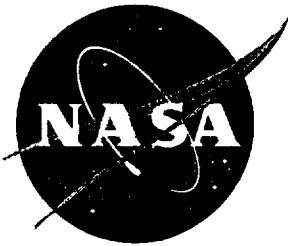


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A Wind Tunnel Investigation of Three NACA 1-Series Inlets at Mach Numbers Up to 0.92

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SUMMARY

Pressure distributions on three NACA 1-series inlets have been obtained in the Langley 16-Foot Transonic Tunnel. The cowl diameter ratio (ratio of cowl highlight diameter to cowl maximum diameter) was 0.85 for all three inlets. The cowl length ratio (ratio of cowl length to cowl maximum diameter) was 1.0 for two of the inlets (NACA 1-85-100) and 0.439 for the other (NACA 1-85-43.9) inlet. One of the inlets with a cowl length ratio of 1.0 had an internal contraction ratio (ratio of highlight area to throat area) of 1.009 and the other had a contraction ratio of 1.250. The inlet with a cowl length ratio of 0.439 also had an internal contraction ratio of 1.250. All three inlets had longitudinal rows of static pressure orifices on the top and bottom external cowl surfaces. The inlet with a contraction ratio of 1.009 also had a row of static pressure orifices on the side of the cowl (external surface). The two inlets with a contraction ratio of 1.250 had a longitudinal row of static pressure orifices on the diffuser surface.

The NACA 1-85-100 inlets were tested in the Mach number range from 0.79 to 0.92 and the NACA 1-85-43.9 inlet was tested in the Mach number range from 0.60 to 0.92. Inlet mass-flow ratios ranged from 0.27 to 0.96 depending on inlet configuration and freestream Mach number. Angle of attack was varied within the range -3° to 3.1° at selected Mach numbers and mass-flow ratios. The Reynolds number of the test varied with Mach number from 3.2×10^6 to 4.2×10^6 per foot.

INTRODUCTION

Engine installation on jet-powered subsonic transport aircraft generally results in each engine being wrapped separately in a nacelle that is essentially symmetric (in external contour) about the axis of the engine rotating components. The nacelle is pylon mounted (displaced from the airframe) so that during cruise flight at least the forward portion of the nacelle will pass through air that has not been significantly disturbed by the passage of any main airframe components. Such installations permit some decoupling of nacelle design from airframe design in that substantial development of at least the inlet portion of the nacelle can be done independently. This independence of inlet geometry from airframe geometry makes the pitot-type subsonic inlet data base available in the literature directly useable for many aircraft applications.

Inlets for turbojet and turbofan powered subsonic aircraft must provide high quality flow to the engine fan and compressor, produce low external drag, be low in weight and have noise characteristics acceptable to the community. High quality flow for the engine is provided by designing the internal flow lines (cowl lip, throat contour, and diffuser) for separation-free flow. Based on internal flow considerations, cowl length and weight are minimized by making the inlet throat radius as large as possible and by designing the diffuser contour so that the diffusion angle is close to the maximum for separation-free flow while allowing some margin at the most adverse operating conditions. For commercial applications it is also important to consider noise suppression during diffuser design since this may have some effect on how short the cowl portion of the nacelle can be. The external drag is minimized, based on external flow considerations, by making the maximum cowl diameter and length as small as

possible while still obtaining the desired drag divergence Mach number and spillage critical mass-flow ratio.

Many of the pitot-type subsonic transport nacelle forebodies (cowls) used in the past have been based (at least in part) on the NACA 1-series contour which was developed in the 1940's. The NACA 1-series contour has a relatively small leading edge radius (external to the highlight) and because of this has good high speed spillage drag characteristics. However, high speed external performance of the NACA 1-series contour must often be compromised by increasing the leading edge radius to achieve acceptable internal performance at low speed and static crosswind conditions. The NACA 1-series contour was developed concentrating on the inlet external performance with the assumption that throat and diffuser shape would be essentially a separate design endeavor. Most of the published experimental data obtained on NACA 1-series inlets is contained in references 1 to 10.

Evolutionary changes in transport aircraft speeds, engine cycle and mass flow needs, and advances in analytical and computational techniques applicable to inlet forebody design and analysis have produced the need for some expansion of the experimental data base. To this end, three inlet models having the same cowl highlight diameter have been investigated to obtain pressure data on the inlet forebody exterior and lip over a range of mass-flow ratios. Two of the inlets had an NACA 1-85-100 external contour but had different internal lip contours and internal contraction ratios. One of these inlets had a contraction ratio of 1.009 and has been tested previously over a limited range of mass-flow ratios (refs. 9 and 10). The other NACA 1-85-100 inlet had a contraction ratio of 1.250 and therefore had a different internal lip shape and throat diameter. The third inlet had an NACA 1-85-43.9 contour and a contraction ratio of 1.250. The two inlets with 1.250 contraction ratio had identical internal surface contours so that the effect of the 53.1 percent change in external cowl length on the surface pressure distributions could be determined. The difference in inlet lip contour and contraction ratio between the two NACA 1-85-100 inlets will show the effect, if any, of the internal contour change on the external surface pressure distributions.

The investigation was conducted in the Langley Research Center 16-Foot Transonic Tunnel at Mach numbers ranging from 0.60 to 0.92, mass-flow ratios from 0.27 to 0.96, and at angles of attack within the range from -3° to 3.1° at selected mass-flow ratios and Mach numbers. Cowl external static pressures were measured in rows on the top and bottom surfaces of the inlets (in the plane of vertical symmetry). The NACA 1-85-100 inlet with a contraction ratio of 1.009 also had a longitudinal row of cowl external static pressure orifices on the side of the inlet. Diffuser wall static pressures were measured in the two inlets with a contraction ratio of 1.250.

SYMBOLS

Symbols in parenthesis are used in computer generated tables.

A area normal to model centerline, in²

C_p	(CP)	local pressure coefficient, $(p-p_0)/q_0$
D_{max}		maximum diameter of model, 18.0 in.
d		inlet internal diameter at end of lip radius (see Table I), in.
L	(L)	length of cowl from lip (highlight) to start of cylindrical portion of model, in., see fig. 1
mfr		mass-flow ratio based on highlight area, $1/(\rho A_h V_0) \int \rho_r V_r dA$
M		freestream Mach number
p		local static pressure, psi
p_0		freestream static pressure, psi
q_0		freestream dynamic pressure, psi
R_p		pressure probe radial distance from model centerline, in.
R_w		radial distance from model centerline to duct outer wall, 8.40 in.
(RMAX)		maximum external cowl radius, in.
(R/RMAX)		nondimensionalized radius, in percent, from centerline of model to cowl or diffuser surface, RMAX = 9.0 in.
R_0		freestream Reynolds number, per foot
r		lip radius internal to highlight for NACA 1-series inlet (see Table I), in.
V		velocity, ft/sec
x/L	(X/L)	nondimensionalized distance, in percent, from cowl lip measured longitudinally (aft) with negative values indicating locations on the internal surface
x	(X)	longitudinal distance measured aft of the cowl lip (highlight), in.
Y		radial distance at RMAX minus inlet highlight radius (see Table I), in.
y		radial distance minus inlet highlight radius (see Table I), in.
α		angle of attack with respect to forebody centerline, deg
ρ		density slug/ft ³
ϕ		meridian angle, measured from top of model in clockwise direction when looking upstream, deg

Subscripts:

h	highlight, most forward point on cowl lip
max	maximum
r	axial mass-flow rake measuring station in duct
0	freestream condition

MODELS

A complete model test installation consisted of an inlet cowl and cylindrical section which were supported by a force balance, and an afterbody (also cylindrical) which was supported by the sting upon which a remote controlled mass-flow throttle plug was mounted. A simplified cross-sectional sketch of the model assembly is shown in figure 1 and a photograph of a typical model installation in the wind tunnel test section is shown in figure 2.

The basic nondimensionalized NACA 1-series outer profile ordinates, as presented for a given lip radius of $0.025Y$ in reference 1, are reproduced in table I. The NACA 1-85-100 inlet with an internal contraction ratio of 1.009 (table II) was used in the investigations of references 9 and 10. The second NACA 1-85-100 cowl had the same external profile, but had a different lip radius and an internal contraction ratio of 1.250 (table III). The third inlet (table IV) also had an internal contraction ratio of 1.250 but had a shorter cowl profile (NACA 1-85-43.9). This third inlet was designed to have the same overall assembled model length by including a section of constant (external) diameter at the end of the cowl profile. The internal contours (including the diffuser) of the two inlets with a 1.250 contraction ratio were identical.

Total model length was 52.0 inches (fig. 1) with the forward 27.50 inches, which included the cowl, supported by four struts that connected to a force-balance mounted centerbody. The aft 24.50 inches (cylindrical in external shape) of the model was supported by four struts attached to the support sting. A 0.10 inch gap between the forward and aft portions of the model was spanned by a free floating flexible strip to inhibit flow leakage. Three of the four struts supporting the forward portion of the model were instrumented with pressure (fig. 3) probes to measure the internal mass flow. These struts were also used to route the tubes from the inlet surface static-pressure orifices to differential pressure-scanning units mounted in the nose of the centerbody. All pressure tubes associated with the aft portion of the model were routed through the four rear support struts; into the sting; and out through the tunnel support system to another differential pressure-scanning unit.

The mass-flow throttle plug was driven by an internally housed remote controlled electric motor and had a travel capability of about 10 inches (fig. 1). The open area at the exit of the model (normal to the centerline of the model) could be varied from 27.5 in^2 to 244.9 in^2 (plug in its two extreme positions).

WIND TUNNEL

The investigation was conducted in the Langley Research Center 16-Foot Transonic Tunnel which is a single-return atmospheric wind tunnel with continuous air exchange. The test section is octagonal in shape with 15.5 feet between opposite walls (equivalent in area to a circle 16 feet in diameter) and has axial slots at the wall vertices. The total width of the eight slots in the vicinity of the model is approximately 3.7 percent of the test section perimeter. The extreme limits of solid blockage of the model in the test section is between 0.88 percent for the hypothetical case of no flow through the model and 0.79 percent for the case of the throttle plug only (the throttle plug in its most rearward position). The tunnel sting support system pivots in such a manner that the model remains on or near the test section centerline through the angle of attack range. Details of the operation of the tunnel and its flow qualities are presented in references 11 to 13.

TESTS AND METHODS

Each inlet was tested at Mach numbers up to 0.92 at an angle of attack of 0° and over a nominal angle of attack range (less than 3.1°) at selected Mach numbers and mass-flow ratios. Freestream Reynolds number per foot varied with Mach number from 3.2×10^6 to 4.2×10^6 (fig. 4). All the data presented herein are for artificially fixed boundary layer transition on the internal and external surfaces of the model. Boundary-layer transition on the external surface of the model was fixed by applying a 0.10 inch wide circumferential strip of number 120 silicon carbide particles 0.6 inch aft (streamwise) of the cowl lip. Boundary-layer transition was fixed on the internal flow surface of the model by applying a 0.10 inch wide circumferential strip of number 120 silicon carbide particles at the geometric throat of each inlet.

Angle of attack was computed by correcting the measured angle of attack of the support system for deflection of the sting and force balance due to aerodynamic forces and moments and for tunnel stream angularity. Although the test was conducted with the model mounted on a force balance, the data from it will not be presented since the balance was damaged during the test. Duct mass flow was calculated from the freestream total temperature, rake area-weighted stagnation pressures, and static pressures from the rake, centerbody surface, and duct wall.

No corrections have been made to the pressure data for test section wall interference effects. The presence and geometry of the mass-flow plug will have an effect on the afterbody external flow field. Therefore, the afterbody pressure data presented in the pressure tabulations should be considered qualitative, especially for pressures near the model aft end. The effect of the mass-flow plug should be the greatest for cases with large mass-flow ratios where the internal flow exits the afterbody before passing over the front face of the mass-flow plug and therefore has not been turned back streamwise by the internal afterbody surface.

PRESENTATION OF RESULTS

The results of this investigation are presented primarily in tabular form as local internal and external pressure coefficients in tables V to VII. The surface pressure coefficients are tabulated against nondimensionalized orifice location (X/L) where L is the length of the NACA cowl portion of the model. The ratio X/L is presented in percentage form in the tables. A negative value of X/L indicates the orifice is located on the internal surface (downstream of the highlight) of the inlet. The pressure coefficients are presented for either two or three meridian angles (Φ) depending on the number of rows of orifices on the configuration. Inlet mass-flow ratio and angle of attack are given at the top of each table. In addition, some data are presented graphically (figs. 5 to 11) to illustrate the variation of pressure coefficient with X/L over the lip and cowl portion of the model over a range of Mach numbers, mass-flow ratios, and angles of attack. Some graphical data are presented in figures 12 to 15 for the two inlets with a contraction ratio of 1.250 to show the effect of mass-flow ratio and angle of attack on the lip and diffuser pressure coefficient distributions.

Pressure coefficients						
M	mfr	α .deg	Table	Figure		
0.60 ↓	0.28	0	VI(a) ↓	14(a)		
	.31	↓		8(a)		
	.40			8(a),9(a),14(a),15(a)		
	.50			9(a),15(a)		
	↓	1.0		15(a)		
		2.0		14(a)		
		3.0		8(a),9(b),15(b)		
	↓	.56		0	9(b),15(b)	
		.63		2.0	14(a)	
		.69		0	8(a),9(c),14(a),15(c)	
.69		0	9(c),15(c)			
.75		2.0				
0.64 ↓	.82	0	VI(b) ↓	14(b)		
	.93	0		14(b)		
	0.27	0		14(b)		
	.30	↓		14(b)		
	.40			14(b)		
	.50			14(b)		
	↓	.55		0	14(b)	
		.62		2.0	14(b)	
		.68		0	14(c)	
		.75		0	8(b)	
.81		2.0	8(b),9(d),14(c),15(d)			
0.69 ↓	.81	0	VI(c) ↓	9(d),15(d)		
	0.28	0		14(c)		
	.30	↓		8(b)		
	.40			8(b),9(d),14(c),15(d)		
	.49			9(d),15(d)		
	↓	.49		2.0	14(c)	
		.55		0	8(b)	
		.61		0	14(c)	
		.68		0	8(b),14(c)	
		.74		2.0		
0.72 ↓	.81	0	VI(d) ↓	14(d)		
	0.30	0		14(d)		
	.40	↓				
	.49					
	.54					
	0.74 ↓	.54		0	VI(e) ↓	14(e)
		0.27		0		14(e)
		.31		↓		14(e)
		.40				14(e)
		.49				14(e)
↓		.54	0	14(e)		
		.61	2.1	14(k)		
		.68	0	8(f),14(k)		
		.74	0	14(k)		
		.80	0	8(f),9(k),14(k),15(k)		
0.77 ↓	.80	0	VI(f) ↓	9(k),15(k)		
	0.27	0		14(f)		
	.30	↓		14(f)		
	.40			14(f)		
	.48			14(f)		
	↓	.54		0	14(f)	
		.61		2.0	14(f)	
		.68		0	14(f)	
		.74		0	14(f)	
		.80		0	14(f)	
0.79 ↓	.80	0	VI(g) ↓	14(g)		
	0.27	0		8(c)		
	.30	↓		8(c),9(e),14(g),15(e)		
	.39			9(e),15(e)		
	.49			14(g)		
	↓	.49		2.0	14(g)	
		.54		0	8(c),14(g)	
		.61		0	14(g)	
		.68		0	14(g)	
		.74		2.0	8(c),14(g)	
0.82 ↓	.80	0	VI(h) ↓	14(h)		
	0.27	0		14(h)		
	.30	↓		14(h)		
	.40			14(h)		
	.49			14(h)		
	↓	.54		0	14(h)	
		.61		2.0	14(h)	
		.68		0	14(h)	
		.74		0	14(h)	
		.80		0	14(h)	
0.84 ↓	.80	0	VI(i) ↓	14(i)		
	0.27	0		8(d)		
	.30	↓		8(d),9(f),14(i),15(f)		
	.39			9(f),15(f)		
	.49			15(f)		
	↓	.54		0	14(i)	
		.61		2.0	8(d),9(g),14(i),15(g)	
		.67		0	9(g),15(g)	
		.73		2.0	15(g)	
		.82		3.1	14(i)	
0.87 ↓	.81	0	VI(j) ↓	14(j)		
	0.27	0		8(e)		
	.31	↓		8(e),9(i),14(j),15(i)		
	.39			9(i),15(i)		
	.50			14(j)		
	↓	.49		2.0	8(e),9(j),14(j),15(j)	
		.54		0	9(j),15(j)	
		.61		0	14(j)	
		.68		2.0	8(e),9(j),14(j),15(j)	
		.68		0	9(j),15(j)	
0.89 ↓	.74	0	VI(k) ↓	14(k)		
	.83	0		8(e),14(j)		
	0.27	0		14(k)		
	.32	↓		8(f)		
	.39			8(f),9(k),14(k),15(k)		
	.49			9(k),15(k)		
	↓	.54		0	14(k)	
		.61		0	8(f),14(k)	
		.68		0	14(k)	
		.74		0	14(k)	
.81		0	8(f),9(k),14(k)			
0.92 ↓	.81	0	VI(l) ↓	14(l)		
	0.27	0		8(g)		
	.32	↓		8(g),9(l),14(l),15(l)		
	.40			9(l),15(l)		
	.49			15(l)		
	↓	.54		0	14(l)	
		.61		1.0	8(g),9(m),14(l),15(m)	
		.68		2.0	9(m),15(m)	
		.68		3.1	14(l)	
		.74		0	8(g),9(n),14(l),15(n)	
0.92 ↓	.82	0	VI(m) ↓	9(n),15(n)		
	0.27	0		14(m)		
	.32	↓		8(g)		
	.40			8(g),9(l),14(l),15(l)		
	.49			9(l),15(l)		
	↓	.54		0	14(l)	
		.61		1.0	8(g),9(m),14(l),15(m)	
		.68		2.0	9(m),15(m)	
		.68		3.1	14(l)	
		.74		0	8(g),9(n),14(l),15(n)	
0.92 ↓	.82	0	VI(n) ↓	9(n),15(n)		
	0.27	0		14(n)		
	.32	↓		8(g)		
	.40			8(g),9(l),14(l),15(l)		
	.49			9(l),15(l)		
	↓	.54		0	14(l)	
		.61		1.0	8(g),9(m),14(l),15(m)	
		.68		2.0	9(m),15(m)	
		.68		3.1	14(l)	
		.74		0	8(g),9(n),14(l),15(n)	
0.92 ↓	.82	0	VI(o) ↓	9(n),15(n)		
	0.27	0		14(o)		
	.32	↓		8(g)		
	.40			8(g),9(l),14(l),15(l)		
	.49			9(l),15(l)		
	↓	.54		0	14(l)	
		.61		1.0	8(g),9(m),14(l),15(m)	
		.68		2.0	9(m),15(m)	
		.68		3.1	14(l)	
		.74		0	8(g),9(n),14(l),15(n)	
0.92 ↓	.82	0	VI(p) ↓	9(n),15(n)		
	0.27	0		14(p)		
	.32	↓		8(g)		
	.40			8(g),9(l),14(l),15(l)		
	.49			9(l),15(l)		
	↓	.54		0	14(l)	
		.61		1.0	8(g),9(m),14(l),15(m)	
		.68		2.0	9(m),15(m)	
		.68		3.1	14(l)	
		.74		0	8(g),9(n),14(l),15(n)	

Pressure coefficients					
M	mfr	α .deg	Table	Figure	
0.82 ↓	0.27	0	VI(h) ↓	14(h)	
	.30	↓		14(h)	
	.40			14(h)	
	.49			14(h)	
	↓	.54		0	14(h)
		.61		2.0	14(h)
		.68		0	14(h)
		.74		0	14(h)
		.80		0	14(h)
	0.84 ↓	.80		0	VI(i) ↓
0.27		0	8(d)		
.30		↓	8(d),9(f),14(i),15(f)		
.39			9(f),15(f)		
.49			15(f)		
↓		.54	0	14(i)	
		.61	2.0	8(d),9(g),14(i),15(g)	
		.67	0	9(g),15(g)	
		.73	2.0	15(g)	
		.82	3.1	14(i)	
0.87 ↓	.81	0	VI(j) ↓	14(j)	
	0.27	0		8(e)	
	.31	↓		8(e),9(i),14(j),15(i)	
	.39			9(i),15(i)	
	.50			14(j)	
	↓	.49		2.0	8(e),9(j),14(j),15(j)
		.54		0	9(j),15(j)
		.61		0	14(j)
		.68		2.0	8(e),9(j),14(j),15(j)
		.68		0	9(j),15(j)
0.89 ↓	.74	0	VI(k) ↓	14(k)	
	.83	0		8(e),14(j)	
	0.27	0		14(k)	
	.32	↓		8(f)	
	.39			8(f),9(k),14(k),15(k)	
	.49			9(k),15(k)	
	↓	.54		0	14(k)
		.61		0	8(f),14(k)
		.68		0	14(k)
		.74		0	14(k)
.81		0	8(f),9(k),14(k)		
0.92 ↓	.81	0	VI(l) ↓	14(l)	
	0.27	0		8(g)	
	.32	↓		8(g),9(l),14(l),15(l)	
	.40			9(l),15(l)	
	.49			15(l)	
	↓	.54		0	14(l)
		.61		1.0	8(g),9(m),14(l),15(m)
		.68		2.0	9(m),15(m)
		.68		3.1	14(l)
		.74		0	8(g),9(n),14(l),15(n)
0.92 ↓	.82	0	VI(m) ↓	9(n),15(n)	
	0.27	0		14(m)	
	.32	↓		8(g)	
	.40			8(g),9(l),14(l),15(l)	
	.49			9(l),15(l)	
	↓	.54		0	14(l)
		.61		1.0	8(g),9(m),14(l),15(m)
		.68		2.0	9(m),15(m)
		.68		3.1	14(l)
		.74		0	8(g),9(n),14(l),15(n)
0.92 ↓	.82	0	VI(n) ↓	9(n),15(n)	
	0.27	0		14(n)	
	.32	↓		8(g)	
	.40			8(g),9(l),14(l),15(l)	
	.49			9(l),15(l)	
	↓	.54		0	14(l)
		.61		1.0	8(g),9(m),14(l),15(m)
		.68		2.0	9(m),15(m)
		.68		3.1	14(l)
		.74		0	8(g),9(n),14(l),15(n)

reference 10 for high mass flows through the model. However, the geometry of the throttle plug used in that investigation was not capable of reducing the afterbody exit area enough over the range of plug travel to obtain low mass flows for the NACA 1-85-43.9 cowl, which should have significantly better performance at low mass-flow ratios at the lower Mach numbers. That is, it should have a lower critical mass-flow ratio which is a measure of cowl performance when operating below the compressibility drag-rise condition. At a given Mach number, drag changes only gradually as inlet mass flow is decreased until a critical mass flow is reached where drag abruptly increases. The drag increase results from flow separation caused by shocks or strong pressure gradients resulting from flow separation around the initial cowl lip curvature. Conversely the term lower critical Mach number would indicate the Mach number at which an abrupt drag increase results for a given mass-flow ratio as Mach number is decreased.

To expand the mass flow range capability of this apparatus to encompass lower mass flow rates, the throttle plug geometry was altered so that it was blunter and had a larger maximum diameter. Comparisons made in reference 10 of the results of references 9 (last 14 inches of afterbody boattailed) and 10 (cylindrical afterbody) at high mass-flow ratios indicate no significant effects fed forward from the exit plume/mass-flow plug combination to the cowl pressure distributions over the range of test Mach numbers.

Cowl Pressure Distributions

At 0° angle of attack.- NACA 1-series cowls that are designed for moderate or high subsonic Mach numbers often have high negative pressure peaks near the lip at low Mach numbers and low mass-flow ratios because of the relatively sharp cowl lip. This often results in flow separation on the forward portion of the cowl when the pressure can not recover from the peak. The pressure distributions of reference 9 for the NACA 1-85-100 inlet with a contraction ratio of 1.009 show that flow separation occurred on the cowl at a mass-flow ratio of 0.56 for Mach numbers of 0.4, 0.6, and 0.7. However at a Mach number of 0.79, which was the lowest test Mach number for that inlet in the present investigation, flow separation did not occur (fig. 5(a)) at that mass-flow ratio. Larger contraction ratios of 1.046 and 1.093 (reference 9) did not significantly affect flow separation on the forward portion of the cowl under the aforementioned conditions. At higher Mach numbers where flow separation did not occur on the forward portion of the cowl, larger contraction ratio had only small effects on the cowl pressure distributions. However, these small effects did result in some decrease in cowl critical Mach number at a given mass-flow ratio (see ref. 9) for a contraction ratio of 1.093.

The NACA 1-85-43.9 inlet, which because of its blunter lip profile is capable of better performance at lower Mach numbers than the NACA 1-85-100 inlets was tested at lower Mach numbers and lower mass-flow ratios. This inlet did not encounter flow separation at 0° angle of attack on the forward portion of the cowl at the lowest Mach numbers and mass-flow ratios tested (fig. 8) which indicates that it had lower critical Mach numbers relative to the NACA 1-85-100 inlets. Three non-NACA 1-series inlets ($X/L = 0.337, 0.439, \text{ and } 0.547$), whose external

contour changes with length were made in the same manner as the NACA 1-series inlets, were tested on the same apparatus described herein and the pressure coefficients are reported in reference 14. Those data showed the same improvements in performance at the lower Mach numbers and lower mass-flow ratios for the blunter lip profiles.

At small angles of attack.- The NACA 1-85-100 inlets were tested at angles of attack within the range from -3.0° to 3.1° at selected Mach numbers and mass-flow ratios (figs. 6 and 11). As would be expected, at low mass-flow ratios an increase in angle of attack caused an increase in the severity of the negative pressure peaks on the cowl upper surface and shifted the onset of strong recompression aft (see fig. 6(e) for example). At the high mass-flow ratios an increase in angle of attack decreased the extent of positive pressure on the forward portion of the cowl upper surface (see fig. 6(c) for example). The NACA 1-85-43.9 inlet was tested only at positive angles of attack so the row of pressure orifices on the bottom of the cowl can be considered to represent the equivalent negative angle of attack and are included in figure 9 for that purpose. The effects of angle of attack on the forward pressure peaks on this inlet were similar to those encountered on the NACA 1-85-100 inlets. This inlet was tested at angle of attack at lower Mach numbers than the others since it has more potential for good performance in the lower Mach number range. At a Mach number of 0.69 (fig. 9(d)) there appears to be flow separation near the cowl upper surface leading edge at 2.0° angle of attack. This can be seen by comparing the extent of constant pressure coefficient at the peak relative to that at 0° angle of attack for the top and bottom rows of pressure orifices.

At small angles of sideslip.- The NACA 1-85-100 inlet with a contraction ratio of 1.009 had a row of external pressure orifices on the side of the cowl at a meridian angle of 90° . Because of the inlet axial symmetry this row of orifices can be considered to represent the top of an inlet at 0° angle of attack that moves in sideslip when the model is moved in what has been defined as the angle of attack direction in this investigation. To determine the effect of sideslip on the pressure distributions, data from this row of orifices are presented in figure 7 for the maximum positive angle of attack at each Mach number. The data indicate a negligible effect of sideslip over the small angle range of this test.

Diffuser Pressure Distributions

The variation of pressure coefficient (internal to the highlight) with X/D_{\max} for various mass-flow ratios for the two inlets with a contraction ratio of 1.250 is shown in figures 12 ($\alpha = 0^\circ$) and 13 (small α 's) for the NACA 1-85-100 cowl and in figures 14 ($\alpha = 0^\circ$) and 15 (small α 's) for the NACA 1-85-43.9 cowl.

At 0° angle of attack.- An illustration of the effect of changing mass-flow ratio at a Mach number of 0.60 on the location of the stagnation point on the inlet lip of the NACA 1-85-43.9 inlet can be seen in the pressure coefficients of table VI(a). As expected the stagnation point was farthest inside the inlet on the contraction surface (at an X/L of -5.13 percent) at the lowest mass-flow ratio of 0.28. The

stagnation point moved forward on the contraction surface with increasing mass flow until it reached the highlight ($X/L = 0$) at the maximum mass-flow ratio of 0.93.

The pressure distributions of figure 14 (or figure 12) indicate that the lowest internal pressure occurred approximately at the geometric throat ($X/D_{\max} = 0.113$) for all mass-flow ratios up through a Mach number of 0.77. At a Mach number of 0.79 a shock occurred at the throat at a mass-flow ratio of 0.80. Above a Mach number of 0.79 the shock moved downstream to an X/D_{\max} of about 0.18 where the lowest pressure also occurred.

The effect of changes in external cowl shape on the pressure distributions internal to the highlight at 0° angle of attack was negligible as can be seen by comparing the data of figure 12 (NACA 1-85-100) with data at the appropriate Mach number and mass-flow conditions in figure 14 (NACA 1-85-43.9). The inlets both had a contraction ratio of 1.250 and identical diffuser geometry.

At small angles of attack.- The effect of angle of attack on the pressure distributions internal to the highlight is shown in tables VI and VII and figures 13 and 15 for the two different external cowl shapes. In general the effect of angle of attack is as would be expected. For example, examination of the pressure coefficients of tables VI and VII show that as angle of attack was increased for a given mass-flow ratio, the stagnation point of the incoming stream tube on the upper lip moved slightly farther into the contraction section while on the lower lip (the windward side) of the inlet the streamtube stagnation point moved slightly closer to the highlight.

CONCLUDING REMARKS

An investigation has been conducted over a range of subsonic speeds to determine pressure distributions on three isolated inlets having NACA 1-series cowl profiles. Two had NACA 1-85-100 cowls that differed only in internal contraction ratio (1.009 and 1.250). The third inlet had an NACA 1-85-43.9 cowl and had a contraction ratio of 1.250. Angle of attack was varied over a small range at selected Mach numbers and mass-flow ratios for each inlet.

At low Mach numbers and low mass-flow ratios, the NACA 1-85-100 inlets encountered flow separation over the forward portion of the cowl surface that was not significantly affected by the variation in contraction ratio. However the critical Mach number at a given mass-flow ratio was decreased somewhat by the increase in contraction ratio. The NACA 1-85-43.9 inlet did not encounter flow separation at the lowest mass-flow ratios since its blunter lip profile was more conducive to better performance at lower Mach numbers. At an angle of attack of 2.0° , the NACA 1-85-43.9 inlet did encounter separation at the lowest mass-flow ratio at the two lowest Mach numbers (0.60 and 0.69). Pressure coefficients from a row of pressure orifices on the side of the NACA 1-85-100 inlet with a contraction ratio of 1.009 showed no significant effect of angle change when the model was moved through a small range of angles of attack thus indicating insensitivity to small angles of sideslip.

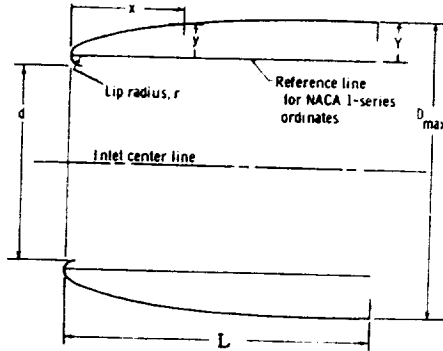
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TABLE I.- NACA 1-SERIES ORDINATES

[Coordinates in percent]



$$x = \left(\frac{x}{D_{max}}\right) D_{max} \quad y = \frac{D_{max} - d}{2} - r$$

$\left. \begin{matrix} \text{Series} \\ d \\ D_{max} \\ L \end{matrix} \right\} \begin{matrix} \text{in percent} \\ \text{in percent} \\ \text{in percent} \end{matrix}$

Sample NACA 1-series designation: NACA 1 - 81 - 100

x/L	y/Y	x/L	y/Y	x/L	y/Y
0	0	20.0	52.70	48.0	81.25
.2	4.80	21.0	54.05	49.0	81.99
.4	6.63	22.0	55.37	50.0	82.69
.6	8.12	23.0	56.66	52.0	84.10
.8	9.33	24.0	57.92	54.0	85.45
1.0	10.38	25.0	59.15	56.0	86.73
1.5	12.72	26.0	60.35	58.0	87.95
2.0	14.72	27.0	61.52	60.0	89.11
2.5	16.57	28.0	62.67	62.0	90.20
3.0	18.31	29.0	63.79	64.0	91.23
3.5	19.94	30.0	64.89	66.0	92.20
4.0	21.48	31.0	65.97	68.0	93.11
4.5	22.96	32.0	67.03	70.0	93.95
5.0	24.36	33.0	68.07	72.0	94.75
6.0	27.01	34.0	69.08	74.0	95.48
7.0	29.47	35.0	70.08	76.0	96.16
8.0	31.81	36.0	71.05	78.0	96.79
9.0	34.03	37.0	72.00	80.0	97.35
10.0	36.13	38.0	72.94	82.0	97.87
11.0	38.15	39.0	73.85	84.0	98.33
12.0	40.09	40.0	74.75	86.0	98.74
13.0	41.94	41.0	75.63	88.0	99.09
14.0	43.66	42.0	76.48	90.0	99.40
15.0	45.30	43.0	77.32	92.0	99.65
16.0	46.88	44.0	78.15	94.0	99.85
17.0	48.40	45.0	78.95	96.0	99.93
18.0	49.88	46.0	79.74	98.0	99.98
19.0	51.31	47.0	80.50	100.0	100.00

Lip radius: 0.025Y

TABLE II. - DESIGN ORDINATES FOR NACA 1-85-100 INLET WITH INTERNAL CONTRACTION
 RATIO OF 1.009

[Coordinates in percent]
 L = 18.00in. and RMAX = 9.00in.

External ordinates			
X/L	R/RMAX	X/L	R/RMAX
0.0	85.36	20.00	93.09
.20	86.06	25.00	94.02
.40	86.33	30.00	94.87
.60	86.56	35.00	95.62
1.50	87.22	40.00	96.29
2.00	87.51	45.00	96.91
2.50	87.80	50.00	97.47
3.00	88.04	60.00	98.40
4.00	88.51	70.00	99.11
5.00	88.93	80.00	99.62
7.00	89.69	90.00	99.91
10.00	90.64	100.00	100.00
15.00	92.00		

Internal ordinates			
X/L	R/RMAX	X/L	R/RMAX
0.0	85.36	45.00	86.71
.18	85.00	60.00	87.98
12.50	85.42	80.00	90.89
25.00	85.87	90.00	92.38
35.00	86.22	100.00	93.33

TABLE III.- DESIGN ORDINATES FOR NACA 1-85-100 INLET WITH INTERNAL CONTRACTION
RATIO OF 1.250

[Coordinates in percent]
L = 18.00in. and RMAX = 9.00in.

External ordinates				Internal ordinates			
X/L	R/RMAX	X/L	R/RMAX	X/L	R/RMAX	X/L	R/RMAX
0.0	85.36	21.54	93.38	0.0	85.36	12.01	76.36
.02	85.58	23.16	93.68	.01	85.00	12.43	76.38
.08	85.81	24.87	94.00	.04	84.64	12.91	76.40
.18	86.02	26.68	94.31	.08	84.28	13.42	76.44
.32	86.24	28.59	94.63	.14	83.92	13.99	76.49
.50	86.45	30.60	94.95	.23	83.56	14.62	76.55
.72	86.65	32.74	95.28	.33	83.20	15.31	76.64
.98	86.86	35.01	95.62	.45	82.83	16.07	76.74
1.29	87.08	37.42	95.96	.59	82.47	16.90	76.88
1.63	87.30	40.00	96.30	.76	82.11	17.82	77.04
2.02	87.53	43.00	96.68	.94	81.75	18.83	77.23
2.45	87.77	46.00	97.03	1.15	81.39	19.94	77.46
2.92	88.01	49.00	97.36	1.38	81.03	21.16	77.74
3.44	88.25	52.00	97.67	1.64	80.67	22.50	78.07
4.00	88.51	55.00	97.96	1.93	80.31	23.98	78.46
4.61	88.76	58.00	98.24	2.25	79.95	25.61	78.92
5.26	89.02	61.00	98.49	2.61	79.59	27.39	79.46
5.96	89.29	64.00	98.72	3.00	79.23	29.36	80.07
6.71	89.57	67.00	98.93	3.45	78.87	31.52	80.78
7.50	89.85	70.00	99.11	3.94	78.51	33.90	81.59
8.35	90.13	73.00	99.29	4.51	78.15	36.52	82.49
9.25	90.42	76.00	99.44	5.18	77.77	39.40	83.51
10.20	90.71	79.00	99.57	5.86	77.45	42.57	84.62
11.21	91.01	82.00	99.69	6.53	77.18	46.05	85.83
12.27	91.31	85.00	99.79	7.21	76.95	49.89	87.12
13.40	91.61	88.00	99.87	7.88	76.76	54.10	88.46
14.58	91.90	91.00	99.93	8.56	76.61	58.74	89.81
15.83	92.19	94.00	99.98	9.24	76.49	63.84	91.09
17.15	92.48	97.00	99.99	9.91	76.41	69.45	92.21
18.54	92.78	100.00	100.00	10.59	76.36	75.62	93.02
20.00	93.07			11.26	76.35	82.25	93.33
				11.62	76.35	89.72	93.33

TABLE IV.- DESIGN ORDINATES FOR NACA 1-85-43.9 INLET WITH INTERNAL CONTRACTION
RATIO OF 1.250

[Coordinates in percent]
L = 7.897in. and RMAX = 9.00in.

External ordinates			Internal ordinates		
X/L	R/RMAX	X/L	R/RMAX	X/L	R/RMAX
0.0	85.36	21.54	93.38	0.0	85.36
.02	85.58	23.16	93.68	.02	85.00
.08	85.81	24.87	94.00	.08	84.64
.18	86.02	26.68	94.31	.19	84.28
.32	86.24	28.59	94.63	.33	83.92
.50	86.45	30.60	94.95	.52	83.56
.72	86.65	32.74	95.28	.75	83.20
.98	86.86	35.01	95.62	1.03	82.83
1.29	87.08	37.42	95.96	1.35	82.47
1.63	87.30	40.00	96.30	1.72	82.11
2.02	87.53	43.00	96.68	2.14	81.75
2.45	87.77	46.00	97.03	2.62	81.39
2.92	88.01	49.00	97.36	3.15	81.03
3.44	88.25	52.00	97.67	3.74	80.67
4.00	88.51	55.00	97.96	4.40	80.31
4.61	88.76	58.00	98.24	5.13	79.95
5.26	89.02	61.00	98.49	5.95	79.59
5.96	89.29	64.00	98.72	6.85	79.23
6.71	89.57	67.00	98.93	7.86	78.87
7.50	89.85	70.00	99.11	8.99	78.51
8.35	90.13	73.00	99.29	10.27	78.15
9.25	90.42	76.00	99.44	11.81	77.77
10.20	90.71	79.00	99.57	13.35	77.45
11.21	91.01	82.00	99.69	14.89	77.18
12.27	91.31	85.00	99.79	16.43	76.95
13.40	91.61	88.00	99.87	17.97	76.76
14.58	91.90	91.00	99.93	19.51	76.61
15.83	92.19	94.00	99.98	21.05	76.49
17.15	92.48	97.00	99.99	22.59	76.41
18.54	92.78	100.00	100.00	24.13	76.36
20.00	93.07			25.67	76.35
				26.48	76.35

TABLE V. Continued

(a) Concluded

mfr = 0.85 and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody	
X/L	CP	X/L	X/L	CP	X/L	X/L	CP	X/L
-3.75	0.3215	166.70	0.0075	0.0200	166.70	-3.75	0.5078	166.70
-3.12	0.5348	183.30	0.0200	0.0350	183.30	-3.12	0.5194	183.30
-1.88	0.5260	200.00	0.0350	0.0568	200.00	-1.88	0.5215	200.00
-1.25	0.5039	216.70	0.0568	0.1042	216.70	-1.25	0.4909	216.70
-0.62	0.4948	238.90	0.1042	0.1541	238.90	-0.62	0.4538	238.90
0.00	1.1662	255.60	0.1542	0.2149	255.60	0.00	1.1646	255.60
0.31	-0.2507	266.70	0.2149	0.2578	266.70	0.62	-0.0833	266.70
0.62	-0.1173	272.20	0.2578	0.3089	272.20	1.25	-0.1696	272.20
1.25	-0.2531	277.80	0.3089	0.3735	277.80	1.88	-0.1878	277.80
2.50	-0.1404	283.30	0.3735		283.30	2.50	-0.1901	283.30
3.12	-0.1197					3.12	-0.1526	
4.38	-0.1162					4.38	-0.1262	
5.00	-0.1800					5.00	-0.1361	
7.50	-0.1824					7.50	-0.1444	
10.00	-0.1551					10.00	-0.1459	
12.50	-0.1590					12.50	-0.1475	
15.00	-0.1232					15.00	-0.1191	
30.00	-0.1274					20.00	-0.1164	
40.00	-0.1036					30.00	-0.1112	
50.00	-0.1064					40.00	-0.1048	
60.00	-0.1001					50.00	-0.0876	
70.00	-0.1033					60.00	-0.0986	
90.00	-0.0695					70.00	-0.0775	
122.00	-0.0197					80.00	-0.0679	
139.00	-0.0094					90.00	-0.0251	
						122.00	-0.0243	
						139.00	-0.0181	

TABLE V. Continued
(b) Continued

mfr = 0.67 and $\alpha = 2.0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP
-3.75	1.0547	166.70	0.0014	166.70	0.0014	-3.75	1.0743	166.70
-3.12	1.0726	183.30	0.0074	183.30	0.0014	-3.12	1.0821	183.30
-1.88	1.1172	200.00	0.0213	200.00	0.0183	-1.88	1.1255	200.00
-1.25	1.1442	216.70	0.0389	216.70	0.0336	-1.25	1.1503	216.70
-0.62	1.1793	238.90	0.0847	238.90	0.0771	-0.62	1.1865	238.90
0.00	0.0963	255.60	0.1352	255.60	0.1329	0.00	-0.1785	255.60
0.31	-1.3897	266.70	0.1939	266.70	0.1993	0.31	-1.6360	266.70
0.62	-1.6047	272.20	0.2345	272.20	0.2491	0.62	-1.6668	272.20
1.25	-1.5576	277.80	0.2826	277.80	0.3056	1.25	-1.6542	277.80
2.50	-1.4493	283.30	0.3368	283.30	0.3769	2.50	-1.5077	283.30
3.12	-1.4215					3.12	-1.4920	
4.38	-1.2785					4.38	-1.3470	
5.00	-1.2445					5.00	-1.3286	
7.50	-1.1371					7.50	-1.2325	
10.00	-1.0795					10.00	-1.1696	
12.50	-1.0245					12.50	-1.0908	
15.00	-0.9483					15.00	-1.0117	
30.00	-0.0878					30.00	-0.1110	
40.00	-0.0717					40.00	-0.0464	
50.00	-0.1133					50.00	-0.0965	
60.00	-0.1231					60.00	-0.1188	
70.00	-0.1234					70.00	-0.1139	
80.00	-0.1247					80.00	-0.0913	
90.00	-0.0912					90.00	-0.0985	
122.00	-0.0352					122.00	-0.0389	
139.00	-0.0206					139.00	-0.0250	

mfr = 0.67 and $\alpha = 1.0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP
-3.75	1.0888	166.70	0.0175	166.70	-0.0264	-3.75	0.9642	166.70
-3.12	1.0979	183.30	0.0168	183.30	0.0127	-3.12	0.9796	183.30
-1.88	1.1412	200.00	0.0274	200.00	0.0165	-1.88	1.0354	200.00
-1.25	1.1617	216.70	0.0444	216.70	0.0344	-1.25	1.0553	216.70
-0.62	1.1891	238.90	0.0859	238.90	0.0763	-0.62	1.1157	238.90
0.00	-0.2901	255.60	0.1340	255.60	0.1311	0.00	0.5571	255.60
0.31	-1.6632	266.70	0.1862	266.70	0.1972	0.31	-1.3412	266.70
0.62	-1.7057	272.20	0.2181	272.20	0.2306	0.62	-1.4370	272.20
1.25	-1.6455	277.80	0.2573	277.80	0.3114	1.25	-1.3448	277.80
2.50	-1.5666	283.30	0.3094	283.30	0.3915	2.50	-1.2139	283.30
3.12	-1.5299					3.12	-1.1397	
4.38	-1.4310					4.38	-1.0672	
5.00	-1.4153					5.00	-1.0298	
7.50	-1.3079					7.50	-0.9529	
10.00	-1.2300					10.00	-0.8079	
12.50	-1.1482					12.50	-0.7117	
15.00	-1.0572					15.00	-0.1743	
30.00	-0.3097					30.00	-0.1452	
40.00	-0.0639					40.00	-0.1350	
50.00	-0.0655					50.00	-0.1350	
60.00	-0.1032					60.00	-0.1320	
70.00	-0.1048					70.00	-0.1192	
80.00	-0.0630					80.00	-0.0836	
90.00	-0.0385					90.00	-0.0338	
122.00	-0.0273					122.00	-0.0338	
139.00	-0.0213					139.00	-0.0145	

mfr = 0.64 and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP
-3.75	1.0888	166.70	0.0175	166.70	-0.0009	-3.75	0.9660	166.70
-3.12	1.0979	183.30	0.0168	183.30	0.0127	-3.12	0.9678	183.30
-1.88	1.1412	200.00	0.0274	200.00	0.0280	-1.88	1.0256	200.00
-1.25	1.1617	216.70	0.0444	216.70	0.0508	-1.25	1.0461	216.70
-0.62	1.1891	238.90	0.0859	238.90	0.0974	-0.62	1.1257	238.90
0.00	-0.2901	255.60	0.1340	255.60	0.1533	0.00	0.4721	255.60
0.31	-1.6632	266.70	0.1862	266.70	0.2189	0.31	-1.3256	266.70
0.62	-1.7057	272.20	0.2181	272.20	0.2642	0.62	-1.3555	266.70
1.25	-1.6455	277.80	0.2573	277.80	0.3194	1.25	-1.2690	272.20
2.50	-1.5666	283.30	0.3094	283.30	0.3811	2.50	-1.2302	277.80
3.12	-1.5299					3.12	-1.1793	283.30
4.38	-1.4310					4.38	-1.0767	283.30
5.00	-1.4153					5.00	-0.9978	283.30
7.50	-1.3079					7.50	-0.9198	283.30
10.00	-1.2300					10.00	-0.8555	283.30
12.50	-1.1482					12.50	-0.8079	283.30
15.00	-1.0572					15.00	-0.7117	283.30
30.00	-0.3097					30.00	-0.1412	283.30
40.00	-0.0639					40.00	-0.1444	283.30
50.00	-0.0655					50.00	-0.1342	283.30
60.00	-0.1032					60.00	-0.1282	283.30
70.00	-0.1048					70.00	-0.1169	283.30
80.00	-0.0630					80.00	-0.1190	283.30
90.00	-0.0385					90.00	-0.0962	283.30
122.00	-0.0273					122.00	-0.0876	283.30
139.00	-0.0213					139.00	-0.0343	283.30

TABLE V. Continued
(b) Continued

	mf = 0.71 and $\alpha = 0^\circ$																										
	$\phi = 90^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 90^\circ$				$\phi = 180^\circ$										
	Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody				
	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP			
-3.75	0.8666	166.70	0.0046	-3.75	0.8669	166.70	0.0139	-3.75	0.8690	166.70	0.0041	-3.75	0.7155	166.70	0.0041	-3.75	0.7155	166.70	0.0041	-3.75	0.7155	166.70	0.0041	-3.75	0.7297	166.70	0.0276
-3.12	0.8761	183.30	0.0222	-3.12	0.8725	183.30	0.0222	-3.12	0.8844	183.30	0.0381	-3.12	0.7161	183.30	0.0263	-3.12	0.7161	183.30	0.0263	-3.12	0.7161	183.30	0.0263	-3.12	0.7326	183.30	0.0326
-1.88	0.9201	200.00	0.0358	-1.88	0.9062	200.00	0.0428	-1.88	0.8979	200.00	0.0511	-1.88	0.7513	200.00	0.0416	-1.88	0.7513	200.00	0.0416	-1.88	0.7513	200.00	0.0416	-1.88	0.7565	200.00	0.0479
-1.25	0.9647	216.70	0.0604	-1.25	0.9531	216.70	0.0601	-1.25	0.9421	216.70	0.0676	-1.25	0.7256	216.70	0.0676	-1.25	0.7256	216.70	0.0676	-1.25	0.7256	216.70	0.0676	-1.25	0.7968	216.70	0.0686
-0.62	1.0245	238.90	0.1092	0.00	1.0086	238.90	0.1096	-0.62	1.0347	238.90	0.1220	-0.62	0.7866	238.90	0.1194	-0.62	0.7866	238.90	0.1194	-0.62	0.7866	238.90	0.1194	-0.62	0.9246	238.90	0.1218
0.00	0.9162	255.60	0.1700	0.62	-1.1272	255.60	0.1726	0.00	0.8461	255.60	0.1885	0.00	1.1823	255.60	0.1776	0.62	-1.1805	255.60	0.1776	0.62	-1.1805	255.60	0.1776	0.62	-0.9858	255.60	0.1856
0.31	-1.0925	266.70	0.2360	1.25	-1.0601	266.70	0.2417	0.62	-1.1189	266.70	0.2555	0.31	-0.3258	266.70	0.2457	1.25	-0.6550	266.70	0.2457	1.25	-0.6550	266.70	0.2457	1.25	-0.9354	266.70	0.2553
0.62	-1.2018	272.20	0.2845	1.88	-0.9917	272.20	0.2941	1.25	-1.0833	272.20	0.3004	0.62	-0.5158	272.20	0.2935	1.88	-0.6578	272.20	0.2935	1.88	-0.6578	272.20	0.2935	1.88	-0.8887	272.20	0.3035
1.25	-1.1092	277.80	0.3384	2.50	-0.9895	277.80	0.3480	1.88	-1.0436	277.80	0.3526	1.25	-0.4417	277.80	0.3494	2.50	-0.3272	277.80	0.3494	2.50	-0.3272	277.80	0.3494	2.50	-0.8887	277.80	0.3557
2.50	-0.9933	283.30	0.4031	3.12	-0.9289	283.30	0.4177	2.50	-0.9289	283.30	0.4102	2.50	-0.2767	283.30	0.4195	3.12	-0.3940	283.30	0.4195	3.12	-0.3940	283.30	0.4195	3.12	-0.8743	283.30	0.4182
4.38	-0.8395			4.38	-0.8438			3.12	-0.9112			3.12	-0.2132			4.38	-0.2589			4.38	-0.2589			4.38	-0.8128		
5.00	-0.7941			5.00	-0.7865			3.75	-0.8480			4.38	-0.1548			5.00	-0.2402			5.00	-0.2402			5.00	-0.76174		
7.50	-0.5597			7.50	-0.4525			4.38	-0.7876			5.00	-0.2184			7.50	-0.2865			7.50	-0.2865			7.50	-0.6998		
10.00	-0.1814			10.00	-0.1746			5.00	-0.8019			7.50	-0.2525			10.00	-0.1900			10.00	-0.1900			10.00	-0.5883		
12.50	-0.2001			12.50	-0.1926			7.50	-0.7505			10.00	-0.2022			15.00	-0.1250			15.00	-0.1250			15.00	-0.5000		
15.00	-0.1745			15.00	-0.1568			15.00	-0.1948			12.50	-0.2142			17.50	-0.0929			17.50	-0.0929			17.50	-0.4552		
30.00	-0.1673			30.00	-0.1452			17.50	-0.2070			15.00	-0.2142			20.00	-0.0929			20.00	-0.0929			20.00	-0.4167		
40.00	-0.1356			40.00	-0.1303			20.00	-0.1656			17.50	-0.2142			30.00	-0.0929			30.00	-0.0929			30.00	-0.364		
50.00	-0.1349			50.00	-0.1210			40.00	-0.1474			15.00	-0.2142			40.00	-0.0929			40.00	-0.0929			40.00	-0.2992		
60.00	-0.1290			60.00	-0.1123			60.00	-0.1379			12.50	-0.2142			50.00	-0.0929			50.00	-0.0929			50.00	-0.2557		
70.00	-0.1172			70.00	-0.1107			70.00	-0.1284			10.00	-0.2142			60.00	-0.0929			60.00	-0.0929			60.00	-0.2114		
90.00	-0.0791			80.00	-0.0839			80.00	-0.1085			7.50	-0.2142			70.00	-0.0929			70.00	-0.0929			70.00	-0.1647		
122.00	-0.0252			90.00	-0.0839			90.00	-0.1189			5.00	-0.2142			80.00	-0.0644			80.00	-0.0644			80.00	-0.1253		
139.00	-0.0098			122.00	-0.0287			122.00	-0.0846			3.12	-0.2142			90.00	-0.0846			90.00	-0.0846			90.00	-0.0997		
				139.00	-0.0194			139.00	-0.0287			3.12	-0.2132			139.00	-0.0039			139.00	-0.0039			139.00	-0.0224		
												3.12	-0.2132			139.00	-0.0213			139.00	-0.0213			139.00	-0.0181		

TABLE V. Continued

(b) Continued

mfr = 0.78 and $\alpha = 0^\circ$			mfr = 0.78 and $\alpha = 1.0^\circ$		
$\phi = 0^\circ$			$\phi = 0^\circ$		
Forebody	Afterbody		Forebody	Afterbody	
X/L	CP		X/L	CP	
-3.75	0.7611	0.0144	-3.75	0.7796	0.0251
-3.12	0.7881	0.0273	-3.12	0.7994	0.0337
-1.88	0.7865	0.0413	-1.88	0.8274	0.0473
-1.25	0.7826	0.0673	-1.25	0.8420	0.0725
0.00	-0.62	0.0673	0.00	-0.62	0.09317
0.00	-0.62	0.0673	0.00	-0.62	0.1242
0.31	-0.8132	0.2483	0.31	-0.9399	0.2530
0.62	-0.8263	0.2720	0.62	-1.0053	0.2964
1.25	-0.6756	0.3488	1.25	-0.9742	0.3495
2.50	-0.5780	0.3488	2.50	-0.7522	0.4108
3.12	-0.3337		3.12	-0.7375	
4.38	-0.2282		4.38	-0.7457	
5.00	-0.2646		5.00	-0.4168	
7.50	-0.2927		7.50	-0.2705	
10.00	-0.2354		10.00	-0.2150	
12.50	-0.2603		12.50	-0.2539	
15.00	-0.1948		15.00	-0.2072	
30.00	-0.1545		30.00	-0.1631	
40.00	-0.1080		40.00	-0.1259	
50.00	-0.1253		50.00	-0.1242	
60.00	-0.1034		60.00	-0.1232	
70.00	-0.1106		70.00	-0.1141	
90.00	-0.0815		90.00	-0.0740	
122.00	-0.0181		122.00	-0.0184	
139.00	-0.0065		139.00	-0.0057	

mfr = 0.78 and $\alpha = 90^\circ$			mfr = 0.78 and $\alpha = 180^\circ$		
$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody	Afterbody		Forebody	Afterbody	
X/L	CP		X/L	CP	
-3.75	0.7358	0.0251	-3.75	0.7030	0.0160
-3.12	0.7534	0.0337	-3.12	0.7576	0.0270
-1.88	0.7713	0.0473	-1.88	0.7985	0.0456
-1.25	0.7895	0.0725	-1.25	0.7968	0.0629
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.62	-0.4754	0.2504	0.62	-0.4754	0.2504
1.25	-0.3778	0.3011	1.25	-0.3778	0.3011
1.88	-0.2872	0.3601	1.88	-0.2872	0.3601
2.50	-0.3481	0.4287	2.50	-0.3481	0.4287
3.12	-0.2740		3.12	-0.2740	
3.75	-0.1998		3.75	-0.1998	
4.38	-0.2069		4.38	-0.2069	
5.00	-0.1977		5.00	-0.1977	
7.50	-0.2366		7.50	-0.2366	
10.00	-0.1731		10.00	-0.1731	
15.00	-0.1811		15.00	-0.1811	
17.50	-0.1405		17.50	-0.1405	
20.00	-0.1309		20.00	-0.1309	
30.00	-0.1191		30.00	-0.1191	
40.00	-0.1166		40.00	-0.1166	
50.00	-0.1141		50.00	-0.1141	
60.00	-0.1000		60.00	-0.1000	
70.00	-0.0937		70.00	-0.0937	
80.00	-0.1072		80.00	-0.1072	
90.00	-0.0751		90.00	-0.0751	
122.00	-0.0188		122.00	-0.0188	
139.00	-0.0100		139.00	-0.0100	

mfr = 0.78 and $\alpha = 2.0^\circ$			mfr = 0.78 and $\alpha = 3.0^\circ$		
$\phi = 90^\circ$			$\phi = 90^\circ$		
Forebody	Afterbody		Forebody	Afterbody	
X/L	CP		X/L	CP	
-3.75	0.8105	0.0347	-3.75	0.8373	0.0431
-3.12	0.8271	0.0354	-3.12	0.8493	0.0415
-1.88	0.8736	0.0463	-1.88	0.9061	0.0544
-1.25	0.8856	0.0723	-1.25	0.9321	0.0760
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.31	-0.9804	0.2525	0.31	-1.0533	0.2964
0.62	-1.0715	0.2957	0.62	-1.2427	0.2964
1.25	-1.1085	0.3455	1.25	-1.1907	0.3413
1.25	-1.0424	0.3455	1.25	-1.0606	0.3941
2.50	-0.9433	0.4026	2.50	-0.8979	0.4318
3.12	-0.8808		3.12	-0.8979	
4.38	-0.8301		4.38	-0.9371	
5.00	-0.8438		5.00	-0.9298	
7.50	-0.7900		7.50	-0.8964	
10.00	-0.2991		10.00	-0.7867	
12.50	-0.1796		12.50	-0.7431	
15.00	-0.1482		15.00	-0.7152	
30.00	-0.1744		30.00	-0.6299	
40.00	-0.1329		40.00	-0.5529	
50.00	-0.1368		50.00	-0.5051	
60.00	-0.1250		60.00	-0.4729	
70.00	-0.1152		70.00	-0.4452	
90.00	-0.0751		90.00	-0.4152	
122.00	-0.0200		122.00	-0.3569	
139.00	-0.0046		139.00	-0.3337	

$\phi = 180^\circ$			$\phi = 180^\circ$		
Forebody	Afterbody		Forebody	Afterbody	
X/L	CP		X/L	CP	
-3.75	0.6008	0.0205	-3.75	0.6008	0.0205
-3.12	0.5850	0.0405	-3.12	0.6008	0.0205
-1.25	0.5427	0.0637	-1.25	0.5427	0.0637
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.00	-0.62	0.1865	0.00	-0.62	0.1865
0.62	-0.4352	0.2462	0.62	-0.4352	0.2462
1.25	-0.3716	0.2977	1.25	-0.3716	0.2977
1.88	-0.3371	0.3569	1.88	-0.3371	0.3569
2.50	-0.3481	0.4337	2.50	-0.3481	0.4337
3.12	-0.2740		3.12	-0.2740	
3.75	-0.2069		3.75	-0.2069	
4.38	-0.1991		4.38	-0.1991	
5.00	-0.1977		5.00	-0.1977	
7.50	-0.2366		7.50	-0.2366	
10.00	-0.1731		10.00	-0.1731	
15.00	-0.1811		15.00	-0.1811	
17.50	-0.1405		17.50	-0.1405	
20.00	-0.1309		20.00	-0.1309	
30.00	-0.1191		30.00	-0.1191	
40.00	-0.1166		40.00	-0.1166	
50.00	-0.1141		50.00	-0.1141	
60.00	-0.1000		60.00	-0.1000	
70.00	-0.0937		70.00	-0.0937	
80.00	-0.1072		80.00	-0.1072	
90.00	-0.0751		90.00	-0.0751	
122.00	-0.0188		122.00	-0.0188	
139.00	-0.0100		139.00	-0.0100	

TABLE V. Continued
(b) Concluded

mfr = 0.95 and $\alpha = 2.0^\circ$

$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-3.75	0.1833	-3.75	-0.0544	-3.75	-0.1976	-3.75	0.2291	-3.75	-0.0570	-3.75	-0.4510
-3.12	0.1941	-3.12	-0.0104	-3.12	-0.1798	-3.12	0.3035	-3.12	0.0259	-3.12	-0.4510
-1.88	0.0507	-1.88	-0.3674	-1.88	-0.4261	-1.88	0.2524	-1.88	-0.3240	-1.88	-0.6029
-1.25	-0.2129	-1.25	-0.5302	-1.25	-0.6078	-1.25	0.1784	-1.25	-0.5425	-1.25	-0.8072
-0.62	-0.5209	-0.62	0.9182	-0.62	0.8519	-0.62	-0.1156	-0.62	0.8964	-0.62	-0.9403
0.00	1.1382	0.00	0.4217	0.00	1.0200	0.00	1.1632	0.00	0.4247	0.00	0.9771
0.31	0.4822	0.31	0.2460	0.31	0.4940	0.31	0.2442	0.31	0.2457	0.31	0.6039
0.62	0.2019	0.62	0.2116	0.62	0.3329	0.62	0.0902	0.62	0.1954	0.62	0.4078
1.25	0.1489	1.25	0.1192	1.25	0.2443	1.25	-0.0296	1.25	0.1199	1.25	0.3103
2.50	0.0706	2.50	0.1142	2.50	0.1780	2.50	-0.0494	2.50	0.1015	2.50	0.2501
3.12	0.0895	3.12	0.0877	3.12	0.1660	3.12	-0.0022	3.12	0.0884	3.12	0.2363
4.38	0.0390	4.38	0.0298	4.38	0.1447	4.38	-0.0469	4.38	0.0314	4.38	0.2010
5.00	-0.0485	5.00	-0.0240	5.00	0.1487	5.00	-0.1024	5.00	-0.0182	5.00	0.2010
7.50	-0.0844	7.50	-0.0372	7.50	0.1084	7.50	-0.1610	7.50	-0.0493	7.50	0.1820
10.00	-0.0880	10.00	-0.0529	10.00	0.0309	10.00	-0.1833	10.00	-0.0647	10.00	0.0531
12.50	-0.1129	12.50	-0.0974	12.50	-0.0577	12.50	-0.1489	12.50	-0.0867	12.50	-0.0173
15.00	-0.0877	15.00	-0.0880	15.00	-0.0745	15.00	-0.1397	15.00	-0.0885	15.00	-0.0463
30.00	-0.1145	30.00	-0.0962	30.00	-0.0782	30.00	-0.1194	30.00	-0.0944	30.00	-0.0727
40.00	-0.0965	40.00	-0.0824	40.00	-0.0856	40.00	-0.1156	40.00	-0.1039	40.00	-0.0716
50.00	-0.1011	50.00	-0.0893	50.00	-0.0830	50.00	-0.1038	50.00	-0.0922	50.00	-0.0952
60.00	-0.1018	60.00	-0.0840	60.00	-0.0924	60.00	-0.1194	60.00	-0.1012	60.00	-0.0943
70.00	-0.0932	70.00	-0.0893	70.00	-0.0771	70.00	-0.0916	70.00	-0.0897	70.00	-0.0827
90.00	-0.0684	90.00	-0.0698	90.00	-0.0901	90.00	-0.0610	90.00	-0.0647	90.00	-0.0993
122.00	-0.0117	122.00	-0.0148	122.00	-0.0148	122.00	-0.0209	122.00	-0.0097	122.00	-0.0097
139.00	0.0020	139.00	-0.0057	139.00	-0.0117	139.00	-0.0117	139.00	-0.0043	139.00	-0.0163
											-0.0032

mfr = 0.95 and $\alpha = 3.0^\circ$

$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-3.75	0.3175	-3.75	0.0596	-3.75	-0.5046	-3.75	0.0056	-3.75	-0.5046	-3.75	0.0056
-3.12	0.3477	-3.12	0.1913	-3.12	-0.5723	-3.12	0.0341	-3.12	-0.5723	-3.12	0.0341
-1.88	0.3308	-1.88	-0.3157	-1.88	-0.7790	-1.88	0.0660	-1.88	-0.7790	-1.88	0.0660
-1.25	0.3188	-1.25	-0.4987	-1.25	-0.8918	-1.25	0.0771	-1.25	-0.8918	-1.25	0.0771
0.00	1.1869	0.00	0.8808	0.00	0.9642	0.00	1.242	0.00	0.9642	0.00	1.242
0.31	0.0738	0.31	0.3835	0.31	0.2932	0.31	0.2556	0.31	0.2932	0.31	0.2556
0.62	-0.0614	0.62	0.2514	0.62	0.6619	0.62	0.2418	0.62	0.6619	0.62	0.2418
1.25	-0.0836	1.25	0.2879	1.25	0.4817	1.25	0.2872	1.25	0.4817	1.25	0.2872
2.50	-0.1342	2.50	0.0930	2.50	0.3456	2.50	0.3449	2.50	0.3456	2.50	0.3449
3.12	-0.1254	3.12	0.1410	3.12	0.2894	3.12	0.2894	3.12	0.2894	3.12	0.2894
4.38	-0.1364	4.38	0.0321	4.38	0.2584	4.38	0.2584	4.38	0.2584	4.38	0.2584
5.00	-0.1946	5.00	-0.0993	5.00	0.2496	5.00	0.2496	5.00	-0.0993	5.00	0.2496
7.50	-0.2416	7.50	-0.0995	7.50	0.1991	7.50	0.1991	7.50	-0.0995	7.50	0.1991
10.00	-0.2053	10.00	-0.0746	10.00	0.1062	10.00	0.1062	10.00	-0.0746	10.00	0.1062
12.50	-0.1901	12.50	-0.0875	12.50	0.0044	12.50	0.0044	12.50	-0.0875	12.50	0.0044
15.00	-0.1652	15.00	-0.0956	15.00	-0.0274	15.00	-0.0274	15.00	-0.0956	15.00	-0.0274
30.00	-0.1469	30.00	-0.0941	30.00	-0.0520	30.00	-0.0520	30.00	-0.0941	30.00	-0.0520
40.00	-0.1202	40.00	-0.0982	40.00	-0.0663	40.00	-0.0663	40.00	-0.0982	40.00	-0.0663
50.00	-0.1231	50.00	-0.0926	50.00	-0.0765	50.00	-0.0765	50.00	-0.0926	50.00	-0.0765
60.00	-0.1120	60.00	-0.0967	60.00	-0.0784	60.00	-0.0784	60.00	-0.0967	60.00	-0.0784
70.00	-0.1091	70.00	-0.0908	70.00	-0.0681	70.00	-0.0681	70.00	-0.0908	70.00	-0.0681
90.00	-0.0604	90.00	-0.0680	90.00	-0.0872	90.00	-0.0872	90.00	-0.0680	90.00	-0.0872
122.00	-0.0170	122.00	-0.0216	122.00	-0.0162	122.00	-0.0162	122.00	-0.0216	122.00	-0.0162
139.00	-0.0021	139.00	-0.0151	139.00	-0.0037	139.00	-0.0037	139.00	-0.0151	139.00	-0.0037

TABLE V. Continued
(c) Concluded

$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 90^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-3.75	0.8860	166.70	0.0158	-3.75	0.8818	166.70	0.0236	-3.75	0.7610	166.70	0.0212
-3.12	0.8927	183.30	0.0306	-3.12	0.8733	183.30	0.0313	-3.12	0.7803	183.30	0.0367
-1.88	0.9448	200.00	0.0477	-1.88	0.9319	200.00	0.0509	-1.88	0.8125	200.00	0.0560
-1.25	0.9643	216.70	0.0728	-1.25	0.9433	216.70	0.0683	-1.25	0.8106	216.70	0.0814
0.00	1.0384	238.90	0.1243	0.00	1.0700	238.90	0.1263	0.00	0.9021	238.90	0.1359
0.31	-0.9999	255.60	0.1887	0.62	-1.0389	255.60	0.1903	0.00	1.1829	255.60	0.1990
0.62	-1.0874	272.20	0.3054	1.25	-1.0183	266.70	0.2611	0.31	-0.7015	266.70	0.2692
1.25	-1.0636	277.80	0.3608	1.88	-0.9618	272.20	0.3128	0.62	-0.7681	272.20	0.3137
3.12	-0.8974	283.30	0.4255	2.50	-0.9280	277.80	0.3679	1.25	-0.7011	277.80	0.3681
4.38	-0.7516			3.12	-0.8154	283.30	0.4349	2.50	-0.5741	283.30	0.4309
5.00	-0.7312			5.00	-0.7185	3.75	-0.7535	4.38	-0.5211	4.38	-0.2937
7.50	-0.6894			7.50	-0.6793	4.38	-0.7859	5.00	-0.2684	5.00	-0.3067
10.00	-0.6522			10.00	-0.5881	5.00	-0.7642	7.50	-0.3119	7.50	-0.2425
12.50	-0.4211			15.00	-0.1315	7.50	-0.7320	10.00	-0.2484	10.00	-0.1888
15.00	-0.1300			17.50	-0.1833	15.00	-0.1465	12.50	-0.2376	12.50	-0.1987
30.00	-0.1620			20.00	-0.1501	17.50	-0.1216	15.00	-0.2011	15.00	-0.1456
40.00	-0.1360			40.00	-0.1451	20.00	-0.1543	30.00	-0.1545	30.00	-0.1359
50.00	-0.1430			50.00	-0.1296	40.00	-0.1533	40.00	-0.1230	40.00	-0.1226
60.00	-0.1306			60.00	-0.1135	50.00	-0.1433	50.00	-0.1218	50.00	-0.1173
70.00	-0.1217			70.00	-0.1166	60.00	-0.1345	60.00	-0.1126	60.00	-0.1047
90.00	-0.0856			80.00	-0.1173	70.00	-0.1141	70.00	-0.1088	70.00	-0.1095
122.00	-0.0245			90.00	-0.0873	80.00	-0.1200	90.00	-0.0792	80.00	-0.0854
139.00	-0.0051			122.00	-0.0237	90.00	-0.0827	122.00	-0.0180	90.00	-0.0670
				139.00	-0.0167	139.00	-0.0245	139.00	-0.0061	139.00	-0.0232
						139.00	-0.0207				

mfr = 0.78 and $\alpha = 0^\circ$

mfr = 0.70 and $\alpha = 0^\circ$

TABLE V. Continued

(e) $M = 0.92$

$mfr = 0.87$ and $\alpha = 0^\circ$ $mfr = 0.83$ and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	CP	Afterbody X/L	Forebody X/L	CP	Afterbody X/L	Forebody X/L	CP	Afterbody X/L
-3.75	1.0836	166.70	-3.75	1.0847	166.70	-3.75	1.0897	166.70
-3.12	1.0956	183.30	-3.12	1.0954	183.30	-3.12	1.1006	183.30
-1.88	1.1406	200.00	-1.88	1.1350	200.00	-1.88	1.1344	200.00
-1.25	1.1641	216.70	-1.25	1.1622	216.70	-1.25	1.1605	216.70
-0.62	1.2100	238.90	0.00	0.5484	0.00	-0.62	1.2143	238.90
0.00	0.3029	255.60	0.62	-1.2859	0.00	0.00	0.0958	255.60
0.31	-1.2646	266.70	1.25	-1.2211	0.62	-0.62	-1.2722	266.70
0.62	-1.2931	272.20	1.88	-1.1762	1.25	-1.2298	-1.1987	272.20
1.25	-1.2463	277.80	2.50	-1.1347	1.88	-1.1948	-1.1948	277.80
2.50	-1.1256	283.30	3.12	-1.0813	2.50	-1.1278	-1.1278	283.30
3.12	-1.1154		4.38	-1.0079	3.12	-1.0992		
4.38	-0.9668		5.00	-0.9787	3.75	-1.0403		
5.00	-0.9761		7.50	-0.9177	4.38	-1.0201		
7.50	-0.9087		10.00	-0.8316	5.00	-0.9898		
10.00	-0.8554		15.00	-0.7406	7.50	-0.9128		
12.50	-0.8188		17.50	-0.6761	15.00	-0.7441		
15.00	-0.7520		20.00	-0.5573	17.50	-0.6775		
30.00	-0.5420		40.00	-0.4616	20.00	-0.5730		
40.00	-0.5048		50.00	-0.3052	40.00	-0.5020		
50.00	-0.3886		60.00	-0.0351	50.00	-0.4064		
60.00	-0.0351		70.00	-0.0204	60.00	-0.0348		
70.00	-0.0144		80.00	-0.0402	70.00	-0.0247		
90.00	-0.0365		90.00	-0.0369	80.00	-0.0454		
122.00	-0.0039		122.00	-0.0088	90.00	-0.0331		
139.00	0.0038		139.00	-0.0032	122.00	-0.0110		
					139.00	-0.0081		

$mfr = 0.71$ and $\alpha = 0^\circ$ $mfr = 0.77$ and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	CP	Afterbody X/L	Forebody X/L	CP	Afterbody X/L	Forebody X/L	CP	Afterbody X/L
-3.75	0.9174	166.70	-3.75	0.9147	166.70	-3.75	0.8157	166.70
-3.12	0.9282	183.30	-3.12	0.9228	183.30	-3.12	0.8134	183.30
-1.88	0.9655	200.00	-1.88	0.9537	200.00	-1.88	0.8554	200.00
-1.25	0.9864	216.70	-1.25	0.9732	216.70	-1.25	0.8620	216.70
-0.62	1.0693	238.90	0.00	0.1995	0.00	-0.62	0.9040	238.90
0.00	1.0081	255.60	0.62	-0.9094	0.00	0.00	0.9429	255.60
0.31	-0.8623	266.70	1.25	-0.8691	0.62	-0.62	-0.8630	266.70
0.62	-0.9840	272.20	1.88	-0.7880	1.25	-0.8445	-0.7880	272.20
1.25	-0.8800	277.80	2.50	-0.8041	1.88	-0.7731	-0.7731	277.80
2.50	-0.7898	283.30	3.12	-0.7476	2.50	-0.8084	-0.8084	283.30
3.12	-0.6927		4.38	-0.6868	3.12	-0.7276		
4.38	-0.6923		5.00	-0.6022	3.75	-0.6889		
5.00	-0.6104		7.50	-0.6016	4.38	-0.6653		
7.50	-0.6248		10.00	-0.5456	5.00	-0.6548		
10.00	-0.5553		15.00	-0.4730	7.50	-0.6156		
12.50	-0.5300		17.50	-0.4260	15.00	-0.5102		
15.00	-0.4922		20.00	-0.1240	17.50	-0.4287		
30.00	-0.1813		40.00	-0.0632	20.00	-0.2242		
40.00	-0.0530		50.00	-0.1110	40.00	-0.0797		
50.00	-0.1084		60.00	-0.1228	50.00	-0.1144		
60.00	-0.1225		70.00	-0.1145	60.00	-0.1289		
70.00	-0.1195		80.00	-0.1170	70.00	-0.1127		
90.00	-0.0817		90.00	-0.0889	80.00	-0.1219		
122.00	-0.0109		122.00	-0.0130	90.00	-0.0780		
139.00	0.0035		139.00	0.0025	122.00	-0.0140		
					139.00	-0.0045		

TABLE V. Concluded

(e) Concluded

mfr = 0.98 and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 90^\circ$			$\phi = 180^\circ$		
Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP
-3.75	166.70	0.0465	-3.75	166.70	0.0465	-3.75	166.70	0.0465
-3.12	183.30	0.0632	-3.12	183.30	0.0632	-3.12	183.30	0.0632
-1.88	200.00	0.0824	-1.88	200.00	0.0824	-1.88	200.00	0.0824
-1.25	216.70	0.1135	-1.25	216.70	0.1135	-1.25	216.70	0.1135
-0.62	238.90	0.1725	0.00	238.90	0.1725	-0.62	238.90	0.1689
0.00	255.60	0.2355	0.62	255.60	0.2355	0.00	255.60	0.2346
0.31	266.70	0.2994	1.25	266.70	0.2994	0.62	266.70	0.3025
0.62	272.20	0.3411	1.88	272.20	0.3411	1.25	272.20	0.3463
1.25	277.80	0.3886	2.50	277.80	0.3886	1.88	277.80	0.3959
2.50	283.30	0.4455	3.12	283.30	0.4455	2.50	283.30	0.4531
3.12	0.1711		4.38	0.1099		3.12	0.1864	
4.38	0.1003		5.00	0.0846		3.75	0.1239	
5.00	0.0615		7.50	-0.0107		4.38	0.1031	
7.50	-0.0258		10.00	-0.0462		5.00	0.1068	
10.00	-0.0393		15.00	-0.0591		7.50	-0.0212	
12.50	-0.0882		17.50	-0.1092		15.00	-0.1001	
15.00	-0.0579		20.00	-0.1017		17.50	-0.1297	
30.00	-0.1140		40.00	-0.1129		20.00	-0.1135	
40.00	-0.0984		50.00	-0.1107		40.00	-0.1122	
50.00	-0.1161		60.00	-0.1102		50.00	-0.1213	
60.00	-0.1134		70.00	-0.0989		60.00	-0.1122	
70.00	-0.0996		80.00	-0.1011		70.00	-0.0923	
90.00	-0.0660		90.00	-0.0771		80.00	-0.1070	
122.00	0.0020		122.00	-0.0030		90.00	-0.0643	
139.00	0.0196		139.00	0.0122		122.00	-0.0001	
						139.00	0.0062	

TABLE VI. PRESSURE COEFFICIENTS ON MODEL WITH NACA 1-85-43.9 INLET AND CONTRACTION RATIO OF 1.250

(a) $M = 0.60$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0366	343.16	-0.0610	-187.47	1.0403	343.16	-0.0541	-187.47	1.0318	343.16	-0.0486	-187.47	0.9909	343.16	-0.0453
-171.29	1.0377	384.14	-0.0594	-171.29	1.0243	384.14	-0.0573	-171.29	1.0327	384.14	-0.0529	-171.29	0.9935	384.14	-0.0432
-155.11	1.0377	419.13	-0.0573	-155.11	1.0312	419.13	-0.0503	-155.11	1.0312	419.13	-0.0497	-155.11	0.9898	419.13	-0.0400
-130.84	1.0298	457.12	-0.0557	-130.84	1.0239	457.12	-0.0557	-130.84	1.0239	457.12	-0.0465	-130.84	0.9783	457.12	-0.0356
-106.57	1.0220	507.77	-0.0530	-106.57	1.0145	507.77	-0.0557	-106.57	1.0145	507.77	-0.0496	-106.57	0.9568	507.77	-0.0352
-90.39	1.0120	545.76	-0.0536	-90.39	1.0009	545.76	-0.0589	-90.39	0.9738	545.76	-0.0465	-90.39	0.9375	545.76	-0.0176
-74.21	1.0015	571.08	-0.0461	-74.21	1.0111	571.08	-0.0536	-74.21	0.9910	571.08	-0.0311	-74.21	0.9129	571.08	0.0033
-58.03	0.9884	583.74	-0.0455	-58.03	1.0270	583.74	-0.0461	-58.03	0.9743	583.74	-0.0226	-58.03	0.8872	583.74	0.0236
-41.85	0.9842	596.41	-0.0375	-41.85	1.0541	596.41	-0.0305	-41.85	0.9655	596.41	-0.0183	-41.85	0.8615	596.41	0.0417
-33.76	0.9883	609.07	-0.0241	-33.76	1.0895	609.07	-0.0182	-33.76	0.9607	609.07	0.0189	-33.76	0.8488	609.07	0.0888
-25.67	0.9954			-25.67	1.0777			-25.67	0.9678			-25.67	0.8535		
-23.11	1.0007			-23.11	1.1173			-23.11	0.9754			-23.11	0.8582		
-17.97	1.0214			-17.97	1.1671			-17.97	0.9977			-17.97	0.8901		
-10.27	1.0722			-10.27	1.1970			-10.27	1.0588			-10.27	0.9862		
-5.13	1.0833			-5.13	1.1808			-5.13	1.0892			-5.13	1.0774		
-3.34	1.0343			-3.34	1.1840			-3.34	1.0560			-3.34	1.0873		
-2.05	0.9166			-2.05	1.1707			-2.05	0.9331			-2.05	1.0434		
-0.90	0.6353			-0.90	1.1643			-0.90	0.6852			-0.90	0.8461		
-0.44	0.3284			-0.44	1.1731			-0.44	0.3882			-0.44	0.3925		
0.00	-1.0201			0.00	-1.1547			0.00	-0.9112			0.00	-0.6269		
0.31	-1.2174			0.31	-1.2993			0.31	-1.8324			0.31	-2.1421		
0.63	-2.0895			0.63	-1.2928			0.63	-1.9657			0.63	-2.2311		
1.25	-1.9850			1.25	-1.2436			1.25	-1.6925			1.25	-2.0463		
1.88	-2.0336			20.00	-1.1322			1.88	-1.6841			1.88	-2.2358		
2.50	-1.9369			50.00	-0.6873			2.50	-1.8628			2.50	-2.0484		
3.13	-1.8858			60.00	-0.5225			3.13	-1.5362			3.13	-2.0099		
3.75	-1.8098			70.00	-0.3973			3.75	-1.6427			3.75	-1.9689		
4.37	-1.7760			80.00	-0.3448			4.37	-1.6594			4.37	-1.8239		
5.00	-1.7291			90.00	-0.2993			5.00	-1.6290			5.00	-1.7760		
6.25	-1.6384			100.00	-0.2680			6.25	-1.6710			6.25	-1.5917		
7.50	-1.5951			110.00	-0.2208			7.50	-1.6484			7.50	-1.4833		
8.75	-1.4707			241.85	-0.0724			8.75	-1.6306			8.75	-1.2232		
10.00	-1.4913							10.00	-1.5661			10.00	-1.0894		
12.50	-1.1747							12.50	-1.4791			12.50	-0.9288		
15.00	-1.2063							15.00	-1.3857			15.00	-0.7913		
17.50	-1.2069							17.50	-1.3076			17.50	-0.7484		
20.00	-1.2007							20.00	-1.0766			20.00	-0.7270		
30.00	-1.0655							30.00	-0.6607			30.00	-0.5405		
40.00	-0.8681							40.00	-0.5992			40.00	-0.4740		
50.00	-0.6113							50.00	-0.4756			50.00	-0.4284		
60.00	-0.4926							60.00	-0.4224			60.00	-0.4054		
70.00	-0.4180							70.00	-0.3826			70.00	-0.3787		
80.00	-0.3202							80.00	-0.3473			80.00	-0.3528		
90.00	-0.3165							90.00	-0.3076			90.00	-0.3206		
100.00	-0.2651							100.00	-0.2640			100.00	-0.2582		
110.00	-0.2305							110.00	-0.2237			110.00	-0.2059		
241.85	-0.0817							241.85	-0.0805			241.85	-0.0757		
279.84	-0.0650							279.84	-0.0700			279.84	-0.0652		

TABLE VI. Continued

(a) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
mfr = 0.50 and $\alpha = 0^\circ$				mfr = 0.50 and $\alpha = 1.0^\circ$				mfr = 0.50 and $\alpha = 2.0^\circ$				mfr = 0.50 and $\alpha = 2.0^\circ$			
Forebody	Afterbody			Forebody	Afterbody			Forebody	Afterbody			Forebody	Afterbody		
XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP
-187.47	0.9328	343.16	-0.0307	-187.47	0.9328	343.16	-0.0222	-187.47	0.9350	343.16	-0.0445	-187.47	0.9328	343.16	-0.0370
-171.29	0.9370	384.14	-0.0286	-106.57	0.8751	384.14	-0.0238	-106.57	0.9376	384.14	-0.0413	-106.57	0.9376	384.14	-0.0397
-155.11	0.9302	419.13	-0.0222	-25.67	0.6658	419.13	-0.0168	-155.11	0.9335	419.13	-0.0381	-155.11	0.9324	419.13	-0.0251
-130.84	0.9129	457.12	-0.0147	-10.27	0.8362	457.12	-0.0147	-130.84	0.9141	457.12	-0.0328	-130.84	0.9147	457.12	-0.0267
-96.57	0.8773	507.77	-0.0035	-2.05	1.0889	507.77	0.0045	-106.57	0.8843	507.77	-0.0173	-106.57	0.8824	507.77	-0.0269
-90.39	0.8443	545.76	0.0189	0.00	-0.1281	545.76	0.0227	-90.39	0.8504	545.76	0.0008	-90.39	0.8490	545.76	0.0074
-74.21	0.8035	571.08	0.0419	0.31	-1.4858	571.08	0.0552	-74.21	0.8143	571.08	0.0296	-74.21	0.8166	571.08	0.0329
-58.03	0.7580	583.74	0.0649	0.63	-2.2251	583.74	0.0814	-58.03	0.7714	583.74	0.0520	-58.03	0.7744	583.74	0.0584
-41.85	0.7077	596.41	0.0980	1.25	-2.0782	596.41	0.1092	-41.85	0.7228	596.41	0.0856	-41.85	0.7322	596.41	0.0834
-33.76	0.6870	609.07	0.1734	1.88	-2.0493	609.07	0.1707	-33.76	0.7014	609.07	0.1395	-33.76	0.7183	609.07	0.1366
-25.67	0.6640			2.50	-2.1090			-25.67	0.6826			-25.67	0.7119		
-23.11	0.6711			3.13	-1.6317			-23.11	0.6997			-23.11	0.7183		
-17.97	0.7011			3.75	-1.2079			-17.97	0.7291			-17.97	0.7559		
-10.27	0.8391			4.37	-1.0236			-10.27	0.8693			-10.27	0.8934		
-5.13	1.0039			5.00	-0.9589			-5.13	1.0217			-5.13	1.0479		
-3.34	1.0713			6.25	-0.8193			-3.34	1.0797			-3.34	1.0855		
-2.05	0.9928			7.50	-0.8591			-2.05	1.0847			-2.05	1.0719		
-0.90	0.9585			8.75	-0.7815			-0.90	0.9525			-0.90	0.9185		
-0.44	0.8172			10.00	-0.7801			-0.44	0.7710			-0.44	0.7128		
0.00	-0.2167			12.50	-0.7513			0.00	-0.3640			0.00	-0.4617		
0.31	-1.6150			15.00	-0.6965			0.31	-1.8075			0.31	-2.0331		
0.63	-2.1953			17.50	-0.6387			0.63	-2.3599			0.63	-2.4798		
1.25	-2.1593			20.00	-0.5827			1.25	-2.1975			1.25	-2.3094		
1.88	-2.0709			30.00	-0.4838			1.88	-2.2385			1.88	-2.2936		
2.50	-1.8876			50.00	-0.4078			2.50	-2.0751			2.50	-2.2412		
3.13	-1.5740			60.00	-0.4024			3.13	-2.0231			3.13	-2.0378		
3.75	-1.1662			70.00	-0.3665			3.75	-1.5316			3.75	-1.9160		
4.37	-1.0762			80.00	-0.3600			4.37	-1.3892			4.37	-1.7828		
5.00	-0.9462			90.00	-0.3058			5.00	-1.3981			5.00	-1.5846		
6.25	-0.9031			100.00	-0.2622			6.25	-1.0891			6.25	-1.4457		
7.50	-0.8207			110.00	-0.1956			7.50	-0.8778			7.50	-1.1442		
8.75	-0.8417			241.85	-0.0651			8.75	-0.8757			8.75	-1.0839		
10.00	-0.7831							10.00	-0.8491			10.00	-0.9911		
12.50	-0.7579							12.50	-0.7780			12.50	-0.8716		
15.00	-0.7129							15.00	-0.7256			15.00	-0.7730		
17.50	-0.6569							17.50	-0.6666			17.50	-0.7146		
20.00	-0.5992							20.00	-0.6478			20.00	-0.6596		
30.00	-0.5046							30.00	-0.5219			30.00	-0.5435		
40.00	-0.4453							40.00	-0.4774			40.00	-0.4859		
50.00	-0.4271							50.00	-0.4278			50.00	-0.4413		
60.00	-0.4038							60.00	-0.4144			60.00	-0.4182		
70.00	-0.3518							70.00	-0.3883			70.00	-0.3912		
80.00	-0.3544							80.00	-0.3576			80.00	-0.3560		
90.00	-0.3178							90.00	-0.3232			90.00	-0.3177		
100.00	-0.2512							100.00	-0.2342			100.00	-0.2562		
110.00	-0.1801							110.00	-0.2061			110.00	-0.2061		
241.85	-0.0675							241.85	-0.0459			241.85	-0.0677		
279.84								279.84	-0.0335			279.84	-0.0579		

