Nonlinear Instability of a Uni-directional Transversely Sheared Mean Flow

David W. Wundrow NYMA Inc. Engineering Services Division Brook Park, Ohio

and

Marvin E. Goldstein National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio

November 1994



National Aeronautics and Space Administration (NASA-TM-106779) NONLINEAR INSTABILITY OF A UNI-DIRECTIONAL TRANSVERSELY SHEARED MEAN FLOW (NASA. Lewis Research Center) 35 p

N95-15969

Unclas

G3/34 0031429

Nonlinear instability of a uni-directional transversely sheared mean flow

By DAVID W. WUNDROW¹ AND M. E. GOLDSTEIN²

¹Nyma, Inc., Lewis Research Center Group, Cleveland, Ohio 44135, USA ²NASA, Lewis Research Center, Cleveland, Ohio 44135, USA

It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein & Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of the shear layer, means that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonlinear effects can then become important within a thin spanwise-modulated critical layer once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein & Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer.

1. Formulation

To fix ideas, we consider an incompressible shear flow formed at the interface between two parallel streams of differing velocity or alternatively between a single parallel stream and a flat plate. The Cartesian coordinate system (x, y, z) is attached to the interface with x in the direction of the external flow, y normal to the interface, and z in the spanwise direction. All lengths are non-dimensionalized by δ_* where δ_* characterizes the local shearlayer thickness at x = 0. The time t, velocity u = iu + jv + kw, and pressure variation p from the external value P_* are non-dimensionalized by δ_*/U_* , U_* and $\rho_*U_*^2$, respectively, where U_* characterizes the velocity of the external flow and ρ_* is the density. With this non-dimensionalization, the Navier-Stokes equations become

$$\nabla \cdot \boldsymbol{u} = \boldsymbol{0}, \tag{1.1}$$

$$u_t + u \cdot \nabla u + \nabla p = R^{-1} \nabla^2 u, \qquad (1.2)$$

where $\nabla \equiv i\partial/\partial x + j\partial/\partial y + k\partial/\partial z$ is the gradient operator,

$$R \equiv \delta_* U_* / \nu_* \gg 1 \tag{1.3}$$

is the local Reynolds number, ν_* is the kinematic viscosity and an independent variable used as a subscript denotes differentiation with respect to that variable.

The solutions to (1.1) and (1.2) that are of interest here can be represented as the sum of a steady base flow plus a time-dependent perturbation,

$$\boldsymbol{u} = \boldsymbol{U}(\boldsymbol{x}) + \epsilon \boldsymbol{\dot{u}}(\boldsymbol{x}, t), \tag{1.4}$$

$$p = P(x) + \epsilon \dot{p}(x, t), \qquad (1.5)$$

where ϵ characterizes the local amplitude of the perturbation at x = 0. Substituting (1.4) and (1.5) into (1.1) and (1.2) gives

$$\nabla \cdot U = 0, \tag{1.6}$$

$$U \cdot \nabla U + \nabla P = R^{-1} \nabla^2 U, \tag{1.7}$$

for the base flow and

$$\nabla \cdot \acute{u} = 0, \tag{1.8}$$

$$\dot{u}_t + U \cdot \nabla \dot{u} + \dot{u} \cdot \nabla (U + \epsilon \dot{u}) + \nabla \dot{p} = R^{-1} \nabla^2 \dot{u}, \qquad (1.9)$$

for the perturbation.

The steady spanwise-periodic base flow $\{U, P\}$ evolves over the long streamwise scale,

$$x_2 \equiv x/R, \tag{1.10}$$

and has an $O(\delta_*)$ wavelength in the spanwise direction. This implies that the base-flow solution expands like

$$U = iU_0(x_2, y, z) + R^{-1}V_0(x_2, y, z) + \cdots,$$
(1.11)

$$P = R^{-2} P_0(x_2, y, z) + \cdots,$$
(1.12)

where V denotes the base-flow velocity in the transverse (or y-z) plane. Substituting (1.11) and (1.12) into (1.6) and (1.7) shows that the leading-order base-flow solution is determined by the parabolized Navier-Stokes equations (Rudman & Rubin 1968),

$$U_{0x_2} + \boldsymbol{\nabla}_T \cdot \boldsymbol{V}_0 = 0, \tag{1.13}$$

$$U_0(iU_0 + V_0)_{x_2} + V_0 \cdot \nabla_T (iU_0 + V_0) + \nabla_T P_0 = \nabla_T^2 (iU_0 + V_0), \qquad (1.14)$$

where $\nabla_T \equiv j\partial/\partial y + k\partial/\partial z$ is the gradient operator in the transverse plane.

It is assumed that the initial amplitude of the perturbation is small enough so that $\epsilon \acute{u} \ll U_0$ over the streamwise region of interest. Substituting (1.11) into (1.8) and (1.9) then yields

$$\nabla \cdot \hat{\boldsymbol{u}} = \boldsymbol{0}, \tag{1.15}$$

$$\mathbf{D}\dot{\boldsymbol{u}} + \boldsymbol{i}(\boldsymbol{\nabla}_{T}\boldsymbol{U}_{0}\boldsymbol{\cdot}\dot{\boldsymbol{u}}) + \boldsymbol{\nabla}\dot{\boldsymbol{p}} = O(R^{-1})$$
(1.16)

where $D \equiv \partial/\partial t + U_0 \partial/\partial x$ is the leading-order convective derivative relative to the base flow. These equations are just the familiar equations for the linear perturbations about a uni-directional transversely sheared base flow (Goldstein 1976; Henningson 1987). It is well known that the velocity fluctuations can be eliminated between (1.15) and (1.16) (see Goldstein 1976, pp. 6-10 for a detailed derivation) to obtain the following equation for the pressure fluctuation

$$D\nabla^2 \dot{p} - 2\nabla_T U_0 \cdot \nabla_T \dot{p}_x = O(R^{-1}). \tag{1.17}$$

Attention will be restricted to perturbations that are spatially growing and periodic in time with, at least initially, a single angular frequency, say F_* . The relevant solutions to (1.15)-(1.17) then form a spanwise periodic instability wave that propagates in the streamwise direction. The local amplitude of the instability wave increases as the wave propagates downstream, but its local growth rate will ultimately decrease owing to the combined effects of the viscous spread of the basic shear layer and the viscous decay of the mean streamwise vorticity. Nonlinear effects can then become important first within a thin critical layer located at the transverse position where the phase speed of the instability wave equals the base-flow velocity U_0 (once the instability-wave amplitude and growth rate become sufficiently large and small respectively). In this stage of development, the unsteady flow outside the critical layer remains essentially linear but the instability-wave amplitude is completely determined by the nonlinear motion inside the critical layer.

With this in mind, the origin of the x axis is chosen so that the deviation,

$$\sigma S_1 \equiv S - S_0 < 0, \tag{1.18}$$

of the local Strouhal number (or non-dimensional angular frequency) $S \equiv \delta_* F_*/U_*$ from its neutral (or zero-growth) value S_0 is $O(\sigma)$ where $\sigma \ll 1$. The precise relationship between ϵ and σ will be specified below when the flow in the critical layer is analyzed. The relevant solutions to (1.16) and (1.17) are then of the form

$$\acute{\boldsymbol{u}} = \operatorname{Re}\left(A\hat{\boldsymbol{u}}\mathrm{e}^{\mathrm{i}X}\right) + \dots,$$
(1.19)

$$\acute{p} = \operatorname{Re}\left(A\hat{p}\mathrm{e}^{\mathrm{i}X}\right) + \dots,$$
(1.20)

where $A(x_1)$ is an amplitude function that accounts for the slow growth of the instability wave,

$$x_1 \equiv \sigma x \tag{1.21}$$

is the streamwise scale over which the wave growth occurs,

$$X \equiv \alpha_0 x - St, \tag{1.22}$$

is a normalized streamwise coordinate in a reference moving with the wave, and α_0 is the neutral wavenumber. The ellipses in (1.19) and (1.20) indicate harmonics of the fundamental instability wave that are generated by the critical-layer nonlinearity. Since these harmonics do not interact outside the critical layer (to the order of accuracy considered here), their outer solutions can be determined *a posteriori*.

Substituting (1.20) into (1.17) shows that, outside the critical layer, the function \hat{p} of x_1, y and z is determined to the required order of accuracy by

$$\nabla_T \cdot \left[\frac{\nabla_T \hat{p}}{(U_0 - c)^2} \right] - \frac{\alpha^2 \hat{p}}{(U_0 - c)^2} = 0$$
(1.23)

where

$$\alpha \equiv \alpha_0 - \sigma i A'/A, \tag{1.24}$$

and

$$c \equiv S/\alpha, \tag{1.25}$$

are the generalized wavenumber and phase speed, respectively, and a prime denotes differentiation with respect to the argument. It follows from (1.15), (1.16) and (1.19) that the velocity fluctuations are determined in terms of \hat{p} by

$$\mathbf{i} \cdot (\mathbf{i} \alpha \hat{\mathbf{u}}) + \nabla_T \cdot \hat{\mathbf{u}} = 0, \qquad (1.26)$$

and

$$i\alpha(U_0 - c)\hat{\boldsymbol{u}} + i(\nabla_T U_0 \cdot \hat{\boldsymbol{u}} + i\alpha\hat{\boldsymbol{p}}) + \nabla_T \hat{\boldsymbol{p}} = 0.$$
(1.27)

The solution to (1.23) that satisfies

$$\begin{array}{c|c} \hat{p}_y = 0 \text{ at } y = 0 \quad \text{; boundary layer} \\ \hat{p} \to 0 \text{ as } y \to -\infty \text{ ; free-shear layer} \end{array} \right\},$$

$$(1.28)$$

and

$$\hat{p} \to 0 \quad \text{as} \quad y \to \infty, \tag{1.29}$$

is analyzed in the following section.

2. Unsteady flow outside the critical layer

Outside the critical layer, the shape functions $\{\hat{u}, \hat{p}\}$ expand like

$$\hat{u} = \hat{u}_0(y, z) + \sigma \hat{u}_1(x_1, y, z) + \cdots,$$
 (2.1)

$$\hat{p} = \hat{p}_0(y, z) + \sigma \hat{p}_1(x_1, y, z) + \cdots,$$
 (2.2)

as $\sigma \to 0$, where the Reynolds number R has been assumed to be large enough so that the coefficients $\{\hat{u}_m, \hat{p}_m\}$ depend only parametrically on the slow streamwise variable x_2 , i.e. x_2 plays the role of a constant. Substituting (2.2), (1.24) and (1.25) into (1.23) and equating like powers of σ leads to

$$\nabla_T \cdot \left[\frac{\nabla_T \hat{p}_0}{(U_0 - c_0)^2} \right] - \frac{\alpha_0^2 \hat{p}_0}{(U_0 - c_0)^2} = 0, \qquad (2.3)$$

and

$$\nabla_T \cdot \left[\frac{\nabla_T \hat{p}_1}{(U_0 - c_0)^2} \right] - \frac{\alpha_0^2 \hat{p}_1}{(U_0 - c_0)^2} = 2\alpha_1 \frac{\alpha_0 \hat{p}_0}{(U_0 - c_0)^2} + 2c_1 \frac{\nabla_T U_0 \cdot \nabla_T \hat{p}_0}{(U_0 - c_0)^4}, \tag{2.4}$$

where $c_0 \equiv S_0/\alpha_0$, $\alpha_1 \equiv -iA'/A$, and $c_1 \equiv (S_1 - \alpha_1 c_0)/\alpha_0$.

Equations (2.3) and (2.4) must, of course, be solved numerically subject to the boundary conditions (1.28) and (1.29). However, for the present analysis, it is only necessary to know the behavior of the solutions near the critical level. This is most easily determined by first expressing (2.3) and (2.4) in orthogonal curvilinear coordinates, say (η, ζ) , with one set of coordinate surfaces corresponding to surfaces of constant base-flow velocity U_0 - as was done, for example, by Goldstein (1976, pp. 6–10). The functions η and ζ of y and z are chosen so that

$$U_0 = U_0(x_2, \eta), \tag{2.5}$$

$$\eta = y_0 \quad \text{at} \quad y = y_0, \quad \eta \to \infty \quad \text{as} \quad y \to \infty,$$
 (2.6)

 \mathbf{and}

$$\nabla_T U_0 \cdot \nabla_T \zeta = 0, \tag{2.7}$$

$$\zeta = 0$$
 at $z = 0$, $\zeta = 2\pi/\beta$ at $z = 2\pi/\beta$, (2.8)

where

$$y_0 = \begin{cases} 0 ; \text{ boundary layer} \\ -\infty ; \text{ free-shear layer} \end{cases},$$
(2.9)

 β is the (non-dimensional) spanwise wavenumber of the base flow and (2.8) requires (without loss of generality) that z = 0 and $z = 2\pi/\beta$ be the planes of symmetry of U_0 . In terms of η and ζ , the gradient operator in the transverse plane is

$$\nabla_T = l \frac{1}{g} \frac{\partial}{\partial \eta} + m \frac{1}{h} \frac{\partial}{\partial \zeta}, \qquad (2.10)$$

where $(l, m) \equiv (g \nabla \eta, h \nabla \zeta)$ are the unit vectors and $(g, h) \equiv (|\nabla \eta|^{-1}, |\nabla \zeta|^{-1})$ are the scale factors corresponding to the coordinates (η, ζ) , respectively.

It follows from (2.5) that the critical-level position is given by $\eta = \eta_c$ where

$$U_0(x_2,\eta) = c_0 \quad \text{at} \quad \eta = \eta_c.$$
 (2.11)

The near-critical-level expansions of \hat{p}_0 and \hat{p}_1 can now be found by the method of Frobenius (Hall & Horseman 1991; Horseman 1991; and Hall & Smith 1991). To the required level of approximation, these expansions are

$$\hat{p}_{0} = a_{00} + a_{02}(\eta - \eta_{c})^{2} + (a_{03}^{(L)} \ln |\eta - \eta_{c}| + b_{03}^{\pm})(\eta - \eta_{c})^{3} + (a_{04}^{(L)} \ln |\eta - \eta_{c}| + a_{04} + b_{04}^{\pm})(\eta - \eta_{c})^{4} + O[(\eta - \eta_{c})^{5} \ln |\eta - \eta_{c}|],$$
(2.12)

and

$$\hat{p}_1 = a_{10} + d_{11}(\eta - \eta_c) + (d_{12}^{(L)} \ln |\eta - \eta_c| + a_{12} + d_{12}^{\pm})(\eta - \eta_c)^2$$

+
$$[(a_{13}^{(L)} + d_{13}^{(L)}) \ln |\eta - \eta_c| + b_{13}^{\pm}](\eta - \eta_c)^3 + O[(\eta - \eta_c)^4 \ln |\eta - \eta_c|],$$
 (2.13)

where the \pm superscript denotes differing values for $\eta \ge \eta_c$ and the fact that the pressure is continuous across the critical layer to $O(\sigma\epsilon)$ (see (3.13), (3.17) and (B3) below) has been used. At this point, the coefficients a_{m0} and b_{m3}^{\pm} are arbitrary functions of ζ . Expressions for the remaining coefficients in terms of these functions are given in appendix A.

