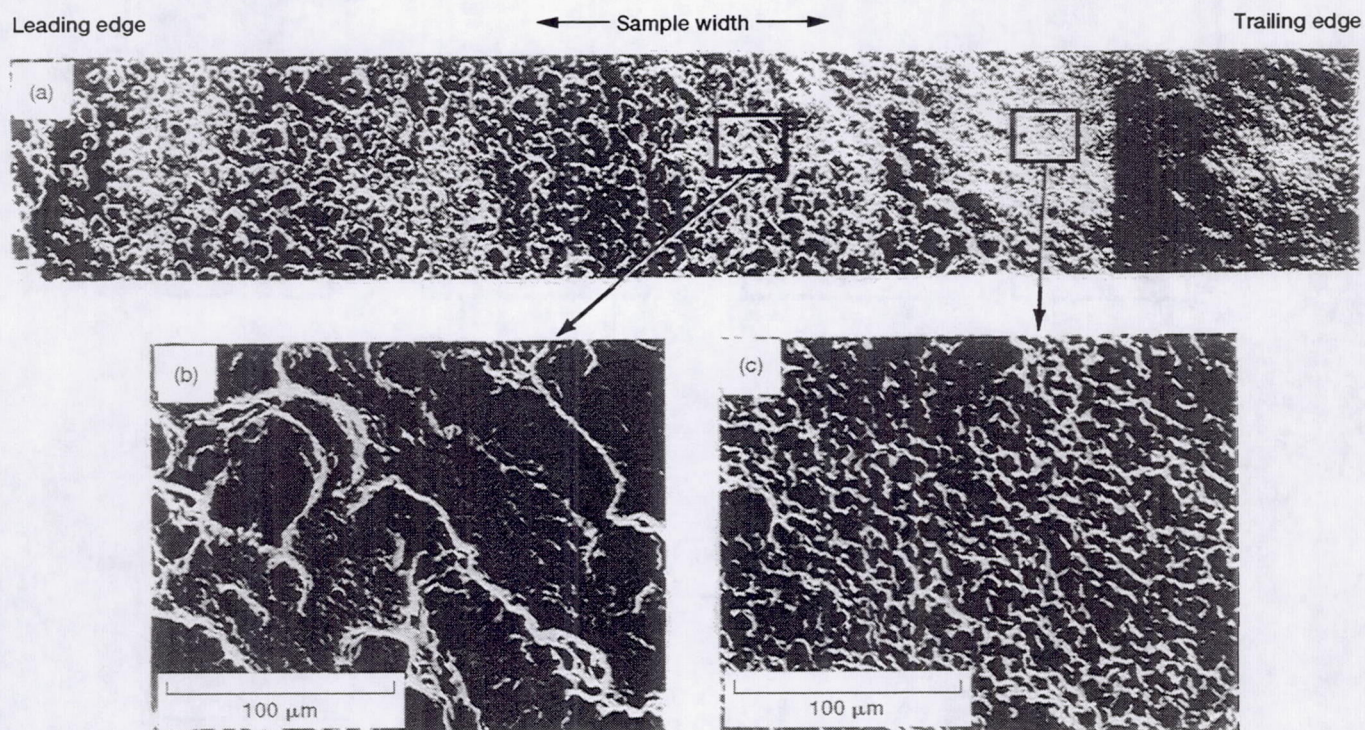


Figure 2.—Surface views of corroded SiC (products removed by HF); (a) the entire sample (bar = 100 μm), (b) enlargement of leading edge region (bar = 100 μm), (c) enlargement of trailing edge region (bar = 100 μm).