TABLE VI. Continued

(a) Continued

mfr = 0.50 and $\alpha = 3.0^\circ$				mfr = 0.56 and $\alpha = 0^\circ$				mfr = 0.63 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.9353	343.16	-0.0422	-187.47	0.9275	343.16	-0.0342	-187.47	0.8370	343.16	-0.0253
-171.29	0.9343	384.14	-0.0455	-106.57	0.8712	384.14	-0.0315	-171.29	0.8403	384.14	-0.0253
-155.11	0.9322	419.13	-0.0401	-25.67	0.5897	419.13	-0.0181	-155.11	0.8335	419.13	-0.0141
-130.84	0.9343	457.12	-0.0277	-10.27	0.7147	457.12	-0.0175	-130.84	0.8016	457.12	-0.0130
-106.57	0.8822	507.77	-0.0052	-2.05	1.0732	507.77	-0.0009	-106.57	0.7451	507.77	0.0089
-90.39	0.8501	545.76	0.0104	0.00	0.3156	545.76	0.0200	-90.39	0.6891	545.76	0.0367
-74.21	0.8143	571.08	0.0388	0.31	-0.8420	571.08	0.0560	-74.21	0.6225	571.08	0.0772
-58.03	0.7785	583.74	0.0549	0.63	-1.3031	583.74	0.0855	-58.03	0.5419	583.74	0.1109
-41.85	0.7438	596.41	0.0796	1.25	-1.3037	596.41	0.1263	-41.85	0.4461	596.41	0.1526
-33.76	0.7266	609.07	0.1258	1.88	-1.0631	609.07	0.1994	-33.76	0.4068	609.07	0.2343
-25.67	0.7165			2.50	-0.9096			-25.67	0.3479		
-23.11	0.7449			3.13	-0.7404			-23.11	0.3402		
-17.97	0.7269			3.75	-0.6365			-17.97	0.3803		
-10.27	0.9269			4.37	-0.6335			-10.27	0.5629		
-5.13	1.0627			5.00	-0.6033			-5.13	0.7975		
-3.34	1.0895			6.25	-0.5365			-3.34	0.9335		
-2.05	1.0702			7.50	-0.5589			-2.05	1.0702		
-0.90	0.8788			8.75	-0.5291			-0.90	1.0521		
-0.44	0.6675			10.00	-0.5032			-0.44	1.0861		
0.00	-0.6260			12.50	-0.5210			0.00	-0.4644		
0.31	-2.1944			15.00	-0.4925			0.31	-1.1270		
0.63	-2.3558			17.50	-0.4547			0.63	-1.3959		
1.25	-2.1336			20.00	-0.4227			1.25	-1.7159		
1.88	-2.2865			30.00	-0.3563			1.88	-1.0201		
2.50	-2.1643			50.00	-0.3255			2.50	-0.9320		
3.13	-2.0749			60.00	-0.3208			3.13	-0.8704		
3.75	-2.0326			70.00	-0.3113			3.75	-0.7079		
4.37	-1.8510			80.00	-0.2947			4.37	-0.6243		
5.00	-1.8436			90.00	-0.2722			5.00	-0.5558		
6.25	-1.6330			100.00	-0.2106			6.25	-0.6207		
7.50	-1.4659			110.00	-0.1644			7.50	-0.5984		
8.75	-1.3849			241.85	-0.0485			8.75	-0.5341		
10.00	-1.1859							10.00	-0.5984		
12.50	-1.0404							12.50	-0.5836		
15.00	-0.9087							15.00	-0.5341		
17.50	-0.8581							17.50	-0.4705		
20.00	-0.8056							20.00	-0.4682		
30.00	-0.5750							30.00	-0.4004		
40.00	-0.4955							40.00	-0.3509		
50.00	-0.4577							50.00	-0.3498		
60.00	-0.4247							60.00	-0.3274		
70.00	-0.3895							70.00	-0.3274		
80.00	-0.3575							80.00	-0.3150		
90.00	-0.3203							90.00	-0.2797		
100.00	-0.2555							100.00	-0.2237		
110.00	-0.2077							110.00	-0.1724		
241.85	-0.0672							241.85	-0.0544		
279.84	-0.0560							279.84	-0.0470		

TABLE VI. Continued

(a) Continued

mfr = 0.69 and $\alpha = 0^\circ$				mfr = 0.69 and $\alpha = 2.0^\circ$				mfr = 0.75 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.7769	343.16	-0.0235	-187.47	0.7766	343.16	-0.0138	-187.47	0.7721	343.16	-0.0140
-171.29	0.7759	384.14	-0.0165	-171.29	0.7786	384.14	-0.0117	-171.29	0.7168	384.14	-0.0082
-155.11	0.7680	419.13	-0.0096	-155.11	0.7697	419.13	-0.0058	-155.11	0.6996	419.13	-0.0013
-130.84	0.7280	457.12	0.0081	-130.84	0.7326	457.12	0.0047	-130.84	0.6557	457.12	0.0163
-106.57	0.6580	507.77	0.0312	-106.57	0.6644	507.77	0.0215	-106.57	0.5666	507.77	0.0444
-90.39	0.5850	545.76	0.0644	-90.39	0.5930	545.76	0.0701	-90.39	0.4750	545.76	0.0795
-74.21	0.5046	571.08	0.1111	-74.21	0.5138	571.08	0.1140	-74.21	0.3745	571.08	0.1257
-58.03	0.3932	583.74	0.1427	-58.03	0.4147	583.74	0.1487	-58.03	0.2344	583.74	0.1577
-41.85	0.2744	596.41	0.1889	-41.85	0.3057	596.41	0.1879	-41.85	0.0734	596.41	0.2007
-33.76	0.2013	609.07	0.2322	-33.76	0.2659	609.07	0.2457	-33.76	-0.0232	609.07	0.2645
-25.67	0.1084			-25.67	0.1880			-25.67	-0.1369		
-23.11	0.0952			-23.11	0.1921			-23.11	-0.1640		
-17.97	0.1332			-17.97	0.2181			-17.97	-0.1433		
-10.27	0.3320			-10.27	0.4387			-10.27	0.0788		
-5.13	0.6436			-5.13	0.7133			-5.13	0.4573		
-3.34	0.8156			-3.34	0.8600			-3.34	0.6382		
-2.05	0.9826			-2.05	0.9943			-2.05	0.8541		
-0.90	1.0812			-0.90	1.0925			-0.90	1.0486		
-0.44	1.0756			-0.44	0.9906			-0.44	1.0929		
0.00	0.9907			0.00	0.4946			0.00	0.7917		
0.31	0.4199			0.31	-0.4443			0.31	-0.0801		
0.63	-0.8051			0.63	-1.3211			0.63	-0.3986		
1.25	-0.8146			1.25	-0.3981			1.25	-0.4058		
1.88	-0.6900			1.88	-1.1351			1.88	-0.3939		
2.50	-0.5765			2.50	-0.3325			2.50	-0.3819		
3.13	-0.5797			3.13	-0.3319			3.13	-0.4064		
3.75	-0.5329			3.75	-0.3159			3.75	-0.3340		
4.37	-0.4898			4.37	-0.2964			4.37	-0.3512		
5.00	-0.4371			5.00	-0.2698			5.00	-0.3397		
6.25	-0.4882			6.25	-0.2083			6.25	-0.3324		
7.50	-0.4625			7.50	-0.1621			7.50	-0.3288		
8.75	-0.4972			8.75	-0.0888			8.75	-0.3986		
10.00	-0.4551			10.00	-0.5933			10.00	-0.3876		
12.50	-0.4609			12.50	-0.6079			12.50	-0.3808		
15.00	-0.4602			15.00	-0.6359			15.00	-0.3695		
17.50	-0.4283			17.50	-0.5288			17.50	-0.3777		
20.00	-0.4006			20.00	-0.5325			20.00	-0.3296		
30.00	-0.3605			30.00	-0.4245			30.00	-0.3204		
40.00	-0.3479			40.00	-0.4378			40.00	-0.3271		
50.00	-0.3322			50.00	-0.3846			50.00	-0.3017		
60.00	-0.3285			60.00	-0.3982			60.00	-0.3007		
70.00	-0.3183			70.00	-0.3514			70.00	-0.2976		
80.00	-0.2981			80.00	-0.3398			80.00	-0.2904		
90.00	-0.2686			90.00	-0.2856			90.00	-0.2580		
100.00	-0.2081			100.00	-0.2533			100.00	-0.1949		
110.00	-0.1635			110.00	-0.1797			110.00	-0.1485		
241.85	-0.0461			241.85	-0.0874			241.85	-0.0434		
279.84	-0.0411			279.84	-0.0806			279.84	-0.0452		

TABLE VI. Continued

(b) $M = 0.64$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0889	343.16	-0.0615	-187.47	1.0525	343.16	-0.0542	-187.47	1.0529	343.16	-0.0518	-187.47	1.0122	343.16	-0.0399
-171.29	1.0603	384.14	-0.0596	-171.29	1.0548	384.14	-0.0532	-106.57	1.0324	384.14	-0.0523	-171.29	1.0122	384.14	-0.0384
-155.11	1.0575	419.13	-0.0582	-155.11	1.0502	419.13	-0.0534	-106.57	0.9842	419.13	-0.0461	-155.11	1.0099	419.13	-0.0351
-130.84	1.0538	457.12	-0.0558	-130.84	1.0411	457.12	-0.0538	-106.57	0.9842	457.12	-0.0461	-130.84	0.9964	457.12	-0.0294
-106.57	1.0426	507.77	-0.0520	-106.57	1.0325	507.77	-0.0433	-2.05	0.9784	507.77	-0.0437	-106.57	0.9783	507.77	-0.0181
-90.39	1.0366	545.76	-0.0530	-90.39	1.0232	545.76	-0.0466	0.00	-0.6322	545.76	-0.0395	-90.39	0.9565	545.76	-0.0081
-74.21	1.0264	571.08	-0.0506	-74.21	1.0071	571.08	-0.0404	0.31	-1.7982	571.08	-0.0262	-74.21	0.9361	571.08	0.0203
-58.03	1.0148	583.74	-0.0397	-58.03	0.9971	583.74	-0.0195	0.63	-1.8164	583.74	-0.0091	-58.03	0.9059	583.74	0.0397
-41.85	1.0069	596.41	-0.0340	-41.85	0.9864	596.41	-0.0238	1.25	-1.4740	596.41	-0.0024	-41.85	0.8827	596.41	0.0534
-33.76	1.0101	609.07	-0.0132	-33.76	0.9826	609.07	0.0085	1.88	-1.3291	609.07	0.0456	-33.76	0.8753	609.07	0.1126
-25.67	1.0127			-25.67	0.9894			2.50	-1.1994			-25.67	0.8663		
-23.11	1.0211			-23.11	0.9947			3.13	-1.3324			-23.11	0.8785		
-17.97	1.0357			-17.97	1.0162			3.75	-1.2141			-17.97	0.9056		
-10.27	1.0896			-10.27	1.0775			4.37	-1.2589			-10.27	1.0055		
-5.13	1.0894			-5.13	1.1041			5.00	-1.4719			-5.13	1.0962		
-3.34	1.0482			-3.34	1.0717			6.25	-1.2578			-3.34	1.1067		
-2.05	0.9473			-2.05	0.9488			7.50	-1.2857			-2.05	1.0710		
-0.90	0.6702			-0.90	0.7285			8.75	-1.4943			-0.90	0.8824		
-0.44	0.3947			-0.44	0.4704			10.00	-1.3146			-0.44	0.6719		
0.00	-0.8431			0.00	-0.7553			12.50	-1.3478			0.00	-0.4912		
0.31	-1.9982			0.31	-1.7189			15.00	-1.2252			0.31	-1.9067		
0.63	-2.0276			0.63	-1.4758			17.50	-1.2536			0.63	-2.1579		
1.25	-1.9188			1.25	-1.5928			20.00	-1.2294			1.25	-2.0734		
1.88	-1.9375			1.88	-1.5174			30.00	-0.9853			1.88	-2.0220		
2.50	-1.8361			2.50	-1.5792			50.00	-0.4920			2.50	-2.1130		
3.13	-1.7885			3.13	-1.4271			60.00	-0.4223			3.13	-1.9443		
3.75	-1.7623			3.75	-1.4613			70.00	-0.3835			3.75	-1.9436		
4.37	-1.6715			4.37	-1.4159			80.00	-0.3164			4.37	-1.7910		
5.00	-1.6712			5.00	-1.4908			90.00	-0.2938			5.00	-1.7667		
6.25	-1.6194			6.25	-1.4482			100.00	-0.2508			6.25	-1.6009		
7.50	-1.5651			7.50	-1.5643			110.00	-0.2183			7.50	-1.5309		
8.75	-1.2924			8.75	-1.5287			241.85	-0.0762			8.75	-1.3829		
10.00	-1.2998			10.00	-1.4683							10.00	-1.3148		
12.50	-1.1243			12.50	-1.4149							12.50	-1.0427		
15.00	-1.0818			15.00	-1.4065							15.00	-0.9244		
17.50	-1.0794			17.50	-1.3396							17.50	-0.8335		
20.00	-1.1382			20.00	-1.2984							20.00	-0.8227		
30.00	-1.0467			30.00	-0.9154							30.00	-0.5460		
40.00	-0.9488			40.00	-0.6196							40.00	-0.4985		
50.00	-0.7866			50.00	-0.5214							50.00	-0.4532		
60.00	-0.6483			60.00	-0.4260							60.00	-0.4256		
70.00	-0.4620			70.00	-0.3918							70.00	-0.3807		
80.00	-0.4234			80.00	-0.3518							80.00	-0.3729		
90.00	-0.3181			90.00	-0.3156							90.00	-0.3366		
100.00	-0.2851			100.00	-0.2632							100.00	-0.2731		
110.00	-0.2331			110.00	-0.2267							110.00	-0.2062		
241.85	-0.0925			241.85	-0.0812							241.85	-0.0860		
279.84	-0.0837			279.84	-0.0735							279.84	-0.0707		

TABLE VI. Continued

(b) Continued

mfr = 0.80 and $\alpha = 0^\circ$				mfr = 0.55 and $\alpha = 0^\circ$				mfr = 0.62 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.9524	343.16	-0.0389	-187.47	0.9505	343.16	-0.0271	-187.47	0.8663	343.16	-0.0179
-171.29	0.9543	384.14	-0.0337	-171.29	0.9499	384.14	-0.0332	-171.29	0.8677	384.14	-0.0189
-155.11	0.9482	419.13	-0.0256	-155.11	0.6913	419.13	-0.0247	-155.11	0.8607	384.14	-0.0084
-130.84	0.9329	457.12	-0.0204	-102.7	0.8696	457.12	-0.0247	-130.84	0.8301	457.12	-0.0037
-106.57	0.8970	507.77	-0.0014	-106.57	0.8468	507.77	-0.0109	-106.57	0.7775	507.77	0.0243
-90.39	0.8649	545.76	0.0209	-90.39	0.8030	545.76	0.0129	-90.39	0.7249	545.76	0.0561
-74.21	0.8267	571.08	0.0609	-74.21	0.7560	571.08	0.0466	-74.21	0.6617	571.08	0.1002
-58.03	0.7796	583.74	0.0846	-58.03	0.6959	583.74	0.0799	-58.03	0.5803	583.74	0.1410
-41.85	0.7363	596.41	0.1222	-41.85	0.6340	596.41	0.1591	-41.85	0.4882	596.41	0.1889
-25.67	0.6871	609.07	0.1934	-25.67	0.6016	609.07	0.2284	-25.67	0.4416	609.07	0.2576
-23.11	0.6928			-23.11	0.5644			-23.11	0.3898		
-17.97	0.7243			-17.97	0.5665			-17.97	0.3819		
-10.27	0.8596			-10.27	0.5869			-10.27	0.4160		
-5.13	1.0277			-5.13	0.9552			-5.13	0.8379		
-3.34	1.0844			-3.34	1.0486			-3.34	0.9637		
-2.05	1.1042			-2.05	1.1014			-2.05	1.0740		
-0.90	1.0162			-0.90	1.0706			-0.90	1.1026		
-0.44	0.8621			-0.44	0.7664			-0.44	1.0329		
0.00	-0.1270			0.00	-0.7527			0.00	0.2986		
0.31	-1.4899			0.31	-1.4799			0.31	-0.8435		
0.63	-1.9780			0.63	-1.6908			0.63	-1.3891		
1.25	-2.1340			1.25	-1.8649			1.25	-1.2096		
1.88	-1.9467			1.88	-1.7484			1.88	-1.0717		
2.50	-1.9518			2.50	-1.6105			2.50	-1.0138		
3.13	-1.9940			3.13	-1.4188			3.13	-0.9061		
3.75	-1.7378			3.75	-0.9222			3.75	-0.7678		
4.37	-1.3850			4.37	-0.8871			4.37	-0.7014		
5.00	-1.2604			5.00	-0.8179			5.00	-0.7257		
6.25	-0.8804			6.25	-0.7650			6.25	-0.6318		
7.50	-0.7794			7.50	-0.7233			7.50	-0.6355		
8.75	-0.8206			8.75	-0.7701			8.75	-0.6505		
10.00	-0.7705			10.00	-0.7215			10.00	-0.6309		
12.50	-0.7182			12.50	-0.7065			12.50	-0.6192		
15.00	-0.7010			15.00	-0.6475			15.00	-0.5856		
17.50	-0.6189			17.50	-0.6033			17.50	-0.5026		
20.00	-0.5828			20.00	-0.5486			20.00	-0.4620		
30.00	-0.5076			30.00	-0.4622			30.00	-0.4189		
40.00	-0.4557			40.00	-0.4276			40.00	-0.3967		
50.00	-0.4242			50.00	-0.3994			50.00	-0.3784		
60.00	-0.4029			60.00	-0.3820			60.00	-0.3566		
70.00	-0.3779			70.00	-0.3673			70.00	-0.3487		
80.00	-0.3534			80.00	-0.3424			80.00	-0.3192		
90.00	-0.3161			90.00	-0.3026			90.00	-0.2896		
100.00	-0.2532			100.00	-0.2380			100.00	-0.2254		
110.00	-0.1969			110.00	-0.1890			110.00	-0.1757		
241.85	-0.0678			241.85	-0.0625			241.85	-0.0501		
279.84	-0.0601			279.84	-0.0531			279.84	-0.0429		

TABLE VI. Continued

(b) Concluded

mfr = 0.88 and $\alpha = 0^\circ$				mfr = 0.75 and $\alpha = 0^\circ$				mfr = 0.81 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L
-187.47	0.8042	343.16	-0.0216	-187.47	0.8013	343.16	-0.0121	-187.47	0.7367	343.16	-0.0040
-171.29	0.8046	384.14	-0.0126	-106.57	0.6906	384.14	-0.0131	-171.29	0.7417	384.14	-0.0021
-155.11	0.7976	419.13	-0.0036	-25.67	0.7127	419.13	0.0045	-155.11	0.6437	419.13	0.0050
-130.84	0.7603	457.12	0.0107	-106.57	0.4073	457.12	0.0116	-130.84	0.3863	457.12	0.0135
-106.57	0.6922	507.77	0.0416	-2.05	0.5966	507.77	0.0397	-106.57	0.4852	507.77	0.0486
-90.39	0.6195	545.76	0.0792	0.00	0.5695	545.76	0.0744	-90.39	0.3687	545.76	0.0880
-74.21	0.5402	571.08	0.1310	0.31	-0.3735	571.08	0.1283	-74.21	0.2391	571.08	0.1519
-58.03	0.4274	583.74	0.1676	0.63	-0.8610	583.74	0.1667	-58.03	0.0424	583.74	0.1861
-41.85	0.3090	596.41	0.2118	1.25	-0.8643	596.41	0.2090	-41.85	-0.1837	596.41	0.2285
-33.76	0.2504	609.07	0.2809	1.88	-0.7978	609.07	0.2842	-33.76	-0.3105	609.07	0.2937
-25.67	0.1607			2.50	-0.7600			-25.67	-0.4967		
-23.11	0.1428			3.13	-0.6259			-23.11	-0.4482		
-17.97	0.1727			3.75	-0.5902			-17.97	-0.4999		
-10.27	0.3690			4.37	-0.5526			-10.27	-0.1751		
-5.13	0.6575			5.00	-0.4747			-5.13	0.1884		
-3.34	0.8276			6.25	-0.5130			-3.34	0.4703		
-2.05	0.9713			7.50	-0.5036			-2.05	0.7115		
-0.90	1.0737			8.75	-0.5400			-0.90	0.9890		
-0.44	1.0633			10.00	-0.4763			-0.44	1.0947		
0.00	0.6060			12.50	-0.5067			0.00	0.9197		
0.31	-0.4558			15.00	-0.4905			0.31	0.2936		
0.63	-0.7969			17.50	-0.4585			0.63	-0.0550		
1.25	-0.8714			20.00	-0.4349			1.25	-0.0811		
1.88	-0.7482			30.00	-0.3761			1.88	-0.1767		
2.50	-0.6269			50.00	-0.3604			2.50	-0.1184		
3.13	-0.6106			60.00	-0.3388			3.13	-0.2116		
3.75	-0.5542			70.00	-0.3273			3.75	-0.1799		
4.37	-0.5570			80.00	-0.3084			4.37	-0.1855		
5.00	-0.5719			90.00	-0.2733			5.00	-0.2275		
6.25	-0.5225			100.00	-0.2124			6.25	-0.2312		
7.50	-0.4735			110.00	-0.1610			7.50	-0.2545		
8.75	-0.5672			241.85	-0.0517			8.75	-0.2671		
10.00	-0.5188							10.00	-0.3281		
12.50	-0.5020							12.50	-0.3193		
15.00	-0.5097							15.00	-0.3258		
17.50	-0.4684							17.50	-0.3002		
20.00	-0.4519							20.00	-0.2944		
30.00	-0.3622							30.00	-0.2946		
40.00	-0.3902							40.00	-0.2955		
50.00	-0.3444							50.00	-0.2988		
60.00	-0.3688							60.00	-0.2894		
70.00	-0.3220							70.00	-0.2937		
80.00	-0.3324							80.00	-0.2779		
90.00	-0.2759							90.00	-0.2484		
100.00	-0.2405							100.00	-0.1903		
110.00	-0.1594							110.00	-0.1431		
241.85	-0.0786							241.85	-0.0362		
279.84	-0.0676							279.84	-0.0252		

TABLE VI. Continued

(c) $M = 0.69$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP
-187.47	1.0780	343.16	-0.0544	-187.47	1.0719	343.16	-0.0542	-187.47	1.0719	343.16	-0.0486	-187.47	1.0305	343.16	-0.0348
-171.29	1.0784	384.14	-0.0548	-171.29	1.0736	384.14	-0.0525	-106.57	1.0572	384.14	-0.0520	-106.57	1.0322	384.14	-0.0442
-155.11	1.0776	419.13	-0.0539	-155.11	1.0358	419.13	-0.0505	-25.67	1.0062	419.13	-0.0486	-155.11	1.0292	419.13	-0.0400
-130.84	1.0747	457.12	-0.0527	-130.84	1.0640	457.12	-0.0516	-10.27	1.0936	457.12	-0.0546	-130.84	1.0204	457.12	-0.0314
-106.57	1.0642	507.77	-0.0514	-106.57	1.0523	507.77	-0.0405	-2.05	1.0109	507.77	-0.0482	-106.57	1.0205	507.77	-0.0198
-90.39	1.0541	545.76	-0.0484	-90.39	1.0439	545.76	-0.0444	0.00	-0.4968	545.76	-0.0478	-90.39	0.9784	545.76	-0.0018
-74.21	1.0457	571.08	-0.0415	-74.21	1.0326	571.08	-0.0273	0.31	-1.5259	571.08	-0.0380	-74.21	0.9583	571.08	0.0243
-58.03	1.0323	583.74	-0.0360	-58.03	1.0172	583.74	-0.0205	0.63	-1.3879	583.74	-0.0239	-58.03	0.9289	583.74	0.0466
-41.85	1.0227	596.41	-0.0279	-41.85	1.0059	596.41	0.0003	1.25	-1.4377	596.41	-0.0082	-41.85	0.9087	596.41	0.0761
-33.76	1.0263	609.07	-0.0026	-33.76	1.0043	609.07	0.0280	1.88	-1.3229	609.07	0.0395	-33.76	0.8952	609.07	0.1310
-25.67	1.0343			-25.67	1.0066			2.50	-1.3135			-25.67	0.8981		
-23.11	1.0424			-23.11	1.0123			3.13	-1.4956			-23.11	0.8990		
-17.97	1.0608			-17.97	1.0311			3.75	-1.4286			-17.97	0.9264		
-10.27	1.0779			-10.27	1.0945			4.37	-1.4656			-10.27	1.0205		
-5.13	1.0750			-5.13	1.1245			5.00	-1.3300			-5.13	1.1203		
-3.34	1.0993			-3.34	1.0979			6.25	-1.3052			-3.34	1.1302		
-2.05	0.9443			-2.05	1.0141			7.50	-1.2810			-2.05	1.0886		
-0.90	0.6800			-0.90	0.7887			8.75	-1.1511			-0.90	0.9195		
-0.44	0.4284			-0.44	0.5307			10.00	-1.2169			-0.44	0.7231		
0.00	-0.6890			0.00	-0.6095			12.50	-1.2819			0.00	-0.3353		
0.31	-1.7333			0.31	-1.5482			15.00	-1.3282			0.31	-1.6581		
0.63	-1.9107			0.63	-1.5503			17.50	-1.3036			0.63	-2.0216		
1.25	-1.8930			1.25	-1.2856			20.00	-1.2701			1.25	-2.1799		
1.88	-1.6827			30.00	-1.0934			30.00	-1.0754			1.88	-2.2014		
2.50	-1.7699			50.00	-0.6791			50.00	-0.6357			1.88	-2.2014		
3.13	-1.7324			60.00	-0.6090			60.00	-0.5292			2.50	-2.1486		
3.75	-1.6418			70.00	-0.4741			70.00	-0.4438			3.13	-2.1377		
4.37	-1.7665			80.00	-0.4221			80.00	-0.3559			3.75	-2.0469		
5.00	-1.6646			90.00	-0.3528			90.00	-0.3362			4.37	-2.0676		
6.25	-1.6515			100.00	-0.3127			100.00	-0.2540			5.00	-1.9950		
7.50	-1.5896			100.00	-0.2311			100.00	-0.2540			6.25	-1.9924		
8.75	-0.9136			241.85	-0.1201			110.00	-0.2211			7.50	-1.9927		
10.00	-1.1011							12.50	-1.4122			8.75	-1.8827		
12.50	-0.9225							15.00	-1.3642			10.00	-1.7978		
15.00	-1.1896							17.50	-1.2849			12.50	-1.3761		
17.50	-1.0434							20.00	-1.2471			15.00	-0.8866		
20.00	-1.1333							30.00	-1.0318			17.50	-0.7383		
30.00	-1.0674							40.00	-0.7920			20.00	-0.5318		
40.00	-0.9960							50.00	-0.6040			30.00	-0.4917		
50.00	-0.8272							60.00	-0.4707			40.00	-0.4725		
60.00	-0.7500							70.00	-0.4147			50.00	-0.4525		
70.00	-0.5967							80.00	-0.3549			60.00	-0.4209		
80.00	-0.5307							90.00	-0.3143			70.00	-0.4050		
90.00	-0.3806							100.00	-0.2701			80.00	-0.3614		
100.00	-0.3324							110.00	-0.2279			90.00	-0.3324		
110.00	-0.2594							241.85	-0.0862			100.00	-0.2563		
241.85	-0.1235							279.84	-0.0724			110.00	-0.2119		
279.84	-0.1116											241.85	-0.0649		
												279.84	-0.0579		

TABLE VI. Continued

(c) Continued

mfr = 0.49 and $\alpha = 0^\circ$				mfr = 0.49 and $\alpha = 2.0^\circ$				mfr = 0.55 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.9756	343.16	-0.0334	-187.47	0.9788	343.16	-0.0276	-187.47	0.9458	343.16	-0.0251
-171.29	0.9769	384.14	-0.0282	-171.29	0.9809	384.14	-0.0287	-171.29	0.9453	384.14	-0.0191
-155.11	0.9760	419.13	-0.0214	-155.11	0.9788	419.13	-0.0225	-155.11	0.9428	419.13	-0.0131
-130.84	0.9555	457.12	-0.0107	-130.84	0.9596	457.12	-0.0154	-130.84	0.9177	457.12	-0.0067
-106.57	0.9261	507.77	0.0133	-106.57	0.9358	507.77	0.0069	-106.57	0.8800	507.77	0.0279
-90.39	0.8937	545.76	0.0399	-90.39	0.8982	545.76	0.0449	-90.39	0.8385	545.76	0.0817
-74.21	0.8572	571.08	0.0836	-74.21	0.8656	571.08	0.0870	-74.21	0.7946	571.08	0.1104
-58.03	0.8122	583.74	0.1153	-58.03	0.8226	583.74	0.1147	-58.03	0.7346	583.74	0.1458
-41.85	0.7621	596.41	0.1595	-41.85	0.7783	596.41	0.1548	-41.85	0.6772	596.41	0.1911
-33.76	0.7139	609.07	0.2268	-33.76	0.7263	609.07	0.2042	-33.76	0.6476	609.07	0.2629
-25.67	0.7289			-25.67	0.7674			-25.67	0.6084		
-23.11	0.7336			-23.11	0.7745			-23.11	0.6141		
-17.97	0.7643			-17.97	0.8045			-17.97	0.6419		
-10.27	0.8996			-10.27	0.9359			-10.27	0.7833		
-5.13	1.0436			-5.13	1.0772			-5.13	0.9873		
-3.34	1.1081			-3.34	1.1206			-3.34	1.0813		
-2.05	1.1720			-2.05	1.1732			-2.05	1.1273		
-0.90	1.0476			-0.90	0.9844			-0.90	0.8977		
-0.44	0.8928			-0.44	0.8058			-0.44	0.6794		
0.00	-0.0394			0.00	-0.1901			0.00	0.1716		
0.31	-1.2915			0.31	-1.5199			0.31	-1.0854		
0.63	-1.7452			0.63	-1.8882			0.63	-1.5284		
1.25	-1.9783			1.25	-2.0780			1.25	-1.8345		
1.88	-1.9593			1.88	-2.1003			1.88	-1.7831		
2.50	-1.8385			2.50	-2.0902			2.50	-1.6358		
3.13	-1.8064			3.13	-2.0826			3.13	-1.6240		
3.75	-1.7929			3.75	-2.0134			3.75	-1.6017		
4.37	-1.7342			4.37	-1.9802			4.37	-1.4055		
5.00	-1.6932			5.00	-1.9331			5.00	-1.0942		
6.25	-1.6958			6.25	-1.8890			6.25	-0.8870		
7.50	-1.2448			7.50	-1.8252			7.50	-0.6709		
8.75	-0.7720			8.75	-1.7647			8.75	-0.7244		
10.00	-0.8344			10.00	-1.7341			10.00	-0.7004		
12.50	-0.6559			12.50	-1.6164			12.50	-0.7063		
15.00	-0.6628			15.00	-0.8551			15.00	-0.6699		
17.50	-0.6267			17.50	-0.6126			17.50	-0.6133		
20.00	-0.5826			20.00	-0.5642			20.00	-0.5549		
30.00	-0.4929			30.00	-0.4979			30.00	-0.4764		
40.00	-0.4529			40.00	-0.4859			40.00	-0.4369		
50.00	-0.4212			50.00	-0.4509			50.00	-0.4193		
60.00	-0.4062			60.00	-0.4303			60.00	-0.3894		
70.00	-0.3847			70.00	-0.4101			70.00	-0.3868		
80.00	-0.3616			80.00	-0.3706			80.00	-0.3439		
90.00	-0.3141			90.00	-0.3288			90.00	-0.3108		
100.00	-0.2465			100.00	-0.2561			100.00	-0.2381		
110.00	-0.1969			110.00	-0.2081			110.00	-0.1952		
241.85	-0.0580			241.85	-0.0592			241.85	-0.0501		
279.84	-0.0460			279.84	-0.0479			279.84	-0.0383		

TABLE VI. Continued

(c) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.8928	343.16	-0.0155	-187.47	0.8910	343.16	-0.0066	-187.47	0.8283	343.16	0.0077	-187.47	0.7631	343.16	-0.0076
-171.29	0.8949	384.14	-0.0083	-171.29	0.8813	384.14	-0.0061	-171.29	0.7699	384.14	0.0149	-171.29	0.7699	384.14	-0.0029
-155.11	0.8886	419.13	0.0011	-155.11	0.8250	419.13	0.0041	-155.11	0.7033	419.13	0.0082	-155.11	0.7566	419.13	0.0094
-130.84	0.8639	457.12	0.0132	-130.84	0.7876	457.12	0.0198	-130.84	0.7117	457.12	0.0177	-130.84	0.7117	457.12	0.0195
-106.57	0.8086	507.77	0.0482	-106.57	0.7216	507.77	0.0447	-106.57	0.6235	457.12	0.0177	-106.57	0.6281	507.77	0.0578
-90.39	0.7544	545.76	0.0845	-90.39	0.6511	545.76	0.0794	-90.39	0.5249	545.76	0.0964	-90.39	0.5350	545.76	0.1040
-74.21	0.6961	571.08	0.1384	-74.21	0.5759	571.08	0.1290	-74.21	0.4389	571.08	0.1542	-74.21	0.4389	571.08	0.1621
-58.03	0.6318	583.74	0.1743	-58.03	0.4703	583.74	0.1885	-58.03	0.3296	583.74	0.1936	-58.03	0.2868	583.74	0.1948
-41.85	0.5318	596.41	0.2222	-41.85	0.3511	596.41	0.2381	-41.85	0.2193	596.41	0.2484	-41.85	0.1193	596.41	0.2456
-33.76	0.4829	609.07	0.2928	-33.76	0.2850	609.07	0.3088	-33.76	0.1796	609.07	0.3126	-33.76	0.0179	609.07	0.3126
-25.67	0.4286			-25.67	0.1995			-25.67	-0.0576			-25.67	-0.0780		
-23.11	0.4418			-23.11	0.1735			-23.11	-0.1346			-23.11	-0.1346		
-17.97	0.4706			-17.97	0.1602			-17.97	-0.1079			-17.97	-0.1079		
-10.27	0.6391			-10.27	0.7187			-10.27	0.4254			-10.27	0.1213		
-5.13	0.8641			-5.13	0.7011			-5.13	0.6993			-5.13	0.5266		
-3.34	0.9973			-3.34	0.6229			-3.34	0.8465			-3.34	0.7226		
-2.05	1.0919			-2.05	0.6589			-2.05	1.0056			-2.05	0.9293		
-0.90	1.1171			-0.90	0.6595			-0.90	1.0277			-0.90	0.9293		
-0.44	1.0508			-0.44	0.6433			-0.44	1.0854			-0.44	1.0865		
0.00	0.3708			0.00	0.6466			0.00	1.0854			0.00	1.1253		
0.31	-0.7201			0.31	-0.6215			0.31	-0.4119			0.31	-0.3961		
0.63	-1.3247			0.63	-0.5495			0.63	-0.8880			0.63	-0.4317		
1.25	-1.2681			1.25	-0.5202			1.25	-1.0945			1.25	-0.4018		
1.88	-1.2533			1.88	-0.4293			1.88	-0.8142			1.88	-0.3283		
2.50	-1.1851			2.50	-0.3859			2.50	-0.6378			2.50	-0.3456		
3.13	-1.2040			3.13	-0.3831			3.13	-0.6188			3.13	-0.3381		
3.75	-0.8197			3.75	-0.3642			3.75	-0.5922			3.75	-0.3180		
4.37	-0.7041			4.37	-0.3397			4.37	-0.5648			4.37	-0.3180		
5.00	-0.7088			5.00	-0.3015			5.00	-0.5504			5.00	-0.3026		
6.25	-0.6603			6.25	-0.2335			6.25	-0.5019			6.25	-0.3026		
7.50	-0.6325			7.50	-0.1797			7.50	-0.4745			7.50	-0.3026		
8.75	-0.6759			8.75	-0.1429			8.75	-0.4474			8.75	-0.3026		
10.00	-0.6599			10.00	-0.1100			10.00	-0.4200			10.00	-0.3026		
12.50	-0.6333			12.50	-0.0833			12.50	-0.3933			12.50	-0.3026		
15.00	-0.6130			15.00	-0.0630			15.00	-0.3666			15.00	-0.3026		
17.50	-0.5503			17.50	-0.5321			17.50	-0.3400			17.50	-0.3026		
20.00	-0.5221			20.00	-0.4478			20.00	-0.3133			20.00	-0.3026		
30.00	-0.4454			30.00	-0.3938			30.00	-0.2866			30.00	-0.3026		
40.00	-0.4178			40.00	-0.3794			40.00	-0.2720			40.00	-0.3026		
50.00	-0.3959			50.00	-0.3552			50.00	-0.2576			50.00	-0.3026		
60.00	-0.3708			60.00	-0.3385			60.00	-0.2432			60.00	-0.3026		
70.00	-0.3529			70.00	-0.3218			70.00	-0.2288			70.00	-0.3026		
80.00	-0.3381			80.00	-0.3071			80.00	-0.2144			80.00	-0.3026		
90.00	-0.3029			90.00	-0.2827			90.00	-0.2000			90.00	-0.3026		
100.00	-0.2287			100.00	-0.1683			100.00	-0.1856			100.00	-0.3026		
110.00	-0.1683			110.00	-0.1683			110.00	-0.1683			110.00	-0.3026		
241.85	-0.0525			241.85	-0.0525			241.85	-0.0525			241.85	-0.0525		
279.84	-0.0416			279.84	-0.0513			279.84	-0.0513			279.84	-0.0513		

TABLE VI. Continued

(c) Concluded

$m\bar{r} = 0.81$ and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 180^\circ$		
Forebody		Afterbody	Forebody		Afterbody
X/L	CP	X/L CP	X/L	CP	X/L CP
-187.47	0.6797	343.16 -0.0017	-187.47	0.6772	343.16 0.0064
-171.29	0.6830	384.14 0.0073	-106.57	0.4996	384.14 0.0081
-155.11	0.6709	419.13 0.0188	-25.67	-0.5596	419.13 0.0222
-130.84	0.6083	457.12 0.0376	-10.27	-0.1951	457.12 0.0338
-106.57	0.5060	507.77 0.0774	-2.05	0.7182	507.77 0.0719
-90.39	0.3893	545.76 0.1194	0.00	0.9743	545.76 0.1155
-74.21	0.2564	571.08 0.1716	0.31	0.3423	571.08 0.1712
-58.03	0.0617	583.74 0.2054	0.63	0.0673	583.74 0.2114
-41.85	-0.1947	596.41 0.2533	1.25	-0.1328	596.41 0.2623
-33.76	-0.3326	609.07 0.3188	1.88	-0.1517	609.07 0.3295
-25.67	-0.5620		2.50	-0.1635	
-23.11	-0.6336		3.13	-0.1433	
-17.97	-0.5264		3.75	-0.1791	
-10.27	-0.1932		4.37	-0.1878	
-5.13	0.2284		5.00	-0.1819	
-3.34	0.3123		6.25	-0.1631	
-2.05	0.7399		7.50	-0.2438	
-0.90	1.0030		8.75	-0.2602	
-0.44	1.1100		10.00	-0.2882	
0.00	0.9651		12.50	-0.3392	
0.31	0.2475		15.00	-0.3236	
0.63	-0.0839		17.50	-0.3321	
1.25	-0.1959		20.00	-0.3023	
1.88	-0.1296		30.00	-0.3014	
2.50	-0.1921		50.00	-0.3156	
3.13	-0.1846		60.00	-0.3127	
3.75	-0.1653		70.00	-0.2981	
4.37	-0.1842		80.00	-0.2929	
5.00	-0.2173		90.00	-0.2565	
6.25	-0.2375		100.00	-0.1947	
7.50	-0.2031		110.00	-0.1460	
8.75	-0.2660		241.85	-0.0342	
10.00	-0.2840				
12.50	-0.3029				
15.00	-0.3415				
17.50	-0.3008				
20.00	-0.2919				
30.00	-0.3033				
40.00	-0.3083				
50.00	-0.3121				
60.00	-0.3083				
70.00	-0.3042				
80.00	-0.2884				
90.00	-0.2593				
100.00	-0.1968				
110.00	-0.1439				
241.85	-0.0342				
279.84	-0.0263				

TABLE VI. Continued

(d) $M = 0.72$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0829	343.16	-0.0585	-187.47	1.0448	343.16	-0.0436	-187.47	0.9876	343.16	-0.0366	-187.47	0.9876	343.16	-0.0231
-171.29	1.0838	384.14	-0.0528	-171.29	1.0456	384.14	-0.0391	-106.57	0.9888	384.14	-0.0395	-106.57	0.9888	384.14	-0.0252
-155.11	1.0826	419.13	-0.0524	-155.11	1.0440	419.13	-0.0350	-25.67	0.9668	419.13	-0.0342	-25.67	0.9668	419.13	-0.0154
-130.84	1.0770	457.12	-0.0491	-130.84	1.0333	457.12	-0.0257	-10.27	0.9606	457.12	-0.0322	-10.27	0.9606	457.12	-0.0125
-106.57	1.0634	507.77	-0.0422	-106.57	1.0113	507.77	-0.0106	-2.05	0.9596	507.77	0.0000	-2.05	0.9596	507.77	0.0156
-90.39	1.0330	545.76	-0.0410	-90.39	0.9918	545.76	0.0122	0.00	-0.1767	545.76	0.0000	0.00	-0.1767	545.76	0.0450
-74.21	1.0399	571.08	-0.0300	-74.21	0.9703	571.08	0.0435	0.31	-1.4358	571.08	0.0297	0.31	-1.4358	571.08	0.0903
-58.03	1.0279	583.74	-0.0223	-58.03	0.9443	583.74	0.0638	0.63	-1.8707	583.74	0.0586	0.63	-1.8707	583.74	0.1283
-41.85	1.0187	596.41	-0.0060	-41.85	0.9220	596.41	0.1018	1.88	-2.0277	596.41	0.0953	1.88	-2.0277	596.41	0.1736
-33.76	1.0164	609.07	0.0282	-33.76	0.9097	609.07	0.1571	2.50	-2.0522	609.07	0.1555	2.50	-2.0522	609.07	0.2479
-25.67	1.0182			-25.67	0.9035			3.13	-2.0112			3.13	-2.0112		
-23.11	1.0236			-23.11	0.9075			3.75	-1.9450			3.75	-1.9450		
-17.97	1.0469			-17.97	0.9417			4.37	-1.9243			4.37	-1.9243		
-10.27	1.062			-10.27	1.0306			5.00	-1.9203			5.00	-1.9203		
-5.13	1.1339			-5.13	1.1234			6.25	-1.8594			6.25	-1.8594		
-3.34	1.1075			-3.34	1.1361			7.50	-1.8233			7.50	-1.8233		
-2.05	1.0275			-2.05	1.1069			8.75	-1.7786			8.75	-1.7786		
-0.90	0.8013			-0.90	0.9504			10.00	-1.7305			10.00	-1.7305		
-0.44	0.5638			-0.44	0.7436			12.50	-1.5975			12.50	-1.5975		
0.00	-0.5426			0.00	-0.2456			15.00	-1.5908			15.00	-1.5908		
0.31	-1.4994			0.31	-1.5143			17.50	-1.4712			17.50	-1.4712		
0.63	-1.3671			0.63	-1.8472			20.00	-1.3374			20.00	-1.3374		
1.25	-1.4393			1.25	-2.0233			30.00	-0.8544			30.00	-0.8544		
1.88	-1.4461			1.88	-2.0382			40.00	-0.4101			40.00	-0.4101		
2.50	-1.3250			2.50	-2.0253			50.00	-0.4375			50.00	-0.4375		
3.13	-1.4012			3.13	-1.9904			60.00	-0.4281			60.00	-0.4281		
3.75	-1.4597			3.75	-1.9720			70.00	-0.4051			70.00	-0.4051		
4.37	-1.4389			4.37	-1.8974			80.00	-0.3776			80.00	-0.3776		
5.00	-1.3968			5.00	-1.9046			90.00	-0.3363			90.00	-0.3363		
6.25	-1.3659			6.25	-1.8633			100.00	-0.2678			100.00	-0.2678		
7.50	-1.3960			7.50	-1.7851			110.00	-0.2314			110.00	-0.2314		
8.75	-1.4465			8.75	-1.7530			120.00	-0.1998			120.00	-0.1998		
10.00	-1.4200			10.00	-1.7329			130.00	-0.1698			130.00	-0.1698		
12.50	-1.3001			12.50	-1.5806			140.00	-0.1440			140.00	-0.1440		
15.00	-1.3531			15.00	-1.5675			150.00	-0.1185			150.00	-0.1185		
17.50	-1.2785			17.50	-1.5198			160.00	-0.0965			160.00	-0.0965		
20.00	-1.2478			20.00	-1.4865			170.00	-0.0865			170.00	-0.0865		
30.00	-1.0667			30.00	-0.6865			200.00	-0.4066			200.00	-0.4066		
40.00	-0.8906			40.00	-0.4440			300.00	-0.4440			300.00	-0.4440		
50.00	-0.6681			50.00	-0.4435			400.00	-0.4435			400.00	-0.4435		
60.00	-0.5498			60.00	-0.4323			500.00	-0.4323			500.00	-0.4323		
70.00	-0.4472			70.00	-0.4105			600.00	-0.4105			600.00	-0.4105		
80.00	-0.3975			80.00	-0.3782			700.00	-0.3782			700.00	-0.3782		
90.00	-0.3282			90.00	-0.3377			800.00	-0.3377			800.00	-0.3377		
100.00	-0.2733			100.00	-0.2699			900.00	-0.2699			900.00	-0.2699		
110.00	-0.2289			110.00	-0.2125			1000.00	-0.2125			1000.00	-0.2125		
241.85	-0.0773			241.85	-0.0696			279.84	-0.0696			279.84	-0.0696		
279.84	-0.0688			279.84	-0.0602										

TABLE VI. Continued

(d) Concluded

mfr = 0.54 and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 180^\circ$		
Forebody		Afterbody	Forebody		Afterbody
X/L	CP	X/L CP	X/L	CP	X/L CP
-187.47	0.9620	343.16 -0.0231	-187.47	0.9565	343.16 -0.0190
-171.29	0.9660	384.14 -0.0190	-106.57	0.8963	384.14 -0.0190
-155.11	0.9580	419.13 -0.0101	-25.67	0.6472	419.13 -0.0060
-130.84	0.9341	457.12 0.0066	-10.27	0.8195	457.12 -0.0007
-106.57	0.8974	507.77 0.0334	-2.05	1.1320	507.77 0.0253
-90.39	0.8571	545.76 0.0700	0.00	0.2203	545.76 0.0615
-74.21	0.8140	571.08 0.1189	0.31	-0.8566	571.08 0.1152
-58.03	0.7594	583.74 0.1575	0.63	-1.4653	583.74 0.1575
-41.85	0.7000	596.41 0.2042	1.25	-1.6983	596.41 0.2083
-33.76	0.6674	609.07 0.2746	1.88	-1.7214	609.07 0.2831
-25.67	0.6342		2.30	-1.5867	
-23.11	0.6405		3.13	-1.6325	
-17.97	0.6710		3.75	-1.5407	
-10.27	0.8106		4.37	-1.5287	
-5.13	0.9858		5.00	-1.4826	
-3.34	1.0905		6.25	-1.4634	
-2.05	1.1305		7.50	-1.2997	
-0.90	1.0975		8.75	-0.7859	
-0.44	0.9699		10.00	-0.8859	
0.00	0.1897		12.50	-0.6691	
0.31	-0.9894		15.00	-0.6151	
0.63	-1.4507		17.50	-0.6079	
1.25	-1.7270		20.00	-0.5777	
1.88	-1.7262		30.00	-0.4845	
2.50	-1.5934		50.00	-0.4368	
3.13	-1.5778		60.00	-0.4071	
3.75	-1.5008		70.00	-0.3904	
4.37	-1.4632		80.00	-0.3593	
5.00	-1.3722		90.00	-0.3176	
6.25	-1.4271		100.00	-0.2436	
7.50	-1.2896		110.00	-0.1893	
8.75	-0.6690		241.85	-0.0444	
10.00	-0.6848				
12.50	-0.6181				
15.00	-0.6548				
17.50	-0.6053				
20.00	-0.5576				
30.00	-0.4811				
40.00	-0.4472				
50.00	-0.4166				
60.00	-0.4049				
70.00	-0.3954				
80.00	-0.3641				
90.00	-0.3134				
100.00	-0.2455				
110.00	-0.1938				
241.85	-0.0548				
279.84	-0.0421				

TABLE VI. Continued

(e) $M = 0.74$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP
-187.47	1.1018	343.16	-0.0507	-187.47	1.0915	343.16	-0.0560	-187.47	1.0913	343.16	-0.0397	-187.47	1.0551	343.16	-0.0415
-171.29	1.1018	384.14	-0.0507	-171.29	1.0931	384.14	-0.0525	-171.29	1.0931	384.14	-0.0490	-171.29	1.0562	384.14	-0.0384
-155.11	1.1026	419.13	-0.0499	-155.11	1.0927	419.13	-0.0501	-155.11	1.0927	419.13	-0.0470	-155.11	1.0532	419.13	-0.0310
-130.84	1.0965	457.12	-0.0429	-130.84	1.0866	457.12	-0.0474	-130.84	1.0866	457.12	-0.0521	-130.84	1.0433	457.12	-0.0201
-106.57	1.0862	507.77	-0.0444	-106.57	1.0740	507.77	-0.0408	-106.57	1.0740	507.77	-0.0404	-106.57	1.0234	507.77	-0.0017
-90.39	1.0786	545.76	-0.0518	-90.39	1.0649	545.76	-0.0334	-90.39	1.0649	545.76	-0.0366	-90.39	1.0020	545.76	0.0181
-74.21	1.0690	571.08	-0.0464	-74.21	1.0508	571.08	-0.0166	-74.21	1.0508	571.08	-0.0226	-74.21	0.9817	571.08	0.0544
-58.03	1.0588	583.74	-0.0394	-58.03	1.0375	583.74	-0.0093	-58.03	1.0375	583.74	-0.0003	-58.03	0.9588	583.74	0.0809
-41.85	1.0542	596.41	-0.0285	-41.85	1.0272	596.41	0.0021	-41.85	1.0272	596.41	0.0179	-41.85	0.9376	596.41	0.1176
-33.76	1.0542	609.07	0.0089	-33.76	1.0272	609.07	0.0536	-33.76	1.0272	609.07	0.0630	-33.76	0.9197	609.07	0.1714
-25.67	1.0598			-25.67	1.0275			-25.67	1.0272			-25.67	0.9184		
-23.11	1.0645			-23.11	1.0303			-23.11	1.0210			-23.11	0.9223		
-17.97	1.0842			-17.97	1.0538			-17.97	1.0538			-17.97	0.9545		
-10.27	1.1297			-10.27	1.1162			-10.27	1.1162			-10.27	1.0389		
-5.13	1.1258			-5.13	1.1412			-5.13	1.1412			-5.13	1.1325		
-3.34	1.0830			-3.34	1.1160			-3.34	1.1160			-3.34	1.1460		
-2.05	0.9908			-2.05	1.0414			-2.05	1.0414			-2.05	1.1325		
-0.90	0.7609			-0.90	0.8454			-0.90	0.8454			-0.90	1.1135		
-0.44	0.5169			-0.44	0.5885			-0.44	0.5885			-0.44	0.9650		
0.00	-0.5419			0.00	-0.4899			0.00	-0.4899			0.00	-0.7614		
0.31	-1.3520			0.31	-1.6261			0.31	-1.6261			0.31	-1.4169		
0.63	-1.3141			0.63	-1.8986			0.63	-1.8986			0.63	-1.7378		
1.25	-1.4570			1.25	-2.0380			1.25	-2.0380			1.25	-1.6509		
1.88	-1.4669			1.88	-2.0587			1.88	-2.0587			1.88	-1.6117		
2.50	-1.5539			2.50	-2.0514			2.50	-2.0514			2.50	-1.5768		
3.13	-1.5477			3.13	-2.0199			3.13	-2.0199			3.13	-1.5026		
3.75	-1.4355			3.75	-2.0346			3.75	-2.0346			3.75	-1.4803		
4.37	-1.4631			4.37	-1.9725			4.37	-1.9725			4.37	-1.4507		
5.00	-1.5037			5.00	-1.9694			5.00	-1.9694			5.00	-1.4240		
6.25	-1.3949			6.25	-1.9189			6.25	-1.9189			6.25	-1.4089		
7.50	-1.3831			7.50	-1.8829			7.50	-1.8829			7.50	-1.3850		
8.75	-1.3007			8.75	-1.8818			8.75	-1.8818			8.75	-1.3665		
10.00	-1.3451			10.00	-1.8125			10.00	-1.8125			10.00	-1.3462		
12.50	-1.2919			12.50	-1.7708			12.50	-1.7708			12.50	-1.3253		
15.00	-1.2361			15.00	-1.7021			15.00	-1.7021			15.00	-1.3035		
17.50	-1.1088			17.50	-1.6651			17.50	-1.6651			17.50	-1.2842		
20.00	-1.1185			20.00	-1.5948			20.00	-1.5948			20.00	-1.2642		
30.00	-1.0141			30.00	-0.9133			30.00	-0.9133			30.00	-1.2420		
40.00	-0.9766			40.00	-0.5952			40.00	-0.5952			40.00	-1.2240		
50.00	-0.8621			50.00	-0.3307			50.00	-0.3307			50.00	-1.2089		
60.00	-0.7746			60.00	-0.3426			60.00	-0.3426			60.00	-1.1926		
70.00	-0.6023			70.00	-0.3519			70.00	-0.3519			70.00	-1.1768		
80.00	-0.5906			80.00	-0.3529			80.00	-0.3529			80.00	-1.1617		
90.00	-0.4718			90.00	-0.3211			90.00	-0.3211			90.00	-1.1463		
100.00	-0.3971			100.00	-0.2641			100.00	-0.2641			100.00	-1.1314		
110.00	-0.2731			110.00	-0.2151			110.00	-0.2151			110.00	-1.1169		
241.85	-0.0829			241.85	-0.0806			241.85	-0.0806			241.85	-0.0647		
279.84	-0.0802			279.84	-0.0734			279.84	-0.0734			279.84	-0.0516		

TABLE VI. Continued

(c) Continued

mfr = 0.49 and $\alpha = 0^\circ$				mfr = 0.54 and $\alpha = 0^\circ$				mfr = 0.61 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L
-187.47	1.0034	343.16	-0.0252	-187.47	0.9756	343.16	-0.0224	-187.47	0.9220	343.16	-0.0105
-171.29	1.0034	384.14	-0.0182	-171.29	0.9711	384.14	-0.0138	-171.29	0.9239	384.14	-0.0024
-155.11	1.0026	419.13	-0.0096	-155.11	0.9687	419.13	-0.0045	-155.11	0.9182	419.13	0.0078
-130.84	0.9831	457.12	0.0048	-130.84	0.9496	457.12	0.0103	-130.84	0.8903	457.12	0.0195
-106.57	0.9525	507.77	0.0325	-106.57	0.9103	507.77	0.0400	-106.57	0.8397	507.77	0.0588
-90.39	0.9197	545.76	0.0664	-90.39	0.8740	545.76	0.0786	-90.39	0.7874	545.76	0.1017
-74.21	0.8852	571.08	0.1160	-74.21	0.8307	571.08	0.1312	-74.21	0.7290	571.08	0.1583
-58.03	0.8421	583.74	0.1518	-58.03	0.7760	583.74	0.1729	-58.03	0.6488	583.74	0.2000
-41.85	0.7984	596.41	0.1979	-41.85	0.7226	596.41	0.2200	-41.85	0.5624	596.41	0.2506
-33.76	0.7788	609.07	0.2653	-33.76	0.6984	609.07	0.2941	-33.76	0.5279	609.07	0.3223
-25.67	0.7552			-25.67	0.6675			-25.67	0.4703		
-23.11	0.7659			-23.11	0.6606			-23.11	0.4655		
-17.97	0.7962			-17.97	0.6993			-17.97	0.5098		
-10.27	0.9243			-10.27	0.8417			-10.27	0.6609		
-5.13	1.0608			-5.13	1.0245			-5.13	0.9016		
-3.34	1.1249			-3.34	1.0990			-3.34	1.0225		
-2.05	1.1407			-2.05	1.1464			-2.05	1.1169		
-0.90	1.0608			-0.90	1.1071			-0.90	1.1399		
-0.44	0.9064			-0.44	0.9776			-0.44	1.0835		
0.00	0.0569			0.00	0.2036			0.00	0.4462		
0.31	-1.1253			0.31	-0.9086			0.31	-0.6065		
0.63	-1.5230			0.63	-1.3655			0.63	-1.1479		
1.25	-1.7101			1.25	-1.6275			1.25	-1.3860		
1.88	-1.7048			1.88	-1.6141			1.88	-1.3334		
2.50	-1.7052			2.50	-1.5945			2.50	-1.2500		
3.13	-1.6852			3.13	-1.5207			3.13	-1.1951		
3.75	-1.6417			3.75	-1.4987			3.75	-1.1375		
4.37	-1.5845			4.37	-1.4599			4.37	-1.0694		
5.00	-1.5899			5.00	-1.4246			5.00	-0.9838		
6.25	-1.5165			6.25	-1.3420			6.25	-0.6200		
7.50	-1.4673			7.50	-1.3048			7.50	-0.5490		
8.75	-1.3885			8.75	-1.2979			8.75	-0.7014		
10.00	-1.3628			10.00	-1.1519			10.00	-0.6546		
12.50	-1.2667			12.50	-0.6155			12.50	-0.6930		
15.00	-1.2998			15.00	-0.5419			15.00	-0.6522		
17.50	-0.9111			17.50	-0.5494			17.50	-0.5896		
20.00	-0.4994			20.00	-0.5365			20.00	-0.5329		
30.00	-0.4681			30.00	-0.4864			30.00	-0.4637		
40.00	-0.4665			40.00	-0.4541			40.00	-0.4316		
50.00	-0.4500			50.00	-0.4268			50.00	-0.4075		
60.00	-0.4368			60.00	-0.4140			60.00	-0.3983		
70.00	-0.4087			70.00	-0.3984			70.00	-0.3807		
80.00	-0.3886			80.00	-0.3641			80.00	-0.3537		
90.00	-0.3374			90.00	-0.3216			90.00	-0.3069		
100.00	-0.2642			100.00	-0.2469			100.00	-0.2384		
110.00	-0.1961			110.00	-0.1892			110.00	-0.1750		
241.85	-0.0620			241.85	-0.0488			241.85	-0.0447		
279.84	-0.0521			279.84	-0.0416			279.84	-0.0339		

TABLE VI. Continued

(e) Concluded

		mfr = 0.88 and $\alpha = 0^\circ$				mfr = 0.74 and $\alpha = 0^\circ$				mfr = 0.60 and $\alpha = 0^\circ$					
		$\psi = 0^\circ$		$\psi = 180^\circ$		$\psi = 0^\circ$		$\psi = 180^\circ$		$\psi = 0^\circ$		$\psi = 180^\circ$			
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody		
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP		
-187.47	0.8622	343.16	-0.0086	-187.47	0.8532	343.16	0.0007	-187.47	0.7988	343.16	0.0034	-187.47	0.7222	343.16	0.0005
-171.29	0.8614	384.14	0.0027	-106.57	0.7471	384.14	0.0027	-106.57	0.6633	384.14	0.0070	-106.57	0.5516	384.14	0.0107
-155.11	0.8534	419.13	0.0159	-25.67	0.2259	419.13	0.0190	-155.11	0.7919	419.13	0.0183	-155.11	0.7091	419.13	0.0286
-130.84	0.8171	457.12	0.0346	-102.7	0.4627	457.12	0.0311	-130.84	0.7461	457.12	0.0358	-102.7	0.6243	457.12	0.0399
-106.57	0.7530	507.77	0.0673	-2.05	1.0444	507.77	0.0696	-106.57	0.6654	507.77	0.0767	-106.57	0.5522	507.77	0.0835
-90.39	0.6797	545.76	0.1163	0.00	0.6901	545.76	0.1175	-90.39	0.5791	545.76	0.1239	-90.39	0.4403	545.76	0.1291
-74.21	0.6068	571.08	0.1720	0.31	-0.2295	571.08	0.1782	-74.21	0.4767	571.08	0.1824	-74.21	0.3112	571.08	0.1902
-58.03	0.4918	583.74	0.2148	0.63	-0.7204	583.74	0.2238	-58.03	0.3333	583.74	0.2237	-58.03	0.1240	583.74	0.2280
-41.85	0.3763	596.41	0.2662	1.25	-0.8778	596.41	0.2771	-41.85	0.1754	596.41	0.2837	-41.85	-0.1211	596.41	0.2771
-33.76	0.3101	609.07	0.3371	1.88	-0.8778	609.07	0.3476	-33.76	0.0855	609.07	0.3434	-33.76	-0.2828	609.07	0.3441
-25.67	0.2216			2.50	-0.7553			-25.67	-0.0388			-25.67	-0.3775		
-23.11	0.2066			3.13	-0.7213			-23.11	-0.0741			-23.11	-0.3822		
-17.97	0.2439			3.75	-0.5845			-17.97	-0.0057			-17.97	-0.3132		
-10.27	0.4683			4.37	-0.3666			-10.27	0.2357			-10.27	-0.1023		
-5.13	0.7225			5.00	-0.3357			-5.13	0.5547			-5.13	0.3391		
-3.34	0.9010			6.25	-0.3050			-3.34	0.7710			-3.34	0.5989		
-2.05	1.0407			7.50	-0.5396			-2.05	0.9510			-2.05	0.7799		
-0.90	1.1367			8.75	-0.5729			-0.90	1.1126			-0.90	1.0528		
-0.44	1.1187			10.00	-0.5301			-0.44	1.1466			-0.44	1.1349		
0.00	0.6175			12.50	-0.5745			0.00	0.7763			0.00	0.9567		
0.31	-0.2836			15.00	-0.5517			0.31	-0.0707			0.31	0.2997		
0.63	-0.8016			17.50	-0.4957			0.63	-0.4675			0.63	-0.0276		
1.25	-0.8975			20.00	-0.4806			1.25	-0.4936			1.25	-0.1597		
1.88	-0.8166			30.00	-0.4686			1.88	-0.4467			1.88	-0.1570		
2.50	-0.6973			50.00	-0.3853			2.50	-0.4233			2.50	-0.1402		
3.13	-0.6504			60.00	-0.3935			3.13	-0.4141			3.13	-0.2307		
3.75	-0.6347			70.00	-0.3599			3.75	-0.3657			3.75	-0.1937		
4.37	-0.5640			80.00	-0.3405			4.37	-0.3887			4.37	-0.1700		
5.00	-0.5763			90.00	-0.3004			5.00	-0.4041			5.00	-0.2265		
6.25	-0.5475			100.00	-0.2299			6.25	-0.4053			6.25	-0.2865		
7.50	-0.4984			110.00	-0.1650			7.50	-0.3691			7.50	-0.2181		
8.75	-0.5398			1241.85	-0.0205			8.75	-0.4264			8.75	-0.3225		
10.00	-0.5617							10.00	-0.4114			10.00	-0.2957		
12.50	-0.5026							12.50	-0.4494			12.50	-0.3790		
15.00	-0.5308							15.00	-0.4615			15.00	-0.3504		
17.50	-0.4938							17.50	-0.4175			17.50	-0.3606		
20.00	-0.4856							20.00	-0.4016			20.00	-0.3468		
30.00	-0.4071							30.00	-0.3653			30.00	-0.3233		
40.00	-0.4092							40.00	-0.3809			40.00	-0.3374		
50.00	-0.3802							50.00	-0.3607			50.00	-0.3187		
60.00	-0.3871							60.00	-0.3665			60.00	-0.3333		
70.00	-0.3659							70.00	-0.3500			70.00	-0.3247		
80.00	-0.3476							80.00	-0.3232			80.00	-0.3072		
90.00	-0.3031							90.00	-0.2923			90.00	-0.2773		
100.00	-0.2332							100.00	-0.2181			100.00	-0.1985		
110.00	-0.1626							110.00	-0.1601			110.00	-0.1482		
241.85	-0.0493							241.85	-0.0376			241.85	-0.0303		
279.84	-0.0313							279.84	-0.0263			279.84	-0.0213		

TABLE VI. Continued

(f) $M = 0.77$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1135	343.16	-0.0566	-187.47	1.1030	343.16	-0.0524	-187.47	1.0676	343.16	-0.0394	-187.47	1.0658	343.16	-0.0323
-171.29	1.1135	384.14	-0.0540	-171.29	1.1034	384.14	-0.0498	-171.29	1.0657	384.14	-0.0502	-171.29	1.0658	384.14	-0.0334
-155.11	1.1161	419.13	-0.0525	-155.11	1.1041	419.13	-0.0446	-155.11	1.0658	419.13	-0.0442	-155.11	1.0658	419.13	-0.0249
-130.84	1.1135	457.12	-0.0491	-130.84	1.0986	457.12	-0.0397	-130.84	1.0545	457.12	-0.0461	-130.84	1.0545	457.12	-0.0193
-106.57	1.1037	507.77	-0.0432	-106.57	1.0887	507.77	-0.0341	-106.57	1.0373	507.77	0.0016	-106.57	1.0373	507.77	-0.0021
-90.39	1.0927	545.76	-0.0417	-90.39	1.0755	545.76	-0.0233	-90.39	1.0172	545.76	0.0303	-90.39	1.0172	545.76	0.0243
-74.21	1.0814	571.08	-0.0320	-74.21	1.0627	571.08	-0.0080	-74.21	0.9967	571.08	0.0688	-74.21	0.9967	571.08	0.0606
-58.03	1.0723	583.74	-0.0216	-58.03	1.0514	583.74	0.0107	-58.03	0.9761	583.74	0.0979	-58.03	0.9761	583.74	0.0919
-41.85	1.0716	596.41	-0.0037	-41.85	1.0415	596.41	0.0331	-41.85	0.9489	596.41	0.1344	-41.85	0.9489	596.41	0.1333
-33.76	1.0748	609.07	0.0365	-33.76	1.0392	609.07	0.0807	-33.76	0.9180	609.07	0.1940	-33.76	0.9180	609.07	0.1933
-25.67	1.0707			-25.67	1.0429			-25.67	0.9373			-25.67	0.9373		
-23.11	1.0859			-23.11	1.0466			-23.11	0.9410			-23.11	0.9410		
-17.97	1.1011			-17.97	1.0709			-17.97	0.9674			-17.97	0.9674		
-10.27	1.1422			-10.27	1.1274			-10.27	1.0579			-10.27	1.0579		
-5.13	1.1544			-5.13	1.1531			-5.13	1.1405			-5.13	1.1405		
-3.34	1.1221			-3.34	1.1268			-3.34	1.1539			-3.34	1.1539		
-2.05	1.0358			-2.05	1.0315			-2.05	1.0912			-2.05	1.0912		
-0.90	0.7732			-0.90	0.8400			-0.90	0.9761			-0.90	0.9761		
-0.44	0.5903			-0.44	0.6241			-0.44	0.7858			-0.44	0.7858		
0.00	-0.4629			0.00	-0.4042			0.00	-0.1518			0.00	-0.1518		
0.31	-1.5584			0.31	-1.5236			0.31	-1.3010			0.31	-1.3010		
0.63	-1.7713			0.63	-1.7773			0.63	-1.6049			0.63	-1.6049		
1.25	-1.9333			1.25	-1.9096			1.25	-1.7504			1.25	-1.7504		
1.88	-1.9549			1.88	-1.9339			1.88	-1.7772			1.88	-1.7772		
2.50	-1.9656			2.50	-1.9261			2.50	-1.7581			2.50	-1.7581		
3.13	-1.9817			3.13	-1.9232			3.13	-1.7544			3.13	-1.7544		
3.75	-1.9421			3.75	-1.8852			3.75	-1.7320			3.75	-1.7320		
4.37	-1.9072			4.37	-1.8664			4.37	-1.7129			4.37	-1.7129		
5.00	-1.9006			5.00	-1.8520			5.00	-1.6589			5.00	-1.6589		
6.25	-1.8330			6.25	-1.8068			6.25	-1.6148			6.25	-1.6148		
7.50	-1.7941			7.50	-1.7574			7.50	-1.5590			7.50	-1.5590		
8.75	-1.7581			8.75	-1.7405			8.75	-1.5450			8.75	-1.5450		
10.00	-1.7100			10.00	-1.7147			10.00	-1.5311			10.00	-1.5311		
12.50	-1.6810			12.50	-1.6485			12.50	-1.4572			12.50	-1.4572		
15.00	-1.6533			15.00	-1.6017			15.00	-1.4100			15.00	-1.4100		
17.50	-1.6326			17.50	-1.5675			17.50	-1.4079			17.50	-1.4079		
20.00	-1.5388			20.00	-1.5236			20.00	-1.3631			20.00	-1.3631		
30.00	-1.4365			30.00	-1.3623			30.00	-1.1769			30.00	-1.1769		
40.00	-1.1390			40.00	-0.8325			40.00	-0.4325			40.00	-0.4325		
50.00	-0.5162			50.00	-0.4554			50.00	-0.3171			50.00	-0.3171		
60.00	-0.4270			60.00	-0.3013			60.00	-0.3606			60.00	-0.3606		
70.00	-0.2918			70.00	-0.3101			70.00	-0.3860			70.00	-0.3860		
80.00	-0.2574			80.00	-0.2948			80.00	-0.3641			80.00	-0.3641		
90.00	-0.2908			90.00	-0.2927			90.00	-0.3300			90.00	-0.3300		
100.00	-0.2191			100.00	-0.2401			100.00	-0.2543			100.00	-0.2543		
110.00	-0.2096			110.00	-0.1986			110.00	-0.1997			110.00	-0.1997		
241.85	-0.0747			241.85	-0.0788			241.85	-0.0656			241.85	-0.0656		
279.84	-0.0652			279.84	-0.0680			279.84	-0.0524			279.84	-0.0524		

TABLE VI. Continued

(f) Continued

$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0142	343.16	-0.0258	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
-171.29	1.0167	384.14	-0.0180	X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-155.11	1.0131	419.13	-0.0064	CP	CP	CP	CP	CP	CP	CP	CP
-130.84	0.9944	457.12	0.0060	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
-106.57	0.9668	507.77	0.0390	X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-90.39	0.9138	545.76	0.0760	CP	CP	CP	CP	CP	CP	CP	CP
-74.21	0.8997	571.08	0.1255	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
-58.03	0.8593	583.74	0.1629	X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-41.85	0.8149	596.41	0.2127	CP	CP	CP	CP	CP	CP	CP	CP
-33.76	0.7938	609.07	0.2778	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
-25.67	0.7789			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-23.11	0.7793			CP	CP	CP	CP	CP	CP	CP	CP
-17.97	0.8021			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
-10.27	0.9297			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-5.13	1.0791			CP	CP	CP	CP	CP	CP	CP	CP
-3.34	1.1367			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
-2.05	1.1532			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
-0.90	1.0782			CP	CP	CP	CP	CP	CP	CP	CP
-0.44	0.9365			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
0.00	0.1265			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
0.31	-0.9568			CP	CP	CP	CP	CP	CP	CP	CP
0.63	-1.3814			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
1.25	-1.5966			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
1.88	-1.6084			CP	CP	CP	CP	CP	CP	CP	CP
2.50	-1.5862			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
3.13	-1.5634			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
3.75	-1.5409			CP	CP	CP	CP	CP	CP	CP	CP
4.37	-1.5199			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
5.00	-1.4830			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
6.25	-1.4394			CP	CP	CP	CP	CP	CP	CP	CP
7.50	-1.3768			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
8.75	-1.3434			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
10.00	-1.2922			CP	CP	CP	CP	CP	CP	CP	CP
12.50	-1.2719			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
15.00	-1.2392			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
17.50	-1.1801			CP	CP	CP	CP	CP	CP	CP	CP
20.00	-1.1424			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
30.00	-0.3636			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
40.00	-0.3875			CP	CP	CP	CP	CP	CP	CP	CP
50.00	-0.4315			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
60.00	-0.4216			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
70.00	-0.4182			CP	CP	CP	CP	CP	CP	CP	CP
80.00	-0.3879			Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody	Forebody
90.00	-0.3356			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
100.00	-0.2547			CP	CP	CP	CP	CP	CP	CP	CP
110.00	-0.1981			Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody	Afterbody
241.85	-0.0564			X/L	X/L	X/L	X/L	X/L	X/L	X/L	X/L
279.84	-0.0416			CP	CP	CP	CP	CP	CP	CP	CP

TABLE VI. Continued

(f) Concluded

mfr = 0.68 and $\alpha = 0^\circ$				mfr = 0.74 and $\alpha = 0^\circ$				mfr = 0.80 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.8725	343.16	-0.0061	-187.47	0.8644	343.16	0.0000	-187.47	0.8114	343.16	0.0075
-171.29	0.8740	384.14	0.0047	-106.57	0.7569	384.14	0.0070	-171.29	0.8017	384.14	0.0101
-155.11	0.8652	419.13	0.0137	-25.67	0.2279	419.13	0.0219	-155.11	0.8162	419.13	0.0258
-130.84	0.8303	457.12	0.0358	-10.27	0.4429	457.12	0.0353	-130.84	0.7624	457.12	0.0404
-106.57	0.7659	507.77	0.0746	-2.05	1.0321	507.77	0.0841	-106.57	0.6834	507.77	0.0815
-90.39	0.6956	545.76	0.1247	0.00	0.7204	545.76	0.1359	-90.39	0.4552	545.76	0.1416
-74.21	0.6210	571.08	0.1848	0.31	-0.1416	571.08	0.1956	-74.21	0.3252	571.08	0.1999
-58.03	0.5156	583.74	0.2296	0.63	-0.6537	583.74	0.2374	-58.03	0.1260	583.74	0.2432
-41.85	0.3915	596.41	0.2811	1.25	-0.8111	596.41	0.2900	-41.85	-0.1212	596.41	0.2944
-33.76	0.3230	609.07	0.3505	1.88	-0.9375	609.07	0.3576	-33.76	-0.2737	609.07	0.3602
-25.67	0.2332			2.50	-0.6772			-25.67	-0.6195		
-23.11	0.2204			3.13	-0.7102			-23.11	-0.7056		
-17.97	0.2559			3.75	-0.6102			-17.97	-0.4901		
-10.27	0.4589			4.37	-0.6623			-10.27	-0.0826		
-5.13	0.7653			5.00	-0.5382			-5.13	0.3589		
-3.34	0.9265			6.25	-0.4851			-3.34	0.5920		
-2.05	1.0566			7.50	-0.5386			-2.05	0.8201		
-0.90	1.1513			8.75	-0.5368			-0.90	1.0567		
-0.44	1.1292			10.00	-0.5776			-0.44	1.1406		
0.00	0.6850			12.50	-0.5821			0.00	0.9673		
0.31	-0.2259			15.00	-0.6003			0.31	0.2560		
0.63	-0.7487			17.50	-0.5027			0.63	-0.0901		
1.25	-0.8341			20.00	-0.4799			1.25	-0.0894		
1.88	-0.7738			30.00	-0.4150			1.88	-0.1677		
2.50	-0.7212			50.00	-0.4051			2.50	-0.1472		
3.13	-0.6483			60.00	-0.3894			3.13	-0.2022		
3.75	-0.6399			70.00	-0.3832			3.75	-0.1967		
4.37	-0.5685			80.00	-0.3501			4.37	-0.1967		
5.00	-0.6064			90.00	-0.3208			5.00	-0.2150		
6.25	-0.5541			100.00	-0.2265			6.25	-0.2470		
7.50	-0.4886			110.00	-0.1746			7.50	-0.2352		
8.75	-0.6384			241.85	-0.0401			8.75	-0.3320		
10.00	-0.5777							10.00	-0.3202		
12.50	-0.6137							12.50	-0.3780		
15.00	-0.6239							15.00	-0.3549		
17.50	-0.5221							17.50	-0.3559		
20.00	-0.4799							20.00	-0.3437		
30.00	-0.4334							30.00	-0.3202		
40.00	-0.4195							40.00	-0.3290		
50.00	-0.4036							50.00	-0.3328		
60.00	-0.3971							60.00	-0.3467		
70.00	-0.3741							70.00	-0.3378		
80.00	-0.3604							80.00	-0.3165		
90.00	-0.3134							90.00	-0.2753		
100.00	-0.2341							100.00	-0.2099		
110.00	-0.1603							110.00	-0.1458		
241.85	-0.0418							241.85	-0.0291		
279.84	-0.0327							279.84	-0.0204		

TABLE VI. Continued

(g) $M = 0.79$

$mfr = 0.27$ and $\alpha = 0^\circ$				$mfr = 0.30$ and $\alpha = 0^\circ$				$mfr = 0.40$ and $\alpha = 0^\circ$							
$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1250	343.16	-0.0505	-187.47	1.1272	343.16	-0.0451	-187.47	1.1163	343.16	-0.0489	-187.47	1.1155	343.16	-0.0374
-171.29	1.1250	384.14	-0.0494	-106.57	1.1141	384.14	-0.0487	-171.29	1.1170	384.14	-0.0453	-106.57	1.0992	384.14	-0.0425
-155.11	1.1257	419.13	-0.0483	-25.67	1.0828	419.13	-0.0437	-155.11	1.1156	419.13	-0.0435	-25.67	1.0779	419.13	-0.0288
-130.84	1.1201	457.12	-0.0426	-10.27	1.1537	457.12	-0.0483	-130.84	1.1110	457.12	-0.0378	-10.27	1.1388	457.12	-0.0418
-106.57	1.1110	507.77	-0.0368	-2.05	1.0314	507.77	-0.0447	-106.57	1.0997	507.77	-0.0274	-2.05	1.0600	507.77	-0.0335
-90.39	1.1033	545.76	-0.0336	0.00	-0.3463	545.76	-0.0415	-90.39	1.0888	545.76	-0.0190	0.00	-0.2627	545.76	-0.0217
-74.21	1.0959	571.08	-0.0182	0.31	-1.3649	571.08	-0.0285	-74.21	1.0800	571.08	0.0096	0.31	-1.3194	571.08	0.0006
-58.03	1.0857	583.74	-0.0046	0.63	-1.6642	583.74	-0.0067	-58.03	1.0677	583.74	0.0264	0.63	-1.6544	583.74	0.0254
-41.85	1.0748	596.41	0.0162	1.25	-1.8187	596.41	0.0187	-41.85	1.0551	596.41	0.0544	1.25	-1.7800	596.41	0.0523
-33.76	1.0613	609.07	0.0628	1.88	-1.8759	609.07	0.0632	-33.76	1.0521	609.07	0.1072	1.88	-1.8319	609.07	0.1057
-25.67	1.0488			2.50	-1.8592			-25.67	1.0596			2.50	-1.8404		
-23.11	1.0500			3.13	-1.8170			-23.11	1.0612			3.13	-1.8157		
-10.27	1.1038			3.75	-1.8116			-10.27	1.0810			3.75	-1.7757		
-10.27	1.1537			4.37	-1.7976			-10.27	1.1388			4.37	-1.7535		
-5.13	1.1522			5.00	-1.7838			-5.13	1.1631			5.00	-1.7232		
-3.34	1.1198			6.25	-1.7615			-3.34	1.1390			6.25	-1.7013		
-2.05	1.0297			7.50	-1.7278			-2.05	1.0626			7.50	-1.6683		
-0.90	0.8040			8.75	-1.7123			-0.90	0.8656			8.75	-1.6453		
-0.44	0.5669			10.00	-1.6476			-0.44	0.6316			10.00	-1.6087		
0.00	-0.4387			12.50	-1.5857			0.00	-0.3529			12.50	-1.5531		
0.31	-1.4713			15.00	-1.5662			0.31	-1.4257			15.00	-1.5257		
0.63	-1.6663			17.50	-1.5253			0.63	-1.4667			17.50	-1.5070		
1.25	-1.8190			20.00	-1.4944			1.25	-1.7950			20.00	-1.4549		
1.88	-1.8420			30.00	-1.3303			1.88	-1.8013			30.00	-1.3024		
2.50	-1.8678			50.00	-1.1303			2.50	-1.8035			50.00	-1.1092		
3.13	-1.8420			60.00	-0.8650			3.13	-1.7992			60.00	-0.5869		
3.75	-1.8173			70.00	-0.4413			3.75	-1.7798			70.00	-0.4276		
4.37	-1.8028			80.00	-0.3151			4.37	-1.7720			80.00	-0.2659		
5.00	-1.7685			90.00	-0.2122			5.00	-1.7372			90.00	-0.2078		
6.25	-1.7253			100.00	-0.1682			6.25	-1.6941			100.00	-0.1744		
7.50	-1.6963			110.00	-0.1357			7.50	-1.6552			110.00	-0.1459		
8.75	-1.6829			241.85	-0.0741			8.75	-1.6410			241.85	-0.0677		
10.00	-1.6271							10.00	-1.6113						
12.50	-1.5967							12.50	-1.5222						
15.00	-1.5632							15.00	-1.5164						
17.50	-1.5285							17.50	-1.4780						
20.00	-1.4882							20.00	-1.4542						
30.00	-1.2903							30.00	-1.2944						
40.00	-1.1925							40.00	-1.1888						
50.00	-1.0875							50.00	-1.0783						
60.00	-0.7484							60.00	-0.5682						
70.00	-0.4139							70.00	-0.3521						
80.00	-0.2850							80.00	-0.2461						
90.00	-0.2143							90.00	-0.2078						
100.00	-0.1774							100.00	-0.1848						
110.00	-0.1409							110.00	-0.1576						
241.85	-0.0803							241.85	-0.0714						
279.84	-0.0724							279.84	-0.0627						

TABLE VI. Continued

(g.) Continued

Forebody		φ = 0°		φ = 180°		Forebody		φ = 0°		φ = 180°		Afterbody		φ = 0°		φ = 180°	
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
mfr = 0.49 and α = 0°		-187.47	1.0281	343.16	-0.0175	-187.47	1.0276	343.16	-0.0093	-187.47	0.9977	343.16	-0.0143	-187.47	0.9984	343.16	-0.0049
mfr = 0.61 and α = 0°		-171.29	1.0302	384.14	-0.0114	-106.57	0.9775	384.14	-0.0114	-171.29	0.9998	384.14	-0.0085	-106.57	0.9357	384.14	-0.0087
		-155.11	1.0281	419.13	-0.0003	-25.67	0.7905	419.13	0.0008	-155.11	0.9928	419.13	0.0037	-25.67	0.6862	419.13	0.0084
		-130.84	1.0101	457.12	0.0152	-10.27	0.9362	457.12	0.0069	-130.84	0.9764	457.12	0.0213	-10.27	0.8635	457.12	0.0199
		-106.57	0.9604	507.77	0.0462	-2.05	1.1666	507.77	0.0390	-106.57	0.9385	507.77	0.0572	-2.05	1.1603	507.77	0.0518
		-90.39	0.9498	545.76	0.0868	0.00	0.2309	545.76	0.0807	-90.39	0.8969	545.76	0.1040	0.00	0.3835	545.76	0.1011
		-74.21	0.9180	571.08	0.1422	0.31	-0.8439	571.08	0.1329	-74.21	0.8581	571.08	0.1604	0.31	-0.6667	571.08	0.1593
		-58.03	0.8735	583.74	0.1789	0.63	-1.2639	583.74	0.1797	-58.03	0.8074	583.74	0.2010	0.63	-1.1327	583.74	0.2060
		-41.85	0.8308	596.41	0.2257	1.25	-1.4911	596.41	0.2304	-41.85	0.7485	596.41	0.2535	1.25	-1.3685	596.41	0.2617
		-33.76	0.8087	609.07	0.2955	1.88	-1.4955	609.07	0.3031	-33.76	0.7231	609.07	0.3228	1.88	-1.4192	609.07	0.3354
		-25.67	0.7905			2.50	-1.5134			-25.67	0.6894			2.50	-1.3884		
		-23.11	0.7881			3.13	-1.4872			-23.11	0.6894			3.13	-1.3495		
		-17.97	0.8274			3.75	-1.4636			-17.97	0.7283			3.75	-1.3386		
		-10.27	0.9317			4.37	-1.4140			-10.27	0.8615			4.37	-1.3066		
		-5.13	1.0821			5.00	-1.3978			-5.13	1.0339			5.00	-1.2924		
		-3.34	1.1467			6.25	-1.3320			-3.34	1.1101			6.25	-1.2053		
		-2.05	1.1617			7.50	-1.2887			-2.05	1.1604			7.50	-1.1734		
		-0.90	1.0988			8.75	-1.2747			-0.90	1.1284			8.75	-1.1509		
		-0.44	0.9576			10.00	-1.2265			-0.44	1.0160			10.00	-1.1066		
		0.00	0.1476			12.50	-1.1819			0.00	0.2856			12.50	-1.0903		
		0.31	-0.9183			15.00	-1.1875			0.31	-0.7672			15.00	-1.0473		
		0.63	-1.3119			17.50	-1.1811			0.63	-1.1774			17.50	-1.0604		
		1.25	-1.4949			20.00	-1.1221			1.25	-1.3829			20.00	-1.0091		
		1.88	-1.5042			30.00	-0.8945			1.88	-1.4077			30.00	-0.4088		
		2.50	-1.4839			50.00	-0.3534			2.50	-1.3744			50.00	-0.4450		
		3.13	-1.4481			60.00	-0.4095			3.13	-1.3517			60.00	-0.4462		
		3.75	-1.4382			70.00	-0.4175			3.75	-1.3237			70.00	-0.4287		
		4.37	-1.4144			80.00	-0.3908			4.37	-1.3018			80.00	-0.3909		
		5.00	-1.4024			90.00	-0.3442			5.00	-1.2660			90.00	-0.3475		
		6.25	-1.3616			100.00	-0.2561			6.25	-1.1806			100.00	-0.2528		
		7.50	-1.2850							7.50	-1.1357						
		8.75	-1.2524							8.75	-1.1473						
		10.00	-1.2449							10.00	-1.0967						
		12.50	-1.2119							12.50	-1.0570						
		15.00	-1.1978							15.00	-1.0783						
		17.50	-1.1754							17.50	-0.9968						
		20.00	-1.1400							20.00	-1.0040						
		30.00	-0.9470							30.00	-0.4010						
		40.00	-0.3851							40.00	-0.3974						
		50.00	-0.3473							50.00	-0.4225						
		60.00	-0.3959							60.00	-0.4431						
		70.00	-0.4099							70.00	-0.4319						
		80.00	-0.3997							80.00	-0.3953						
		90.00	-0.3434							90.00	-0.3436						
		100.00	-0.2625							100.00	-0.2504						
		241.85	-0.1884							110.00	-0.1881						
		279.84	-0.0549							241.85	-0.0476						
			-0.0445							279.84	-0.0410						