The boundary-value problem (1.28), (1.29), and (2.4) only possesses solutions for certain values of α_1 since \hat{p}_0 is a homogeneous solution to (2.3). These values can be found without explicitly solving for \hat{p}_1 by integrating the difference between \hat{p}_0 times (2.4) and \hat{p}_1 times (2.3) over the transverse domain, applying the divergence theorem to the simply connected regions and then making use of (1.28), (1.29), the z periodicity of \hat{p} and the expansions (2.12) and (2.13) to arrive at a solvability condition. For definiteness, we consider the simplest case where the critical level forms a single closed or open curve that divides the transverse domain into two simply connect regions. In this case, the solvability condition becomes

$$\int_{0}^{2\pi/\beta} \Phi_{0} \left[\left(2a_{00} \frac{c_{1} \Phi_{1}}{U_{0\eta_{c}} \Phi_{0}} + a_{10} \right) (b_{03}^{+} - b_{03}^{-}) - a_{00} (b_{13}^{+} - b_{13}^{-}) \right] d\zeta \\ = \frac{2U_{0\eta_{c}}}{3\alpha_{0}} \left(I_{P} \frac{\alpha_{1}}{\alpha_{0}} + J_{P} \frac{c_{1}}{c_{0}} \right), \quad (2.14)$$

where the functions Φ_0 and Φ_1 of ζ are given by (A 26), the *c* subscript denotes evaluation at $\eta = \eta_c$,

$$I_P \equiv \int_0^{2\pi/\beta} \int_{y_0}^\infty \frac{\alpha_0^2 \hat{p}_0^2}{(U_0 - c_0)^2} g h \mathrm{d}\eta \mathrm{d}\zeta, \qquad (2.15)$$

$$J_{P} \equiv \int_{0}^{2\pi/\beta} \int_{y_{0}}^{\infty} \frac{c_{0}}{(U_{0} - c_{0})^{3}} \left(\nabla_{T} \hat{p}_{0} \cdot \nabla_{T} \hat{p}_{0} + \alpha_{0}^{2} \hat{p}_{0}^{2} \right) gh d\eta d\zeta, \qquad (2.16)$$

and f denotes the Cauchy principal value.

For purposes of analyzing the nonlinear flow within the critical layer, it is convenient to express the velocity perturbation as

$$\acute{u} = i\frac{\acute{u}}{gh} + l\frac{\acute{v}}{h} + m\frac{\acute{w}}{g}. \tag{2.17}$$

The near-critical-level expansions of the shape functions corresponding to \hat{u} , \hat{v} and \hat{w} are given in appendix A where it is shown that the discontinuities in (2.12) and (2.13) lead to a jump in the streamwise velocity component

$$\Delta \hat{u} = -\frac{3\Phi_0}{\alpha_0} \left[b_{03}^+ - b_{03}^- + \sigma (b_{13}^+ - b_{13}^-) - 2\sigma \left(\frac{c_1 \Phi_1}{U_{0\eta_c} \Phi_0} + \frac{\alpha_1}{\alpha_0} \right) (b_{03}^+ - b_{03}^-) \right] + \cdots$$
(2.18)

across the critical layer. Matching this jump with the one induced by the flow in the critical layer determines the functions b_{m3}^{\pm} . However, when determining b_{13}^{\pm} , it is more convenient to express the jump condition as

$$\Delta \left[\hat{\bar{v}}_{\eta} - \frac{U_{0\eta\bar{\eta}_c}}{U_{0\eta_c}} \hat{\bar{v}} - \left(e^{(L)}_{02} + 2e^{\pm}_{02} - \frac{U_{0\eta\bar{\eta}_c}}{U_{0\eta_c}} e^{\pm}_{01} \right) (\eta - \eta_c) \right]$$

= $i3 \Phi_0 \left[(b^+_{03} - b^-_{03}) + \sigma (b^+_{13} - b^-_{13}) + \sigma \left(2\frac{c_1\bar{g}_{\eta_c}}{U_{0\eta_c}\bar{g}_c} - \frac{\alpha_1}{\alpha_0} \right) (b^+_{03} - b^-_{03}) \right] + \cdots, \quad (2.19)$

which follows directly from (A 29) and (A 30).

3. Unsteady flow inside the critical layer

As already noted, nonlinear effects first come into play locally within the so-called critical layer once the deviation of the local Strouhal number from its neutral value becomes sufficiently small. The thickness of the critical layer, which is determined by the balance of wave-growth and base-flow-convection effects, turns out to be order σ on the η scale so the appropriate scaled coordinate for this region is

$$\bar{\eta} \equiv (\eta - \eta_c) / \sigma. \tag{3.1}$$

The nonlinear terms in (1.9) produce a critical-layer velocity jump at the same order as the linear-growth effects when the scale of the frequency deviation σ , which was introduced in (1.18), is chosen to be

$$\sigma = \epsilon^{\frac{1}{3}} \tag{3.2}$$

(Goldstein & Choi 1989). Viscous effects will enter into the dominant balance for the criticallayer while making only insignificant modifications to the outer flow when the Benney-Bergeron parameter

$$\lambda \equiv 1/\sigma^3 R \tag{3.3}$$

(Benney & Bergeron 1969) is order one. In the present analysis, λ is assumed to be small enough so that viscous effects, which may arise from the x_2 dependence of the base-flow solution as well as the viscous-diffusions terms in (1.9), are negligible.

Since the flow inside the critical layer depends on x and t only through the variables (1.21) and (1.22), the appropriate governing equations for this region are obtained by expressing (1.8) and (1.9) in terms of x_1 , X, $\bar{\eta}$ and ζ . Upon introducing (2.17), these equations become

$$\sigma^2 \acute{u}_{x_1} + \sigma \alpha_0 \acute{u}_X + \acute{v}_{\bar{\eta}} + \sigma \acute{w}_{\zeta} = 0, \qquad (3.4)$$

 \mathbf{and}

$$\mathcal{L}\dot{\tilde{u}} + ghU_{0\bar{\eta}}\frac{\dot{\tilde{v}}}{\sigma} + g^2h^2(\sigma\dot{p}_{x_1} + \alpha_0\dot{p}_X) = -\sigma^3gh\mathcal{N}\left(\frac{\dot{\tilde{u}}}{gh}\right),\tag{3.5}$$

$$\sigma \mathcal{L}\hat{v} + h^2 \dot{p}_{\bar{\eta}} = -\sigma^3 \left[\sigma \frac{h}{g} \mathcal{N} \left(\frac{g \hat{v}}{h} \right) - \frac{g_{\bar{\eta}}}{g} \dot{v}^2 - \frac{h h_{\bar{\eta}}}{g^2} \dot{w}^2 \right], \tag{3.6}$$

$$\mathcal{L}\dot{\bar{w}} + g^2 \dot{p}_{\zeta} = -\sigma^3 \left[\frac{g}{h} \mathcal{N} \left(\frac{h\dot{\bar{w}}}{g} \right) - \frac{gg_{\zeta}}{h^2} \dot{\bar{v}}^2 - \frac{h_{\zeta}}{h} \dot{\bar{w}}^2 \right], \qquad (3.7)$$

where

$$\mathcal{L} \equiv \sigma g h U_0 \frac{\partial}{\partial x_1} + \alpha_0 g h \left(U_0 - c_0 - \sigma \frac{S_1}{\alpha_0} \right) \frac{\partial}{\partial X}, \qquad (3.8)$$

$$\mathcal{N} \equiv \sigma \hat{u} \frac{\partial}{\partial x_1} + \alpha_0 \hat{u} \frac{\partial}{\partial X} + \frac{\dot{v}}{\sigma} \frac{\partial}{\partial \bar{\eta}} + \hat{w} \frac{\partial}{\partial \zeta}.$$
(3.9)

Introducing (3.1) into the expressions for $\hat{\hat{u}}$, $\hat{\hat{v}}$, $\hat{\hat{w}}$ and \hat{p} obtained from (A 18), (A 29)-(A 34), (2.2), (2.12) and (2.13) and re-expanding the result shows that the unsteady flow in the critical layer should expand like

$$\dot{\bar{u}} = \sigma^{-1}\bar{u}_0 + \bar{u}_1 + \sigma\bar{u}_2 + \cdots,$$
(3.10)

$$\dot{\bar{v}} = \bar{v}_0 + \sigma \bar{v}_1 + \sigma^2 \bar{v}_2 + \cdots,$$
 (3.11)

$$\dot{\bar{w}} = \sigma^{-1}\bar{w}_0 + \bar{w}_1 + \sigma\bar{w}_2 + \cdots, \qquad (3.12)$$

$$\dot{p} = p_0 + \sigma p_1 + \sigma^2 p_2 + \cdots, \qquad (3.13)$$

where, in general, the functions \bar{u}_m , \bar{v}_m , \bar{w}_m and p_m of x_1 , X, $\bar{\eta}$ and ζ have an implicit σ dependence of the form

$$\bar{u}_m = \bar{u}_m^{(L)} \ln \sigma + \bar{u}_m^{(0)}. \tag{3.14}$$

In this region, the known functions U_0 , g and h are given by their Taylor series expansions about $\eta = \eta_c$ when expressed in terms of $\bar{\eta}$.

Substituting (3.10)–(3.13) into (3.4)–(3.7) and equating like powers of σ leads to the following set of equations at leading order

$$\alpha_0 \bar{u}_{0X} + \bar{v}_{0\bar{\eta}} + \bar{w}_{0\zeta} = 0, \qquad (3.15)$$

$$\mathcal{L}_0 \bar{u}_0 + U_{0\eta_c} \bar{v}_0 + \alpha_0 g_c h_c p_{0X} = 0, \qquad (3.16)$$

$$p_{0\bar{n}} = 0, \tag{3.17}$$

$$\mathcal{L}_0 \bar{w}_0 + \frac{g_c}{h_c} p_{0\zeta} = 0, \qquad (3.18)$$

where

$$\mathcal{L}_0 \equiv c_0 \frac{\partial}{\partial x_1} + (\alpha_0 U_{0\eta_c} \bar{\eta} - S_1) \frac{\partial}{\partial X}.$$
(3.19)

The solutions to (3.15)-(3.18) must reduce to the appropriate linear solutions as $x_1 \rightarrow -\infty$, they must be periodic in X, and they must match with the outer solutions discussed in §2. It follows from (2.12), (2.13) and (A 29)-(A 34) that the last condition implies that

$$\{\bar{u}_0, \bar{v}_0, \bar{w}_0, p_0\} \to \operatorname{Re}\left(\{\mathrm{i}f_{0-1\zeta}/\alpha_0\bar{\eta}, e_{00}, f_{0-1}/\bar{\eta}, a_{00}\}A\mathrm{e}^{\mathrm{i}X}\right),\tag{3.20}$$

as $\bar{\eta} \to \pm \infty$, where the functions e_{00} and f_{0-1} of ζ are given in terms of a_{00} by (A 35) and (A 44). It is easy to show that the appropriate solutions to (3.15)-(3.18) are

$$\{\bar{u}_0, \bar{v}_0, \bar{w}_0, p_0\} = \operatorname{Re}\left(\{-U_{0\eta_c} f_{0-1\zeta} E, e_{00} A e^{iX}, i\alpha_0 U_{0\eta_c} f_{0-1} E, a_{00} A e^{iX}\}\right),$$
(3.21)

where the function $E(x_1, X, \bar{\eta})$ is determined by

$$\mathcal{L}_0 E = A \mathrm{e}^{\mathrm{i}X} \tag{3.22}$$

together with the condition that $E \to 0$ as $x_1 \to -\infty$ and that E be periodic in X. Therefore

$$E = \frac{1}{c_0} \int_{-\infty}^{x_1} A(\xi) \mathrm{e}^{\mathrm{i}[X + \bar{Y}(\xi - x_1)]} \mathrm{d}\xi$$
 (3.23)

where $\bar{Y} \equiv (\alpha_0 U_{0\eta_c} \bar{\eta} - S_1)/c_0$.

The higher-order critical-layer problems are derived in appendix B. There it is shown that the relevant solutions to the order- σ problem can be expressed as

$$\bar{u}_{1\bar{\eta}} = \bar{u}_{1\bar{\eta}}^{\dagger} + \bar{u}_{1\bar{\eta}}^{\dagger} + \left(\frac{\bar{u}_0\bar{u}_{0\bar{\eta}}}{g_ch_cU_{0\eta_c}}\right)_{\bar{\eta}}, \qquad (3.24)$$

$$\bar{w}_1 = \bar{w}_1^{\dagger} + \bar{w}_1^{\dagger} + \left(\frac{\bar{u}_0 \bar{w}_0}{g_c h_c U_{0\eta_c}}\right)_{\bar{\eta}},\tag{3.25}$$

where the linear components $\bar{u}_{1\bar{\eta}}^{\dagger}$ and \bar{w}_{1}^{\dagger} are given by (B18)-(B20) and the nonlinear components $\bar{u}_{1\bar{\eta}}^{\dagger}$ and \bar{w}_{1}^{\dagger} must be determined from

$$\alpha_0 \mathcal{L}_0 \bar{u}_{1\bar{\eta}}^{\dagger} = \alpha_0 U_{0\eta_c} \bar{w}_{1\zeta}^{\dagger} - (\gamma_{3\zeta} - 2\gamma_4) \operatorname{Re}\left(\mathrm{i}A\mathrm{e}^{\mathrm{i}X}\right) \operatorname{Re}(\mathrm{i}E_{\bar{\eta}\bar{\eta}}), \qquad (3.26)$$

$$\mathcal{L}_{0}\bar{w}_{1}^{\dagger} = (\gamma_{1} - 2\gamma_{2})\operatorname{Re}\left(Ae^{iX}\right)\operatorname{Re}(iE_{\bar{\eta}}) - \gamma_{3}\operatorname{Re}\left(iAe^{iX}\right)\operatorname{Re}(E_{\bar{\eta}}) - 2\gamma_{2}\alpha_{0}U_{0\eta_{c}}\operatorname{Re}(E)^{2}, \quad (3.27)$$

where the functions $\gamma_n(\zeta)$ are given as

$$\{\gamma_1, \gamma_2, \gamma_3, \gamma_4\} \equiv \frac{g_c}{2\alpha_0 h_c U_{0\eta_c}} \left\{ \left(\frac{a_{00\zeta}^2}{h_c^2}\right)_{\zeta}, \frac{1}{g_c} \left(\frac{g_c a_{00\zeta}^2}{h_c^2}\right)_{\zeta}, \left(\alpha_0^2 a_{00}^2\right)_{\zeta}, \alpha_0^2 a_{00\zeta}^2 \right\}, \quad (3.28)$$

and it has been assumed (without loss of generality) that a_{00} is purely real. The solutions to (3.26) and (3.27) turn out to be

$$\alpha_0 \bar{u}_{1\bar{\eta}}^{\ddagger} = -\frac{1}{2} (\gamma_1 - \gamma_3)_{\zeta} \operatorname{Re}(F_{\bar{\eta}} - G) - (\gamma_{3\zeta} - 2\gamma_4) \operatorname{Re}(\mathrm{i}G_X + G) - \gamma_{2\zeta} \operatorname{Re}(G) + \frac{1}{2} (\gamma_1 + \gamma_3)_{\zeta} \operatorname{Re}(H) + \gamma_{2\zeta} \operatorname{Re}(E) \operatorname{Re}(E_{\bar{\eta}\bar{\eta}}),$$
(3.29)

$$\bar{w}_{1}^{\ddagger} = \gamma_{1} \operatorname{Re}(F_{X} - \mathrm{i}F) - \gamma_{3} \operatorname{Re}(\mathrm{i}F) - 2\gamma_{2} \operatorname{Re}(E) \operatorname{Re}(\mathrm{i}E_{\bar{\eta}}), \qquad (3.30)$$

where the functions F, G and H of x_1, X and $\bar{\eta}$ are determined by

$$\mathcal{L}_0\{F, G, H\} = \{A e^{iX} \operatorname{Re}(E_{\bar{\eta}}), A e^{iX} \operatorname{Re}(E_{\bar{\eta}\bar{\eta}}), \alpha_0 U_{0\eta_c}(F_X - i2F)\}$$
(3.31)

together with the condition that $\{F, G, H\} \to 0$ as $x_1 \to -\infty$ and that $\{F, G, H\}$ be periodic in X. Therefore

$$F = i \frac{\alpha_0 U_{0\eta_c}}{2c_0^3} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_2} (\xi_2 - \xi_1) A(\xi_2) \left\{ A^*(\xi_1) e^{i\bar{Y}(\xi_2 - \xi_1)} - A(\xi_1) e^{i[2X + \bar{Y}(\xi_1 + \xi_2 - 2x_1)]} \right\} d\xi_1 d\xi_2, \quad (3.32)$$

$$G = -\frac{\alpha_0^2 U_{0\eta_c}^2}{2c_0^4} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_2} (\xi_2 - \xi_1)^2 A(\xi_2) \left\{ A^*(\xi_1) \mathrm{e}^{\mathrm{i}\bar{Y}(\xi_2 - \xi_1)} + A(\xi_1) \mathrm{e}^{\mathrm{i}[2X + \bar{Y}(\xi_1 + \xi_2 - 2x_1)]} \right\} \mathrm{d}\xi_1 \mathrm{d}\xi_2, \quad (3.33)$$

and

$$H = \frac{\alpha_0^2 U_{0\eta_c}^2}{c_0^4} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_2} (x_1 - \xi_2) (\xi_2 - \xi_1) A(\xi_2) A^*(\xi_1) \mathrm{e}^{\mathrm{i}\bar{Y}(\xi_2 - \xi_1)} \mathrm{d}\xi_1 \mathrm{d}\xi_2, \tag{3.34}$$

where the asterisk denotes complex conjugation.