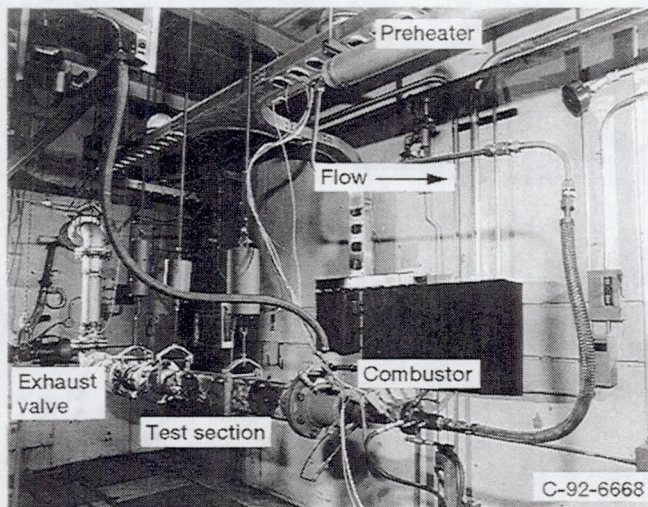


Figure 3.—Hot corrosion test facility at the NASA Lewis Research Center.

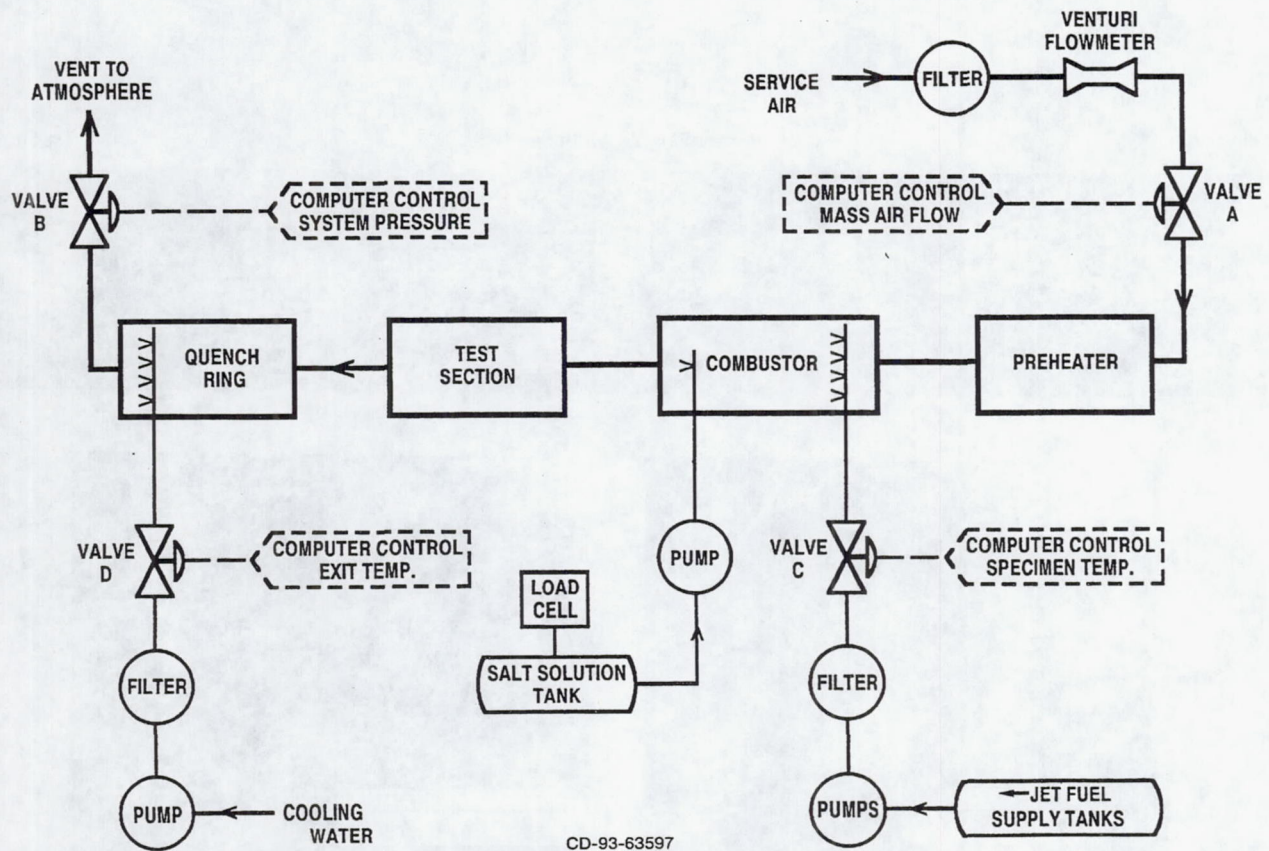


Figure 4.—Schematic of HCTF's components and support systems.