TABLE VI. Continued
(g) Concluded

$mfr = 0.68$ and $\alpha = 0^\circ$						$mfr = 0.74$ and $\alpha = 0^\circ$						$mfr = 0.80$ and $\alpha = 0^\circ$					
$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$		
Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody	
X/L	CP	X/L CP	X/L	CP	X/L CP	X/L	CP	X/L CP	X/L	CP	X/L CP	X/L	CP	X/L CP	X/L	CP	X/L CP
-187.47	0.8852	343.16	-0.0025	0.8862	343.16	-187.47	0.8828	343.16	-187.47	0.8237	343.16	-187.47	0.7504	343.16	-187.47	0.7442	343.16
-171.29	0.8887	384.14	0.0105	0.8862	384.14	-171.29	0.8281	384.14	-106.57	0.6928	384.14	-106.57	0.6281	384.14	-106.57	0.5804	384.14
-155.11	0.8788	419.13	0.0216	0.8862	419.13	-155.11	0.8190	419.13	-25.67	-0.0205	419.13	-155.11	0.7324	419.13	-25.67	-0.7652	419.13
-130.84	0.8442	457.12	0.0417	0.8862	457.12	-130.84	0.7739	457.12	-10.27	0.0495	457.12	-130.84	0.6769	457.12	-10.27	-0.0699	457.12
-106.57	0.7797	507.77	0.0824	0.8862	507.77	-106.57	0.6964	507.77	-2.05	0.10767	507.77	-106.57	0.5803	507.77	-2.05	0.8178	507.77
-90.39	0.7114	545.76	0.1363	0.8862	545.76	-90.39	0.6086	545.76	0.00	0.19996	545.76	-90.39	0.4717	545.76	0.00	1.0272	545.76
-74.21	0.6542	571.08	0.1996	0.8862	571.08	-74.21	0.5113	571.08	0.31	0.1053	571.08	-74.21	0.3385	571.08	0.31	0.3747	571.08
-58.03	0.5260	583.74	0.2434	0.8862	583.74	-58.03	0.4288	583.74	0.63	-0.3570	583.74	-58.03	0.1403	583.74	0.63	0.0637	583.74
-41.85	0.4002	596.41	0.2977	0.8862	596.41	-41.85	0.3710	596.41	1.25	-0.8863	596.41	-41.85	-0.1138	596.41	1.25	-0.1585	596.41
-33.76	0.3408	609.07	0.3682	0.8862	609.07	-33.76	0.2989	609.07	1.88	-0.4874	609.07	-33.76	-0.2491	609.07	1.88	-0.1093	609.07
-25.67	0.2492			0.8862		-25.67	-0.0316		2.30	-0.7940		-25.67	-0.7727		2.30	-0.2118	
-23.11	0.2333			0.8862		-23.11	-0.0681		3.13	-0.4218		-23.11	-0.7207		3.13	-0.1400	
-17.97	0.2611			0.8862		-17.97	-0.0145		3.75	-0.3942		-17.97	-0.5031		3.75	-0.1482	
-10.27	0.4832			0.8862		-10.27	0.2619		4.37	-0.3503		-10.27	-0.0525		4.37	-0.1359	
-5.13	0.7630			0.8862		-5.13	0.6016		5.00	-0.3651		-5.13	0.3584		5.00	-0.1788	
-3.34	0.9120			0.8862		-3.34	0.7973		6.25	-0.3437		-3.34	0.6004		6.25	-0.1413	
-2.05	1.0389			0.8862		-2.05	0.9609		7.50	-0.4121		-2.05	0.8172		7.50	-0.2268	
-0.90	1.1380			0.8862		-0.90	1.1315		8.75	-0.4542		-0.90	1.0604		8.75	-0.2685	
-0.44	1.1280			0.8862		-0.44	1.1644		10.00	-0.4336		-0.44	1.1555		10.00	-0.2868	
0.00	0.6955			0.8862		0.00	0.8296		12.50	-0.4885		0.00	0.9761		12.50	-0.3610	
0.31	-0.1874			0.8862		0.31	0.0912		15.00	-0.5085		0.31	0.2847		15.00	-0.3789	
0.63	-0.6175			0.8862		0.63	-0.3428		17.50	-0.4408		0.63	0.0377		17.50	-0.3551	
1.25	-0.8432			0.8862		1.25	-0.4478		20.00	-0.4161		1.25	-0.1927		20.00	-0.3293	
1.88	-0.8290			0.8862		1.88	-0.4233		30.00	-0.3667		1.88	-0.1321		30.00	-0.3344	
2.50	-0.5466			0.8862		2.50	-0.3460		50.00	-0.3922		2.50	-0.1917		50.00	-0.3447	
3.13	-0.6062			0.8862		3.13	-0.3715		60.00	-0.3715		3.13	-0.1507		60.00	-0.3698	
3.75	-0.5728			0.8862		3.75	-0.3595		70.00	-0.3771		3.75	-0.1446		70.00	-0.3459	
4.37	-0.5399			0.8862		4.37	-0.3297		80.00	-0.3480		4.37	-0.1525		80.00	-0.3400	
5.00	-0.6019			0.8862		5.00	-0.4240		90.00	-0.3066		5.00	-0.2044		90.00	-0.2888	
6.25	-0.5399			0.8862		6.25	-0.3850		100.00	-0.2230		6.25	-0.2203		100.00	-0.2145	
7.50	-0.4414			0.8862		7.50	-0.3382		110.00	-0.1573		7.50	-0.2139		110.00	-0.1455	
8.75	-0.6210			0.8862		8.75	-0.4698		241.85	-0.0249		8.75	-0.3016		241.85	-0.0234	
10.00	-0.6168			0.8862		10.00	-0.4087					10.00	-0.3019				
12.50	-0.5367			0.8862		12.50	-0.4868					12.50	-0.3524				
15.00	-0.6665			0.8862		15.00	-0.5231					15.00	-0.3844				
17.50	-0.5824			0.8862		17.50	-0.4475					17.50	-0.3613				
20.00	-0.5103			0.8862		20.00	-0.4205					20.00	-0.3542				
30.00	-0.4198			0.8862		30.00	-0.3935					30.00	-0.3461				
40.00	-0.4551			0.8862		40.00	-0.3848					40.00	-0.3612				
50.00	-0.4170			0.8862		50.00	-0.3871					50.00	-0.3546				
60.00	-0.4269			0.8862		60.00	-0.3798					60.00	-0.3666				
70.00	-0.3955			0.8862		70.00	-0.3767					70.00	-0.3559				
80.00	-0.3891			0.8862		80.00	-0.3470					80.00	-0.3347				
90.00	-0.3195			0.8862		90.00	-0.3071					90.00	-0.2924				
100.00	-0.2550			0.8862		100.00	-0.2175					100.00	-0.2117				
110.00	-0.1658			0.8862		110.00	-0.1579					110.00	-0.1486				
241.85	-0.0604			0.8862		241.85	-0.0311					241.85	-0.0234				
279.84	-0.0504			0.8862		279.84	-0.0174					279.84	-0.0151				

TABLE VI. Continued

(h) $M = 0.82$

$mfr = 0.27$ and $\alpha = 0^\circ$				$mfr = 0.30$ and $\alpha = 0^\circ$				$mfr = 0.40$ and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1372	343.16	-0.0462	-187.47	1.1388	343.16	-0.0383	-187.47	1.0942	343.16	-0.0316
-171.29	1.1365	384.14	-0.0445	-106.57	1.1266	384.14	-0.0428	-106.57	1.0935	384.14	-0.0247
-155.11	1.1355	419.13	-0.0421	-25.67	1.0987	419.13	-0.0358	-155.11	1.0932	419.13	-0.0167
-130.84	1.1314	457.12	-0.0365	-10.27	1.1637	457.12	-0.0400	-130.84	1.0817	457.12	-0.0036
-106.57	1.1243	507.77	-0.0289	-2.05	1.0479	507.77	-0.0365	-106.57	1.0644	507.77	0.0224
-90.39	1.1141	545.76	-0.0241	0.00	-0.2801	545.76	-0.0306	-90.39	1.0444	545.76	0.0545
-74.21	1.1073	571.08	-0.0060	0.31	-1.2743	571.08	-0.0109	-74.21	1.0261	571.08	0.0964
-58.03	1.0961	583.74	0.0106	0.63	-1.5922	583.74	0.0127	-58.03	1.0013	583.74	0.1299
-41.85	1.0896	596.41	0.0341	1.25	-1.7140	596.41	0.0321	-41.85	0.9775	596.41	0.1711
-33.76	1.0903	609.07	0.0823	1.88	-1.7824	609.07	0.0840	-33.76	0.9719	609.07	0.2375
-25.67	1.0960			2.50	-1.7704			-25.67	0.9677		
-23.11	1.1041			3.13	-1.7555			-23.11	0.9700		
-17.97	1.1171			3.75	-1.7078			-17.97	0.9990		
-10.27	1.1618			4.37	-1.7091			-10.27	1.0838		
-5.13	1.1494			5.00	-1.6802			-5.13	1.1630		
-3.34	1.1133			6.25	-1.6742			-3.34	1.1778		
-2.05	1.1023			7.50	-1.6208			-2.05	1.1458		
-0.90	0.8077			8.75	-1.6138			-0.90	1.0108		
-0.44	0.5963			10.00	-1.5636			-0.44	0.8347		
0.00	-0.3665			12.50	-1.5011			0.00	0.6048		
0.31	-1.3775			15.00	-1.4674			0.31	-1.0987		
0.63	-1.5765			17.50	-1.4486			0.63	-1.3956		
1.25	-1.7156			20.00	-1.3999			1.25	-1.5329		
1.88	-1.7343			30.00	-1.2697			1.88	-1.5591		
2.50	-1.7500			50.00	-1.0703			2.50	-1.5278		
3.13	-1.7412			60.00	-1.0243			3.13	-1.5411		
3.75	-1.7220			70.00	-0.9656			3.75	-1.5206		
4.37	-1.6869			80.00	-0.8711			4.37	-1.5131		
5.00	-1.6787			90.00	-0.8328			5.00	-1.4807		
6.25	-1.6441			100.00	-0.2826			6.25	-1.4235		
7.50	-1.6052			110.00	-0.1860			7.50	-1.4068		
8.75	-1.5888			241.85	-0.0783			8.75	-1.3751		
10.00	-1.5642							10.00	-1.3489		
12.50	-1.5172							12.50	-1.2751		
15.00	-1.5022							15.00	-1.2606		
17.50	-1.4564							17.50	-1.2306		
20.00	-1.4238							20.00	-1.2306		
30.00	-1.2693							30.00	-1.1232		
40.00	-1.1676							40.00	-1.0042		
50.00	-1.0815							50.00	-0.9610		
60.00	-1.0232							60.00	-0.9031		
70.00	-0.9801							70.00	-0.8554		
80.00	-0.9121							80.00	-0.2612		
90.00	-0.3720							90.00	-0.2152		
100.00	-0.2864							100.00	-0.1621		
241.85	-0.0832							110.00	-0.1297		
279.84	-0.0779							241.85	-0.0570		
								279.84	-0.0450		

TABLE VI. Continued
(h) Continued

mfr = 0.48 and $\alpha = 0^\circ$				mfr = 0.54 and $\alpha = 0^\circ$				mfr = 0.61 and $\alpha = 0^\circ$			
$\psi = 0^\circ$		$\psi = 180^\circ$		$\psi = 0^\circ$		$\psi = 180^\circ$		$\psi = 0^\circ$		$\psi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-187.47	1.0443	343.16	-0.0134	-187.47	1.0153	343.16	-0.0072	-187.47	0.9644	343.16	-0.0066
-171.29	1.0450	384.14	-0.0079	-106.57	0.9944	384.14	-0.0072	-171.29	0.9637	384.14	0.0056
-155.11	1.0402	419.13	0.0025	-25.67	0.8054	419.13	0.0056	-155.11	0.9579	419.13	0.0181
-130.84	1.0239	457.12	0.0181	-10.27	0.9607	457.12	0.0119	-130.84	0.9308	457.12	0.0396
-106.57	0.9964	507.77	0.0521	-2.05	1.1750	507.77	0.0490	-106.57	0.8838	507.77	0.0808
-90.39	0.9645	545.76	0.0978	0.00	0.2716	545.76	0.0916	-90.39	0.8307	545.76	0.1329
-74.21	0.9319	571.08	0.1550	0.31	-0.7691	571.08	0.1505	-74.21	0.7446	571.08	0.1968
-58.03	0.8913	583.74	0.1945	0.63	-1.1465	583.74	0.1970	-58.03	0.6954	583.74	0.2425
-41.85	0.8462	596.41	0.2465	1.25	-1.3840	596.41	0.2493	-41.85	0.6070	596.41	0.2963
-33.76	0.8257	609.07	0.3137	1.88	-1.4096	609.07	0.3228	-33.76	0.5717	609.07	0.3677
-25.67	0.8070			2.50	-1.3936			-25.67	0.5238		
-23.11	0.8135			3.13	-1.3724			-23.11	0.5181		
-17.97	0.8353			3.75	-1.3530			-17.97	0.5496		
-10.27	0.9592			4.37	-1.3199			-10.27	0.7118		
-5.13	1.0983			5.00	-1.2996			-5.13	0.9472		
-3.34	1.1580			6.25	-1.2635			-3.34	1.0608		
-2.05	1.1741			7.50	-1.2217			-2.05	1.1459		
-0.90	1.1087			8.75	-1.1965			-0.90	1.1700		
-0.44	0.9707			10.00	-1.1338			-0.44	1.1094		
0.00	0.2197			12.50	-1.1070			0.00	1.0511		
0.31	-0.8522			15.00	-1.0924			0.31	-0.4872		
0.63	-1.1982			17.50	-1.0958			0.63	-0.8652		
1.25	-1.3847			20.00	-1.0985			1.25	-1.1469		
1.88	-1.4004			30.00	-0.9603			1.88	-0.9887		
2.50	-1.3864			50.00	-0.6816			2.50	-0.7583		
3.13	-1.3619			60.00	-0.3051			3.13	-0.4976		
3.75	-1.3451			70.00	-0.3623			3.75	-0.3496		
4.37	-1.3113			80.00	-0.3343			4.37	-0.2329		
5.00	-1.2925			90.00	-0.3209			5.00	-0.1710		
6.25	-1.2652			100.00	-0.2449			6.25	-0.0856		
7.50	-1.2177			110.00	-0.1781			7.50	-0.7969		
8.75	-1.1859			120.00	-0.1181			8.75	-0.8656		
10.00	-1.1856			130.00	-0.0748			10.00	-0.8393		
12.50	-1.1180			150.00	-0.0423			12.50	-0.8072		
15.00	-1.1469			17.50	-0.1122			15.00	-0.7657		
20.00	-1.0933			30.00	-0.9161			20.00	-0.8397		
30.00	-0.9161			40.00	-0.8674			30.00	-0.7087		
40.00	-0.8674			50.00	-0.6260			40.00	-0.5354		
50.00	-0.6260			60.00	-0.3098			50.00	-0.4688		
60.00	-0.3098			70.00	-0.3539			60.00	-0.4411		
70.00	-0.3539			80.00	-0.3450			70.00	-0.4623		
80.00	-0.3450			90.00	-0.3241			80.00	-0.4499		
90.00	-0.3241			100.00	-0.2333			90.00	-0.3517		
100.00	-0.2333			241.85	-0.1803			100.00	-0.2456		
241.85	-0.0538			279.84	-0.0330			241.85	-0.1692		
279.84	-0.0330							279.84	-0.0383		
									-0.0279		

TABLE VI. Continued

(h) Concluded

mfr = 0.80 and $\alpha = 0^\circ$															
$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.9058	343.16	0.0027	-187.47	0.8443	343.16	0.0086	-187.47	0.8398	343.16	0.0165	-187.47	0.7516	343.16	0.0252
-171.29	0.9068	384.14	0.0141	-106.57	0.7983	384.14	0.0152	-106.57	0.7107	384.14	0.0210	-171.29	0.7516	384.14	0.0279
-155.11	0.8989	419.13	0.0297	-25.67	0.2922	419.13	0.0318	-25.67	0.0194	419.13	0.0377	-155.11	0.7383	419.13	0.0477
-130.84	0.8643	457.12	0.0508	-10.27	0.5256	457.12	0.0463	-10.27	0.2697	457.12	0.0522	-130.84	0.6850	457.12	0.0619
-106.57	0.8043	507.77	0.0941	-2.05	1.0776	507.77	0.0944	-2.05	1.0017	507.77	0.1034	-106.57	0.5909	507.77	0.1108
-90.39	0.7351	545.76	0.1523	0.00	1.7421	545.76	0.1626	0.00	0.8832	545.76	0.1602	-90.39	0.4811	545.76	0.1683
-74.21	0.6601	571.08	0.2171	0.31	-0.0836	571.08	0.2209	-74.21	0.3249	571.08	0.2283	-74.21	0.3520	571.08	0.2376
-58.03	0.5519	583.74	0.2617	0.63	-0.5273	583.74	0.2683	0.63	-0.3203	583.74	0.2795	-58.03	0.3259	583.74	0.2848
-41.85	0.4347	596.41	0.3143	1.25	-0.8143	596.41	0.3254	1.25	-0.4878	596.41	0.3363	1.25	-0.1575	596.41	0.3392
-33.76	0.3652	609.07	0.3866	1.88	-0.8616	609.07	0.3960	1.88	-0.5010	609.07	0.4045	1.88	-0.1972	609.07	0.4064
-25.67	0.2838			2.50	-0.8653			2.50	-0.4019			2.50	-0.1456		
-23.11	0.2705			3.13	-0.6152			3.13	-0.3703			3.13	-0.1640		
-17.97	0.2987			3.75	-0.6434			3.75	-0.3483			3.75	-0.1598		
-10.27	0.5202			4.37	-0.5657			4.37	-0.3379			4.37	-0.1948		
-5.13	0.8031			5.00	-0.5235			5.00	-0.3644			5.00	-0.1632		
-3.34	0.9473			6.25	-0.4165			6.25	-0.3163			6.25	-0.1620		
-2.05	1.0775			7.50	-0.4694			7.50	-0.2732			7.50	-0.2120		
-0.90	1.1697			8.75	-0.4981			8.75	-0.2470			8.75	-0.2436		
-0.44	1.1545			10.00	-0.5292			10.00	-0.4452			10.00	-0.2999		
0.00	0.7035			12.50	-0.6036			12.50	-0.4341			12.50	-0.3713		
0.31	-0.2009			15.00	-0.6197			15.00	-0.5575			15.00	-0.4150		
0.63	-0.5946			17.50	-0.6768			17.50	-0.5491			17.50	-0.3740		
1.25	-0.8263			20.00	-0.6415			20.00	-0.4770			20.00	-0.3417		
1.88	-0.8379			30.00	-0.4067			30.00	-0.3904			30.00	-0.3421		
2.50	-0.8137			50.00	-0.4449			50.00	-0.4073			50.00	-0.3809		
3.13	-0.6161			60.00	-0.4388			60.00	-0.4184			60.00	-0.3759		
3.75	-0.5840			70.00	-0.4293			70.00	-0.4157			70.00	-0.3835		
4.37	-0.5530			80.00	-0.3910			80.00	-0.3789			80.00	-0.3421		
5.00	-0.5342			90.00	-0.3272			90.00	-0.3176			90.00	-0.3079		
6.25	-0.5250			100.00	-0.2321			100.00	-0.2257			100.00	-0.2127		
7.50	-0.4189			110.00	-0.1599			110.00	-0.1548			110.00	-0.1486		
8.75	-0.5701			241.85	-0.0170			241.85	-0.0236			241.85	-0.0196		
10.00	-0.5902														
12.50	-0.6171														
15.00	-0.6376														
17.50	-0.6710														
20.00	-0.6600														
30.00	-0.4449														
40.00	-0.4413														
50.00	-0.4428														
60.00	-0.4437														
70.00	-0.4350														
80.00	-0.4065														
90.00	-0.3285														
100.00	-0.2402														
110.00	-0.1634														
241.85	-0.0386														
279.84	-0.0242														

TABLE VI. Continued

(i) $M = 0.84$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1500	343.16	-0.0368	-187.47	1.1525	343.16	-0.0291	-187.47	1.1436	343.16	-0.0234	-187.47	1.1043	343.16	-0.0133
-171.29	1.1513	384.14	-0.0358	-106.57	1.1381	384.14	-0.0362	-171.29	1.1439	384.14	-0.0308	-171.29	1.1064	384.14	-0.0197
-155.11	1.1503	419.13	-0.0368	-23.67	1.1116	419.13	-0.0345	-155.11	1.1417	419.13	-0.0264	-155.11	1.1034	419.13	-0.0103
-130.84	1.1470	457.12	-0.0305	-10.27	1.1779	457.12	-0.0352	-130.84	1.1344	457.12	-0.0291	-130.84	1.0939	457.12	-0.0029
-106.57	1.1395	507.77	-0.0238	-2.05	1.0637	507.77	-0.0285	-106.57	1.1249	507.77	-0.0164	-106.57	1.0761	507.77	0.0276
-90.39	1.1294	545.76	-0.0105	0.00	-0.1979	545.76	-0.0171	-90.39	1.1170	545.76	0.0070	-90.39	1.0581	545.76	0.0641
-74.21	1.1222	571.08	0.0102	0.31	-1.1763	571.08	0.0082	-74.21	1.1052	571.08	0.0355	-74.21	1.0381	571.08	0.1126
-58.03	1.1101	583.74	0.0259	0.63	-1.4728	583.74	0.0283	-58.03	1.0934	583.74	0.0606	-58.03	1.0131	583.74	0.1454
-41.85	1.1032	596.41	0.0540	1.25	-1.9989	596.41	0.0543	-41.85	1.0819	596.41	0.0891	-41.85	0.9934	596.41	0.1874
-33.76	1.1064	609.07	0.1004	1.88	-1.6402	609.07	0.1074	-33.76	1.0794	609.07	0.1436	-33.76	0.9825	609.07	0.2510
-23.67	1.1112			2.50	-1.6487			-23.67	1.0846			-23.67	0.9821		
-23.11	1.1175			3.13	-1.6379			-23.11	1.0905			-23.11	0.9869		
-17.97	1.1348			3.75	-1.6203			-17.97	1.1112			-17.97	1.0128		
-10.27	1.1775			4.37	-1.5746			-10.27	1.1644			-10.27	1.0890		
-5.13	1.1811			5.00	-1.5637			-5.13	1.1859			-5.13	1.1758		
-3.34	1.1436			6.25	-1.5492			-3.34	1.1619			-3.34	1.1862		
-2.05	1.0644			7.50	-1.5172			-2.05	1.0913			-2.05	1.1568		
-0.90	0.8322			8.75	-1.4983			-0.90	0.8999			-0.90	1.1588		
-0.44	0.6400			10.00	-1.4639			-0.44	0.6916			-0.44	1.1568		
0.00	-0.3244			12.50	-1.4125			0.00	-0.2511			0.00	1.1568		
0.31	-1.2779			15.00	-1.3778			0.31	-1.2388			0.31	1.1568		
0.63	-1.4658			17.50	-1.3541			0.63	-1.4592			0.63	1.1568		
1.25	-1.6083			20.00	-1.3242			1.25	-1.5751			1.25	1.1568		
1.88	-1.6254			30.00	-1.2007			1.88	-1.3963			1.88	1.1568		
2.50	-1.6326			50.00	-1.0174			2.50	-1.6088			2.50	1.1568		
3.13	-1.6214			60.00	-0.9886			3.13	-1.5979			3.13	1.1568		
3.75	-1.6057			70.00	-0.9412			3.75	-1.5748			3.75	1.1568		
4.37	-1.5856			80.00	-0.9405			4.37	-1.5666			4.37	1.1568		
5.00	-1.5701			90.00	-0.7423			5.00	-1.5338			5.00	1.1568		
6.25	-1.5395			100.00	-0.4118			6.25	-1.5038			6.25	1.1568		
7.50	-1.5000			110.00	-0.3686			7.50	-1.4790			7.50	1.1568		
8.75	-1.4908			241.85	-0.3821			8.75	-1.4592			8.75	1.1568		
10.00	-1.4582							10.00	-1.4338			10.00	1.1568		
12.50	-1.4046							12.50	-1.3943			12.50	1.1568		
15.00	-1.3926							15.00	-1.3542			15.00	1.1568		
17.50	-1.3625							17.50	-1.3269			17.50	1.1568		
20.00	-1.3194							20.00	-1.3038			20.00	1.1568		
30.00	-1.1792							30.00	-1.1761			30.00	1.1568		
40.00	-1.0763							40.00	-1.0783			40.00	1.1568		
50.00	-1.0259							50.00	-1.0045			50.00	1.1568		
60.00	-0.9676							60.00	-1.0045			60.00	1.1568		
70.00	-0.9553							70.00	-0.9639			70.00	1.1568		
80.00	-0.9317							80.00	-0.9574			80.00	1.1568		
90.00	-0.7588							90.00	-0.9256			90.00	1.1568		
100.00	-0.4208							100.00	-0.4894			100.00	1.1568		
110.00	-0.3777							110.00	-0.3748			110.00	1.1568		
241.85	-0.0406							241.85	-0.3521			241.85	1.1568		
279.84	-0.0398							279.84	-0.0438			279.84	1.1568		

mfr = 0.38 and $\alpha = 0^\circ$

mfr = 0.30 and $\alpha = 0^\circ$

mfr = 0.27 and $\alpha = 0^\circ$

TABLE VI. Continued

(i) Continued

mfr = 0.49 and $\alpha = 2.0^\circ$															
$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0567	343.16	-0.0105	-187.47	1.0550	343.16	-0.0002	-187.47	1.0588	343.16	-0.0152	-187.47	1.0568	343.16	0.0045
-171.29	1.0574	384.14	-0.0028	-171.29	1.0590	384.14	-0.0002	-171.29	1.0588	384.14	-0.0089	-171.29	1.0588	384.14	0.0032
-155.11	1.0538	419.13	0.0072	-155.11	1.0560	419.13	0.0109	-155.11	1.0539	419.13	0.0095	-155.11	1.0539	419.13	0.0086
-130.84	1.0353	457.12	0.0263	-130.84	1.0390	457.12	0.0223	-130.84	1.0390	457.12	0.0186	-130.84	1.0388	457.12	0.0206
-106.57	1.0078	507.77	0.0619	-106.57	1.0101	507.77	0.0661	-106.57	1.0099	507.77	0.0567	-106.57	1.0099	507.77	0.0662
-90.39	0.9775	545.76	0.1108	-90.39	0.9835	545.76	0.1137	-90.39	0.9835	545.76	0.1083	-90.39	0.9810	545.76	0.1100
-74.21	0.9453	571.08	0.1701	-74.21	0.9510	571.08	0.1692	-74.21	0.9515	571.08	0.1646	-74.21	0.9515	571.08	0.1646
-58.03	0.9009	583.74	0.2101	-58.03	0.9112	583.74	0.2064	-58.03	0.9143	583.74	0.2161	-58.03	0.9143	583.74	0.1998
-41.85	0.8615	596.41	0.2620	-41.85	0.8692	596.41	0.2506	-41.85	0.8805	596.41	0.2727	-41.85	0.8805	596.41	0.2423
-33.76	0.8475	609.07	0.3321	-33.76	0.8543	609.07	0.3152	-33.76	0.8666	609.07	0.3510	-33.76	0.8666	609.07	0.2999
-25.67	0.8301			-25.67	0.8362			-25.67	0.8625			-25.67	0.8625		
-23.11	0.8245			-23.11	0.8399			-23.11	0.8603			-23.11	0.8603		
-17.97	0.8578			-17.97	0.8727			-17.97	0.9002			-17.97	0.9002		
-10.27	0.9850			-10.27	0.9883			-10.27	1.0199			-10.27	1.0199		
-5.13	1.1094			-5.13	1.1306			-5.13	1.1423			-5.13	1.1423		
-3.34	1.1703			-3.34	1.1786			-3.34	1.1823			-3.34	1.1823		
-2.05	1.1882			-2.05	1.1879			-2.05	1.1815			-2.05	1.1815		
-0.90	1.1265			-0.90	1.1123			-0.90	1.0474			-0.90	1.0885		
-0.44	0.9980			-0.44	0.9666			-0.44	0.9932			-0.44	0.9373		
0.00	0.2323			0.00	0.2159			0.00	0.2159			0.00	0.1177		
0.31	-0.7719			0.31	-0.8432			0.31	-0.8432			0.31	-0.9051		
0.63	-1.1137			0.63	-1.1606			0.63	-1.1606			0.63	-1.2222		
1.25	-1.2843			1.25	-1.3229			1.25	-1.3229			1.25	-1.3826		
1.88	-1.3074			1.88	-1.3463			1.88	-1.3463			1.88	-1.3955		
2.50	-1.2922			2.50	-1.3209			2.50	-1.3209			2.50	-1.3806		
3.13	-1.2625			3.13	-1.3206			3.13	-1.3206			3.13	-1.3826		
3.75	-1.2625			3.75	-1.3064			3.75	-1.3064			3.75	-1.3645		
4.37	-1.2393			4.37	-1.2770			4.37	-1.2770			4.37	-1.3625		
5.00	-1.2119			5.00	-1.2236			5.00	-1.2236			5.00	-1.3262		
6.25	-1.1743			6.25	-1.2394			6.25	-1.2394			6.25	-1.3044		
7.50	-1.1459			7.50	-1.1787			7.50	-1.1787			7.50	-1.2582		
8.75	-1.0999			8.75	-1.1820			8.75	-1.1820			8.75	-1.2411		
10.00	-1.0589			10.00	-1.1691			10.00	-1.1691			10.00	-1.2226		
12.50	-1.0589			12.50	-1.1510			12.50	-1.1510			12.50	-1.1866		
15.00	-1.0317			15.00	-1.1349			15.00	-1.1349			15.00	-1.2005		
17.50	-1.0444			17.50	-1.1233			17.50	-1.1233			17.50	-1.1506		
20.00	-1.0158			20.00	-1.0961			20.00	-1.0961			20.00	-1.1417		
30.00	-0.8905			30.00	-0.9752			30.00	-0.9752			30.00	-1.0810		
40.00	-0.8436			40.00	-0.9194			40.00	-0.9194			40.00	-0.9645		
50.00	-0.7626			50.00	-0.8782			50.00	-0.8782			50.00	-0.9510		
60.00	-0.7650			60.00	-0.8316			60.00	-0.8316			60.00	-0.9084		
70.00	-0.6980			70.00	-0.8412			70.00	-0.8412			70.00	-0.8652		
80.00	-0.2744			80.00	-0.4140			80.00	-0.4140			80.00	-0.4474		
90.00	-0.2350			90.00	-0.2337			90.00	-0.2337			90.00	-0.2850		
100.00	-0.1969			100.00	-0.1510			100.00	-0.1510			100.00	-0.2014		
110.00	-0.1283			110.00	-0.0985			110.00	-0.0985			110.00	-0.0893		
241.85	-0.0428			241.85	-0.0377			241.85	-0.0377			241.85	-0.0397		
279.84	-0.0343			279.84	-0.0327			279.84	-0.0327			279.84	-0.0343		

TABLE VI. Continued

(i) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
$mfr = 0.48$ and $\alpha = 3.1^\circ$				$mfr = 0.54$ and $\alpha = 0^\circ$				$mfr = 0.61$ and $\alpha = 0^\circ$				$mfr = 0.61$ and $\alpha = 0^\circ$			
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0592	343.16	0.0136	-187.47	1.0270	343.16	-0.0085	-187.47	1.0259	343.16	0.0049	-187.47	0.9793	343.16	0.0026
-171.29	1.0373	384.14	0.0083	-171.29	1.0296	384.14	0.0022	-171.29	0.9663	384.14	0.0035	-171.29	0.9816	384.14	0.0110
-155.11	1.0580	419.13	0.0126	-155.11	1.0237	419.13	0.0133	-155.11	0.9663	419.13	0.0206	-155.11	0.9747	419.13	0.0257
-130.84	1.0415	457.12	0.0304	-130.84	1.0077	457.12	0.0187	-130.84	0.8957	457.12	0.0327	-130.84	0.9472	457.12	0.0478
-106.57	1.0122	507.77	0.0646	-106.57	0.9672	507.77	0.0559	-106.57	0.8257	507.77	0.0736	-106.57	0.8999	507.77	0.0906
-90.39	0.9840	545.76	0.1075	-90.39	0.9304	545.76	0.1296	-90.39	0.7506	545.76	0.1259	-90.39	0.8500	545.76	0.1502
-74.21	0.9557	571.08	0.1568	-74.21	0.8896	571.08	0.1937	-74.21	0.6004	571.08	0.1937	-74.21	0.7959	571.08	0.2162
-58.03	0.9212	583.74	0.1894	-58.03	0.8368	583.74	0.2182	-58.03	0.4647	583.74	0.2409	-58.03	0.7208	583.74	0.2654
-41.85	0.8886	596.41	0.2272	-41.85	0.7769	596.41	0.2892	-41.85	0.3417	596.41	0.2979	-41.85	0.6417	596.41	0.3166
-33.76	0.8799	609.07	0.2809	-33.76	0.7559	609.07	0.3586	-33.76	0.2316	609.07	0.3706	-33.76	0.5862	609.07	0.3875
-25.67	0.8736			-25.67	0.7191			-25.67	0.1937			-25.67	0.5370		
-23.11	0.8765			-23.11	0.7230			-23.11	0.1782			-23.11	0.5362		
-17.97	0.9113			-17.97	0.7570			-17.97	0.1708			-17.97	0.5788		
-10.27	1.0326			-10.27	0.8861			-10.27	0.1437			-10.27	0.7398		
-5.13	1.1328			-5.13	1.0510			-5.13	0.1174			-5.13	0.9595		
-3.34	1.1854			-3.34	1.1398			-3.34	0.1046			-3.34	1.0818		
-2.05	1.1765			-2.05	1.1856			-2.05	0.1041			-2.05	1.1536		
-0.90	1.0678			-0.90	1.1600			-0.90	0.10251			-0.90	1.1834		
-0.44	0.9059			-0.44	1.0579			-0.44	0.09585			-0.44	1.1327		
0.00	0.0798			0.00	0.3849			0.00	0.0440			0.00	0.5440		
0.31	-0.9835			0.31	-0.7211			0.31	-0.5933			0.31	-0.7681		
0.63	-1.2591			0.63	-0.7136			0.63	-0.9574			0.63	-1.0751		
1.25	-1.4276			1.25	-0.6528			1.25	-1.1950			1.25	-1.0309		
1.88	-1.4447			1.88	-0.5484			1.88	-1.2294			1.88	-1.0263		
2.50	-1.4355			2.50	-0.4352			2.50	-1.1987			2.50	-1.0131		
3.13	-1.4355			3.13	-0.4809			3.13	-1.1656			3.13	-0.9960		
3.75	-1.4200			3.75	-0.5128			3.75	-1.1465			3.75	-0.9702		
4.37	-1.4134			4.37	-0.5418			4.37	-1.1163			4.37	-0.9237		
5.00	-1.3972			5.00	-0.4612			5.00	-1.0998			5.00	-0.9349		
6.25	-1.3585			6.25	-0.2406			6.25	-1.0529			6.25	-0.8004		
7.50	-1.3304			7.50	-0.1656			7.50	-1.0063			7.50	-0.8228		
8.75	-1.3050			8.75	-0.0350			8.75	-0.9746			8.75	-0.8119		
10.00	-1.2977			10.00	-0.9835			10.00	-0.9835			10.00	-0.7931		
12.50	-1.2733			12.50	-0.9964			12.50	-0.9964			12.50	-0.7730		
15.00	-1.2577			15.00	-0.9686			15.00	-0.9686			15.00	-0.7903		
17.50	-1.2267			17.50	-0.9178			17.50	-0.9178			17.50	-0.7588		
20.00	-1.2074			20.00	-0.9388			20.00	-0.9388			20.00	-0.7609		
30.00	-1.1116			30.00	-0.8438			30.00	-0.8438			30.00	-0.6555		
40.00	-1.0497			40.00	-0.7491			40.00	-0.7491			40.00	-0.6321		
50.00	-1.0185			50.00	-0.6142			50.00	-0.6142			50.00	-0.5846		
60.00	-0.9641			60.00	-0.6142			60.00	-0.6142			60.00	-0.4237		
70.00	-0.8340			70.00	-0.3850			70.00	-0.3850			70.00	-0.4427		
80.00	-0.4277			80.00	-0.3173			80.00	-0.3173			80.00	-0.4257		
90.00	-0.3923			90.00	-0.2969			90.00	-0.2969			90.00	-0.3956		
100.00	-0.3034			100.00	-0.2182			100.00	-0.2182			100.00	-0.2397		
110.00	-0.1914			110.00	-0.1589			110.00	-0.1589			110.00	-0.1644		
241.85	-0.0288			241.85	-0.0350			241.85	-0.0350			241.85	-0.0383		
279.84	-0.0276			279.84	-0.0280			279.84	-0.0280			279.84	-0.0290		

TABLE VI. Continued

(i) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.9258	343.16	0.0055	-187.47	0.9252	343.16	0.0176	-187.47	0.9253	343.16	0.0070	-187.47	0.9260	343.16	0.0270
-171.29	0.9272	384.14	0.0186	-106.57	0.8239	384.14	0.0196	-106.57	0.8238	384.14	0.0170	-171.29	0.9280	384.14	0.0277
-155.11	0.9202	419.13	0.0346	-25.67	0.3258	419.13	0.0396	-155.11	0.9195	419.13	0.0358	-155.11	0.9200	419.13	0.0384
-130.84	0.8865	457.12	0.0584	-102.7	0.3345	457.12	0.0557	-130.84	0.8861	457.12	0.0538	-130.84	0.8849	457.12	0.0611
-90.39	0.8275	507.77	0.1062	-2.05	0.0978	507.77	0.1065	-106.57	0.8270	507.77	0.1020	-90.39	0.8263	507.77	0.1096
-74.21	0.6861	571.08	0.2331	0.31	-0.0653	571.08	0.2364	-74.21	0.6919	571.08	0.2331	-74.21	0.6961	571.08	0.2341
-58.03	0.5839	583.74	0.2778	0.63	-0.3517	583.74	0.2888	-58.03	0.5932	583.74	0.2853	-58.03	0.6007	583.74	0.2782
-41.85	0.4683	596.41	0.3333	1.25	-0.7648	596.41	0.3457	-41.85	0.4851	596.41	0.3455	-41.85	0.5010	596.41	0.3291
-25.67	0.3339	609.07	0.4038	1.88	-0.8152	609.07	0.4162	-25.67	0.3376	609.07	0.4181	-25.67	0.3498	609.07	0.3909
-23.11	0.3151			3.13	-0.7381			-23.11	0.3528			-23.11	0.3811		
-17.97	0.3561			3.75	-0.6205			-17.97	0.3956			-17.97	0.4350		
-10.27	0.3673			4.37	-0.6173			-10.27	0.3942			-10.27	0.6476		
-5.13	0.8282			5.00	-0.5987			-5.13	0.8535			-5.13	0.9020		
-3.34	0.9697			6.25	-0.4818			-3.34	0.9809			-3.34	1.0337		
-2.05	1.1004			7.50	-0.4710			-2.05	1.0711			-2.05	1.1401		
-0.90	1.1798			8.75	-0.4529			-0.90	1.1745			-0.90	1.1851		
-0.44	1.1628			10.00	-0.4932			-0.44	1.1459			-0.44	1.1382		
0.00	0.7048			12.50	-0.5366			0.00	0.6621			0.00	0.5797		
0.31	-0.1119			15.00	-0.6065			0.31	-0.2401			0.31	-0.3208		
0.63	-0.6097			17.50	-0.6265			0.63	-0.7043			0.63	-0.7668		
1.25	-0.8116			20.00	-0.6105			1.25	-0.9213			1.25	-1.0575		
1.88	-0.8099			30.00	-0.5677			1.88	-0.9223			1.88	-0.9959		
2.50	-0.7247			50.00	-0.4233			2.50	-0.8966			2.50	-1.0078		
3.13	-0.6370			60.00	-0.4204			3.13	-0.8986			3.13	-0.9903		
3.75	-0.6848			70.00	-0.4533			3.75	-0.7927			3.75	-0.9468		
4.37	-0.6120			80.00	-0.4936			4.37	-0.7729			4.37	-0.9148		
5.00	-0.6025			90.00	-0.3930			5.00	-0.7881			5.00	-0.8970		
6.25	-0.3600			100.00	-0.2181			6.25	-0.6317			6.25	-0.8364		
7.50	-0.4814			110.00	-0.1544			7.50	-0.7235			7.50	-0.7859		
8.75	-0.5291							8.75	-0.7172			8.75	-0.8182		
10.00	-0.5284							10.00	-0.6608			10.00	-0.7883		
12.50	-0.5663							12.50	-0.5922			12.50	-0.8212		
15.00	-0.6038							15.00	-0.7149			15.00	-0.8048		
17.50	-0.6298							17.50	-0.6624			17.50	-0.8120		
20.00	-0.6397							20.00	-0.6809			20.00	-0.8268		
30.00	-0.6143							30.00	-0.6311			30.00	-0.7286		
40.00	-0.5398							40.00	-0.6380			40.00	-0.6966		
50.00	-0.4131							50.00	-0.5668			50.00	-0.6372		
60.00	-0.4320							60.00	-0.4517			60.00	-0.4956		
70.00	-0.4766							70.00	-0.4096			70.00	-0.3911		
80.00	-0.4930							80.00	-0.4386			80.00	-0.3740		
90.00	-0.3760							90.00	-0.3842			90.00	-0.3317		
100.00	-0.2322							100.00	-0.2388			100.00	-0.2241		
110.00	-0.1504							110.00	-0.1517			110.00	-0.1543		
241.85	-0.0370							241.85	-0.0436			241.85	-0.0282		
279.84	-0.0231							279.84	-0.0359			279.84	-0.0274		

TABLE VI. Continued

(i) Continued

$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$		
Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody		Forebody	Afterbody	
XL	CP	X/L	XL	CP	X/L	XL	CP	X/L	XL	CP	X/L
-187.47	0.9275	343.16	-187.47	0.9285	343.16	-187.47	0.8654	343.16	-187.47	0.1338	343.16
-171.29	0.9271	384.14	-171.29	0.9281	384.14	-171.29	0.8668	384.14	-171.29	0.0881	384.14
-155.11	0.9212	419.13	-155.11	0.9222	419.13	-155.11	0.8576	419.13	-155.11	0.0077	419.13
-130.84	0.8867	457.12	-130.84	0.8877	457.12	-130.84	0.8153	457.12	-130.84	-0.1032	457.12
-106.57	0.8297	507.77	-106.57	0.8307	507.77	-106.57	0.7405	507.77	-106.57	-0.1871	507.77
-90.39	0.7661	545.76	-90.39	0.7671	545.76	-90.39	0.6569	545.76	-90.39	-0.2693	545.76
-58.03	0.6035	571.08	-58.03	0.6045	571.08	-58.03	0.5615	571.08	-58.03	-0.3102	571.08
-41.85	0.5100	583.74	-41.85	0.5110	583.74	-41.85	0.4238	583.74	-41.85	-0.3666	583.74
-33.76	0.4651	609.07	-33.76	0.4661	609.07	-33.76	0.2589	596.41	-33.76	-0.4037	596.41
-25.67	0.4205	641.11	-25.67	0.4215	641.11	-25.67	0.1725	609.07	-25.67	-0.4377	609.07
-23.11	0.4234	673.15	-23.11	0.4244	673.15	-23.11	0.0604	609.07	-23.11	-0.4670	609.07
-17.97	0.4755	705.19	-17.97	0.4765	705.19	-17.97	0.0120	641.11	-17.97	-0.4963	641.11
-10.27	0.6770	737.23	-10.27	0.6780	737.23	-10.27	0.0784	673.15	-10.27	-0.5256	673.15
-5.13	0.9379	769.27	-5.13	0.9389	769.27	-5.13	0.0590	705.19	-5.13	-0.5549	705.19
-3.34	1.0679	801.31	-3.34	1.0689	801.31	-3.34	0.0611	737.23	-3.34	-0.5842	737.23
-2.05	1.1504	833.35	-2.05	1.1514	833.35	-2.05	0.0811	769.27	-2.05	-0.6135	769.27
-0.90	1.1729	865.39	-0.90	1.1739	865.39	-0.90	0.1017	801.31	-0.90	-0.6428	801.31
-0.44	1.1229	897.43	-0.44	1.1239	897.43	-0.44	0.1651	833.35	-0.44	-0.6721	833.35
0.00	0.5288	929.47	0.00	0.5298	929.47	-0.44	0.1887	865.39	-0.44	-0.7014	865.39
0.31	-0.4095	961.51	0.31	-0.4105	961.51	0.00	0.8458	897.43	0.00	-0.7307	897.43
0.63	-0.8456	993.55	0.63	-0.8466	993.55	0.31	0.0921	929.47	0.31	-0.7600	929.47
1.25	-1.0947	1025.59	1.25	-1.0957	1025.59	0.63	0.3673	961.51	0.63	-0.7893	961.51
1.88	-1.1198	1057.63	1.88	-1.1208	1057.63	1.25	-0.4672	993.55	1.25	-0.8186	993.55
2.50	-1.0904	1089.67	2.50	-1.0914	1089.67	1.88	-0.4290	1025.59	1.88	-0.8479	1025.59
3.13	-1.0907	1121.71	3.13	-1.0917	1121.71	2.50	-0.3044	1057.63	2.50	-0.8772	1057.63
3.75	-1.0410	1153.75	3.75	-1.0420	1153.75	3.13	-0.3937	1089.67	3.13	-0.9065	1089.67
4.37	-1.0255	1185.79	4.37	-1.0265	1185.79	3.75	0.3568	1121.71	3.75	-0.9358	1121.71
5.00	-1.0057	1217.83	5.00	-1.0067	1217.83	4.37	-0.3449	1153.75	4.37	-0.9651	1153.75
6.25	-0.9830	1249.87	6.25	-0.9840	1249.87	5.00	-0.3406	1185.79	5.00	-0.9944	1185.79
7.50	-0.9421	1281.91	7.50	-0.9431	1281.91	6.25	-0.3832	1217.83	6.25	-1.0237	1217.83
8.75	-0.9042	1313.95	8.75	-0.9052	1313.95	7.50	-0.3007	1249.87	7.50	-1.0530	1249.87
10.00	-0.9174	1345.99	10.00	-0.9184	1345.99	8.75	-0.4487	1281.91	8.75	-1.0823	1281.91
12.50	-0.9494	1378.03	12.50	-0.9504	1378.03	10.00	-0.4794	1313.95	10.00	-1.1116	1313.95
15.00	-0.9485	1410.07	15.00	-0.9495	1410.07	12.50	-0.4306	1345.99	12.50	-1.1409	1345.99
17.50	-0.9022	1442.11	17.50	-0.9032	1442.11	15.00	-0.5441	1378.03	15.00	-1.1702	1378.03
20.00	-0.9307	1474.15	20.00	-0.9317	1474.15	17.50	-0.5400	1410.07	17.50	-1.1995	1410.07
30.00	-0.8297	1506.19	30.00	-0.8307	1506.19	20.00	-0.5178	1442.11	20.00	-1.2288	1442.11
40.00	-0.7835	1538.23	40.00	-0.7845	1538.23	30.00	-0.4537	1474.15	30.00	-1.2581	1474.15
50.00	-0.7388	1570.27	50.00	-0.7398	1570.27	40.00	-0.3988	1506.19	40.00	-1.2874	1506.19
60.00	-0.6989	1602.31	60.00	-0.7000	1602.31	50.00	-0.4504	1538.23	50.00	-1.3167	1538.23
70.00	-0.3807	1634.35	70.00	-0.3817	1634.35	60.00	-0.4571	1570.27	60.00	-1.3460	1570.27
80.00	-0.2901	1666.39	80.00	-0.2911	1666.39	70.00	-0.4945	1602.31	70.00	-1.3753	1602.31
90.00	-0.2799	1698.43	90.00	-0.2809	1698.43	80.00	-0.4282	1634.35	80.00	-1.4046	1634.35
100.00	-0.2179	1730.47	100.00	-0.2189	1730.47	90.00	-0.3650	1666.39	90.00	-1.4339	1666.39
110.00	-0.1418	1762.51	110.00	-0.1428	1762.51	100.00	-0.2138	1698.43	100.00	-1.4632	1698.43
241.85	-0.0375	1794.55	241.85	-0.0385	1794.55	110.00	-0.1514	1730.47	110.00	-1.4925	1730.47
279.84	-0.0286	1826.59	279.84	-0.0296	1826.59	241.85	-0.0229	1762.51	241.85	-1.5218	1762.51
						279.84	-0.0109	1794.55	279.84	-1.5511	1794.55

mfr = 0.82 and $\alpha = 0^\circ$

mfr = 0.74 and $\alpha = 0^\circ$

mfr = 0.67 and $\alpha = 3.1^\circ$

TABLE VI. Continued

(i) Concluded

mfr = 0.80 and $\alpha = 1.0^\circ$				mfr = 0.84 and $\alpha = 2.0^\circ$				mfr = 0.81 and $\alpha = 3.0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.1703	343.16	0.0209	-187.47	0.1085	343.16	0.0145	-187.47	0.2196	343.16	0.0778
-171.29	0.0991	384.14	0.0279	-106.57	-0.2080	384.14	0.0259	-171.29	0.1286	384.14	0.0375
-155.11	0.0132	419.13	0.0406	-25.67	-0.7066	419.13	0.0399	-155.11	0.0784	419.13	0.0455
-130.84	-0.0953	457.12	0.0614	-10.27	-0.0221	457.12	0.0510	-130.84	-0.0463	457.12	0.0630
-106.57	-0.1962	507.77	0.1012	-2.05	0.8232	507.77	0.0931	-106.57	-0.1813	507.77	0.1055
-90.39	-0.2601	545.76	0.1510	0.00	1.0630	545.76	0.1410	-90.39	-0.2566	545.76	0.1510
-74.21	-0.3152	571.08	0.2022	0.31	0.5201	571.08	0.1955	-74.21	-0.3015	571.08	0.2060
-58.03	-0.4197	583.74	0.2370	0.63	0.2287	583.74	0.2353	-58.03	-0.3899	583.74	0.2394
-41.85	-0.4777	596.41	0.2765	1.25	0.0174	596.41	0.2791	-41.85	-0.3303	596.41	0.2786
-33.76	-0.7907	609.07	0.3393	1.88	-0.0277	609.07	0.3393	-33.76	-0.7088	609.07	0.3265
-25.67	-0.6451			2.50	-0.0410			-25.67	-0.5600		
-23.11	-0.5688			3.13	-0.0366			-23.11	-0.5018		
-17.97	-0.3525			3.75	-0.0288			-17.97	-0.2704		
-10.27	0.0668			4.37	-0.0249			-10.27	0.1632		
-5.13	0.4816			5.00	-0.0606			-5.13	0.5853		
-3.34	0.7101			6.25	-0.0660			-3.34	0.8083		
-2.05	0.9190			7.50	-0.1410			-2.05	0.9987		
-0.90	1.1335			8.75	-0.1900			-0.90	1.1588		
-0.44	1.1846			10.00	-0.2054			-0.44	1.1856		
0.00	0.9658			12.50	-0.2991			0.00	0.8479		
0.31	0.2473			15.00	-0.3065			0.31	0.0269		
0.63	-0.1101			17.50	-0.2776			0.63	-0.4691		
1.25	-0.2354			20.00	-0.2991			1.25	-0.5619		
1.88	-0.2469			30.00	-0.2954			1.88	-0.5612		
2.50	-0.2423			50.00	-0.3751			2.50	-0.4451		
3.13	-0.3116			60.00	-0.4014			3.13	-0.4929		
3.75	-0.2202			70.00	-0.4077			3.75	-0.4850		
4.37	-0.2526			80.00	-0.3984			4.37	-0.5074		
5.00	-0.2878			90.00	-0.3347			5.00	-0.4688		
6.25	-0.2839			100.00	-0.2143			6.25	-0.5167		
7.50	-0.2585			110.00	-0.1380			7.50	-0.3810		
8.75	-0.3976			241.85	-0.0184			8.75	-0.4903		
10.00	-0.3762							10.00	-0.5581		
12.50	-0.4032							12.50	-0.5837		
15.00	-0.5188							15.00	-0.6530		
17.50	-0.5193							17.50	-0.6517		
20.00	-0.4491							20.00	-0.6472		
30.00	-0.3907							30.00	-0.6302		
40.00	-0.4288							40.00	-0.6418		
50.00	-0.4675							50.00	-0.4827		
60.00	-0.4381							60.00	-0.3795		
70.00	-0.4788							70.00	-0.4536		
80.00	-0.4099							80.00	-0.4522		
90.00	-0.3469							90.00	-0.3417		
100.00	-0.2186							100.00	-0.2131		
110.00	-0.1510							110.00	-0.1440		
241.85	-0.0222							241.85	-0.0227		
279.84	-0.0133							279.84	-0.0138		

TABLE VI. Continued

(j) $M = 0.87$

		$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
$mfr = 0.27$ and $\alpha = 0^\circ$		-187.47	1.1646	343.16	-0.0196	-187.47	1.1657	343.16	-0.0092	-187.47	1.1203	343.16	-0.0124	-187.47	1.1186	343.16	-0.0020
		-171.29	1.1632	384.14	-0.0231	-171.29	1.1528	384.14	-0.0225	-171.29	1.1203	384.14	-0.0085	-106.57	1.0904	384.14	-0.0075
		-155.11	1.1636	419.13	-0.0247	-155.11	1.1722	419.13	-0.0196	-155.11	1.1184	419.13	-0.0004	-25.67	1.0032	419.13	0.0019
		-130.84	1.1595	457.12	-0.0199	-130.84	1.1855	457.12	-0.0228	-130.84	1.1095	457.12	0.0035	-10.27	1.1083	457.12	0.0100
		-106.57	1.1535	507.77	-0.0092	-106.57	1.1866	507.77	-0.0150	-106.57	1.1198	507.77	0.0077	-2.05	1.1733	507.77	0.0372
		-90.39	1.1443	545.76	0.0028	-90.39	1.1240	545.76	-0.0014	-90.39	1.0940	545.76	0.0082	0.00	1.1419	545.76	0.0354
		-74.21	1.1354	571.08	0.0277	-74.21	1.1122	571.08	0.0231	-74.21	1.0533	571.08	0.1275	0.31	-0.8799	571.08	0.1220
		-58.03	1.1259	583.74	0.0493	-58.03	1.1385	583.74	0.0480	-58.03	1.0318	583.74	0.1993	0.63	-1.2258	583.74	0.1625
		-41.85	1.1221	596.41	0.0755	-41.85	1.1502	596.41	0.0791	-41.85	1.0143	596.41	0.2059	1.25	-1.3489	596.41	0.2091
		-33.76	1.1204	609.07	0.1292	-33.76	1.1641	609.07	0.1347	-33.76	1.0007	609.07	0.2719	1.88	-1.3751	609.07	0.2790
		-25.67	1.1247			-25.67	1.1597			-25.67	1.0011			2.50	-1.3919		
		-23.11	1.1307			-23.11	1.1519			-23.11	1.0068			3.13	-1.3616		
		-17.97	1.1453			-17.97	1.1500			-17.97	1.0325			3.75	-1.3493		
		-10.27	1.1864			-10.27	1.1486			-10.27	1.1122			4.37	-1.3324		
		-5.13	1.1946			-5.13	1.1470			-5.13	1.1870			5.00	-1.3095		
		-3.34	1.1612			-3.34	1.1450			-3.34	1.2016			6.25	-1.2745		
		-2.05	1.0804			-2.05	1.1420			-2.05	1.1720			7.50	-1.2338		
		-0.90	0.8695			-0.90	1.1372			-0.90	1.1667			8.75	-1.2098		
		-0.44	0.6729			-0.44	1.1321			-0.44	1.1537			10.00	-1.1854		
		0.00	-0.2276			0.00	1.1284			0.00	1.1303			12.50	-1.1514		
		0.31	-1.0921			0.31	-1.3058			0.31	-1.1266			15.00	-1.1381		
		0.63	-1.3853			0.63	-1.4204			0.63	-1.2423			17.50	-1.1288		
		1.25	-1.5113			1.25	-1.2449			1.25	-1.1962			20.00	-1.0951		
		1.88	-1.5288			1.88	-1.2288			1.88	-1.1813			30.00	-0.9918		
		2.50	-1.5339			2.50	-1.2499			2.50	-1.1621			40.00	-0.8644		
		3.13	-1.5333			3.13	-1.2728			3.13	-1.1478			50.00	-0.8444		
		3.75	-1.5202			3.75	-1.2940			3.75	-1.1369			60.00	-0.8416		
		4.37	-1.5062			4.37	-1.3072			4.37	-1.1259			70.00	-0.8416		
		5.00	-1.4756			5.00	-1.3288			5.00	-1.1141			80.00	-0.8416		
		6.25	-1.4440			6.25	-1.4440			6.25	-1.1009			90.00	-0.8416		
		7.50	-1.4216			7.50	-1.4665			7.50	-1.0889			100.00	-0.8416		
		8.75	-1.4089			8.75	-1.4829			8.75	-1.0792			110.00	-0.8416		
		10.00	-1.3764			10.00	-1.5001			10.00	-1.0728			120.00	-0.8416		
		12.50	-1.3222			12.50	-1.5239			12.50	-1.0684			130.00	-0.8416		
		15.00	-1.3005			15.00	-1.5440			15.00	-1.0659			140.00	-0.8416		
		17.50	-1.2731			17.50	-1.5613			17.50	-1.0641			150.00	-0.8416		
		20.00	-1.2527			20.00	-1.5757			20.00	-1.0628			160.00	-0.8416		
		30.00	-1.1191			30.00	-1.6074			30.00	-1.0618			170.00	-0.8416		
		40.00	-1.0371			40.00	-1.6467			40.00	-1.0611			180.00	-0.8416		
		50.00	-0.9674			50.00	-1.6929			50.00	-1.0606			190.00	-0.8416		
		60.00	-0.9429			60.00	-1.7479			60.00	-1.0603			200.00	-0.8416		
		70.00	-0.9029			70.00	-1.8185			70.00	-1.0601			210.00	-0.8416		
		80.00	-0.8907			80.00	-1.8947			80.00	-1.0600			220.00	-0.8416		
		90.00	-0.8947			90.00	-1.9764			90.00	-1.0600			230.00	-0.8416		
		100.00	-0.8906			100.00	-2.0633			100.00	-1.0600			240.00	-0.8416		
		110.00	-0.7360			110.00	-2.1585			110.00	-1.0600			250.00	-0.8416		
		241.85	0.0116			241.85	-0.0131			241.85	-0.0131			250.00	-0.8416		
		279.84	-0.0130			279.84	-0.0243			279.84	-0.0243			279.84	-0.0192		

TABLE VI. Continued

(j) Continued

$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0706	343.16	-0.0048	-187.47	1.0706	343.16	-0.0068	-187.47	1.0404	343.16	-0.0011
-171.29	1.0715	384.14	0.0029	-106.57	1.0224	384.14	0.0046	-106.57	1.0436	384.14	0.0109
-155.11	1.0677	419.13	0.0143	-25.67	0.8438	419.13	0.0188	-155.11	1.0375	419.13	0.0265
-130.84	1.0521	457.12	0.0334	-10.27	0.9887	457.12	0.0289	-130.84	1.0172	457.12	0.0449
-106.57	1.0245	507.77	0.0720	-2.05	1.1995	507.77	0.0691	-106.57	0.9822	507.77	0.0877
-90.39	0.9949	545.76	0.1226	0.00	0.3469	545.76	0.1206	-90.39	0.9463	545.76	0.1451
-74.21	0.9619	571.08	0.1845	0.31	-0.6053	571.08	0.1842	-74.21	0.9065	571.08	0.2115
-58.03	0.9205	583.74	0.2267	0.63	-1.0076	583.74	0.2315	-58.03	0.8544	583.74	0.2537
-41.85	0.8776	596.41	0.2789	1.25	-1.1956	596.41	0.2844	-41.85	0.7957	596.41	0.3088
-33.76	0.8588	609.07	0.3467	1.88	-1.2260	609.07	0.3570	-33.76	0.7726	609.07	0.3781
-25.67	0.8424			2.50	-1.2146			-25.67	0.7429		
-23.11	0.8492			3.13	-1.2065			-23.11	0.7401		
-17.97	0.8724			3.75	-1.1701			-17.97	0.7740		
-10.27	0.9927			4.37	-1.1810			-10.27	0.8892		
-5.13	1.1206			5.00	-1.1389			-5.13	1.0710		
-3.34	1.1810			6.25	-1.0941			-3.34	1.1501		
-2.05	1.2005			7.50	-1.0620			-2.05	1.1952		
-0.90	1.1345			8.75	-1.0428			-0.90	1.1723		
-0.44	1.0034			10.00	-1.0046			-0.44	1.0710		
0.00	0.2941			12.50	-0.9640			0.00	0.4579		
0.31	-0.6717			15.00	-0.9985			0.31	-0.5258		
0.63	-1.0252			17.50	-0.9751			0.63	-0.9010		
1.25	-1.1955			20.00	-0.9791			1.25	-1.1124		
1.88	-1.2195			30.00	-0.8419			1.88	-1.1402		
2.50	-1.1993			50.00	-0.7942			2.50	-1.1243		
3.13	-1.1965			60.00	-0.7698			3.13	-1.0722		
3.75	-1.1719			70.00	-0.7608			3.75	-1.0696		
4.37	-1.1466			80.00	-0.7741			4.37	-1.0572		
5.00	-1.1463			90.00	-0.7529			5.00	-1.0233		
6.25	-1.0894			100.00	-0.3421			6.25	-0.9930		
7.50	-1.0578			110.00	-0.2103			7.50	-0.9546		
8.75	-1.0239			241.85	-0.0273			8.75	-0.9383		
10.00	-1.0418							10.00	-0.9051		
12.50	-0.9689							12.50	-0.9032		
15.00	-0.9855							15.00	-0.8973		
17.50	-0.9737							17.50	-0.8716		
20.00	-0.9589							20.00	-0.8591		
30.00	-0.8299							30.00	-0.7732		
40.00	-0.8229							40.00	-0.7370		
50.00	-0.7583							50.00	-0.6876		
60.00	-0.7529							60.00	-0.6924		
70.00	-0.7518							70.00	-0.6849		
80.00	-0.7630							80.00	-0.7149		
90.00	-0.7548							90.00	-0.6997		
100.00	-0.3633							100.00	-0.2577		
110.00	-0.1940							110.00	-0.1169		
241.85	-0.0292							241.85	-0.0342		
279.84	-0.0232							279.84	-0.0263		

TABLE VI. Continued

(j) Continued

mfr = 0.61 and $\alpha = 0^\circ$				mfr = 0.68 and $\alpha = 0^\circ$				mfr = 0.68 and $\alpha = 2.0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L
CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP
-187.47	0.9929	343.16	0.0091	-187.47	0.9911	343.16	0.0207	-187.47	0.9426	343.16	0.0351
-171.29	0.9935	384.14	0.0204	-106.57	0.9143	384.14	0.0227	-171.29	0.9429	384.14	0.0367
-155.11	0.9878	419.13	0.0340	-106.57	0.5673	419.13	0.0411	-155.11	0.9429	384.14	0.0367
-130.84	0.9618	457.12	0.0554	-102.27	0.7557	457.12	0.0567	-155.11	0.9352	419.13	0.0513
-106.57	0.9141	507.77	0.1044	-2.05	1.1731	507.77	0.1034	-106.57	0.9008	457.12	0.0750
-90.39	0.8658	545.76	0.1678	0.00	0.6280	545.76	0.1665	-106.57	0.8408	507.77	0.1220
-74.21	0.8148	571.08	0.2345	0.31	-0.1911	571.08	0.2374	-90.39	0.7798	545.76	0.1849
-58.03	0.7370	583.74	0.2818	0.63	-0.6948	583.74	0.2886	-74.21	0.7077	571.08	0.2527
-41.85	0.6518	596.41	0.3362	1.25	-0.9037	596.41	0.3449	-58.03	0.6124	583.74	0.2964
-33.76	0.6148	609.07	0.4082	1.88	-0.9765	609.07	0.4159	-41.85	0.5128	596.41	0.3470
-25.67	0.5601			2.50	-0.9664			-33.76	0.4649	609.07	0.4073
-23.11	0.5512			3.13	-0.9155			-25.67	0.4112		
-17.97	0.5951			3.75	-0.9087			-23.11	0.4062		
-10.27	0.7571			4.37	-0.9084			-17.97	0.4430		
-5.13	0.9658			5.00	-0.8001			-10.27	0.6602		
-3.34	1.0745			6.25	-0.8059			-5.13	0.9165		
-2.05	1.1624			7.50	-0.7484			-3.34	1.0524		
-0.90	1.1905			8.75	-0.7652			-2.05	1.1556		
-0.44	1.1294			10.00	-0.7082			-0.90	1.1946		
0.00	0.5801			12.50	-0.7281			-0.44	1.1533		
0.31	-0.3175			15.00	-0.7059			0.00	0.6235		
0.63	-0.7261			17.50	-0.7060			0.31	-0.2569		
1.25	-0.9563			20.00	-0.6716			0.63	-0.6873		
1.88	-0.9624			30.00	-0.6143			1.25	-0.9457		
2.50	-0.9592			50.00	-0.6082			1.88	-0.9499		
3.13	-0.8997			60.00	-0.6089			2.50	-0.8924		
3.75	-0.8806			70.00	-0.5935			3.13	-0.8922		
4.37	-0.8509			80.00	-0.6103			3.75	-0.8940		
5.00	-0.8295			90.00	-0.6039			4.37	-0.8972		
6.25	-0.7616			100.00	-0.2635			5.00	-0.8579		
7.50	-0.7386			110.00	-0.1272			6.25	-0.8272		
8.75	-0.7539			241.85	-0.0323			7.50	-0.7205		
10.00	-0.7003							8.75	-0.7806		
12.50	-0.7472							10.00	-0.7905		
15.00	-0.6875							12.50	-0.7668		
20.00	-0.7322							15.00	-0.7905		
30.00	-0.6035							17.50	-0.7665		
40.00	-0.6334							20.00	-0.7662		
50.00	-0.5991							30.00	-0.6656		
60.00	-0.6256							40.00	-0.6737		
70.00	-0.6261							50.00	-0.6678		
80.00	-0.6166							60.00	-0.6531		
90.00	-0.6240							70.00	-0.6603		
100.00	-0.2140							80.00	-0.6617		
110.00	-0.1075							90.00	-0.6499		
241.85	-0.0315							100.00	-0.1843		
279.84	-0.0233							110.00	-0.0949		
								241.85	-0.0263		
								279.84	-0.0218		

TABLE VI. Continued

(j) Concluded

$\phi = 0^\circ$				$\phi = 180^\circ$				$mfr = 0.74$ and $\alpha = 0^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.8827	343.16	0.0176	-187.47	0.8784	343.16	0.0312	-187.47	0.1376	343.16	0.0189	-187.47	0.1364	343.16	0.0267	-106.57	-0.1786	384.14	0.0309
-171.29	0.8817	384.14	0.0335	-106.57	0.7545	384.14	0.0341	-171.29	0.0677	384.14	0.0309	-106.57	-0.1786	384.14	0.0309	-155.11	-0.0011	419.13	0.0439
-155.11	0.8706	419.13	0.0487	-25.67	0.0475	419.13	0.0516	-155.11	-0.0011	419.13	0.0439	-25.67	-0.5982	419.13	0.0475	-130.84	0.8286	457.12	0.0640
-130.84	0.8286	457.12	0.0776	-10.27	0.3392	457.12	0.0724	-130.84	-0.0947	457.12	0.0656	-10.27	0.0623	457.12	0.0640	-106.57	0.7552	507.77	0.1085
-106.57	0.7552	507.77	0.1275	-2.05	1.0187	507.77	0.1266	-106.57	-0.1910	507.77	0.1062	-2.05	0.9043	507.77	0.1085	-90.39	0.6725	545.76	0.1571
-90.39	0.6725	545.76	0.1928	0.00	0.9150	545.76	0.1921	-90.39	-0.2437	545.76	0.1581	0.00	1.0201	545.76	0.1571	-74.21	0.5767	571.08	0.2142
-74.21	0.5767	571.08	0.2628	0.31	0.2086	571.08	0.2638	-74.21	-0.2780	571.08	0.2123	0.31	0.4342	571.08	0.2142	-58.03	0.4368	583.74	0.2536
-58.03	0.4368	583.74	0.3095	0.63	-0.1848	583.74	0.3164	-58.03	-0.3611	583.74	0.2477	0.63	0.9302	583.74	0.2536	-41.85	0.2666	596.41	0.2990
-41.85	0.2666	596.41	0.3647	1.25	-0.4474	596.41	0.3725	-41.85	-0.8392	596.41	0.2896	1.25	-0.1628	596.41	0.2990	-33.76	0.1706	609.07	0.3564
-33.76	0.1706	609.07	0.4273	1.88	-0.3909	609.07	0.4416	-33.76	-0.7639	609.07	0.3447	1.88	-0.0789	609.07	0.3564	-25.67	0.0360		
-25.67	0.0360			2.50	-0.3975			-25.67	-0.6263			2.50	-0.1549			-23.11	0.0213		
-23.11	0.0213			3.13	-0.3493			-23.11	-0.5487			3.13	-0.1007			-17.97	0.0818		
-17.97	0.0818			3.75	-0.2919			-17.97	-0.3421			3.75	-0.1128			-10.27	0.3342		
-10.27	0.3342			4.37	-0.3791			-10.27	0.0870			4.37	-0.1351			-5.13	0.6780		
-5.13	0.6780			5.00	-0.2578			-5.13	0.4660			5.00	-0.1523			-3.34	0.8545		
-3.34	0.8545			6.25	-0.2322			-3.34	0.7075			6.25	-0.1014			-2.05	1.0119		
-2.05	1.0119			7.50	-0.3081			-2.05	0.8935			7.50	-0.1911			-0.90	1.1772		
-0.90	1.1772			8.75	-0.3658			-0.90	1.1245			8.75	-0.2543			-0.44	1.1997		
-0.44	1.1997			10.00	-0.4144			-0.44	1.1883			10.00	-0.2511			0.00	0.9008		
0.00	0.9008			12.50	-0.4669			0.00	0.9932			12.50	-0.3037			0.31	1.1375		
0.31	1.1375			15.00	-0.4963			0.31	0.3268			15.00	-0.4258			0.63	-0.3081		
0.63	-0.3081			17.50	-0.5243			0.63	0.0543			17.50	-0.4265			1.25	-0.3561		
1.25	-0.3561			20.00	-0.5082			1.25	-0.1232			20.00	-0.4060			1.88	-0.3484		
1.88	-0.3484			30.00	-0.4927			1.88	-0.0829			30.00	-0.3306			2.50	-0.3315		
2.50	-0.3315			50.00	-0.4589			2.50	-0.0842			50.00	-0.4269			3.13	-0.3618		
3.13	-0.3618			60.00	-0.4521			3.13	-0.1660			60.00	-0.4434			4.37	-0.2768		
4.37	-0.2768			70.00	-0.4916			4.37	-0.1082			70.00	-0.4836			5.00	-0.3056		
5.00	-0.3056			80.00	-0.5247			5.00	-0.1149			80.00	-0.5084			6.25	-0.3084		
6.25	-0.3084			90.00	-0.5347			6.25	-0.2022			90.00	-0.5095			7.50	-0.2547		
7.50	-0.2547			100.00	-0.2333			7.50	-0.1852			100.00	-0.2069			8.75	-0.4050		
8.75	-0.4050			110.00	-0.1191			8.75	-0.2905			110.00	-0.1071			10.00	-0.4226		
10.00	-0.4226			12.50	-0.4741			10.00	-0.2962			12.50	-0.4741			15.00	-0.4775		
15.00	-0.4775			17.50	-0.4232			12.50	-0.3407			15.00	-0.4241			17.50	-0.5102		
17.50	-0.5102			20.00	-0.4677			17.50	-0.4232			20.00	-0.4151			30.00	-0.4658		
30.00	-0.4658			30.00	-0.3503			20.00	-0.4151			30.00	-0.3503			40.00	-0.4651		
40.00	-0.4651			40.00	-0.3806			30.00	-0.1082			40.00	-0.3806			50.00	-0.4283		
50.00	-0.4283			50.00	-0.4219			40.00	-0.3806			50.00	-0.4219			60.00	-0.4625		
60.00	-0.4625			60.00	-0.4402			50.00	-0.4219			60.00	-0.4402			70.00	-0.4927		
70.00	-0.4927			70.00	-0.4998			60.00	-0.4521			70.00	-0.4998			80.00	-0.5236		
80.00	-0.5236			80.00	-0.5189			70.00	-0.4916			80.00	-0.5189			90.00	-0.5390		
90.00	-0.5390			90.00	-0.5373			80.00	-0.5247			90.00	-0.5373			100.00	-0.2676		
100.00	-0.2676			100.00	-0.2161			90.00	-0.5347			100.00	-0.2161			110.00	-0.1191		
110.00	-0.1191			110.00	-0.1123			100.00	-0.2333			110.00	-0.1123			241.85	-0.0191		
241.85	-0.0191			241.85	-0.0201			110.00	-0.1191			241.85	-0.0201			279.84	-0.0060		
279.84	-0.0060			279.84	-0.0089			241.85	-0.1852			279.84	-0.0089						

TABLE VI. Continued

(k) $M = 0.89$

$\phi = 0^\circ$				$\phi = 0^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1775	343.16	0.0112	-187.47	1.1785	343.16	0.0206	-187.47	1.1656	343.16	0.0037	-187.47	1.1610	343.16	0.0157	-187.47	1.1339	343.16	0.0044
-171.29	1.1788	384.14	0.0005	-106.57	1.1657	384.14	0.0021	-171.29	1.1617	384.14	-0.0004	-106.57	1.1447	384.14	0.0012	-171.29	1.1345	384.14	0.0066
-155.11	1.1778	419.13	-0.0039	-25.67	1.1397	419.13	-0.0017	-155.11	1.1608	419.13	-0.0020	-25.67	1.0953	419.13	0.0040	-155.11	1.1370	419.13	0.0116
-130.84	1.1726	457.12	-0.0023	-10.27	1.2010	457.12	-0.0080	-130.84	1.1543	457.12	0.0046	-10.27	1.1774	457.12	0.0031	-130.84	1.1224	457.12	0.0251
-106.57	1.1674	507.77	0.0062	-2.05	1.0974	507.77	0.0040	-106.57	1.1426	507.77	0.0251	-2.05	1.1405	507.77	0.0239	-106.57	1.1064	507.77	0.0569
-90.39	1.1563	545.76	0.0228	0.00	-0.1067	545.76	0.0200	-90.39	1.1309	545.76	0.0535	0.00	0.0035	545.76	0.0516	-90.39	1.0879	545.76	0.0962
-74.21	1.1511	571.08	0.0514	0.31	-0.1047	571.08	0.0504	-74.21	1.1207	571.08	0.0932	0.31	-0.9582	571.08	0.0916	-74.21	1.0700	571.08	0.1481
-58.03	1.1415	583.74	0.0759	0.63	-1.3044	583.74	0.0781	-58.03	1.1065	583.74	0.1234	0.63	-1.2654	583.74	0.1266	-58.03	1.0463	583.74	0.1837
-41.85	1.1341	596.41	0.1076	1.25	-1.4126	596.41	0.1111	-41.85	1.0917	596.41	0.1615	1.25	-1.3692	596.41	0.1678	-41.85	1.0284	596.41	0.2306
-33.76	1.1317	609.07	0.1670	1.88	-1.4571	609.07	0.1723	-33.76	1.0929	609.07	0.2252	1.88	-1.4053	609.07	0.2321	-33.76	1.0213	609.07	0.2929
-25.67	1.1366			2.50	-1.4623			-25.67	1.0960			2.50	-1.4089			-25.67	1.0098		
-23.11	1.1442			3.13	-1.4593			-23.11	1.1019			3.13	-1.4032			-23.11	1.0188		
-17.97	1.1605			3.75	-1.4352			-17.97	1.1207			3.75	-1.3859			-17.97	1.0480		
-10.27	1.2017			4.37	-1.4103			-10.27	1.1739			4.37	-1.3602			-10.27	1.1241		
-5.13	1.2047			5.00	-1.3942			-5.13	1.2086			5.00	-1.3430			-5.13	1.1996		
-3.34	1.1759			6.25	-1.3700			-3.34	1.1962			6.25	-1.2998			-3.34	1.2134		
-2.05	1.1010			7.50	-1.3420			-2.05	1.1357			7.50	-1.2820			-2.05	1.1890		
-0.90	0.8909			8.75	-1.3207			-0.90	0.9599			8.75	-1.2551			-0.90	1.0594		
-0.44	0.6948			10.00	-1.2982			-0.44	0.7818			10.00	-1.2202			-0.44	0.8969		
0.00	-0.1933			12.50	-1.2589			0.00	-0.0594			12.50	-1.1878			0.00	0.8969		
0.31	-1.1090			15.00	-1.2182			0.31	-1.0359			15.00	-1.1766			0.31	-0.8661		
0.63	-1.3049			17.50	-1.1942			0.63	-1.2605			17.50	-1.1431			0.63	-1.1501		
1.25	-1.4248			20.00	-1.1872			1.25	-1.3674			20.00	-1.1166			1.25	-1.2623		
1.88	-1.4396			30.00	-1.0610			1.88	-1.3876			30.00	-1.0241			1.88	-1.2853		
2.50	-1.4461			50.00	-0.9232			2.50	-1.3873			50.00	-0.8964			2.50	-1.2785		
3.13	-1.4427			60.00	-0.8881			3.13	-1.3951			60.00	-0.8772			3.13	-1.2757		
3.75	-1.4319			70.00	-0.8758			3.75	-1.3926			70.00	-0.8545			3.75	-1.2558		
4.37	-1.4124			80.00	-0.8728			4.37	-1.3714			80.00	-0.8338			4.37	-1.2329		
5.00	-1.4006			90.00	-0.8599			5.00	-1.3378			90.00	-0.8444			5.00	-1.2326		
6.25	-1.3635			100.00	-0.8558			6.25	-1.3021			100.00	-0.8497			6.25	-1.1991		
7.50	-1.3427			110.00	-0.8154			7.50	-1.2816			110.00	-0.8074			7.50	-1.1492		
8.75	-1.3114			241.85	0.0632			8.75	-1.2580			241.85	0.0475			8.75	-1.1330		
10.00	-1.2965							10.00	-1.2363							10.00	-1.1250		
12.50	-1.2634							12.50	-1.1988							12.50	-1.0912		
15.00	-1.2365							15.00	-1.1699							15.00	-1.0660		
17.50	-1.2055							17.50	-1.1584							17.50	-1.0493		
20.00	-1.1796							20.00	-1.1295							20.00	-1.0391		
30.00	-1.0467							30.00	-1.0212							30.00	-0.9241		
40.00	-0.9748							40.00	-0.9427							40.00	-0.8686		
50.00	-0.9242							50.00	-0.8895							50.00	-0.8345		
60.00	-0.8798							60.00	-0.8612							60.00	-0.8130		
70.00	-0.8759							70.00	-0.8521							70.00	-0.8189		
80.00	-0.8598							80.00	-0.8456							80.00	-0.7956		
90.00	-0.8471							90.00	-0.8472							90.00	-0.8115		
100.00	-0.8526							100.00	-0.8467							100.00	-0.7916		
110.00	-0.8118							110.00	-0.8038							110.00	-0.7762		
241.85	0.0599							241.85	0.0410							241.85	0.0264		
279.84	0.0370							279.84	0.0184							279.84	0.0115		

TABLE VI. Continued
(k) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0855	343.16	0.0079	-187.47	1.0847	343.16	0.0198	-187.47	1.0878	343.16	0.0333	-187.47	1.0827	343.16	-0.0070
-171.29	1.0877	384.14	0.0142	-106.57	1.0378	384.14	0.0167	-171.29	1.0875	384.14	0.0276	-106.57	1.0372	384.14	0.0075
-155.11	1.0815	419.13	0.0245	-25.67	0.8642	419.13	0.0299	-155.11	1.0854	419.13	0.0339	-25.67	0.8274	419.13	0.0248
-130.84	1.0879	457.12	0.0450	-10.27	1.0006	457.12	0.0418	-130.84	1.0766	457.12	0.0521	-10.27	0.9588	457.12	0.0377
-96.57	1.0399	507.77	0.0872	-2.05	1.2107	507.77	0.0840	-96.57	1.0431	507.77	0.0917	-2.05	1.2127	507.77	0.0823
-74.21	0.9801	571.08	0.2029	0.31	-0.5467	571.08	0.2026	-74.21	0.9880	571.08	0.1954	0.31	-0.3565	571.08	0.2070
-58.03	0.9390	583.74	0.2460	0.63	-0.9206	583.74	0.2514	-58.03	0.9497	583.74	0.2319	0.63	-0.7713	583.74	0.2380
-41.85	0.9004	596.41	0.2961	1.25	-1.1263	596.41	0.3065	-41.85	0.9134	596.41	0.2737	1.25	-1.0004	596.41	0.3202
-25.67	0.8756	609.07	0.3691	1.88	-1.1424	609.07	0.3773	-25.67	0.8961	609.07	0.3290	1.88	-1.0477	609.07	0.3984
-23.11	0.8655			3.13	-1.1264			-23.11	0.8995			3.13	-1.0045		
-17.97	0.8961			3.75	-1.0899			-17.97	0.9342			3.75	-0.9757		
-10.27	1.0020			4.37	-1.0814			-10.27	1.0349			4.37	-0.9568		
-5.13	1.1439			5.00	-1.0540			-5.13	1.1614			5.00	-0.9082		
-3.34	1.1909			6.25	-1.0137			-3.34	1.2043			6.25	-0.8733		
-2.05	1.2113			7.50	-1.0032			-2.05	1.2065			7.50	-0.8469		
-0.90	1.1509			8.75	-0.9686			-0.90	1.1159			8.75	-0.8407		
-0.44	1.0346			10.00	-0.9478			-0.44	0.9700			10.00	-0.8101		
0.00	0.3473			12.50	-0.9014			0.00	0.2002			12.50	-0.7812		
0.31	-0.6184			15.00	-0.9241			0.31	-0.7480			15.00	-0.7937		
0.63	-0.9669			17.50	-0.9248			0.63	-1.0475			17.50	-0.8155		
1.25	-1.1304			20.00	-0.9133			1.25	-1.2076			20.00	-0.7450		
1.88	-1.1447			30.00	-0.7882			1.88	-1.2169			30.00	-0.6220		
2.50	-1.1242			50.00	-0.7415			2.50	-1.2138			50.00	-0.6208		
3.13	-1.1205			60.00	-0.7161			3.13	-1.2086			60.00	-0.5900		
3.75	-1.0957			70.00	-0.7171			3.75	-1.1996			70.00	-0.5904		
4.37	-1.0929			80.00	-0.7227			4.37	-1.1807			80.00	-0.6388		
5.00	-1.0700			90.00	-0.7283			5.00	-1.1729			90.00	-0.6346		
6.25	-1.0194			100.00	-0.7471			6.25	-1.1286			100.00	-0.6688		
7.50	-0.9993			110.00	-0.7014			7.50	-1.0999			110.00	-0.6224		
8.75	-0.9962			241.85	0.0034			8.75	-1.0772			110.00	-0.6224		
10.00	-0.9807							10.00	-1.0683			241.85	-0.0072		
12.50	-0.9372							12.50	-1.0525			12.50	-0.8591		
15.00	-0.9312							15.00	-1.0273			15.00	-0.8623		
17.50	-0.9341							17.50	-1.0460			17.50	-0.8294		
20.00	-0.9075							20.00	-1.0048			20.00	-0.8079		
30.00	-0.8094							30.00	-0.9462			30.00	-0.7362		
40.00	-0.7549							40.00	-0.8711			40.00	-0.6874		
50.00	-0.7353							50.00	-0.8378			50.00	-0.7003		
60.00	-0.7305							60.00	-0.8399			60.00	-0.6399		
70.00	-0.7203							70.00	-0.8351			70.00	-0.6694		
80.00	-0.7182							80.00	-0.8352			80.00	-0.6860		
90.00	-0.7189							90.00	-0.8270			90.00	-0.7003		
100.00	-0.7018							100.00	-0.8268			100.00	-0.6903		
110.00	-0.7034							110.00	-0.8336			110.00	-0.6694		
241.85	-0.0021							241.85	0.0375			241.85	-0.0039		
279.84	-0.0094							279.84	0.0088			279.84	-0.0064		

TABLE VI. Continued

(k) Continued

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0127	343.16	0.0205	-187.47	1.0089	343.16	0.0287	-187.47	0.9579	343.16	0.0250	-187.47	0.9554	343.16	0.0366
-171.29	1.0127	384.14	0.0325	-106.57	0.9337	384.14	0.0315	-171.29	0.9585	384.14	0.0375	-106.57	0.8579	384.14	0.0388
-155.11	1.0068	419.13	0.0466	-25.67	0.5789	419.13	0.0501	-155.11	0.9118	419.13	0.0545	-25.67	0.5590	419.13	0.0589
-130.84	0.9806	457.12	0.0749	-10.27	0.7783	457.12	0.0680	-130.84	0.9179	457.12	0.0806	-10.27	0.5770	457.12	0.0771
-106.57	0.9334	507.77	0.1239	-2.05	1.1807	507.77	0.1183	-106.57	0.8594	507.77	0.1349	-2.05	1.1246	507.77	0.1353
-90.39	0.8863	545.76	0.1836	0.00	0.6630	545.76	0.1836	-90.39	0.7953	545.76	0.1978	0.00	0.7944	545.76	0.2000
-74.21	0.8309	571.08	0.2531	0.31	-0.1438	571.08	0.2547	-74.21	0.7242	571.08	0.2700	0.31	0.0469	571.08	0.2745
-58.03	0.7585	583.74	0.2987	0.63	-0.6295	583.74	0.3053	-58.03	0.6235	583.74	0.3166	0.63	-0.4409	583.74	0.3245
-41.85	0.6790	596.41	0.3547	1.25	-0.8783	596.41	0.3644	-41.85	0.5036	596.41	0.3722	1.25	-0.6208	596.41	0.3820
-33.76	0.6376	609.07	0.4238	1.88	-0.9144	609.07	0.4329	-33.76	0.4484	609.07	0.4394	1.88	-0.7041	609.07	0.4514
-25.67	0.5751			2.50	-0.8999			-25.67	0.3531			2.50	-0.6612		
-23.11	0.5893			3.13	-0.8785			-23.11	0.3382			3.13	-0.6363		
-17.97	0.6115			3.75	-0.8167			-17.97	0.3954			3.75	-0.5460		
-10.27	0.7808			4.37	-0.8197			-10.27	0.5958			4.37	-0.5782		
-5.13	0.9909			5.00	-0.7725			-5.13	0.8502			5.00	-0.5450		
-3.34	1.1040			6.25	-0.7587			-3.34	0.9898			6.25	-0.3546		
-2.05	1.1764			7.50	-0.6921			-2.05	1.1186			7.50	-0.3508		
-0.90	1.2095			8.75	-0.6828			-0.90	1.2084			8.75	-0.4130		
-0.44	1.1611			10.00	-0.7022			-0.44	1.1968			10.00	-0.4190		
0.00	0.6217			12.50	-0.7116			0.00	0.7648			12.50	-0.4437		
0.31	-0.2427			15.00	-0.6886			0.31	-0.0269			15.00	-0.5126		
0.63	-0.6413			17.50	-0.6928			0.63	-0.4967			17.50	-0.5377		
1.25	-0.8622			20.00	-0.6789			1.25	-0.6333			20.00	-0.5290		
1.88	-0.8801			30.00	-0.5796			1.88	-0.6761			30.00	-0.5164		
2.50	-0.8708			50.00	-0.5981			2.50	-0.4871			50.00	-0.5638		
3.13	-0.8835			60.00	-0.5880			3.13	-0.5326			60.00	-0.5304		
3.75	-0.8278			70.00	-0.6130			3.75	-0.4211			70.00	-0.5724		
4.37	-0.7377			80.00	-0.6398			4.37	-0.4119			80.00	-0.6038		
5.00	-0.7779			90.00	-0.6555			5.00	-0.4843			90.00	-0.6145		
6.25	-0.7596			100.00	-0.6611			6.25	-0.4403			100.00	-0.6354		
7.50	-0.6311			110.00	-0.6040			7.50	-0.4366			110.00	-0.5387		
8.75	-0.6946			241.85	-0.0072			8.75	-0.4422			241.85	-0.0080		
10.00	-0.6206							10.00	-0.4744			10.00	-0.3798		
12.50	-0.6801							12.50	-0.4812			12.50	-0.4291		
15.00	-0.6770							15.00	-0.5142			15.00	-0.4263		
17.50	-0.6689							17.50	-0.5441			17.50	-0.4830		
20.00	-0.6527							20.00	-0.5401			20.00	-0.4760		
30.00	-0.5694							30.00	-0.5351			30.00	-0.4840		
40.00	-0.5946							40.00	-0.5412			40.00	-0.4597		
50.00	-0.5706							50.00	-0.5435			50.00	-0.4592		
60.00	-0.5895							60.00	-0.5361			60.00	-0.4819		
70.00	-0.5998							70.00	-0.5389			70.00	-0.4819		
80.00	-0.6385							80.00	-0.5945			80.00	-0.5274		
90.00	-0.6454							90.00	-0.6113			90.00	-0.5425		
100.00	-0.6716							100.00	-0.6308			100.00	-0.5642		
110.00	-0.5961							110.00	-0.5558			110.00	-0.3879		
241.85	-0.0111							241.85	-0.0087			241.85	-0.0052		
279.84	-0.1086							279.84	-0.0050			279.84	0.0007		

mfr = 0.74 and $\alpha = 0^\circ$

mfr = 0.88 and $\alpha = 0^\circ$

mfr = 0.81 and $\alpha = 0^\circ$

TABLE VI. Continued
(k) Concluded

$m\beta = 0.81$ and $\alpha = 0^\circ$

$\phi = 0^\circ$			$\phi = 180^\circ$				
Forebody	Afterbody		Forebody	Afterbody			
X/L	CP	X/L	CP	X/L	CP		
-187.47	0.1304	343.16	0.0235	-187.47	0.1395	343.16	0.0383
-171.29	0.0559	384.14	0.0383	-106.57	-0.1685	384.14	0.0395
-155.11	-0.0066	419.13	0.0321	-25.67	-0.5360	419.13	0.0590
-130.84	-0.0910	457.12	0.0791	-10.27	0.1312	457.12	0.0738
-106.57	-0.1724	507.77	0.1218	-2.05	0.9324	507.77	0.1215
-90.39	-0.2185	545.76	0.1733	0.00	1.0264	545.76	0.1729
-74.21	-0.2467	571.08	0.2294	0.31	0.4415	571.08	0.2310
-58.03	-0.3887	583.74	0.2662	0.63	0.0676	583.74	0.2725
-41.85	-0.7501	596.41	0.3067	1.25	-0.0892	596.41	0.3155
-33.76	-0.6838	609.07	0.3626	1.88	-0.0999	609.07	0.3739
-25.67	-0.5328			2.50	-0.1414		
-23.11	-0.5012			3.13	-0.1264		
-17.97	-0.2798			3.75	-0.0719		
-10.27	0.1218			4.37	-0.1068		
-5.13	0.5285			5.00	-0.1160		
-3.34	0.7156			6.25	-0.1279		
-2.05	0.9283			7.50	-0.1841		
-0.90	1.1111			8.75	-0.2544		
-0.44	1.1932			10.00	-0.2433		
0.00	1.0366			12.50	-0.2836		
0.31	0.3695			15.00	-0.3778		
0.63	0.0882			17.50	-0.4331		
1.25	-0.1065			20.00	-0.3955		
1.88	-0.0709			30.00	-0.3584		
2.50	-0.0858			50.00	-0.3966		
3.13	-0.0690			60.00	-0.4320		
3.75	-0.0972			70.00	-0.4737		
4.37	-0.1300			80.00	-0.5193		
5.00	-0.1547			90.00	-0.5440		
6.25	-0.1510			100.00	-0.5777		
7.50	-0.1260			110.00	-0.4658		
8.75	-0.3045			241.85	-0.0176		
10.00	-0.2823						
12.50	-0.2946						
15.00	-0.4060						
17.50	-0.4218						
20.00	-0.4067						
30.00	-0.4239						
40.00	-0.3871						
50.00	-0.4143						
60.00	-0.4491						
70.00	-0.4817						
80.00	-0.5355						
90.00	-0.5492						
100.00	-0.5822						
110.00	-0.5037						
241.85	-0.0213						
279.84	-0.0115						