In appendix B, it is shown that the relevant solution to the order- σ^2 problem can be expressed as

$$\begin{split} \bar{v}_{2\bar{\eta}\bar{\eta}} &= \bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} + \bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} - \alpha_{0} \left[\frac{\bar{u}_{0}\bar{u}_{1}^{\dagger}}{g_{c}h_{c}U_{0\eta_{c}}} + \left(\frac{\bar{u}_{0}^{3}}{6g_{c}^{2}h_{c}^{2}U_{0\eta_{c}}^{2}} \right)_{\bar{\eta}} \right]_{X\bar{\eta}\bar{\eta}} \\ &- \left[\frac{\bar{u}_{0}\bar{w}_{1}^{\dagger} + \bar{u}_{1}^{\dagger}\bar{w}_{0}}{g_{c}h_{c}U_{0\eta_{c}}} + \left(\frac{\bar{u}_{0}^{2}\bar{w}_{0}}{2g_{c}^{2}h_{c}^{2}U_{0\eta_{c}}^{2}} \right)_{\bar{\eta}} \right]_{\bar{\eta}\bar{\eta}\zeta} \end{split}$$
(3.35)

where the linear component $\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger}$ is given by (B36) and the nonlinear component satisfies (B40). For purposes of obtaining the evolution equation for $A(x_1)$, it is only necessary to determine the quantity

$$\tilde{\bar{v}}_{2\bar{\eta}\bar{\eta}}^{\dagger} \equiv \frac{1}{\pi} \int_{0}^{2\pi} \int_{0}^{2\pi/\beta} a_{00} \mathrm{e}^{-\mathrm{i}X} \bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} \mathrm{d}\zeta \mathrm{d}X$$
(3.36)

which, as shown in appendix B, is determined by

$$L\tilde{\bar{v}}_{2\bar{\eta}\bar{\eta}}^{\ddagger} = A \operatorname{Re}[(2k_{1} + k_{4} + 3k_{5})G_{\bar{\eta}}^{(0)} - (k_{3} + 2k_{4} + k_{5})H_{\bar{\eta}} - (k_{1} + k_{2})(E^{(1)}E_{\bar{\eta}\bar{\eta}}^{(1)*})_{\bar{\eta}}$$

- $(k_{1} + \frac{1}{2}k_{3} - \frac{1}{2}k_{4})(E^{(1)}E_{\bar{\eta}}^{(1)*})_{\bar{\eta}\bar{\eta}}] + iA \operatorname{Re}[-i(k_{3} + 2k_{4} + k_{5})G_{\bar{\eta}}^{(0)}$
+ $i(k_{1} + k_{2})(E^{(1)}E_{\bar{\eta}\bar{\eta}}^{(1)*})_{\bar{\eta}\bar{\eta}}] + \frac{1}{2}A^{*}[(2k_{1} - k_{3} + k_{4} + 2k_{5})G_{\bar{\eta}}^{(2)}$
- $(k_{1} - k_{2})(E^{(1)}E_{\bar{\eta}\bar{\eta}}^{(1)})_{\bar{\eta}} - (k_{2} + \frac{1}{2}k_{3} + \frac{1}{2}k_{4})(E^{(1)}E_{\bar{\eta}}^{(1)})_{\bar{\eta}\bar{\eta}}] - L\tilde{\phi}_{2\bar{\eta}\bar{\eta}}$ (3.37)

where

$$\mathcal{L} \equiv c_0 \frac{\partial}{\partial x_1} + i(\alpha_0 U_{0\eta_c} \bar{\eta} - S_1), \qquad (3.38)$$

$$(\cdot)^{(m)} \equiv \frac{1}{2\pi} \int_0^{2\pi} e^{-imX} (\cdot) dX,$$
 (3.39)

the real constants k_n are given as

$$\{k_1, k_2, k_3, k_4, k_5\} \equiv \int_0^{2\pi/\beta} \frac{h_c}{g_c} \{\gamma_1 \gamma_2, \ \gamma_2 \gamma_3, \ \gamma_1^2, \ \gamma_1 \gamma_3, \ \gamma_3^2\} \mathrm{d}\zeta, \tag{3.40}$$

the function $ilde{\phi}_2(x_1,ar{\eta})$ is given as

$$\tilde{\phi}_{2} \equiv \frac{1}{\pi} \int_{0}^{2\pi} i e^{-iX} \operatorname{Re}(E) [k_{3} \operatorname{Re}(F_{X}) - (k_{3} + k_{4}) \operatorname{Re}(iF) + i(2k_{1} + k_{3}) \operatorname{Re}(iE) \operatorname{Re}(iE_{\bar{\eta}})] dX, \qquad (3.41)$$

and the fact that $F_{\bar{\eta}\bar{\eta}}^{(0)} = G_{\bar{\eta}}^{(0)}$ has been used in arriving at (3.37). The solution to (3.37) turns out to be

$$\tilde{\tilde{v}}_{2\bar{\eta}\bar{\eta}}^{4} = (2k_{1} + k_{3} + 3k_{4} + 4k_{5})Q_{1} + (2k_{1} - k_{3} - k_{4} + 2k_{5})Q_{2}
+ (2k_{1} - k_{3} + k_{4} + 2k_{5})Q_{3} - (k_{3} + 2k_{4} + k_{5})Q_{4} - (k_{1} + k_{2})Q_{5}
- (k_{1} - k_{2})Q_{6} - (2k_{1} + k_{2} + \frac{1}{2}k_{3} - \frac{1}{2}k_{4})Q_{7} + (k_{2} - \frac{1}{2}k_{3} + \frac{1}{2}k_{4})Q_{8}
- (k_{2} + \frac{1}{2}k_{3} + \frac{1}{2}k_{4})Q_{9} - \tilde{\phi}_{2\bar{\eta}\bar{\eta}},$$
(3.42)

where the functions $Q_n(x_1, \bar{\eta})$ are determined by

$$L\{Q_1, Q_2, Q_3, Q_4\} = \frac{1}{2} \{ AG_{\bar{\eta}}^{(0)}, \ AG_{\bar{\eta}}^{(0)*}, \ A^*G_{\bar{\eta}}^{(2)}, \ 2ARe(H_{\bar{\eta}}) \},$$
(3.43)

$$L\{Q_5, Q_6\} = \frac{1}{2} \{2A \operatorname{Re}(E^{(1)} E^{(1)^*}_{\bar{\eta}\bar{\eta}})_{\bar{\eta}}, \ A^*(E^{(1)} E^{(1)}_{\bar{\eta}\bar{\eta}})_{\bar{\eta}}\}$$
(3.44)

$$L\{Q_7, Q_8, Q_9\} = \frac{1}{2} \{ A(E^{(1)}E^{(1)*}_{\bar{\eta}})_{\bar{\eta}\bar{\eta}}, \ A(E^{(1)*}E^{(1)}_{\bar{\eta}})_{\bar{\eta}\bar{\eta}}, \ A^*(E^{(1)}E^{(1)}_{\bar{\eta}})_{\bar{\eta}\bar{\eta}} \},$$
(3.45)

together with the condition that the $Q_n \to 0$ as $x_1 \to -\infty$. Explicit expressions for the Q_n are given in appendix C.

4. Amplitude evolution equation

The velocity jump induced by the flow in the critical layer will now be computed and combined with (2.18) and (2.19) in order to determine the functions b_{m3}^{\pm} . These results will then be used in (2.14) to obtain the governing equation for $A(x_1)$.

By using the relation

$$\int_{-\infty}^{+\infty} \mathrm{e}^{\mathrm{i}\bar{Y}(\xi-x)} \mathrm{d}\bar{\eta} = \frac{2\pi c_0}{\alpha_0 U_{0\eta_c}} \delta(\xi-x)$$
(4.1)

where δ denotes the Dirac delta function, one can show from (3.10), (3.21), (3.24), (B18)–(B20) and (3.29) that

$$\int_{-\infty}^{+\infty} \hat{u}_{\bar{\eta}} \mathrm{d}\bar{\eta} = -\frac{\pi}{\alpha_0} \operatorname{Re}\left(e_{01}^{(L)} A \mathrm{e}^{\mathrm{i}X}\right) - 2\pi \frac{U_{0\eta_c}}{c_0^3} \gamma_{2\zeta} \int_{-\infty}^{x_1} (x_1 - \xi)^2 |A(\xi)|^2 \mathrm{d}\xi + O(\sigma), \quad (4.2)$$

which, when combined with (1.19), (2.18) and (A 36), yields

$$b_{03}^+ - b_{03}^- = \mathrm{i} \, \pi \, a_{03}^{(L)}.$$
 (4.3)

In order to match with the X-independent term on the right-hand side of (4.2), a meanflow component must be included in the solution for the perturbation $\{\dot{u}, \dot{p}\}$. The 'steady' Rayleigh problem that governs this component outside the critical layer is given in appendix D where it is shown that the corresponding streamwise velocity is of the same order of magnitude as the instability wave that produced it and further that the slowly varying amplitude of this velocity component is given by

$$B = \int_{-\infty}^{x_1} (x_1 - \xi)^2 |A(\xi)|^2 \mathrm{d}\xi.$$
(4.4)

Again using (4.1), one can show from (B37) together with the definitions of α_1 and c_1

that

$$\frac{1}{\pi A} \int_{0}^{2\pi} \int_{-\infty}^{+\infty} \int_{0}^{2\pi/\beta} a_{00} e^{-iX} q d\zeta d\bar{\eta} dX = 2i \frac{U_{0\eta_c}}{\alpha_0} \left(I_R \frac{\alpha_1}{\alpha_0} + J_R \frac{c_1}{c_0} \right) + 3\pi \int_{0}^{2\pi/\beta} a_{00} \Phi_0 \left[\left(\frac{\alpha_1}{\alpha_0} - \frac{c_1 U_{0\eta\eta_c}}{U_{0\eta_c}^2} \right) a_{03}^{(L)} - a_{13}^{(L)} \right] d\zeta, \quad (4.5)$$

where

$$I_R \equiv -i\pi \int_0^{2\pi/\beta} \frac{\alpha_0^2 g_c^2}{\bar{g}_c U_{0\eta_c}} \left(\frac{\bar{g}_{\eta_c}}{\bar{g}_c} - 2\frac{g_{\eta_c}}{g_c} \right) a_{00}^2 d\zeta,$$
(4.6)

$$J_R \equiv -i \pi \int_0^{2\pi/\beta} \frac{c_0 a_{00}}{\bar{g}_c U_{0\eta_c}^2} \left[3 \left(\frac{\bar{g}_{\eta_c}}{\bar{g}_c} + \frac{U_{0\eta\eta_c}}{2U_{0\eta_c}} \right) a_{03}^{(L)} - \frac{\bar{g}_{\eta\eta_c}}{\bar{g}_c} a_{02} + \mathcal{D}_2 a_{00} \right] d\zeta, \qquad (4.7)$$

 $\bar{g} \equiv gU_{0\eta}/h$ and \mathcal{D}_2 is defined in appendix A. It now follows from (2.19), (3.11), (3.35), (3.36) and (4.3) that

$$\int_{0}^{2\pi/\beta} a_{00} \left[\frac{2c_{1} \Phi_{1}}{U_{0\eta_{c}}} (b_{03}^{+} - b_{03}^{-}) - \Phi_{0} (b_{13}^{+} - b_{13}^{-} - i\pi a_{13}^{(L)}) \right] d\zeta$$
$$= -\frac{2U_{0\eta_{c}}}{3\alpha_{0}} \left(I_{R} \frac{\alpha_{1}}{\alpha_{0}} + J_{R} \frac{c_{1}}{c_{0}} \right) + \frac{i}{3A} \int_{-\infty}^{+\infty} \tilde{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} d\bar{\eta}.$$
(4.8)

Using (3.42) and the results of appendix C, one can show that

$$\int_{-\infty}^{+\infty} \tilde{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} \mathrm{d}\bar{\eta} = \frac{\mathrm{i}\,\pi}{4c_0^5} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} K(x_1 \,|\, \xi_3, \xi_2) A(\xi_3) A(\xi_2) A^*(\xi_3 + \xi_2 - x_1) \mathrm{d}\xi_2 \mathrm{d}\xi_3, \qquad (4.9)$$

where

$$K \equiv (x_1 - \xi_3) [\nu_1 (x_1 - \xi_2) (\xi_3 - \xi_2) - \nu_2 (x_1 - \xi_3)^2 - \nu_3 (x_1 - \xi_2)^2], \qquad (4.10)$$

$$\nu_1 \equiv 4\alpha_0^2 U_{0\eta_c}^2 (k_3 + 2k_4 + k_5) = \int_0^{2\pi/\beta} \frac{g_c}{h_c} \left(\frac{a_{00\zeta}^2}{h_c^2} + \alpha_0^2 a_{00}^2 \right)_{\zeta}^2 \mathrm{d}\zeta, \tag{4.11}$$

$$\nu_2 \equiv -4\alpha_0^2 U_{0\eta_c}^2(k_3 - k_5) = -\int_0^{2\pi/\beta} \frac{g_c}{h_c} \left[\left(\frac{a_{00\zeta}^2}{h_c^2} \right)_{\zeta}^2 - \left(\alpha_0^2 a_{00}^2 \right)_{\zeta}^2 \right] \mathrm{d}\zeta, \qquad (4.12)$$

$$\nu_3 - \nu_1 \equiv -8\alpha_0^2 U_{0\eta_c}^2(k_1 + k_2) = -\int_0^{2\pi/\beta} \frac{2}{h_c} \left(\frac{g_c a_{00\zeta}^2}{h_c^2}\right)_{\zeta} \left(\frac{a_{00\zeta}^2}{h_c^2} + \alpha_0^2 a_{00}^2\right)_{\zeta} \mathrm{d}\zeta.$$
(4.13)