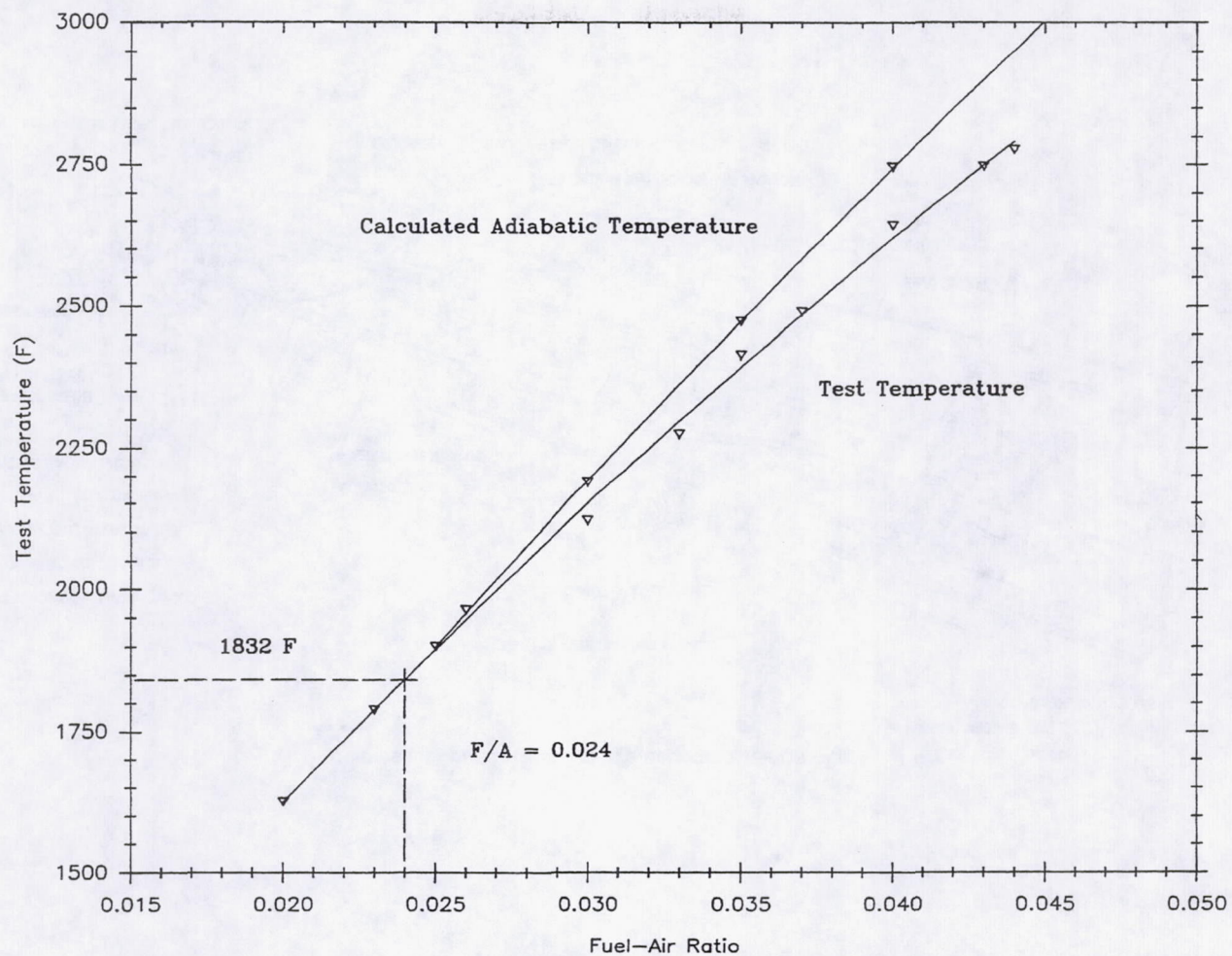


Figure 5.—Fuel-to-air ratio versus operating temperature.