TABLE VI. Continued

(I) $M = 0.92$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.1912	343.16	0.0631	-187.47	1.1928	343.16	0.0726	-187.47	1.1752	343.16	0.0669	-187.47	1.1450	343.16	0.0439
-171.29	1.1917	384.14	0.0450	-171.29	1.1796	384.14	0.0472	-171.29	1.1767	384.14	0.0446	-171.29	1.1447	384.14	0.0375
-155.11	1.1891	419.13	0.0322	-155.11	1.1664	419.13	0.0352	-155.11	1.1764	419.13	0.0391	-155.11	1.1429	419.13	0.0372
-130.84	1.1867	457.12	0.0285	-130.84	1.1701	457.12	0.0252	-130.84	1.1701	457.12	0.0342	-130.84	1.1429	419.13	0.0372
-106.57	1.1783	507.77	0.0340	-106.57	1.1596	507.77	0.0319	-106.57	1.1596	507.77	0.0510	-106.57	1.1154	507.77	0.0791
-90.39	1.1705	545.76	0.0533	0.00	-0.0385	545.76	0.0502	-90.39	1.1485	545.76	0.0847	-90.39	1.0968	545.76	0.1256
-74.21	1.1627	571.08	0.0854	0.31	-0.9420	571.08	0.0823	-74.21	1.1368	571.08	0.1259	-74.21	1.0776	571.08	0.1810
-58.03	1.1531	583.74	0.1099	0.63	-1.2264	583.74	0.1126	-58.03	1.1248	583.74	0.1630	-58.03	1.0533	583.74	0.2205
-41.85	1.1486	596.41	0.1432	1.25	-1.3318	596.41	0.1466	-41.85	1.1122	596.41	0.2007	-41.85	1.0320	596.41	0.2673
-33.76	1.1486	609.07	0.2035	1.88	-1.3688	609.07	0.2039	-33.76	1.1080	609.07	0.2664	-33.76	1.0229	609.07	0.3343
-25.67	1.1543			2.50	-1.3917			-25.67	1.1141			-25.67	1.0181		
-23.11	1.1574			3.13	-1.3819			-23.11	1.1178			-23.11	1.0252		
-17.97	1.1749			3.75	-1.3589			3.75	-1.2979			3.75	-1.1889		
-10.27	1.2194			4.37	-1.3331			4.37	-1.2805			4.37	-1.1553		
-5.13	1.2194			5.00	-1.3226			5.00	-1.2617			5.00	-1.1273		
-3.34	1.1900			6.25	-1.2801			6.25	-1.2143			6.25	-1.0994		
-2.05	1.0869			7.50	-1.2739			7.50	-1.1544			7.50	-1.0750		
-0.90	0.9124			8.75	-1.2487			8.75	-1.0904			8.75	-1.0581		
-0.44	0.7072			10.00	-1.2241			10.00	-1.0431			10.00	-1.0449		
0.00	-0.1639			12.50	-1.1652			12.50	-1.0045			12.50	-1.0386		
0.31	-1.0369			15.00	-1.1533			15.00	-0.9492			15.00	-1.0110		
0.63	-1.2347			17.50	-1.1353			17.50	-0.9176			17.50	-0.9734		
1.25	-1.3490			20.00	-1.0991			20.00	-0.8858			20.00	-0.9522		
1.88	-1.3599			30.00	-0.9901			30.00	-0.8649			30.00	-0.9446		
2.50	-1.3737			50.00	-0.8488			50.00	-0.8314			50.00	-0.9198		
3.13	-1.3635			60.00	-0.8390			60.00	-0.8242			60.00	-0.9116		
3.75	-1.3583			70.00	-0.8170			70.00	-0.8019			70.00	-0.9009		
4.37	-1.3406			80.00	-0.8207			80.00	-0.8019			80.00	-0.8916		
5.00	-1.3216			90.00	-0.8051			90.00	-0.7958			90.00	-0.8858		
6.25	-1.2932			100.00	-0.8156			100.00	-0.7972			100.00	-0.8816		
7.50	-1.2650			110.00	-0.7736			110.00	-0.7972			110.00	-0.8729		
8.75	-1.2458			241.85	0.0374			241.85	0.0642			241.85	0.0761		
10.00	-1.2335														
12.50	-1.1853														
15.00	-1.1685														
17.50	-1.1349														
20.00	-1.1176														
30.00	-1.0107														
40.00	-0.9190														
50.00	-0.8766														
60.00	-0.8250														
70.00	-0.8163														
80.00	-0.8200														
90.00	-0.8076														
100.00	-0.8052														
110.00	-0.7684														
241.85	0.0410														
279.84	0.0752														

mfr = 0.40 and $\alpha = 0^\circ$

mfr = 0.33 and $\alpha = 0^\circ$

mfr = 0.27 and $\alpha = 0^\circ$

TABLE VI. Continued

(I) Continued

		$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$					
		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody			
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP		
mfr = 0.49 and $\alpha = 0^\circ$		-187.47	1.1000	343.16	0.0341	-187.47	1.0973	343.16	0.0408	-187.47	1.1034	1.0073	343.16	0.0309	-187.47	1.026	0.0632	343.16	0.0145
		-171.29	1.0997	384.14	0.0359	-171.29	1.1040	384.14	0.0444	-155.11	1.0998	419.13	0.0463	-155.11	1.005	0.0534	419.13	0.0261	0.0417
		-155.11	1.0970	419.13	0.0439	-155.11	1.0998	419.13	0.0463	-130.84	1.0845	457.12	0.0583	-130.84	1.0870	0.0708	457.12	0.0561	0.0561
		-130.84	1.0823	457.12	0.0635	-130.84	1.0845	457.12	0.0679	-106.57	1.0687	507.77	0.1095	-106.57	1.0605	0.1100	507.77	0.1002	0.1002
		-106.57	1.0555	507.77	0.1045	-106.57	1.0687	507.77	0.1027	-90.39	1.0296	545.76	0.1585	-90.39	1.0323	0.1639	545.76	0.1581	0.1581
		-90.39	1.0261	545.76	0.1609	-90.39	1.0296	545.76	0.1643	-74.21	0.9906	571.08	0.2258	-74.21	1.0026	0.2215	571.08	0.2291	0.2291
		-74.21	0.9957	571.08	0.2262	-74.21	1.0029	571.08	0.2273	-58.03	0.9606	583.74	0.2674	-58.03	0.9659	0.2622	583.74	0.2633	0.2633
		-58.03	0.9442	583.74	0.2200	-58.03	0.9606	583.74	0.2674	-41.85	0.9258	596.41	0.3155	-41.85	0.9338	0.3063	596.41	0.3439	0.3439
		-41.85	0.9133	596.41	0.3237	-41.85	0.9258	596.41	0.3155	-33.76	0.9126	609.07	0.3819	-33.76	0.9240	0.3657	609.07	0.4231	0.4231
		-33.76	0.8981	609.07	0.3911	-33.76	0.9126	609.07	0.4043	-25.67	0.8953	2.50	-1.0389	-25.67	0.9105	2.50	-0.9974	2.50	-0.9974
		-25.67	0.8791			-25.67	0.8953			2.50	-1.0389			2.50	-0.9974			2.50	-0.9974
		2.50	-1.0945			2.50	-1.0389			3.13	-1.0885			3.13	-0.9498			3.13	-0.9498
		3.13	-1.0533			3.13	-1.0885			3.75	-0.9758			3.75	-0.9082			3.75	-0.9082
		3.75	-1.0236			3.75	-0.9758			4.37	-0.9507			4.37	-0.8853			4.37	-0.8853
		4.37	-1.0098			4.37	-0.9507			5.00	-0.9277			5.00	-0.8774			5.00	-0.8774
		5.00	-1.0039			5.00	-0.9277			6.25	-0.8735			6.25	-0.8343			6.25	-0.8343
		6.25	-0.9457			6.25	-0.9277			7.50	-0.8626			7.50	-0.8212			7.50	-0.8212
		7.50	-0.9262			7.50	-0.8626			8.75	-0.8626			8.75	-0.8354			8.75	-0.8354
		8.75	-0.9025			8.75	-0.8626			10.00	-0.8250			10.00	-0.7919			10.00	-0.7919
		10.00	-0.8814			10.00	-0.8250			12.50	-0.7749			12.50	-0.7055			12.50	-0.7055
		12.50	-0.8433			12.50	-0.7749			15.00	-0.7949			15.00	-0.7261			15.00	-0.7261
		15.00	-0.8770			15.00	-0.7949			17.50	-0.7891			17.50	-0.7516			17.50	-0.7516
		17.50	-0.8627			17.50	-0.7891			20.00	-0.7644			20.00	-0.7167			20.00	-0.7167
		20.00	-0.8603			20.00	-0.7644			25.00	-0.7644			25.00	-0.6685			25.00	-0.6685
		25.00	-0.7018			25.00	-0.7644			30.00	-0.6160			30.00	-0.5816			30.00	-0.5816
		30.00	-0.7018			30.00	-0.6160			40.00	-0.6309			40.00	-0.5541			40.00	-0.5541
		40.00	-0.6689			40.00	-0.6309			50.00	-0.6322			50.00	-0.5358			50.00	-0.5358
		50.00	-0.7001			50.00	-0.6322			60.00	-0.6543			60.00	-0.6013			60.00	-0.6013
		60.00	-0.7001			60.00	-0.6543			80.00	-0.6560			80.00	-0.6251			80.00	-0.6251
		80.00	-0.6930			80.00	-0.6560			100.00	-0.6830			100.00	-0.6410			100.00	-0.6410
		100.00	-0.7089			100.00	-0.6830			110.00	-0.6438			110.00	-0.6146			110.00	-0.6146
		110.00	-0.7100			110.00	-0.6438			241.85	0.0526			241.85	0.0443			241.85	0.0443
		110.00	-0.6781			110.00	-0.6438			279.84	0.0526			279.84	0.0581			279.84	0.0581
		241.85	0.0756			241.85	0.0526												
		279.84	0.0379			279.84	0.0526												

TABLE VI. Continued

(I) Continued

$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	1.0108	343.16	0.0777	-187.47	1.0729	343.16	0.0327	-187.47	1.0286	343.16	0.0371
-171.29	1.1009	384.14	0.0587	-171.29	1.0750	384.14	0.0388	-171.29	1.0286	384.14	0.0457
-155.11	1.0988	419.13	0.0599	-155.11	1.0696	419.13	0.0498	-155.11	1.0241	419.13	0.0628
-130.84	1.0844	457.12	0.0734	-130.84	1.0498	457.12	0.0737	-130.84	0.9974	457.12	0.0876
-106.57	1.0892	507.77	0.1135	-106.57	1.0159	507.77	0.1209	-106.57	0.9523	507.77	0.1393
-90.39	1.0322	545.76	0.1644	-90.39	0.9804	545.76	0.1806	-90.39	0.9025	545.76	0.2020
-74.21	1.0049	571.08	0.2183	-74.21	0.9416	571.08	0.2488	-74.21	0.8489	571.08	0.2742
-58.03	0.9715	583.74	0.2519	-58.03	0.8909	583.74	0.2960	-58.03	0.7775	583.74	0.3213
-41.85	0.9421	596.41	0.2918	-41.85	0.8372	596.41	0.3496	-41.85	0.7029	596.41	0.3769
-33.76	0.9327	609.07	0.3482	-33.76	0.8065	609.07	0.4206	-33.76	0.6565	609.07	0.4464
-25.67	0.9229			-25.67	0.7815			-25.67	0.6035		
-23.11	0.9357			-23.11	0.7757			-23.11	0.6038		
-17.97	0.9695			-17.97	0.8126			-17.97	0.6386		
-10.27	1.0716			-10.27	0.9420			-10.27	0.7948		
-5.13	1.1892			-5.13	1.1017			-5.13	1.0010		
-3.34	1.2225			-3.34	1.1790			-3.34	1.1040		
-2.05	1.2154			-2.05	1.2198			-2.05	1.1823		
-0.90	1.1080			-0.90	1.2013			-0.90	1.2145		
-0.44	0.9711			-0.44	1.1074			-0.44	1.1639		
0.00	0.2264			0.00	0.4846			0.00	0.6492		
0.31	-0.7336			0.31	-0.3933			0.31	-0.2052		
0.63	-1.0306			0.63	-0.6254			0.63	-0.3866		
1.25	-1.1791			1.25	-0.9730			1.25	-0.7955		
1.88	-1.1852			1.88	-0.9914			1.88	-0.8133		
2.50	-1.1855			2.50	-0.9652			2.50	-0.8012		
3.13	-1.1960			3.13	-0.9477			3.13	-0.7922		
3.75	-1.1764			3.75	-0.9281			3.75	-0.7612		
4.37	-1.1601			4.37	-0.9124			4.37	-0.7102		
5.00	-1.1414			5.00	-0.8740			5.00	-0.6828		
6.25	-1.1260			6.25	-0.8668			6.25	-0.6484		
7.50	-1.0853			7.50	-0.8318			7.50	-0.6484		
8.75	-1.0735			8.75	-0.8028			8.75	-0.6575		
10.00	-1.0590			10.00	-0.7871			10.00	-0.6478		
12.50	-1.0533			12.50	-0.7659			12.50	-0.6339		
15.00	-1.0254			15.00	-0.7618			15.00	-0.6512		
17.50	-1.0240			17.50	-0.7618			17.50	-0.6547		
20.00	-1.0007			20.00	-0.7680			20.00	-0.6000		
30.00	-0.9344			30.00	-0.6701			30.00	-0.5640		
40.00	-0.8573			40.00	-0.6548			40.00	-0.5607		
50.00	-0.8495			50.00	-0.6326			50.00	-0.5653		
60.00	-0.8237			60.00	-0.6209			60.00	-0.5858		
70.00	-0.8346			70.00	-0.6541			70.00	-0.5769		
80.00	-0.8248			80.00	-0.6698			80.00	-0.6190		
90.00	-0.8205			90.00	-0.6707			90.00	-0.6306		
100.00	-0.8311			100.00	-0.6895			100.00	-0.6554		
110.00	-0.7967			110.00	-0.6526			110.00	-0.6125		
241.85	0.0967			241.85	0.0451			241.85	0.0244		
279.84	0.0706			279.84	0.0263			279.84	0.0166		

mfr = 0.61 and $\alpha = 0^\circ$

mfr = 0.54 and $\alpha = 0^\circ$

mfr = 0.49 and $\alpha = 3.1^\circ$

TABLE VI. Continued
(I) Continued

mfr = 0.68 and $\alpha = 0^\circ$				mfr = 0.68 and $\alpha = 2.1^\circ$				mfr = 0.74 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L	Forebody X/L	Afterbody X/L
-187.47	0.9758	343.16	0.0397	-187.47	0.9750	343.16	0.0674	-187.47	0.9714	343.16	0.0237
-171.29	0.9764	384.14	0.0519	-171.29	0.9771	384.14	0.0646	-171.29	0.9197	384.14	0.0573
-155.11	0.9692	419.13	0.0694	-155.11	0.9699	419.13	0.0775	-155.11	0.9068	419.13	0.0753
-130.84	0.9368	457.12	0.0963	-130.84	0.9379	457.12	0.1031	-130.84	0.8660	457.12	0.1007
-106.57	0.8783	507.77	0.1517	-106.57	0.8783	507.77	0.1569	-106.57	0.7968	507.77	0.1631
-90.39	0.8150	545.76	0.2181	-90.39	0.8202	545.76	0.2276	-90.39	0.7146	545.76	0.2311
-74.21	0.7439	571.08	0.2912	-74.21	0.7523	571.08	0.2928	-74.21	0.6228	571.08	0.3042
-58.03	0.6616	583.74	0.3393	-58.03	0.6591	583.74	0.3372	-58.03	0.4884	583.74	0.3498
-41.85	0.5258	596.41	0.3941	-41.85	0.5576	596.41	0.3879	-41.85	0.3157	596.41	0.4051
-33.76	0.4395	609.07	0.4611	-33.76	0.5103	609.07	0.4487	-33.76	0.2233	609.07	0.4694
-25.67	0.3808			-25.67	0.4435			-25.67	0.0909		
-23.11	0.3778			-23.11	0.4422			-23.11	0.0594		
-17.97	0.4180			-17.97	0.4968			-17.97	0.0892		
-10.27	0.6064			-10.27	0.6819			-10.27	0.3823		
-5.13	0.8851			-5.13	0.9559			-5.13	0.7253		
-3.34	1.0105			-3.34	1.0801			-3.34	0.9004		
-2.05	1.1349			-2.05	1.1798			-2.05	1.0524		
-0.90	1.2238			-0.90	1.2286			-0.90	1.1987		
-0.44	1.2135			-0.44	1.1901			-0.44	1.2252		
0.00	0.8135			0.00	0.7055			0.00	0.9380		
0.31	0.0272			0.31	-0.1496			0.31	0.1879		
0.63	-0.4322			0.63	-0.5675			0.63	-0.0993		
1.25	-0.5700			1.25	-0.8065			1.25	-0.3143		
1.88	-0.5927			1.88	-0.7779			1.88	-0.2612		
2.50	-0.5435			2.50	-0.7752			2.50	-0.2081		
3.13	-0.5734			3.13	-0.7692			3.13	-0.2434		
3.75	-0.5321			3.75	-0.7611			3.75	-0.2319		
4.37	-0.3809			4.37	-0.7334			4.37	-0.2238		
5.00	-0.3845			5.00	-0.7307			5.00	-0.2202		
6.25	-0.4092			6.25	-0.6678			6.25	-0.2537		
7.50	-0.3664			7.50	-0.6088			7.50	-0.1955		
8.75	-0.4696			8.75	-0.6639			8.75	-0.3046		
10.00	-0.4539			10.00	-0.6440			10.00	-0.3441		
12.50	-0.4041			12.50	-0.6076			12.50	-0.3782		
15.00	-0.4603			15.00	-0.6654			15.00	-0.4325		
17.50	-0.4843			17.50	-0.6846			17.50	-0.4385		
20.00	-0.4922			20.00	-0.6690			20.00	-0.4449		
30.00	-0.4900			30.00	-0.5898			30.00	-0.4261		
40.00	-0.5035			40.00	-0.6115			40.00	-0.4421		
50.00	-0.5051			50.00	-0.5976			50.00	-0.4699		
60.00	-0.5124			60.00	-0.6079			60.00	-0.4647		
70.00	-0.5423			70.00	-0.6277			70.00	-0.5166		
80.00	-0.5728			80.00	-0.6414			80.00	-0.5340		
90.00	-0.5960			90.00	-0.6537			90.00	-0.5598		
100.00	-0.6194			100.00	-0.6750			100.00	-0.5849		
110.00	-0.5824			110.00	-0.6392			110.00	-0.5637		
241.85	0.0289			241.85	0.0432			241.85	0.0216		
279.84	0.0218			279.84	0.0266			279.84	0.0230		

TABLE VI. Concluded

(I) Concluded

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-187.47	0.1417	343.16	0.0422	-187.47	0.1319	343.16	0.0492	-187.47	0.1945	343.16	0.0649	-187.47	0.1025	343.16	0.0264
-171.29	0.0782	384.14	0.0541	-106.57	-0.1429	384.14	0.0520	-171.29	0.1239	384.14	0.0637	-106.57	-0.1482	384.14	0.0466
-155.11	0.0140	419.13	0.0676	-25.67	-0.4798	419.13	0.0703	-155.11	0.0355	419.13	0.0753	-25.67	-0.5565	419.13	0.0704
-130.84	-0.0807	457.12	0.0936	-10.27	0.1606	457.12	0.0884	-130.84	-0.0599	457.12	0.0998	-10.27	0.0622	457.12	0.0878
-106.57	-0.1435	507.77	0.1401	-2.05	0.9320	507.77	0.1380	-106.57	-0.1388	507.77	0.1480	-2.05	0.8633	507.77	0.1352
-90.39	-0.1935	545.76	0.1931	0.00	1.0518	545.76	0.1912	-90.39	-0.1825	545.76	0.2015	0.00	1.1286	545.76	0.1871
-74.21	-0.2171	571.08	0.2485	0.31	0.4409	571.08	0.2497	-74.21	-0.2252	571.08	0.2562	0.31	0.6327	571.08	0.2464
-58.03	-0.3585	583.74	0.2852	0.63	0.0932	583.74	0.2919	-58.03	-0.7368	583.74	0.2931	0.63	0.3544	583.74	0.2861
-41.85	-0.7097	596.41	0.3262	1.25	-0.0381	596.41	0.3363	-41.85	-0.6302	596.41	0.3325	1.25	0.1621	596.41	0.3319
-33.76	-0.6273	609.07	0.3816	1.88	-0.0865	609.07	0.3926	-33.76	-0.5413	609.07	0.3839	1.88	0.1151	609.07	0.3924
-25.67	-0.4906			2.50	-0.1283			-25.67	-0.4073			2.50	0.0944		
-23.11	-0.4252			3.13	-0.0698			-23.11	-0.3498			3.13	0.1001		
-17.97	-0.2256			3.75	-0.0927			-17.97	-0.1306			3.75	0.1038		
-10.27	0.1711			4.37	-0.0621			-10.27	0.2555			4.37	0.0863		
-5.13	0.5641			5.00	-0.0968			-5.13	0.6284			5.00	0.0507		
-3.34	0.7629			6.25	-0.0762			-3.34	0.8371			6.25	0.0747		
-2.05	0.9559			7.50	-0.1486			-2.05	1.0197			7.50	-0.0044		
-0.90	1.1570			8.75	-0.1738			-0.90	1.1884			8.75	-0.0598		
-0.44	1.2194			10.00	-0.2445			-0.44	1.2184			10.00	-0.0829		
0.00	1.0175			12.50	-0.2367			0.00	0.9456			12.50	-0.1631		
0.31	0.3700			15.00	-0.3394			0.31	0.2005			15.00	-0.2152		
0.63	0.0710			17.50	-0.3906			0.63	-0.2117			17.50	-0.2371		
1.25	-0.0759			20.00	-0.3655			1.25	-0.3267			20.00	-0.1834		
1.88	-0.0533			30.00	-0.3781			1.88	-0.3122			30.00	-0.2412		
2.50	-0.0412			50.00	-0.4082			2.50	-0.2728			50.00	-0.3146		
3.13	-0.1058			60.00	-0.4313			3.13	-0.2954			60.00	-0.3582		
3.75	-0.0687			70.00	-0.4645			3.75	-0.2936			70.00	-0.4036		
4.37	-0.0628			80.00	-0.5059			4.37	-0.2668			80.00	-0.4638		
5.00	-0.0922			90.00	-0.5282			5.00	-0.2782			90.00	-0.4875		
6.25	-0.1362			100.00	-0.5686			6.25	-0.2704			100.00	-0.5298		
7.50	-0.1079			110.00	-0.5289			7.50	-0.2171			110.00	-0.4905		
8.75	-0.2366			241.85	0.0168			8.75	-0.3038			241.85	0.0115		
10.00	-0.2916							10.00	-0.3472						
12.50	-0.2512							12.50	-0.4041						
15.00	-0.3474							15.00	-0.4779						
17.50	-0.3709							17.50	-0.4682						
20.00	-0.3594							20.00	-0.4981						
30.00	-0.3902							30.00	-0.4875						
40.00	-0.3792							40.00	-0.5175						
50.00	-0.4086							50.00	-0.5336						
60.00	-0.4220							60.00	-0.5238						
70.00	-0.4848							70.00	-0.5379						
80.00	-0.4983							80.00	-0.5849						
90.00	-0.5360							90.00	-0.6068						
100.00	-0.5645							100.00	-0.6194						
110.00	-0.5411							110.00	-0.5733						
241.85	0.0097							241.85	0.0182						
279.84	0.0111							279.84	0.0129						

TABLE VII. PRESSURE COEFFICIENTS ON MODEL WITH NACA 1-85-100 INLET AND A CONTRACTION RATIO OF 1.250

(a) $M = 0.79$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-94.32	0.9402	173.61	-0.0072	-94.32	0.9406	173.61	0.0042	-94.32	0.8914	173.61	-0.0205	-94.32	0.8918	190.28	0.0178
-82.25	0.9515	190.28	0.0025	-82.25	0.9544	206.94	0.0164	-82.25	0.9066	190.28	0.0013	-82.25	0.9058	206.94	0.0285
-75.15	0.9560	206.94	0.0135	-75.15	0.9725	223.61	0.0328	-75.15	0.9101	206.94	0.0149	-75.15	0.9121	206.94	0.0244
-68.05	0.9501	223.61	0.0339	-68.05	0.9843	245.83	0.0721	-68.05	0.9003	223.61	0.0396	-68.05	0.9013	223.61	0.0445
-57.40	0.9186	245.83	0.0724	-57.40	0.9900	262.50	0.1229	-57.40	0.8634	245.83	0.0792	-57.40	0.8662	245.83	0.0816
-46.76	0.8678	262.50	0.1239	-46.76	1.0147	273.61	0.1822	-46.76	0.8015	262.50	0.1335	-46.76	0.8034	262.50	0.1354
-39.66	0.8181	273.61	0.1807	-39.66	1.0497	279.17	0.2261	-39.66	0.7385	273.61	0.1949	-39.66	0.7431	273.61	0.1961
-32.56	0.7537	279.17	0.2179	-32.56	1.0893	284.72	0.2736	-32.56	0.6523	279.17	0.2385	-32.56	0.6618	279.17	0.2354
-25.46	0.6759	284.72	0.2646	-25.46	1.1758	290.28	0.3321	-25.46	0.5409	284.72	0.2936	-25.46	0.5504	284.72	0.2859
-18.36	0.5947	290.28	0.3239	-18.36	1.2648			-18.36	0.4136	290.28	0.3668	-18.36	0.4388	290.28	0.3477
-14.81	0.5592			-14.81	1.3587			-14.81	0.3415			-14.81	0.3804		
-11.26	0.4981			-11.26	1.5826			-11.26	0.2586			-11.26	0.3192		
-10.14	0.4894			-10.14	1.4195			-10.14	0.2263			-10.14	0.2861		
-7.88	0.5231			-7.88	1.3387			-7.88	0.2599			-7.88	0.3332		
-4.51	0.6740			-4.51	1.3220			-4.51	0.4482			-4.51	0.5459		
-2.25	0.9234			-2.25	1.2760			-2.25	0.7312			-2.25	0.8254		
-1.46	1.0433			-1.46	1.2688			-1.46	0.9144			-1.46	0.9694		
-0.90	1.1206			-0.90	1.1088			-0.90	1.0413			-0.90	1.0982		
-0.39	1.1475			-0.39	0.7502			-0.39	1.1622			-0.39	1.1664		
-0.19	1.0780			-0.19	0.4182			-0.19	1.1597			-0.19	1.1329		
0.00	0.4506			0.00	0.2058			0.00	0.6856			0.00	0.5784		
0.31	-1.6781			0.31	-0.1714			0.31	-1.4665			0.31	-1.5876		
0.62	-1.7052			0.62	-0.1580			0.62	-1.4429			0.62	-1.6186		
1.25	-1.6274			1.25	-0.1679			1.25	-1.3412			1.25	-1.5474		
1.88	-1.5669			30.00	-0.1691			1.88	-1.2099			1.88	-1.4403		
2.50	-1.5158			40.00	-0.1501			2.50	-1.0736			2.50	-1.3473		
3.12	-1.4419			50.00	-0.1410			3.12	-1.0732			3.12	-1.2701		
3.75	-1.3578			60.00	-0.1359			3.75	-0.9512			3.75	-1.2415		
4.38	-1.3278			70.00	-0.1241			4.38	-0.8302			4.38	-1.1996		
5.00	-1.2877			80.00	-0.1091			5.00	-0.7658			5.00	-1.1601		
6.25	-1.1804			90.00	-0.0922			6.25	-0.7225			6.25	-0.8708		
7.50	-0.9998			100.00	-0.0544			7.50	-0.7306			7.50	-0.4419		
8.75	-0.6517			129.17	-0.0545			8.75	-0.2358			8.75	-0.1935		
10.00	-0.4733							10.00	-0.2288			10.00	-0.1822		
12.50	-0.2318							12.50	-0.2369			12.50	-0.2298		
15.00	-0.1865							15.00	-0.2164			15.00	-0.2111		
20.00	-0.1934							17.50	-0.1894			17.50	-0.2041		
30.00	-0.1642							20.00	-0.1818			20.00	-0.1991		
40.00	-0.1756							30.00	-0.1413			30.00	-0.1629		
50.00	-0.1408							40.00	-0.1351			40.00	-0.1467		
60.00	-0.1353							50.00	-0.1150			50.00	-0.1345		
70.00	-0.1257							60.00	-0.1243			60.00	-0.1289		
80.00	-0.1152							70.00	-0.1084			70.00	-0.1167		
100.00	-0.0648							80.00	-0.1048			80.00	-0.1068		
129.17	-0.0374							100.00	-0.0481			100.00	-0.0605		
145.83	-0.0450							129.17	-0.0301			129.17	-0.0374		
								145.83	-0.0148			145.83	-0.0188		

TABLE VII. Continued

(a) Concluded

		mfr = 0.67 and $\alpha = 2.1^\circ$						mfr = 0.74 and $\alpha = 0^\circ$					
		$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$		
		Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP	Forebody X/L	Afterbody X/L	CP
-94.32	0.8922	173.61	190.28	0.0138	-94.32	0.8914	190.28	0.0035	-94.32	0.8220	173.61	190.28	0.0161
-82.25	0.9091	190.28	206.94	0.0170	-82.25	0.9096	206.94	0.0217	-82.25	0.8442	190.28	206.94	0.0332
-75.15	0.9126	206.94	0.0263	-46.76	-75.15	0.7992	223.61	0.0374	-75.15	0.8502	206.94	0.0304	0.0482
-68.05	0.9049	223.61	0.0460	-11.26	-68.05	0.9049	245.83	0.0799	-68.05	0.8351	223.61	0.0532	0.0932
-57.40	0.8681	245.83	0.0881	-4.51	-57.40	0.8369	262.50	0.1328	-57.40	0.7893	245.83	0.0954	0.1511
-46.76	0.8067	262.50	0.1410	-0.90	-46.76	0.7092	273.61	0.1960	-46.76	0.7092	262.50	0.1489	0.2153
-39.66	0.7483	273.61	0.1960	0.00	-39.66	0.6291	273.61	0.2439	-39.66	0.6291	273.61	0.2124	0.2599
-32.56	0.6684	279.17	0.2339	0.31	-32.56	0.5200	279.17	0.3018	-32.56	0.5200	279.17	0.2320	0.3124
-25.46	0.5686	284.72	0.2718	0.62	-25.46	0.4355	284.72	0.3687	-25.46	0.3730	284.72	0.3056	0.3784
-18.36	0.4653	290.28	0.3158	1.25	-18.36	0.3140	290.28	0.3765	-18.36	0.2056	290.28	0.3087	
-14.81	0.4180			1.88	-14.81	0.1232			-14.81	0.1182			
-11.26	0.3668			2.50	-11.26	0.1226			-11.26	0.0131			
-10.14	0.3742			3.12	-10.14	0.0968			-10.14	-0.0570			
-7.88	0.4247			3.75	-7.88	0.3582			-7.88	0.0344			
-4.51	0.6154			4.38	-4.51	0.2510			-4.51	0.2635			
-2.25	0.8917			5.00	-2.25	0.2430			-2.25	0.6480			
-1.46	1.0236			6.25	-1.46	0.2329			-1.46	0.8415			
-0.90	1.1312			7.50	-0.90	0.2264			-0.90	1.0224			
-0.39	1.1639			8.75	-0.39	0.2287			-0.39	1.1684			
-0.19	1.0986			10.00	-0.19	0.2228			-0.19	1.1633			
0.00	0.4439			12.50	0.00	0.2283			0.00	0.7578			
0.31	-1.6743			15.00	0.31	-0.2125			0.31	-1.4212			
0.62	-1.7162			17.50	0.62	-0.1860			0.62	-1.4071			
1.25	-1.6658			20.00	1.25	-0.1750			1.25	-1.2804			
1.88	-1.5669			30.00	1.88	-0.1375			1.88	-1.1661			
2.50	-1.5232			40.00	2.50	-0.1260			2.50	-1.1158			
3.12	-1.4559			50.00	3.12	-0.1209			3.12	-1.0254			
3.75	-1.3922			60.00	3.75	-0.1209			3.75	-0.9463			
4.38	-1.3447			70.00	4.38	-0.1083			4.38	-0.8590			
5.00	-1.3317			80.00	5.00	-0.0957			5.00	-0.7807			
6.25	-1.2496			90.00	6.25	-0.0878			6.25	-0.7240			
7.50	-1.1882			100.00	7.50	-0.0452			7.50	-0.2196			
8.75	-0.8979			125.00	8.75	-0.0452			8.75	-0.2459			
10.00	-0.5893			150.00	10.00	-0.2452			10.00	-0.2452			
12.50	-0.4119			175.00	12.50	-0.2593			12.50	-0.2593			
15.00	-0.2217			200.00	15.00	-0.2348			15.00	-0.2348			
17.50	-0.1416			300.00	17.50	-0.2122			17.50	-0.2122			
20.00	-0.1478			40.00	20.00	-0.1940			20.00	-0.1940			
30.00	-0.1658			50.00	30.00	-0.1465			30.00	-0.1465			
40.00	-0.1586			60.00	40.00	-0.1354			40.00	-0.1354			
50.00	-0.1409			70.00	50.00	-0.1237			50.00	-0.1237			
60.00	-0.1391			80.00	60.00	-0.1189			60.00	-0.1189			
70.00	-0.1189			100.00	70.00	-0.1118			70.00	-0.1129			
80.00	-0.1118			125.00	80.00	-0.0996			80.00	-0.0996			
100.00	-0.0565			150.00	100.00	-0.0499			100.00	-0.0499			
125.00	-0.0300			175.00	125.00	-0.0300			125.00	-0.0300			
145.83	-0.0205				145.83	-0.0172			145.83	-0.0172			

TABLE VII. Continued

(b) $M = 0.84$

$mfr = 0.49$ and $\alpha = -2.1^\circ$				$mfr = 0.49$ and $\alpha = -1.0^\circ$				$mfr = 0.49$ and $\alpha = 0^\circ$				$mfr = 0.49$ and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-94.32	1.0533	173.61	-0.0316	173.61	-0.0256	-94.32	1.0535	190.28	-0.0040	-94.32	1.0530	173.61	-0.0142	-94.32	1.0526
-82.25	1.0589	190.28	-0.0093	190.28	-0.0083	-82.25	1.0595	206.94	0.0077	-82.25	1.0596	190.28	-0.0026	-82.25	1.0614
-75.15	1.0616	206.94	0.0050	206.94	-0.0020	-75.15	1.0618	223.61	0.0180	-75.15	1.0618	206.94	0.0076	-46.76	1.0127
-68.05	1.0580	223.61	0.0227	223.61	0.0203	-68.05	1.0586	245.83	0.0569	-68.05	1.0579	223.61	0.0259	-11.26	0.8211
-57.40	1.0391	245.83	0.0613	245.83	0.0553	-57.40	1.0390	262.50	0.0959	-57.40	1.0401	245.83	0.0633	-4.51	0.9721
-46.76	1.0094	262.50	0.1065	262.50	0.0998	-46.76	1.0099	279.17	0.1471	-46.76	1.0089	262.50	0.1064	-0.90	1.1915
-39.66	0.9790	279.17	0.1631	279.17	0.1577	-39.66	0.9809	290.28	0.1847	-39.66	0.9813	279.17	0.1623	0.00	0.2688
-32.56	0.9435	290.28	0.2043	290.28	0.2000	-32.56	0.9467	284.72	0.2336	-32.56	0.9472	279.17	0.1995	0.31	-1.6302
-25.46	0.8945	284.72	0.2582	284.72	0.2492	-25.46	0.8994	284.72	0.2925	-25.46	0.9017	284.72	0.2452	0.62	-1.7129
-18.36	0.8469	290.28	0.3261	290.28	0.3124	-18.36	0.8533	290.28	0.2925	-18.36	0.8606	290.28	0.3075	1.25	-1.6331
-14.81	0.8292					-14.81	0.8280			-14.81	0.8460			1.88	-1.6260
-11.26	0.7951					-11.26	0.8041			-11.26	0.8204			2.50	-1.6104
-10.14	0.8002					-10.14	0.8034			-10.14	0.8270			3.12	-1.5498
-7.88	0.8233					-7.88	0.8471			-7.88	0.8492			3.75	-1.4468
-4.51	0.9312					-4.51	0.9549			-4.51	0.9623			4.38	-1.4346
-2.25	1.0860					-2.25	1.1059			-2.25	1.1146			5.00	-1.3503
-1.46	1.1561					-1.46	1.1679			-1.46	1.1668			6.25	-1.3068
-0.90	1.1862					-0.90	1.1914			-0.90	1.1837			7.50	-1.2641
-0.39	1.1515					-0.39	1.1375			-0.39	1.1169			8.75	-1.1924
-0.19	1.0414					-0.19	1.0231			-0.19	0.9888			10.00	-1.1496
0.00	0.3420					0.00	0.3184			0.00	0.2629			12.50	-1.0638
0.31	-1.5748					0.31	-1.6130			0.31	-1.6251			15.00	-0.9952
0.62	-1.6188					0.62	-1.6494			0.62	-1.6724			17.50	-0.9423
1.25	-1.5256					1.25	-1.5677			1.25	-1.6058			20.00	-0.8547
1.88	-1.5138					1.88	-1.5572			1.88	-1.5853			30.00	-0.1520
2.50	-1.4921					2.50	-1.5276			2.50	-1.5650			40.00	-0.0559
3.12	-1.4456					3.12	-1.5152			3.12	-1.5503			50.00	-0.0911
3.75	-1.3387					3.75	-1.4325			3.75	-1.4480			60.00	-0.1139
4.38	-1.2855					4.38	-1.3653			4.38	-1.4066			70.00	-0.1190
5.00	-1.2544					5.00	-1.3165			5.00	-1.3071			80.00	-0.1084
6.25	-1.1662					6.25	-1.2542			6.25	-1.2913			90.00	-0.0900
7.50	-1.1118					7.50	-1.1535			7.50	-1.1963			100.00	-0.0438
8.75	-1.0367					8.75	-1.1365			8.75	-1.1715			129.17	-0.0484
10.00	-1.0072					10.00	-1.0843			10.00	-1.1362				
12.50	-0.9095					12.50	-0.9905			12.50	-1.0579				
15.00	-0.8079					15.00	-0.9261			15.00	-0.9853				
17.50	-0.7596					17.50	-0.8712			17.50	-0.9374				
20.00	-0.7394					20.00	-0.8548			20.00	-0.8544				
30.00	-0.0785					30.00	-0.0641			30.00	-0.1837				
40.00	-0.1069					40.00	-0.0871			40.00	-0.0771				
50.00	-0.1208					50.00	-0.1019			50.00	-0.0851				
60.00	-0.1357					60.00	-0.1228			60.00	-0.1204				
70.00	-0.1296					70.00	-0.1286			70.00	-0.1201				
80.00	-0.1139					80.00	-0.1081			80.00	-0.1090				
100.00	-0.0591					100.00	-0.0547			100.00	-0.0590				
129.17	-0.0438					129.17	-0.0398			129.17	-0.0534				
145.83	-0.0342					145.83	-0.0336			145.83	-0.0457				

TABLE VII. Continued

(b) Continued

mfr = 0.49 and $\alpha = 1.0^\circ$				mfr = 0.49 and $\alpha = 2.0^\circ$				mfr = 0.49 and $\alpha = 3.1^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-94.32	1.0452	173.61	-0.0068	-94.32	1.0433	190.28	-0.0055	-94.32	1.0518	190.28	-0.0093
-82.25	1.0587	190.28	-0.0005	-82.25	1.0585	190.28	0.0047	-82.25	1.0574	190.28	0.0093
-75.15	1.0603	206.94	0.0038	-75.15	1.0621	206.94	0.0117	-75.15	1.0587	206.94	0.0163
-68.05	1.0574	223.61	0.0268	-68.05	1.0582	223.61	0.0306	-68.05	1.0581	223.61	0.0299
-57.40	1.0411	245.83	0.0626	-57.40	1.0400	245.83	0.0638	-57.40	1.0398	245.83	0.0572
-46.76	1.0108	262.50	0.1041	-46.76	1.0107	262.50	0.1059	-46.76	1.0121	262.50	0.0881
-39.66	0.9829	273.61	0.1559	-39.66	0.9866	273.61	0.1500	-39.66	0.9844	273.61	0.1200
-32.56	0.9487	279.17	0.1918	-32.56	0.9502	279.17	0.1829	-32.56	0.9521	279.17	0.1466
-25.46	0.9057	284.72	0.2347	-25.46	0.9099	284.72	0.2224	-25.46	0.9140	284.72	0.1719
-18.36	0.8579	290.28	0.2904	-18.36	0.8757	290.28	0.2754	-18.36	0.8820	290.28	0.2211
-14.81	0.8447			-14.81	0.8611			-14.81	0.8724		
-11.26	0.8275			-11.26	0.8578			-11.26	0.8713		
-10.14	0.8403			-10.14	0.8644			-10.14	0.8673		
-7.88	0.8952			-7.88	0.9047			-7.88	0.9059		
-4.51	0.9967			-4.51	1.0180			-4.51	1.0264		
-2.25	1.1262			-2.25	1.1440			-2.25	1.1368		
-1.46	1.1758			-1.46	1.1851			-1.46	1.1811		
-0.90	1.1843			-0.90	1.1884			-0.90	1.1760		
-0.39	1.1001			-0.39	1.0921			-0.39	1.1738		
-0.19	0.9829			-0.19	1.0700			-0.19	1.0741		
0.00	0.1955			0.00	0.1952			0.00	0.1979		
0.31	-1.6577			0.31	-1.6487			0.31	-1.6479		
0.62	-1.7012			0.62	-1.6853			0.62	-1.6823		
1.25	-1.6603			1.25	-1.6548			1.25	-1.6501		
1.88	-1.6371			1.88	-1.6267			1.88	-1.6262		
2.50	-1.6165			2.50	-1.6092			2.50	-1.6085		
3.12	-1.5799			3.12	-1.5687			3.12	-1.5683		
3.75	-1.5333			3.75	-1.5304			3.75	-1.5333		
4.38	-1.4846			4.38	-1.4554			4.38	-1.4554		
5.00	-1.4417			5.00	-1.4187			5.00	-1.4187		
6.25	-1.3782			6.25	-1.3490			6.25	-1.3490		
7.50	-1.3026			7.50	-1.3202			7.50	-1.3202		
8.75	-1.2526			8.75	-1.3026			8.75	-1.3026		
10.00	-1.2113			10.00	-1.2866			10.00	-1.2866		
12.50	-1.1233			12.50	-1.1780			12.50	-1.1780		
15.00	-1.0581			15.00	-1.1149			15.00	-1.1149		
20.00	-0.9380			20.00	-0.9952			20.00	-0.9952		
30.00	-0.7927			30.00	-0.9107			30.00	-0.9107		
40.00	-0.6513			40.00	-0.8200			40.00	-0.8200		
50.00	-0.5146			50.00	-0.7499			50.00	-0.7499		
60.00	-0.3846			60.00	-0.6817			60.00	-0.6817		
70.00	-0.2616			70.00	-0.6233			70.00	-0.6233		
80.00	-0.1491			80.00	-0.5747			80.00	-0.5747		
100.00	-0.0551			100.00	-0.5357			100.00	-0.5357		
129.17	-0.0451			129.17	-0.5087			129.17	-0.5087		
145.83	-0.0374			145.83	-0.4868			145.83	-0.4868		

TABLE VII. Continued

(b) Continued

mfr = 0.55 and $\alpha = 0^\circ$				mfr = 0.61 and $\alpha = 0^\circ$				mfr = 0.67 and $\alpha = -2.1^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
XL	CP	XL	CP	XL	CP	XL	CP	XL	CP	XL	CP
-94.32	1.0185	173.61	-0.0116	-94.32	1.0200	190.28	0.0040	-94.32	0.9205	173.61	-0.0127
-82.25	1.0284	190.28	0.0014	-82.25	1.0299	206.94	0.0214	-82.25	0.9356	190.28	0.0120
-75.15	1.0323	206.94	0.0154	-75.15	0.9670	223.61	0.0330	-75.15	0.9392	206.94	0.0311
-68.05	1.0271	223.61	0.0353	-11.26	0.7096	245.83	0.0727	-68.05	0.9304	223.61	0.0564
-57.40	1.0049	245.83	0.0773	-4.51	0.8879	262.50	0.1250	-57.40	0.8920	245.83	0.1005
-46.76	0.9653	262.50	0.1290	-0.90	1.1862	273.61	0.1850	-46.76	0.8305	262.50	0.1579
-39.66	0.9297	273.61	0.1853	0.00	1.3683	279.17	0.2270	-39.66	0.7687	273.61	0.2271
-32.56	0.8830	279.17	0.2230	0.31	1.5641	284.72	0.2747	-32.56	0.6885	279.17	0.2729
-25.46	0.8245	284.72	0.2706	0.62	1.6419	290.28	0.3386	-25.46	0.5795	284.72	0.3293
-18.36	0.7673	290.28	0.3303	1.25	1.5487			-18.36	0.4482	290.28	0.4027
-14.81	0.7405			1.88	1.3221			-14.81	0.3834		
-11.26	0.7048			2.50	1.4951			-11.26	0.3034		
-10.14	0.7059			3.12	1.4324			-10.14	0.2544		
-7.88	0.7372			3.75	1.3427			-7.88	0.2017		
-4.51	0.8800			4.38	1.3000			-4.51	0.4814		
-2.25	1.0610			5.00	1.2575			-2.25	0.7659		
-1.46	1.1393			6.25	1.1799			-1.46	0.9280		
-0.90	1.1821			7.50	1.1394			-0.90	1.0644		
-0.39	1.1551			8.75	1.0613			-0.39	1.1823		
-0.19	1.0498			10.00	1.0360			-0.19	1.1796		
0.00	0.9835			12.50	0.9460			0.00	0.7543		
0.31	1.5341			15.00	0.8792			0.31	1.2897		
0.62	1.5840			17.50	0.8234			0.62	1.2829		
1.25	1.4986			20.00	0.4669			1.25	1.2052		
1.88	1.4776			30.00	0.0764			1.88	1.1071		
2.50	1.4490			40.00	0.0919			2.50	1.0008		
3.12	1.4162			50.00	0.1193			3.12	0.9660		
3.75	1.3423			60.00	0.1322			3.75	0.9311		
4.38	1.2884			70.00	0.1289			4.38	0.8913		
5.00	1.2634			80.00	0.1115			5.00	0.8580		
6.25	1.1820			90.00	0.1012			6.25	0.5533		
7.50	1.0979			100.00	0.0491			7.50	0.3924		
8.75	1.0437			129.17	0.0410			8.75	0.1449		
10.00	1.0167							10.00	0.1364		
12.50	0.9498							12.50	0.2028		
15.00	0.8923							15.00	0.2094		
20.00	0.5597							17.50	0.1903		
30.00	0.0711							20.00	0.1820		
40.00	0.1007							30.00	0.1512		
50.00	0.1105							40.00	0.1357		
60.00	0.1392							50.00	0.1258		
70.00	0.1285							60.00	0.1249		
80.00	0.1122							70.00	0.1156		
100.00	0.0612							80.00	0.1064		
129.17	0.0414							90.00	0.0879		
145.83	0.0314							100.00	0.0443		
								129.17	0.0277		

TABLE VII. Continued

(b) Continued

		mfr = 0.87 and $\alpha = -1.0^{\circ}$						mfr = 0.87 and $\alpha = 1.0^{\circ}$					
		$\phi = 0^{\circ}$			$\phi = 180^{\circ}$			$\phi = 0^{\circ}$			$\phi = 180^{\circ}$		
		Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-94.32	0.9213	173.61	-0.0071	190.28	0.0252	-94.32	0.9243	190.28	0.0252	-94.32	0.9213	173.61	0.0119
-82.25	0.9390	190.28	0.0145	206.94	0.0406	-82.25	0.9405	190.28	0.0199	-82.25	0.9397	190.28	0.0155
-75.15	0.9439	206.94	0.0316	223.61	0.0569	-75.15	0.9435	206.94	0.0342	-75.15	0.9436	206.94	0.0295
-68.05	0.9564	223.61	0.0562	245.83	0.1066	-68.05	0.9371	223.61	0.0662	-68.05	0.9325	223.61	0.0583
-57.40	0.8964	245.83	0.1029	262.50	0.1663	-57.40	0.9372	223.61	0.0572	-57.40	0.9325	223.61	0.0526
-49.66	0.8366	262.50	0.1600	273.61	0.2351	-46.76	0.8344	262.50	0.1624	-46.76	0.8394	245.83	0.1019
-39.66	0.7728	273.61	0.2274	284.72	0.2791	-39.66	0.7750	273.61	0.2288	-39.66	0.7793	262.50	0.1609
-32.56	0.6947	279.17	0.2728	290.28	0.3288	-32.56	0.6992	279.17	0.2735	-32.56	0.7064	279.17	0.2262
-25.46	0.5914	284.72	0.3278	290.28	0.3862	-25.46	0.5954	284.72	0.3268	-25.46	0.6051	284.72	0.3155
-18.36	0.4609	290.28	0.3972			-18.36	0.4829	290.28	0.3894	-18.36	0.4906	290.28	0.3739
-14.81	0.4082					-14.81	0.4351			-14.81	0.4500		
1.88	-1.3388					1.88	-1.2641			1.88	-1.2032		
2.50	-1.2641					2.50	-1.2406			2.50	-1.2032		
3.12	-1.2309					3.12	-1.2216			3.12	-1.1977		
3.75	-1.1946					3.75	-1.1833			3.75	-1.1568		
4.38	-1.1425					4.38	-1.1643			4.38	-1.1026		
5.00	-1.1149					5.00	-1.1491			5.00	-1.0611		
5.62	-1.0459					5.62	-1.0847			5.62	-0.9922		
6.25	-1.0459					6.25	-1.0000			6.25	-0.9749		
7.50	-0.9838					7.50	-0.9838			7.50	-0.8197		
8.75	-0.9176					8.75	-0.9176			8.75	-0.8067		
10.00	-0.9040					10.00	-0.9040			10.00	-0.7929		
12.50	-0.8545					12.50	-0.8545			12.50	-0.7929		
15.00	-0.8524					15.00	-0.8524			15.00	-0.7929		
17.50	-0.8267					17.50	-0.8267			17.50	-0.7929		
20.00	-0.6957					20.00	-0.6957			20.00	-0.7929		
30.00	-0.1290					30.00	-0.1290			30.00	-0.7929		
40.00	-0.1353					40.00	-0.1353			40.00	-0.7929		
50.00	-0.1353					50.00	-0.1353			50.00	-0.7929		
60.00	-0.1327					60.00	-0.1327			60.00	-0.7929		
70.00	-0.1231					70.00	-0.1231			70.00	-0.7929		
80.00	-0.1053					80.00	-0.1053			80.00	-0.7929		
90.00	-0.0928					90.00	-0.0928			90.00	-0.7929		
100.00	-0.0444					100.00	-0.0444			100.00	-0.7929		
129.17	-0.0256					129.17	-0.0256			129.17	-0.7929		
12.50	-0.2976					12.50	-0.2976			12.50	-0.2976		
15.00	-0.1487					15.00	-0.1487			15.00	-0.1487		
17.50	-0.1512					17.50	-0.1512			17.50	-0.1512		
20.00	-0.1507					20.00	-0.1507			20.00	-0.1507		
30.00	-0.1493					30.00	-0.1493			30.00	-0.1493		
40.00	-0.1490					40.00	-0.1490			40.00	-0.1490		
50.00	-0.1385					50.00	-0.1385			50.00	-0.1385		
60.00	-0.1247					60.00	-0.1247			60.00	-0.1247		
70.00	-0.1131					70.00	-0.1131			70.00	-0.1131		
80.00	-0.1030					80.00	-0.1030			80.00	-0.1030		
100.00	-0.0485					100.00	-0.0485			100.00	-0.0485		
129.17	-0.0306					129.17	-0.0306			129.17	-0.0306		
145.83	-0.0124					145.83	-0.0124			145.83	-0.0124		

TABLE VII. Continued

(b) Continued

mfr = 0.87 and $\alpha = 2.0^\circ$				mfr = 0.67 and $\alpha = 3.1^\circ$				mfr = 0.74 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP	Forebody X/L	Afterbody CP
-94.32	0.9204	-94.32	0.9204	-94.32	0.9212	-94.32	0.9212	-94.32	0.8544	-94.32	0.8566
-82.25	0.9361	-82.25	0.9359	-82.25	0.9372	-82.25	0.9363	-82.25	0.8755	-82.25	0.8772
-75.15	0.9427	-75.15	0.9420	-75.15	0.9431	-75.15	0.9431	-75.15	0.8813	-75.15	0.8813
-68.05	0.9348	-68.05	0.9348	-68.05	0.9326	-68.05	0.9326	-68.05	0.8666	-68.05	0.8666
-57.40	0.8974	-57.40	0.8974	-57.40	0.8966	-57.40	0.8966	-57.40	0.8226	-57.40	0.8226
-46.76	0.8349	-46.76	0.8349	-46.76	0.8396	-46.76	0.8396	-46.76	0.7416	-46.76	0.7416
-39.66	0.7767	-39.66	0.7767	-39.66	0.7815	-39.66	0.7815	-39.66	0.6659	-39.66	0.6659
-32.56	0.7050	-32.56	0.7050	-32.56	0.7073	-32.56	0.7073	-32.56	0.5564	-32.56	0.5564
-25.46	0.6016	-25.46	0.6016	-25.46	0.6147	-25.46	0.6147	-25.46	0.4141	-25.46	0.4141
-18.36	0.5022	-18.36	0.5022	-18.36	0.5177	-18.36	0.5177	-18.36	0.2450	-18.36	0.2450
-14.81	0.4621	-14.81	0.4621	-14.81	0.4831	-14.81	0.4831	-14.81	0.1586	-14.81	0.1586
-11.26	0.4020	-11.26	0.4020	-11.26	0.4445	-11.26	0.4445	-11.26	0.0351	-11.26	0.0351
-7.88	0.4554	-7.88	0.4554	-7.88	0.4798	-7.88	0.4798	-7.88	0.0689	-7.88	0.0689
-4.51	0.6684	-4.51	0.6684	-4.51	0.7023	-4.51	0.7023	-4.51	0.3123	-4.51	0.3123
-2.25	0.9228	-2.25	0.9228	-2.25	0.9553	-2.25	0.9553	-2.25	0.6679	-2.25	0.6679
-1.46	1.0503	-1.46	1.0503	-1.46	1.0739	-1.46	1.0739	-1.46	0.8739	-1.46	0.8739
-0.90	1.1436	-0.90	1.1436	-0.90	1.1605	-0.90	1.1605	-0.90	1.0327	-0.90	1.0327
-0.39	1.1841	-0.39	1.1841	-0.39	1.1841	-0.39	1.1841	-0.39	1.1736	-0.39	1.1736
-0.19	1.1273	-0.19	1.1273	-0.19	1.1084	-0.19	1.1084	-0.19	1.1894	-0.19	1.1894
0.00	0.5423	0.00	0.5423	0.00	0.4619	0.00	0.4619	0.00	0.7681	0.00	0.7681
0.31	-1.4742	0.31	-1.4742	0.31	-1.4938	0.31	-1.4938	0.31	-1.2380	0.31	-1.2380
0.62	-1.5009	0.62	-1.5009	0.62	-1.5487	0.62	-1.5487	0.62	-1.2299	0.62	-1.2299
1.25	-1.4542	1.25	-1.4542	1.25	-1.5224	1.25	-1.5224	1.25	-1.1849	1.25	-1.1849
1.88	-1.3969	1.88	-1.3969	1.88	-1.4422	1.88	-1.4422	1.88	-1.0825	1.88	-1.0825
2.50	-1.3338	2.50	-1.3338	2.50	-1.3883	2.50	-1.3883	2.50	-1.0214	2.50	-1.0214
3.12	-1.2810	3.12	-1.2810	3.12	-1.3465	3.12	-1.3465	3.12	-0.9586	3.12	-0.9586
3.75	-1.2439	3.75	-1.2439	3.75	-1.3193	3.75	-1.3193	3.75	-0.8940	3.75	-0.8940
4.38	-1.2027	4.38	-1.2027	4.38	-1.2676	4.38	-1.2676	4.38	-0.8825	4.38	-0.8825
5.00	-1.1590	5.00	-1.1590	5.00	-1.2340	5.00	-1.2340	5.00	-0.8320	5.00	-0.8320
6.25	-1.1353	6.25	-1.1353	6.25	-1.1959	6.25	-1.1959	6.25	-0.7401	6.25	-0.7401
7.50	-1.0777	7.50	-1.0777	7.50	-1.1436	7.50	-1.1436	7.50	-0.2479	7.50	-0.2479
10.00	-1.0096	10.00	-1.0096	10.00	-0.9910	10.00	-0.9910	10.00	-0.0319	10.00	-0.0319
12.50	-0.9161	12.50	-0.9161	12.50	-0.9618	12.50	-0.9618	12.50	-0.1576	12.50	-0.1576
15.00	-0.8108	15.00	-0.8108	15.00	-0.9552	15.00	-0.9552	15.00	-0.1937	15.00	-0.1937
17.50	-0.7351	17.50	-0.7351	17.50	-0.6474	17.50	-0.6474	17.50	-0.1832	17.50	-0.1832
20.00	-0.1436	20.00	-0.1436	20.00	-0.4059	20.00	-0.4059	20.00	-0.1860	20.00	-0.1860
30.00	-0.0852	30.00	-0.0852	30.00	-0.0683	30.00	-0.0683	30.00	-0.1526	30.00	-0.1526
40.00	-0.1239	40.00	-0.1239	40.00	-0.1007	40.00	-0.1007	40.00	-0.1368	40.00	-0.1368
50.00	-0.1250	50.00	-0.1250	50.00	-0.1196	50.00	-0.1196	50.00	-0.1267	50.00	-0.1267
60.00	-0.1308	60.00	-0.1308	60.00	-0.1319	60.00	-0.1319	60.00	-0.1303	60.00	-0.1303
70.00	-0.1225	70.00	-0.1225	70.00	-0.1146	70.00	-0.1146	70.00	-0.1187	70.00	-0.1187
80.00	-0.1096	80.00	-0.1096	80.00	-0.1090	80.00	-0.1090	80.00	-0.1047	80.00	-0.1047
100.00	-0.0510	100.00	-0.0510	100.00	-0.0568	100.00	-0.0568	100.00	-0.0450	100.00	-0.0450
129.17	-0.0348	129.17	-0.0348	129.17	-0.0294	129.17	-0.0294	129.17	-0.0206	129.17	-0.0206
145.83	-0.0193	145.83	-0.0193	145.83	-0.0190	145.83	-0.0190	145.83	-0.0078	145.83	-0.0078

TABLE VII. Continued

(b) Continued

mfr = 0.85 and $\alpha = -2.1^\circ$				mfr = 0.85 and $\alpha = -1.1^\circ$				mfr = 0.84 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody X/L	Afterbody X/L	Forebody CP	Afterbody CP	Forebody X/L	Afterbody X/L	Forebody CP	Afterbody CP	Forebody X/L	Afterbody X/L	Forebody CP	Afterbody CP
-94.32	0.2653	173.61	-0.0038	-94.32	0.2959	190.28	0.0359	-94.32	0.2486	173.61	0.0123
-82.25	0.1439	190.28	0.0203	-82.25	0.2071	206.94	0.0479	-82.25	0.1876	190.28	0.0244
-75.15	0.0781	206.94	0.0353	-66.76	-0.1857	223.61	0.0646	-75.15	0.1654	206.94	0.0351
-68.05	0.0091	223.61	0.0563	-11.26	-0.6125	245.83	0.1077	-68.05	0.0422	223.61	0.0584
-57.40	-0.0553	245.83	0.0980	-4.51	0.1239	262.50	0.1574	-57.40	-0.0830	245.83	0.1009
-46.76	-0.1967	262.50	0.1403	-0.90	0.9839	279.17	0.2105	-46.76	-0.1598	262.50	0.1470
-39.66	-0.3828	279.17	0.1928	0.00	0.8074	296.84	0.2502	-39.66	-0.2750	279.17	0.2008
-32.56	-0.5296	299.17	0.2282	0.31	-1.1693	284.72	0.2902	-32.56	-0.3060	279.17	0.2339
-25.46	-0.3986	284.72	0.2695	0.62	-1.2423	290.28	0.3419	-25.46	-0.3778	284.72	0.2743
-18.36	-0.7776	290.28	0.3262	1.25	-1.1530	290.28	0.3419	-18.36	-0.3060	279.17	0.2339
-14.81	-0.8893			1.88	-1.0619			-14.81	-0.3060	279.17	0.2339
-11.26	-0.6668			2.50	-1.0493			-11.26	-0.3060	279.17	0.2339
-10.14	-0.6535			3.12	-0.9675			-10.14	-0.3060	279.17	0.2339
-7.88	-0.4525			3.75	-0.9166			-7.88	-0.3060	279.17	0.2339
-4.51	-0.0864			4.38	-0.8576			-4.51	-0.3060	279.17	0.2339
-2.25	0.3658			5.00	-0.8501			-2.25	-0.3060	279.17	0.2339
-1.46	0.6103			6.25	-0.8349			-1.46	-0.3060	279.17	0.2339
-0.90	0.8248			7.50	-0.8210			-0.90	-0.3060	279.17	0.2339
-0.39	1.0862			8.75	-0.8185			-0.39	-0.3060	279.17	0.2339
-0.19	1.1820			10.00	-0.8164			-0.19	-0.3060	279.17	0.2339
0.00	0.9724			12.50	-0.8191			0.00	-0.3060	279.17	0.2339
0.31	-0.8110			15.00	-0.2116			0.31	-0.3060	279.17	0.2339
0.62	-0.6117			17.50	-0.1854			0.62	-0.3060	279.17	0.2339
1.25	-0.5028			20.00	-0.1902			1.25	-0.3060	279.17	0.2339
1.88	-0.3470			30.00	-0.1702			1.88	-0.3060	279.17	0.2339
2.50	-0.1954			40.00	-0.1451			2.50	-0.3060	279.17	0.2339
3.12	-0.1454			50.00	-0.1422			3.12	-0.3060	279.17	0.2339
3.75	-0.1862			60.00	-0.1281			3.75	-0.3060	279.17	0.2339
4.38	-0.1536			70.00	-0.1240			4.38	-0.3060	279.17	0.2339
5.00	-0.1470			80.00	-0.0963			5.00	-0.3060	279.17	0.2339
6.25	-0.1368			90.00	-0.0882			6.25	-0.3060	279.17	0.2339
7.50	-0.1447			100.00	-0.0347			7.50	-0.3060	279.17	0.2339
8.75	-0.1549			129.17	-0.0178			8.75	-0.3060	279.17	0.2339
10.00	-0.1618							10.00	-0.3060	279.17	0.2339
12.50	-0.1707							12.50	-0.3060	279.17	0.2339
15.00	-0.1574							15.00	-0.3060	279.17	0.2339
17.50	-0.1372							17.50	-0.3060	279.17	0.2339
20.00	-0.1338							20.00	-0.3060	279.17	0.2339
30.00	-0.1211							30.00	-0.3060	279.17	0.2339
40.00	-0.1061							40.00	-0.3060	279.17	0.2339
50.00	-0.1046							50.00	-0.3060	279.17	0.2339
60.00	-0.1057							60.00	-0.3060	279.17	0.2339
70.00	-0.0997							70.00	-0.3060	279.17	0.2339
80.00	-0.0948							80.00	-0.3060	279.17	0.2339
100.00	-0.0428							100.00	-0.3060	279.17	0.2339
129.17	-0.0213							129.17	-0.3060	279.17	0.2339
145.83	0.0023							145.83	-0.3060	279.17	0.2339

TABLE VII. Continued

(b) Concluded

		mfr = 0.83 and $\alpha = 1.1^\circ$				mfr = 0.83 and $\alpha = 2.0^\circ$				mfr = 0.83 and $\alpha = 3.1^\circ$			
		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
		Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-94.32	0.2934	173.61	0.0272	190.28	0.0219	-94.32	0.2946	173.61	0.0378	190.28	0.0178	-94.32	0.3010
-82.25	0.2207	190.28	0.0326	206.94	0.0405	-82.25	0.2079	190.28	0.0348	206.94	0.0378	-82.25	0.2499
-75.15	0.1314	206.94	0.0422	-46.76	-0.1802	-75.15	0.1495	206.94	0.0448	-46.76	-0.1814	-75.15	0.1966
-68.05	0.0750	233.61	0.0628	-11.26	-0.7103	-68.05	0.0629	223.61	0.0651	-11.26	-0.7517	-68.05	0.1077
-57.40	-0.0707	245.83	0.1047	-4.51	-0.0249	-57.40	-0.0596	245.83	0.1064	-4.51	-0.0741	-57.40	-0.0106
-46.76	-0.1759	262.50	0.1502	-0.90	-0.8876	-46.76	-0.1679	262.50	0.1553	-0.90	-0.8426	-46.76	-0.1675
-39.66	-0.2444	273.61	0.2048	0.31	0.9408	-39.66	-0.2367	273.61	0.2054	0.00	0.9994	-39.66	-0.2477
-32.56	-0.3013	279.17	0.2384	0.31	-0.9282	-32.56	-0.3121	279.17	0.2403	0.31	-0.7237	-32.56	-0.2983
-25.46	-0.3561	284.72	0.2793	0.62	-0.9975	-25.46	-0.3307	284.72	0.2800	0.62	-0.7094	-25.46	-0.5879
-18.36	-0.4035	290.28	0.3314	1.25	-0.7128	-18.36	-0.4603	290.28	0.3293	1.25	-0.4980	-18.36	-0.8042
-14.81	-0.7883			1.88	-0.2410	-14.81	-0.7495			1.88	-0.2219	-14.81	-0.7215
-11.26	-0.5590			2.50	-0.1861	-11.26	-0.5360			2.50	-0.1785	-11.26	-0.5158
-10.14	-0.5244			3.12	-0.1661	-10.14	-0.5087			3.12	-0.1438	-10.14	-0.4803
-7.88	-0.3447			3.75	-0.2015	-7.88	-0.2619			3.75	-0.1744	-7.88	-0.2497
-4.51	0.0922			4.38	-0.2687	-4.51	0.1367			4.38	-0.1877	-4.51	0.1703
-2.25	0.5506			5.00	-0.1997	-2.25	0.5605			5.00	-0.1191	-2.25	0.6163
-1.46	0.7380			6.25	-0.1976	-1.46	0.7761			6.25	-0.1561	-1.46	0.8156
-0.90	0.9658			7.50	-0.1997	-0.90	0.9809			7.50	-0.1280	-0.90	1.0056
-0.39	1.1606			8.75	-0.1919	-0.39	1.1633			8.75	-0.1438	-0.39	1.1758
-0.19	1.1913			10.00	-0.1813	-0.19	1.1887			10.00	-0.1483	-0.19	1.1874
0.00	0.8469			12.50	-0.2199	0.00	0.8152			12.50	-0.1645	0.00	0.7812
0.31	-1.0677			15.00	-0.1850	0.31	-1.1925			15.00	-0.1475	0.31	-1.2638
0.62	-1.1385			17.50	-0.1581	0.62	-1.1238			17.50	-0.1269	0.62	-1.2464
1.25	-1.0939			20.00	-0.1552	1.25	-1.1238			20.00	-0.1202	1.25	-1.2128
1.88	-0.9806			30.00	-0.1187	1.88	-1.0595			30.00	-0.1228	1.88	-1.1504
2.50	-0.9160			40.00	-0.1154	2.50	-0.9899			40.00	-0.1055	2.50	-1.1083
3.12	-0.8230			50.00	-0.1161	3.12	-0.9305			50.00	-0.1022	3.12	-1.0274
3.75	-0.8266			60.00	-0.1110	3.75	-0.9423			60.00	-0.1099	3.75	-1.0304
4.38	-0.8544			70.00	-0.1077	4.38	-0.9049			70.00	-0.1014	4.38	-0.9975
5.00	-0.7745			80.00	-0.0948	5.00	-0.8324			80.00	-0.0889	5.00	-0.9512
6.25	-0.4423			90.00	-0.0768	6.25	-0.8225			90.00	-0.0819	6.25	-0.8976
7.50	-0.1664			100.00	-0.0363	7.50	-0.7677			100.00	-0.0343	7.50	-0.7980
10.00	-0.2113			129.17	-0.0137	10.00	-0.6997			129.17	-0.0183	10.00	-0.8082
15.00	-0.2372					15.00	-0.1915			15.00	-0.1611	15.00	-0.1684
17.50	-0.2090					17.50	-0.1925			17.50	-0.1445	17.50	-0.1445
20.00	-0.1995					20.00	-0.1957			20.00	-0.1576	20.00	-0.1611
30.00	-0.1516					30.00	-0.1620			30.00	-0.1576	30.00	-0.1576
40.00	-0.1335					40.00	-0.1403			40.00	-0.1487	40.00	-0.1487
50.00	-0.1254					50.00	-0.1295			50.00	-0.1340	50.00	-0.1340
60.00	-0.1281					60.00	-0.1319			60.00	-0.1310	60.00	-0.1310
70.00	-0.1158					70.00	-0.1191			70.00	-0.1206	70.00	-0.1206
80.00	-0.0976					80.00	-0.0963			80.00	-0.0998	80.00	-0.0998
100.00	-0.0419					100.00	-0.0451			100.00	-0.0440	100.00	-0.0440
129.17	-0.0217					129.17	-0.0249			129.17	-0.0177	129.17	-0.0177
145.83	-0.0098					145.83	-0.0114			145.83	-0.0084	145.83	-0.0084

TABLE VII. Continued

(c) $M = 0.87$

$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$		
						$mfr = 0.49$ and $\alpha = -2.0^\circ$			$mfr = 0.49$ and $\alpha = 2.1^\circ$			$mfr = 0.49$ and $\alpha = 0^\circ$			$mfr = 0.49$ and $\alpha = 2.1^\circ$		
X/L	CP	Afterbody X/L CP	X/L	CP	Afterbody X/L CP	X/L	CP	Afterbody X/L CP	X/L	CP	Afterbody X/L CP	X/L	CP	Afterbody X/L CP	X/L	CP	Afterbody X/L CP
-94.32	1.0673	173.61	-0.0207	1.0697	190.28	0.0118	1.0650	173.61	-0.0118	1.0650	190.28	0.0040	1.0657	173.61	0.0057	1.0671	190.28
-82.25	1.0741	190.28	0.0008	1.0768	206.94	0.0204	-82.25	1.0723	190.28	0.0014	-82.25	1.0742	190.28	0.0064	-82.25	1.0750	206.94
-75.15	1.0785	206.94	0.0130	1.0906	223.61	0.0310	-75.15	1.0742	206.94	0.0124	-46.76	1.0269	223.61	0.0301	-75.15	1.0784	206.94
-68.05	1.0704	223.61	0.0291	-11.26	0.8689	245.83	0.0674	-68.05	1.0723	223.61	0.0314	-11.26	0.8311	245.83	0.0363	-68.05	1.0733
-57.40	1.0527	245.83	0.0706	-4.51	1.0296	262.50	0.1159	-57.40	1.0534	245.83	0.0745	-4.51	0.9800	262.50	0.1170	-57.40	1.0547
-46.76	1.0231	262.50	0.1195	-0.90	1.1996	273.61	0.1693	-46.76	1.0234	262.50	0.1196	-0.90	1.2018	273.61	0.1760	-46.76	1.0260
-39.66	0.9954	273.61	0.1824	0.00	1.1987	279.17	0.2062	-39.66	0.9959	273.61	0.1766	0.00	1.3166	279.17	0.2194	-39.66	1.0014
-32.56	0.9582	279.17	0.2265	0.31	-1.5851	284.72	0.2496	-32.56	0.9603	279.17	0.2165	0.31	-1.5412	284.72	0.2704	-32.56	0.9664
-25.46	0.9096	284.72	0.2828	0.62	-1.6559	290.28	0.3040	-25.46	0.9189	284.72	0.2656	0.62	-1.6204	290.28	0.3329	-25.46	0.9279
-18.36	0.8607	290.28	0.3551	1.25	-1.5794			-18.36	0.8716	290.28	0.3268	1.25	-1.5423			-18.36	0.8926
-14.81	0.8401			1.88	-1.5980			-14.81	0.8602			1.88	-1.5195			-14.81	0.8820
-11.26	0.8139			2.50	-1.5733			-11.26	0.8442			2.50	-1.5273			-11.26	0.8699
-10.14	0.8075			3.12	-1.5865			-10.14	0.8428			3.12	-1.4633			-10.14	0.8702
-7.88	0.8289			3.75	-1.5374			-7.88	0.8700			3.75	-1.3722			-7.88	0.9104
-4.51	0.9320			4.38	-1.4751			-4.51	0.9833			4.38	-1.3316			-4.51	1.0219
-2.25	1.0801			5.00	-1.4231			-2.25	1.1257			5.00	-1.2859			-2.25	1.1505
-1.46	1.1508			6.25	-1.3644			-1.46	1.1805			6.25	-1.2539			-1.46	1.1907
-0.90	1.1843			7.50	-1.2992			-0.90	1.1999			7.50	-1.1867			-0.90	1.1900
-0.39	1.1479			8.75	-1.2612			-0.39	1.1391			8.75	-1.1166			-0.39	1.0990
-0.19	1.0507			10.00	-1.1988			-0.19	1.0012			10.00	-1.1018			-0.19	0.9578
0.00	0.9969			12.50	-1.1052			0.00	0.9007			12.50	-1.0170			0.00	0.9219
0.31	-1.4542			15.00	-1.0849			0.31	-1.5555			15.00	-0.9809			0.31	-1.6055
0.62	-1.5195			17.50	-1.0013			0.62	-1.5793			17.50	-0.9121			0.62	-1.6394
1.25	-1.4332			20.00	-0.9760			1.25	-1.5108			20.00	-0.8515			1.25	-1.5716
1.88	-1.4171			30.00	-0.7834			1.88	-1.4971			30.00	-0.6157			1.88	-1.5700
2.50	-1.4047			40.00	-0.2191			2.50	-1.4870			40.00	-0.0686			2.50	-1.5649
3.12	-1.3435			50.00	-0.0279			3.12	-1.4702			50.00	-0.0408			3.12	-1.5538
3.75	-1.2533			60.00	-0.0272			3.75	-1.3990			60.00	-0.0736			3.75	-1.5408
4.38	-1.2232			70.00	-0.0575			4.38	-1.3273			70.00	-0.0882			4.38	-1.4630
5.00	-1.1737			80.00	-0.0703			5.00	-1.2879			80.00	-0.0928			5.00	-1.4185
6.25	-1.0999			90.00	-0.0657			6.25	-1.2400			90.00	-0.0836			6.25	-1.3446
7.50	-1.0461			100.00	-0.0265			7.50	-1.1657			100.00	-0.0319			7.50	-1.2786
8.75	-0.9931			129.17	-0.0502			8.75	-1.1204			129.17	-0.0391			8.75	-1.2418
10.00	-0.9561							10.00	-1.0823							10.00	-1.1860
12.50	-0.8594							12.50	-1.0155							12.50	-1.1244
15.00	-0.8133							15.00	-0.9279							15.00	-1.1013
17.50	-0.7514							17.50	-0.8994							17.50	-1.0212
20.00	-0.7268							20.00	-0.8156							20.00	-0.9870
30.00	-0.1922							30.00	-0.6019							30.00	-0.7217
40.00	-0.0840							40.00	-0.0637							40.00	-0.0219
50.00	-0.0806							50.00	-0.0420							50.00	-0.0289
60.00	-0.1244							60.00	-0.0659							60.00	-0.0349
70.00	-0.1137							70.00	-0.0946							70.00	-0.0615
80.00	-0.1057							80.00	-0.0963							80.00	-0.0724
100.00	-0.0509							100.00	-0.0490							100.00	-0.0473
129.17	-0.0554							129.17	-0.0373							129.17	-0.0423
145.83	-0.0434							145.83	-0.0321							145.83	-0.0390

TABLE VII. Continued
(c) Continued

mfr = 0.55 and $\alpha = 0^\circ$				mfr = 0.61 and $\alpha = 0^\circ$				mfr = 0.67 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody XL	Afterbody XL	Forebody CP	Afterbody CP	Forebody XL	Afterbody XL	Forebody CP	Afterbody CP	Forebody XL	Afterbody XL	Forebody CP	Afterbody CP
-94.32	1.0335	-94.32	1.0335	-94.32	0.9862	-94.32	0.9862	-94.32	0.9370	-94.32	0.9373
-82.25	1.0394	-82.25	1.0421	-82.25	0.9997	-82.25	1.0027	-82.25	0.9341	-82.25	0.9559
-75.15	1.0435	-75.15	1.0421	-75.15	1.0032	-75.15	1.0032	-75.15	0.9554	-75.15	0.9568
-68.05	1.0403	-68.05	1.0432	-68.05	0.9958	-68.05	0.9958	-68.05	0.9471	-68.05	0.9556
-57.40	1.0188	-57.40	1.0432	-57.40	0.9658	-57.40	0.9658	-57.40	0.9119	-57.40	0.9584
-46.76	0.9789	-46.76	1.0410	-46.76	0.9179	-46.76	0.9179	-46.76	0.8527	-46.76	0.9131
-39.66	0.9422	-39.66	1.0200	-39.66	0.8710	-39.66	0.8710	-39.66	0.7945	-39.66	0.8743
-32.56	0.8990	-32.56	1.0217	-32.56	0.8117	-32.56	0.8117	-32.56	0.7150	-32.56	0.7919
-25.46	0.8440	-25.46	1.0218	-25.46	0.7315	-25.46	0.7315	-25.46	0.6111	-25.46	0.6936
-18.36	0.7834	-18.36	1.0218	-18.36	0.6497	-18.36	0.6497	-18.36	0.5011	-18.36	0.5844
-14.81	0.7570	-14.81	1.0218	-14.81	0.6169	-14.81	0.6169	-14.81	0.4537	-14.81	0.5371
-11.26	0.7296	-11.26	1.0218	-11.26	0.5662	-11.26	0.5662	-11.26	0.3567	-11.26	0.4465
-10.14	0.7342	-10.14	1.0218	-10.14	0.5562	-10.14	0.5562	-10.14	0.3503	-10.14	0.4416
-7.88	0.7463	-7.88	1.2793	-7.88	0.5959	-7.88	1.1457	-7.88	0.4050	-7.88	1.0416
-4.51	0.8762	-4.51	1.2387	-4.51	0.7588	-4.51	1.0729	-4.51	0.6043	-4.51	0.9813
-2.25	1.0371	-2.25	1.1831	-2.25	0.9872	-2.25	1.0561	-2.25	0.8624	-2.25	0.9794
-1.46	1.1296	-1.46	1.1495	-1.46	1.0925	-1.46	1.0925	-1.46	1.0176	-1.46	0.9164
-0.90	1.1726	-0.90	1.1061	-0.90	1.1719	-0.90	1.1719	-0.90	1.1272	-0.90	0.8492
-0.39	1.1536	-0.39	1.0271	-0.39	1.2018	-0.39	1.2018	-0.39	1.2027	-0.39	0.8250
-0.19	1.0545	-0.19	0.9413	-0.19	1.1415	-0.19	0.8734	-0.19	1.1777	-0.19	0.7934
0.00	0.8974	0.00	0.8680	0.00	0.5498	0.00	0.7843	0.00	0.6710	0.00	0.6986
0.31	-1.4509	0.31	-0.8494	0.31	-1.3729	0.31	-0.7685	0.31	-1.2934	0.31	-0.6972
0.62	-1.4970	0.62	-0.7779	0.62	-1.4134	0.62	-1.4134	0.62	-1.3160	0.62	-0.5924
1.25	-1.4250	1.25	-0.7504	1.25	-1.3719	1.25	-1.3719	1.25	-1.2750	1.25	-0.1198
1.88	-1.3938	1.88	-0.9668	1.88	-1.2932	1.88	-1.0737	1.88	-1.1910	1.88	-0.0998
2.50	-1.3770	2.50	-0.9413	2.50	-1.2199	2.50	-0.9801	2.50	-1.1142	2.50	-0.1166
3.12	-1.3305	3.12	-0.9638	3.12	-1.1784	3.12	-1.0091	3.12	-1.0563	3.12	-0.1255
3.75	-1.2580	3.75	-1.0142	3.75	-1.1443	3.75	-1.0238	3.75	-1.0232	3.75	-0.1345
4.38	-1.2249	4.38	-1.1006	4.38	-1.1054	4.38	-1.0191	4.38	-0.9904	4.38	-0.1177
5.00	-1.1806	5.00	-1.0863	5.00	-1.0563	5.00	-1.0300	5.00	-0.9694	5.00	-0.1055
6.25	-1.0977	6.25	-0.9960	6.25	-1.0229	6.25	-0.9937	6.25	-0.9286	6.25	-0.0898
7.50	-1.0613	7.50	-0.9498	7.50	-0.9639	7.50	-0.9436	7.50	-0.8509	7.50	-0.0383
8.75	-1.0107	8.75	-0.9532	8.75	-0.9295	8.75	-0.8261	8.75	-0.8261	8.75	-0.0213
10.00	-0.9669	10.00	-0.9669	10.00	-0.8947	10.00	-0.8086	10.00	-0.8086	10.00	-0.0213
12.50	-0.9073	12.50	-0.9073	12.50	-0.8170	12.50	-0.7341	12.50	-0.7341	12.50	-0.0213
15.00	-0.8704	15.00	-0.8704	15.00	-0.7841	15.00	-0.6619	15.00	-0.6619	15.00	-0.0213
17.50	-0.7936	17.50	-0.7936	17.50	-0.7408	17.50	-0.6154	17.50	-0.6154	17.50	-0.0213
20.00	-0.7712	20.00	-0.7712	20.00	-0.7034	20.00	-0.5684	20.00	-0.5684	20.00	-0.0213
30.00	-0.2316	30.00	-0.2316	30.00	-0.0624	30.00	-0.0624	30.00	-0.0884	30.00	-0.0884
40.00	-0.0666	40.00	-0.0666	40.00	-0.0843	40.00	-0.0843	40.00	-0.1183	40.00	-0.1183
50.00	-0.0655	50.00	-0.0655	50.00	-0.0985	50.00	-0.0985	50.00	-0.1215	50.00	-0.1215
60.00	-0.1285	60.00	-0.1285	60.00	-0.1202	60.00	-0.1202	60.00	-0.1245	60.00	-0.1245
70.00	-0.1117	70.00	-0.1117	70.00	-0.1242	70.00	-0.1242	70.00	-0.1245	70.00	-0.1245
80.00	-0.1090	80.00	-0.1090	80.00	-0.1067	80.00	-0.1067	80.00	-0.1059	80.00	-0.1059
100.00	-0.0651	100.00	-0.0651	100.00	-0.0567	100.00	-0.0567	100.00	-0.0550	100.00	-0.0550
129.17	-0.0907	129.17	-0.0907	129.17	-0.0260	129.17	-0.0260	129.17	-0.0280	129.17	-0.0280
145.83	-0.0424	145.83	-0.0424	145.83	-0.0114	145.83	-0.0114	145.83	-0.0116	145.83	-0.0116

TABLE VII. Continued

(c) Concluded

$\phi = 0^\circ$		$\phi = 180^\circ$					
Forebody	Afterbody	Forebody	Afterbody				
X/L	CP	X/L	CP				
-94.32	0.8793	173.61	0.0137	-94.32	0.8804	190.28	0.0321
-82.25	0.9009	190.28	0.0302	-82.25	0.9018	206.94	0.0528
-75.15	0.9034	206.94	0.0464	-66.76	0.7722	223.61	0.0703
-68.05	0.8913	223.61	0.0742	-11.26	0.0771	245.83	0.1241
-57.40	0.8476	245.83	0.1274	-4.51	0.3892	262.50	0.1914
-46.76	0.7730	262.50	0.1898	-0.90	1.0672	273.61	0.2630
-39.66	0.6981	273.61	0.2384	0.00	0.7675	279.17	0.3122
-32.56	0.5985	279.17	0.3063	0.31	-1.1451	284.72	0.3672
-25.46	0.4586	284.72	0.3578	0.62	-1.2243	290.28	0.4336
-18.36	0.2945	290.28	0.4220	1.25	-1.1146		
-14.81	0.2106			1.88	-1.0380		
-11.26	0.1074			2.50	-0.9740		
-10.14	0.0742			3.12	-0.9430		
-7.88	0.1049			3.75	-0.8777		
-4.51	0.3778			4.38	-0.8447		
-2.25	0.7061			5.00	-0.8232		
-1.46	0.9006			6.25	-0.7823		
-0.90	1.0509			7.50	-0.7303		
-0.39	1.1919			8.75	-0.6715		
-0.19	1.1978			10.00	-0.6163		
0.00	0.7756			12.50	-0.1499		
0.31	-1.1635			15.00	-0.1320		
0.62	-1.1721			17.50	-0.1424		
1.25	-1.1293			20.00	-0.1248		
1.88	-1.0282			30.00	-0.1517		
2.50	-0.9851			40.00	-0.1352		
3.12	-0.9268			50.00	-0.1345		
3.75	-0.8530			60.00	-0.1312		
4.38	-0.8486			70.00	-0.1148		
5.00	-0.8470			80.00	-0.1033		
6.25	-0.7672			90.00	-0.0843		
7.50	-0.7650			100.00	-0.0359		
8.75	-0.5161			129.17	-0.0183		
10.00	-0.6597						
12.50	-0.3878						
15.00	-0.1398						
17.50	-0.1253						
20.00	-0.1428						
30.00	-0.1461						
40.00	-0.1425						
50.00	-0.1269						
60.00	-0.1331						
70.00	-0.1251						
80.00	-0.1084						
100.00	-0.0474						
129.17	-0.0210						
145.83	-0.0053						