Combining (4.8) and (4.9) with the solvability condition (2.14) and using the result

$$\int_{0}^{2\pi/\beta} \Phi_{0}(a_{00}a_{13}^{(L)} - a_{03}^{(L)}a_{10}) \mathrm{d}\zeta = \left[\frac{\bar{h}_{\eta_{c}}}{3\alpha_{0}\bar{h}_{c}^{2}}(a_{00}a_{10\zeta} - a_{00\zeta}a_{10})\right]_{\zeta=0}^{2\pi/\beta} = 0$$
(4.14)

leads to the following amplitude-evolution equation

$$A' = \kappa A + i\mu \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_1} K(x_1 | \xi_1, \xi_2) A(\xi_1) A(\xi_2) A^*(\xi_1 + \xi_2 - x_1) d\xi_2 d\xi_1$$
(4.15)

where

$$\kappa \equiv \frac{i\alpha_0 J S_1}{(J-I)S_0},\tag{4.16}$$

$$\mu \equiv \frac{\pi \,\alpha_0^2}{8c_0^5 U_{0\eta_c}(J-I)},\tag{4.17}$$

$$I \equiv I_P + I_R = \int_0^{2\pi/\beta} \int_{y_0}^{\infty} \frac{\alpha_0^2 \hat{p}_0^2}{(U_0 - c_0)^2} g h d\eta d\zeta, \qquad (4.18)$$

$$J \equiv J_P + J_R = \int_0^{2\pi/\beta} \int_{y_0}^{\infty} \frac{c_0}{(U_0 - c_0)^3} \left(\nabla_T \hat{p}_0 \cdot \nabla_T \hat{p}_0 + \alpha_0^2 \hat{p}_0^2 \right) gh d\eta d\zeta,$$
(4.19)

and the η integration in (4.18) and (4.19) is performed along a contour in the complex- η plane that lies below the singularity at $\eta = \eta_c$.

Appendix A. Near-critical-level expansions

In this appendix, the near-critical-level expansions of $\{\hat{u}_m, \hat{p}_m\}$ are determined by first expressing (2.3) and (2.4) in terms of η and ζ . The resulting equations are

$$\hat{p}_{0\eta\eta} - \frac{\Pi}{\eta - \eta_c} \hat{p}_{0\eta} + \mathcal{D}\hat{p}_0 = 0,$$
 (A1)

and

$$\hat{p}_{1\eta\eta} - \frac{II}{\eta - \eta_c} \hat{p}_{1\eta} + \mathcal{D}\hat{p}_1 = 2\alpha_1 \Lambda \hat{p}_0 + 2c_1 \frac{\Omega}{(\eta - \eta_c)^2} \hat{p}_{0\eta}, \tag{A2}$$

where

$$\Pi \equiv (\eta - \eta_c) \frac{h}{g(U_0 - c_0)^2} \left[\frac{g(U_0 - c_0)^2}{h} \right]_{\eta} = \sum_{n=0}^{\infty} \Pi_n (\eta - \eta_c)^n,$$
(A3)

$$\mathcal{D}(\ \cdot\) \equiv \frac{g}{h} \frac{\partial}{\partial \zeta} \left[\frac{g}{h} \frac{\partial}{\partial \zeta} (\ \cdot\) \right] - \alpha_0^2 g^2 (\ \cdot\) = \sum_{n=0}^{\infty} \mathcal{D}_n (\ \cdot\) (\eta - \eta_c)^n, \tag{A4}$$

$$\Lambda \equiv \alpha_0 g^2 = \sum_{n=0}^{\infty} \Lambda_n (\eta - \eta_c)^n, \qquad (A5)$$

and

$$\Omega \equiv (\eta - \eta_c)^2 \frac{U_{0\eta}}{(U_0 - c_0)^2} = \sum_{n=0}^{\infty} \Omega_n (\eta - \eta_c)^n.$$
 (A6)

Expressions for \mathcal{D}_n and Λ_n are easily obtained from the Taylor series expansions of \mathcal{D} and Λ about $\eta = \eta_c$. The first few coefficients in the near-critical-level expansions of Π and Ω are

$$\Pi_{0} = 2, \quad \Pi_{1} = \frac{\bar{g}_{\eta_{c}}}{\bar{g}_{c}}, \quad \Pi_{2} = \left(\frac{\bar{g}_{\eta}}{\bar{g}}\right)_{\eta_{c}} - \frac{U_{0\eta\eta\eta_{c}}}{3U_{0\eta_{c}}} + \frac{U_{0\eta\eta_{c}}^{2}}{2U_{0\eta_{c}}^{2}}, \quad (A7)$$

and

$$\Omega_0 = \frac{1}{U_{0\eta_c}}, \quad \Omega_1 = 0, \quad \Omega_2 = \frac{U_{0\eta\eta\eta_c}}{6U_{0\eta_c}^2} - \frac{U_{0\eta\eta_c}^2}{4U_{0\eta_c}^3}, \tag{A8}$$

where $\bar{g} \equiv g U_{0\eta}/h$ and the *c* subscript denotes evaluation at $\eta = \eta_c$.

Substituting (2.12) and (2.13) into (A 1) and (A 2) and equating like powers of $\eta - \eta_c$ leads to

$$a_{m2} = \frac{1}{2} \mathcal{D}_0 a_{m0},\tag{A9}$$

$$a_{m3}^{(L)} = -\frac{1}{3}(\mathcal{D}_1 a_{m0} - 2\Pi_1 a_{m2}), \tag{A10}$$

$$a_{m4}^{(L)} = \frac{3}{4} \Pi_1 a_{m3}^{(L)}, \tag{A11}$$

$$a_{m4} = -\frac{1}{4} [\mathcal{D}_2 a_{m0} + (\mathcal{D}_0 - 2\Pi_2) a_{m2} - \Pi_1 a_{m3}^{(L)} + 5a_{m4}^{(L)}], \qquad (A\,12)$$

$$b_{m4}^{\pm} = \frac{3}{4} \Pi_1 b_{m3}^{\pm},\tag{A13}$$

and

$$d_{11} = -2c_1 \Omega_0 a_{02}, \tag{A14}$$

$$d_{12}^{(L)} = -3c_1 \Omega_0 a_{03}^{(L)}, \tag{A15}$$

$$d_{12}^{\pm} = -\alpha_1 \Lambda_0 a_{00} - c_1 \Omega_0 (a_{03}^{(L)} + 3b_{03}^{\pm}) - \frac{1}{2} (\Pi_1 d_{11} - d_{12}^{(L)}), \qquad (A\,16)$$

$$d_{13}^{(L)} = \frac{2}{3}\alpha_1 \Lambda_1 a_{00} + \frac{2}{3}c_1 [2\Omega_2 a_{02} + \Omega_0 (a_{04}^{(L)} + 4a_{04} + 4b_{04}^{\pm})] - \frac{1}{3} [(\mathcal{D}_0 - \Pi_2)d_{11} - \Pi_1 (d_{12}^{(L)} + 2d_{12}^{\pm})], \qquad (A\,17)$$

where m = 0, 1.

In view of (2.1), the shape functions corresponding to the normalized velocity components introduced in (2.17) should expand like

$$\{\hat{\bar{u}},\hat{\bar{v}},\hat{\bar{w}}\} = \{\hat{\bar{u}}_0,\hat{\bar{v}}_0,\hat{\bar{w}}_0\} + \sigma\{\hat{\bar{u}}_1,\hat{\bar{v}}_1,\hat{\bar{w}}_1\} + \cdots,$$
(A 18)

as $\sigma \to 0$. Substituting (A18) into (2.17) and the result together with (1.24), (1.25), (2.2) and (2.10) into (1.26) and (1.27) and equating like powers of σ leads to

$$i\alpha_0 \hat{\bar{u}}_0 + \hat{\bar{v}}_{0\eta} + \hat{\bar{w}}_{0\zeta} = 0,$$
 (A 19)

$$\mathrm{i}\alpha_0\hat{\bar{u}}_1 + \mathrm{i}\alpha_1\hat{\bar{u}}_0 + \hat{\bar{v}}_{1\eta} + \hat{\bar{w}}_{1\zeta} = 0, \qquad (A\,20)$$

and

$$\{\hat{v}_{0}, \hat{w}_{0}\} = \frac{i}{\eta - \eta_{c}} \{\Phi \hat{p}_{0\eta}, \Theta \hat{p}_{0\zeta}\},$$
(A 21)

$$\{\hat{\bar{v}}_{1},\hat{\bar{w}}_{1}\}=\frac{\mathrm{i}}{\eta-\eta_{c}}\{\Phi\hat{p}_{1\eta},\Theta\hat{p}_{1\zeta}\}-\left(\frac{\alpha_{1}}{\alpha_{0}}-c_{1}\frac{\Psi}{\eta-\eta_{c}}\right)\{\hat{\bar{v}}_{0},\hat{\bar{w}}_{0}\},\qquad(A\,22)$$

where

$$\Phi \equiv (\eta - \eta_c) \frac{h}{\alpha_0 g(U_0 - c_0)} = \sum_{n=0}^{\infty} \Phi_n (\eta - \eta_c)^n,$$
 (A 23)

$$\Theta \equiv (\eta - \eta_c) \frac{g}{\alpha_0 h(U_0 - c_0)} = \sum_{n=0}^{\infty} \Theta_n (\eta - \eta_c)^n, \qquad (A 24)$$

and

$$\Psi \equiv (\eta - \eta_c) \frac{1}{U_0 - c_0} = \sum_{n=0}^{\infty} \Psi_n (\eta - \eta_c)^n.$$
 (A 25)

The first few coefficients in the near-critical-level expansions of Φ , Θ and Ψ are

$$\begin{split} \Phi_{0} &= \frac{1}{\alpha_{0}\bar{g}_{c}}, \quad \Phi_{1} = \frac{1}{\alpha_{0}\bar{g}_{c}} \left(\frac{U_{0\eta\eta_{c}}}{2U_{0\eta_{c}}} - \frac{\bar{g}_{\eta_{c}}}{\bar{g}_{c}} \right), \\ \Phi_{2} &= \frac{1}{\alpha_{0}\bar{g}_{c}} \left(\frac{U_{0\eta\eta_{c}}}{3U_{0\eta_{c}}} - \frac{U_{0\eta\eta_{c}}^{2}}{4U_{0\eta_{c}}^{2}} - \frac{\bar{g}_{\eta\eta_{c}}}{2\bar{g}_{c}} - \frac{\bar{g}_{\eta_{c}}U_{0\eta\eta_{c}}}{2\bar{g}_{c}U_{0\eta_{c}}} + \frac{\bar{g}_{\eta_{c}}^{2}}{\bar{g}_{c}^{2}} \right), \quad (A 26) \\ \Theta_{0} &= \frac{1}{\alpha_{0}\bar{h}_{c}}, \quad \Theta_{1} = \frac{1}{\alpha_{0}\bar{h}_{c}} \left(\frac{U_{0\eta\eta_{c}}}{2U_{0\eta_{c}}} - \frac{\bar{h}_{\eta_{c}}}{\bar{h}_{c}} \right), \\ \Theta_{2} &= \frac{1}{\alpha_{0}\bar{h}_{c}} \left(\frac{U_{0\eta\eta\eta_{c}}}{3U_{0\eta_{c}}} - \frac{U_{0\eta\eta_{c}}^{2}}{4U_{0\eta_{c}}^{2}} - \frac{\bar{h}_{\eta\eta_{c}}}{2\bar{h}_{c}} - \frac{\bar{h}_{\eta_{c}}U_{0\eta\eta_{c}}}{2\bar{h}_{c}U_{0\eta_{c}}} + \frac{\bar{h}_{\eta_{c}}^{2}}{\bar{h}_{c}^{2}} \right), \quad (A 27) \end{split}$$

1 ---

and

$$\Psi_{0} = \frac{1}{U_{0\eta_{c}}}, \quad \Psi_{1} = -\frac{U_{0\eta\eta_{c}}}{2U_{0\eta_{c}}^{2}}, \quad \Psi_{2} = -\frac{U_{0\eta\eta_{c}}}{6U_{0\eta_{c}}^{2}} + \frac{U_{0\eta\eta_{c}}^{2}}{4U_{0\eta_{c}}^{3}}, \quad (A\,28)$$

where $\bar{h} \equiv h U_{0\eta}/g$. It turns out that $\hat{\bar{v}}_m$ and $\hat{\bar{w}}_m$ expand like

$$\hat{\bar{v}}_{0} = e_{00} + (e_{01}^{(L)} \ln |\eta - \eta_{c}| + e_{01}^{\pm})(\eta - \eta_{c}) + (e_{02}^{(L)} \ln |\eta - \eta_{c}| + e_{02}^{\pm})(\eta - \eta_{c})^{2}
+ O[(\eta - \eta_{c})^{3} \ln |\eta - \eta_{c}|],$$
(A 29)

$$\hat{\bar{v}}_{1} = e_{10}^{(L)} \ln |\eta - \eta_{c}| + e_{10}^{\pm} + (e_{11}^{(L)} \ln |\eta - \eta_{c}| + e_{11}^{\pm})(\eta - \eta_{c}) + O[(\eta - \eta_{c})^{2} \ln |\eta - \eta_{c}|], \quad (A 30)$$

and

$$\hat{\bar{w}}_0 = f_{0-1}(\eta - \eta_c)^{-1} + f_{00} + f_{01}(\eta - \eta_c) + O[(\eta - \eta_c)^2 \ln |\eta - \eta_c|], \quad (A 31)$$

$$\hat{\bar{w}}_1 = f_{1-2}(\eta - \eta_c)^{-2} + f_{1-1}(\eta - \eta_c)^{-1} + f_{10} + O[(\eta - \eta_c)\ln|\eta - \eta_c|],$$
(A 32)

as $\eta \to \eta_c$, where the coefficients e_{mn} and f_{mn} are at most functions of x_1 and ζ . It therefore follows from (A 19) and (A 20) that

$$\hat{\bar{u}}_{0} = i\alpha_{0}^{-1} [f_{0-1\zeta}(\eta - \eta_{c})^{-1} + e_{01}^{(L)} \ln |\eta - \eta_{c}| + e_{01}^{(L)} + e_{01}^{\pm} + f_{00\zeta} + (2e_{02}^{(L)} \ln |\eta - \eta_{c}| + e_{02}^{(L)} + 2e_{02}^{\pm} + f_{01\zeta})(\eta - \eta_{c})] + O[(\eta - \eta_{c})^{2} \ln |\eta - \eta_{c}|], \quad (A 33)$$

$$\hat{\bar{u}}_{1} = i\alpha_{0}^{-1} [f_{1-2\zeta}(\eta - \eta_{c})^{-2} + (e_{10}^{(L)} + f_{1-1\zeta} - \alpha_{1}\alpha_{0}^{-1}f_{0-1\zeta})(\eta - \eta_{c})^{-1} \\
+ (e_{11}^{(L)} - \alpha_{1}\alpha_{0}^{-1}e_{01}^{(L)})\ln|\eta - \eta_{c}| + e_{11}^{(L)} + e_{11}^{\pm} + f_{10\zeta} - \alpha_{1}\alpha_{0}^{-1}(e_{01}^{(L)} + e_{01}^{\pm} + f_{00\zeta})] \\
+ O[(\eta - \eta_{c})\ln|\eta - \eta_{c}|],$$
(A 34)

as $\eta \to \eta_c$.