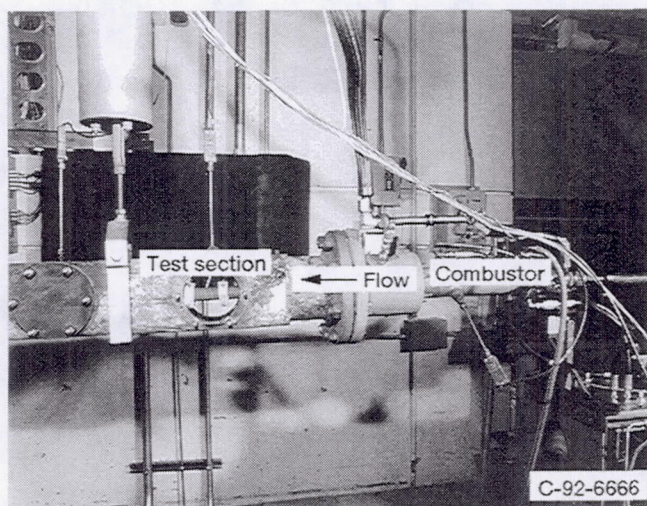


Figure 6.—HCTF combustor and test section.

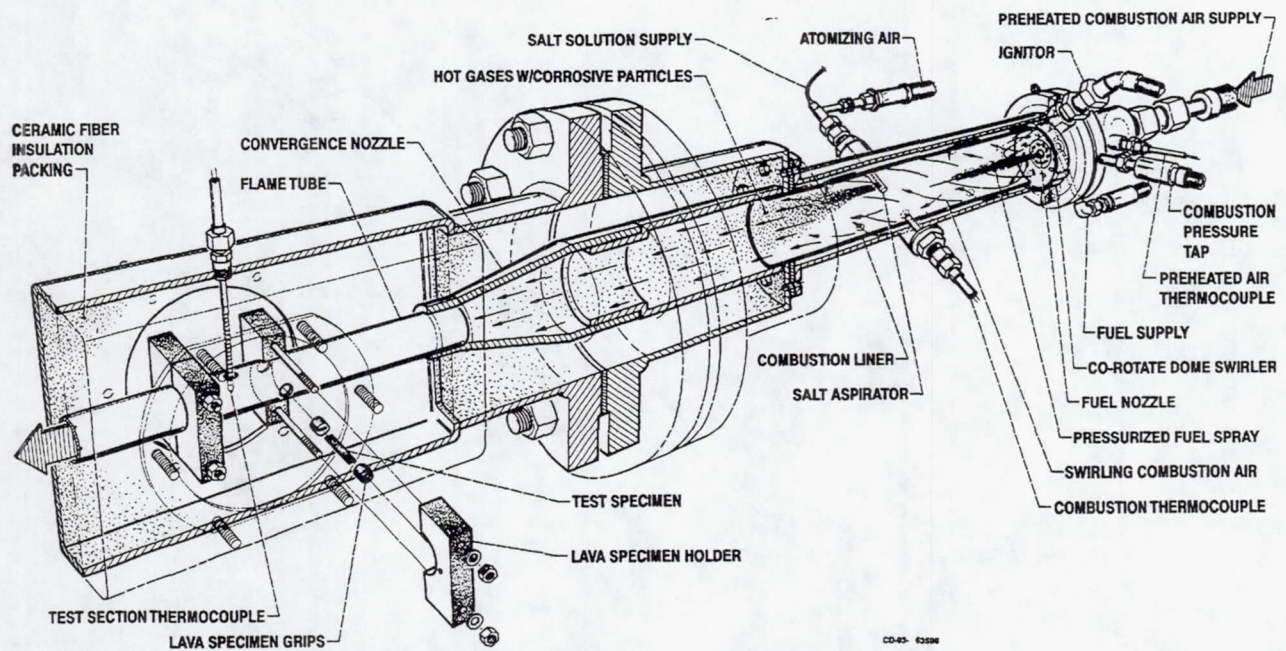


Figure 7.—Components of combustor and test section.