TABLE VII. Continued
(d) Continued

		$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
		X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
$mfr = 0.55$ and $\alpha = 0^\circ$		-94.32	1.0478	173.61	0.0011	190.28	0.0205	-94.32	1.0024	190.28	0.0103	-94.32	0.9557	173.61	0.0160	190.28	0.0342
		-82.25	1.0527	190.28	0.0174	206.94	0.0347	-82.25	1.0152	206.94	0.0254	-82.25	0.9688	190.28	0.0336	206.94	0.0546
		-75.15	1.0570	206.94	0.0347	245.83	0.0975	-75.15	1.0172	206.94	0.0379	-75.15	0.9771	206.94	0.0514	245.83	0.0759
		-68.05	1.0543	223.61	0.0582	284.72	0.2240	-68.05	1.0122	223.61	0.0642	-68.05	0.9626	223.61	0.0812	284.72	0.1195
		-57.40	1.0306	245.83	0.1037	337.70	0.4698	-57.40	0.9821	245.83	0.1194	-57.40	0.9287	245.83	0.1336	337.70	0.1961
		-46.76	0.9936	262.50	0.1603	400.00	0.8488	-46.76	0.9363	262.50	0.1839	-46.76	0.8691	262.50	0.1967	400.00	0.3222
		-39.66	0.9613	273.61	0.2234	475.00	1.3880	-39.66	0.8911	273.61	0.2507	-39.66	0.8137	273.61	0.2682	475.00	0.4710
		-32.56	0.9151	279.17	0.2645	550.00	2.0370	-32.56	0.8324	279.17	0.2943	-32.56	0.7362	279.17	0.3134	550.00	0.6272
		-25.46	0.8597	284.72	0.3126	625.00	2.7817	-25.46	0.7556	284.72	0.3460	-25.46	0.6310	284.72	0.3658	625.00	0.7883
		-18.36	0.8052	290.28	0.3770	700.00	3.6117	-18.36	0.6749	290.28	0.4068	-18.36	0.5223	290.28	0.4295	700.00	0.9404
		-14.81	0.7779					-14.81	0.6372			-14.81	0.4673				
		-11.26	0.7516					-11.26	0.5770			-11.26	0.3911				
		-7.88	0.7853					-10.14	0.5781			-10.14	0.3710				
		-4.51	0.9086					-7.88	0.6092			-7.88	0.4244				
		-2.25	1.0871					-4.51	0.7695			-4.51	0.6085				
		-1.46	1.1685					-2.25	0.9006			-2.25	0.8806				
		-0.90	1.2114					-1.46	1.1063			-1.46	1.0281				
		-0.39	1.1848					-0.90	1.1840			-0.90	1.1374				
		0.00	0.9617					-0.39	1.2047			-0.39	1.2126				
		0.31	-1.3781					-0.19	1.1470			-0.19	1.1934				
		0.62	-1.4215					0.00	0.8295			0.00	0.6975				
		1.25	-1.3477					0.62	-1.3187			0.62	-1.2321				
		1.88	-1.3180					1.25	-1.2915			1.25	-1.1740				
		2.50	-1.2914					1.88	-1.2146			1.88	-1.1164				
		3.12	-1.2685					2.50	-1.1451			2.50	-1.0472				
		3.75	-1.1921					3.12	-1.1276			3.12	-0.9949				
		4.38	-1.1386					3.75	-1.0753			3.75	-0.9498				
		5.00	-1.1067					4.38	-1.0299			4.38	-0.9279				
		6.25	-1.0358					5.00	-0.9861			5.00	-0.9053				
		7.50	-1.0012					6.25	-0.9564			6.25	-0.8499				
		8.75	-0.9494					7.50	-0.9094			7.50	-0.8196				
		10.00	-0.9321					8.75	-0.8625			8.75	-0.7788				
		12.50	-0.8668					10.00	-0.8220			10.00	-0.7488				
		15.00	-0.7820					12.50	-0.7810			12.50	-0.6969				
		17.50	-0.7566					15.00	-0.7435			15.00	-0.6662				
		20.00	-0.7290					17.50	-0.6738			17.50	-0.6245				
		30.00	-0.6103					20.00	-0.6755			20.00	-0.5593				
		40.00	-0.4145					30.00	-0.5523			30.00	-0.4707				
		50.00	-0.2006					40.00	-0.4000			40.00	-0.3566				
		60.00	-0.0438					50.00	-0.2557			50.00	-0.2566				
		70.00	-0.0631					60.00	-0.0959			60.00	-0.1204				
		80.00	-0.0782					70.00	-0.0926			70.00	-0.1190				
		100.00	-0.0210					80.00	-0.0933			80.00	-0.1023				
		129.17	-0.0289					100.00	-0.0489			100.00	-0.0463				
		145.83	-0.0130					129.17	-0.0303			129.17	-0.0186				
								145.83	-0.0137			145.83	-0.0048				

TABLE VII. Continued

(d) Concluded

mfr = 0.78 and $\alpha = 0^\circ$						mfr = 0.81 and $\alpha = 0^\circ$					
$\phi = 0^\circ$			$\phi = 180^\circ$			$\phi = 0^\circ$			$\phi = 180^\circ$		
Forebody X/L	CP	Afterbody X/L	CP	Forebody X/L	CP	Afterbody X/L	CP	Forebody X/L	CP	Afterbody X/L	CP
-94.32	0.8976	173.61	0.0274	-94.32	0.9007	190.28	0.0424	-94.32	0.2853	173.61	0.0212
-82.25	0.9183	190.28	0.0418	-82.25	0.9191	206.94	0.0618	-82.25	0.1964	190.28	0.0385
-75.15	0.9259	206.94	0.0596	-46.76	0.7929	223.61	0.0862	-75.15	0.1442	206.94	0.0541
-68.05	0.9112	223.61	0.0884	-11.26	0.0938	245.83	0.1429	-68.05	0.0756	223.61	0.0799
-57.40	0.8652	245.83	0.1445	-4.51	0.3875	262.50	0.2112	-57.40	-0.0977	245.83	0.1241
-46.76	0.7930	262.50	0.2121	-0.90	1.0774	273.61	0.2861	-46.76	-0.1607	262.50	0.1768
-39.66	0.7206	273.61	0.2842	0.00	0.7885	279.17	0.3381	-39.66	-0.2132	273.61	0.2333
-32.56	0.6184	279.17	0.3287	0.31	-1.0678	284.72	0.3932	-32.56	-0.2197	279.17	0.2697
-25.46	0.4768	284.72	0.3822	0.62	-1.1617	290.28	0.4574	-25.46	-0.4315	284.72	0.3123
-18.36	0.3133	290.28	0.4452	1.25	-1.0234			-18.36	-0.7416	290.28	0.3678
-14.81	0.2324			1.88	-0.9652			-14.81	-0.6832		
-11.26	0.1077			2.50	-0.9190			-11.26	-0.4762		
-10.14	0.0956			3.12	-0.8650			-10.14	-0.4425		
-7.88	0.1547			3.75	-0.8275			-7.88	-0.2329		
-4.51	0.4096			4.38	-0.7966			-4.51	0.1295		
-2.25	0.7323			5.00	-0.7796			-2.25	0.5279		
-1.46	0.9071			6.25	-0.6885			-1.46	0.7897		
-0.90	1.0829			7.50	-0.6923			-0.90	0.9695		
-0.39	1.2040			8.75	-0.6360			-0.39	1.1704		
-0.19	1.2109			10.00	-0.5445			-0.19	1.2121		
0.00	0.8026			12.50	-0.5098			0.00	0.9109		
0.31	-1.0824			15.00	-0.5313			0.31	-0.9091		
0.62	-1.0676			17.50	-0.5171			0.62	-0.9474		
1.25	-1.0373			20.00	-0.2924			1.25	-0.8336		
1.88	-0.9592			30.00	-0.1186			1.88	-0.7990		
2.50	-0.8876			40.00	-0.1345			2.50	-0.7592		
3.12	-0.8274			50.00	-0.1252			3.12	-0.7242		
3.75	-0.8027			60.00	-0.1397			3.75	-0.6640		
4.38	-0.7947			70.00	-0.1238			4.38	-0.5835		
5.00	-0.7678			80.00	-0.1095			5.00	-0.5898		
6.25	-0.7391			90.00	-0.0898			6.25	-0.5421		
7.50	-0.6456			100.00	-0.0336			7.50	-0.4349		
8.75	-0.6555			129.17	-0.0094			8.75	-0.5140		
10.00	-0.6413							10.00	-0.3904		
12.50	-0.5336							12.50	-0.1941		
15.00	-0.5434							15.00	-0.1843		
17.50	-0.5616							17.50	-0.2142		
20.00	-0.3820							20.00	-0.1890		
30.00	-0.1113							30.00	-0.1576		
40.00	-0.1317							40.00	-0.1459		
50.00	-0.1307							50.00	-0.1286		
60.00	-0.1379							60.00	-0.1351		
70.00	-0.1227							70.00	-0.1191		
80.00	-0.1088							80.00	-0.1076		
100.00	-0.0427							100.00	-0.0395		
129.17	-0.0131							129.17	-0.0199		
145.83	0.0014							145.83	-0.0047		

TABLE VII. Continued

(e) $M = 0.92$

$\phi = 0^\circ$				$\phi = 180^\circ$				$\phi = 0^\circ$				$\phi = 180^\circ$			
Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody		Forebody		Afterbody	
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-94.32	1.0983	173.61	0.0168	-94.32	1.0980	190.28	0.0278	-94.32	1.0661	173.61	0.0153	-94.32	1.0667	190.28	0.0330
-82.25	1.1042	190.28	0.0259	-82.25	1.1054	206.94	0.0402	-82.25	1.0745	190.28	0.0302	-82.25	1.0745	206.94	0.0492
-75.15	1.1074	206.94	0.0417	-46.76	1.0584	223.61	0.0566	-75.15	1.0760	206.94	0.0452	-46.76	1.0584	223.61	0.0665
-68.05	1.1021	223.61	0.0584	-11.26	0.8814	245.83	0.1013	-68.05	1.0788	245.83	0.0711	-11.26	0.9245	245.83	0.1187
-57.40	1.0869	245.83	0.1034	-4.51	1.0232	262.50	0.1593	-57.40	1.0900	262.50	0.1212	-4.51	0.9345	262.50	0.1809
-46.76	1.0568	262.50	0.1602	-0.90	0.3784	279.17	0.2258	-46.76	1.0123	279.17	0.1803	-0.90	1.2253	273.61	0.2490
-39.66	1.0315	273.61	0.2234	0.31	0.3784	279.17	0.2702	-39.66	0.9806	273.61	0.2480	0.00	0.4839	279.17	0.2947
-32.56	0.9972	279.17	0.2666	0.31	-1.3635	284.72	0.3241	-32.56	0.9360	279.17	0.2907	0.31	-1.3067	284.72	0.3460
-25.46	0.9558	284.72	0.3149	0.62	-1.4439	290.28	0.3891	-25.46	0.8774	284.72	0.3411	0.62	-1.3748	290.28	0.4092
-18.36	0.9092	290.28	0.3806	1.25	-1.3658			-18.36	0.8237	290.28	0.4000	1.25	-1.2783		
-14.81	0.8974			1.88	-1.3491			-14.81	0.8059			1.88	-1.2649		
-11.26	0.8794			2.50	-1.3315			-11.26	0.7742			2.50	-1.2371		
-10.14	0.8884			3.12	-1.3129			-10.14	0.7705			3.12	-1.1927		
-7.88	0.9037			3.75	-1.2390			-7.88	0.7791			3.75	-1.1355		
-4.51	1.0180			4.38	-1.2056			-4.51	0.9268			4.38	-1.0894		
-2.25	1.1552			5.00	-1.1525			-2.25	1.0882			5.00	-1.0487		
-1.46	1.2002			6.25	-1.0852			-1.46	1.1682			6.25	-1.0049		
-0.90	1.2210			7.50	-1.0398			-0.90	1.2122			7.50	-0.9233		
-0.39	1.1647			8.75	-0.9683			-0.39	1.1913			8.75	-0.9033		
-0.19	1.0447			10.00	-0.9489			-0.19	1.0977			10.00	-0.8500		
0.00	0.3562			12.50	-0.9163			0.00	0.4826			12.50	-0.7922		
0.31	-1.3691			15.00	-0.8285			0.31	-1.2783			15.00	-0.7524		
0.62	-1.3945			17.50	-0.8029			0.62	-1.3328			17.50	-0.6997		
1.25	-1.3463			20.00	-0.7642			1.25	-1.2838			20.00	-0.6706		
1.88	-1.3707			30.00	-0.6417			1.88	-1.2389			30.00	-0.5987		
2.50	-1.3139			40.00	-0.5525			2.50	-1.2146			40.00	-0.5027		
3.12	-1.2975			50.00	-0.4920			3.12	-1.1797			50.00	-0.4435		
3.75	-1.2396			60.00	-0.4479			3.75	-1.1091			60.00	-0.3879		
4.38	-1.1821			70.00	-0.4088			4.38	-1.0606			70.00	-0.3500		
5.00	-1.1501			80.00	-0.3800			5.00	-1.0339			80.00	-0.3204		
6.25	-1.1004			90.00	-0.3610			6.25	-1.0020			90.00	-0.2941		
7.50	-0.9794			100.00	-0.3410			7.50	-0.9341			100.00	-0.2658		
8.75	-0.9456			129.17	-0.0013			8.75	-0.8673			129.17	-0.0167		
10.00	-0.8913							10.00	-0.8577						
12.50	-0.8644							12.50	-0.8069						
15.00	-0.8015							15.00	-0.7747						
17.50	-0.7668							17.50	-0.7095						
20.00	-0.7638							20.00	-0.6951						
30.00	-0.6338							30.00	-0.5805						
40.00	-0.5587							40.00	-0.5249						
50.00	-0.4960							50.00	-0.4442						
60.00	-0.4344							60.00	-0.4509						
70.00	-0.0471							70.00	-0.0108						
80.00	0.0079							80.00	-0.0071						
100.00	0.0250							100.00	-0.0065						
129.17	-0.0066							129.17	-0.0216						
145.83	-0.0052							145.83	-0.0107						

mfr = 0.61 and $\alpha = 0^\circ$

mfr = 0.55 and $\alpha = 0^\circ$

mfr = 0.49 and $\alpha = 0^\circ$

TABLE VII. Concluded

(e) Concluded

mfr = 0.67 and $\alpha = 0^\circ$				mfr = 0.73 and $\alpha = 0^\circ$				mfr = 0.81 and $\alpha = 0^\circ$			
$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$		$\phi = 0^\circ$		$\phi = 180^\circ$	
Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody	Forebody	Afterbody
X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP	X/L	CP
-94.32	0.9172	173.61	0.0468	-94.32	0.9171	173.61	0.0271	-94.32	0.2840	173.61	0.0315
-82.25	0.9851	190.28	0.0462	-82.25	0.9353	190.28	0.0499	-82.25	0.1987	190.28	0.0477
-75.15	0.9904	206.94	0.0645	-75.15	0.9392	206.94	0.0688	-75.15	0.1173	206.94	0.0657
-68.05	0.9803	223.61	0.0943	-68.05	0.9269	223.61	0.1008	-68.05	0.0476	223.61	0.0917
-57.40	0.9467	245.83	0.1323	-57.40	0.8860	245.83	0.1608	-57.40	-0.0367	245.83	0.1390
-46.76	0.8873	262.50	0.2215	-46.76	0.8116	262.50	0.2318	-46.76	-0.1367	262.50	0.1922
-39.66	0.8296	273.61	0.2937	-39.66	0.7366	273.61	0.3059	-39.66	-0.1870	273.61	0.2499
-32.36	0.7573	279.17	0.3394	-32.36	0.6390	279.17	0.3523	-32.36	-0.1906	279.17	0.2874
-25.46	0.6515	284.72	0.3916	-25.46	0.5342	284.72	0.4047	-25.46	-0.3432	284.72	0.3309
-18.36	0.5440	290.28	0.4532	-18.36	0.4407	290.28	0.4659	-18.36	-0.6895	290.28	0.3862
-14.81	0.4962			-14.81	0.2492			-14.81	-0.6113		
1.88	-1.0260			1.88	-0.9155			1.88	-0.7923		
2.50	-0.9614			2.50	-0.8393			2.50	-0.7064		
3.12	-0.9433			3.12	-0.8155			3.12	-0.6008		
3.75	-0.9054			3.75	-0.7674			3.75	-0.5477		
4.38	-0.8449			4.38	-0.7148			4.38	-0.5416		
5.00	-0.8180			5.00	-0.6996			5.00	-0.5427		
6.25	-0.7657			6.25	-0.6532			6.25	-0.5585		
7.50	-0.7380			7.50	-0.6220			7.50	-0.4597		
8.75	-0.7115			8.75	-0.5754			8.75	-0.1873		
10.00	-0.6802			10.00	-0.5416			10.00	-0.3939		
12.50	-0.6576			12.50	-0.5234			12.50	-0.3695		
15.00	-0.6259			15.00	-0.5183			15.00	-0.3705		
17.50	-0.5789			17.50	-0.4407			17.50	-0.2170		
20.00	-0.5414			20.00	-0.4512			20.00	-0.1604		
30.00	-0.4699			30.00	-0.0721			30.00	-0.1557		
40.00	-0.1822			40.00	-0.0904			40.00	-0.1526		
50.00	-0.0381			50.00	-0.1069			50.00	-0.1378		
60.00	-0.0708			60.00	-0.1241			60.00	-0.1493		
70.00	-0.0894			70.00	-0.1201			70.00	-0.1273		
80.00	-0.0881			80.00	-0.0998			80.00	-0.1134		
90.00	-0.0830			90.00	-0.0850			90.00	-0.0864		
100.00	-0.0229			100.00	-0.0203			100.00	-0.0299		
129.17	-0.0075			129.17	-0.0050			129.17	-0.0045		

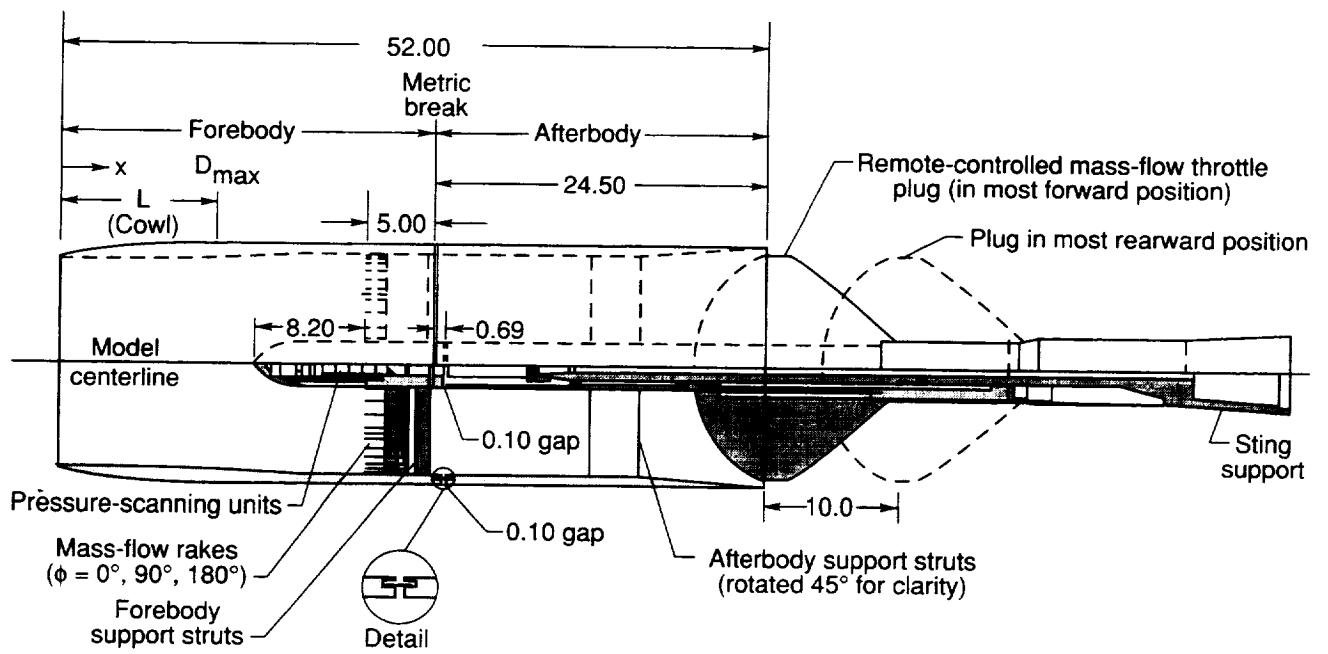
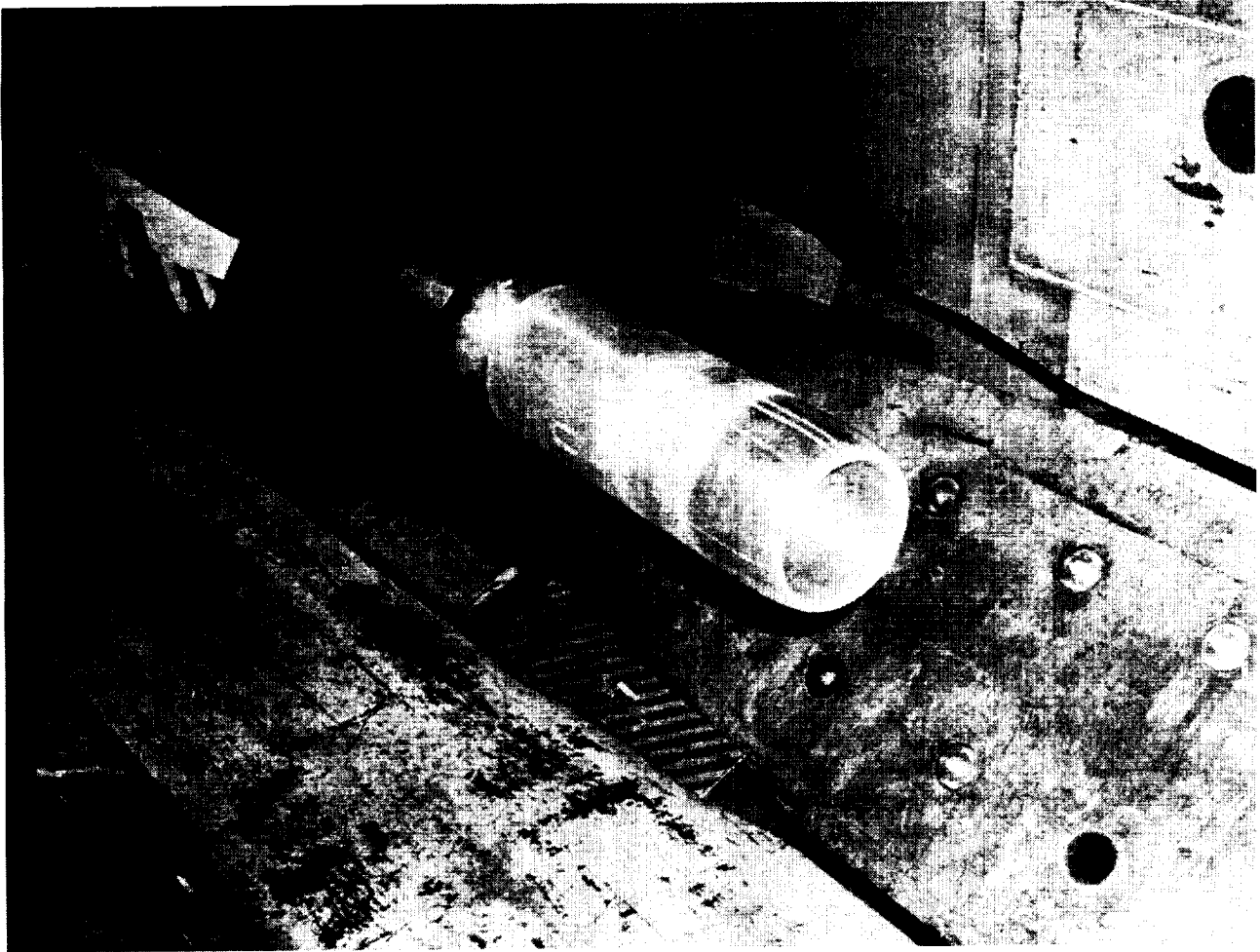


Figure 1. Simplified cross-sectional sketch of complete model. Linear dimensions are in inches.



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Figure 2. Complete model installed in 16-Foot Transonic Tunnel test section.

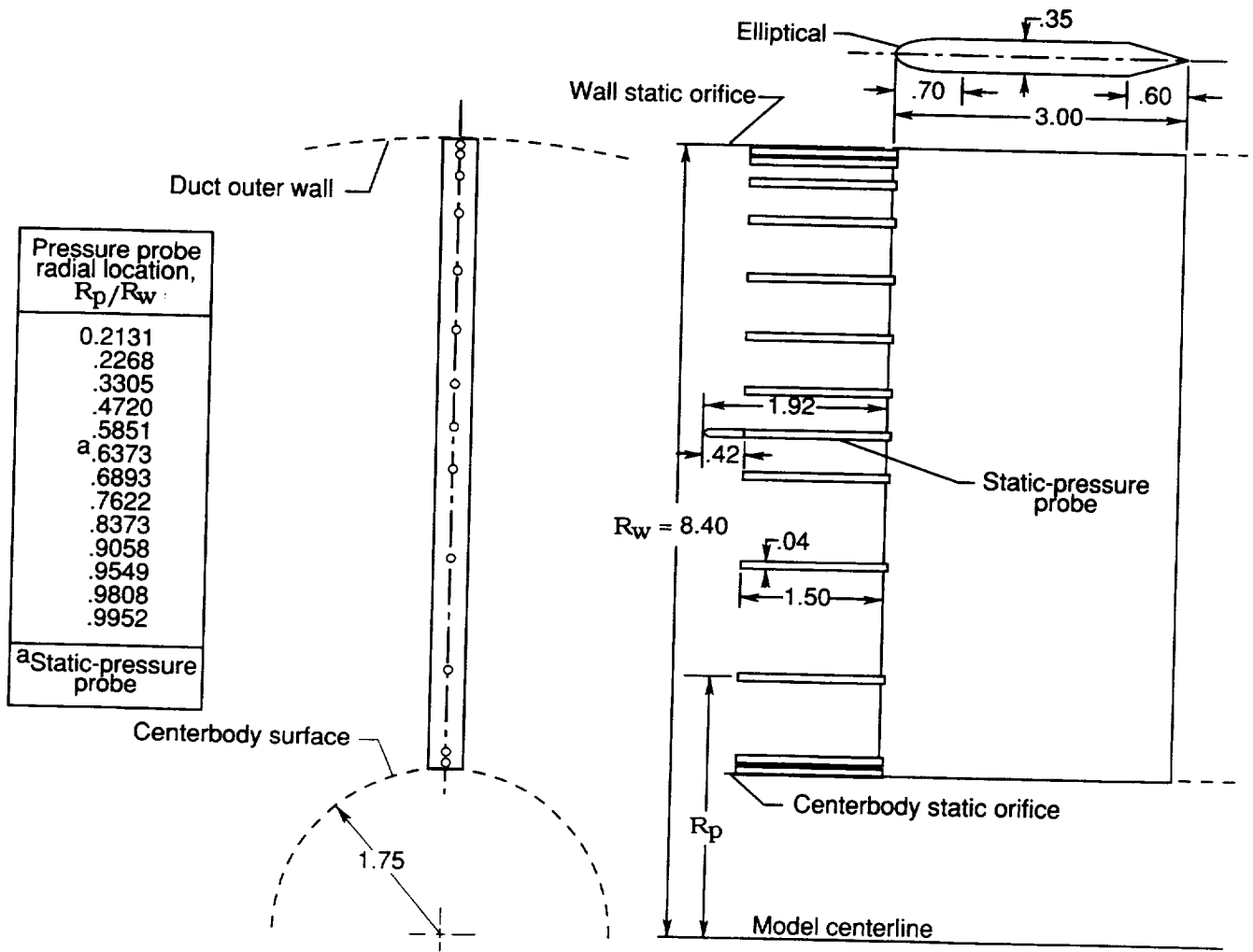


Figure 3. Pressure instrumentation (on struts at $\phi = 0^\circ, 90^\circ,$ and 180°) used to obtain data for mass-flow computations. Linear dimensions are in inches.

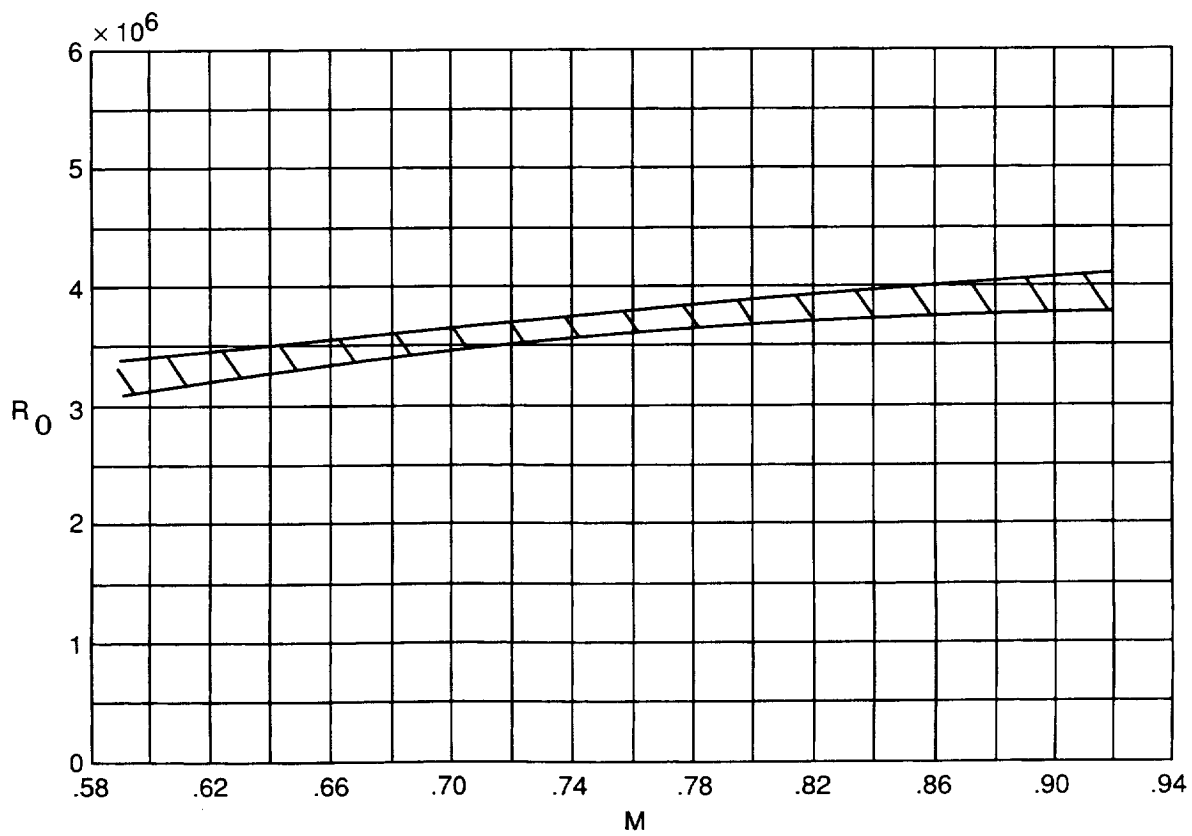


Figure 4. Variation of test Reynolds number with free-stream Mach number.

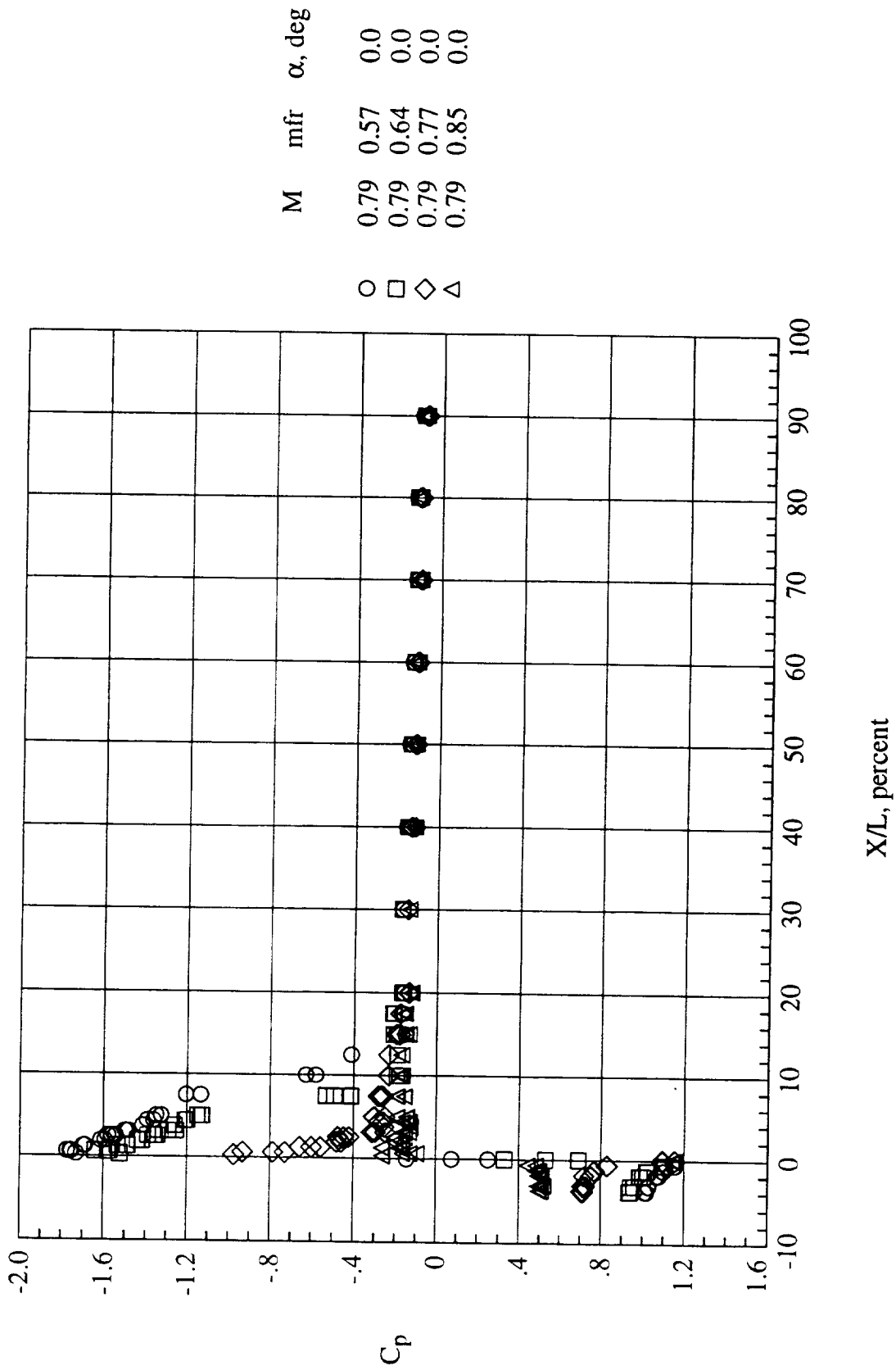
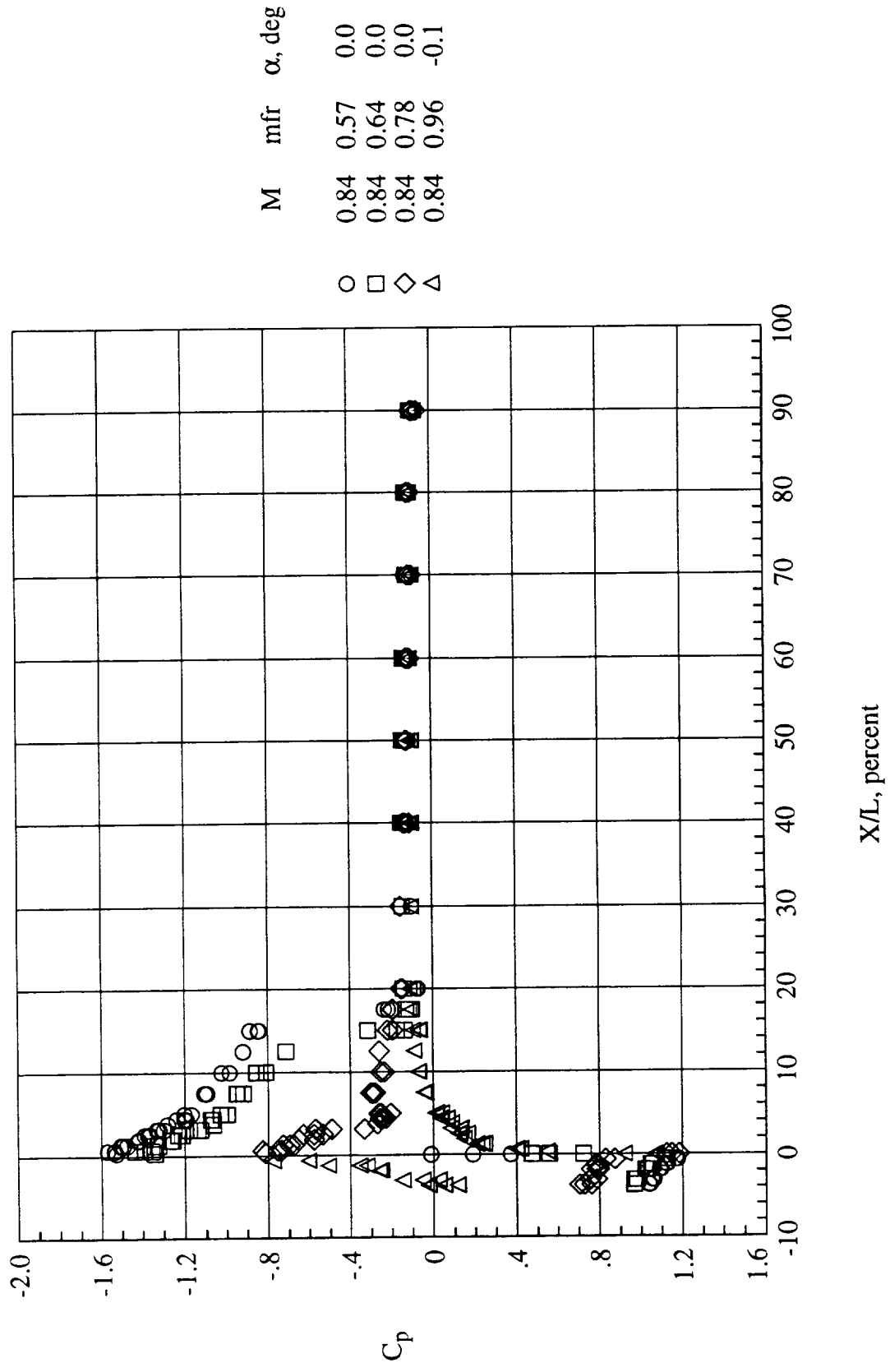
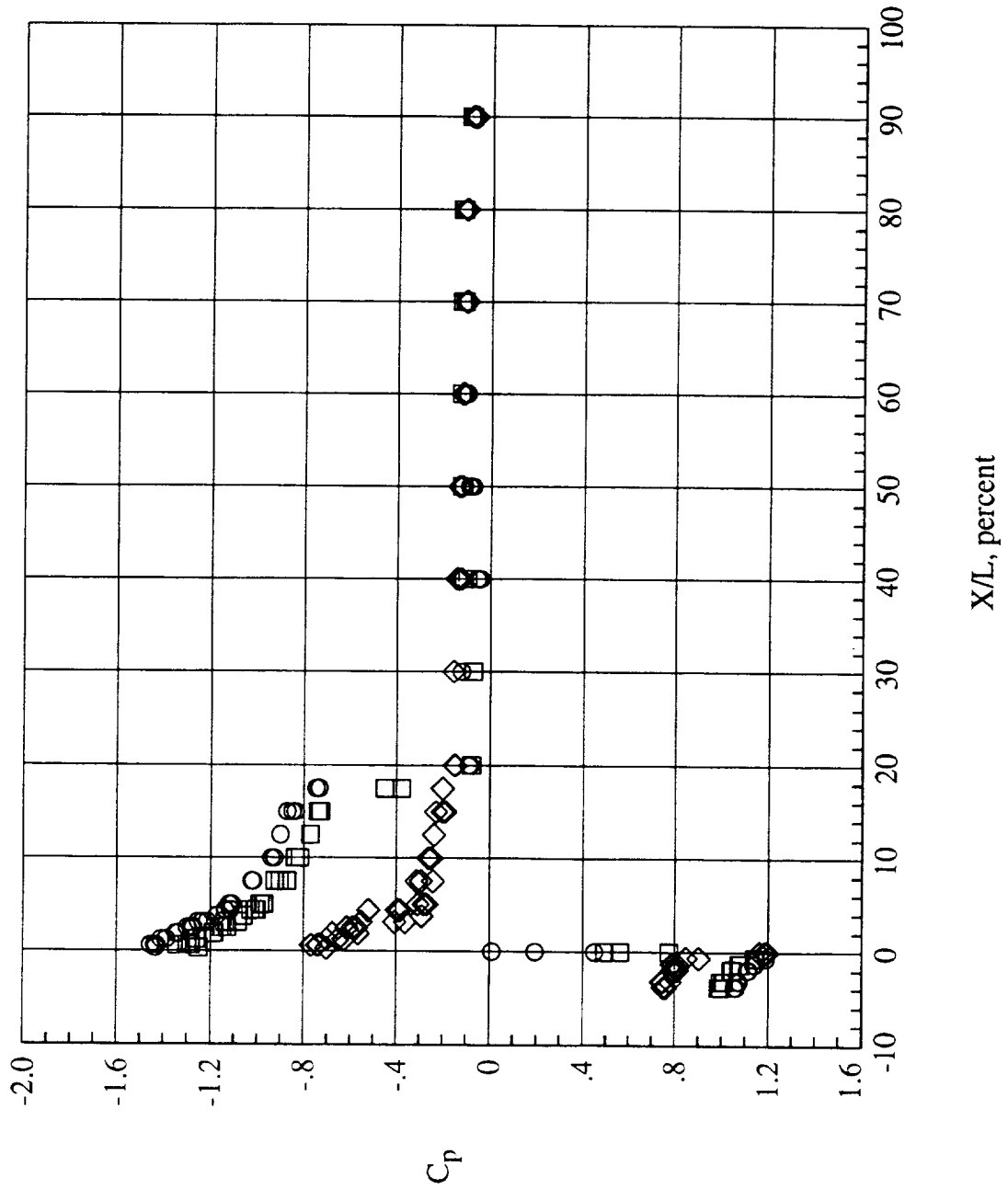


Figure 5.- Pressure coefficient variation with X/L for the NACA 1-85-100 inlet with a contraction ratio of 1.009 for several mass-flow rates at $\alpha = 0^\circ$. Data combined from $\alpha = 0^\circ$, 90° and 180° meridians.



(b) $M = 0.84$.

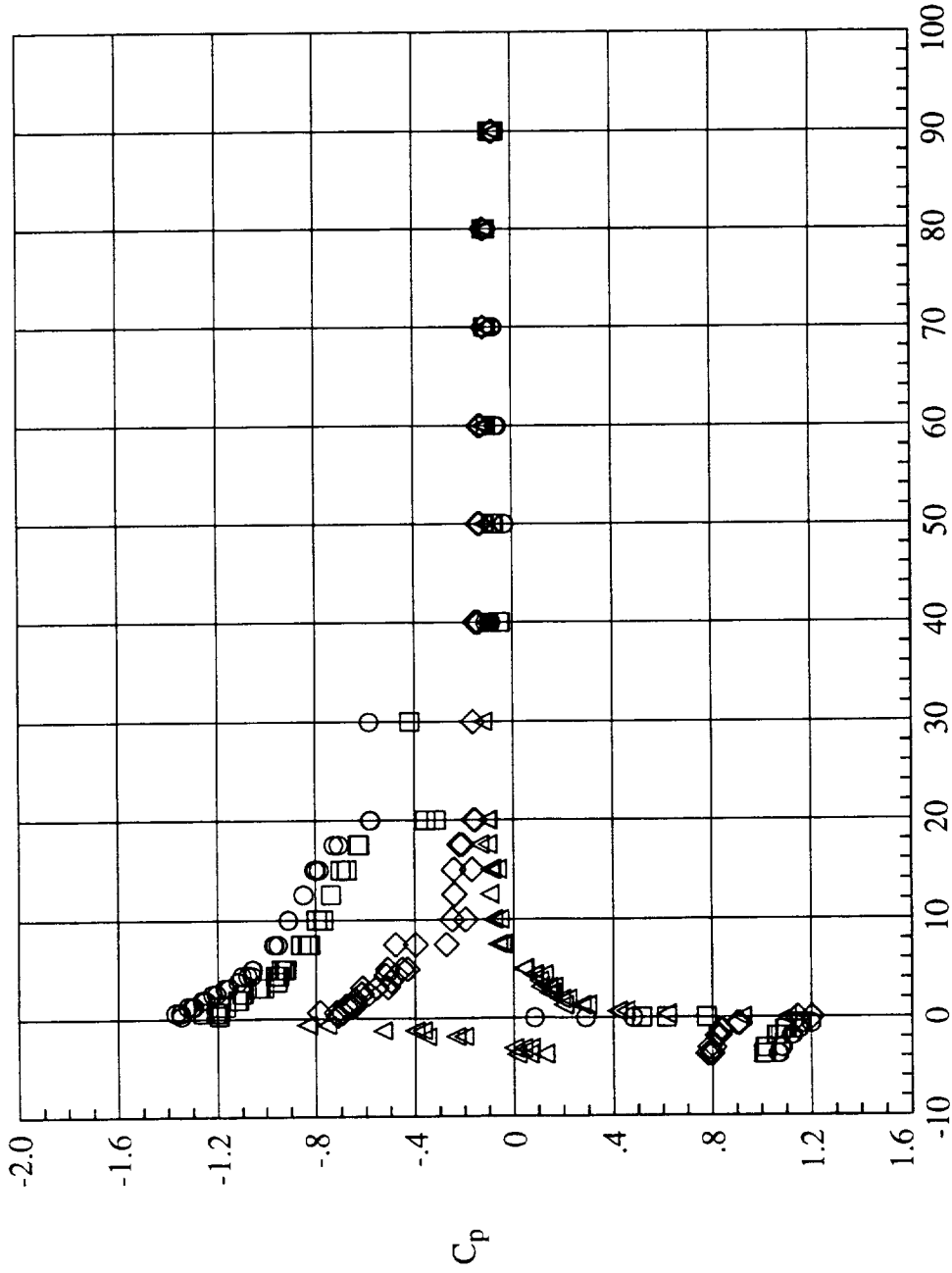
Figure 5.- Continued.



M	mfr	α , deg
0.87	0.57	0.0
0.87	0.63	0.0
0.87	0.78	0.0

○ □ ◇

(c) $M = 0.87$.
 Figure 5.- Continued.



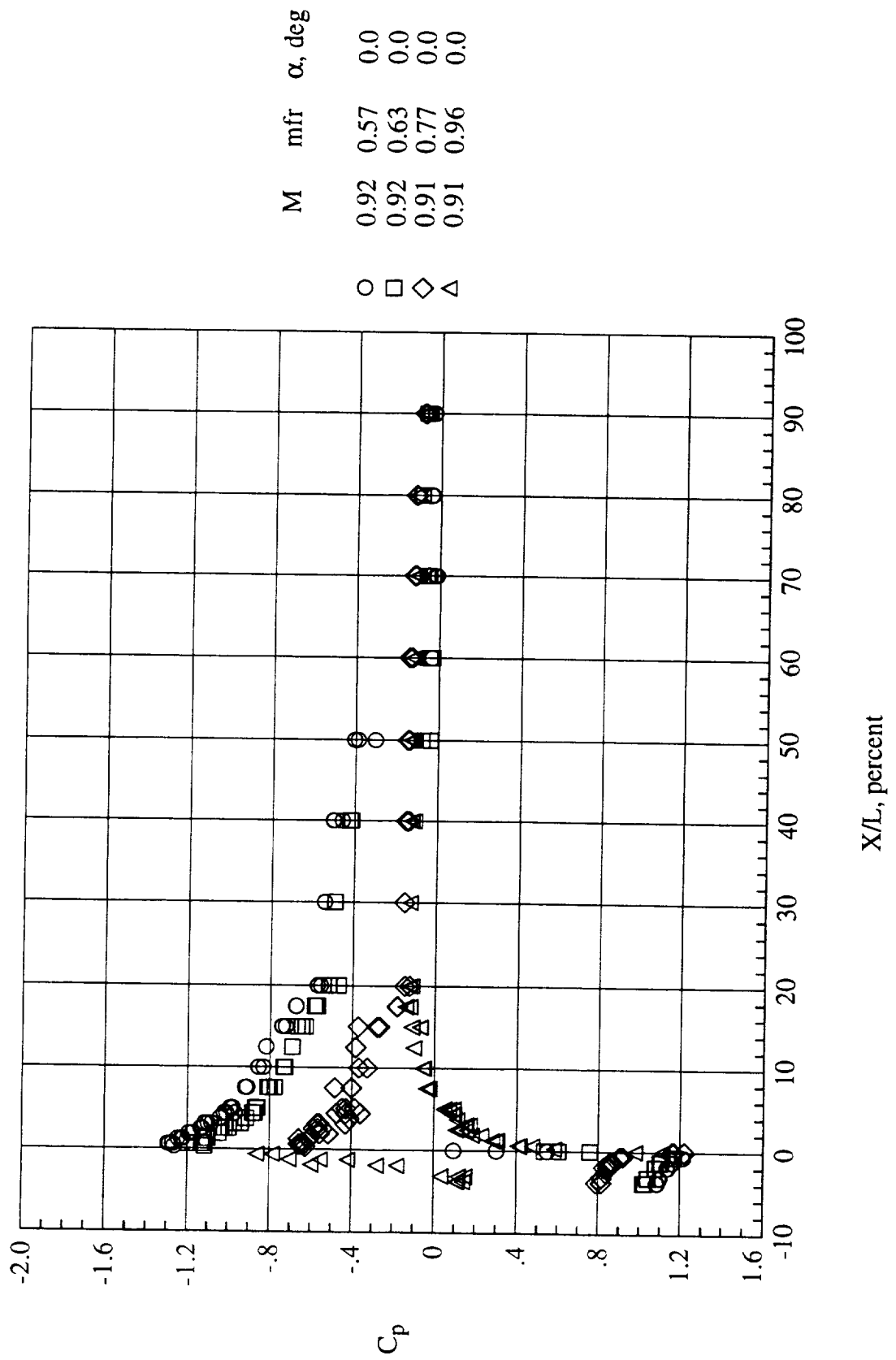
M	mfr	α , deg
0.89	0.56	0.0
0.89	0.62	0.0
0.89	0.77	-0.1
0.89	0.96	0.0

○ □ ◇ △

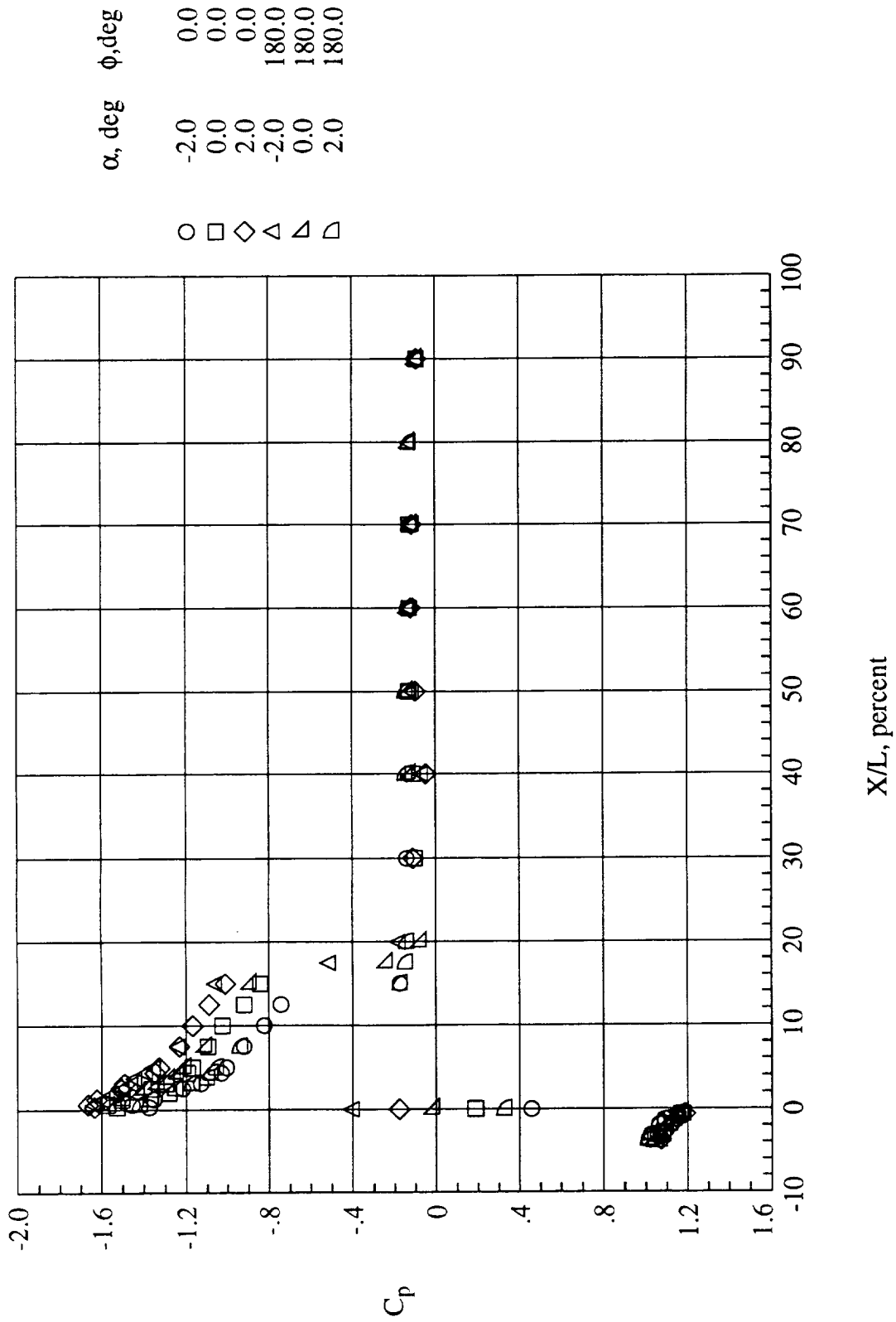
X/L, percent

(d) M = 0.89.

Figure 5. - Continued.

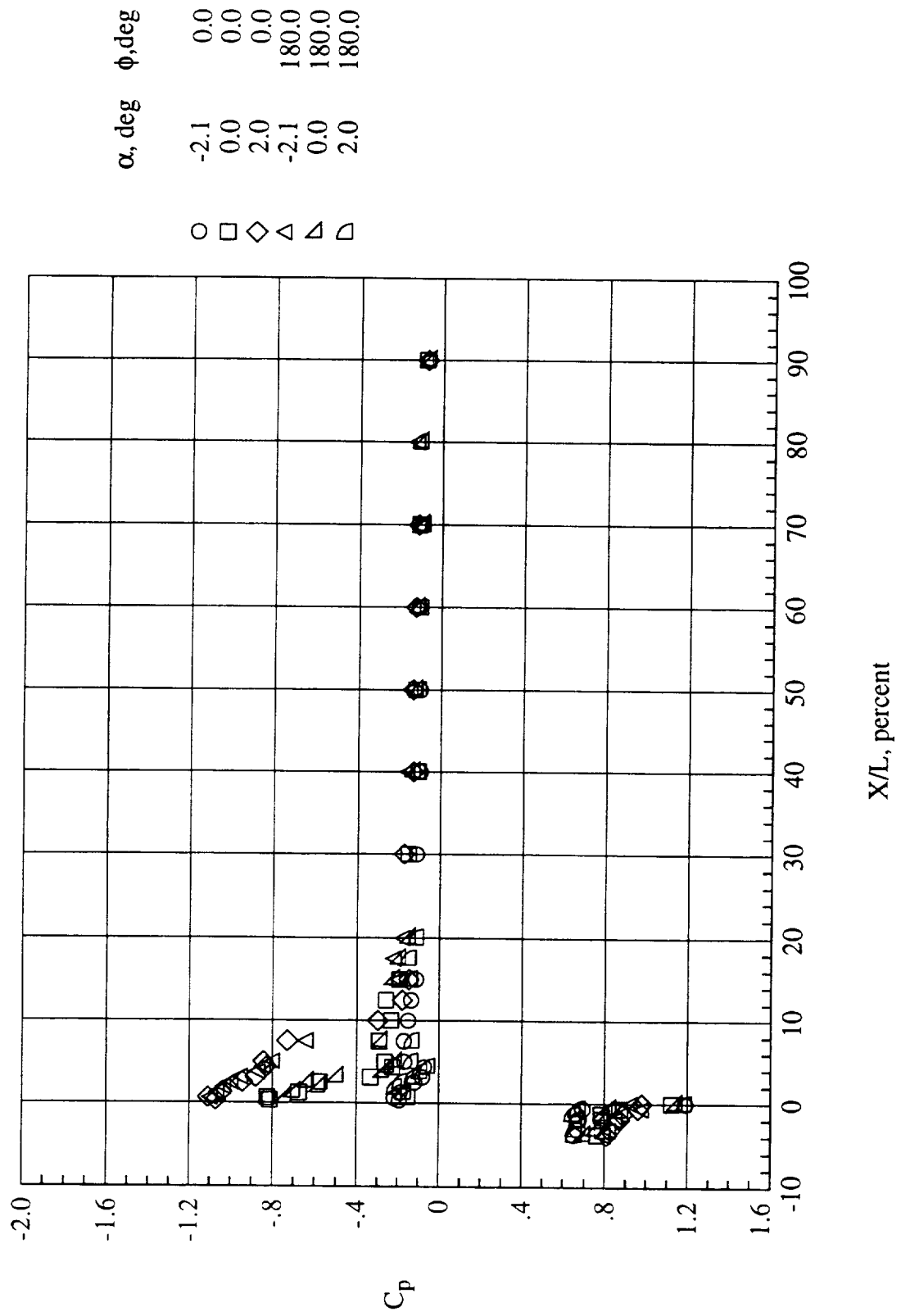


(e) $M = 0.92$.
Figure 5.- Concluded.



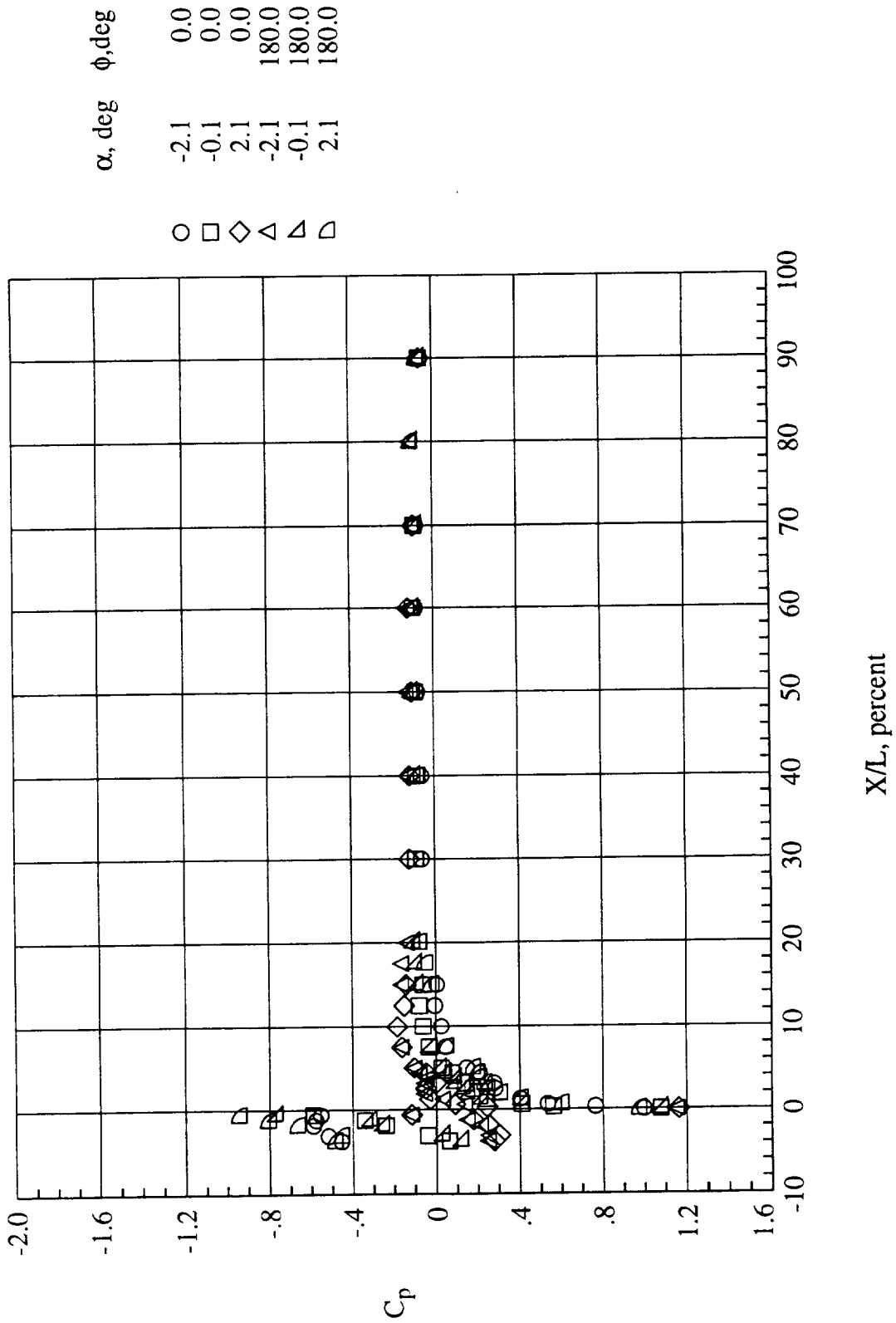
(a) $M = 0.84$ and $mfr = 0.57$.

Figure 6.- Pressure coefficient variation with X/L along the $\phi = 0^\circ$, and 180° meridians for the NACA 1-85-100 inlet with a contraction ratio of 1.009 at several angles of attack.



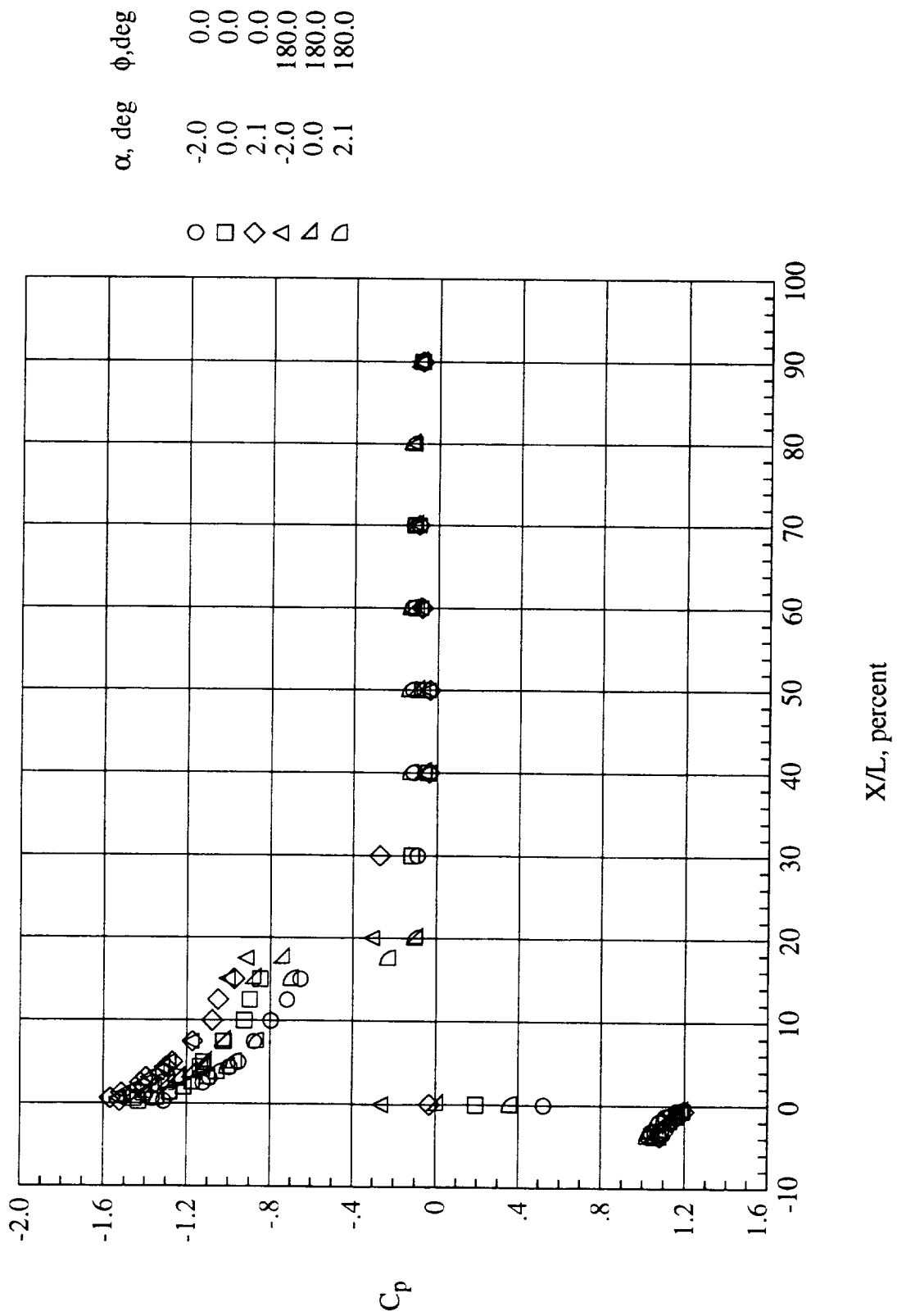
(b) $M = 0.84$ and $mfr = 0.78$.

Figure 6.- Continued.



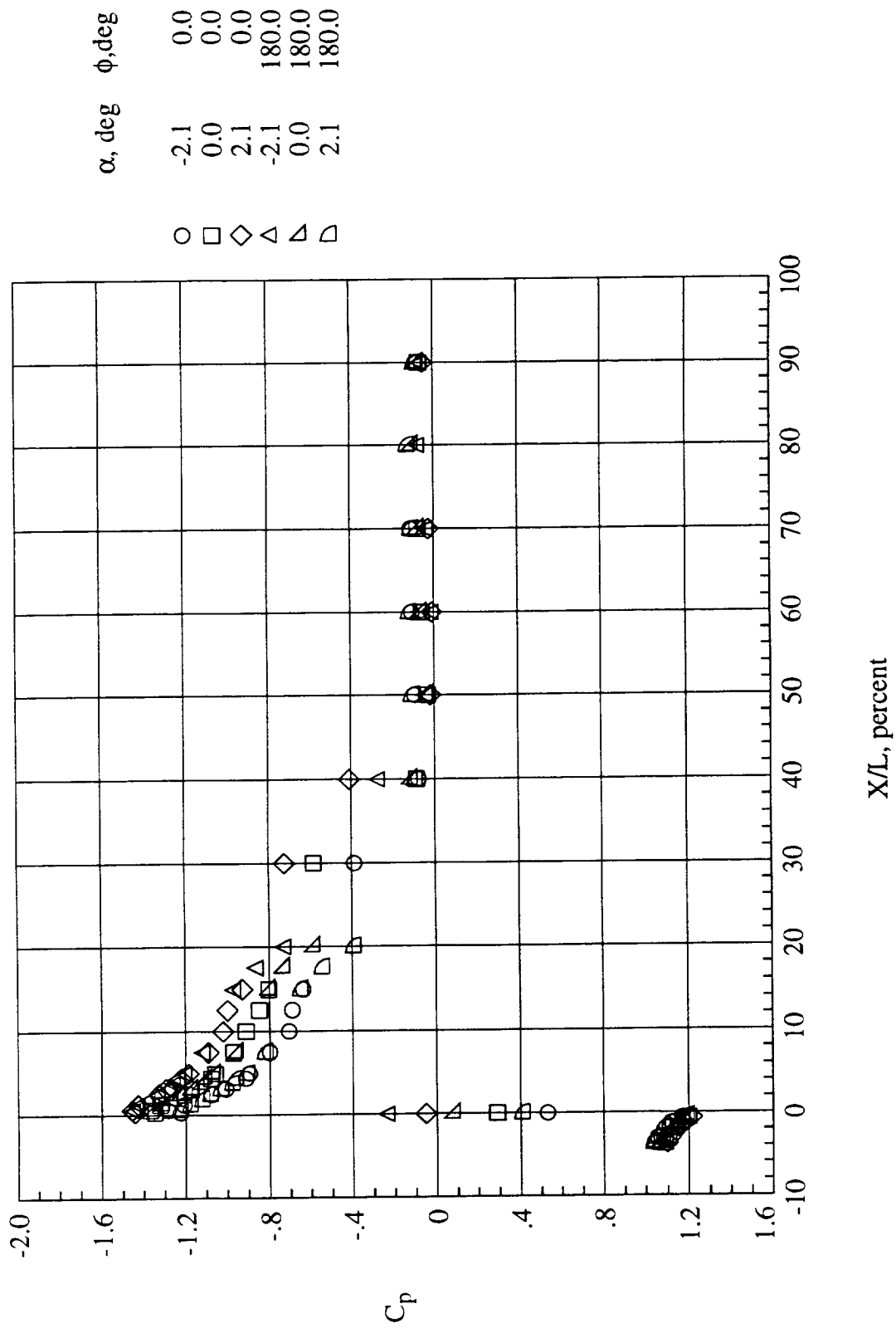
(c) $M = 0.84$ and $mfr = 0.95$.

Figure 6.- Continued.



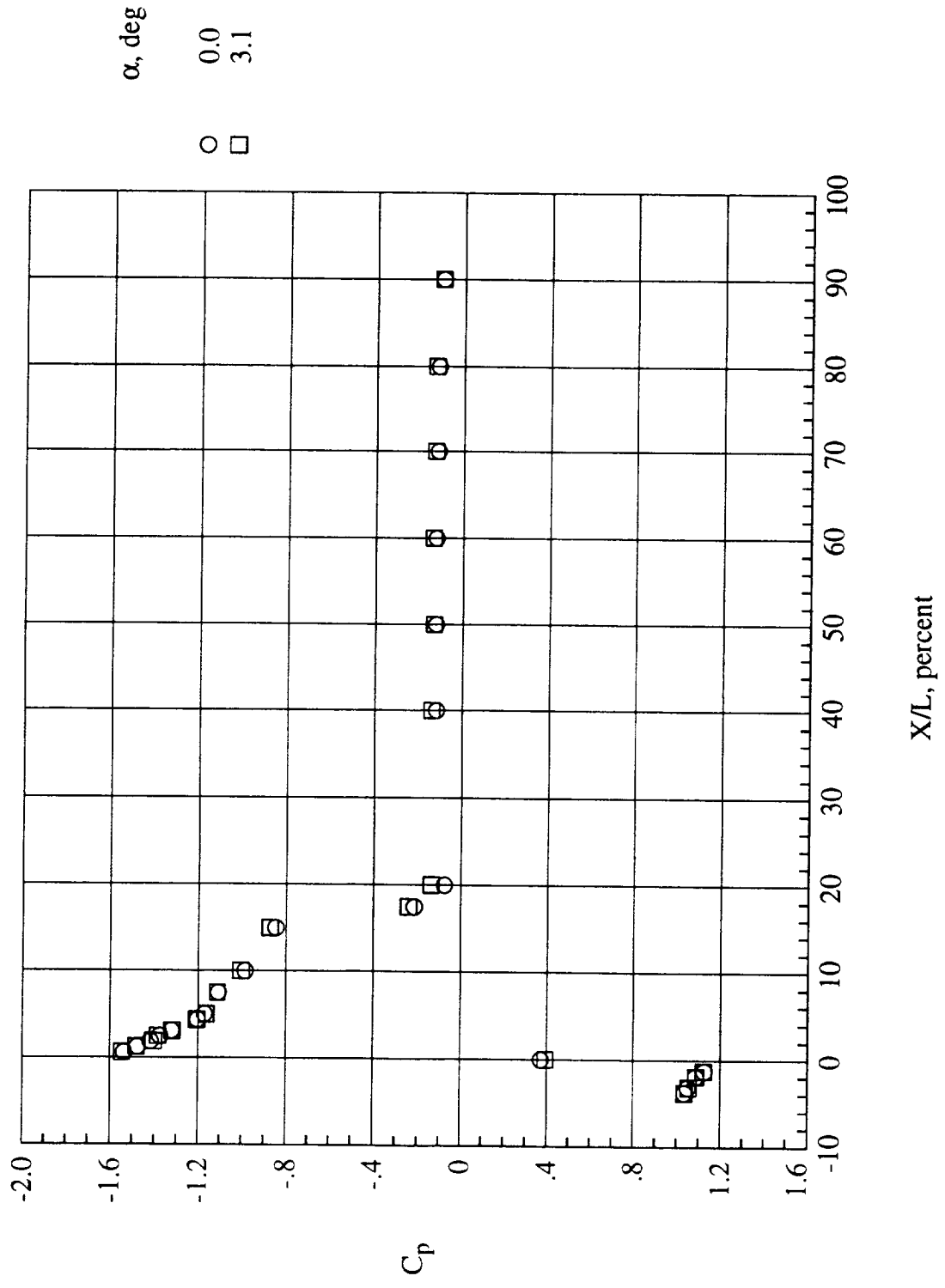
(d) $M = 0.87$ and $mfr = 0.57$.

Figure 6.- Continued.



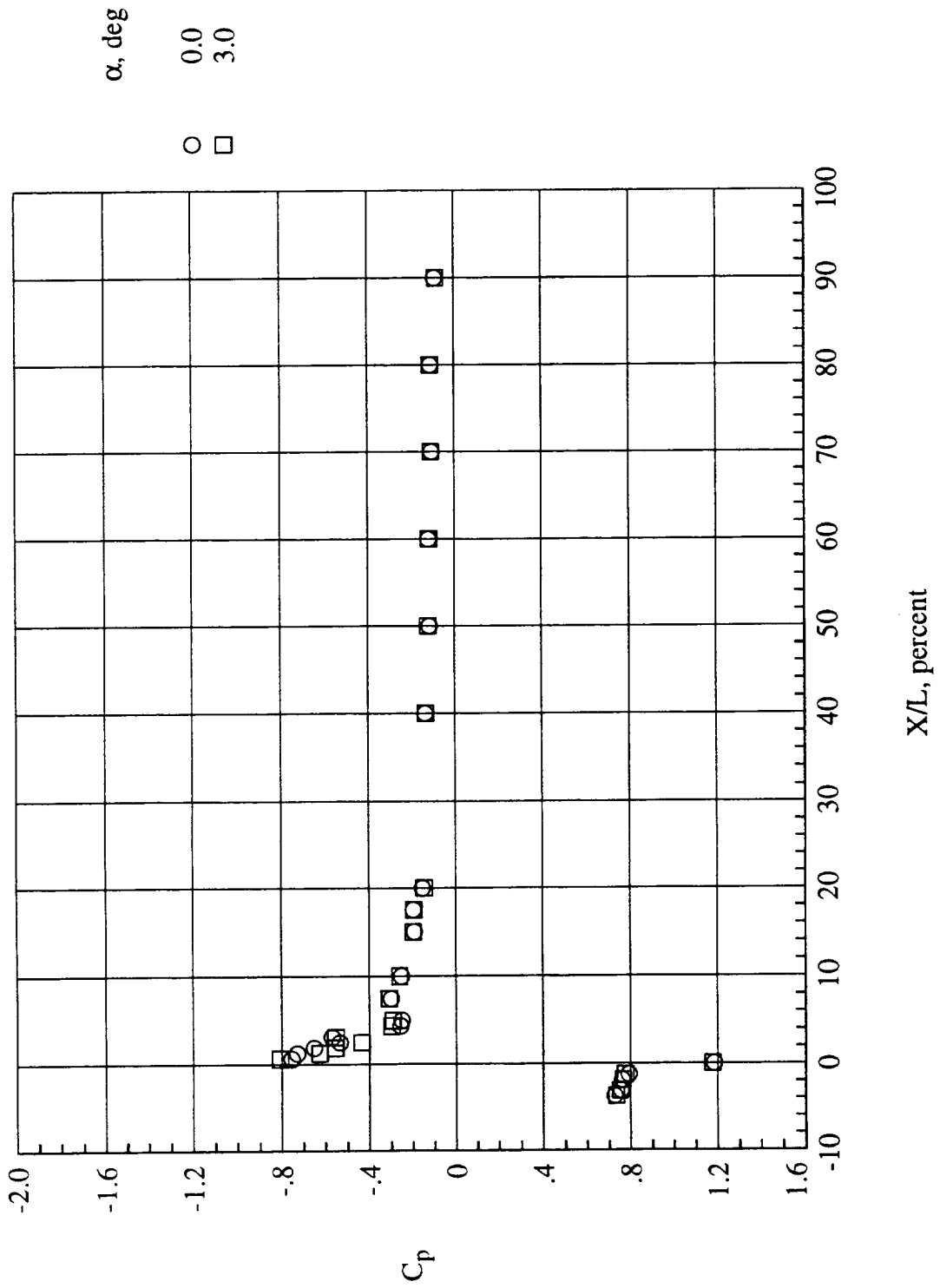
(e) $M = 0.89$ and $mfr = 0.57$.

Figure 6.- Concluded.



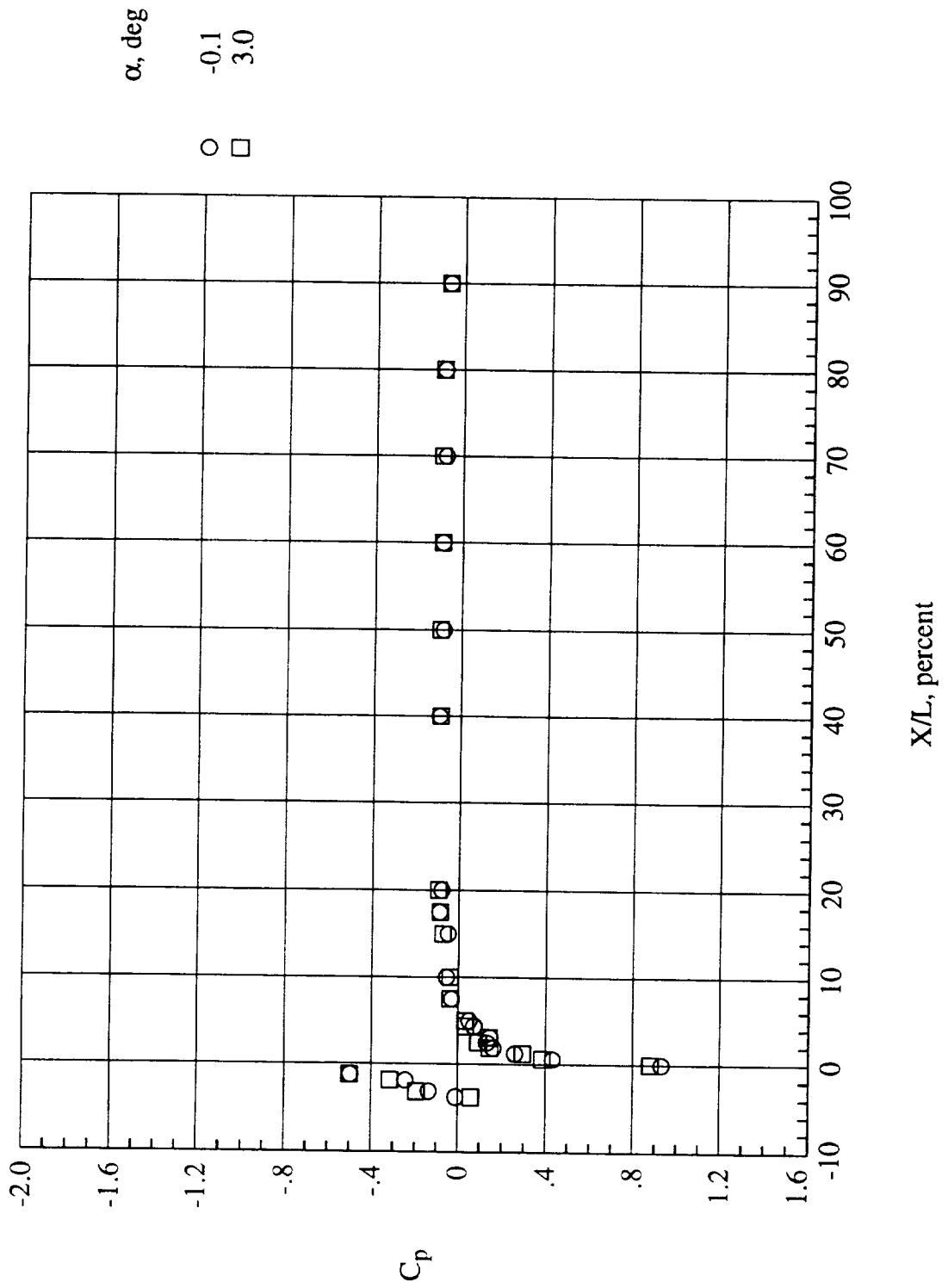
(a) $M = 0.84$ and $mfr = 0.57$.

Figure 7.- Pressure coefficient variation with X/L along the $\phi = 90^\circ$ meridian for the NACA 1-85-100 inlet with a contraction ratio of 1.000 at two angles of attack



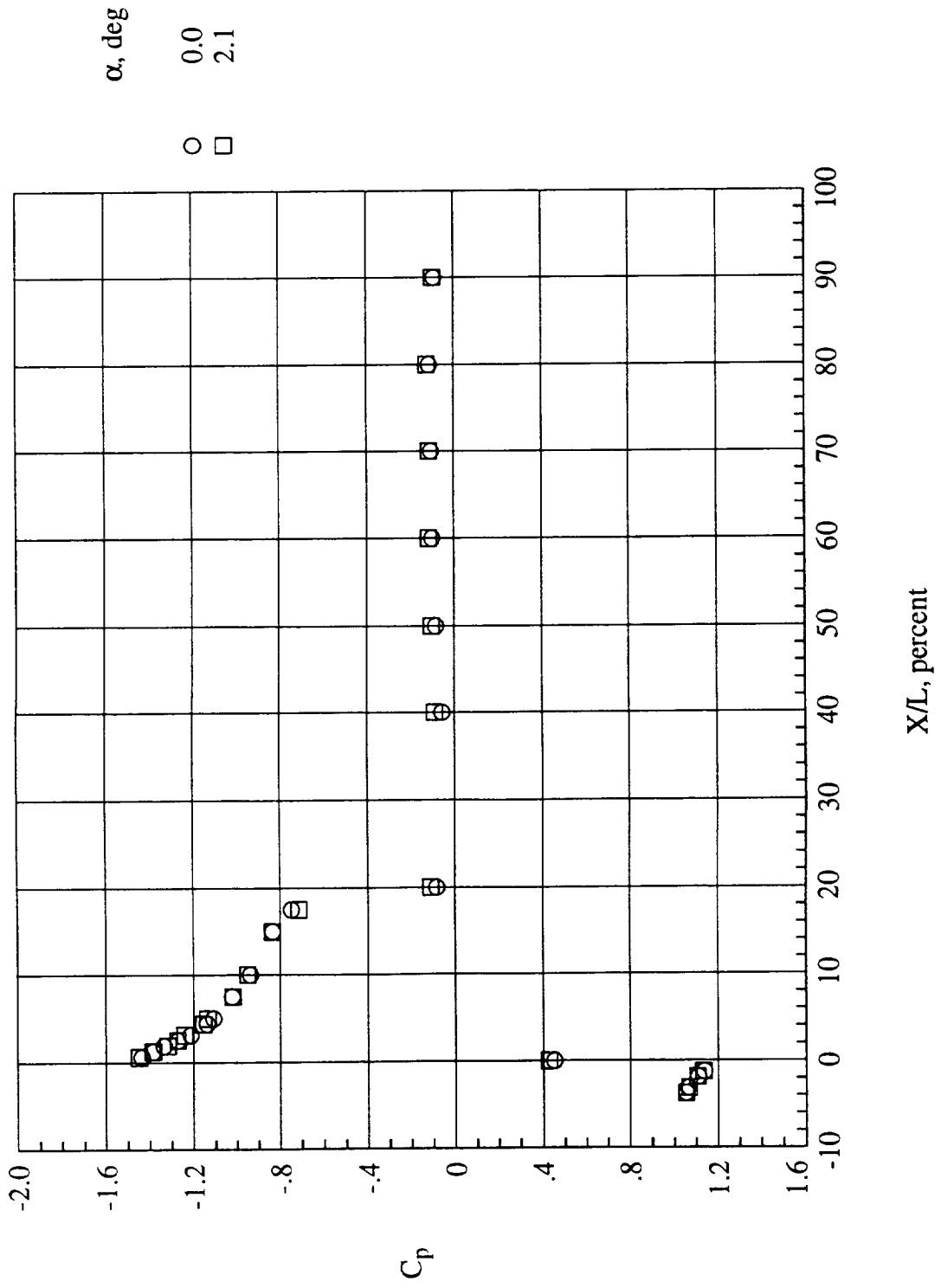
(b) $M = 0.84$ and $mfr = 0.78$.

Figure 7.- Continued.



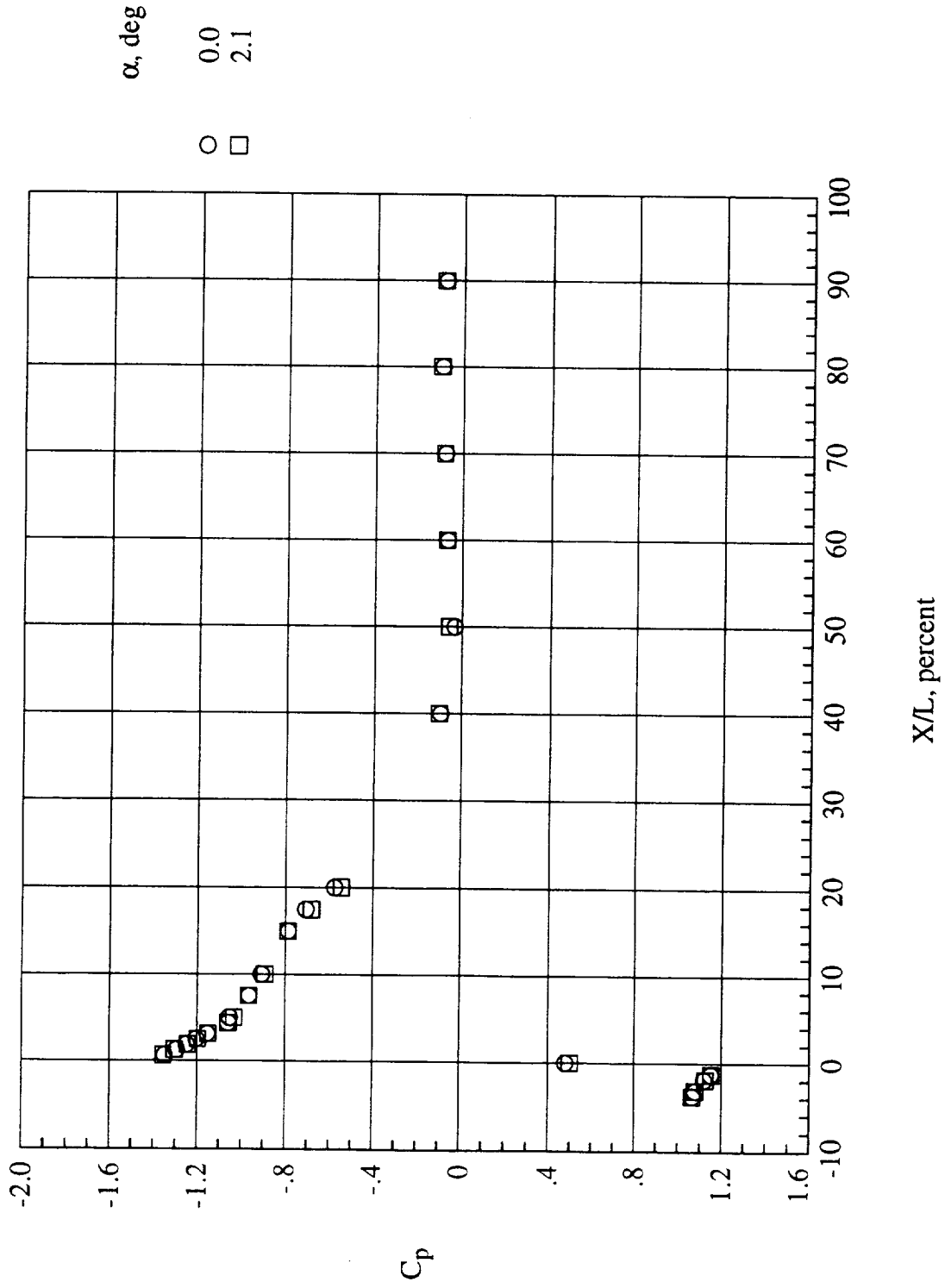
(c) $M = 0.84$ and $mfr = 0.95$.