Substituting (2.12), (2.13) and (A 29)–(A 32) into (A 21) and (A 22) and equating like powers of $\eta - \eta_c$ leads to

$$e_{00} = i2 \Phi_0 a_{02}, \tag{A35}$$

$$e_{01}^{(L)} = \mathrm{i}3\,\Phi_0 a_{03}^{(L)},\tag{A36}$$

$$e_{01}^{\pm} = \mathbf{i}[2\,\Phi_1 a_{02} + \Phi_0(a_{03}^{(L)} + 3b_{03}^{\pm})],\tag{A37}$$

$$e_{02}^{(L)} = i(3\Phi_1 a_{03}^{(L)} + 4\Phi_0 a_{04}^{(L)}), \tag{A38}$$

$$e_{02}^{\pm} = \mathbf{i}[2\Phi_2 a_{02} + \Phi_1(a_{03}^{(L)} + 3b_{03}^{\pm}) + \Phi_0(a_{04}^{(L)} + 4a_{04} + 4b_{04}^{\pm})], \tag{A39}$$

$$e_{10}^{(L)} = i2\Phi_0 d_{12}^{(L)} + c_1 \Psi_0 e_{01}^{(L)}, \tag{A40}$$

$$e_{10}^{\pm} = \mathbf{i}[\Phi_1 d_{11} + \Phi_0 (d_{12}^{(L)} + 2a_{12} + 2d_{12}^{\pm})] - \alpha_1 \alpha_0^{-1} e_{00} + c_1 (\Psi_1 e_{00} + \Psi_0 e_{01}^{\pm}), \quad (A\,41)$$

$$e_{11}^{(L)} = i[2\Phi_1 d_{12}^{(L)} + 3\Phi_0 (a_{13}^{(L)} + d_{13}^{(L)})] - \alpha_1 \alpha_0^{-1} e_{01}^{(L)} + c_1 (\Psi_1 e_{01}^{(L)} + \Psi_0 e_{02}^{(L)}), \qquad (A\,42)$$

$$e_{11}^{\pm} = i[\Phi_2 d_{11} + \Phi_1 (d_{12}^{(L)} + 2a_{12} + 2d_{12}^{\pm}) + \Phi_0 (a_{13}^{(L)} + d_{13}^{(L)} + +3b_{13}^{\pm})]$$

$$-\alpha_1 \alpha_0^{-1} e_{01}^{\pm} + c_1 (\Psi_2 e_{00} + \Psi_1 e_{01}^{\pm} + \Psi_0 e_{02}^{\pm}), \tag{A43}$$

$$f_{0-1} = \mathrm{i}\Theta_0 a_{00\zeta},\tag{A44}$$

$$f_{00} = \mathrm{i}\Theta_1 a_{00\zeta},\tag{A45}$$

$$f_{01} = i(\Theta_2 a_{00\zeta} + \Theta_0 a_{02\zeta}), \tag{A46}$$

and

$$f_{1-2} = c_1 \Psi_0 f_{0-1}, \tag{A47}$$

$$f_{1-1} = i\Theta_0 a_{10\zeta} - \alpha_1 \alpha_0^{-1} f_{0-1} + c_1 (\Psi_1 f_{0-1} + \Psi_0 f_{00}),$$
(A48)

$$f_{10} = i(\Theta_1 a_{10\zeta} + \Theta_0 d_{11\zeta}) - \alpha_1 \alpha_0^{-1} f_{00} + c_1(\Psi_2 f_{0-1} + \Psi_1 f_{00} + \Psi_0 f_{01}).$$
 (A 49)

Appendix B. Higher-order critical-layer problems

In this appendix, the higher-order critical-layer problems obtained by substituting (3.10)-(3.13) into (3.4)-(3.7) and equating like powers of σ are given. The order- σ problem reads

$$\alpha_0 \bar{u}_{1X} + \bar{u}_{0x_1} + \bar{v}_{1\bar{\eta}} + \bar{w}_{1\zeta} = 0, \tag{B1}$$

$$\mathcal{L}_{0}\bar{u}_{1} + \mathcal{L}_{1}\bar{u}_{0} + U_{0\eta_{c}}\left(\bar{v}_{1} + \frac{f_{\eta_{c}}}{\bar{f}_{c}}\bar{\eta}\bar{v}_{0}\right) + g_{c}h_{c}(\alpha_{0}p_{1X} + p_{0x_{1}}) + 2\alpha_{0}(gh)_{\eta_{c}}\bar{\eta}p_{0X} = -\psi_{1}, \quad (B2)$$

$$p_{1\bar{\eta}} = 0, \tag{B3}$$

$$\mathcal{L}_{0}\bar{w}_{1} + \mathcal{L}_{1}\bar{w}_{0} + \frac{g_{c}}{h_{c}}p_{1\zeta} + 2\frac{g_{\eta_{c}}}{h_{c}}\bar{\eta}p_{0\zeta} = -\theta_{1}, \qquad (B4)$$

where $\bar{f} \equiv gh U_{0\eta}$,

$$\mathcal{L}_{1} \equiv \frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\bar{\eta}\mathcal{L}_{0} + U_{0\eta_{c}}\bar{\eta}\frac{\partial}{\partial x_{1}} + \frac{1}{2}\alpha_{0}U_{0\eta\eta_{c}}\bar{\eta}^{2}\frac{\partial}{\partial X}, \tag{B5}$$

$$\psi_1 \equiv \alpha_0 \left(\frac{\bar{u}_0^2}{g_c h_c}\right)_X + \left(\frac{\bar{u}_0 \bar{v}_0}{g_c h_c}\right)_{\bar{\eta}} + \left(\frac{\bar{u}_0 \bar{w}_0}{g_c h_c}\right)_{\zeta}, \tag{B6}$$

$$\theta_1 \equiv \alpha_0 \left(\frac{\bar{u}_0 \bar{w}_0}{g_c h_c}\right)_X + \left(\frac{\bar{v}_0 \bar{w}_0}{g_c h_c}\right)_{\bar{\eta}} + \frac{1}{h_c} \left(\frac{\bar{w}_0^2}{g_c}\right)_{\zeta}.$$
 (B7)

It follows directly from (B3) and matching with the outer linear solution that

$$p_1 = \operatorname{Re}\left(a_{10}Ae^{iX}\right). \tag{B8}$$

It turns out that, for purposes of computing the velocity jump $\Delta \bar{u}$ across the critical layer, it is only necessary to know $\bar{u}_{1\bar{\eta}}$, $\bar{v}_{1\bar{\eta}\bar{\eta}}$ and \bar{w}_1 . Therefore (B1), (B2) and (B4) are rewritten as

$$\alpha_0 (\bar{u}_{1\bar{\eta}} - \bar{u}_{1\bar{\eta}}^{\dagger})_X + \bar{v}_{1\bar{\eta}\bar{\eta}} - \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + (\bar{w}_1 - \bar{w}_1^{\dagger})_{\bar{\eta}\zeta} = 0, \tag{B9}$$

$$\mathcal{L}_{0}(\bar{u}_{1\bar{\eta}} - \bar{u}_{1\bar{\eta}}^{\dagger}) = U_{0\eta_{c}}(\bar{w}_{1} - \bar{w}_{1}^{\dagger})_{\zeta} - \psi_{1\bar{\eta}}, \qquad (B\,10)$$

$$\mathcal{L}_0(\bar{w}_1 - \bar{w}_1^{\dagger}) = -\theta_1, \qquad (B\,11)$$

where $\bar{u}_{1\bar{\eta}}^{\dagger}, \, \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger}$ and \bar{w}_{1}^{\dagger} satisfy the linear equations

$$\alpha_0 \bar{u}_{1\bar{\eta}X}^{\dagger} + \bar{u}_{0x_1\bar{\eta}} + \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + \bar{w}_{1\bar{\eta}\zeta}^{\dagger} = 0, \qquad (B\,12)$$

$$\mathcal{L}_0 \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + \left(\frac{g_c}{h_c} \frac{\bar{h}_{\eta_c}}{\bar{h}_c} p_{0\zeta}\right)_{\zeta} + \alpha_0^2 g_c h_c \left(\frac{\bar{g}_{\eta_c}}{\bar{g}_c} - 2\frac{g_{\eta_c}}{g_c}\right) p_{0XX} = 0, \qquad (B\,13)$$

$$\mathcal{L}_0 \bar{w}_1^{\dagger} + \mathcal{L}_1 \bar{w}_0 + \frac{g_c}{h_c} p_{1\zeta} + 2 \frac{g_{\eta_c}}{h_c} \bar{\eta} p_{0\zeta} = 0, \qquad (B\,14)$$

and have the following large- $\bar{\eta}$ behavior

$$\{\bar{u}_{1\bar{\eta}}^{\dagger}, \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger}, \bar{w}_{1}^{\dagger}\} \sim \operatorname{Re}\left(\{\mathrm{i}e_{01}^{(L)}/\alpha_{0}\bar{\eta}, \mathrm{e}_{01}^{(L)}/\bar{\eta}, f_{00}\}A\mathrm{e}^{\mathrm{i}X}\right)$$
(B15)

which ensures that the solutions to (B9)-(B11) match with the outer linear solution as $\bar{\eta} \to \pm \infty$. By using (3.21) and (3.22) together with the relation

$$\mathcal{L}_{1}(\cdot) = \mathcal{L}_{0}[\mathcal{M}_{1}(\cdot)] - \left[\left(\frac{U_{0\eta_{c}}}{c_{0}} - \frac{U_{0\eta_{c}}}{2U_{0\eta_{c}}} \right) \bar{\eta} - \frac{S_{1}}{S_{0}} \right] \bar{\eta} \frac{\partial}{\partial \bar{\eta}} \mathcal{L}_{0}(\cdot), \quad (B \, 16)$$

where

$$\mathcal{M}_{1}(\cdot) \equiv \left[\left(\frac{U_{0\eta_{c}}}{c_{0}} - \frac{U_{0\eta_{c}}}{2U_{0\eta_{c}}} \right) \bar{\eta} - \frac{S_{1}}{S_{0}} \right] \bar{\eta} \frac{\partial}{\partial \bar{\eta}} (\cdot) + \frac{(ghU_{0})_{\eta_{c}}}{g_{c}h_{c}c_{0}} \bar{\eta} (\cdot), \qquad (B\,17)$$

it can be shown that

$$\alpha_0 \bar{u}_{1\bar{\eta}}^{\dagger} = (\bar{u}_{0x_1\bar{\eta}} + \bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + \bar{w}_{1\bar{\eta}\zeta}^{\dagger})_X, \tag{B18}$$

$$\bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} = \operatorname{Re}(\mathrm{i}\alpha_0 U_{0\eta_c} e_{01}^{(L)} E), \qquad (B\,19)$$

$$\bar{w}_1^{\dagger} = -\operatorname{Re}\left[\left(\mathrm{i}\alpha_0 U_{0\eta_c} f_{0-1} \mathcal{M}_1 + 2\frac{g_{\eta_c}}{h_c} a_{00\zeta} \bar{\eta} + \frac{g_c}{h_c} a_{10\zeta}\right) E\right].$$
(B20)

It follows from (B6), (B7) and (3.15)-(3.18) that

$$\psi_{1\bar{\eta}} = -\frac{\alpha_0}{U_{0\eta_c}} p_{0X} \bar{u}_{0\bar{\eta}\bar{\eta}} + \left(\frac{\bar{u}_0 \bar{w}_0}{g_c h_c}\right)_{\bar{\eta}\zeta} - \mathcal{L}_0 \left[\left(\frac{\bar{u}_0 \bar{u}_{0\bar{\eta}}}{\bar{f}_c}\right)_{\bar{\eta}} \right], \tag{B21}$$

$$\theta_{1} = \frac{1}{h_{c}^{2} U_{0\eta_{c}}} p_{0\zeta} \bar{u}_{0\bar{\eta}} - \frac{\alpha_{0}}{U_{0\eta_{c}}} p_{0X} \bar{w}_{0\bar{\eta}} + \frac{1}{h_{c}} \left(\frac{\bar{w}_{0}^{2}}{g_{c}}\right)_{\zeta} - \mathcal{L}_{0} \left[\left(\frac{\bar{u}_{0} \bar{w}_{0}}{\bar{f}_{c}}\right)_{\bar{\eta}} \right].$$
(B 22)

Combining these expressions with (B10), (B11), (3.21), (A35) and (A44) then leads to (3.26) and (3.27).