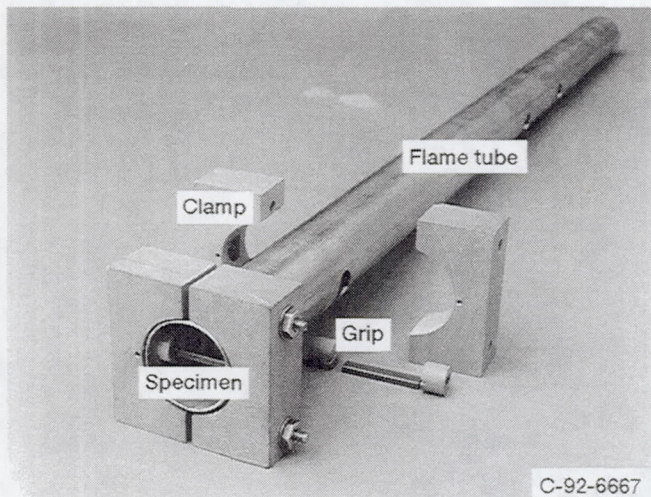


Figure 8.—Assembly of test specimens, lava holder, and flame tubes.

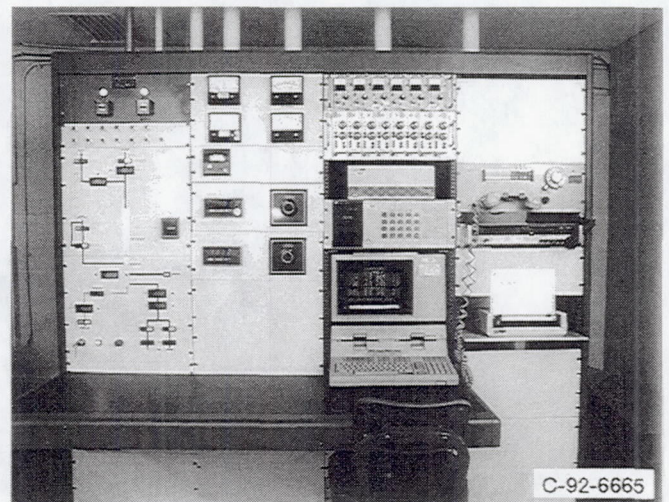


Figure 9.—HCTF control room with safety interlocks, computer and printer.