Figure 7.- Continued.



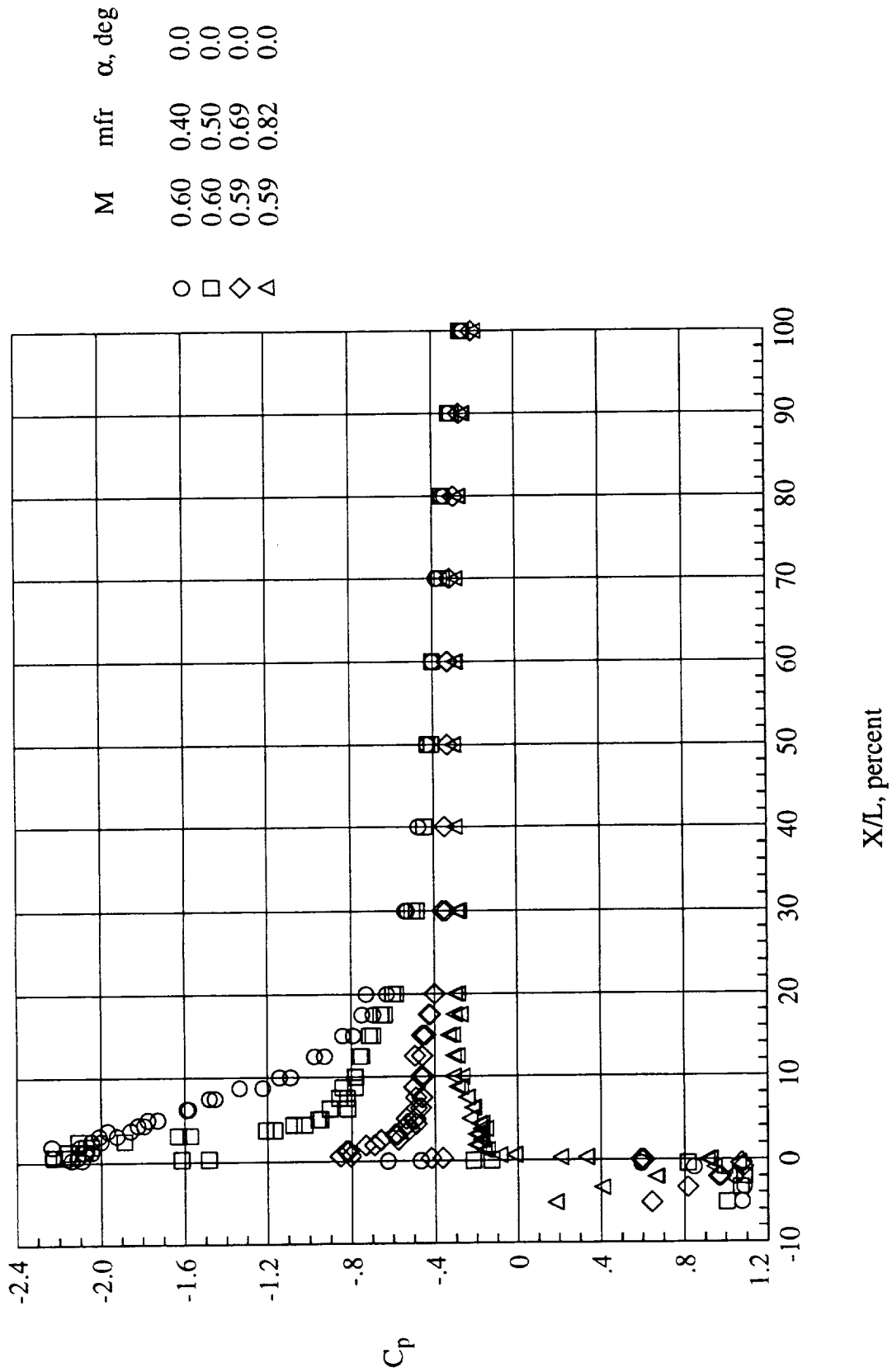
(d) $M = 0.87$ and $mfr = 0.57$.

Figure 7.- Continued.



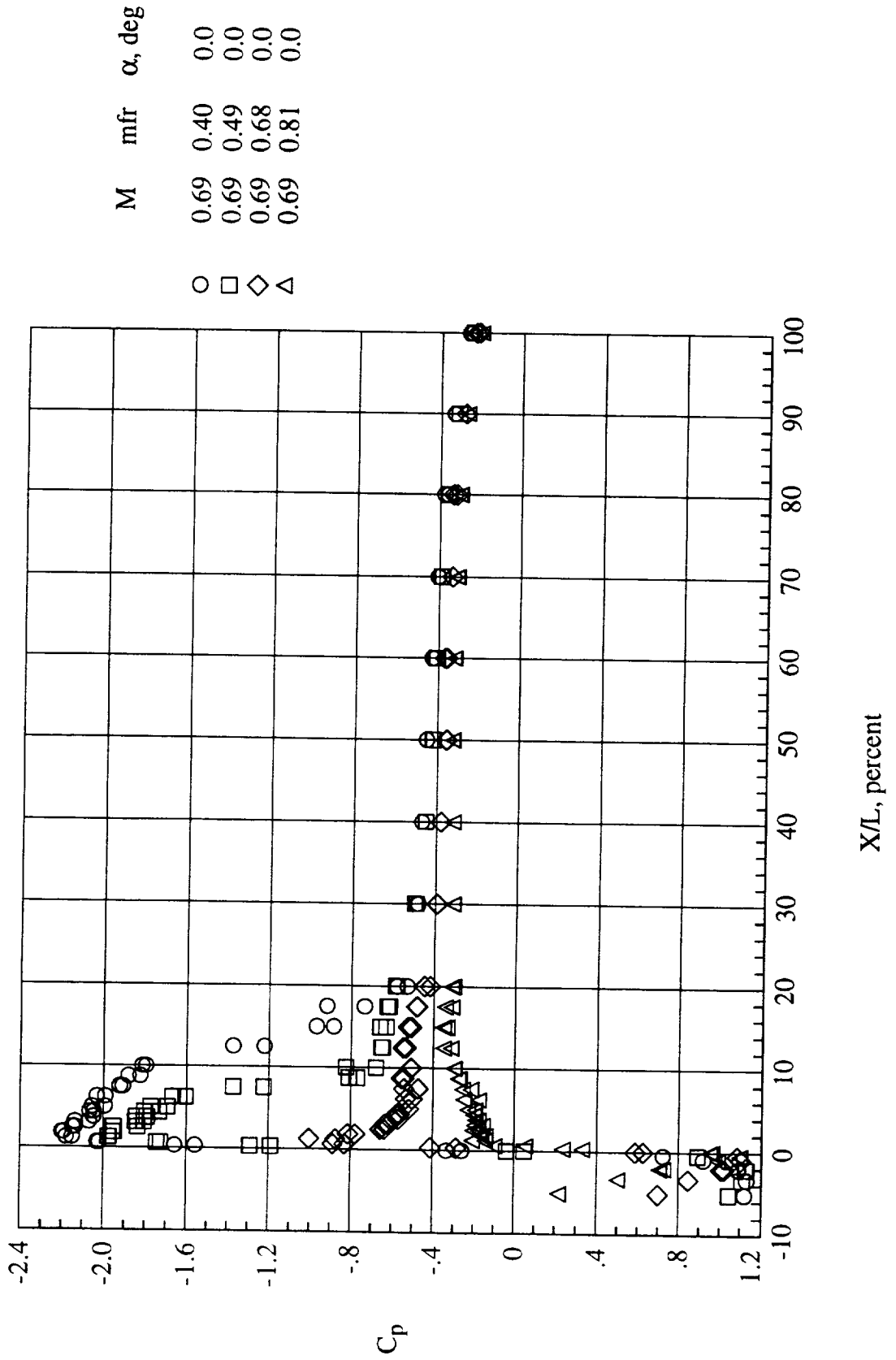
(e) $M = 0.89$ and $mfr = 0.57$.

Figure 7.- Concluded.



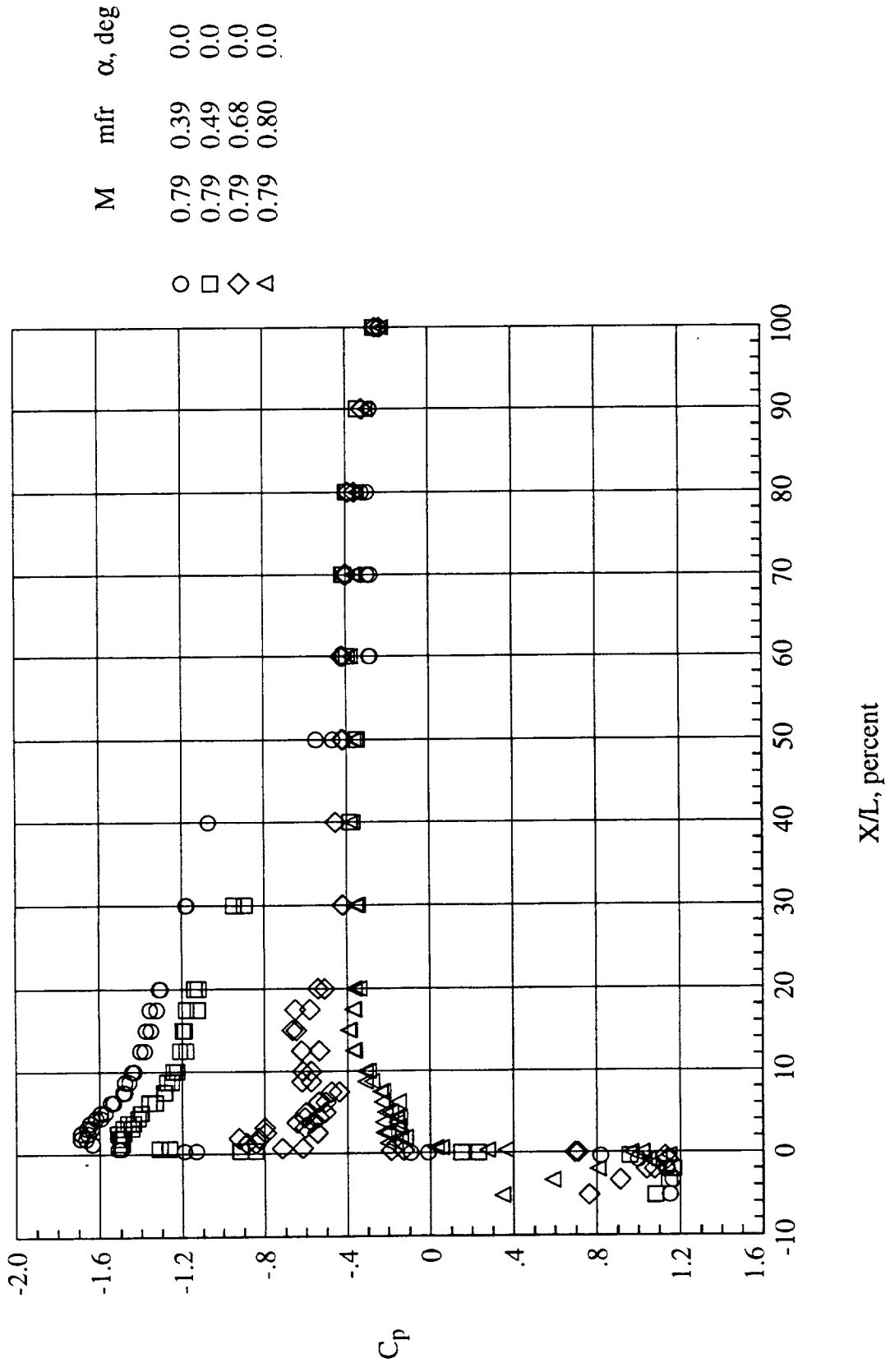
(a) $M = 0.60$.

Figure 8.- Pressure coefficient variation with X/L for the NACA 1-85-43.9 inlet with a contraction ratio of 1.250 for several mass-flow ratios at $\alpha = 0^\circ$. Data combined from $\phi = 0^\circ$ and 180° meridians.



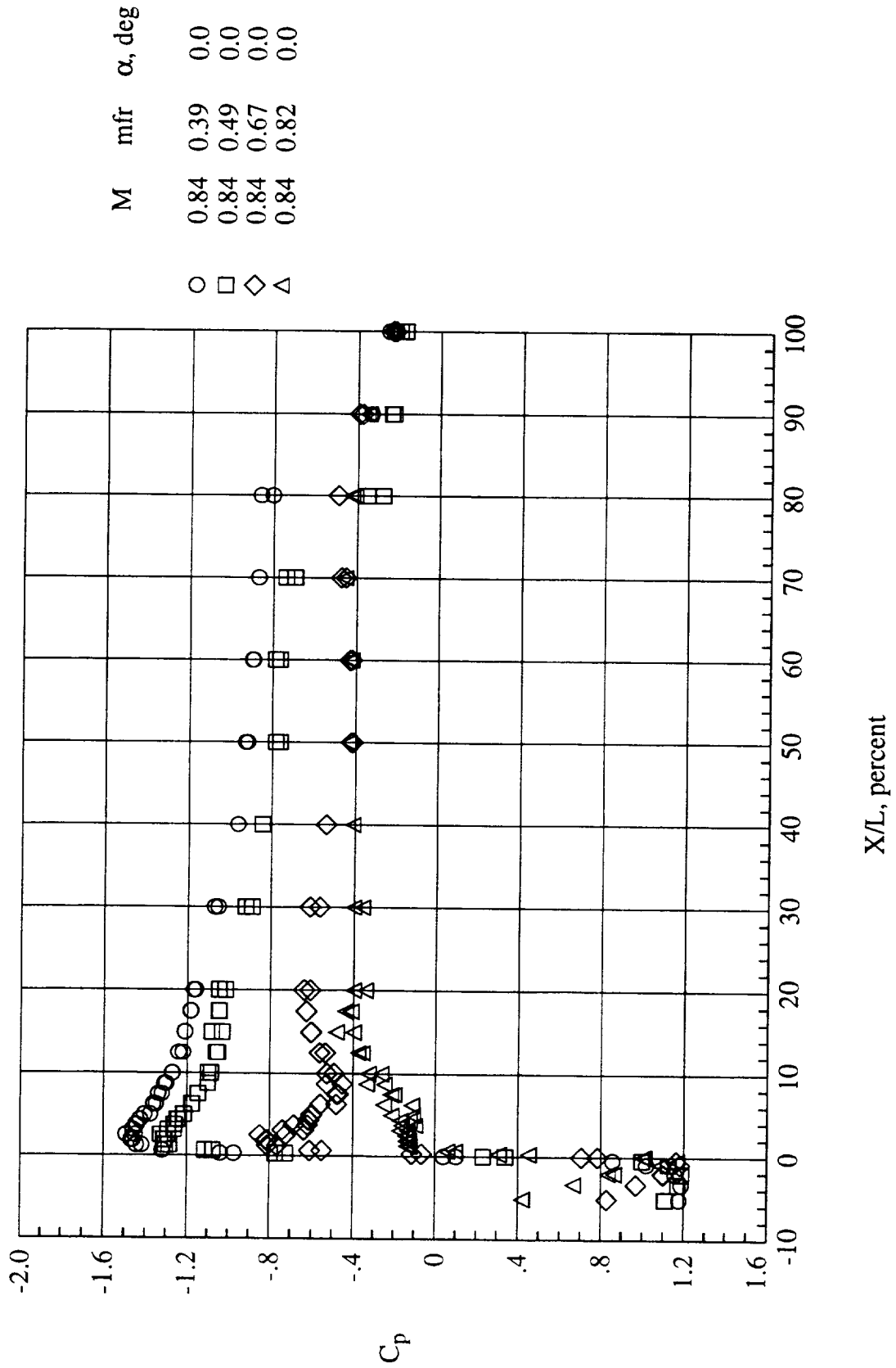
(b) $M = 0.69$.

Figure 8.- Continued.



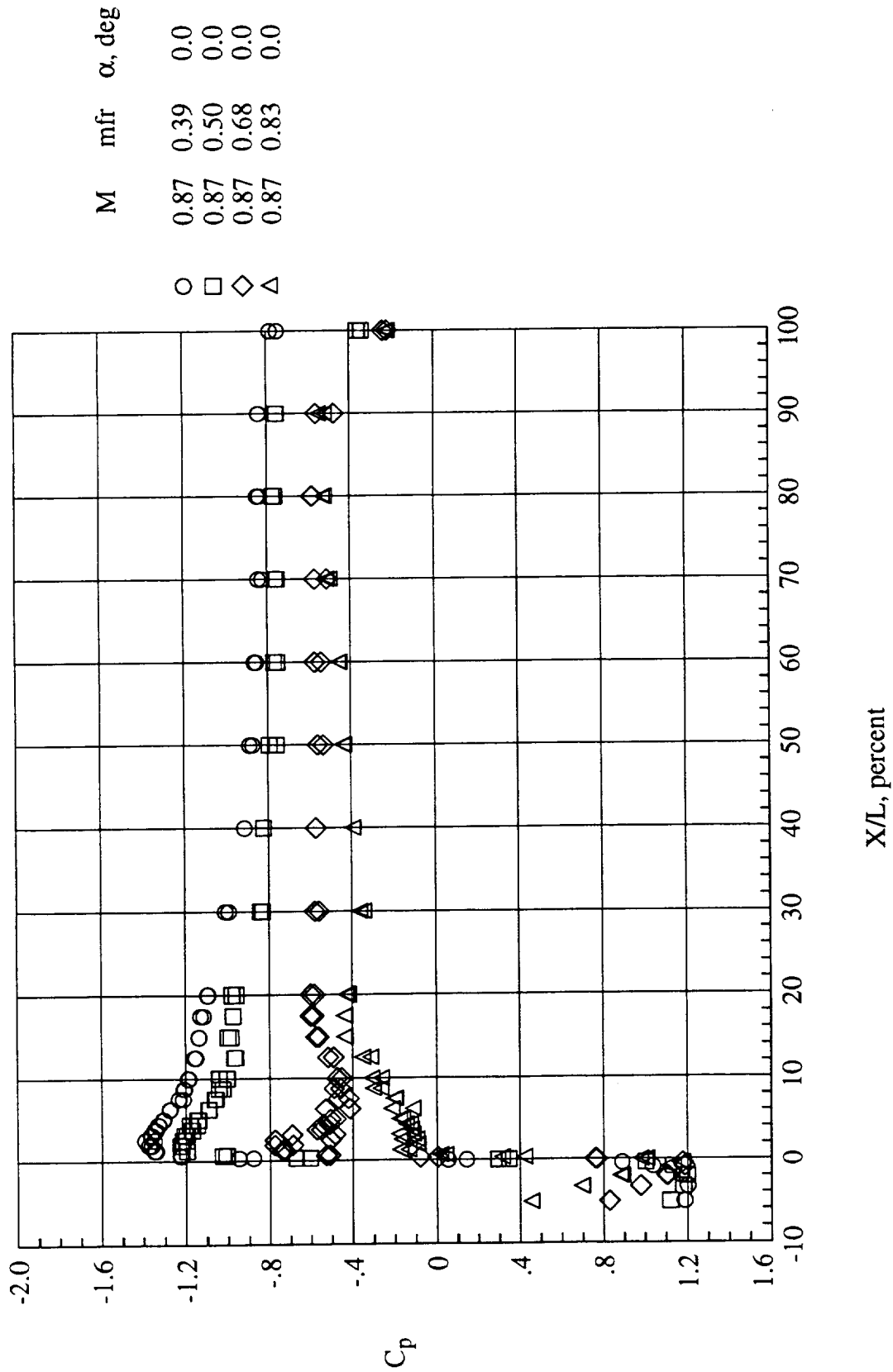
(c) $M = 0.79$.

Figure 8.- Continued.



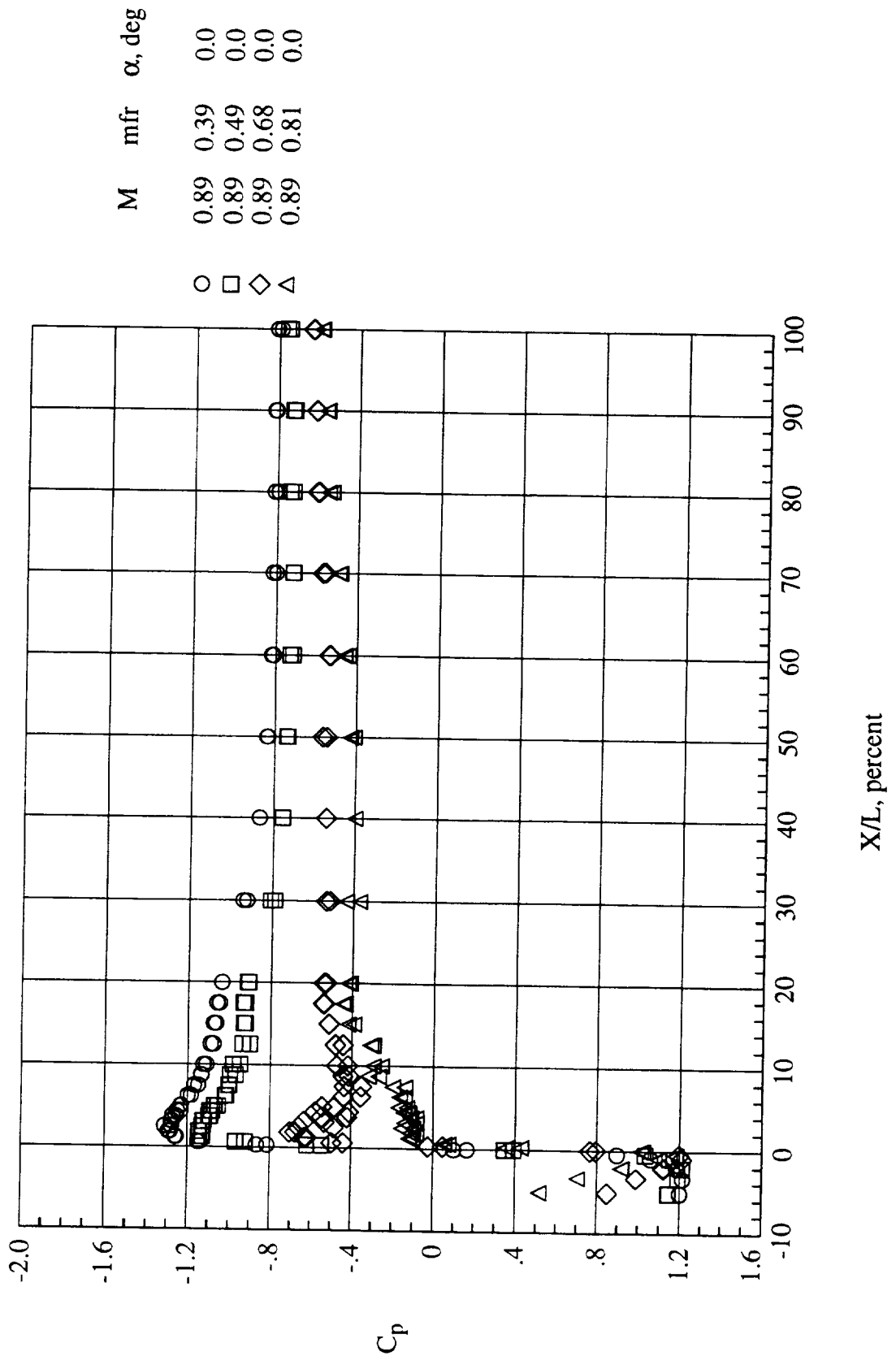
(d) $M = 0.84$.

Figure 8.- Continued.

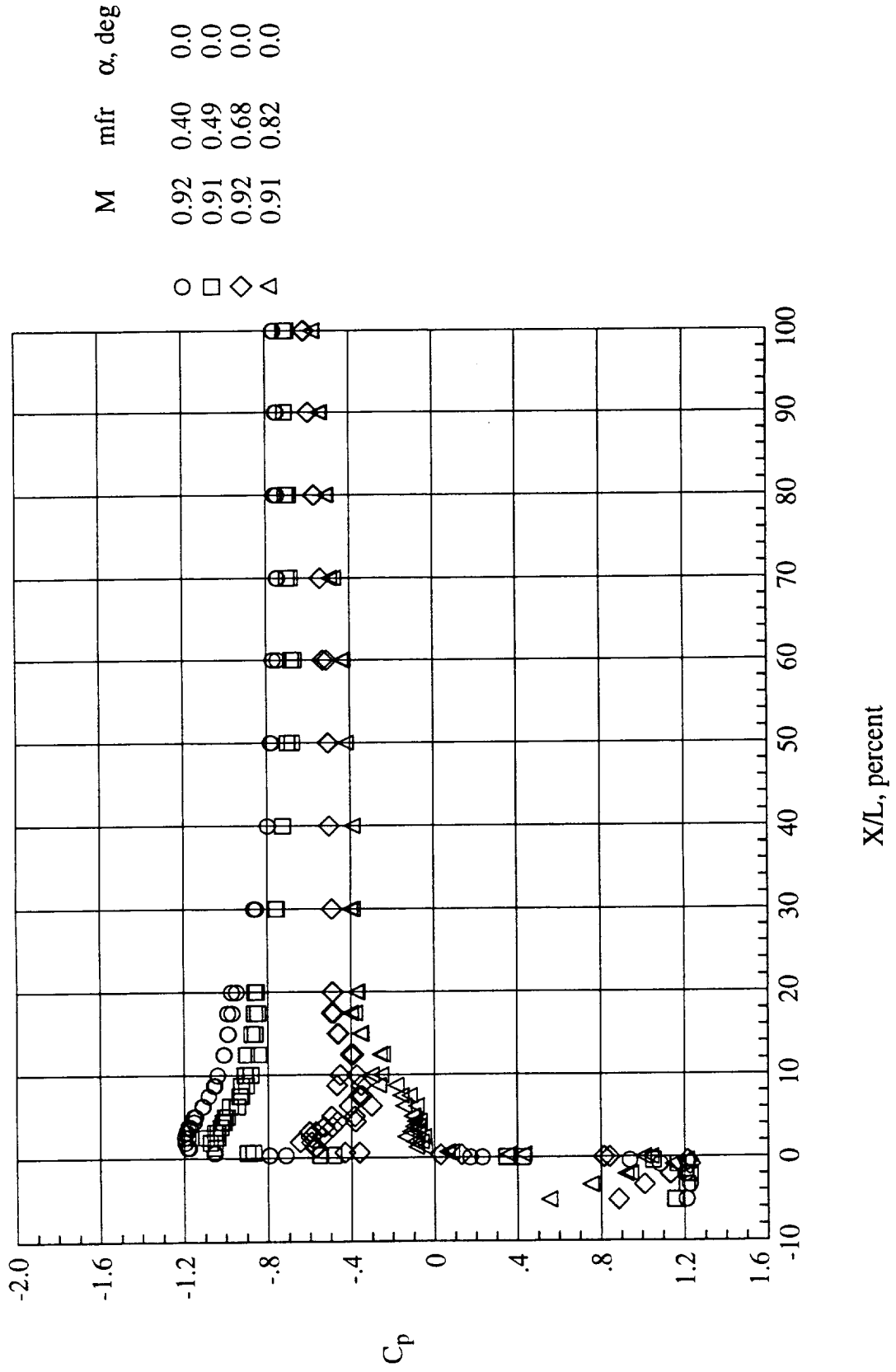


(e) $M = 0.87$.

Figure 8. - Continued.

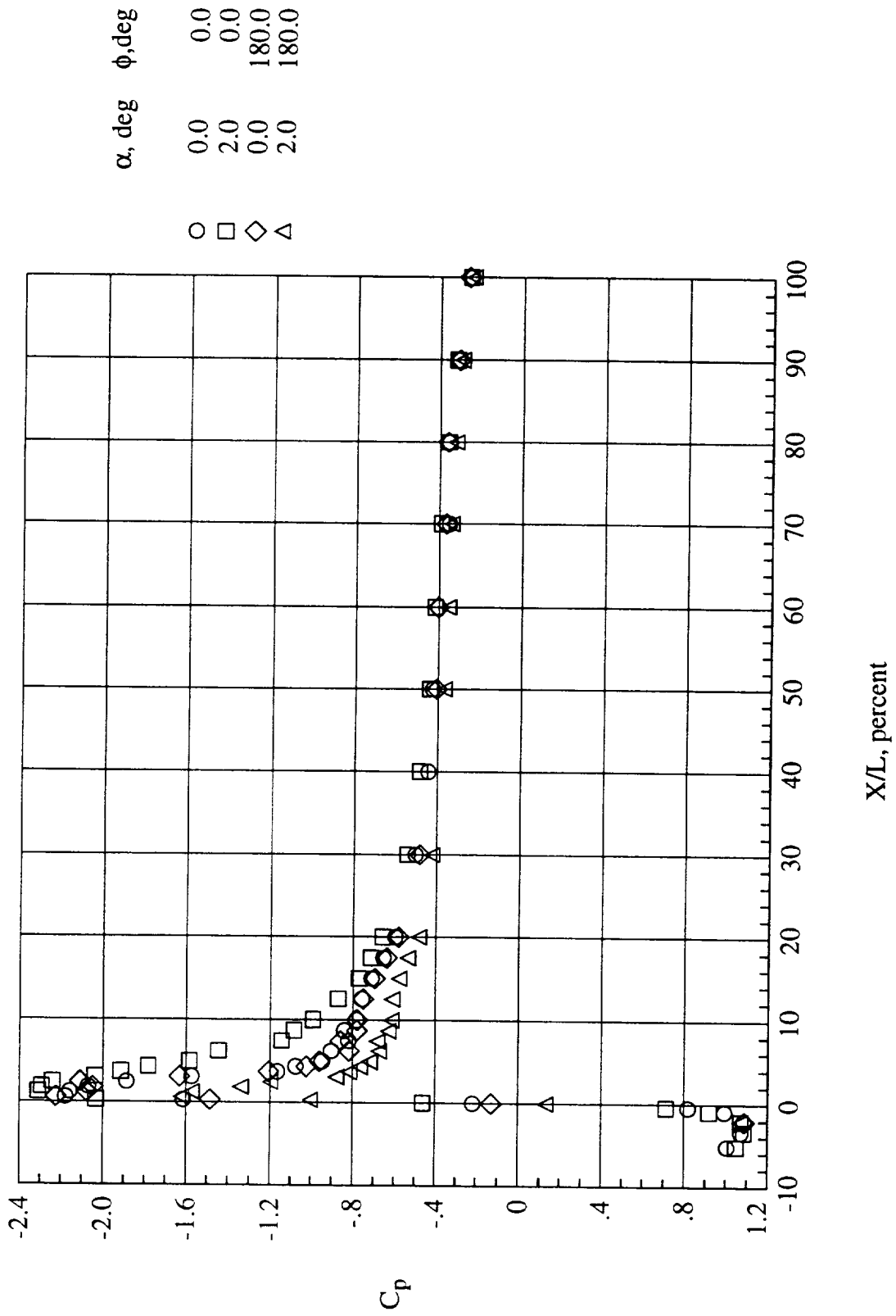


(f) $M = 0.89$.
Figure 8.- Continued.



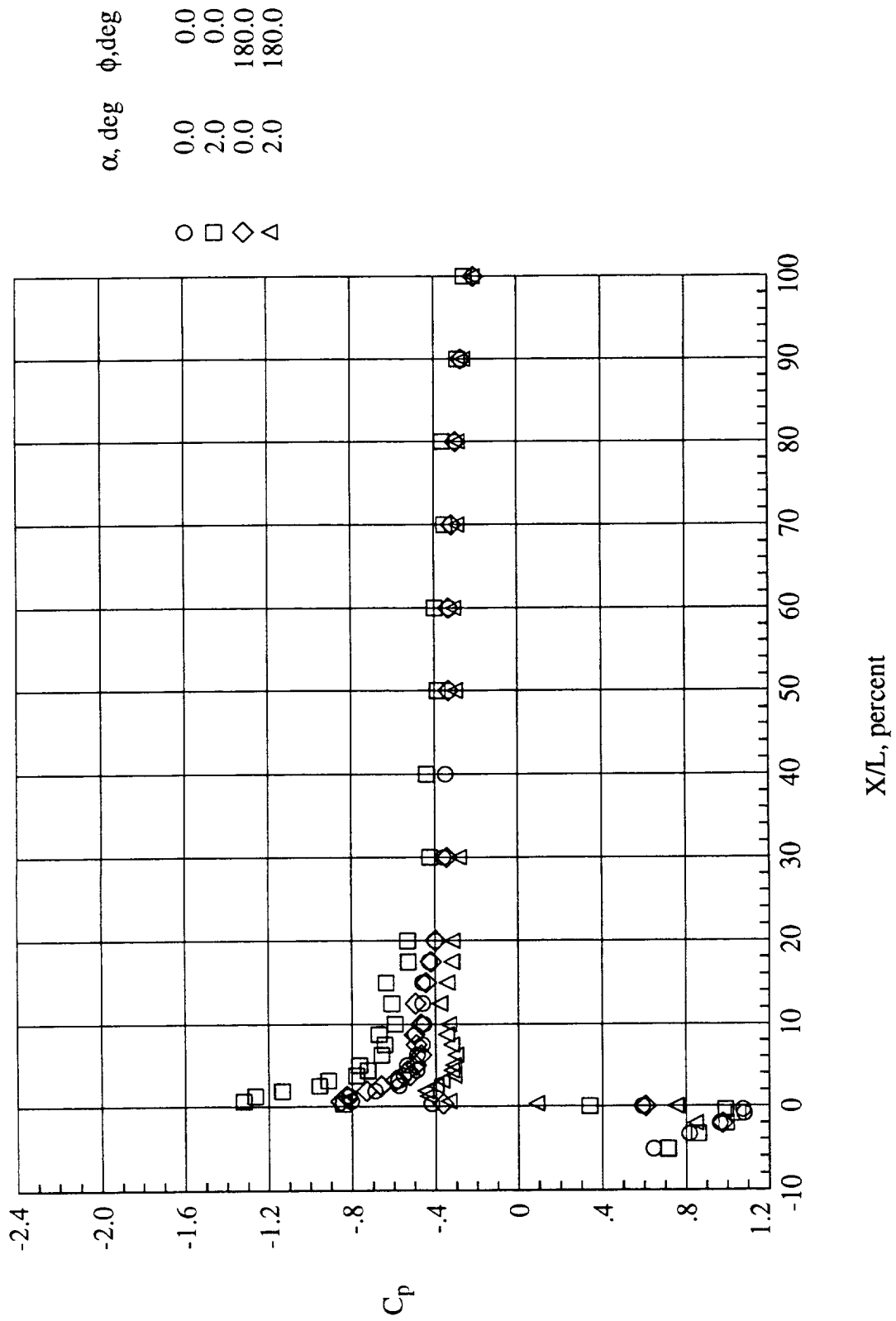
(g) $M = 0.92$.

Figure 8.- Concluded.



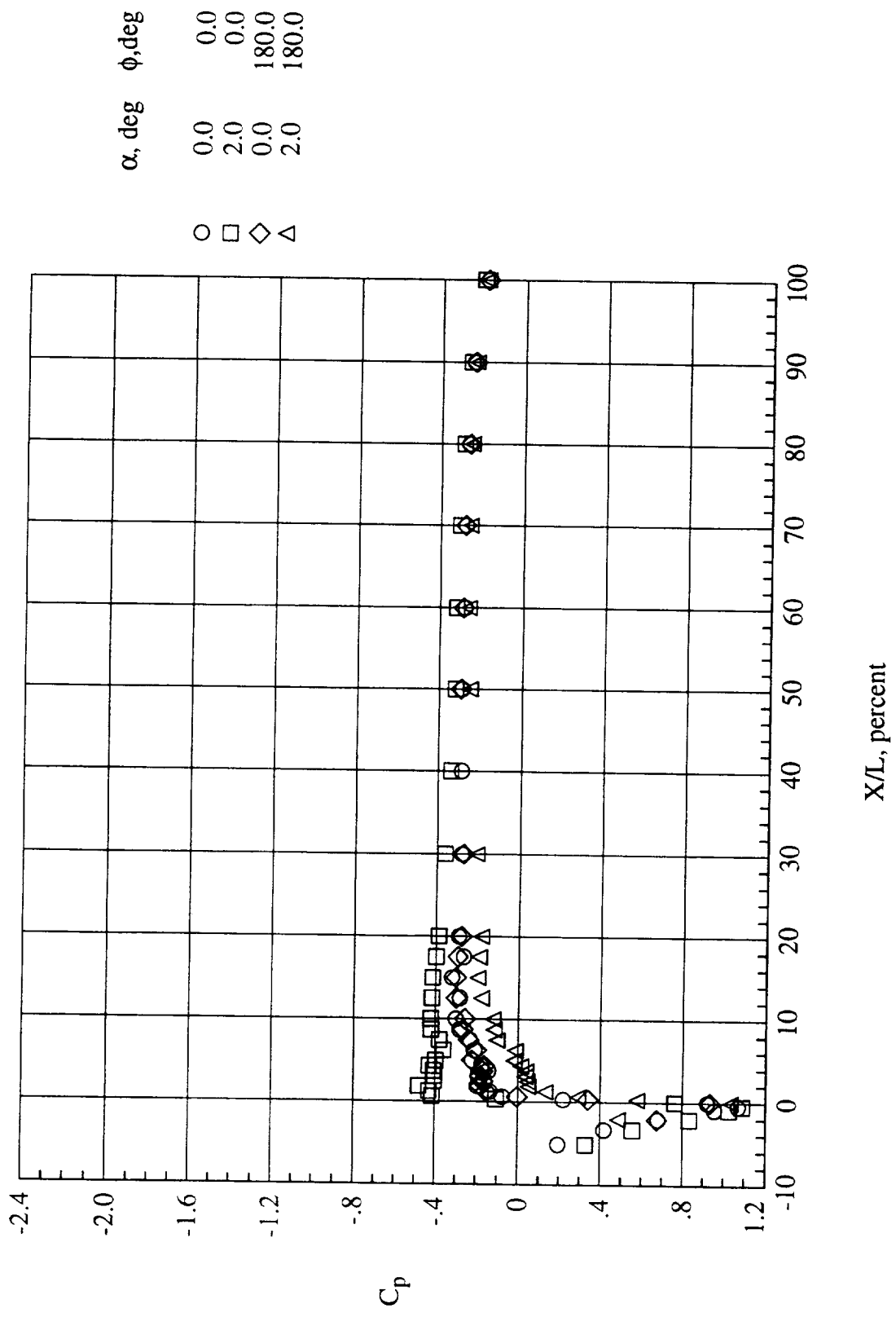
(a) $M = 0.60$ and $mfr = 0.50$.

Figure 9.- Pressure coefficient variation with X/L along the $\phi = 0^\circ$, and 180° meridians for the NACA 1-85-43.9 inlet with a contraction ratio of 1.750 at two angles of attack



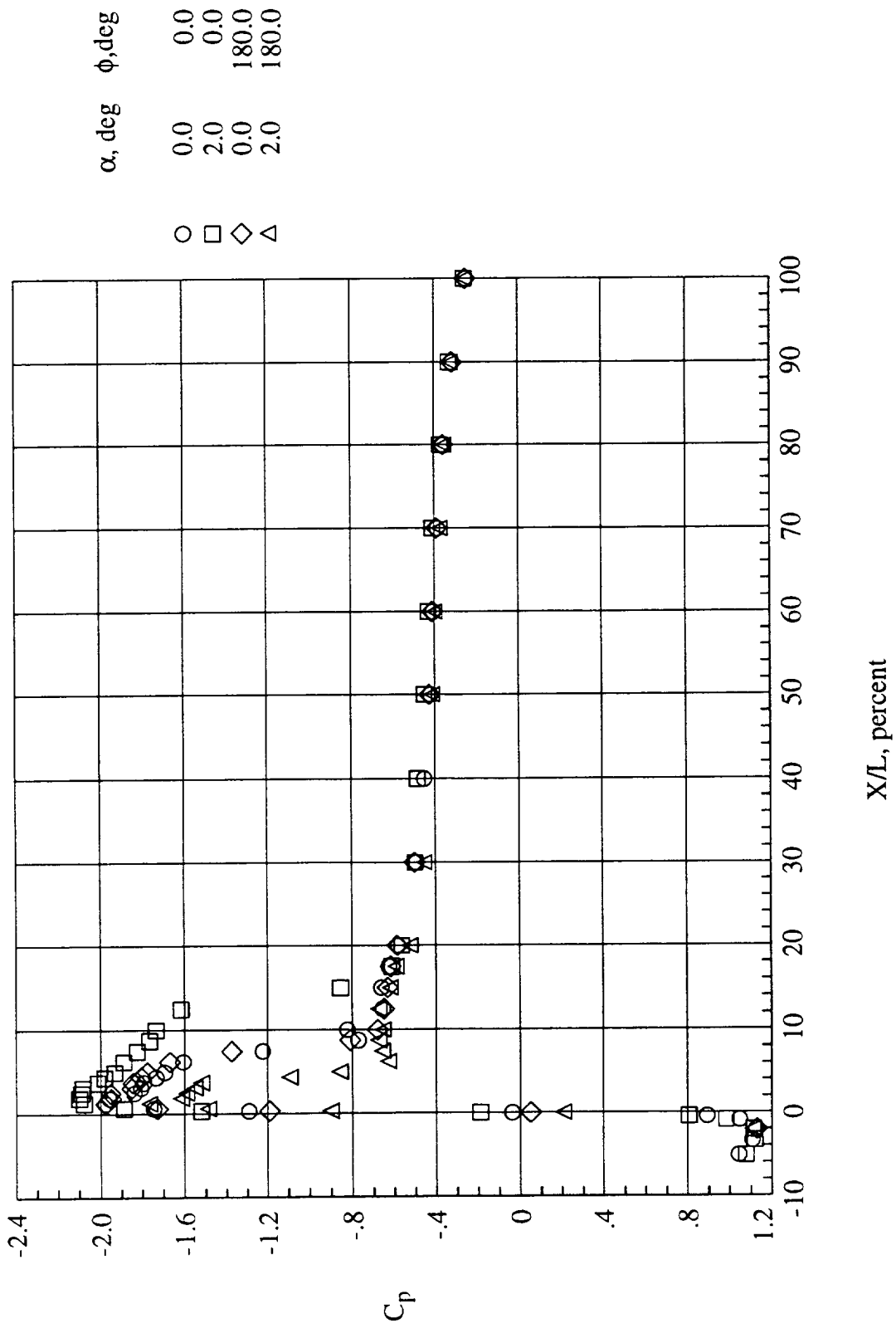
(b) $M = 0.59$ and $mfr = 0.69$.

Figure 9.- Continued.



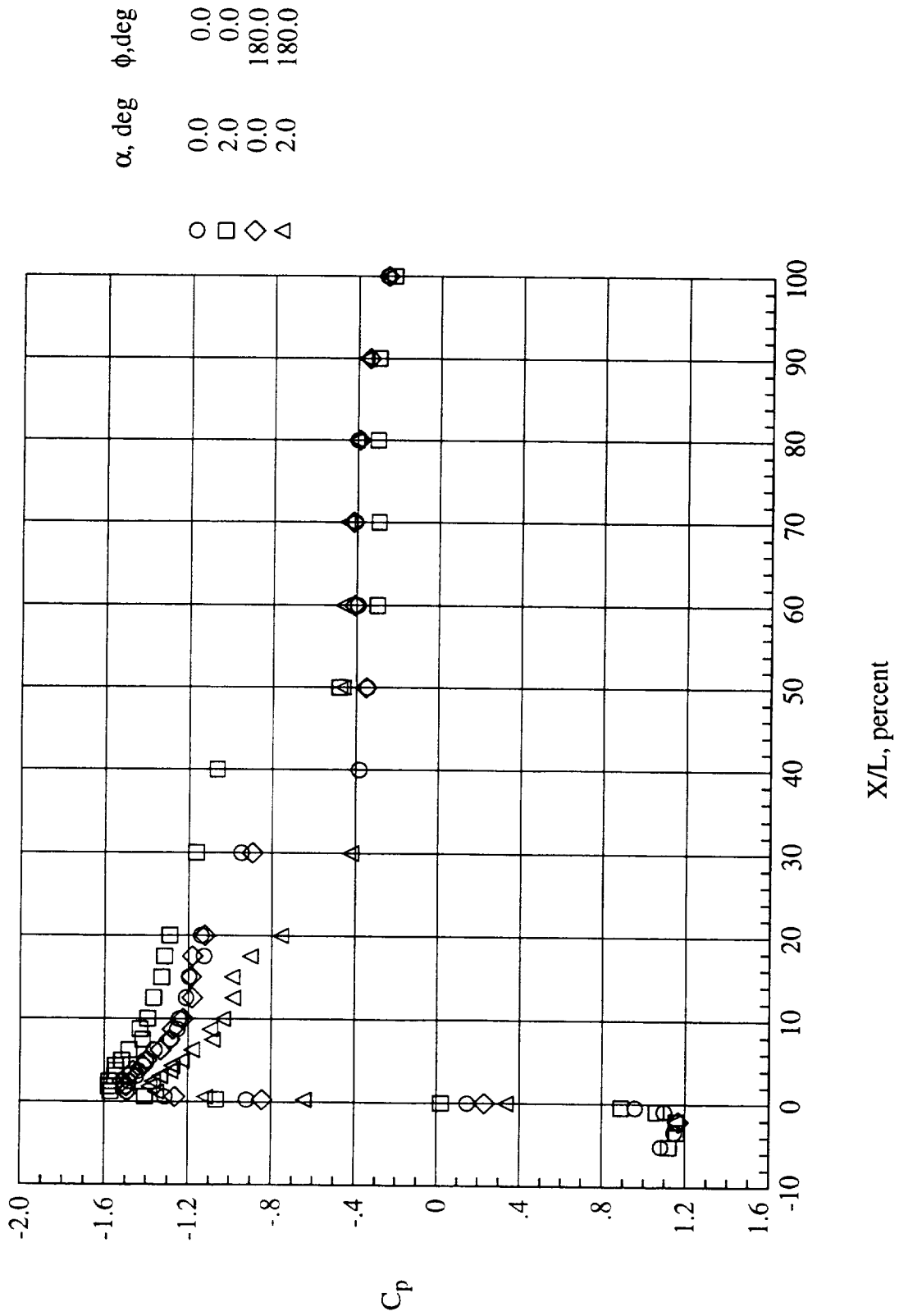
(c) $M = 0.59$ and $mfr = 0.82$.

Figure 9.- Continued.



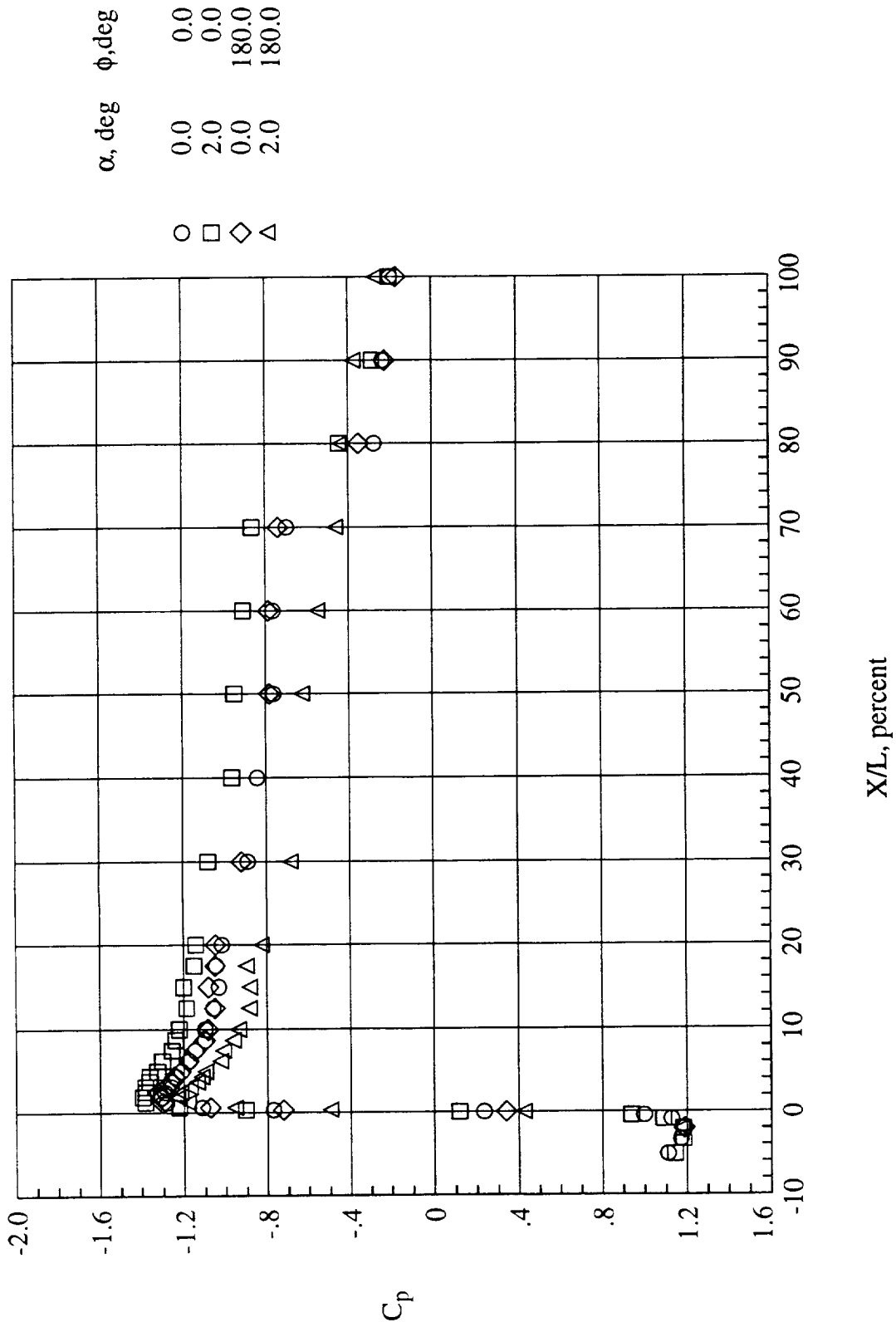
(d) $M = 0.69$ and $mfr = 0.49$.

Figure 9. - Continued.



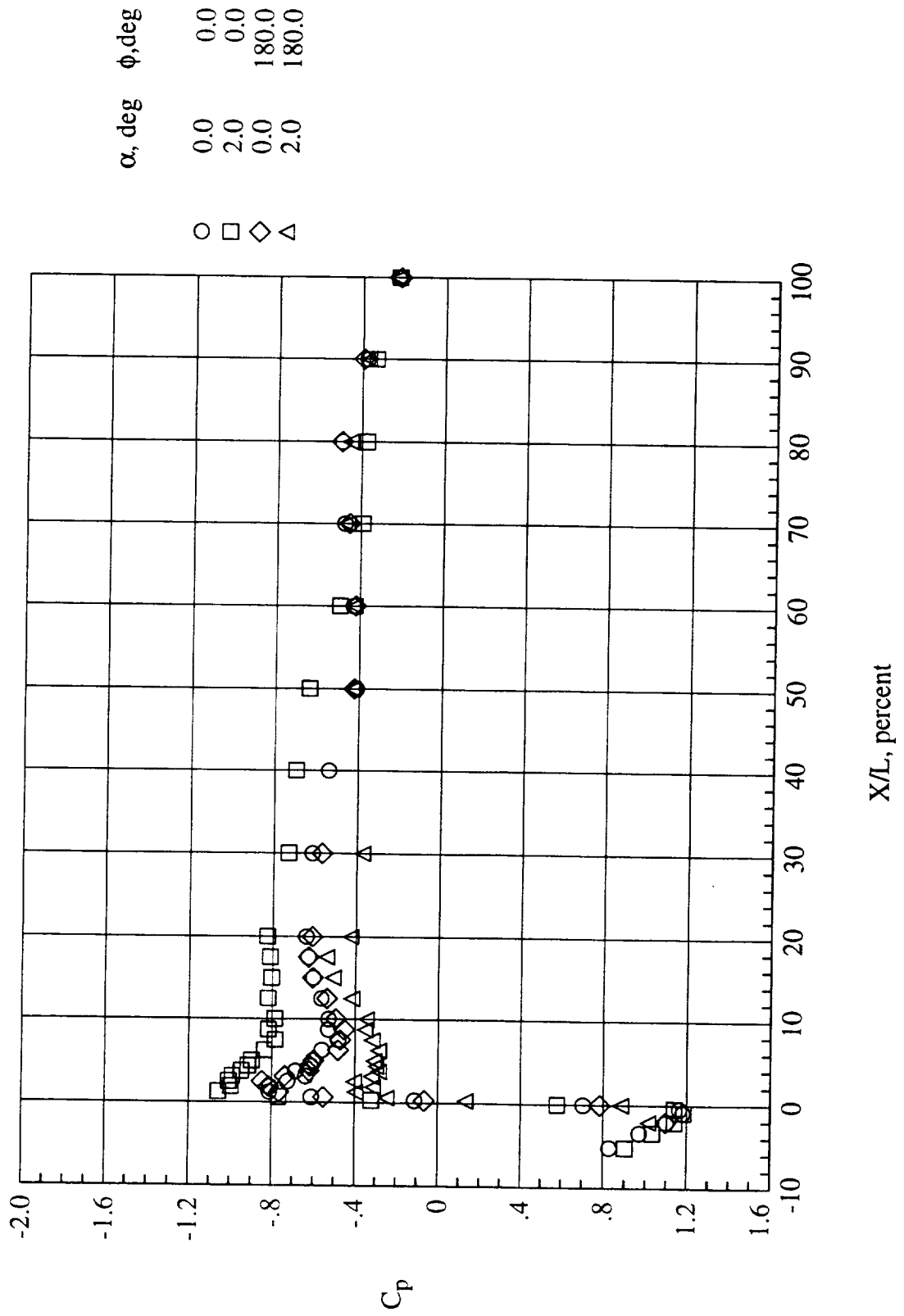
(e) $M = 0.79$ and $mfr = 0.49$.

Figure 9.- Continued.



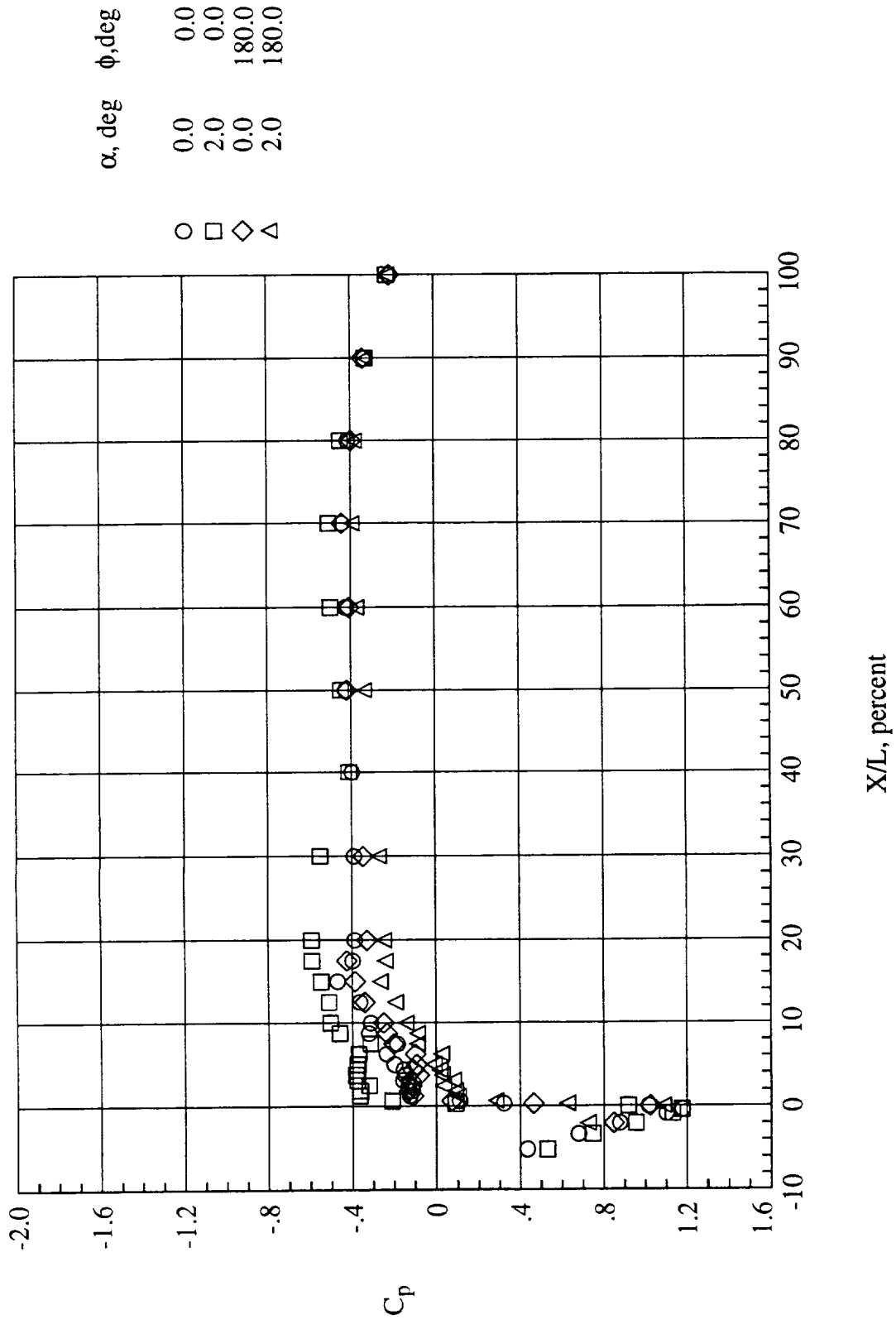
(f) $M = 0.84$ and $mfr = 0.49$.

Figure 9.- Continued.



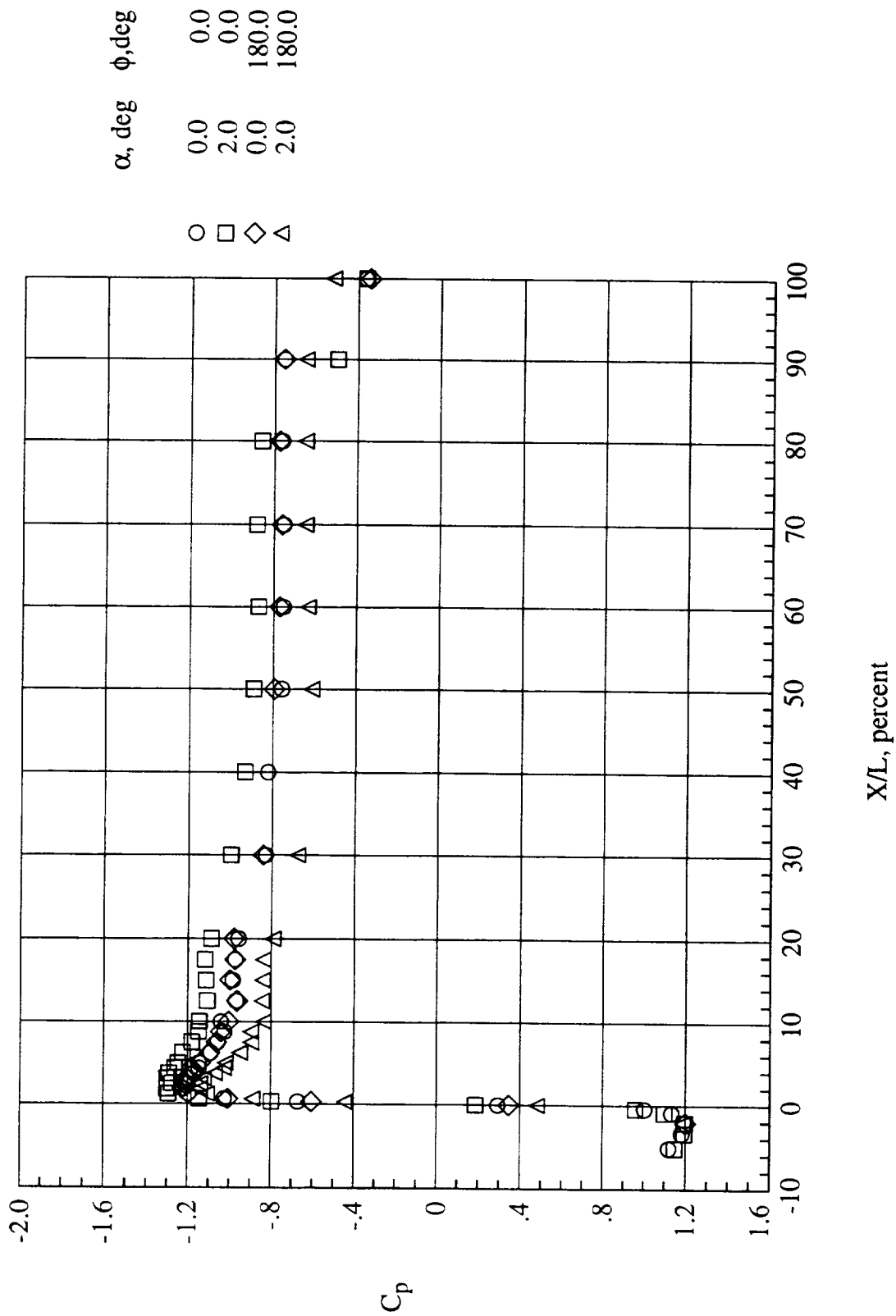
(g) $M = 0.84$ and $mfr = 0.67$.

Figure 9.- Continued.



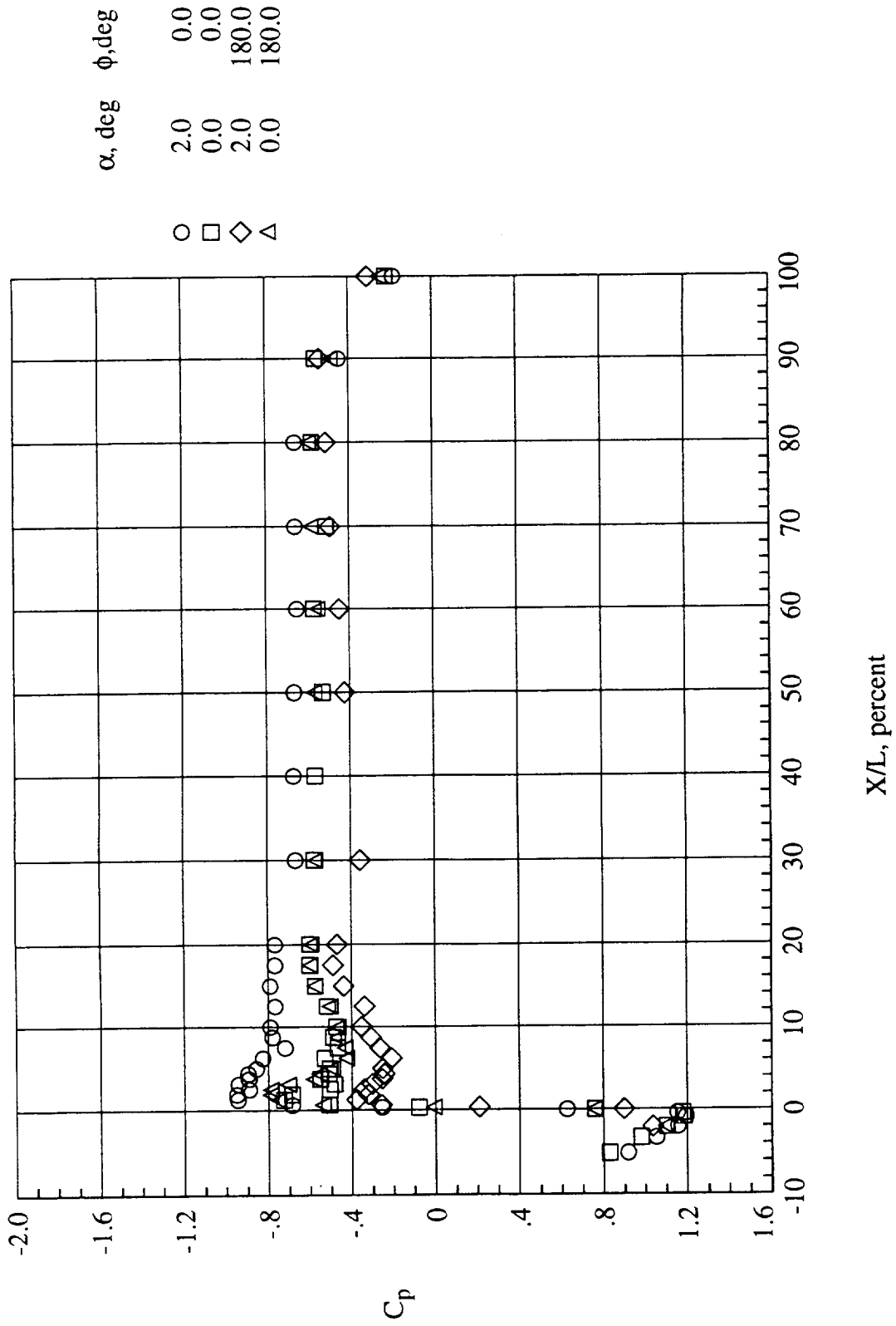
(h) $M = 0.84$ and $mfr = 0.83$.

Figure 9. - Continued.



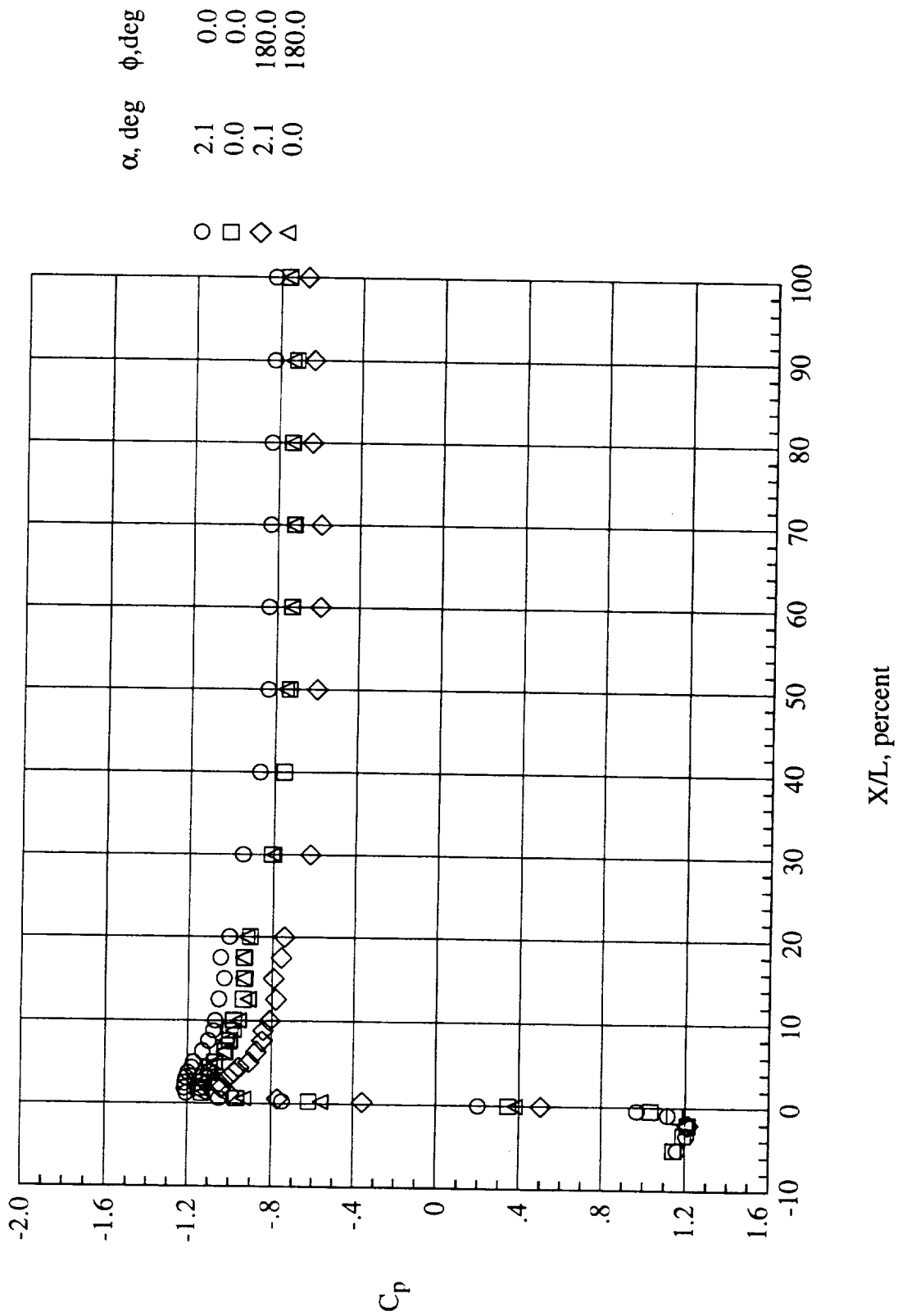
(i) $M = 0.87$ and $mfr = 0.49$.

Figure 9.- Continued.



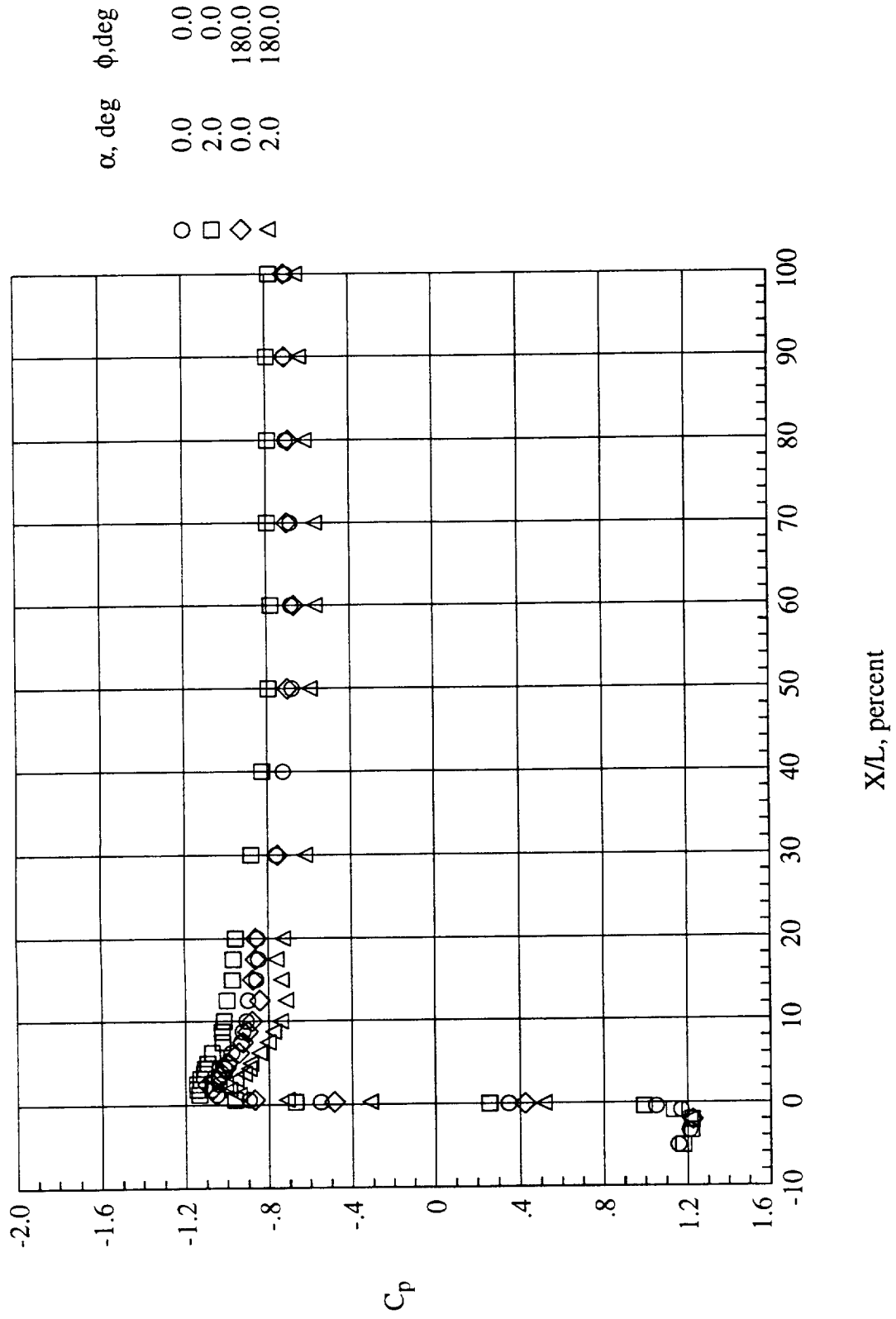
(j) $M = 0.87$ and $mfr = 0.67$.

Figure 9.- Continued.



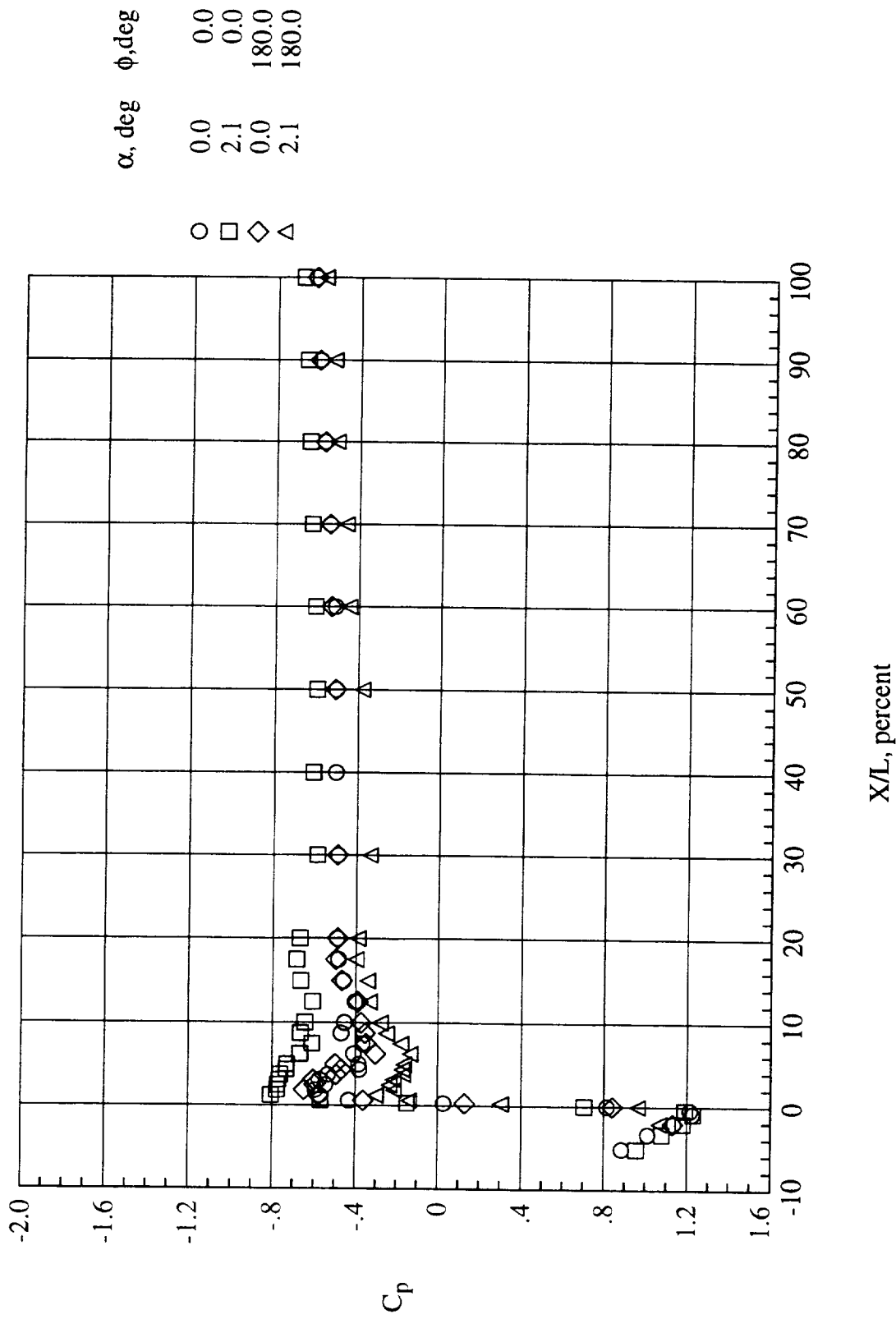
(k) $M = 0.89$ and $mfr = 0.49$.

Figure 9.- Continued.



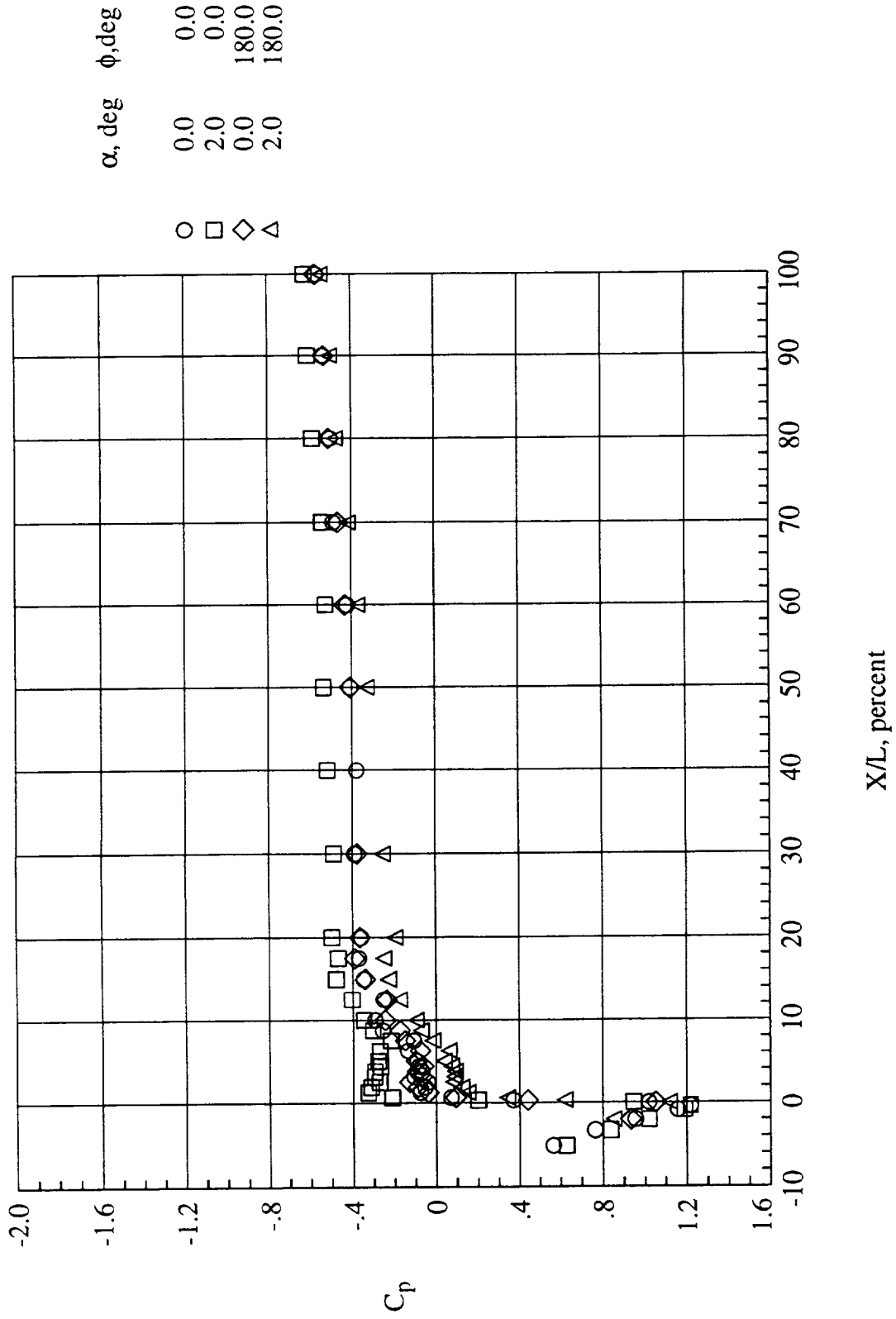
(1) $M = 0.92$ and $mfr = 0.49$.

Figure 9.- Continued.



(m) $M = 0.92$ and $mfr = 0.68$.

Figure 9.- Continued.



(n) $M = 0.92$ and $mfr = 0.82$.

Figure 9.- Concluded.

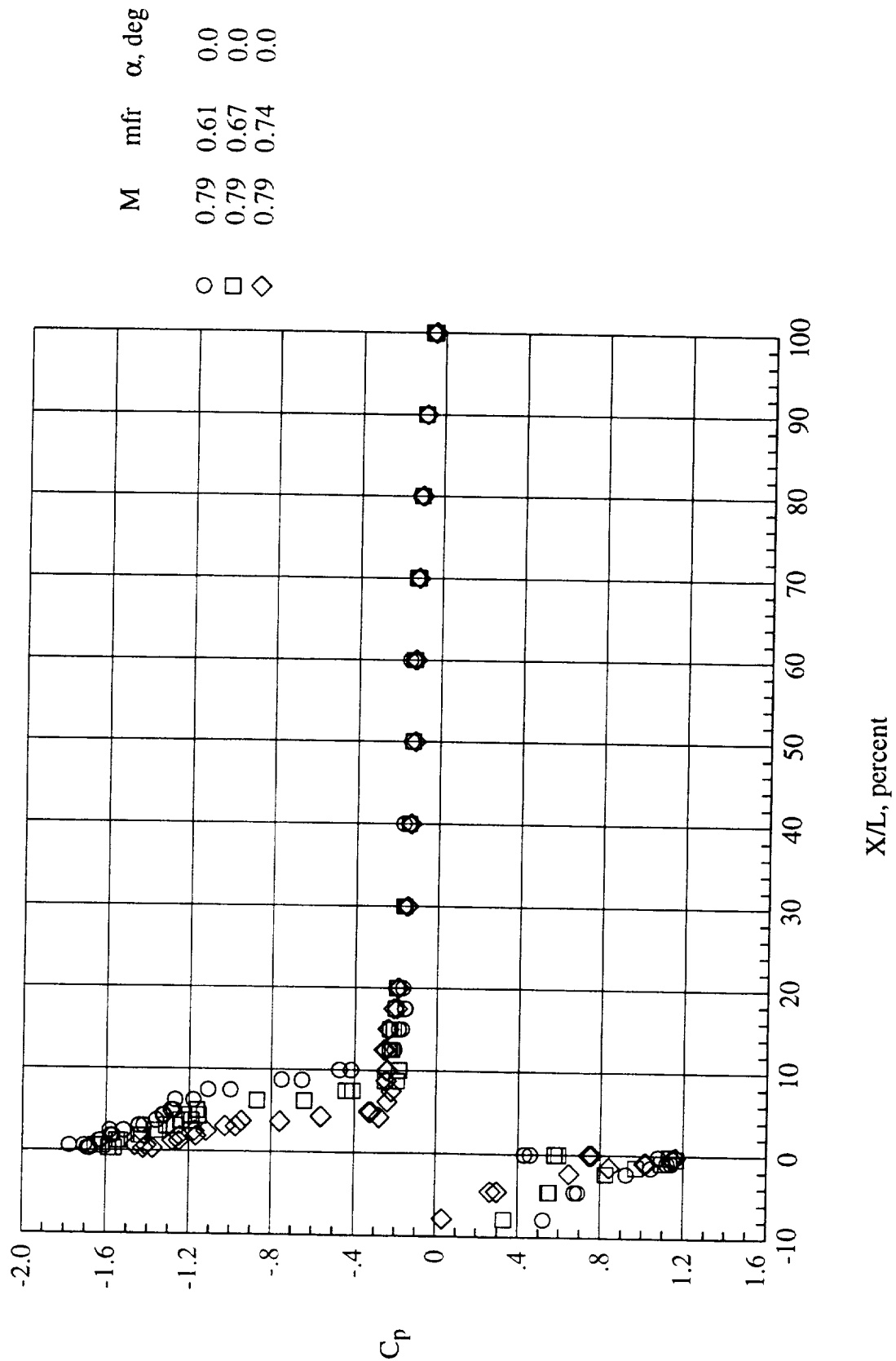
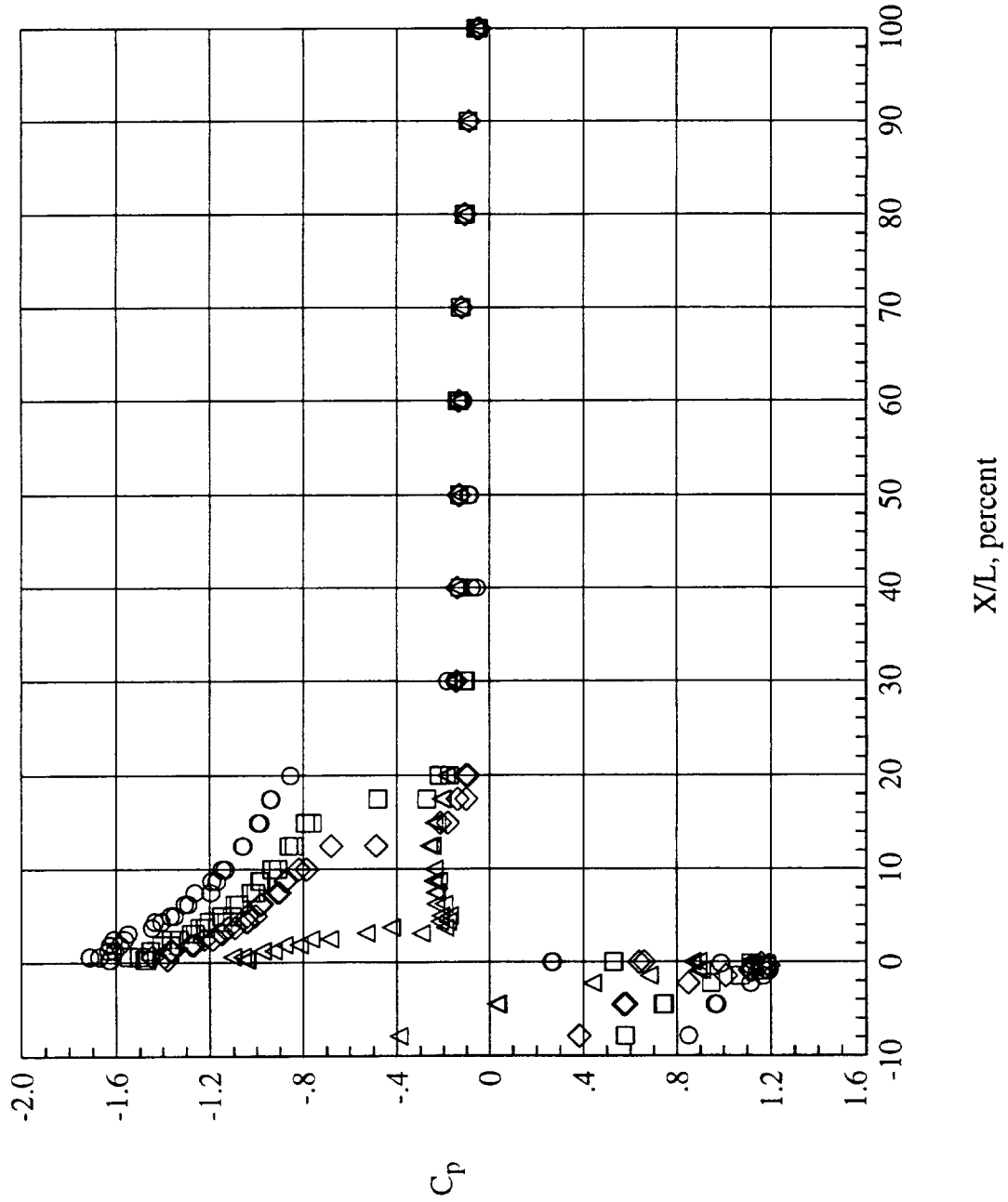
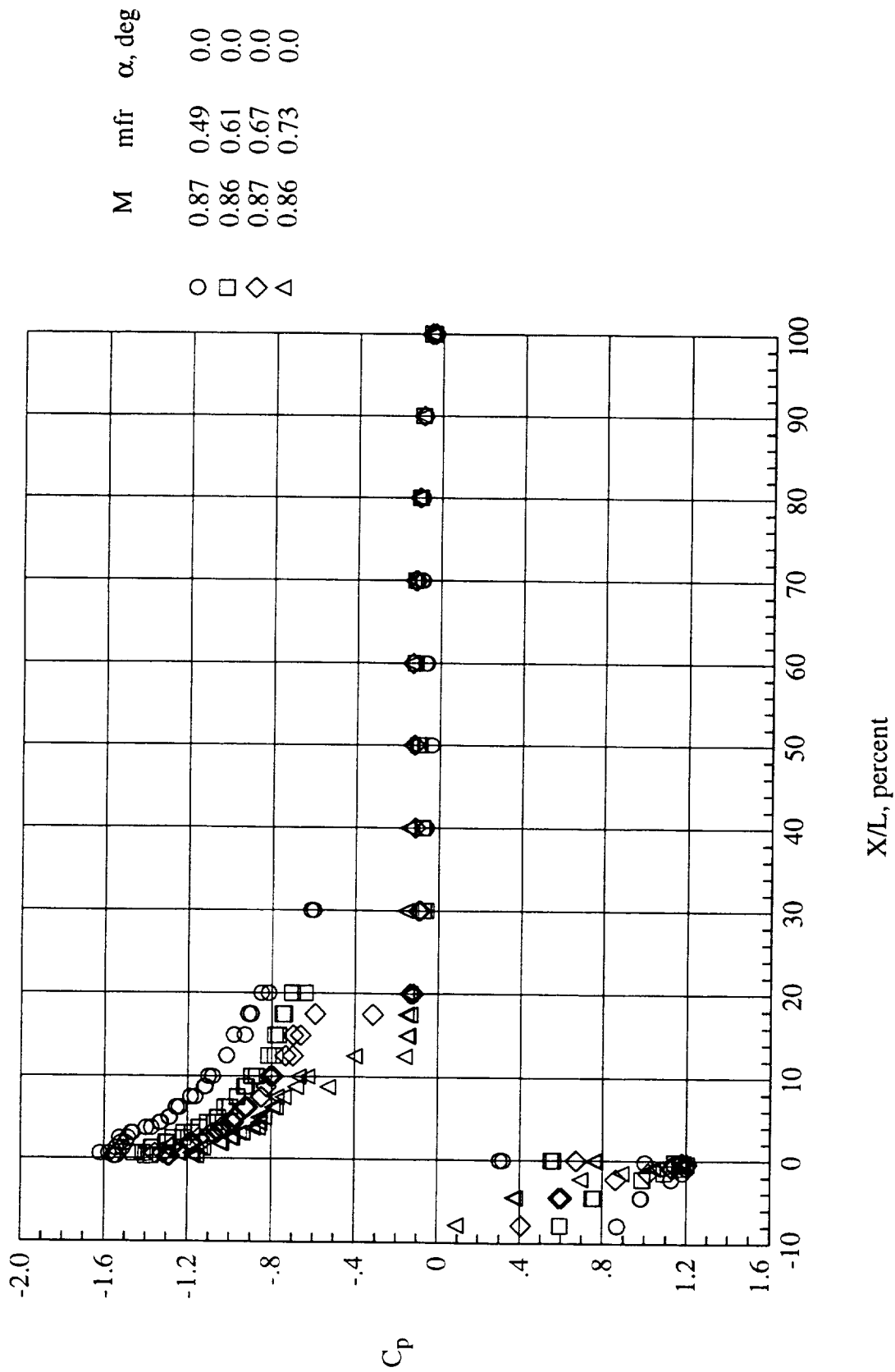


Figure 10.- Pressure coefficient variation with X/L for the NACA 1-85-100 inlet with a contraction ratio of 1.250 for several mass-flow rates at $\alpha = 0^\circ$. Data combined from $\delta = 0^\circ$ and 180° meridians.