The order- σ^2 critical-layer problem reads

$$\alpha_0 \bar{u}_{2X} + \bar{u}_{1x_1} + \bar{v}_{2\bar{\eta}} + \bar{w}_{2\zeta} = 0, \tag{B23}$$

$$\mathcal{L}_{0}\bar{u}_{2} + \mathcal{L}_{1}\bar{u}_{1} + \mathcal{L}_{2}\bar{u}_{0} + U_{0\eta_{c}}\left(\bar{v}_{2} + \frac{\bar{f}_{\eta_{c}}}{\bar{f}_{c}}\bar{\eta}\bar{v}_{1} + \frac{\bar{f}_{\eta\eta_{c}}}{2\bar{f}_{c}}\bar{\eta}^{2}\bar{v}_{0}\right) + g_{c}h_{c}(\alpha_{0}p_{2X} + p_{1x_{1}}) + 2(gh)_{\eta_{c}}\bar{\eta}(\alpha_{0}p_{1X} + p_{0x_{1}}) + \frac{(g^{2}h^{2})_{\eta\eta_{c}}}{2g_{c}h_{c}}\bar{\eta}^{2}\alpha_{0}p_{0X} = -\psi_{2}, \quad (B\,24)$$

$$\frac{g_c}{h_c} \mathcal{L}_0 \bar{v}_0 + p_{2\bar{\eta}} = \frac{h_{\eta_c}}{g_c^2 h_c} \bar{w}_0^2, \tag{B25}$$

$$\mathcal{L}_{0}\bar{w}_{2} + \mathcal{L}_{1}\bar{w}_{1} + \mathcal{L}_{2}\bar{w}_{0} + \frac{g_{c}}{h_{c}}p_{2\zeta} + 2\frac{g_{\eta_{c}}}{h_{c}}\bar{\eta}p_{1\zeta} + \frac{(g^{2})_{\eta\eta_{c}}}{2g_{c}h_{c}}\bar{\eta}^{2}p_{0\zeta} = -\theta_{2}, \qquad (B\,26)$$

where

$$\mathcal{L}_{2} \equiv \left[\frac{(gh)_{\eta\eta_{c}}}{2g_{c}h_{c}} - \frac{(gh)_{\eta_{c}}^{2}}{g_{c}^{2}h_{c}^{2}}\right] \bar{\eta}^{2}\mathcal{L}_{0} + \frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\bar{\eta}\mathcal{L}_{1} + \frac{1}{2}U_{0\eta\eta_{c}}\bar{\eta}^{2}\frac{\partial}{\partial x_{1}} + \frac{1}{6}\alpha_{0}U_{0\eta\eta\eta_{c}}\bar{\eta}^{3}\frac{\partial}{\partial X}, \quad (B\,27)$$

$$\psi_{2} \equiv 2\alpha_{0} \left(\frac{\bar{u}_{0}\bar{u}_{1}}{g_{c}h_{c}}\right)_{X} + \left(\frac{\bar{u}_{1}\bar{v}_{0} + \bar{u}_{0}\bar{v}_{1}}{g_{c}h_{c}}\right)_{\bar{\eta}} + \left(\frac{\bar{u}_{1}\bar{w}_{0} + \bar{u}_{0}\bar{w}_{1}}{g_{c}h_{c}}\right)_{\zeta} + \left(\frac{\bar{u}_{0}^{2}}{g_{c}h_{c}}\right)_{x_{1}} - \frac{(gh)_{\eta_{c}}}{g_{c}^{2}h_{c}^{2}}\bar{u}_{0}\bar{v}_{0} - \frac{1}{g_{c}h_{c}}\left[\frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\right]_{\zeta}\bar{\eta}\bar{u}_{0}\bar{w}_{0}, \tag{B28}$$

$$\theta_{2} \equiv \alpha_{0} \left(\frac{\bar{u}_{0} \bar{w}_{1} + \bar{u}_{1} \bar{w}_{0}}{g_{c} h_{c}} \right)_{X} + \left(\frac{\bar{v}_{0} \bar{w}_{1} + \bar{v}_{1} \bar{w}_{0}}{g_{c} h_{c}} \right)_{\bar{\eta}} + \frac{2}{h_{c}} \left(\frac{\bar{w}_{0} \bar{w}_{1}}{g_{c}} \right)_{\zeta} \\ + \left(\frac{\bar{u}_{0} \bar{w}_{0}}{g_{c} h_{c}} \right)_{x_{1}} - \frac{1}{g_{c}^{2}} \left(\frac{g}{h} \right)_{\eta_{c}} \bar{v}_{0} \bar{w}_{0} - \frac{1}{g_{c} h_{c}} \left(\frac{g_{\eta_{c}}}{g_{c}} \right)_{\zeta} \bar{\eta} \bar{w}_{0}^{2}.$$
(B 29)

Fortunately, only the solution for $\bar{v}_{2\bar{\eta}\bar{\eta}}$ is needed in determining the governing equation for $A(x_1)$. Therefore the above equations are combined to give

$$\mathcal{L}_{0}(\bar{v}_{2\bar{\eta}\bar{\eta}} - \bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger}) = \left[\alpha_{0}\psi_{2X} + \psi_{1x_{1}} + \theta_{2\zeta} + \mathcal{L}_{1\zeta}(\bar{w}_{1} - \bar{w}_{1}^{\dagger})\right]_{\bar{\eta}} - \left[\mathcal{L}_{1}\frac{\partial^{2}}{\partial\bar{\eta}^{2}} + \frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\mathcal{L}_{0}\frac{\partial}{\partial\bar{\eta}} - \alpha_{0}\frac{\bar{f}_{\eta_{c}}}{\bar{f}_{c}}U_{0\eta_{c}}\frac{\partial}{\partial X}\right](\bar{v}_{1} - \bar{v}_{1}^{\dagger}) + \bar{\mathcal{D}}\left(\frac{h_{\eta_{c}}\bar{w}_{0}^{2}}{g_{c}^{2}h_{c}}\right) \quad (B\,30)$$

where

$$\bar{\mathcal{D}} \equiv \frac{\partial}{\partial \zeta} \left(\frac{g_c}{h_c} \frac{\partial}{\partial \zeta} \right) + \alpha_0^2 g_c h_c \frac{\partial^2}{\partial X^2}, \tag{B31}$$

and $ar{v}^{\dagger}_{2ar{\eta}ar{\eta}}$ is determined by the linear equation

$$\mathcal{L}_{0}\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} + \mathcal{L}_{1}\bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + \frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\mathcal{L}_{0}\bar{v}_{1\bar{\eta}}^{\dagger} - \frac{\bar{f}_{\eta_{c}}}{\bar{f}_{c}}U_{0\eta_{c}}(\alpha_{0}\bar{v}_{1X}^{\dagger} + \bar{v}_{0x_{1}}) - (\mathcal{L}_{1\zeta}\bar{w}_{1}^{\dagger} + \mathcal{L}_{2\zeta}\bar{w}_{0})_{\bar{\eta}} + \bar{\mathcal{D}}\left(\frac{g_{c}}{h_{c}}\mathcal{L}_{0}\bar{v}_{0}\right) - \bar{\eta}\left\{\alpha_{0}\frac{\bar{f}_{\eta\eta_{c}}}{\bar{f}_{c}}U_{0\eta_{c}}\bar{v}_{0X} + \left[\frac{(g^{2})_{\eta\eta_{c}}}{g_{c}h_{c}}p_{0\zeta}\right]_{\zeta} + \alpha_{0}^{2}\frac{(g^{2}h^{2})_{\eta\eta_{c}}}{g_{c}h_{c}}p_{0XX}\right\} - 4\alpha_{0}(gh)_{\eta_{c}}p_{0x_{1}X} - 2\left[\left(\frac{g_{\eta_{c}}}{h_{c}}p_{1\zeta}\right)_{\zeta} + \alpha_{0}^{2}(gh)_{\eta_{c}}p_{1XX}\right] = 0, \qquad (B 32)$$

together with the boundary condition

$$\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} \to \operatorname{Re}[(2e_{02}^{(L)}\ln|\sigma\bar{\eta}| + 3e_{02}^{(L)} + 2e_{02}^{\pm} + e_{11}^{(L)}/\bar{\eta})Ae^{iX}] \quad \text{as} \quad \bar{\eta} \to \pm\infty$$
(B33)

which ensures that the solution to (B30) matches with the outer linear solution. By manipulating (3.15)-(3.18) and (B1)-(B4), one can show that

$$U_{0\eta_{c}}(\alpha_{0}\bar{v}_{1X}^{\dagger} + \bar{v}_{0x_{1}}) = \mathcal{L}_{0}\bar{v}_{1\bar{\eta}}^{\dagger} - \bar{\eta} \left(\alpha_{0} \frac{\bar{f}_{\eta_{c}}}{\bar{f}_{c}} U_{0\eta_{c}} \bar{v}_{0X} + \frac{h_{c}}{g_{c}} \mathcal{D}_{1} p_{0} + 2 \frac{h_{\eta_{c}}}{g_{c}} \mathcal{D}_{0} p_{0} \right) - 2\alpha_{0} g_{c} h_{c} p_{0x_{1}X} - \frac{h_{c}}{g_{c}} \mathcal{D}_{0} p_{1}$$
(B 34)

 \mathbf{and}

$$\left(\mathcal{L}_{1\zeta}\bar{w}_{1}^{\dagger} + \mathcal{L}_{2\zeta}\bar{w}_{0}\right)_{\bar{\eta}} = -\left[\frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\right]_{\zeta} \left[2\bar{\eta}\left(\frac{g}{h}\right)_{\eta_{c}}p_{0\zeta} + \frac{g_{c}}{h_{c}}p_{1\zeta}\right] - \bar{\eta}\left[\frac{(gh)_{\eta\eta_{c}}}{g_{c}h_{c}}\right]_{\zeta}\frac{g_{c}}{h_{c}}p_{0\zeta} \quad (B\,35)$$

where the \mathcal{D}_n are defined in appendix A. Combining these results with (3.21), (B8), (B16) and (B19) then leads to

$$\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} = -\left[\mathcal{M}_{1} + \left(\frac{\bar{g}_{\eta_{c}}}{\bar{g}_{c}} - 2\frac{h_{\eta_{c}}}{h_{c}}\right)\bar{\eta}\right]\bar{v}_{1\bar{\eta}\bar{\eta}}^{\dagger} + \frac{U_{0\eta\eta_{c}}}{U_{0\eta_{c}}}\bar{v}_{1\bar{\eta}}^{\dagger} - \operatorname{Re}\left(\mathrm{i}2\,\varPhi_{0}\mathcal{D}_{0}a_{02}A\mathrm{e}^{\mathrm{i}X}\right) - \operatorname{Re}\left\{2\frac{h_{c}}{g_{c}}\left[\mathrm{i}\alpha_{0}\left(\frac{\bar{g}_{\eta_{c}}}{\bar{g}_{c}} - 2\frac{g_{\eta_{c}}}{g_{c}}\right)g_{c}^{2}a_{00}\frac{\partial}{\partial x_{1}} + \frac{\bar{g}_{\eta\eta_{c}}}{\bar{g}_{c}}a_{02}\bar{\eta} - \mathcal{D}_{2}a_{00}\bar{\eta} + \frac{3}{2}a_{13}^{(L)}\right]E\right\}.$$
 (B 36)

For purposes of computing the induced velocity jump, it is convenient to express (B 36) as

$$q \equiv \bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} - \frac{U_{0\eta\eta_c}}{U_{0\eta_c}} \bar{v}_{1\bar{\eta}}^{\dagger} - \operatorname{Re} \left[\left(e_{02}^{(L)} + 2e_{02}^{\pm} - \frac{U_{0\eta\eta_c}}{U_{0\eta_c}} e_{01}^{\pm} \right) A e^{iX} \right] \\ = -\operatorname{Re} \left\{ 3\frac{h_c}{g_c} \left[a_{13}^{(L)} - \frac{S_1}{S_0} a_{03}^{(L)} + i\frac{2}{3} \alpha_0 \left(\frac{\bar{g}_{\bar{\eta}_c}}{\bar{g}_c} - 2\frac{g_{\eta_c}}{g_c} \right) g_c^2 a_{00} \frac{\partial}{\partial x_1} \right] E \right\} \\ - \operatorname{Re} \left\{ 2\frac{h_c}{g_c} \left[3 \left(\frac{U_{0\eta_c}}{2c_0} - \frac{\bar{g}_{\bar{\eta}_c}}{\bar{g}_c} \right) a_{03}^{(L)} + \frac{\bar{g}_{\bar{\eta}\bar{\eta}_c}}{\bar{g}_c} a_{02} - \mathcal{D}_2 a_{00} \right] \bar{L}E \right\} \\ + \operatorname{Re} \left\{ 3\frac{h_c}{g_c} a_{03}^{(L)} \left[\left(\frac{U_{0\eta_c}}{c_0} - \frac{U_{0\eta\eta_c}}{2U_{0\eta_c}} \right) \bar{L} - \frac{S_1}{S_0} \right] \bar{L}E_{\bar{\eta}} \right\}$$
(B 37)

where

$$\bar{\mathbf{L}} \equiv \frac{1}{\mathrm{i}\alpha_0 U_{0\eta_c}} \left(\mathrm{i}S_1 - c_0 \frac{\partial}{\partial x_1} \right), \qquad (B\,38)$$

and (3.22) and (B19) were used in arriving at (B37).

It follows from (B28), (B29), (3.15)-(3.18) and (B9)-(B11) that

$$\begin{aligned} (\alpha_{0}\psi_{2X} + \theta_{2\zeta})_{\bar{\eta}} &= -\frac{\alpha_{0}^{2}}{U_{0\eta_{c}}} (p_{0X}\bar{u}_{1\bar{\eta}\bar{\eta}}^{\dagger})_{X} - \frac{1}{U_{0\eta_{c}}} \left(\frac{p_{0\zeta}\bar{u}_{1\bar{\eta}\bar{\eta}}^{\dagger}}{h_{c}^{2}}\right)_{\zeta} - \frac{\alpha_{0}}{U_{0\eta_{c}}} \left(p_{0X}\bar{w}_{1\bar{\eta}\bar{\eta}}^{\dagger}\right)_{\zeta} \\ &+ \left[\frac{1}{h_{c}} \left(2\frac{\bar{w}_{0}\bar{w}_{1}^{\dagger}}{g_{c}} + \frac{\bar{u}_{0\bar{\eta}}\bar{w}_{0}^{2}}{g_{c}\bar{f}_{c}}\right)_{\bar{\eta}\zeta}\right]_{\zeta} + (\alpha_{0}\psi_{2X}^{\dagger} + \theta_{2\zeta}^{\dagger})_{\bar{\eta}} \\ &- \mathcal{L}_{0} \left\{\alpha_{0} \left[\frac{\bar{u}_{0}\bar{u}_{1}^{\dagger}}{\bar{f}_{c}} + \left(\frac{\bar{u}_{0}^{3}}{6\bar{f}_{c}^{2}}\right)_{\bar{\eta}}\right]_{X} + \left[\frac{\bar{u}_{0}\bar{w}_{1}^{\dagger} + \bar{u}_{1}^{\dagger}\bar{w}_{0}}{\bar{f}_{c}} + \left(\frac{\bar{u}_{0}^{2}\bar{w}_{0}}{2\bar{f}_{c}^{2}}\right)_{\bar{\eta}}\right]_{\zeta}\right\}_{\bar{\eta}\bar{\eta}} \end{aligned} \tag{B 39}$$

where ψ_2^{\dagger} and θ_2^{\dagger} are given by the right-hand sides of (B28) and (B29), respectively, but with $\{\bar{u}_1, \bar{v}_1, \bar{w}_1\}$ replaced by $\{\bar{u}_1^{\dagger}, \bar{v}_1^{\dagger}, \bar{w}_1^{\dagger}\}$. Introducing the above relation into (B30) leads to

$$\mathcal{L}_{0}\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger} = -\frac{\alpha_{0}^{2}}{U_{0\eta_{c}}}(p_{0X}\bar{u}_{1\bar{\eta}\bar{\eta}}^{\dagger})_{X} - \frac{1}{U_{0\eta_{c}}}\left(\frac{p_{0\zeta}\bar{u}_{1\bar{\eta}\bar{\eta}}^{\dagger}}{h_{c}^{2}}\right)_{\zeta} - \frac{\alpha_{0}}{U_{0\eta_{c}}}(p_{0X}\bar{w}_{1\bar{\eta}\bar{\eta}}^{\dagger})_{\zeta} \\ + \left[\frac{1}{h_{c}}\left(2\frac{\bar{w}_{0}\bar{w}_{1}^{\dagger}}{g_{c}} + \frac{\bar{u}_{0\bar{\eta}}\bar{w}_{0}^{2}}{g_{c}\bar{f}_{c}}\right)_{\bar{\eta}\zeta}\right]_{\zeta} + \left[\alpha_{0}\psi_{2X}^{\dagger} + \psi_{1x_{1}} + \theta_{2\zeta}^{\dagger} + \mathcal{L}_{1\zeta}(\bar{w}_{1} - \bar{w}_{1}^{\dagger})\right]_{\bar{\eta}} \\ - \left[\mathcal{L}_{1}\frac{\partial^{2}}{\partial\bar{\eta}^{2}} + \frac{(gh)_{\eta_{c}}}{g_{c}h_{c}}\mathcal{L}_{0}\frac{\partial}{\partial\bar{\eta}} - \alpha_{0}\frac{\bar{f}_{\eta_{c}}}{\bar{f}_{c}}U_{0\eta_{c}}\frac{\partial}{\partial X}\right](\bar{v}_{1} - \bar{v}_{1}^{\dagger}) + \bar{\mathcal{D}}\left(\frac{h_{\eta_{c}}\bar{w}_{0}^{2}}{g_{c}^{2}h_{c}}\right)$$
(B 40)