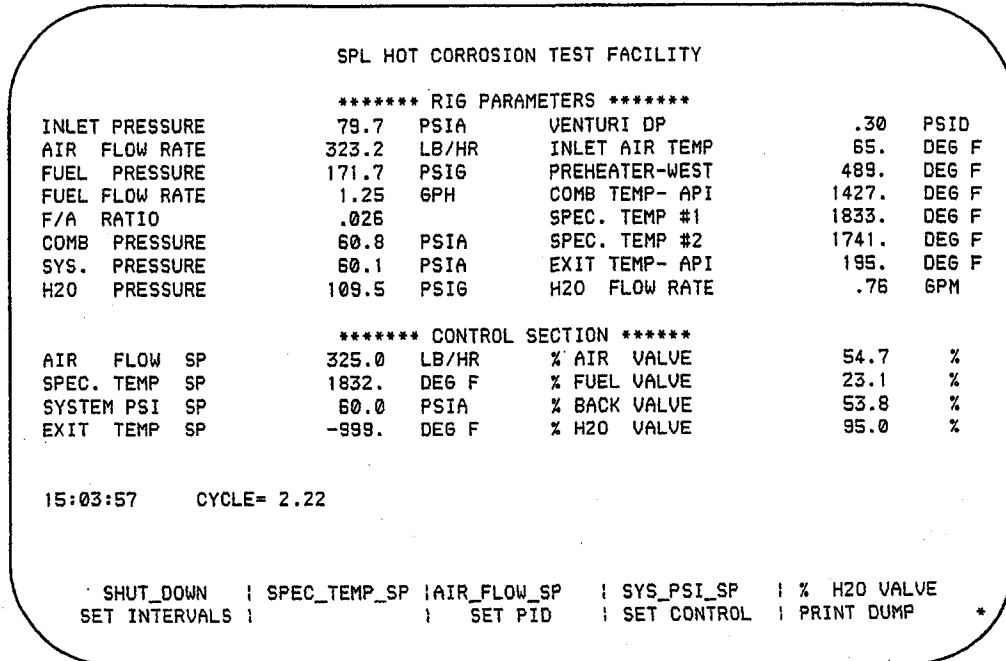


Figure 10.—Computer's data acquisition and control display screen.

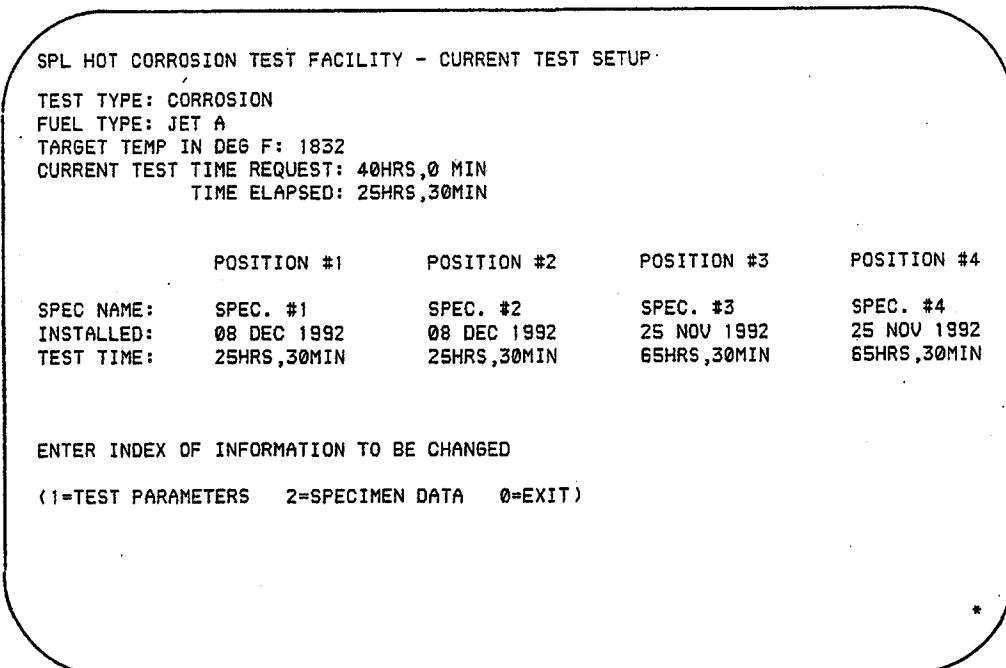


Figure 11.—Test setup and documentation utility.

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13. ABSTRACT (Maximum 200 words) The hot corrosion test facility (HCTF) at the NASA Lewis Special Projects Laboratory (SPL) is a high-velocity, pressurized burner rig currently used to evaluate the environmental durability of advanced ceramic materials such as SiC and Si3N4. The HCTF uses laboratory service air which is preheated, mixed with jet fuel, and ignited to simulate the conditions of a gas turbine engine. Air, fuel, and water systems are computer-controlled to maintain test conditions which include maximum are flows of 250 kg/hr (550lbm/hr), pressures of 100-600 kPa (1-6 atm), and gas temperatures exceeding 1500°C (2732°F). The HCTF provides a relatively inexpensive, yet sophisticated means for researchers to study the high-temperature oxidation of advanced materials, and the injection of a salt solution provides the added capability of conducting hot corrosion studies.				
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