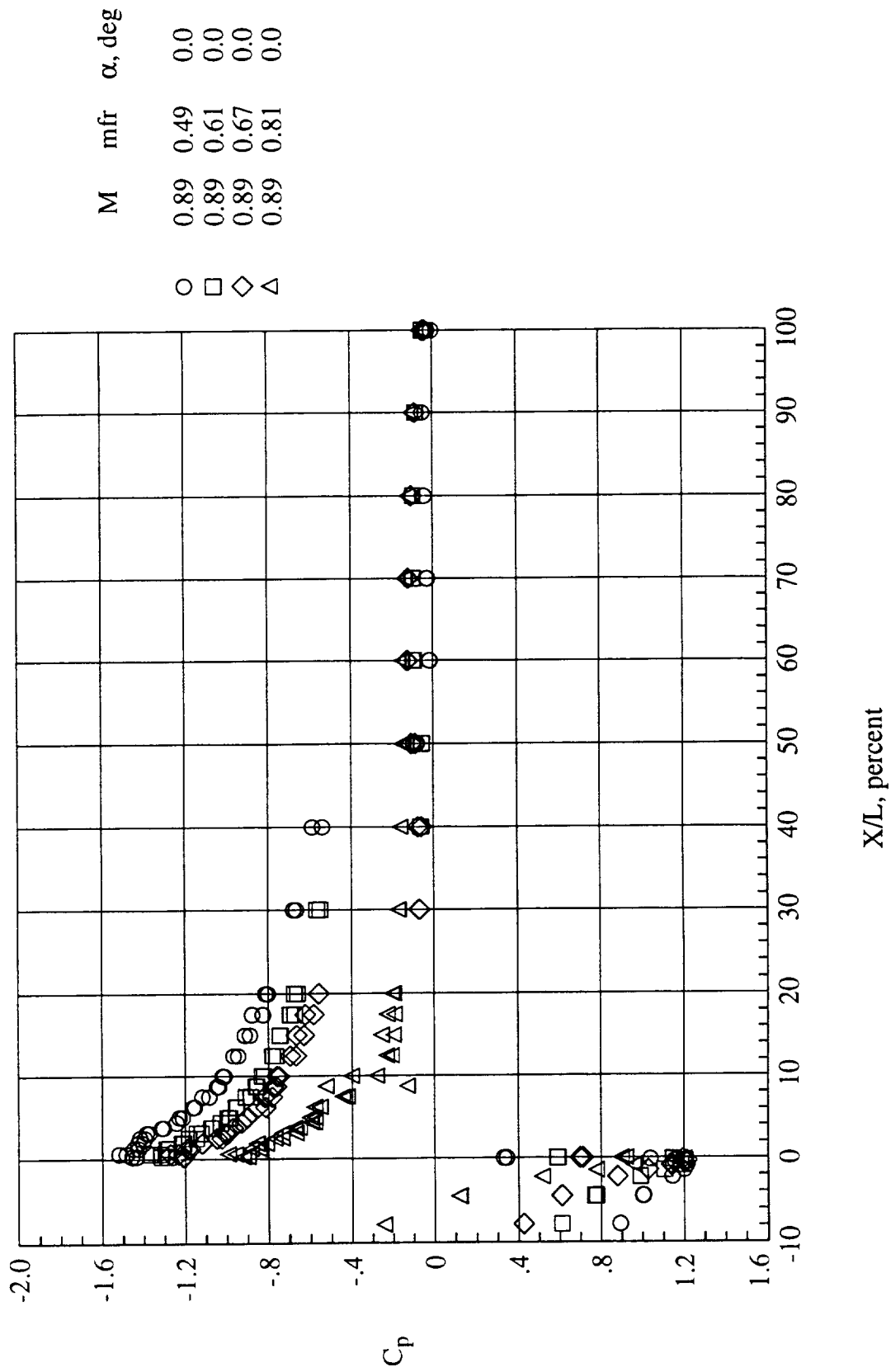


(b) $M = 0.84$.

Figure 10.- Continued.

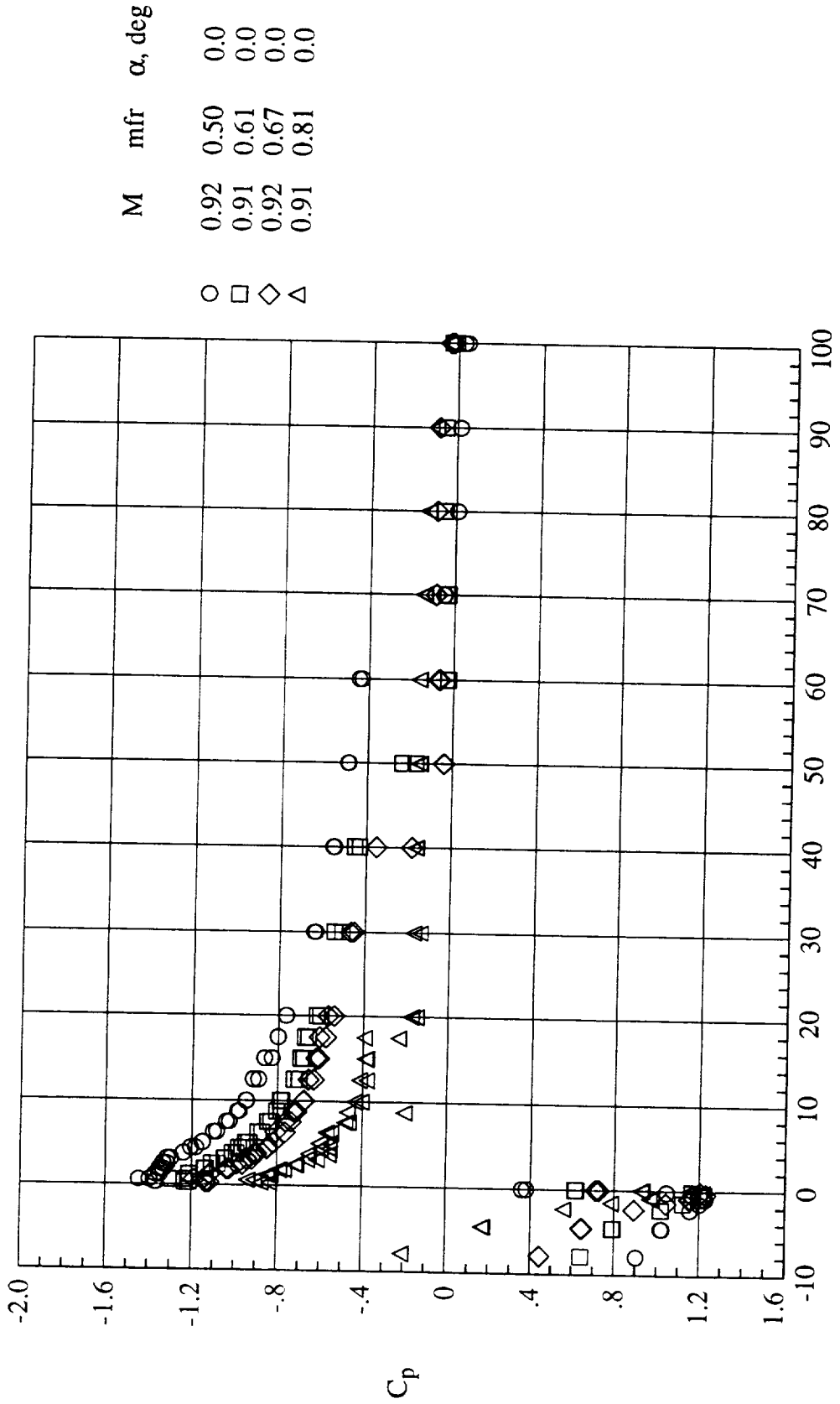


(c) $M = 0.87$.
Figure 10.- Continued.



(d) $M = 0.89$.

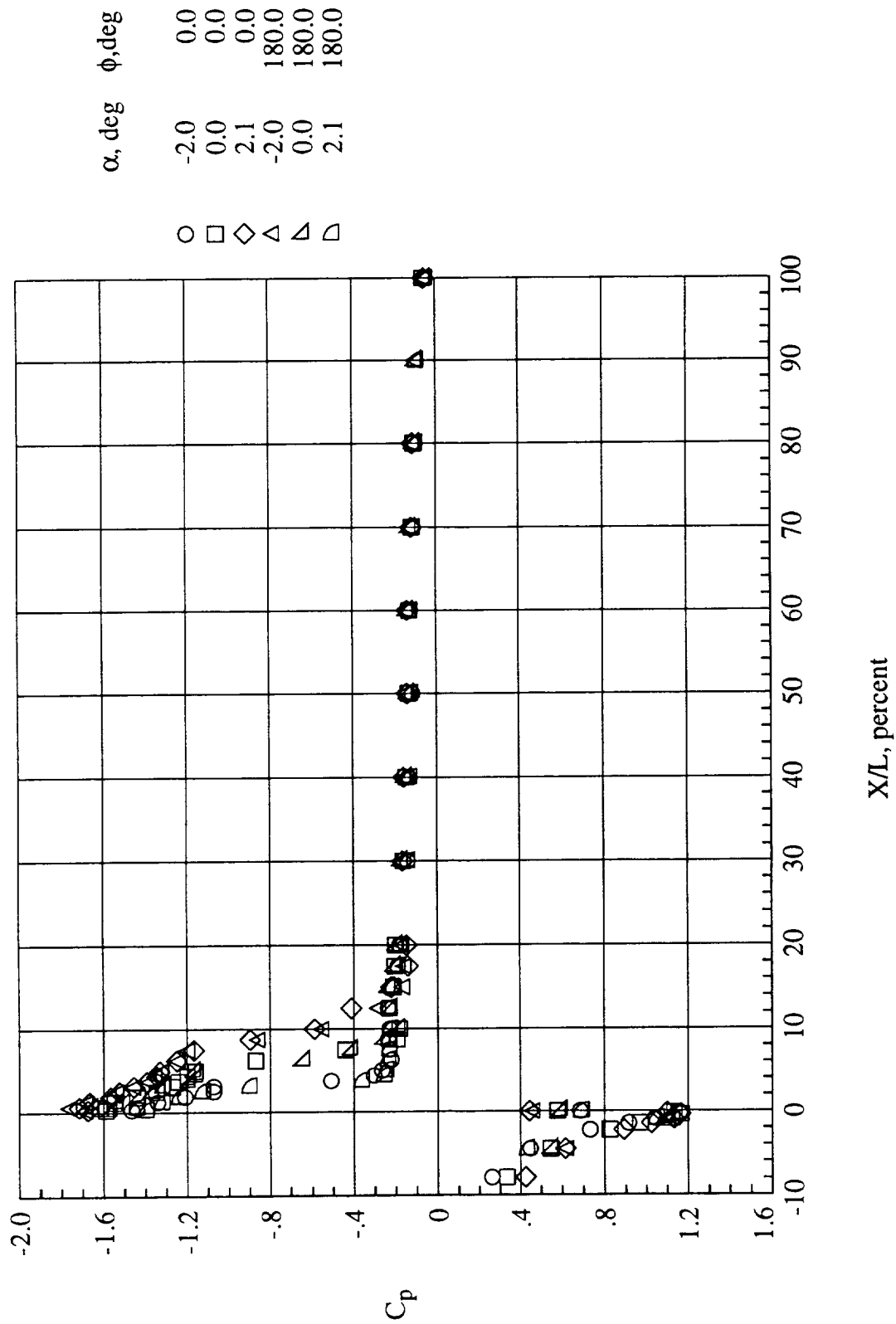
Figure 10.- Continued.



X/L, percent

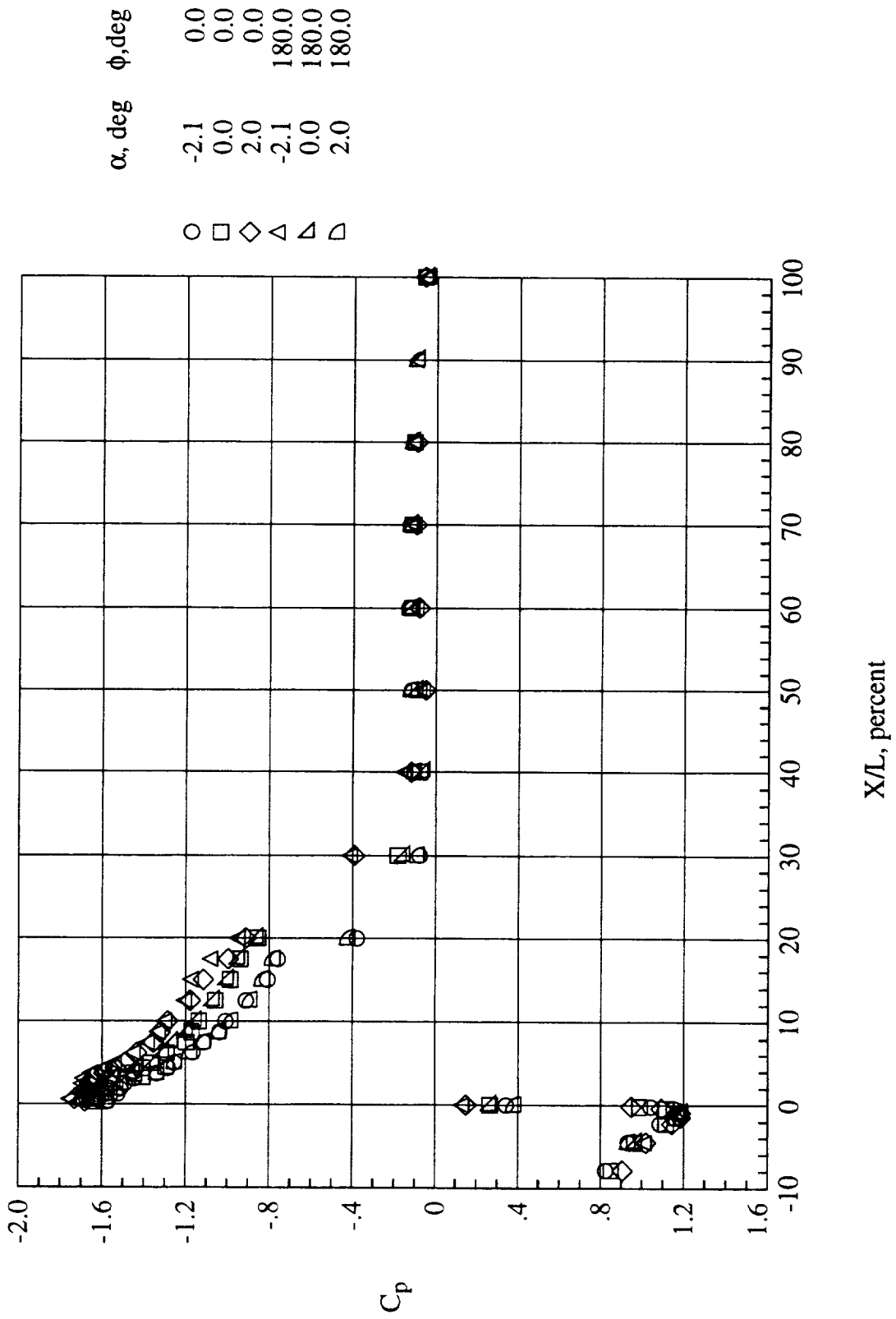
(e) M = 0.92.

Figure 10.- Concluded.



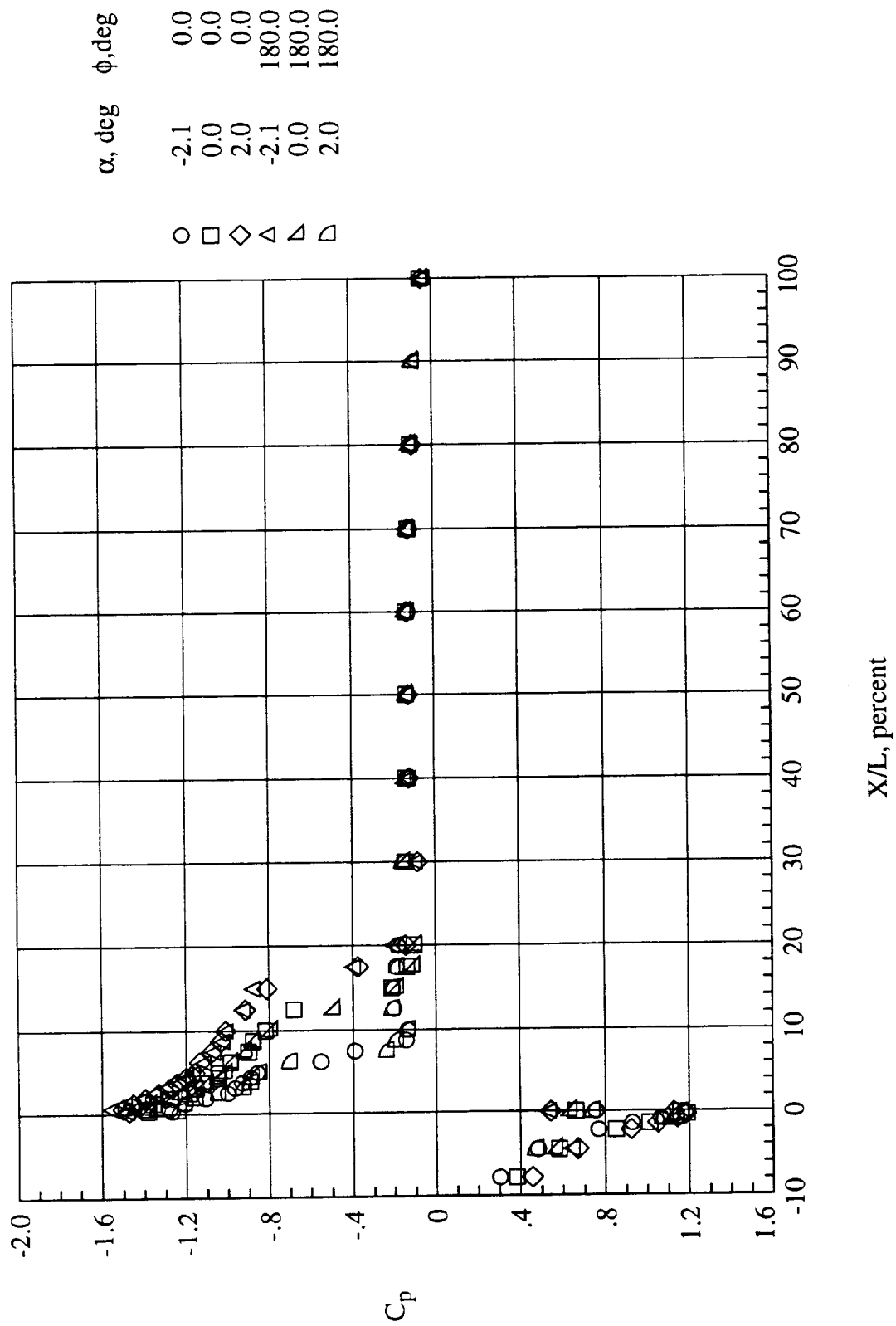
(a) $M = 0.79$ and $mfr = 0.67$.

Figure 11.- Pressure coefficient variation with X/L along the $\phi = 0^\circ$, and 180° meridians for the NACA 1-85-100 inlet with a contraction ratio of 1.250 at several angles of attack.



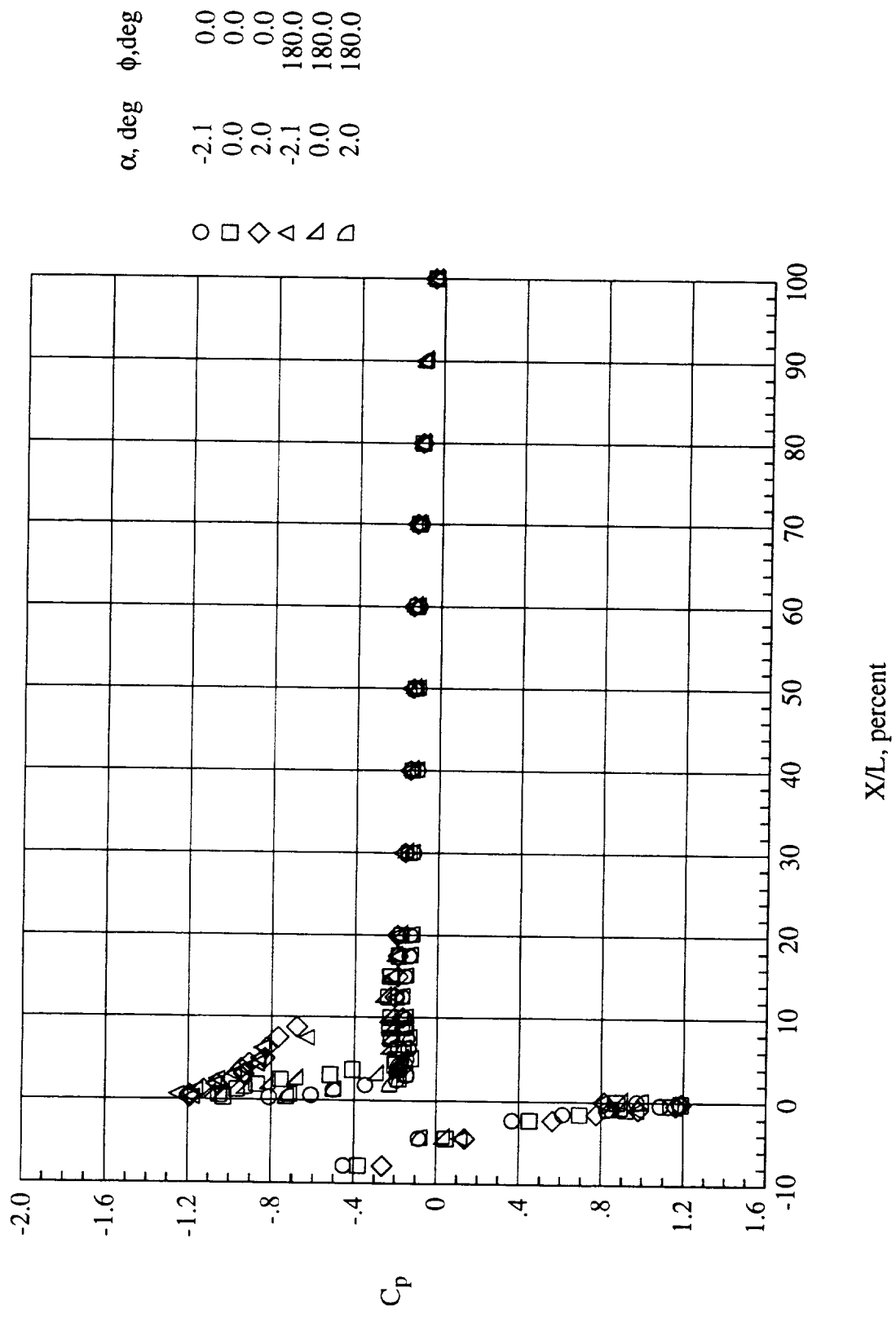
(b) $M = 0.84$ and $mfr = 0.49$.

Figure 11.- Continued.



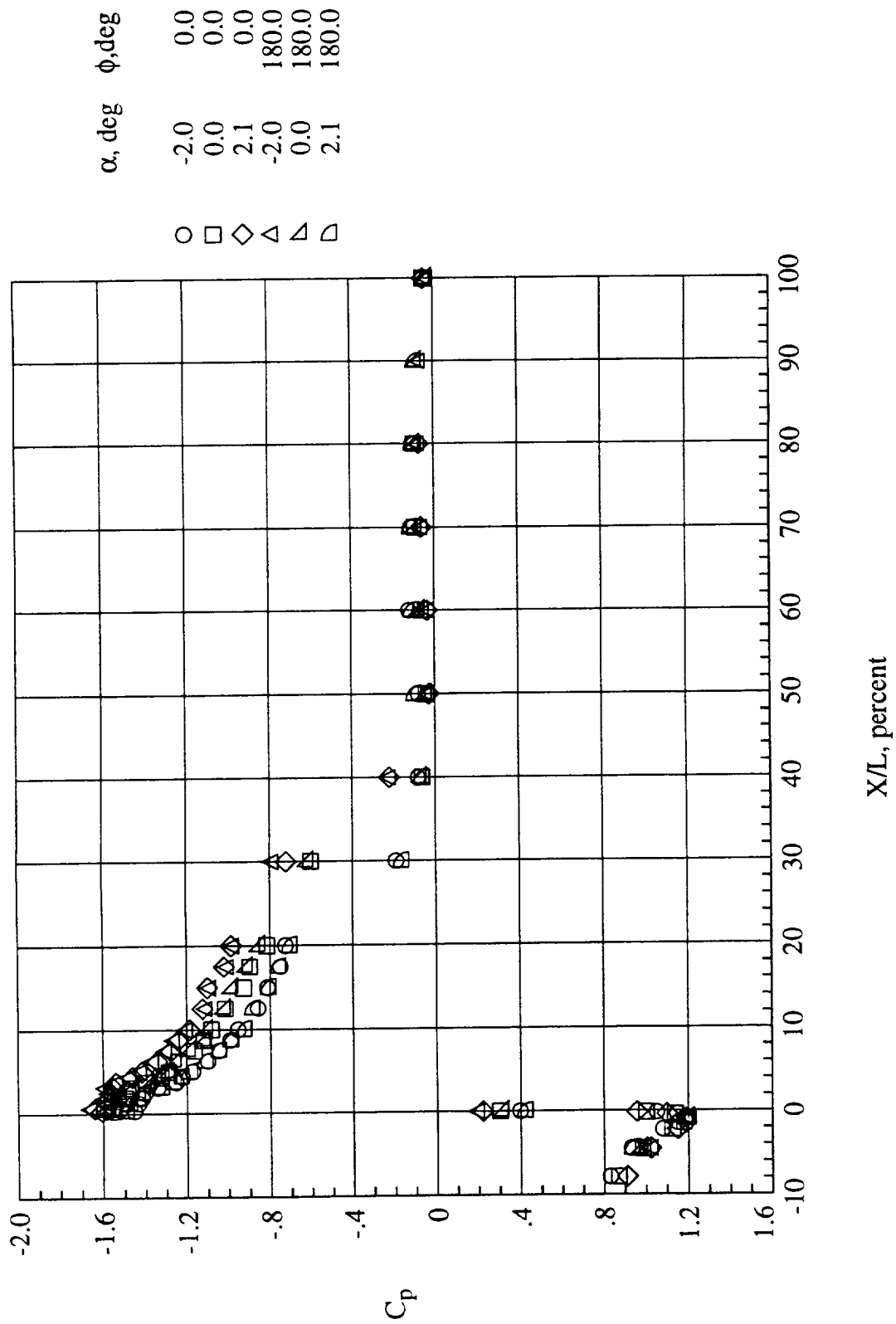
(c) $M = 0.84$ and $mfr = 0.67$.

Figure 11.- Continued.



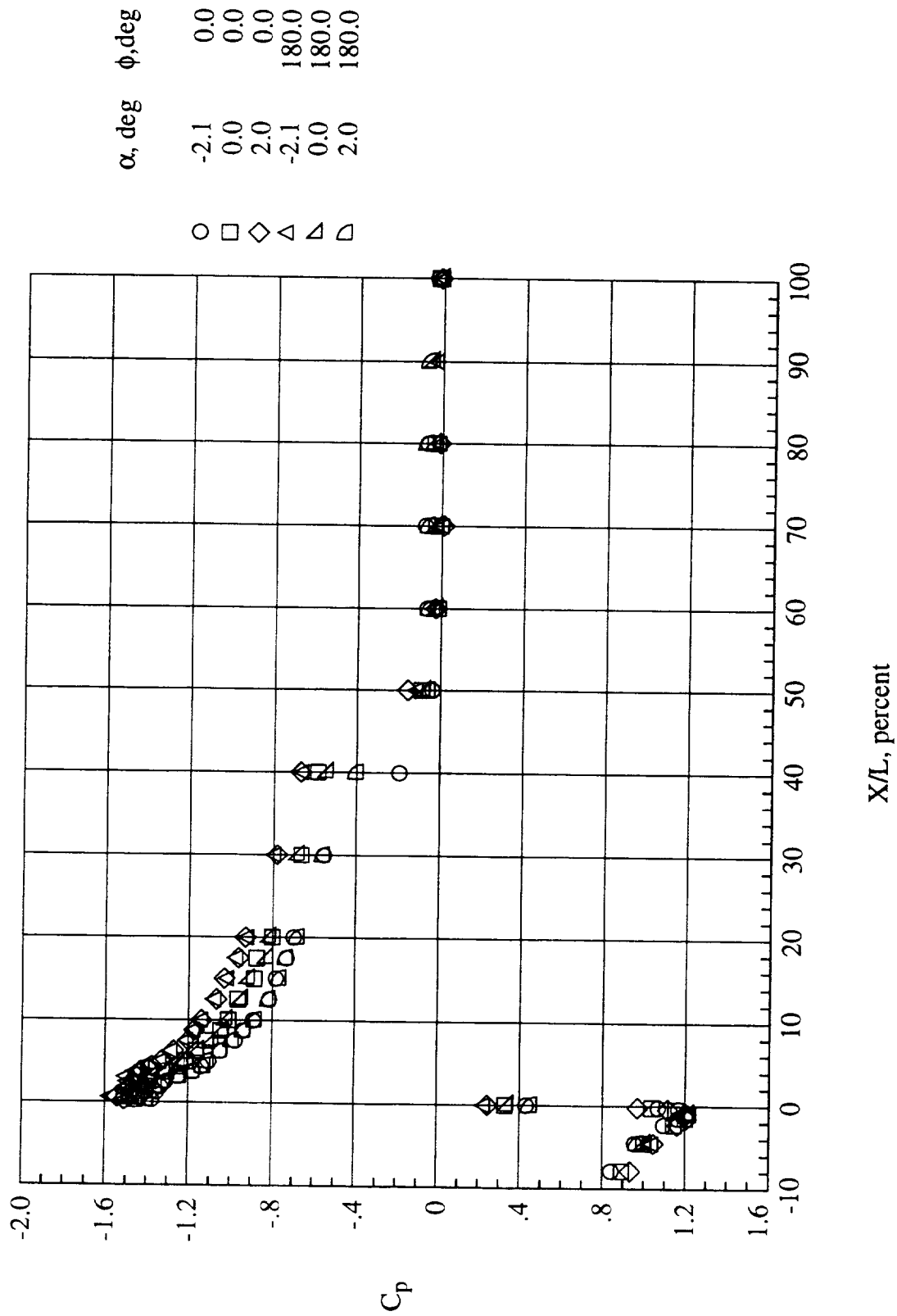
(d) $M = 0.84$ and $mfr = 0.83$.

Figure 11.- Continued.



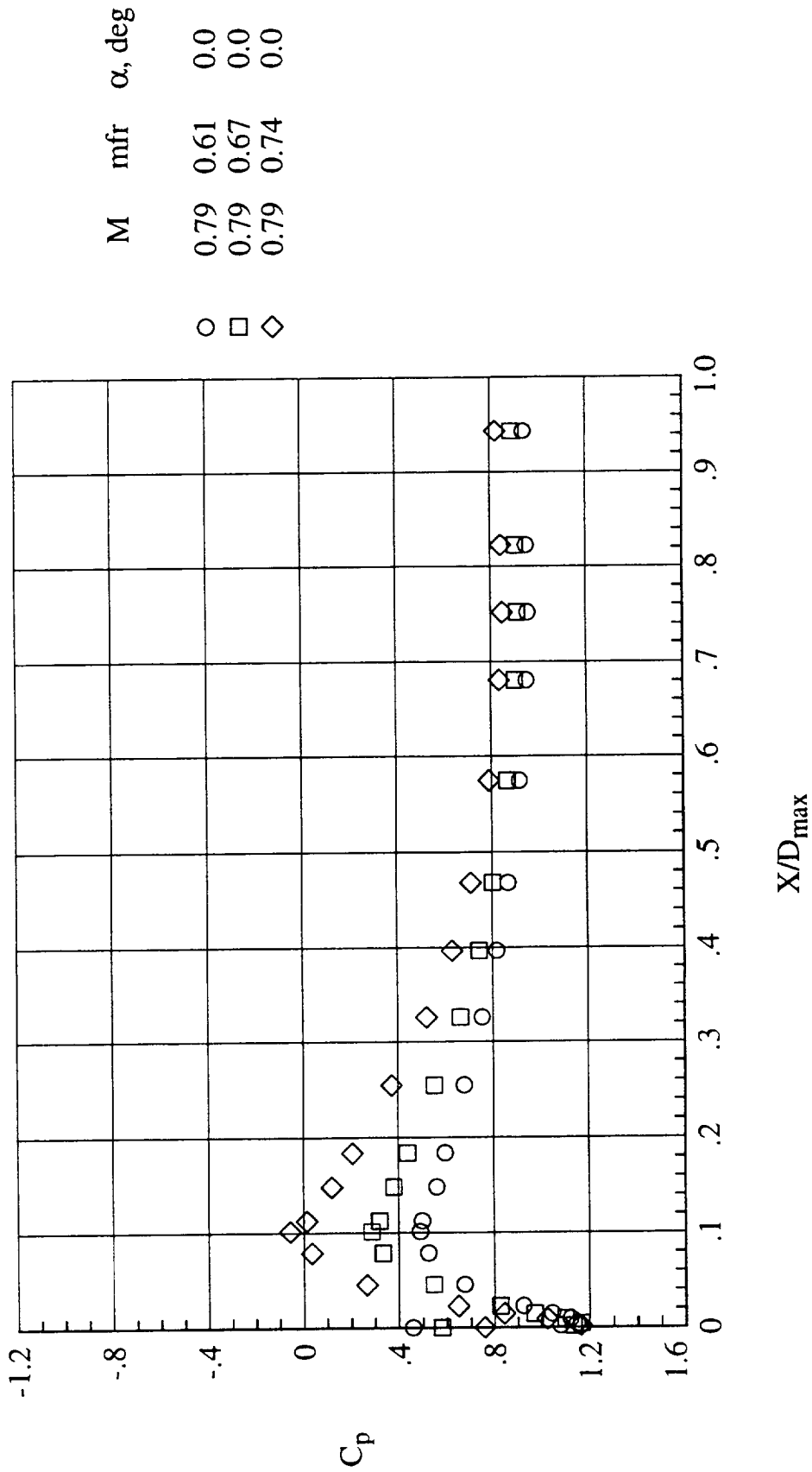
(e) $M = 0.87$ and $mfr = 0.49$.

Figure 11.- Continued.



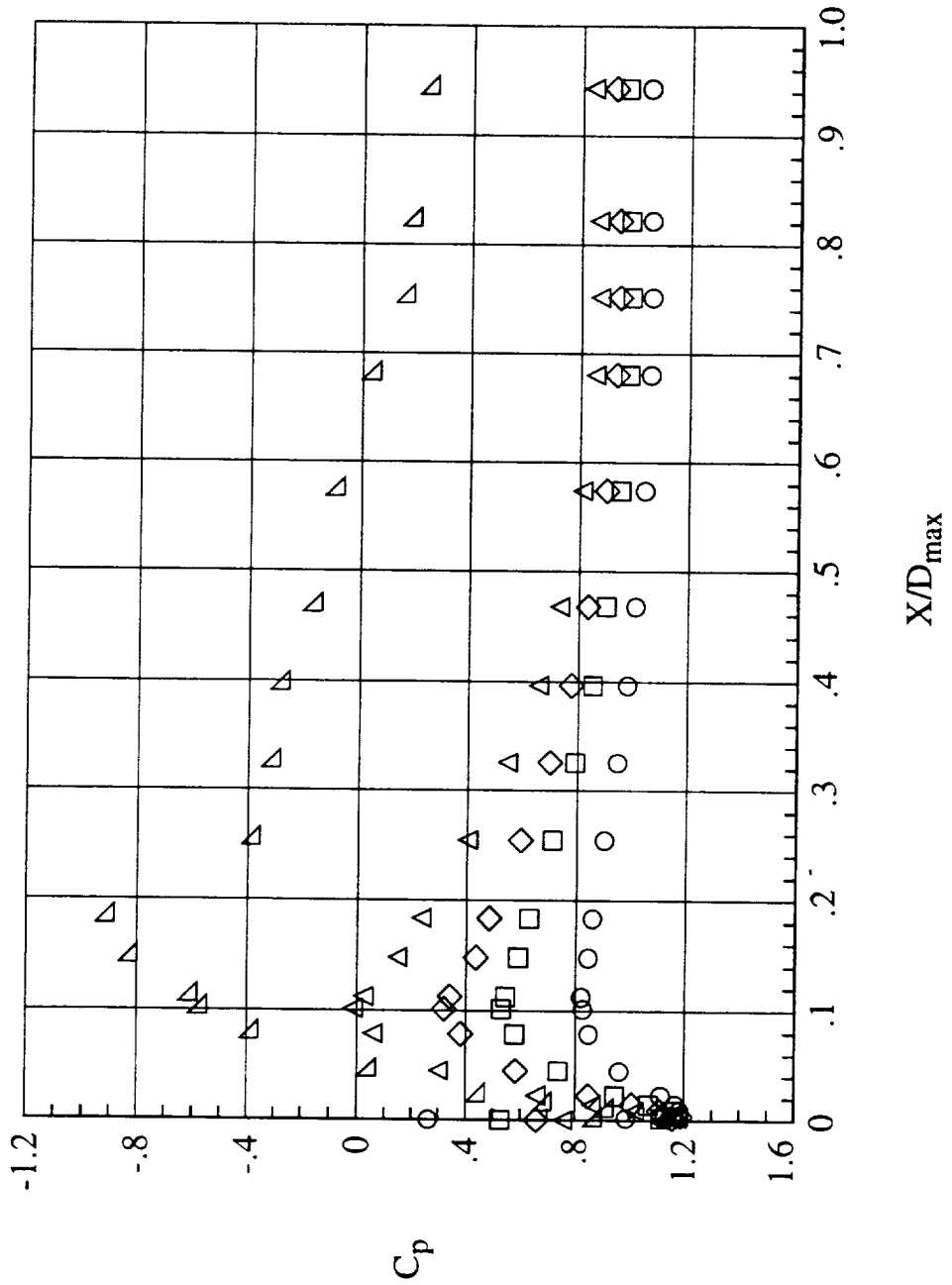
(f) $M = 0.89$ and $mfr = 0.49$.

Figure 11.- Concluded.



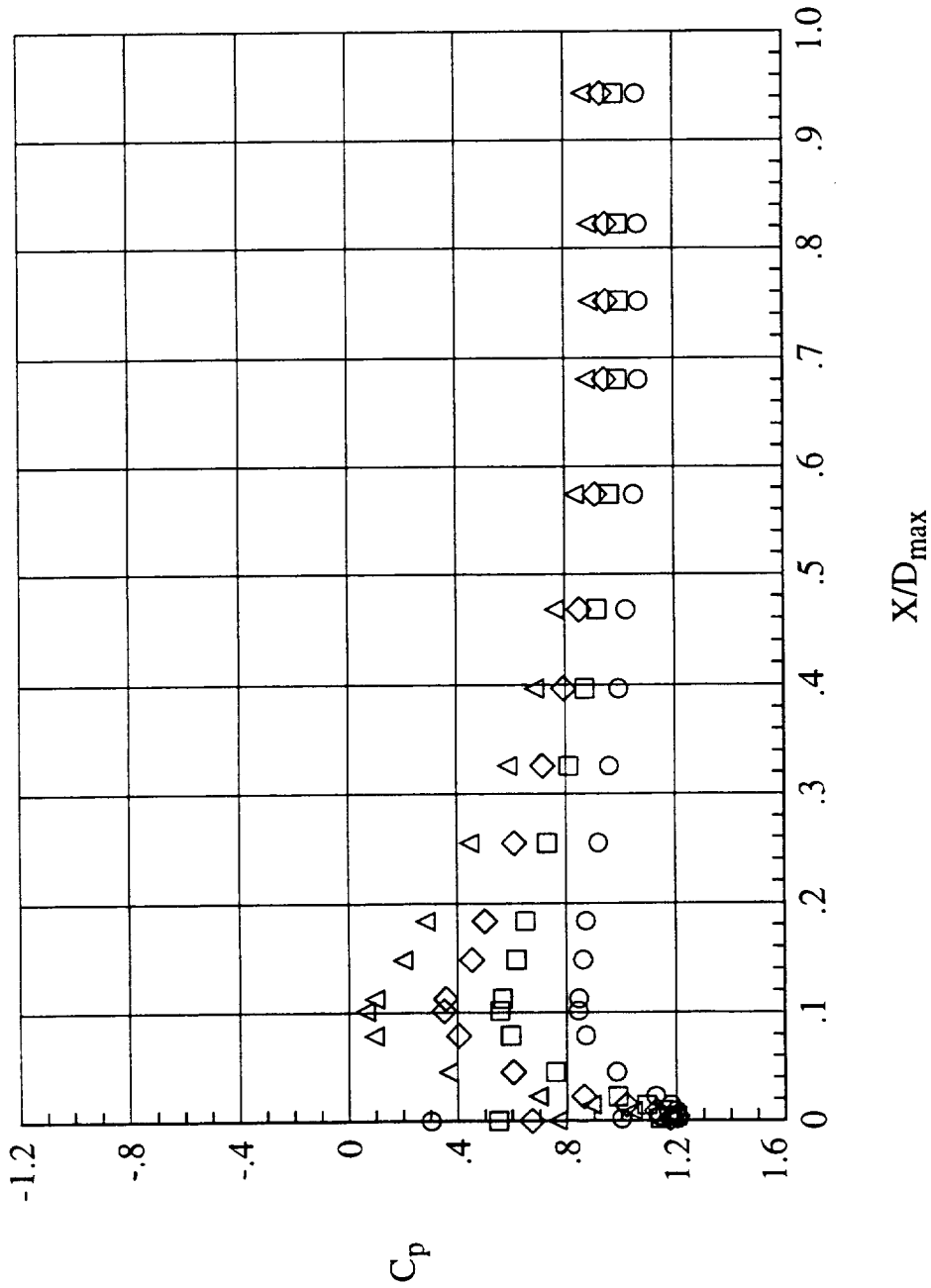
(a) $M = 0.79$.

Figure 12.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the NACA 1-85-100 inlet with a contraction ratio of 1.25 for several mass-flow ratios at $\alpha = 0^\circ$.



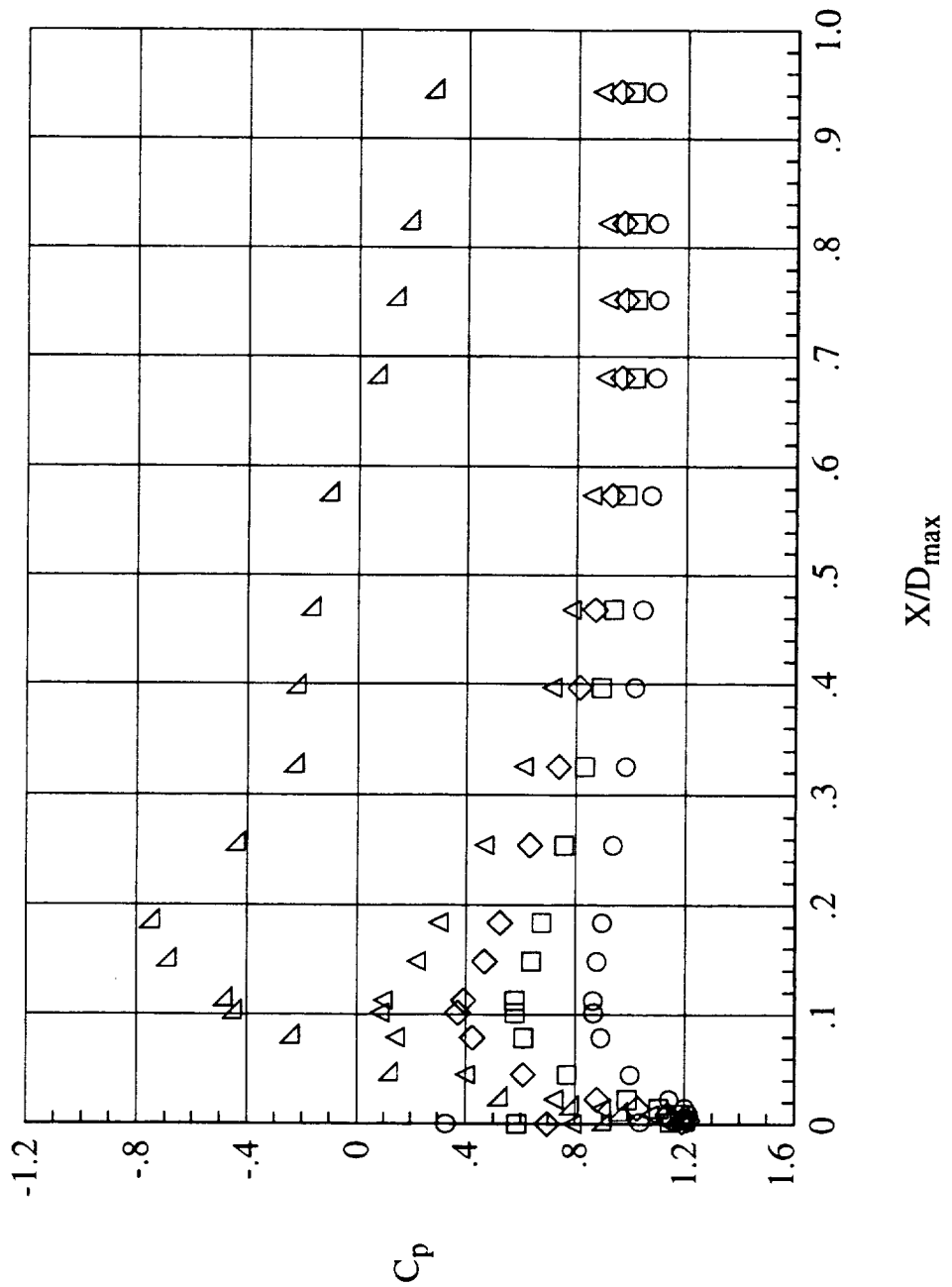
(b) $M = 0.84$.

Figure 12.- Continued.



(c) $M = 0.87$.

Figure 12.- Continued.

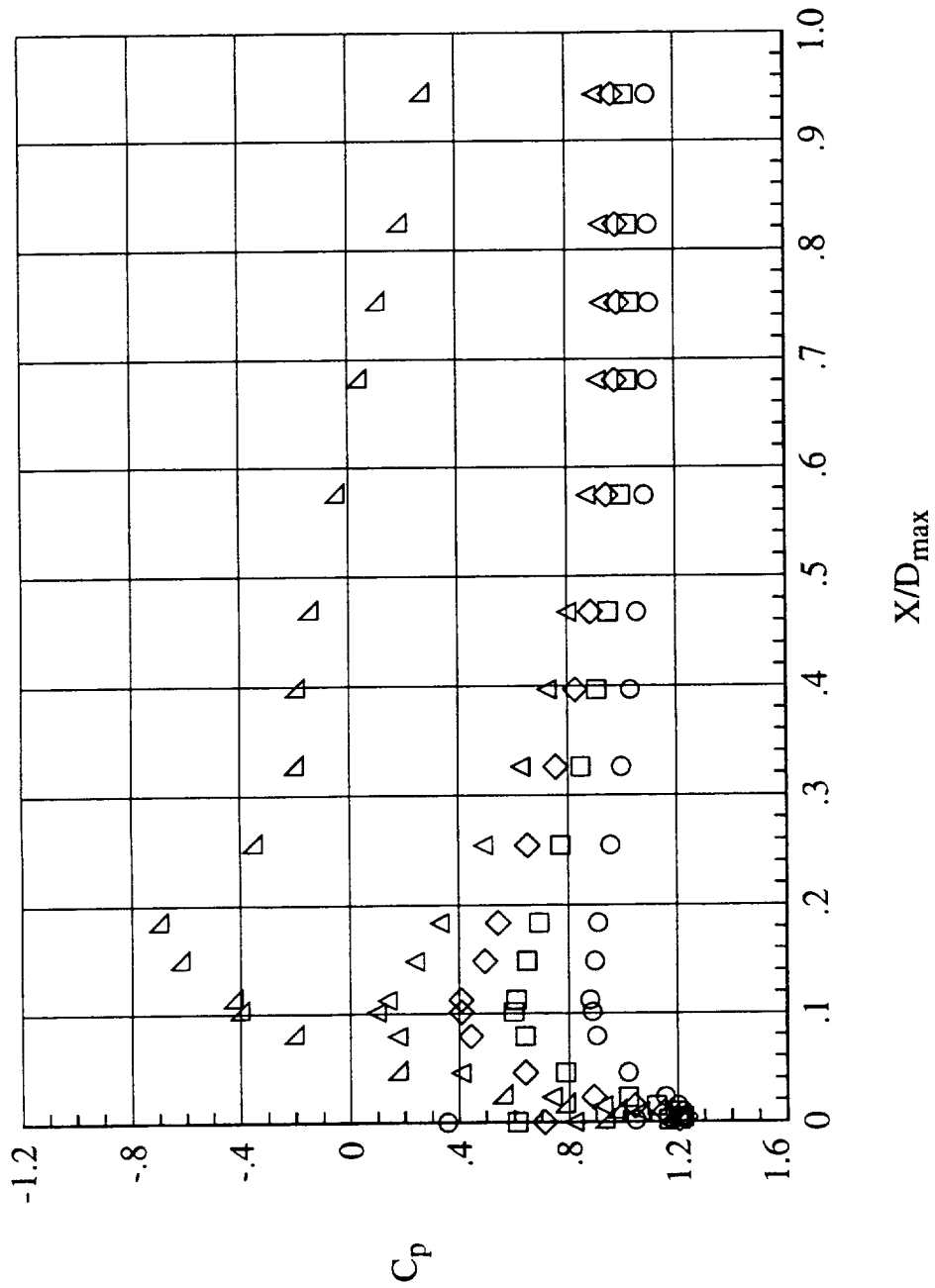


M	mfr	α , deg
0.89	0.49	0.0
0.89	0.61	0.0
0.89	0.67	0.0
0.89	0.73	0.0
0.89	0.81	0.0

○ □ ◇ △ ▽

(d) $M = 0.89$.

Figure 12.- Continued.

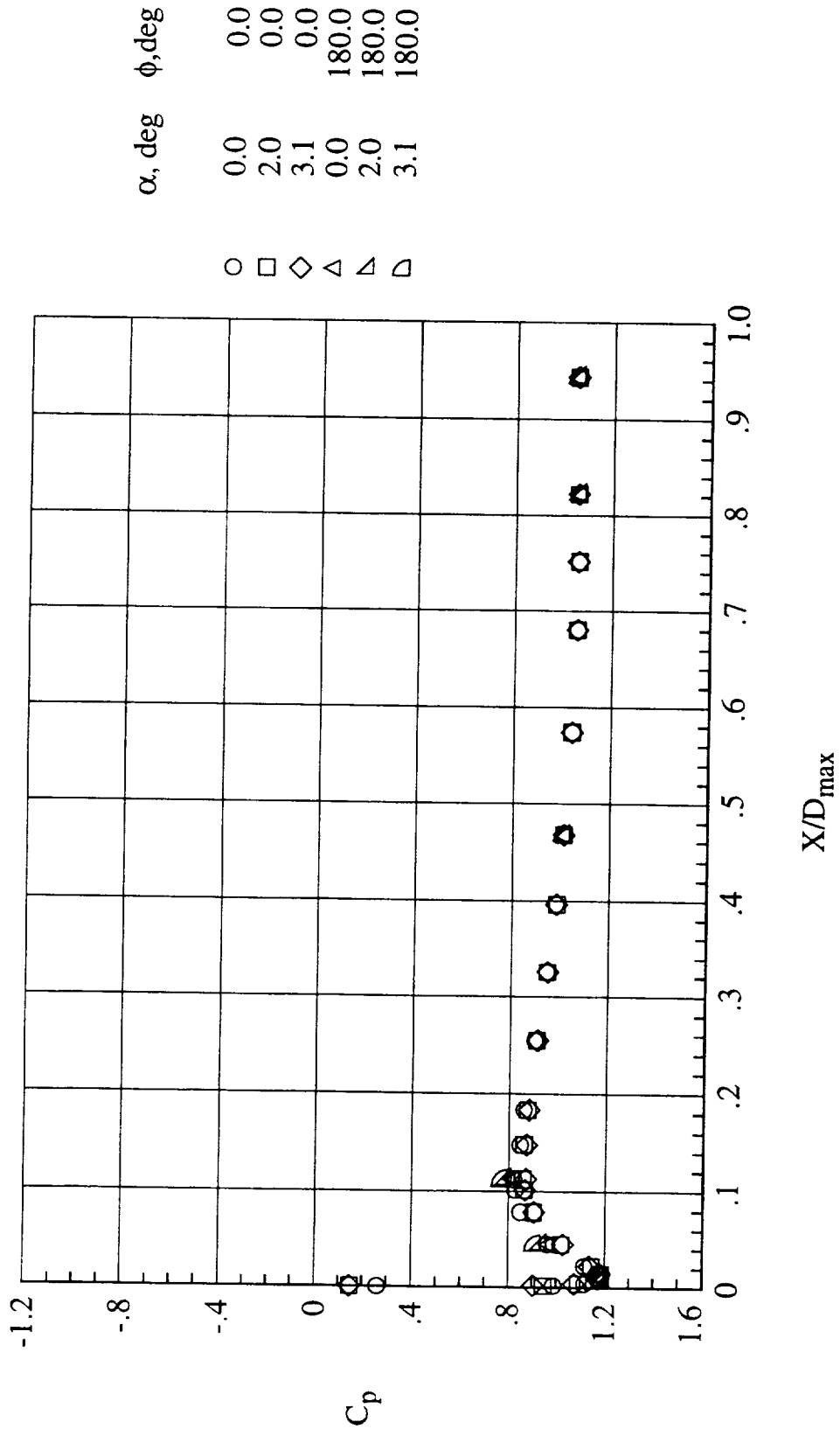


M	mfr	α , deg
0.92	0.50	0.0
0.91	0.61	0.0
0.92	0.67	0.0
0.92	0.73	0.0
0.91	0.81	0.0

○ □ ◇ △ ▽

(e) $M = 0.92$.

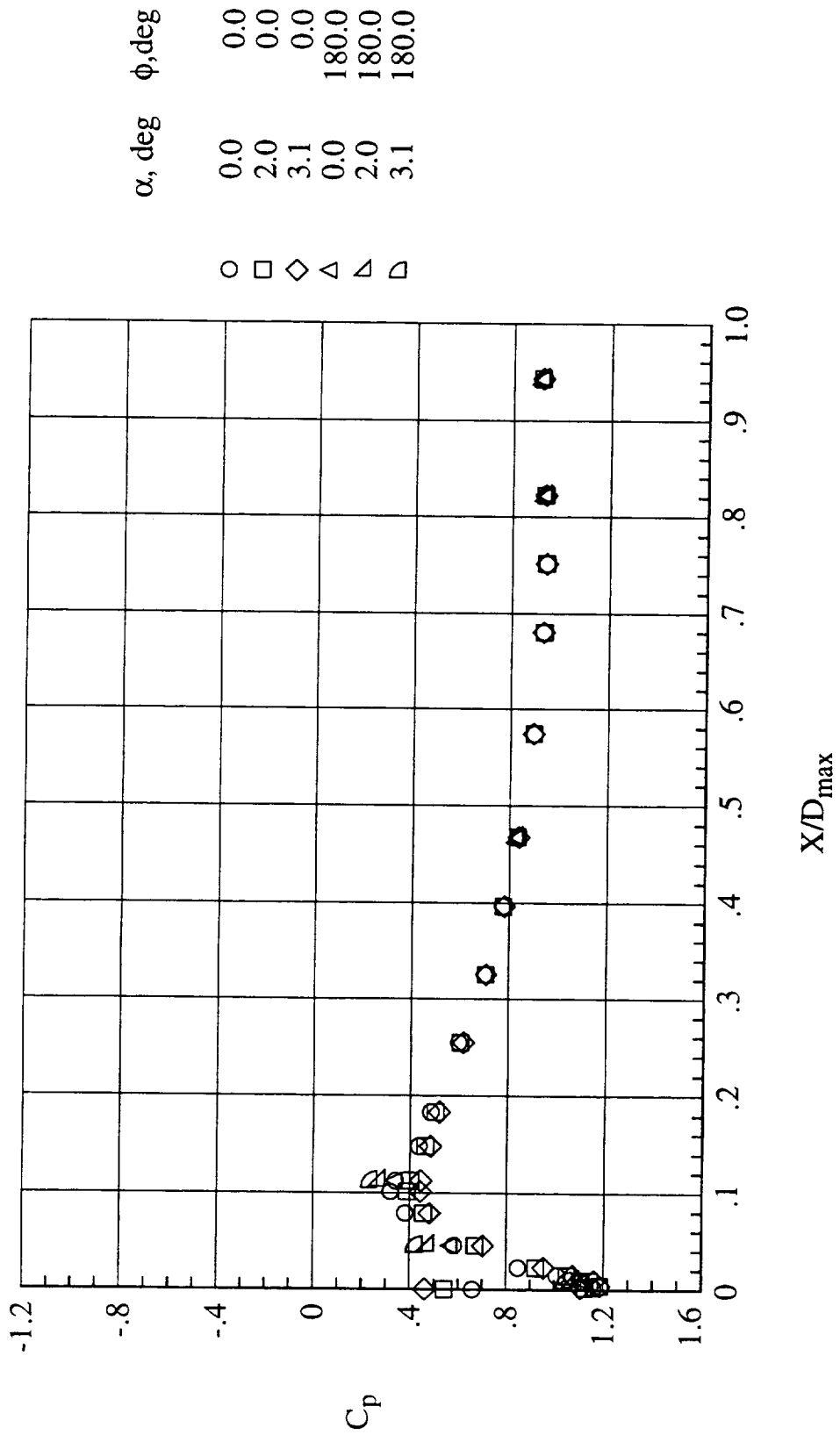
Figure 12.- Concluded.



(a) $M = 0.84$ and $mfr = 0.49$.

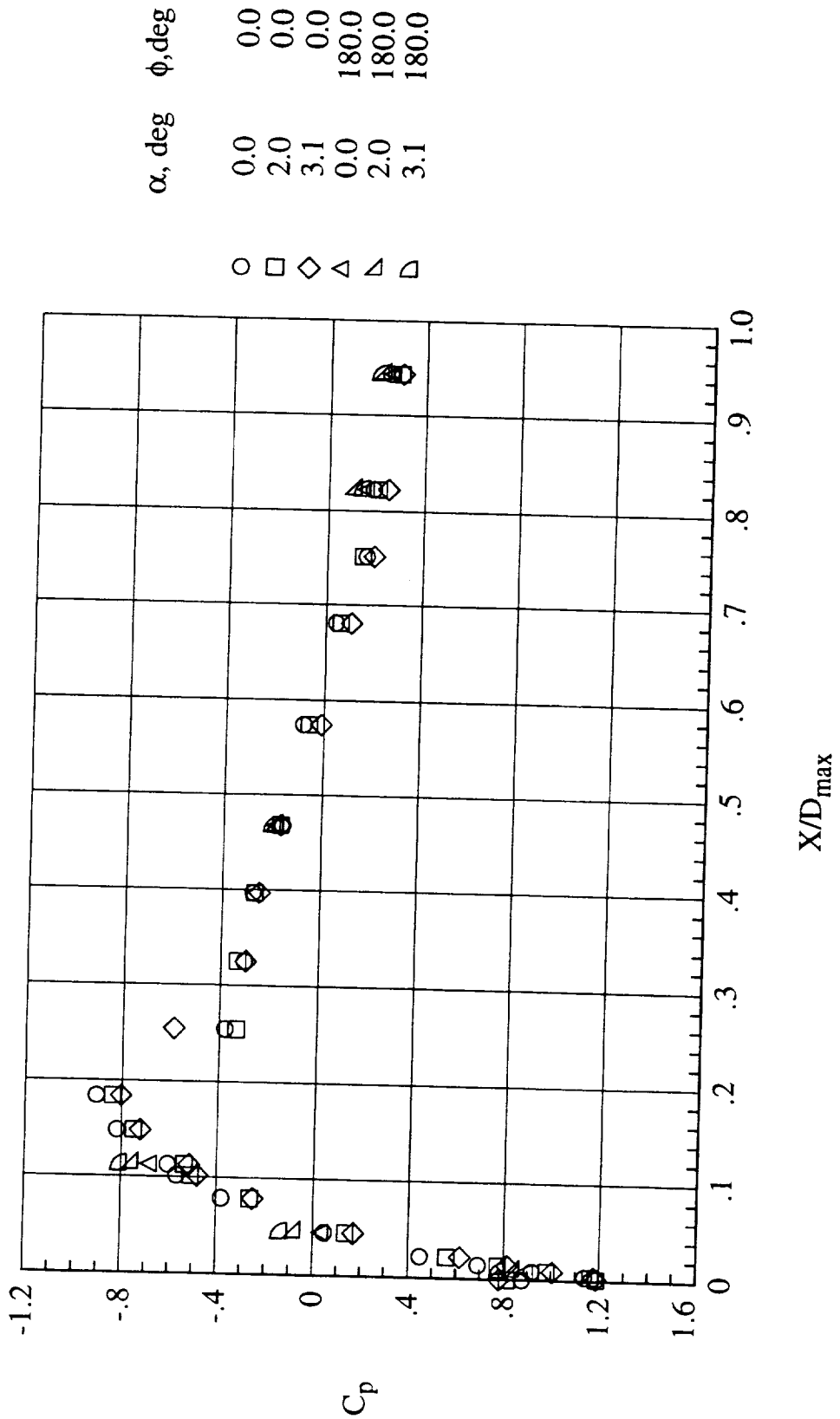
Figure 13.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the

NACA 1-85-100 inlet with a contraction ratio of 1.25 for several mass-flow ratios and angles of attack.



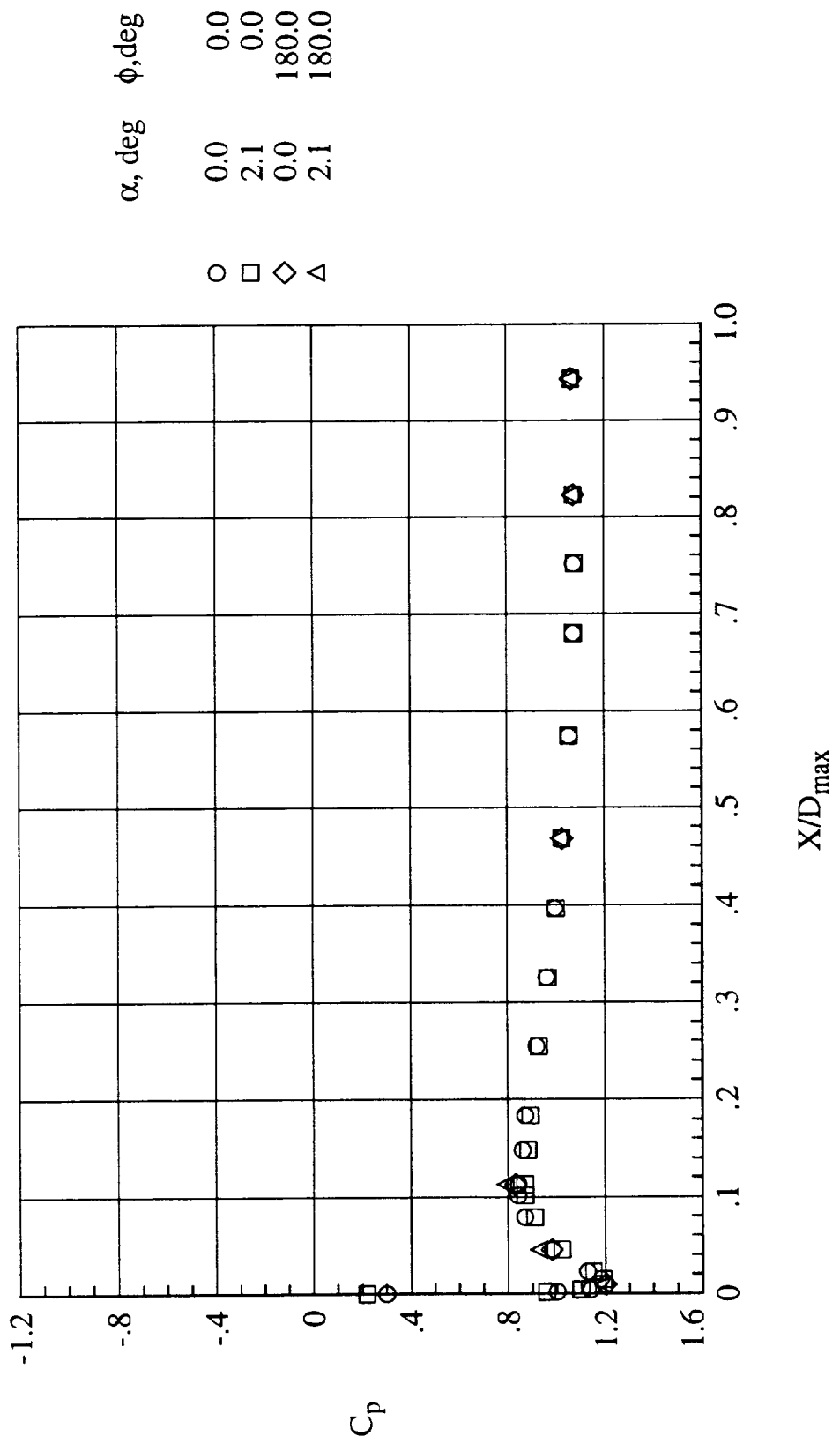
(b) $M = 0.84$ and $mfr = 0.67$.

Figure 13.- Continued.



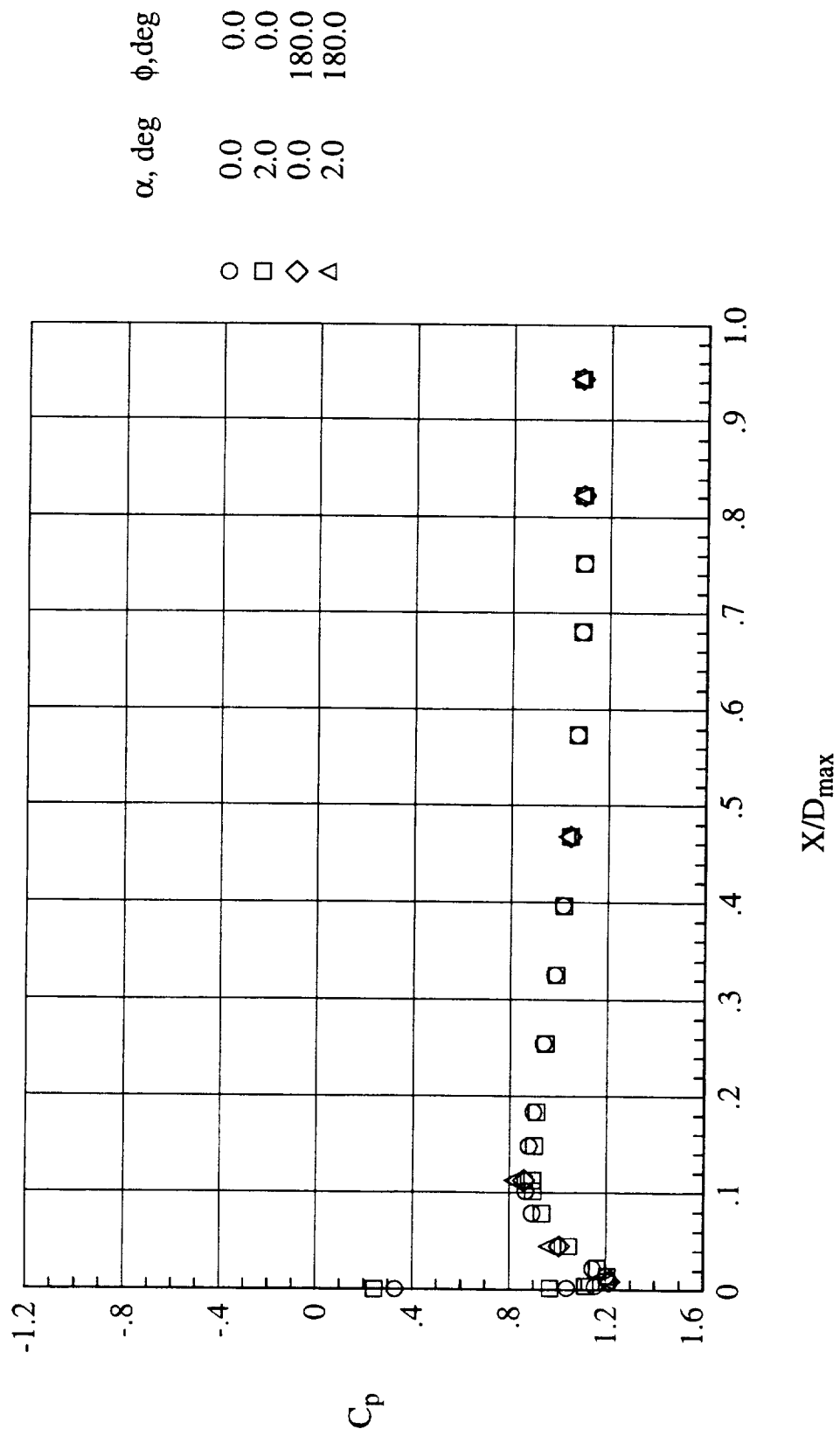
(c) $M = 0.84$ and $mfr = 0.84$.

Figure 13.- Continued.



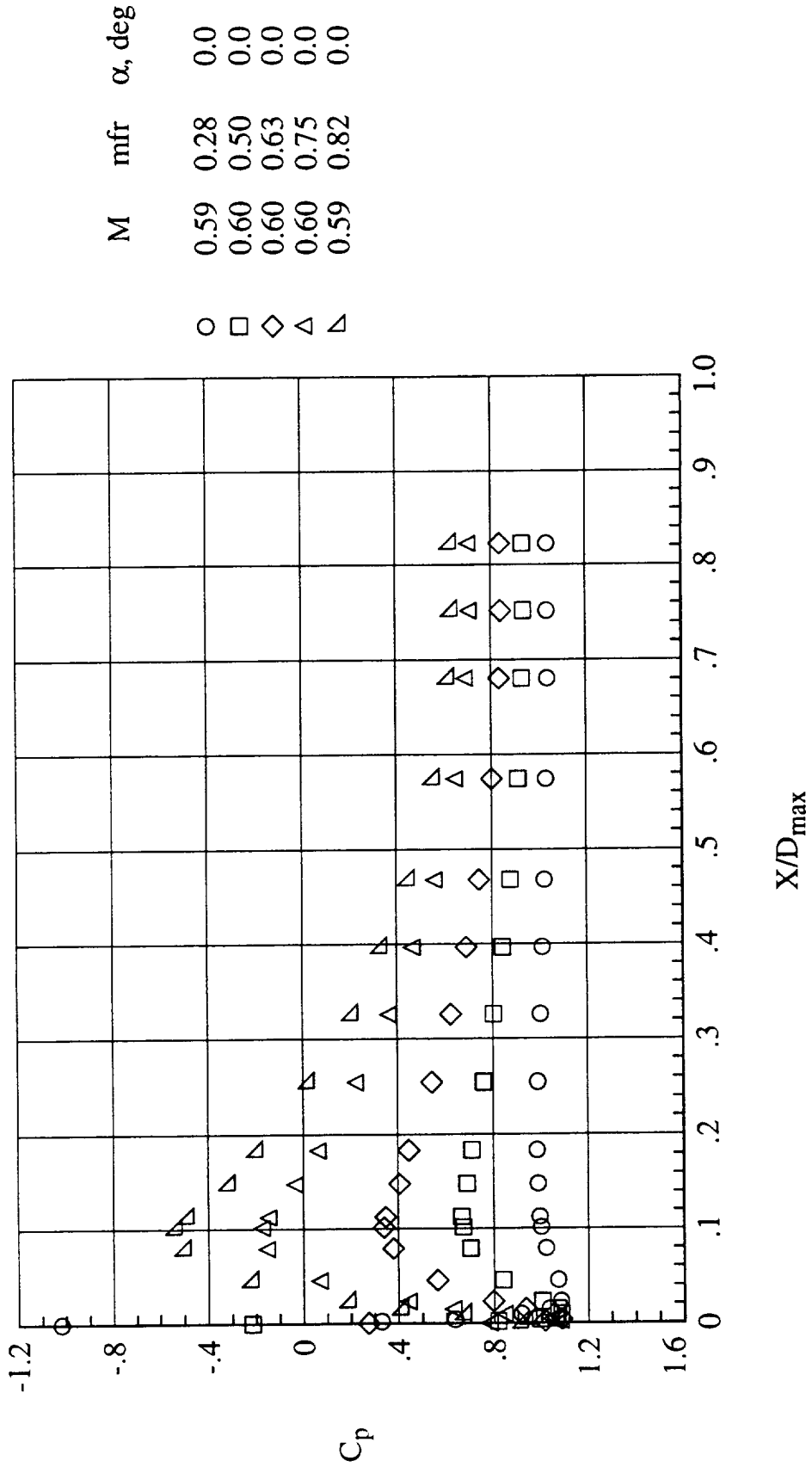
(d) $M = 0.87$ and $mfr = 0.49$.

Figure 13.- Continued.



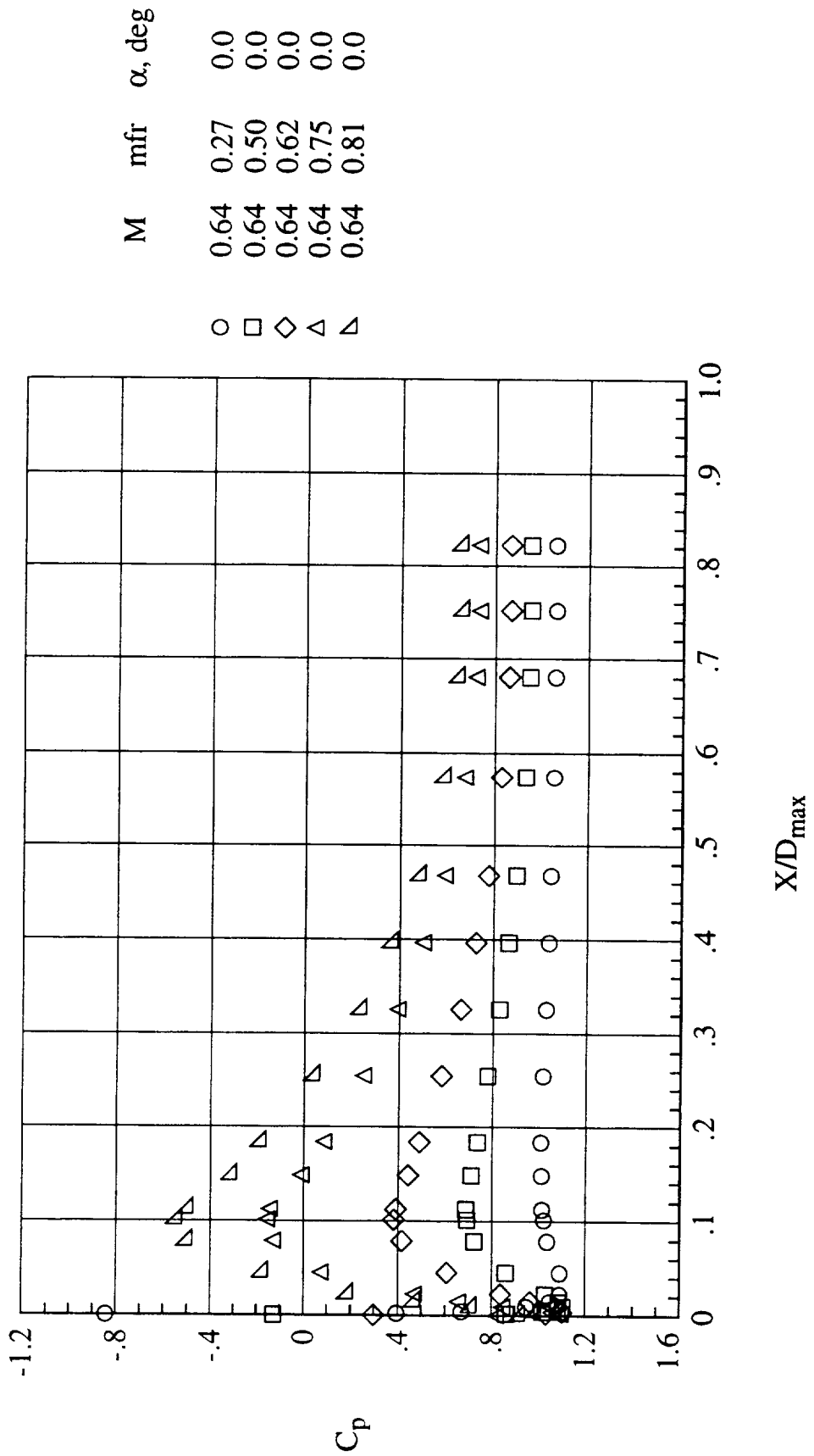
(e) $M = 0.89$ and $mfr = 0.49$.

Figure 13.- Concluded.



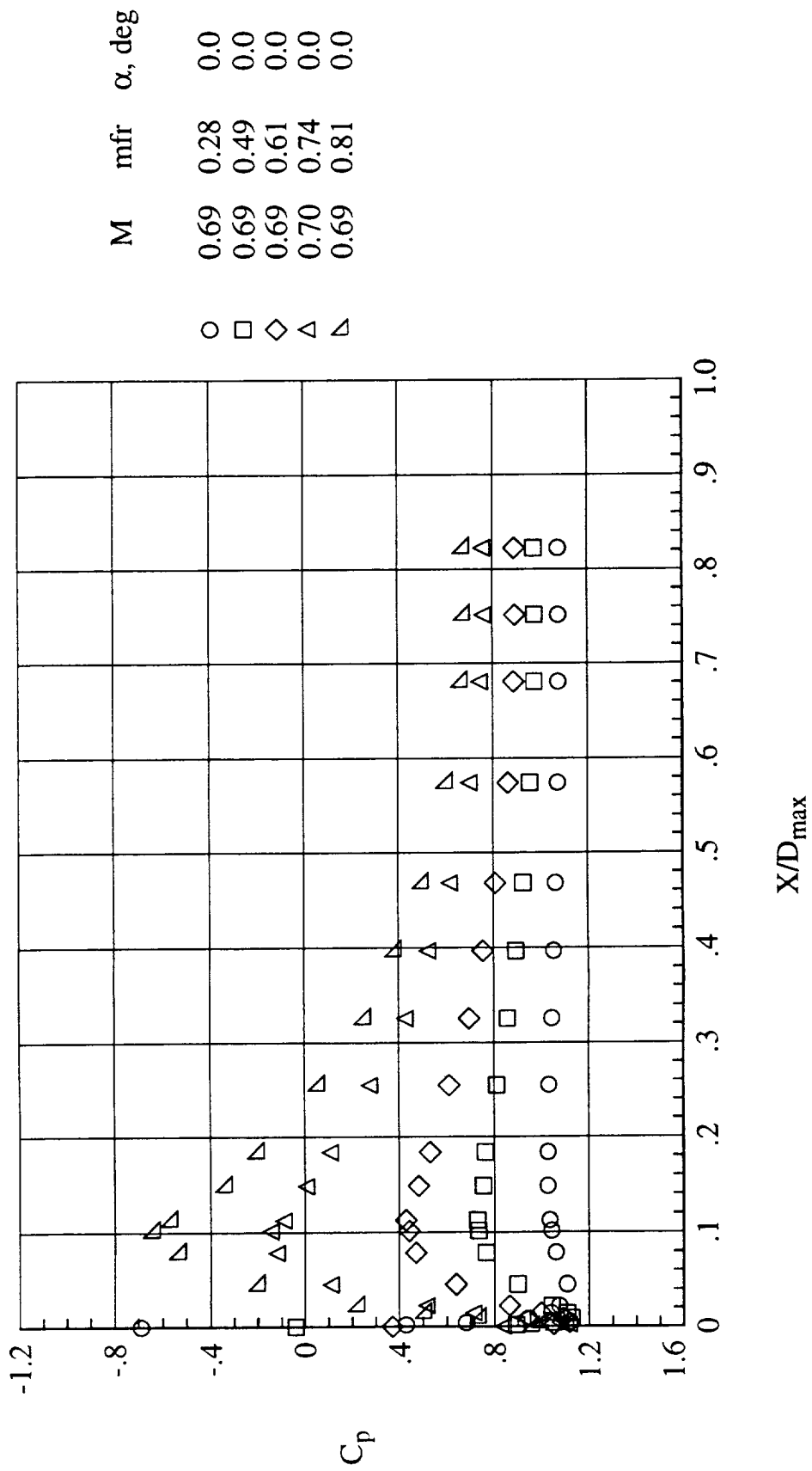
(a) $M = 0.60$.

Figure 14.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the NACA 1-85-43.9 inlet with a contraction ratio of 1.25 for several mass-flow ratios at $\alpha = 0^\circ$.



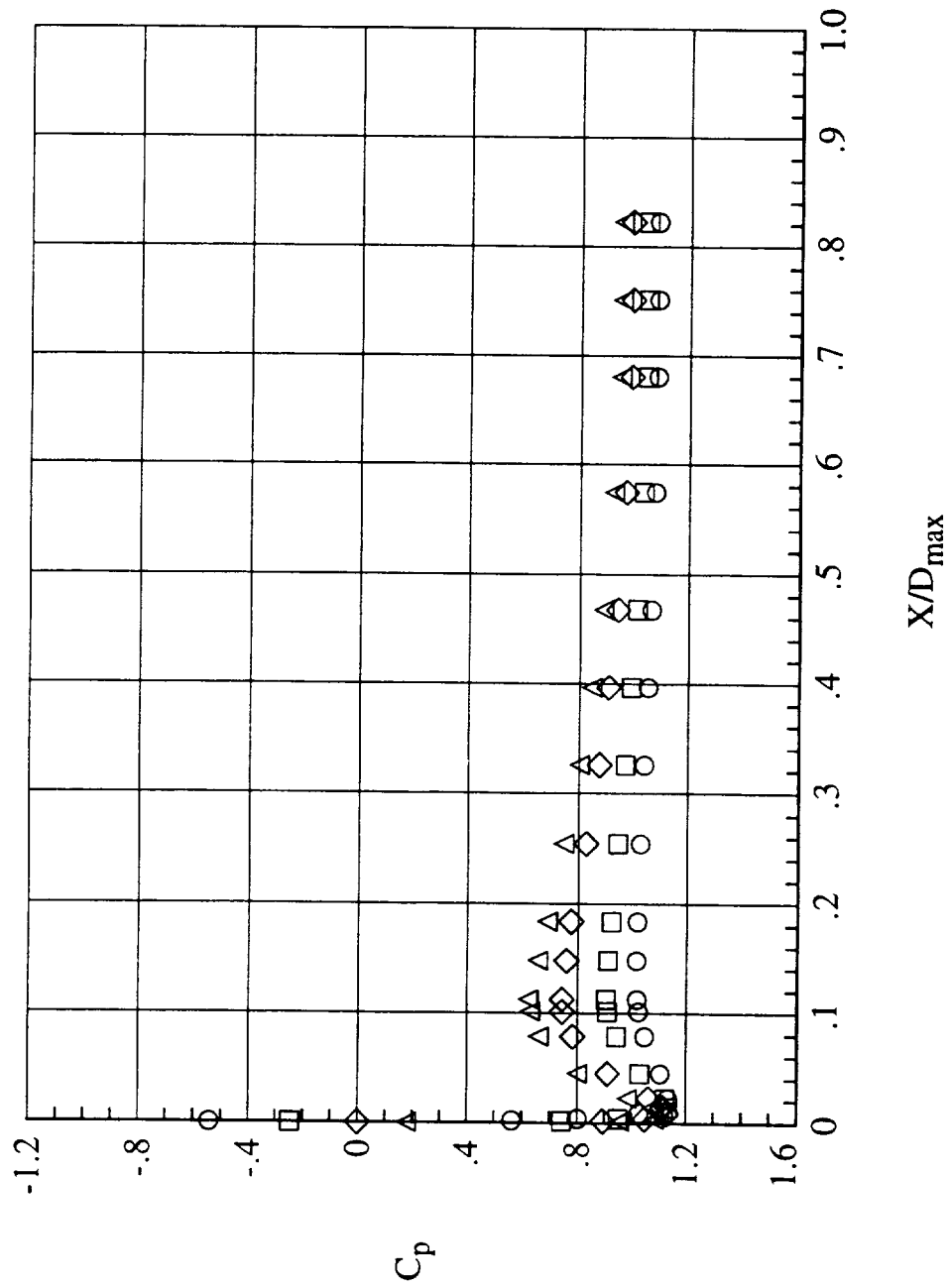
(b) $M = 0.64$.