where $\bar{v}_{2\bar{\eta}\bar{\eta}}^{\dagger}$ is given by (3.35). Substituting (3.21), (3.29) and (3.30) into (B 40), multiplying the result by $a_{00}e^{-iX}/\pi$, and integrating from $\zeta = 0$ to $2\pi/\beta$ then using the relations

$$[2\alpha_0 U_{0\eta_c} \operatorname{Re}(E) \operatorname{Re}(F_X)]_{X\bar{\eta}} = \operatorname{Re}\left(A e^{iX}\right) [\operatorname{Re}(F_X) + \operatorname{Re}(E) \operatorname{Re}(iE_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}} + \operatorname{Re}\left(iA e^{iX}\right) [\operatorname{Re}(E) \operatorname{Re}(E_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}} - \mathcal{L}_0[\operatorname{Re}(E) \operatorname{Re}(F_X)]_{\bar{\eta}\bar{\eta}}, \quad (B\,41)$$

$$[2\alpha_0 U_{0\eta_c} \operatorname{Re}(E) \operatorname{Re}(\mathrm{i}F)]_{X\bar{\eta}} = \operatorname{Re}\left(A \mathrm{e}^{\mathrm{i}X}\right) [\operatorname{Re}(\mathrm{i}F)]_{\bar{\eta}\bar{\eta}} + \operatorname{Re}\left(\mathrm{i}A \mathrm{e}^{\mathrm{i}X}\right) [\operatorname{Re}(E) \operatorname{Re}(E_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}} - \mathcal{L}_0[\operatorname{Re}(E) \operatorname{Re}(\mathrm{i}F)]_{\bar{\eta}\bar{\eta}}, \qquad (B\,42)$$

$$\begin{aligned} &[\alpha_0 U_{0\eta_c} \operatorname{Re}(E)^2 \operatorname{Re}(\mathrm{i}E_{\bar{\eta}})]_{XX\bar{\eta}} = \operatorname{Re}\left(A\mathrm{e}^{\mathrm{i}X}\right) [\operatorname{Re}(\mathrm{i}E)\operatorname{Re}(\mathrm{i}E_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}} \\ &+ \operatorname{Re}\left(\mathrm{i}A\mathrm{e}^{\mathrm{i}X}\right) [\operatorname{Re}(E)\operatorname{Re}(\mathrm{i}E_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}} - \mathcal{L}_0[\operatorname{Re}(E)\operatorname{Re}(\mathrm{i}E)\operatorname{Re}(\mathrm{i}E_{\bar{\eta}})]_{\bar{\eta}\bar{\eta}}, \quad (B\,43) \end{aligned}$$

and integrating from X = 0 to 2π leads to (3.37).

Appendix C. Expressions for the Q_n

The solutions to (3.43)-(3.45) are

$$Q_1 = -i\frac{M}{2} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_2} (\xi_2 - \xi_1)^3 C_1(x_1, \bar{\eta} \,|\, \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3, \tag{C1}$$

$$Q_2 = i\frac{M}{2} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_2} (\xi_2 - \xi_1)^3 C_2(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3,$$
(C2)

$$Q_3 = i\frac{M}{2} \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_2} (\xi_2 - \xi_1)^2 (2\xi_3 - \xi_1 - \xi_2) C_3(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3, \quad (C3)$$

$$Q_{4} = iM \int_{-\infty}^{x_{1}} \int_{-\infty}^{\xi_{3}} \int_{-\infty}^{\xi_{2}} (\xi_{3} - \xi_{2})(\xi_{2} - \xi_{1})^{2} [C_{1}(x_{1}, \bar{\eta} | \xi_{3}, \xi_{2}, \xi_{1}) - C_{2}(x_{1}, \bar{\eta} | \xi_{3}, \xi_{2}, \xi_{1})] d\xi_{1} d\xi_{2} d\xi_{3}, \quad (C4)$$

$$Q_{5} = -iM \int_{-\infty}^{x_{1}} \int_{-\infty}^{\xi_{3}} \int_{-\infty}^{\xi_{3}} (\xi_{2} - \xi_{1}) [(\xi_{3} - \xi_{2})^{2} + (\xi_{3} - \xi_{1})^{2}] C_{1}(x_{1}, \bar{\eta} | \xi_{3}, \xi_{2}, \xi_{1}) d\xi_{1} d\xi_{2} d\xi_{3}, \quad (C5)$$

$$Q_6 = iM \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_3} (\xi_3 - \xi_1)^2 (2\xi_3 - \xi_2 - \xi_1) C_3(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3, \quad (C 6)$$

$$Q_7 = -iM \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_3} (\xi_3 - \xi_1)(\xi_2 - \xi_1)^2 C_1(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3,$$
(C7)

$$Q_8 = iM \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_3} (\xi_3 - \xi_2)(\xi_2 - \xi_1)^2 C_1(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3, \quad (C8)$$

and

$$Q_9 = iM \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \int_{-\infty}^{\xi_3} (\xi_3 - \xi_1) (2\xi_3 - \xi_2 - \xi_1)^2 C_3(x_1, \bar{\eta} \mid \xi_3, \xi_2, \xi_1) d\xi_1 d\xi_2 d\xi_3, \quad (C9)$$

where

$$C_1 \equiv A(\xi_3) A(\xi_2) A^*(\xi_1) e^{i\bar{Y}(\xi_3 + \xi_2 - \xi_1 - x_1)},$$
(C10)

$$C_2 \equiv A(\xi_3) A^*(\xi_2) A(\xi_1) e^{i\bar{Y}(\xi_3 - \xi_2 + \xi_1 - x_1)},$$
(C11)

$$C_3 \equiv A^*(\xi_3) A(\xi_2) A(\xi_1) e^{i\bar{Y}(-\xi_3 + \xi_2 + \xi_1 - x_1)},$$
(C12)

and $M \equiv \alpha_0^3 U_{0 \eta_c}^3 / 2c_0^6$.

By using (4.1), one can show that

$$\int_{-\infty}^{+\infty} Q_1 d\bar{\eta} = -iN \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} \frac{1}{2} (x_1 - \xi_3)^3 D(x_1 | \xi_3, \xi_2) d\xi_2 d\xi_3,$$
(C13)

$$\int_{-\infty}^{+\infty} Q_4 d\bar{\eta} = \int_{-\infty}^{+\infty} Q_8 d\bar{\eta} = iN \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} (x_1 - \xi_3)^2 (\xi_3 - \xi_2) D(x_1 | \xi_3, \xi_2) d\xi_2 d\xi_3, \quad (C\,14)$$

$$\int_{-\infty}^{+\infty} Q_5 d\bar{\eta} = -iN \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} (x_1 - \xi_3) [(x_1 - \xi_2)^2 + (\xi_3 - \xi_2)^2] D(x_1 | \xi_3, \xi_2) d\xi_2 d\xi_3, \quad (C15)$$

$$\int_{-\infty}^{+\infty} Q_7 d\bar{\eta} = -iN \int_{-\infty}^{x_1} \int_{-\infty}^{\xi_3} (x_1 - \xi_3)^2 (x_1 - \xi_2) D(x_1 | \xi_3, \xi_2) d\xi_2 d\xi_3,$$
(C16)

and

$$\int_{-\infty}^{+\infty} Q_2 d\bar{\eta} = \int_{-\infty}^{+\infty} Q_3 d\bar{\eta} = \int_{-\infty}^{+\infty} Q_6 d\bar{\eta} = \int_{-\infty}^{+\infty} Q_9 d\bar{\eta} = 0, \quad (C17)$$

where

$$D \equiv A(\xi_3)A(\xi_2)A^*(\xi_3 + \xi_2 - x_1), \tag{C18}$$

and $N \equiv \pi \alpha_0^2 U_{0 \eta_c}^2 / c_0^5$.

Appendix D. Mean-flow distortion

In this appendix, the solution for the mean-flow distortion generated by the criticallayer nonlinearity is analyzed. When the mean-flow distortion terms are made explicit in (1.19) and (1.20), these equations become

$$\dot{u} = \operatorname{Re}\left(A\hat{u}e^{iX}\right) + \operatorname{Re}\left(iB\frac{\check{u}}{gh} + l\sigma B'\frac{\check{v}}{h} + m\sigma B'\frac{\check{w}}{g}\right) + \dots,$$
(D1)

$$\dot{p} = \operatorname{Re}\left(A\hat{p}e^{iX}\right) + \operatorname{Re}(\sigma^2 B''\check{p}) + \dots,$$
(D2)

where $B(x_1)$ is a slowly varying amplitude function and the functions \tilde{u} , \tilde{v} , \tilde{w} and \check{p} of x_1 , y and z expand like

$$\{ \tilde{u}, \tilde{v}, \tilde{w}, \tilde{p} \} = \{ \tilde{u}_0, \tilde{v}_0, \tilde{w}_0, \tilde{p}_0 \} (y, z) + \cdots,$$
 (D 3)

as $\sigma \to 0$. Substituting (D1)-(D3) into (1.15)-(1.17) shows that \check{p}_0 satisfies the 'steady' Rayleigh equation

$$\nabla_T \cdot \left(\frac{\nabla_T \check{p}_0}{U_0^2}\right) = 0, \tag{D4}$$

while the velocity fluctuations are determined in terms of \check{p}_0 by

$$\{\check{u}_{0},\check{v}_{0},\check{w}_{0}\} = \frac{1}{U_{0}} \left\{ \frac{hU_{0\eta}}{gU_{0}}\check{p}_{0\eta}, -\frac{h}{g}\check{p}_{0\eta}, -\frac{g}{h}\check{p}_{0\zeta} \right\}.$$
 (D 5)

Near the critical level, \check{p}_0 expands like

$$\check{p}_0 = r_{00} + r_{01}^{\pm} (\eta - \eta_c) + \cdots$$
 (D 6)

where (3.21), (B 8) and (B 25) have been used to conclude that the mean pressure fluctuation is continuous across the critical layer to $O(\sigma^2 \epsilon)$. It follows from (D 5) that the discontinuity in (D 6) leads to a jump in the streamwise velocity component

$$\Delta \check{\bar{u}}_0 = \frac{h_c U_{0\eta_c}}{g_c c_0^2} (r_{01}^+ - r_{01}^-) \tag{D7}$$

across the critical layer. Matching this jump with (4.2) yields

$$r_{01}^{+} - \bar{r_{01}} = -2\pi \frac{g_c \gamma_{2\zeta}}{h_c c_0},$$
 (D8)

and the amplitude equation (4.4).

REFERENCES

- BENNEY, D. J. & BERGERON, R. F. 1969 A new class of nonlinear waves in parallel flows. Stud. Appl. Math. 48, 181-204.
- GOLDSTEIN, M. E. 1976 Aeroacoustics. McGraw-Hill.
- GOLDSTEIN, M. E. & CHOI, S. W. 1989 Nonlinear evolution of interacting oblique waves on two-dimensional shear layers. J. Fluid Mech. 207, 97-120. Also Corrigendum, J. Fluid Mech. 216, 659-663.
- GOLDSTEIN, M. E. & WUNDROW, D. W. 1994 Interaction of oblique instability waves with weak streamwise vortices. To appear in *J. Fluid Mech.*
- HALL, P. & HORSEMAN, N. J. 1991 The linear inviscid secondary instability of longitudinal vortex structures in boundary layers. J. Fluid Mech. 232, 357-375.
- HALL, P. & SMITH, F.T. 1991 On strongly nonlinear vortex/wave interactions in boundary-layer transition. J. Fluid Mech. 227, 641-666.

- HENNINGSON, D. S. 1987 Stability of parallel inviscid shear flow with mean spanwise variation. The Aeronautical Research Institute of Sweden, Aerodynamics Department. FFA TN 1987-57.
- HORSEMAN, N.J. 1991 Some centrifugal instabilities in viscous flows. PhD thesis, Exeter University.
- RUDMAN, S. & RUBIN, S. G. 1968 Hypersonic viscous flow over slender bodies with sharp leading edges. AIAA J. 6(10), 1883-1890.

Phile Registry is the first first and advances is entitleased to average 1 for a weakers. Becademine 3 and and advances are advanced to a strengthy in a local strengthy in local stren	REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
1. AGENCY USE ONLY (Lown blumb) 2. REPORT DATE 5. REPORT TYPE AND DATES COVERED November 1994 Technical Memorandum 4. TITLE AND SUBTITLE S. FUNDING NUMBERS Nonlinear Instability of a Uni-directional Transversely Sheared Mean Flow S. FUNDING NUMBERS 6. AUTHOR(S) WU-505-90-51 David W. Wundrow and Marvin E. Goldstein WU-505-90-51 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration E-9232 Levis Research Center E-9232 Cleveland, Ohio 44135-3191 E-9232 10. SPONSORINGAMONTORING AGENCY NAME(S) AND ADDRESS(ES) NASA TM-106779 National Aeronautics and Space Administration NASA TM-106779 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Enginecring Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-252(6), and Marvin E. Goldstein, NASA Lewis Research Center. Nasa TM-106779 12. DISTRIBUTION AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE 12. DISTRIBUTION WALLABILITY STATEMENT 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) 11 is well known that the presence of a weak cross flow in an	Public reporting burden for this collection o gathering and maintaining the data needed collection of information, including suggesti Davis Highway, Suite 1204, Arlington, VA	I information is estimated to average 1 hour pe , and completing and reviewing the collection of ons for reducing this burden, to Washington He 22202-4302, and to the Office of Management	r response, including the time for re f information. Send comments rega adquarters Services, Directorate for and Budget, Paperwork Reduction F	viewing instructions, searching existing data sources, rding this burden estimate or any other aspect of this Information Operations and Reports, 1215 Jefferson Project (0704-0188), Washington, DC 20503.	
NTLE AND SUBTITLE Nonlinear Instability of a Uni-directional Transversely Sheared Mean Flow Fehnical Memorandum a. AUTHOR(S) David W. Wundrow and Marvin E. Goldstein WU-505-90-51 David W. Wundrow and Marvin E. Goldstein Report Mumber Report Mumber 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Report Mumber Report Mumber National Aeronautics and Space Administration E-9232 Report Mumber 1. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NASA-2525(6), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 10. SITHBUTION CODE 12. DISTRIBUTIONAVALABILITY STATEMENT 12b. DISTRIBUTION CODE 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamistic velocity profile that can lead to an amplification of certain three-dimensional distur- barces through a kind of resonant-Interaction mechanism. (Goldstein and Wundrow 1994). The spatial distur- barces through a teation of viscosity. This decay, which coincides with the viscous spread of of the spatibility wave will ocetain a spanwise velocity on an otherwise two-dimensional shear flow as one fined streamy we can use the wave propagates downstream. Nonline effects can then become im	1. AGENCY USE ONLY (Leave blan	nk) 2. REPORT DATE	3. REPORT TYPE AN	D DATES COVERED	
4. TITLE AND SUBTITLE 5. FUNDING NUMBERS Nonlinear Instability of a Uni-directional Transversely Sheared Mean Flow 5. FUNDING NUMBERS 6. AUTHOR(S) WU-505-90-51 David W. Wundrow and Marvin E. Goldstein WU-505-90-51 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) a. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration E-9232 10. SPONSORING/MONTORING AGENCY MAME(S) AND ADDRESS(ES) 10. SPONSORING/MONTORING AGENCY MAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration NASA TM-106779 11. SUPPLEMENTARY MOTES NASA TM-106779 David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12a. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 12b. DISTRIBUTION CODE 11 swell known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbance finder group on an otherwise two-dimensional shear flow stress in initially ling a spanwise-wise velocity on an otherwise two-dimensional shear flow results in a spanwise velocity on an otherwise two-dimensional shear flow results in a spanwise v		November 1994	Te	chnical Memorandum	
Nonlinear Instability of a Uni-directional Transversely Sheared Mean Flow a. AUTHOR(5) David W. Wundrow and Marvin E. Goldstein 7. PERFORMING ORGANIZATION NAME(5) AND ADDRESS(ES) National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135–3191 a. SPONSORING/MONITORING AGENCY NAME(5) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, D.C. 20546–0001 11. SUPPLEMENTARY NOTES David W. Wundrow NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3–32566), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12a. DISTRIBUTIONAVALABULTY STATEMENT Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) 14. Bertard Marking Action relation mechanism. (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such as panwise-verying shear (Mov is considered. The base flow, which is governed by the three-dimensional probolized Navier-Stexter equitons, is in distance and prown hat of the instability wave will centanisg streamwise distance, raches a maximum and eventually decays through the action of viscosity. This decay, which coinclose with the viscous spread of of the shear Hayer. 14. SUBJECT TEMMS 15. NUMBER OF PAGES <u>AGENT Proversion </u>	4. TITLE AND SUBTITLE			5. FUNDING NUMBERS	
a. AUTHOR(S) WU-505-90-51 David W. Wundrow and Marvin E. Goldstein WU-505-90-51 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) a. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration E-9232 2. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) i. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, D.C. 20546-0001 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12a. DISTRIBUTION/AMALABILITY STATEMENT 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) 11. Sevent Hard Wordrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered, The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional shear flow is considered. The base flow, which is governe	Nonlinear Instability of a	Uni-directional Transversely She	eared Mean Flow		
David W. Wundrow and Marvin E. Goldstein 7. PERFORMING ORGANIZATION NAME(9) AND ADDRESS(E5) National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135–3191 a. SPONSORING/MONTORING AGENCY NAME(9) AND ADDRESS(E5) National Aeronautics and Space Administration Washington, D.C. 20546–0001 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12. DISTRIBUTIONAVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) 14. ABSTRACT (Maximum 200 words) 15. is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise- varing shear flow is considered. These dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise- periodic cross-flow velocity on an otherwise two-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise- periodic cross-flow velocity on an otherwise two-dimensional shear low is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise- verindit cross-flow velocity on an otherwise two-d	6. AUTHOR(S)			WU-505-90-51	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. PERFORMING ORGANIZATION National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135–3191 E-9232 9. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration NASA TM-106779 11. SUPPLEMENTARY MOTES NASA TM-106779 David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, Organization code 0100, (216) 433-5825. 12a. DISTRIBUTION/AVALABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 worde) 11. is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbaces through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability ware will evolution distability ware will evolution of an initially linear, finite-growth-rate, instability ware will evolution of an initially incert finite dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations,	David W. Wundrow and M	Aarvin E. Goldstein			
National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135–3191 E-9232 9. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, D.C. 20546–0001 10. SPONSORING/MONTORING AGENCY NAME(S) AND ADDRESS(ES) 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3–25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 12b. DISTRIBUTION code 11. is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional distur- bances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of a initially finear, finite-growth-rate, instability wave with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous specad of of the shear layer, mean that the local growth rate to the instability wave with increasing streamwise distance, reaches a maximum and eventually decays through the action of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERIMS Boundary layer; Instability; Transition 16. NUMEER OF PAGES 16. PRICE CODE A03	7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. F			8. PERFORMING ORGANIZATION	
Lewis Research Center Cleveland, Ohio 44135-3191 E-9232 9. SPONSORING/MONTORING AGENCY NAME(5) AND ADDRESS(E5) 10. SPONSORING/MONTORING AGENCY REPORT NUMBER National Aeronautics and Space Administration Washington, D.C. 20546-0001 NASA TM-106779 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12b. DISTRIBUTIONAVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 12b. DISTRIBUTION CODE 12. ABSTRACT (Maximum 200 words) 11. is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional distur- barces through a kind of resonan-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the chreve dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise- periodic cross-flow velocity on an otherwise two-dimensional shear flow as spanwise boctain. The resulting mean-flow distortion nitially grows with increasing streamwise distance, reaches a maximum and evennually decays through that eaction of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate become sufficiently large and small, respectively. The amplitinde equation that describes this stag of ev	National Aeronautics and Space Administration				
Cleveland, Ohio 44135–3191 Image: Cleveland, Ohio 44135–3191 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) Image: Cleveland, Ohio 44135–3191 National Aeronautics and Space Administration NASA TM-106779 Int. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3–25260), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, ONASA Lewis Research Center. Responsib person, Marvin E. Goldstein, ONASA Lewis Research Center. Responsib person, Marvin E. Goldstein, Onas Companization code 0100, (216) 433–5825. 12a. DISTRIBUTIONAVALLABILITY STATEMENT Image: Cleve Code Code Code Code Code Code Code Cod	Lewis Research Center			F_9232	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration NASA TM-106779 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12b. DISTRIBUTIONAVALABILITY STATEMENT Unclassified - Unlimited Subject Category 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) 14 is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise varying shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier Stokes equations, is initiated by imposing a spamwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow discursion parabolized Navier Stokes equations, is initiated by imposing a spamwise-periodic cross-flow velocity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional alsear layer. 4. SUBJECT TERMS Boundary layer; Instability; Transitio	Cleveland, Ohio 44135-				
AGENCY REPORT NUMBER National Aeronautics and Space Administration Washington, D.C. 20546–0001 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25260), and Marvin E. Goldstein, NASA Lewis Research Center. Responsible person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12a. DISTRIBUTIONAVALABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) 12b. DISTRIBUTION action of eratin three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered, The base flow, which is governed by the three-dimensional arbaicized Navier Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decrease as the wave propagates downstream. Nonline effects can then become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. N	9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10.			10. SPONSORING/MONITORING	
National Aeronautics and Space Administration NASA TM-106779 Washington, D.C. 20546-0001 NASA TM-106779 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12. DISTRIBUTIONAVALLABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) 11 is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varing shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow as some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean: that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a				AGENCY REPORT NUMBER	
Washington, D.C. 20546-0001 NASA TM-106/79 11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) 12b. DISTRIBUTION code (Maximum 200 words) 14. Bis well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagets downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and	National Aeronautics and Space Administration				
11. SUPPLEMENTARY NOTES David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433-5825. 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited 12b. DISTRIBUTION code Subject Category 12b. DISTRIBUTION code 11. ABSTRACT (Maximum 200 words) 11. ABSTRACT (Maximum 200 words) 11. Is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwis variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanvise-varying shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate of two oblique modes in a	Washington, D.C. 20546-	-0001		NASA TM-106779	
David W. Wundrow, NYMA, Inc., Engineering Services Division, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 12b. DISTRIBUTION code 13. ABSTRACT (Maximum 200 words) 12b. DISTRIBUTION of Category 14. Bis well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwite variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, meant that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one	11. SUPPLEMENTARY NOTES		1	······································	
(WOR Funded by NASA Contract NASA-25260), and Marvin E. Goldstein, NASA Lewis Research Center. Responsib person, Marvin E. Goldstein, organization code 0100, (216) 433–5825. 12a. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwis variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional distur- bances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise- periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, means that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this tagg of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS Boundary layer; Instability; Tra	David W. Wundrow, NYN	1A, Inc., Engineering Services D	ivision, 2001 Aerospace	Parkway, Brook Park, Ohio 44142	
12a. DISTRIBUTIONAVAILABILITY STATEMENT 12b. DISTRIBUTIONAVAILABILITY STATEMENT 12a. DISTRIBUTIONAVAILABILITY STATEMENT 12b. DISTRIBUTION CODE 12a. ABSTRACT (Maximum 200 words) 12b. DISTRIBUTION CODE 13. ABSTRACT (Maximum 200 words) 12b. DISTRIBUTION of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 14. SECURITY CLASSIFICATION OF ABSTRACT 0F REPORT 18. SECURITY CLASSIFICATION OF	(WOIK IUNGED by NASA C	Contract NAS3 -25266), and Marv	/in E. Goldstein, NASA I	Lewis Research Center. Responsible	
Inclusion of ward and a series of the second series of the sec	12a DISTRIBUTION/AVAILABILITY	STATEMENT			
Unclassified - Unlimited Subject Category 13. ABSTRACT (Maximum 200 words) 14. SUBJECT TERMS Boundary layer; Instability; Transition 17. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified		STATEMENT		12b. DISTRIBUTION CODE	
Subject Category 13. ABSTRACT (Maximum 200 words) 14. ABSTRACT (Maximum 200 words) 15. NUMBER of PAGES 16. PRICE CADE 17. ABSTRACT (Maximum 200 words) It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwis variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean: that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Tra	Unclassified - Unlimited				
13. ABSTRACT (Maximum 200 words) 14. ABSTRACT (Maximum 200 words) 15. NUMBER of FAGES 16. SUBJECT TERMS 17. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION 19. MILLING ASIFICATION	Subject Category				
It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwis variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer.	13 ABSTRACT (Maximum 200 uro	zdo)			
It is well known that the presence of a weak cross flow in an otherwise two-dimensional shear flow results in a spanwise variation in the mean streamwise velocity profile that can lead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean: that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERMS Boundary layer; Instability; Transition 15. NUMBER OF PAGES 16. PRICE CODE A (3) 17. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION 0F REPORT Unclassified 19. SECURITY CLASSIFICATION 0F ABSTRACT 0 0 0 0 0 0 0 0 0 0 0 0 0	IS. ABSTRACT (Maximum 200 Wol	'asj			
Variation in the mean streamwise velocity profile that can fead to an amplification of certain three-dimensional disturbances through a kind of resonant-interaction mechanism (Goldstein and Wundrow 1994). The spatial evolution of an initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean: that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplit tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 17. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT	It is well known that the p	resence of a weak cross flow in a	n otherwise two-dimensi	onal shear flow results in a spanwise	
initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered, The base flow, which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean: that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 16. PRICE CODE A03 17. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF ABSTRACT 19. SECURITY CLASSIFICATION OF ABSTRACT 0F REPORT 18. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT	bances through a kind of r	imwise velocity profile that can le	ead to an amplification of Coldstein and Wundrow	1004) The special evolution of an	
which is governed by the three-dimensional parabolized Navier-Stokes equations, is initiated by imposing a spanwise-periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, means that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 14. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 16. PRICE CODE A03 7. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF ABSTRACT 19. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT	initially linear, finite-growth-rate, instability wave in such a spanwise-varying shear flow is considered. The base flow				
periodic cross-flow velocity on an otherwise two-dimensional shear flow at some fixed streamwise location. The resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean-that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave amplitude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 7. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified 19. SECURITY CLASSIFICATION Unclassified 20. LIMITATION OF ABSTRACT	which is governed by the	three-dimensional parabolized Na	vier-Stokes equations, is	initiated by imposing a spanwise-	
resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 35 16. PRICE CODE A03 7. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT	periodic cross-flow veloci	ty on an otherwise two-dimension	nal shear flow at some fix	xed streamwise location. The	
decays through the action of viscosity. This decay, which coincides with the viscous spread of of the shear layer, mean that the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 7. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT Unclassified Unclassified 19. Classified 20. LIMITATION OF ABSTRACT	resulting mean-flow distortion initially grows with increasing streamwise distance, reaches a maximum and eventually				
Init the local growth rate of the instability wave will eventually decrease as the wave propagates downstream. Nonline effects can then become important within a thin spanwise-modulated critical later once the local instability-wave ampli tude and growth rate become sufficiently large and small, respectively. The amplitude equation that describes this stage of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 35 16. PRICE CODE A03 7. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION 19. SECURITY CLASSIFICATION OF REPORT Unclassified 19. SECURITY CLASSIFICATION 20. LIMITATION OF ABSTRACT	decays inrough the action	of viscosity. This decay, which c	coincides with the viscous	s spread of of the shear layer, means	
4. SUBJECT TERMS 15. NUMBER OF PAGES Boundary layer; Instability; Transition 15. NUMBER OF PAGES 7. SECURITY CLASSIFICATION OF REPORT 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF THIS PAGE Unclassified 19. SECURITY CLASSIFICATION Unclassified 19. SECURITY CLASSIFICATION Unclassified 20. LIMITATION OF ABSTRACT	effects can then become in	nportant within a thin spanwise-r	nodulated critical later or	e propagates downstream. Nonlinear	
of evolution is shown to be a generalization of the one obtained by Goldstein and Choi (1989) who considered the related problem of the interaction of two oblique modes in a two-dimensional shear layer. 15. NUMBER OF PAGES 4. SUBJECT TERMS Boundary layer; Instability; Transition 15. NUMBER OF PAGES 7. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified 19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified 20. LIMITATION OF ABSTRACT	tude and growth rate become	me sufficiently large and small, re	espectively. The amplitu	de equation that describes this stage	
related problem of the interaction of two oblique modes in a two-dimensional shear layer. 4. SUBJECT TERMS Boundary layer; Instability; Transition 15. NUMBER OF PAGES 35 7. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified 19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified 20. LIMITATION OF ABSTRACT	of evolution is shown to be	e a generalization of the one obt	ained by Goldstein and C	Choi (1989) who considered the	
4. SUBJECT TERMS Boundary layer; Instability; Transition 15. NUMBER OF PAGES 35 35 16. PRICE CODE A03 7. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified 19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified 20. LIMITATION OF ABSTRACT	related problem of the inte	raction of two oblique modes in a	a two-dimensional shear	layer.	
14. SUBJECT TERMS Boundary layer; Instability; Transition 15. NUMBER OF PAGES 35 16. PRICE CODE A03 7. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified 19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified 20. LIMITATION OF ABSTRACT					
30 30 16. PRICE CODE A03 7. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION OF REPORT 0F THIS PAGE Unclassified Unclassified	4. SUBJECT TERMS Boundary layer: Instability	15. NUMBER OF PAGES			
A03 17. SECURITY CLASSIFICATION OF REPORT Unclassified 18. SECURITY CLASSIFICATION OF THIS PAGE 19. SECURITY CLASSIFICATION OF ABSTRACT 20. LIMITATION OF ABSTRACT	Dominary layer, filstaolifty	16. PRICE CODE			
OF REPORT OF THIS PAGE OF ABSTRACT Unclassified Unclassified	17. SECURITY CLASSIFICATION	18 SECURITY CLASSIFICATION			
Unclassified Unclassified Unclassified	OF REPORT	OF THIS PAGE	OF ABSTRACT		
	Unclassified	Unclassified	Unclassified		