Figure 14.- Continued.



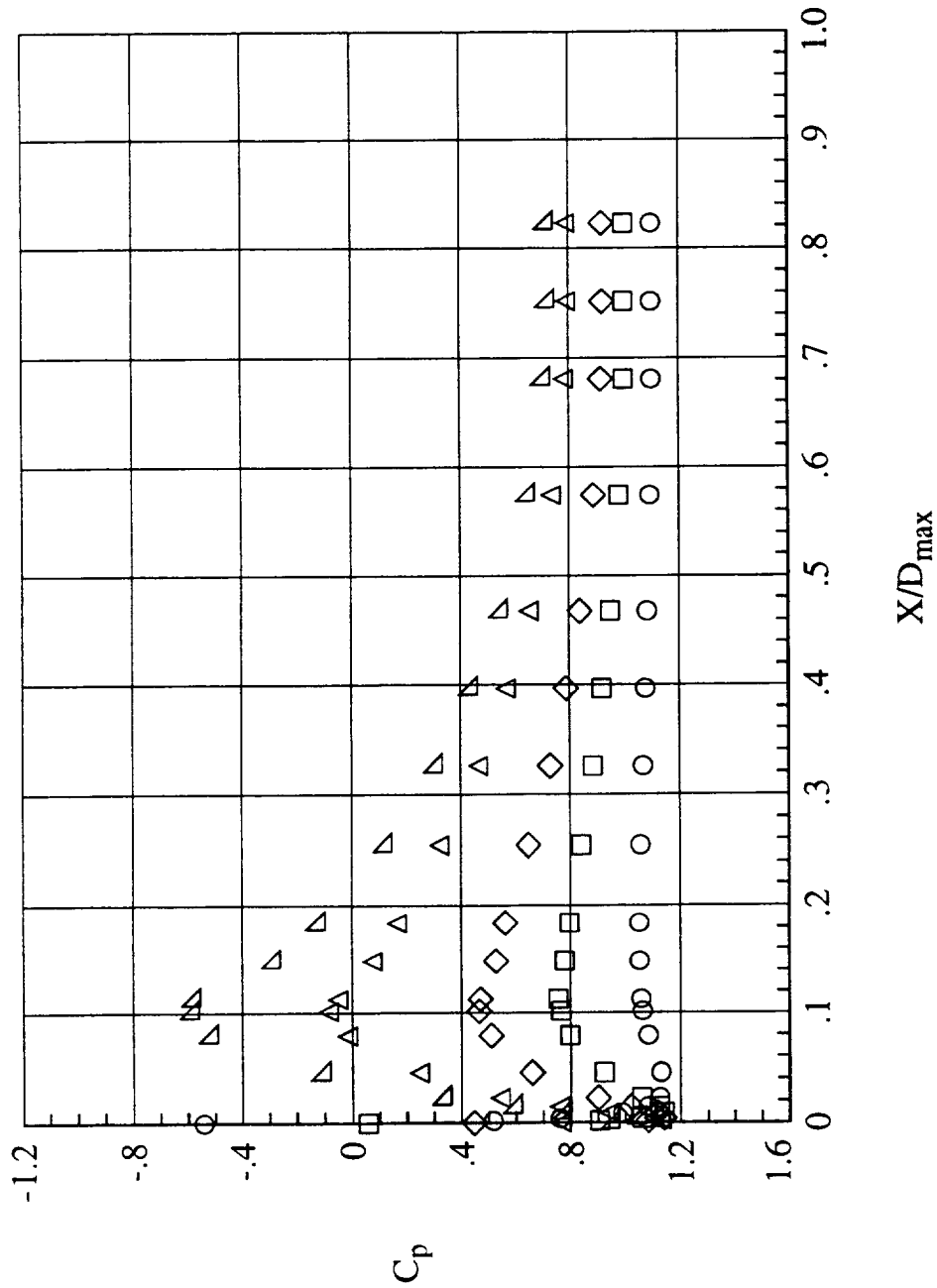
(c) $M = 0.69$.

Figure 14.- Continued.



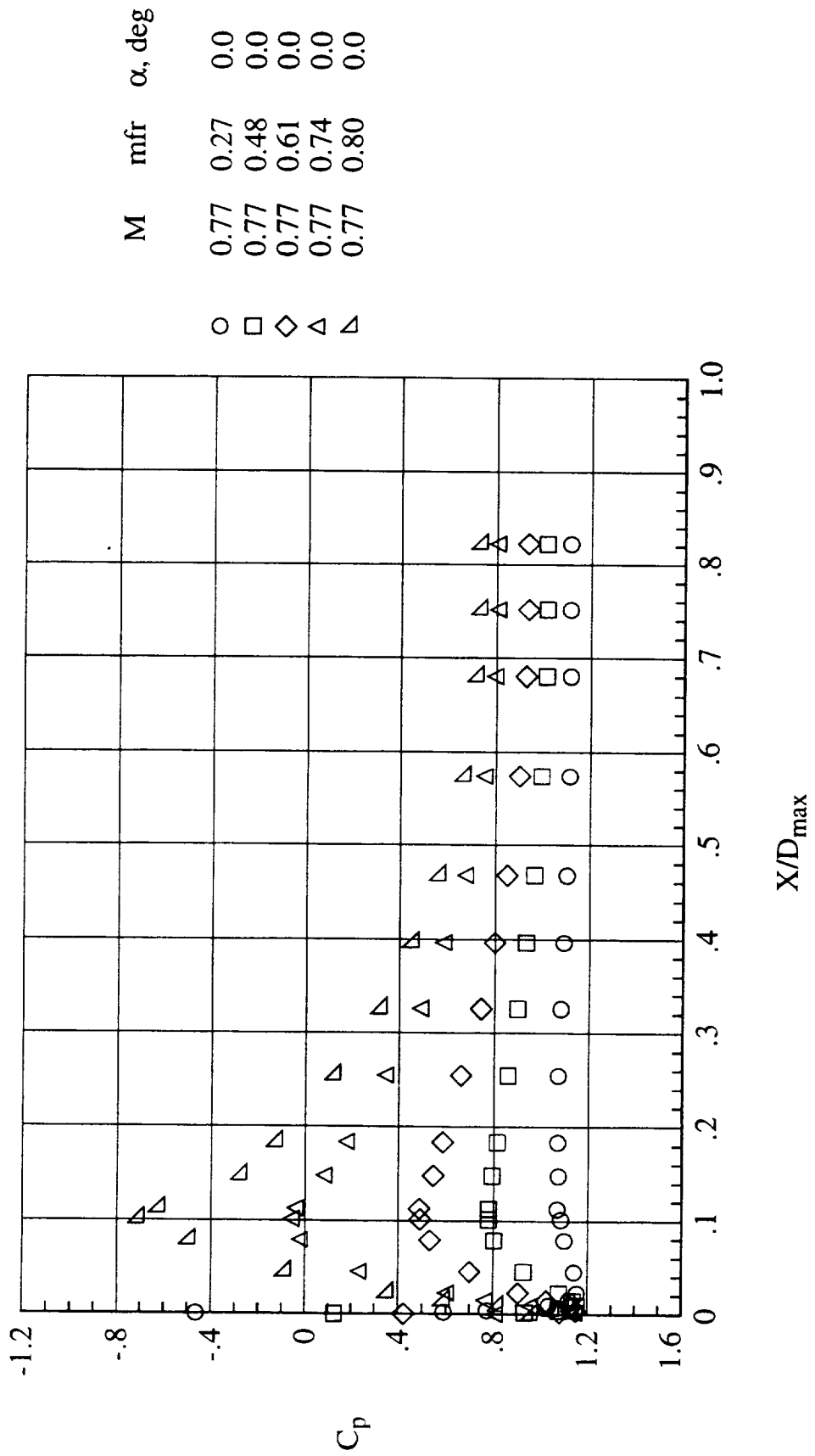
(d) $M = 0.72$.

Figure 14.- Continued.

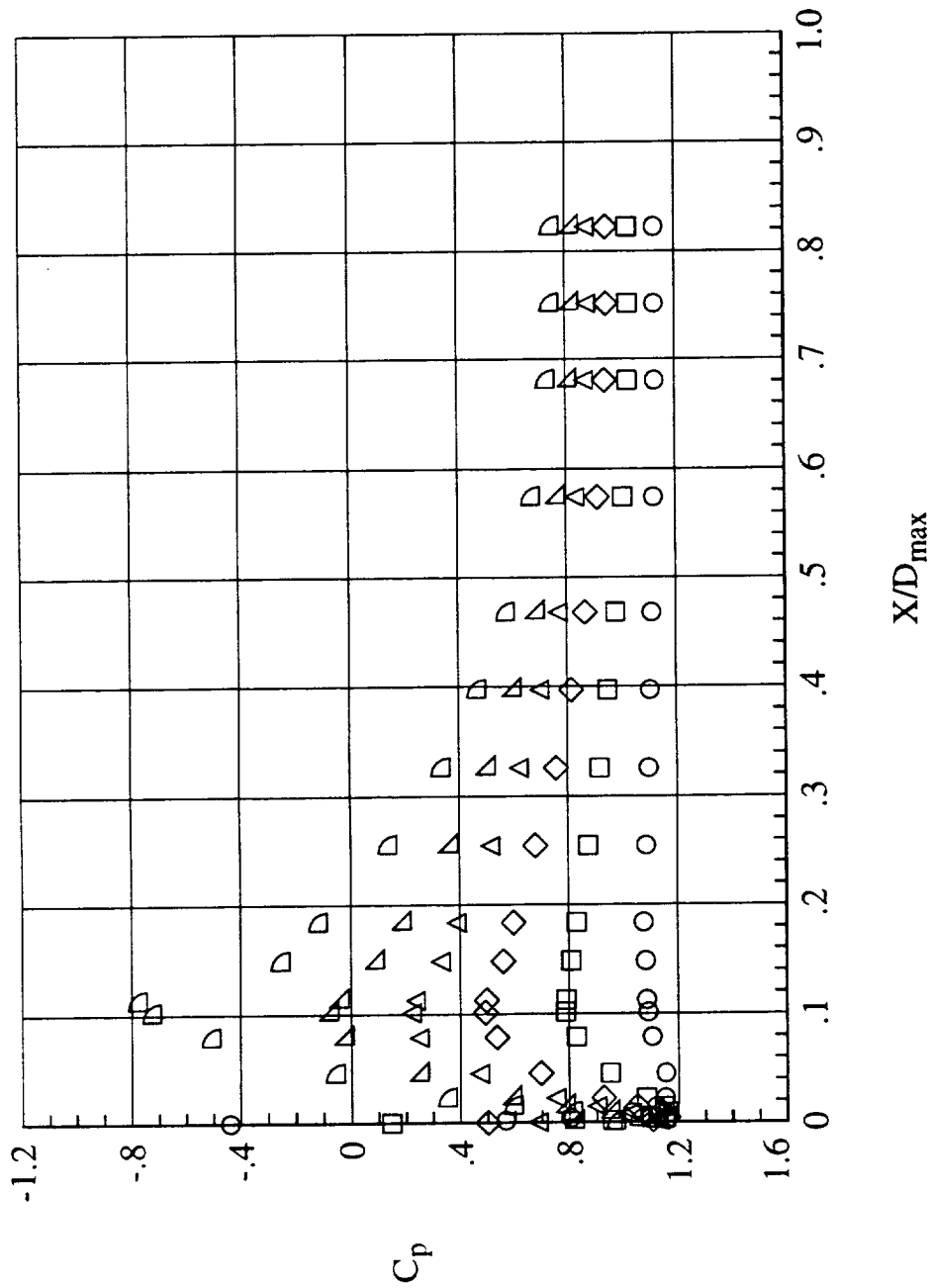


(e) $M = 0.74$.

Figure 14.- Continued.



(f) $M = 0.77$.
 Figure 14.- Continued.

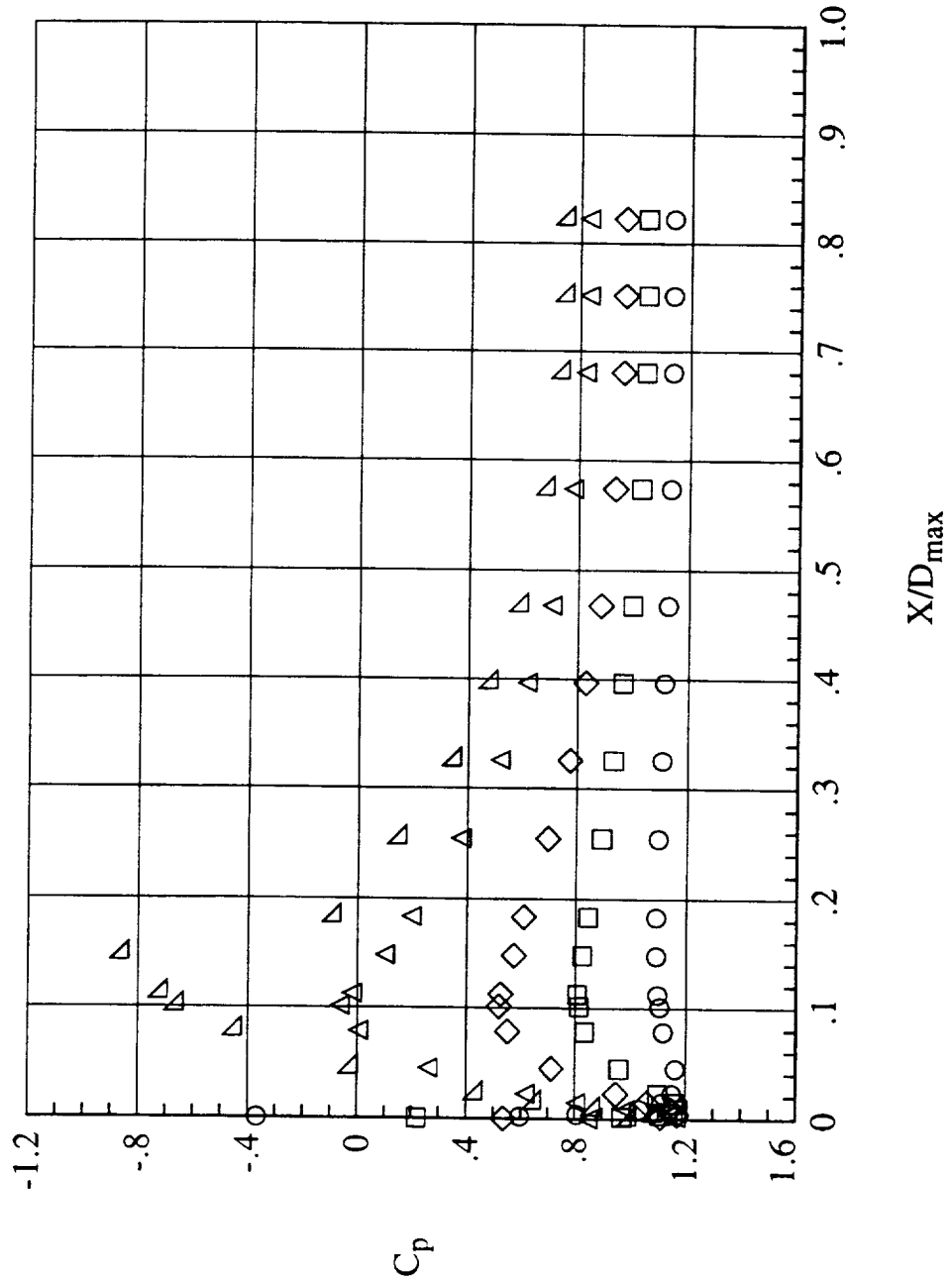


M	mfr	α , deg
0.79	0.27	0.0
0.79	0.49	0.0
0.79	0.61	0.0
0.79	0.68	0.0
0.79	0.74	0.0
0.79	0.80	0.0

○ □ ◇ ▲ ▽ ▹

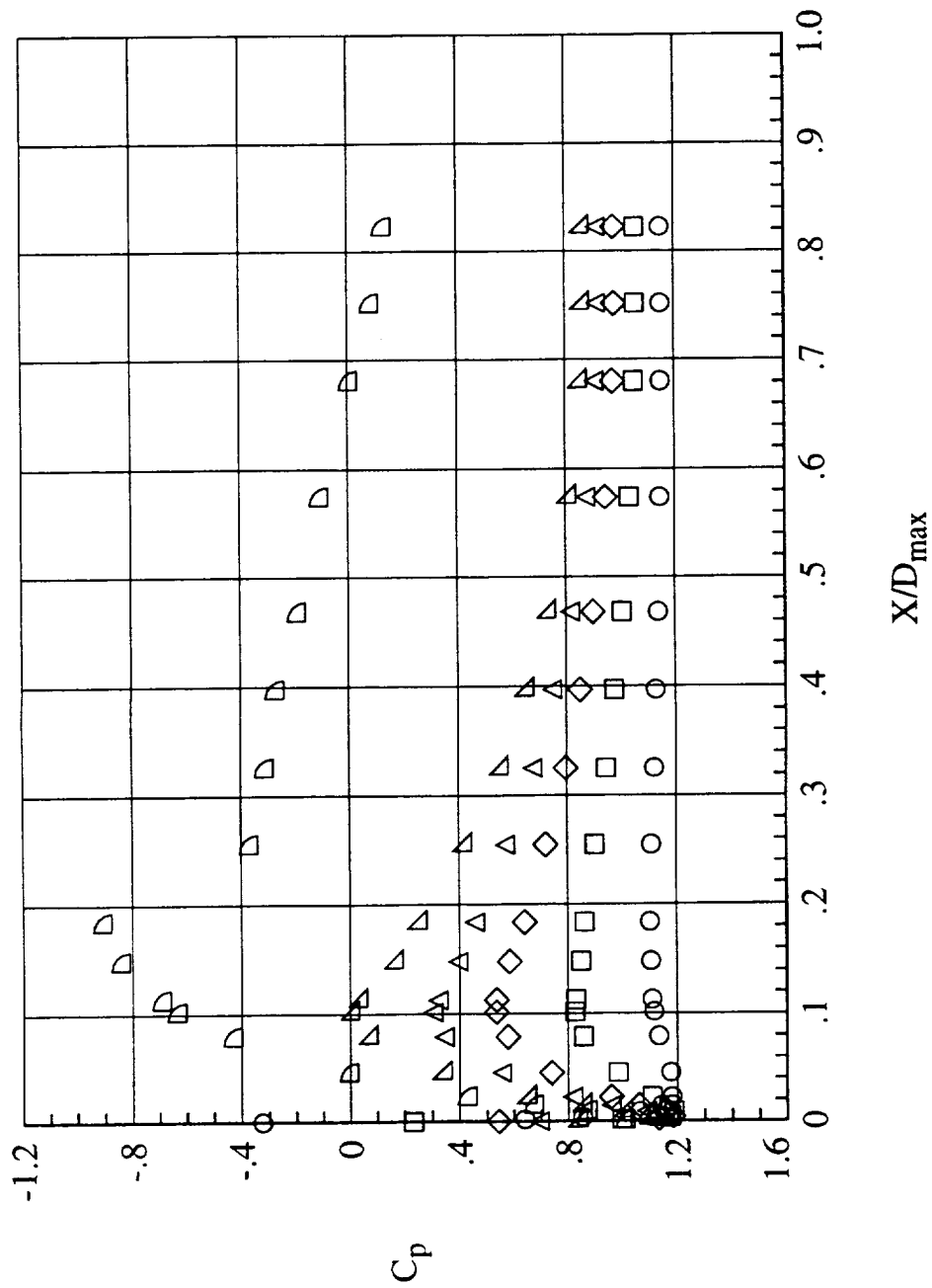
(g) $M = 0.79$.

Figure 14.- Continued.



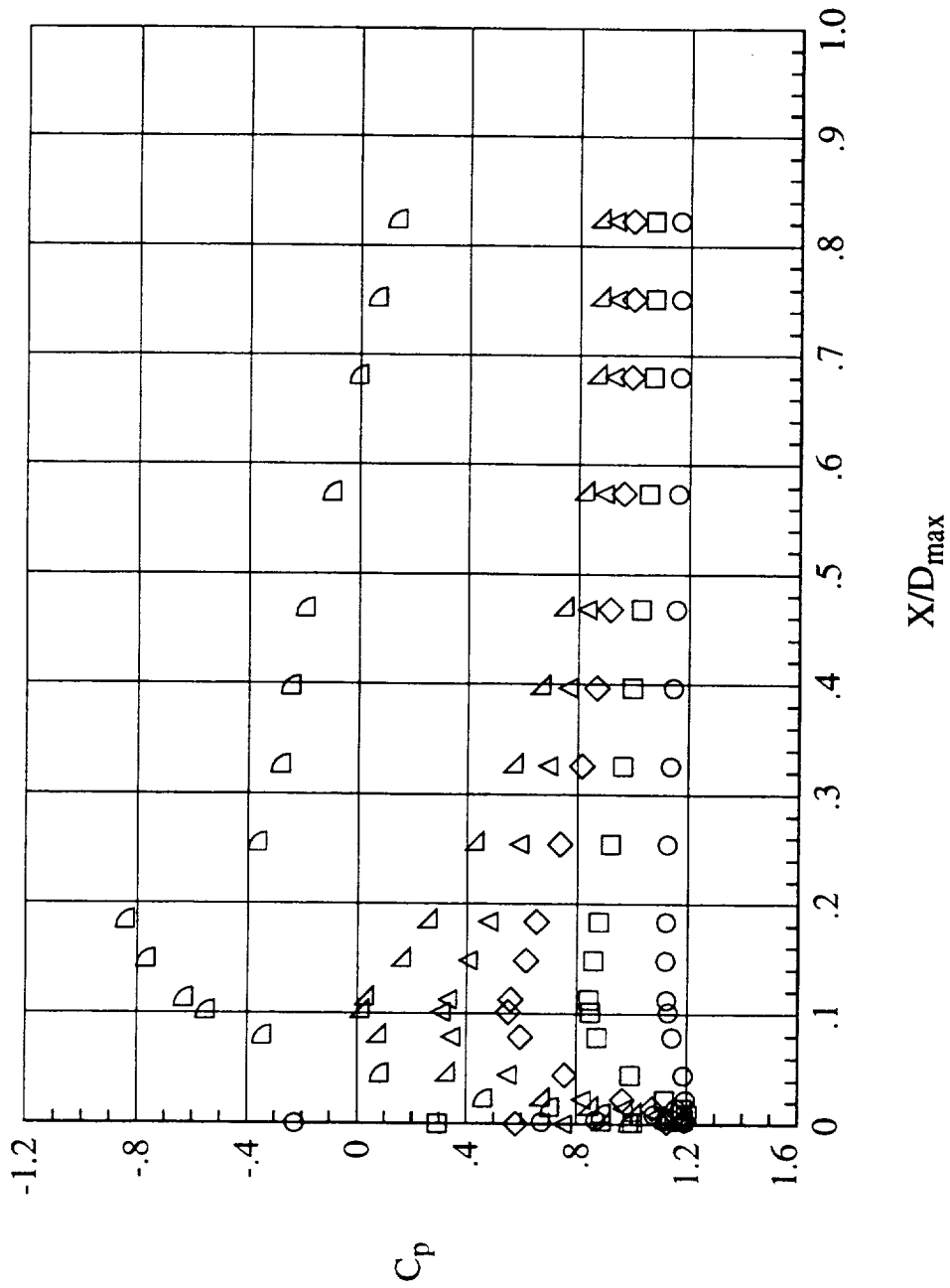
(h) $M = 0.82$.

Figure 14.- Continued.



(i) $M = 0.84$.

Figure 14.- Continued.

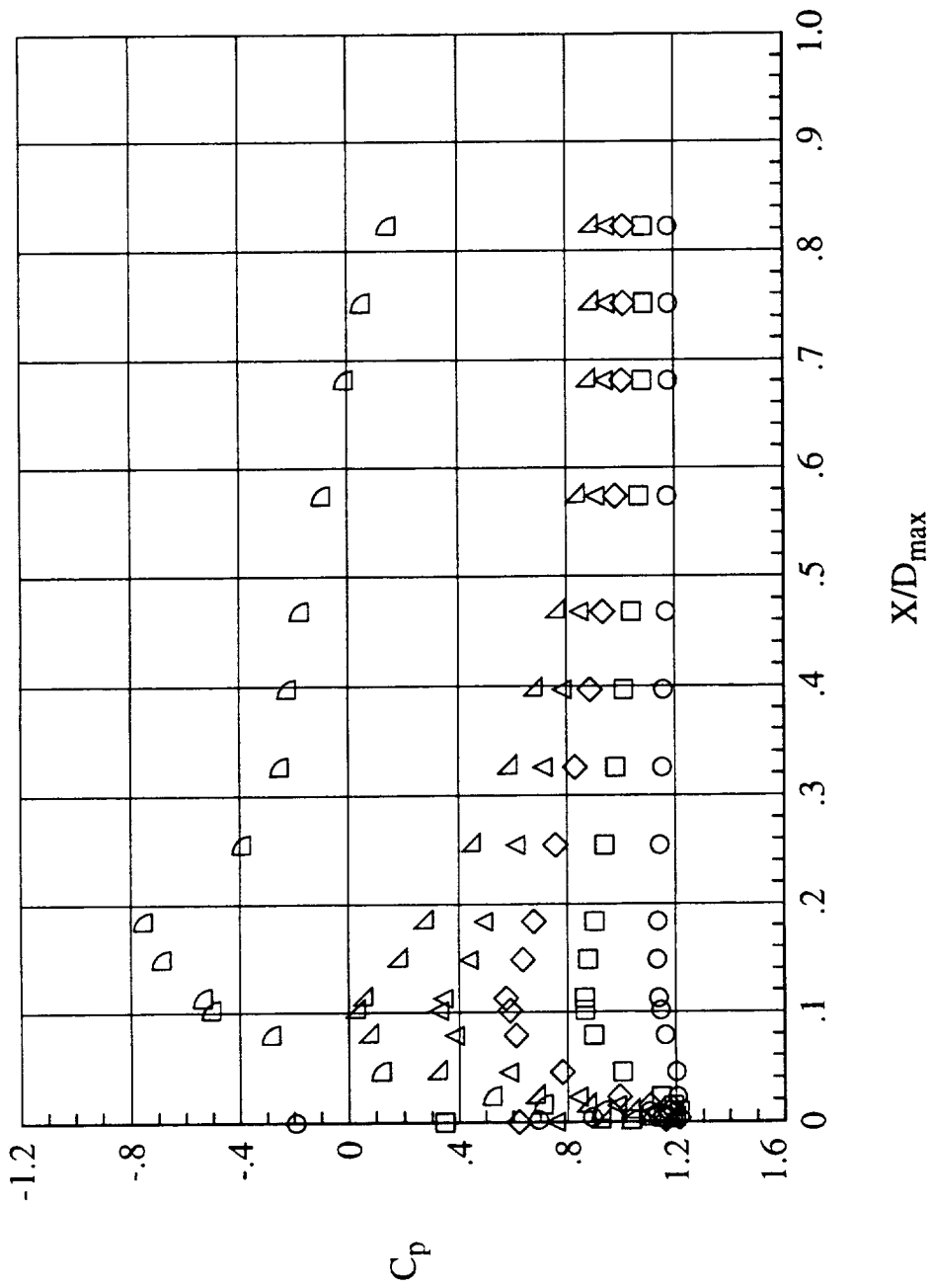


M	mfr	α , deg
0.87	0.27	0.0
0.87	0.50	0.0
0.87	0.61	0.0
0.87	0.68	0.0
0.87	0.74	0.0
0.87	0.83	0.0

○ □ ◇ △ ▴ ▾

(j) $M = 0.87$.

Figure 14.- Continued.

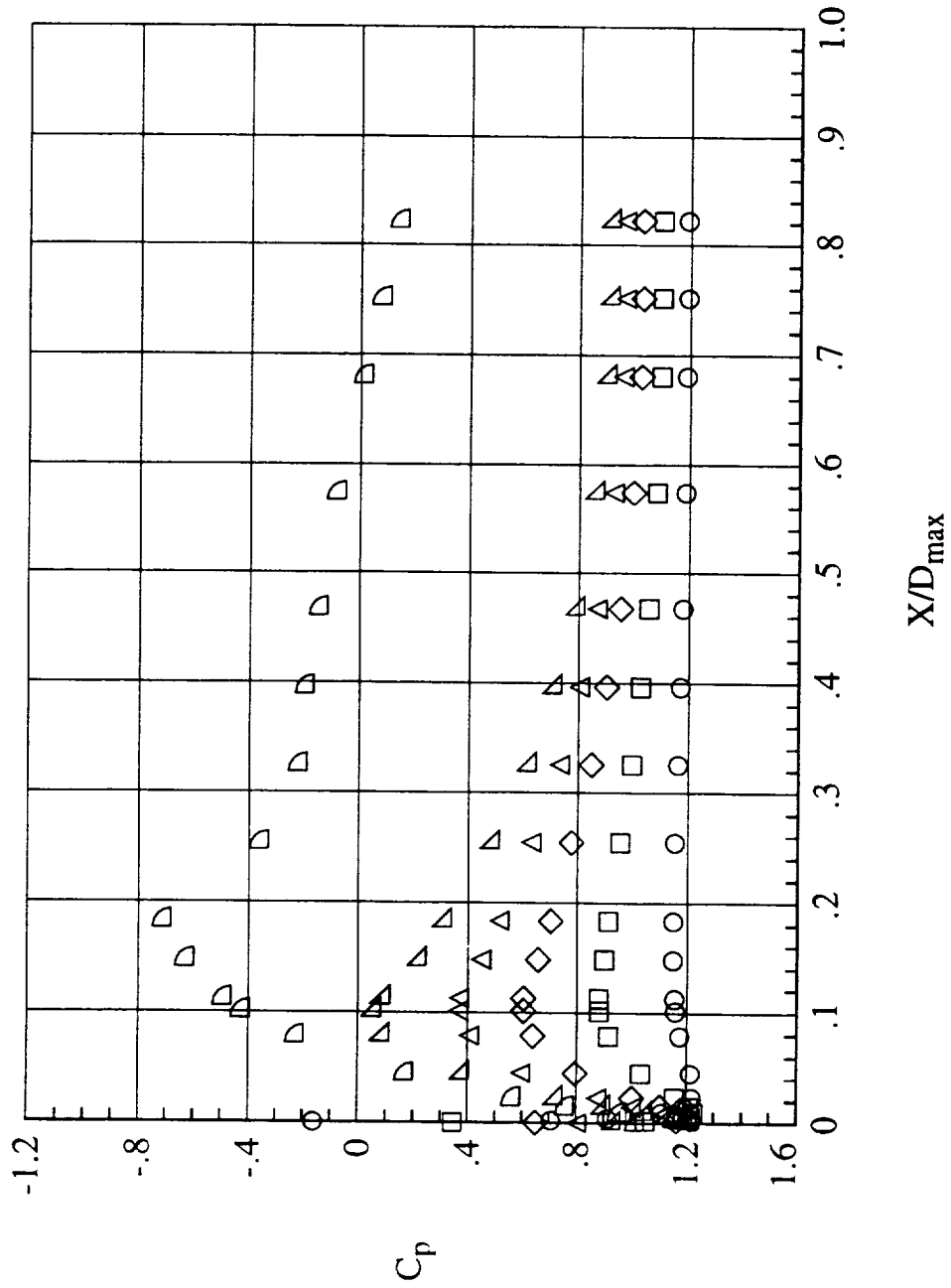


M	mfr	α , deg
0.89	0.27	0.0
0.89	0.49	0.0
0.89	0.61	0.0
0.89	0.68	0.0
0.89	0.74	0.0
0.89	0.81	0.0

○ □ ◇ △ ▽ ▢

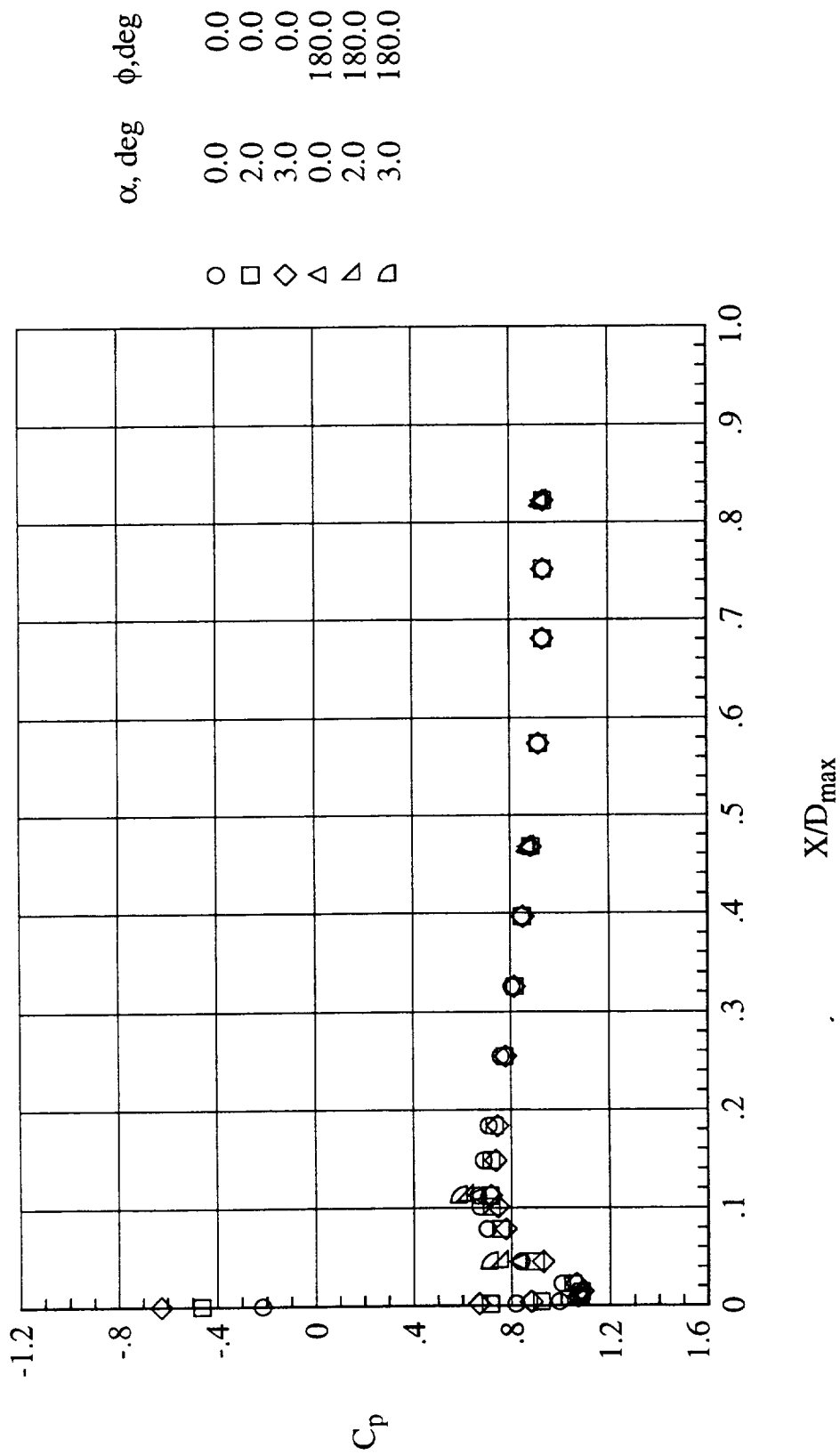
(k) $M = 0.89$.

Figure 14.- Continued.



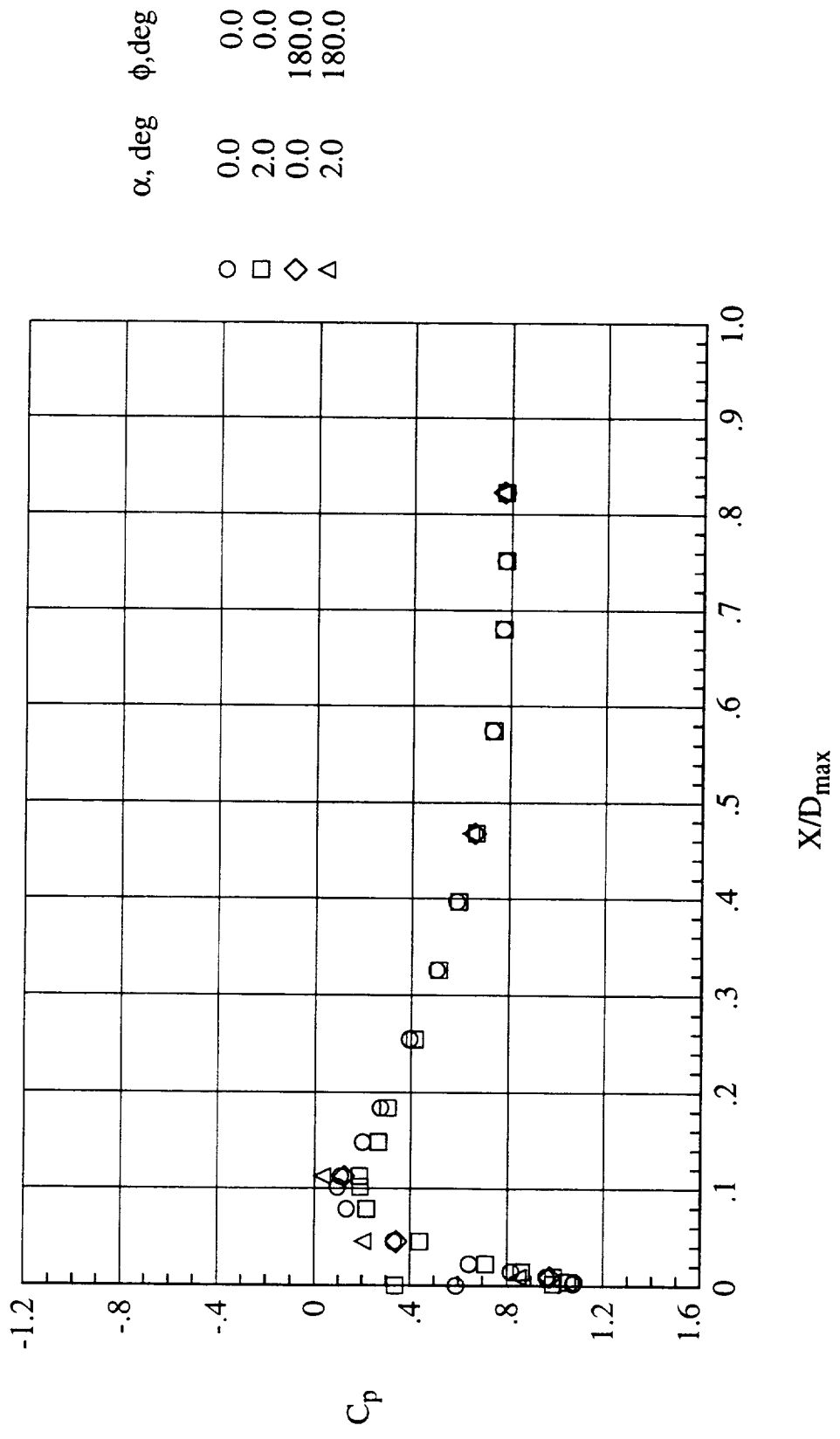
(1) $M = 0.92$.

Figure 14.- Concluded.



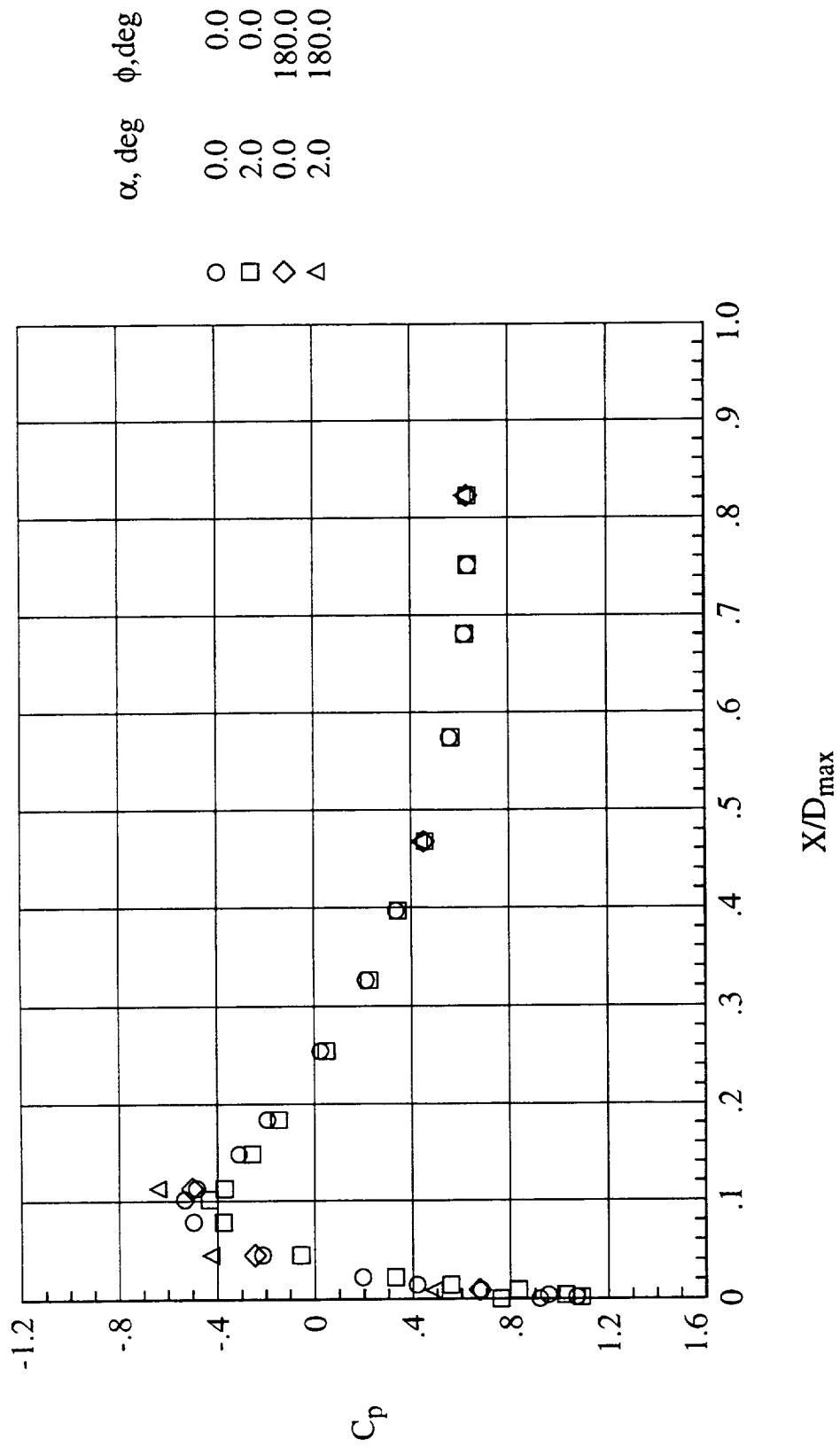
(a) $M = 0.60$ and $mfr = 0.50$.

Figure 15.- Pressure coefficient variation with X/D in the contraction and diffuser portions of the NACA 1-85-43.9 inlet with a contraction ratio of 1.25 for several mass-flow ratios and angles of attack.



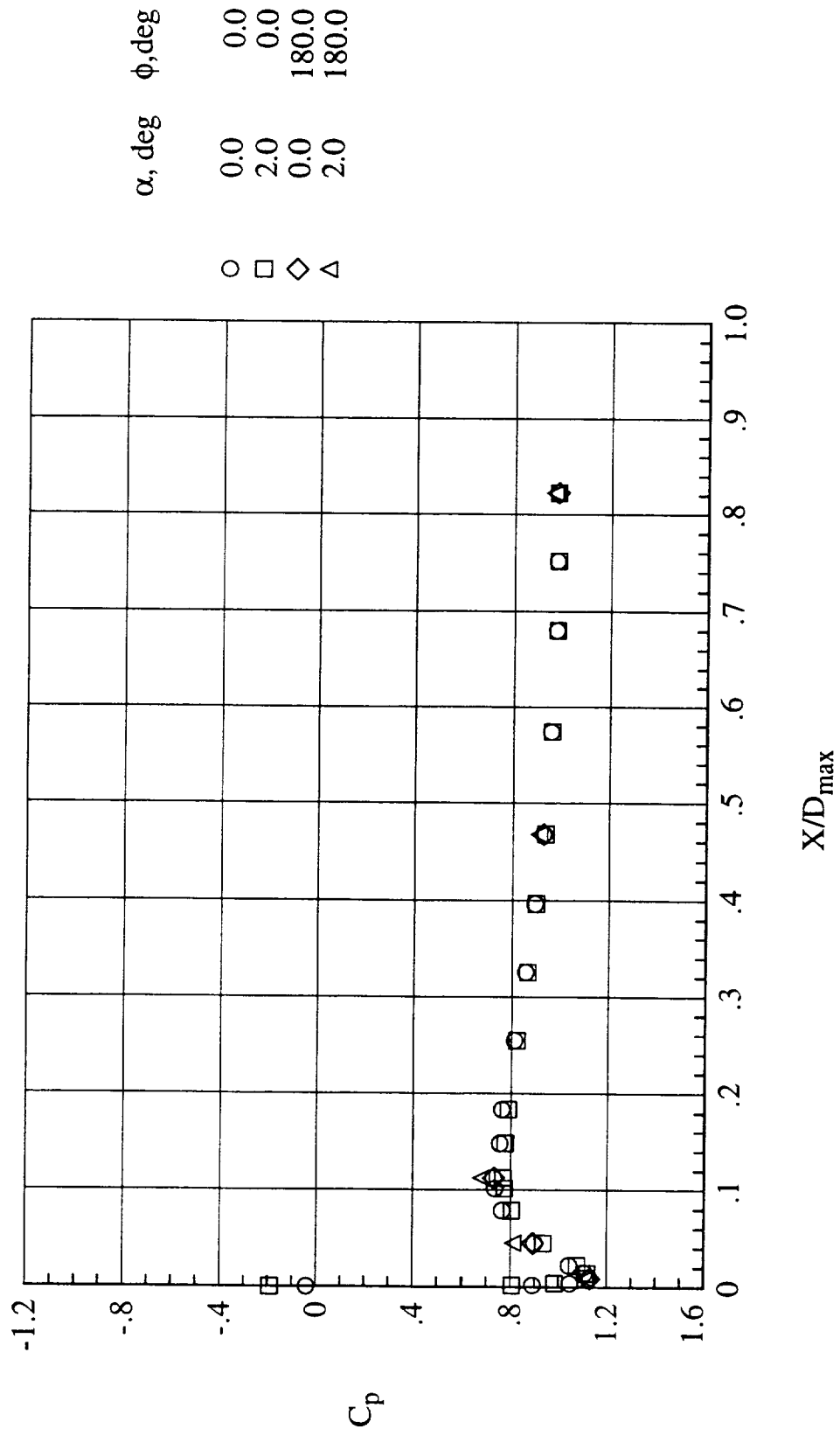
(b) $M = 0.60$ and $mfr = 0.69$.

Figure 15.- Continued.



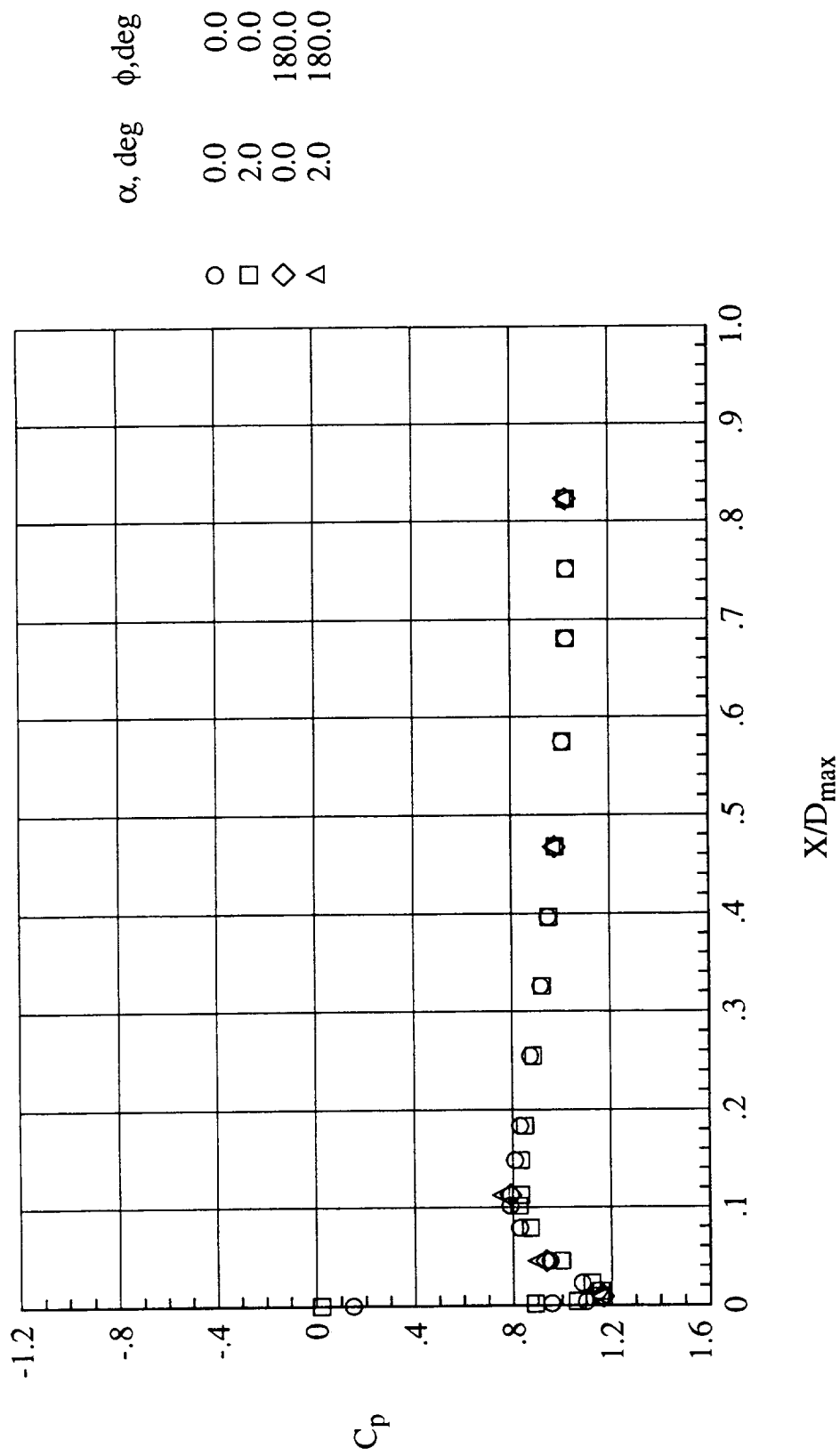
(c) $M = 0.60$ and $mfr = 0.82$.

Figure 15.- Continued.



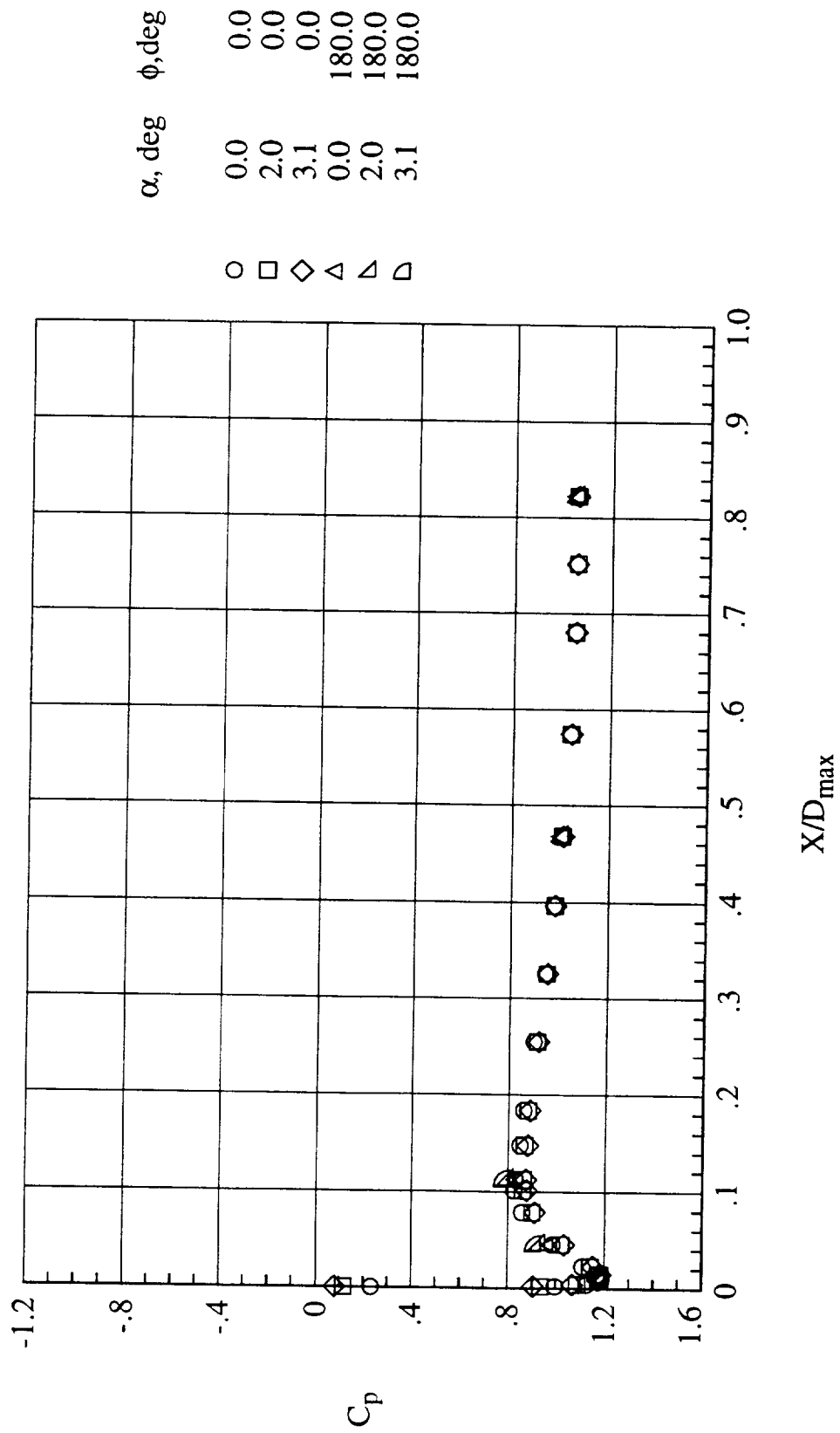
(d) $M = 0.69$ and $mfr = 0.49$.

Figure 15.- Continued.



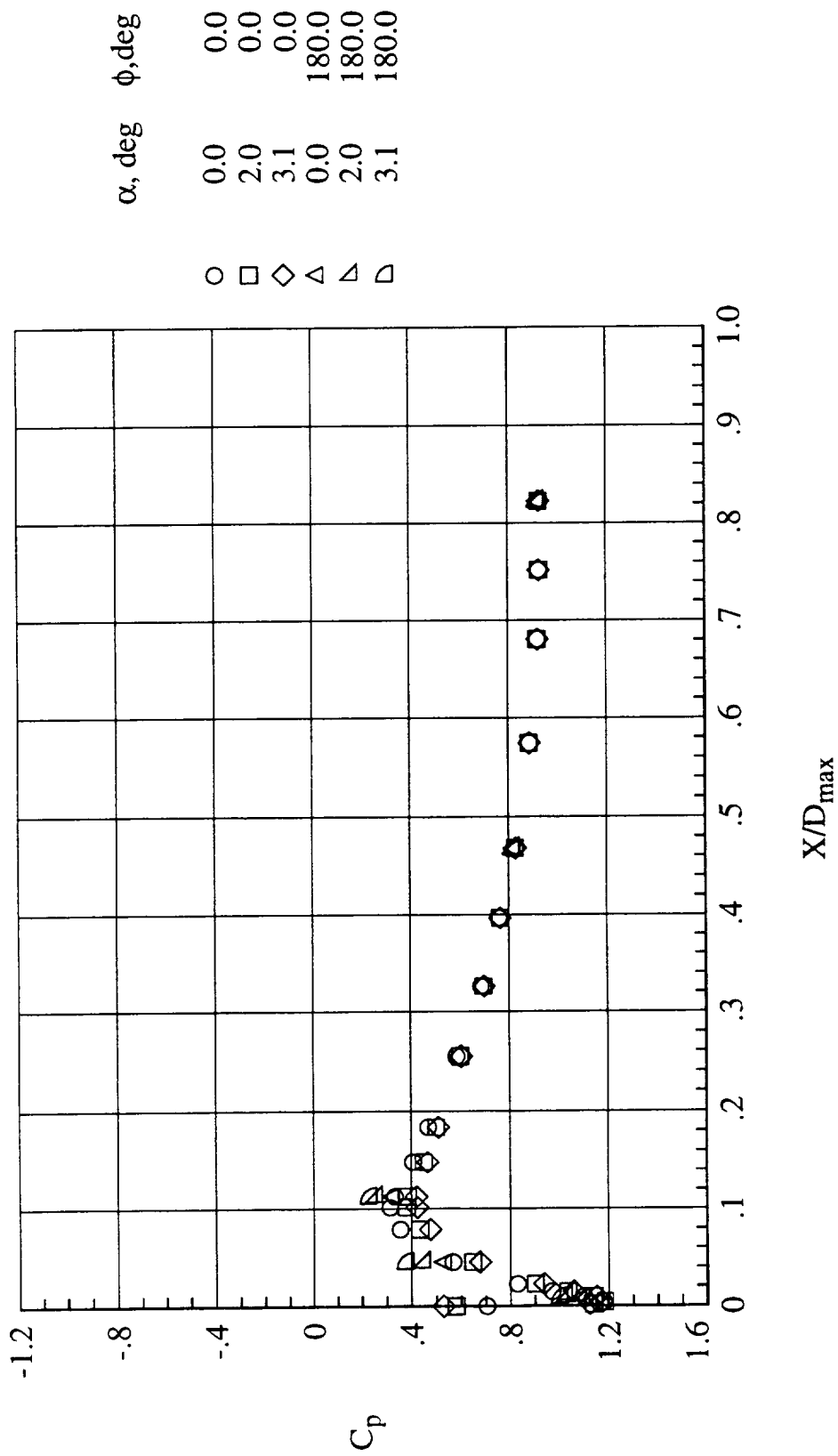
(e) $M = 0.79$ and $mfr = 0.49$.

Figure 15.- Continued.



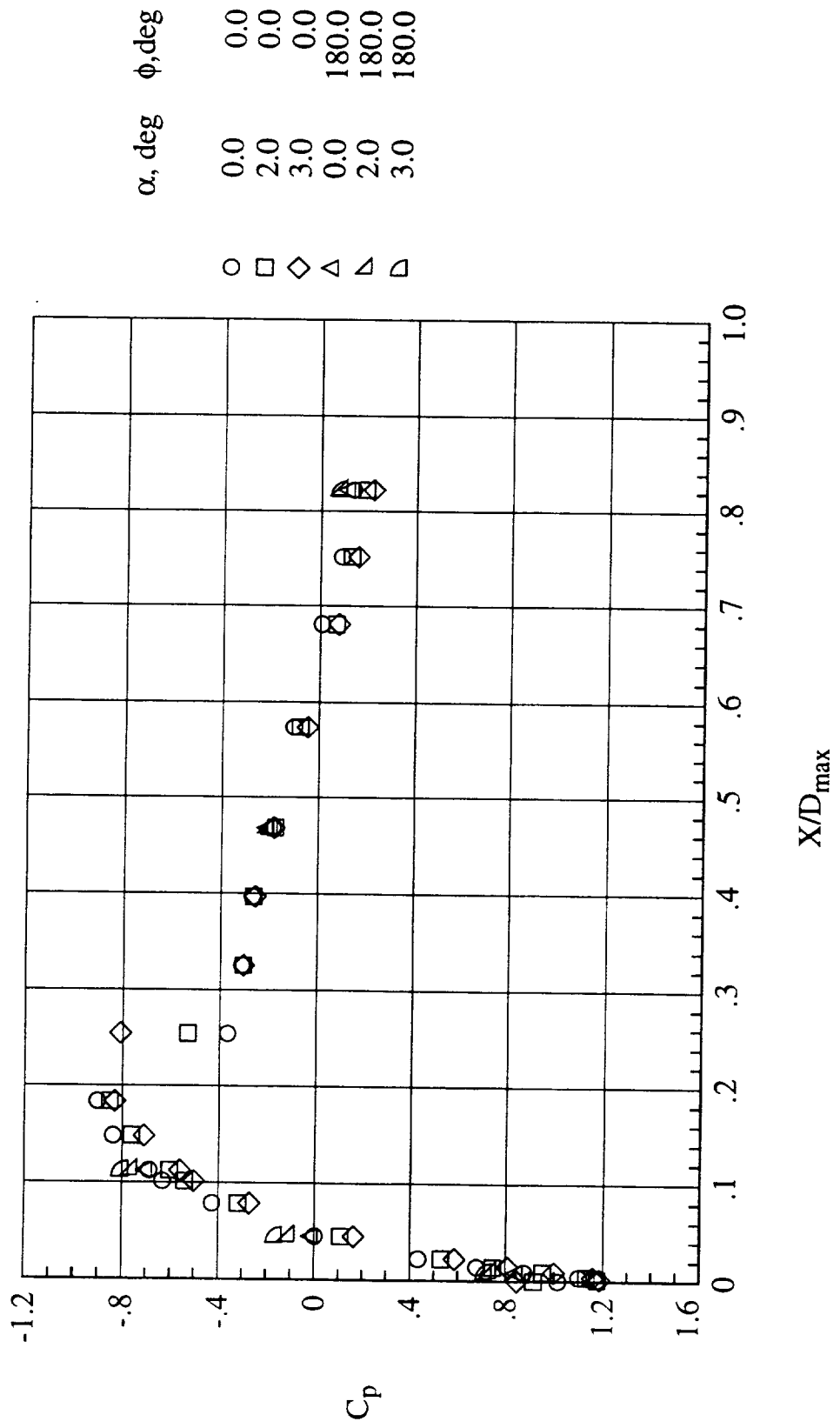
(f) $M = 0.84$ and $mfr = 0.49$.

Figure 15.- Continued.



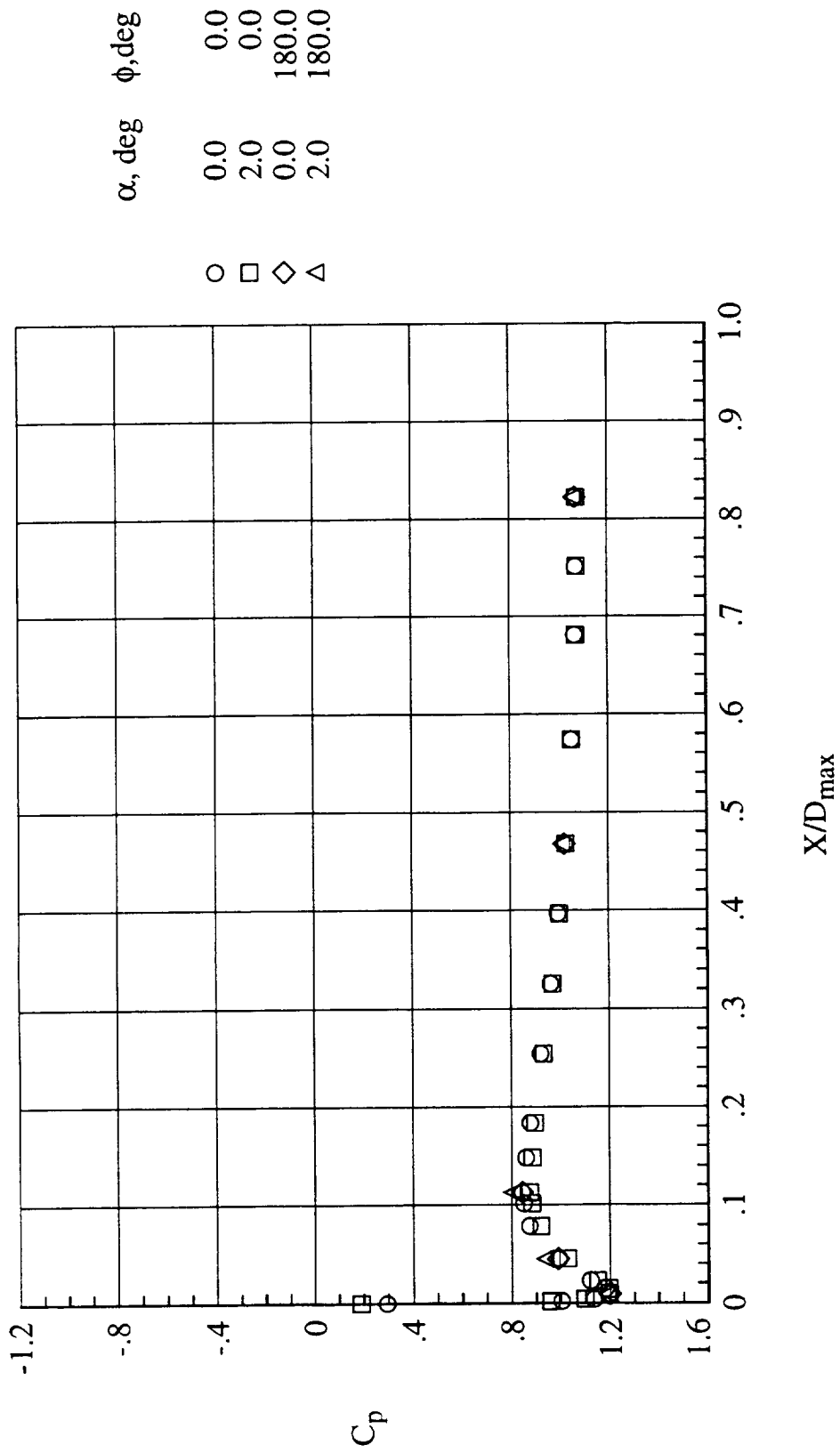
(g) $M = 0.84$ and $mfr = 0.67$.

Figure 15.- Continued.



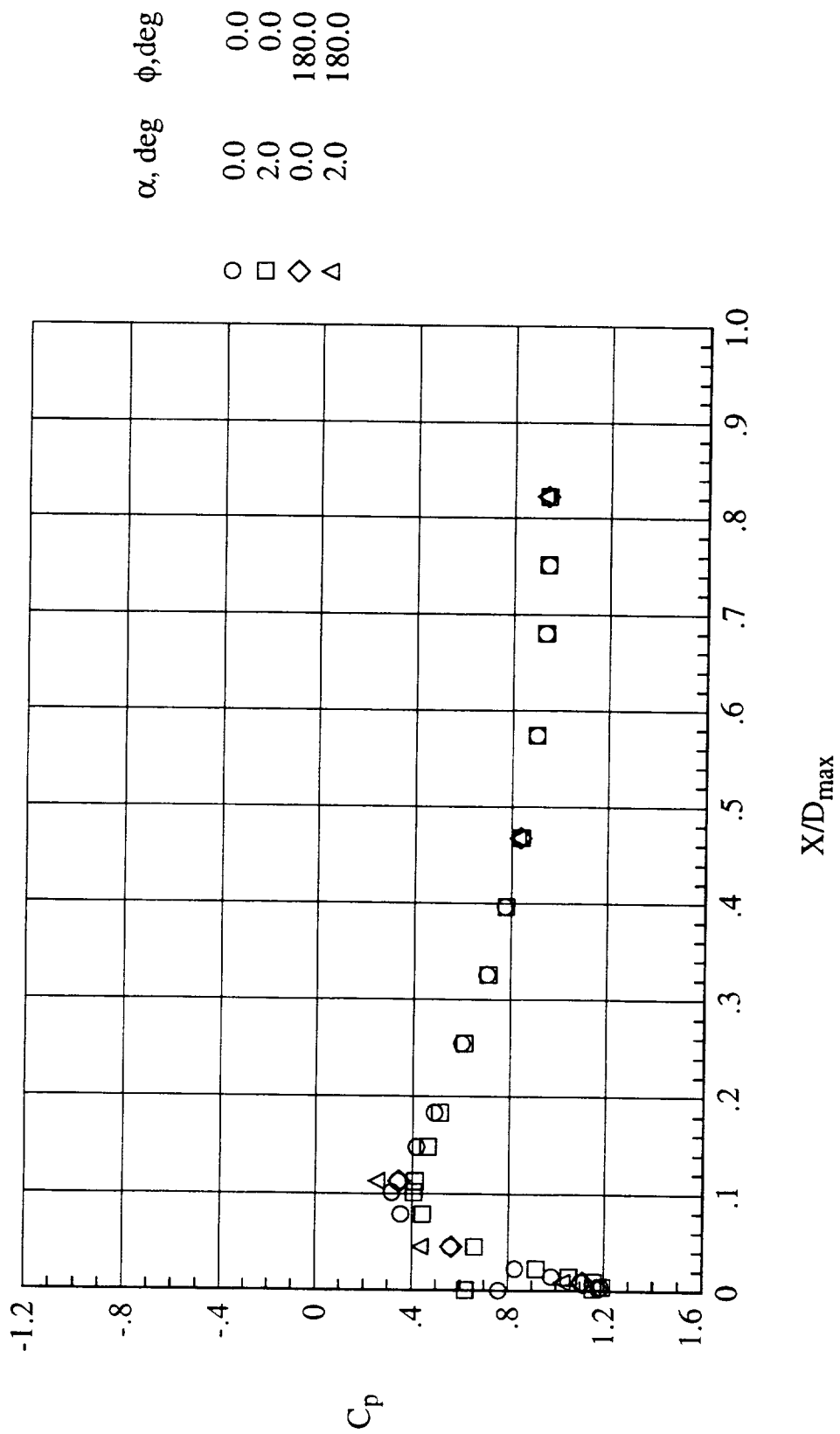
(h) $M = 0.84$ and $mfr = 0.81$.

Figure 15.- Continued.



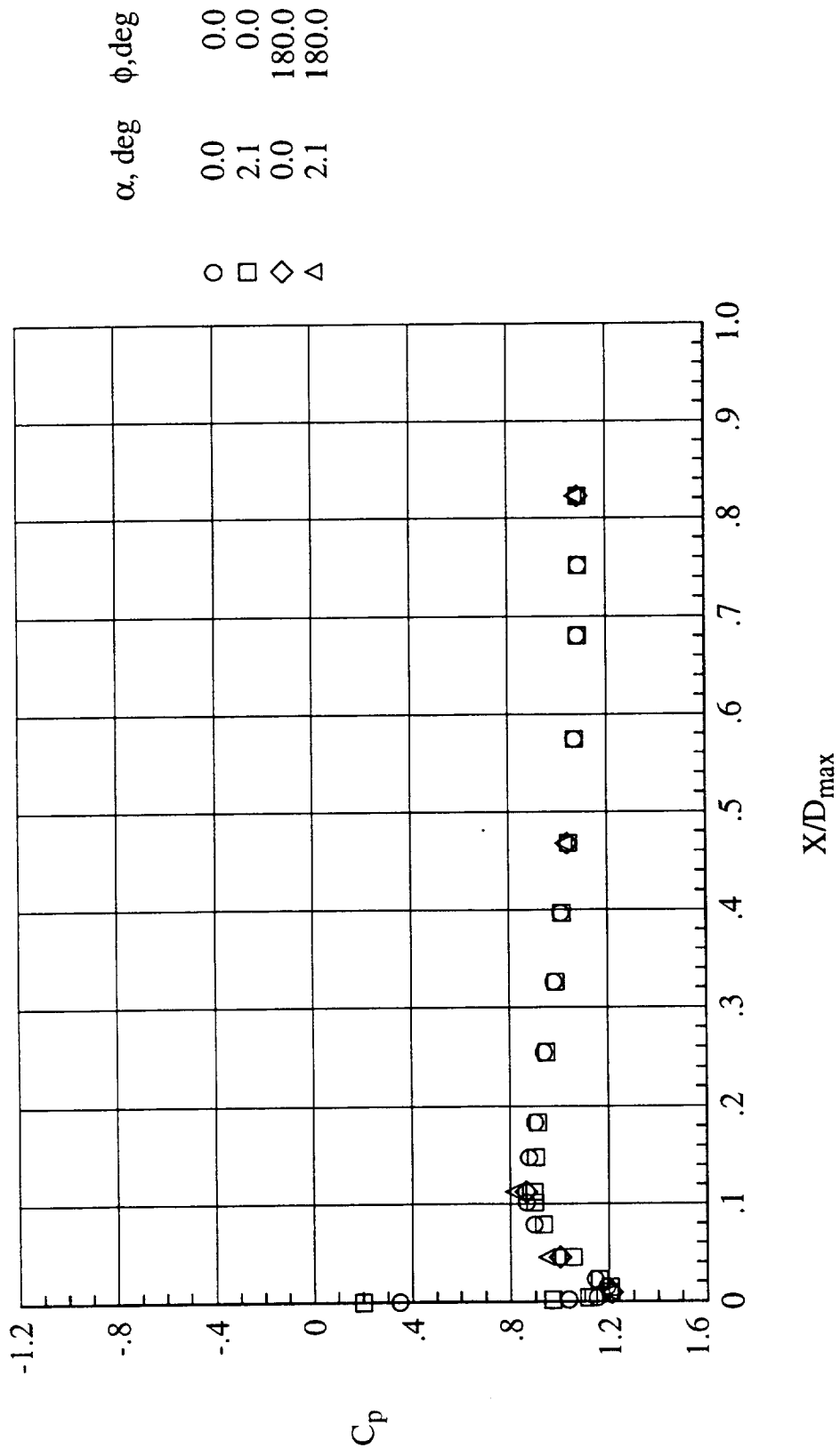
(i) $M = 0.87$ and $mfr = 0.49$.

Figure 15.- Continued.



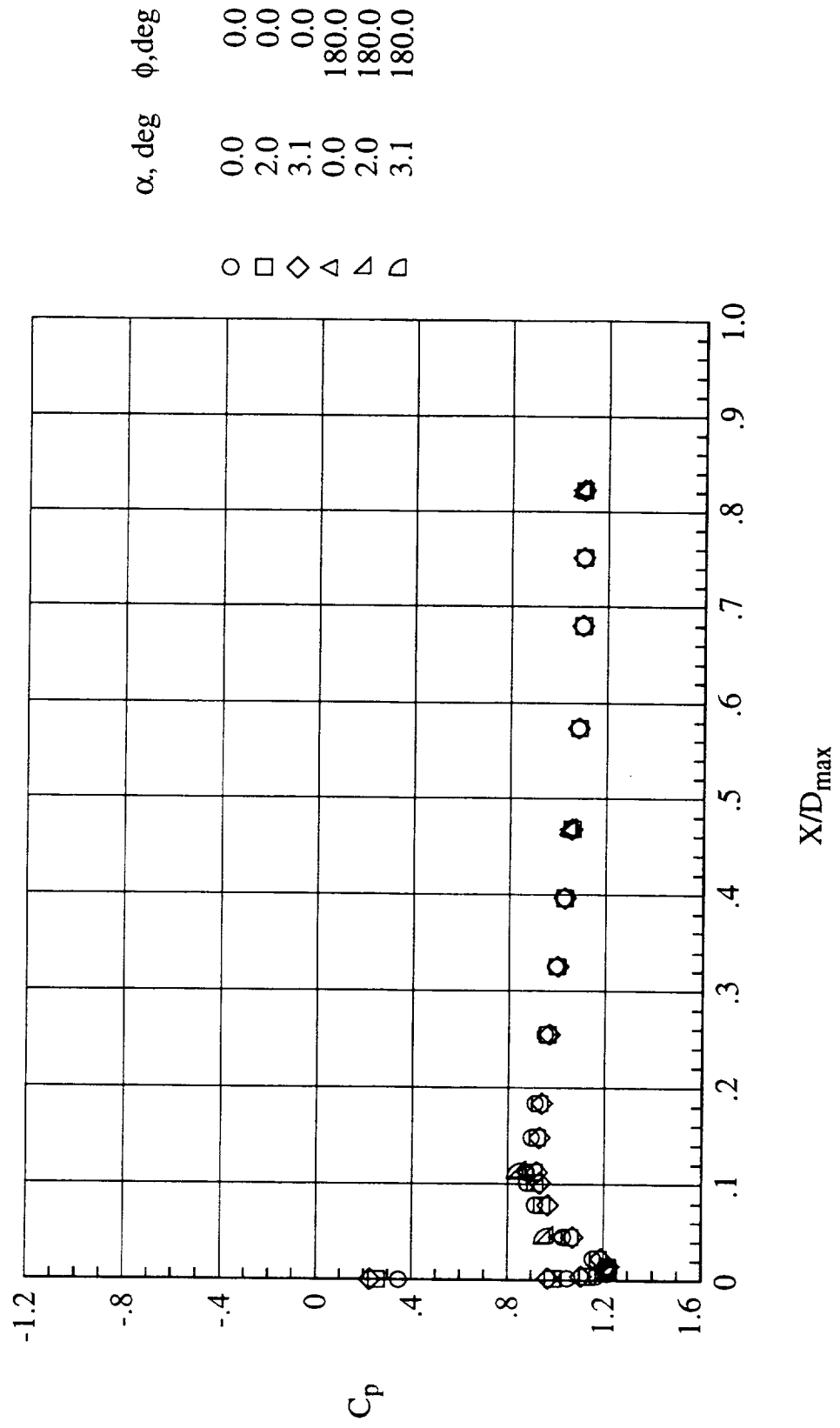
(j) $M = 0.87$ and $mfr = 0.68$.

Figure 15.- Continued.



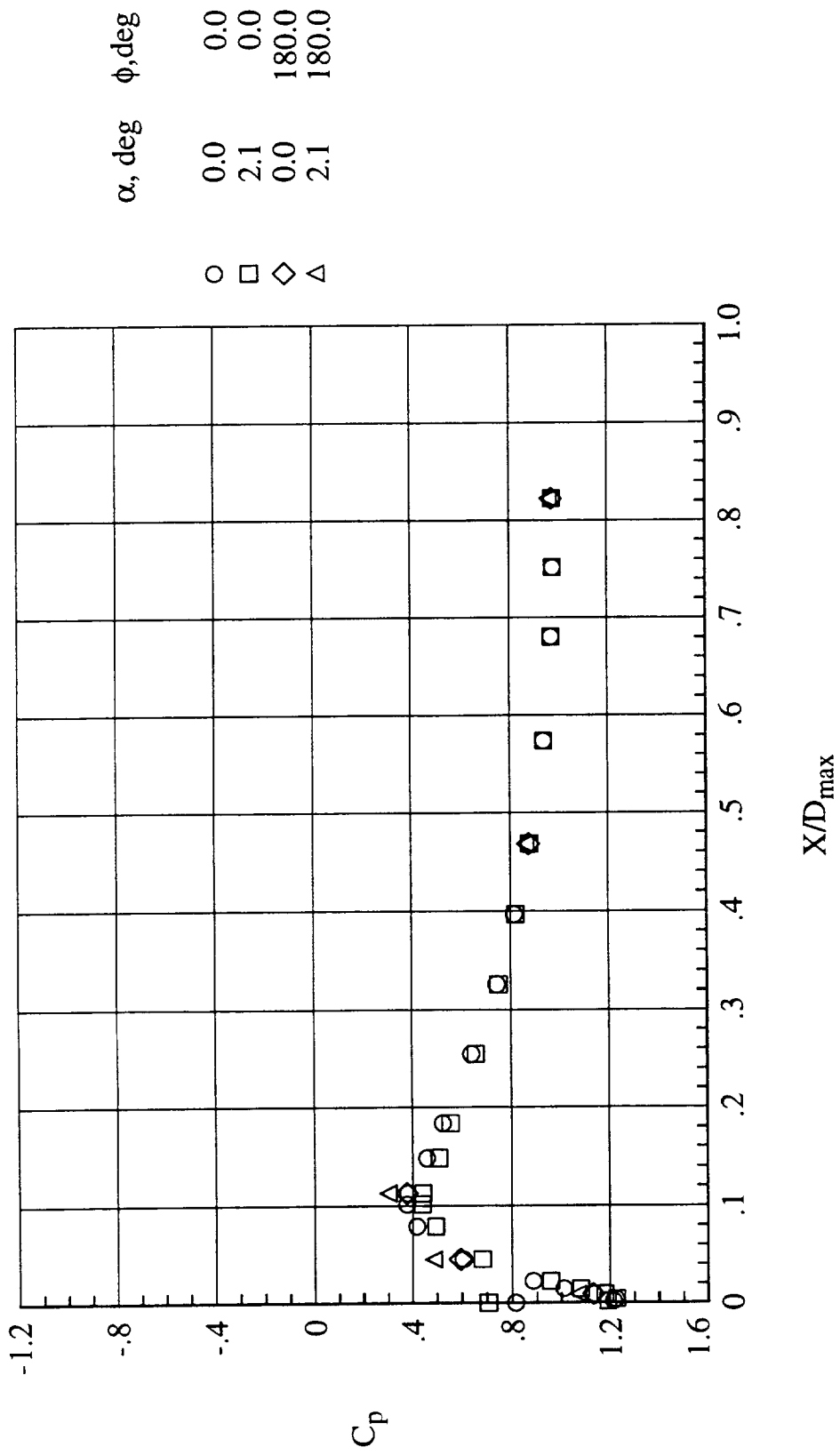
(k) $M = 0.89$ and $mfr = 0.49$.

Figure 15.- Continued.



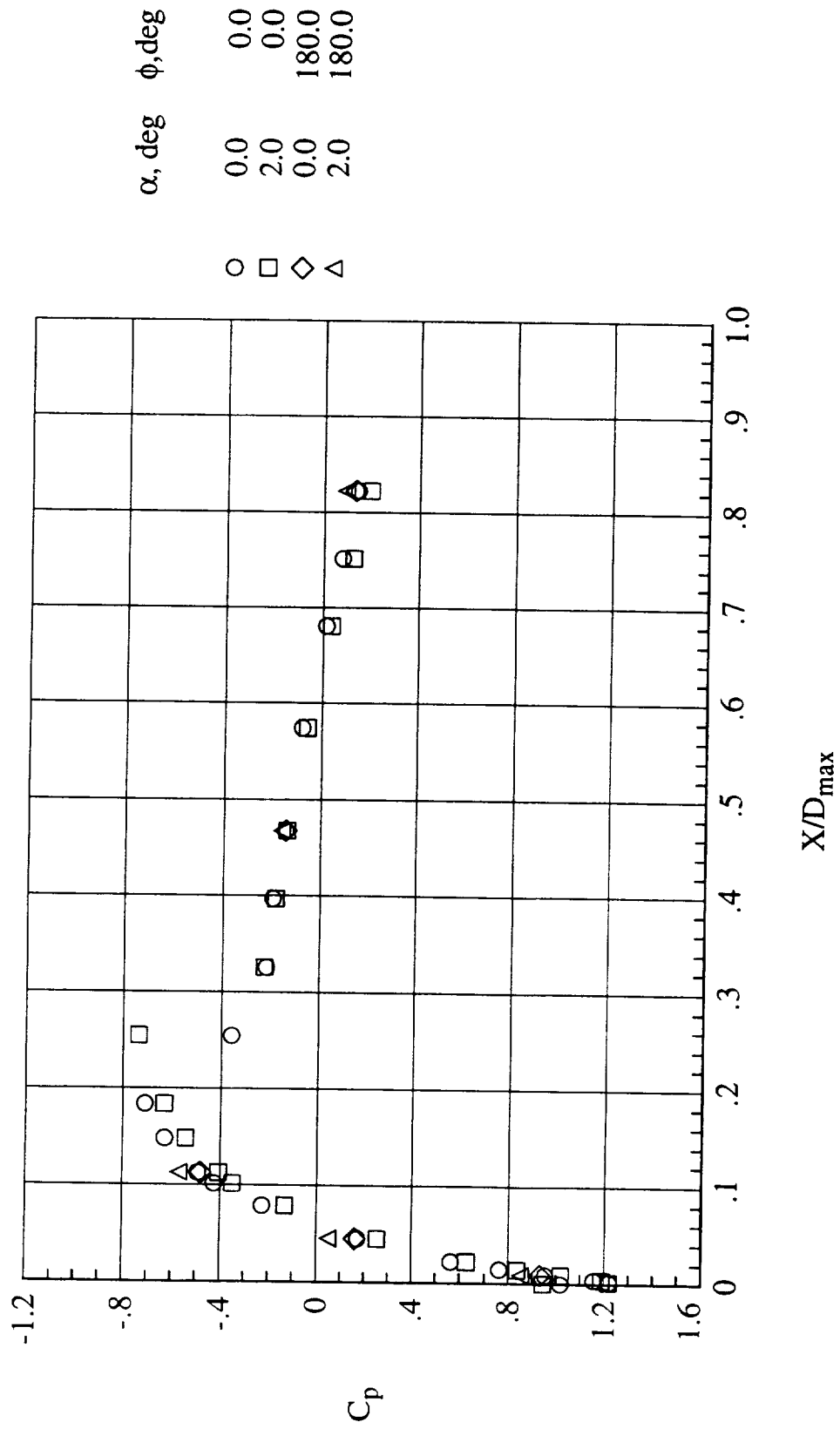
(1) $M = 0.91$ and $mfr = 0.49$.

Figure 15.- Continued.



(m) $M = 0.92$ and $mfr = 0.68$.

Figure 15.- Continued.



(n) $M = 0.92$ and $mfr = 0.82$.

Figure 15.- Concluded.

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13. ABSTRACT (Maximum 200 words) Pressure distributions on three NACA 1-Series inlets have been obtained in the Langley 16-Foot Transonic Tunnel. The cowl diameter ratio (ratio of cowl highlight diameter to cowl maximum diameter) was 0.85 for all three inlets. The cowl length ratio (ratio of cowl length to cowl maximum diameter) was 1.0 for two of the inlets (NACA 1-85-100) and 0.439 for the other (NACA 1-85-43.9) inlet. One of the inlets with a cowl length ratio of 1.0 had an internal contraction ratio (ratio highlight area to throat area) of 1.009 and the other two inlets had a contraction ratio of 1.250. All three inlets had longitudinal rows of static pressure orifices on the top and bottom external cowl surfaces. The two inlets with a contraction ratio of 1.250 had a longitudinal row of static pressure orifices on the diffuser surface.				
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