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## XV-15 Low-Noise Terminal Area Operations Testing

B. D. Edwards Bell Helicopter Textron, Inc., Fort Worth, Texas

National Aeronautics and Space Administration

Langley Research Center Hampton, Virginia 23681-2199 Prepared for Langley Research Center under Contract NAS1-20094

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#### 1. INTRODUCTION

This report describes noise testing of the XV-15 tiltrotor aircraft conducted by the National Aeronautics and Space Administration (NASA) and Bell Helicopter Textron, Incorporated (BHTI) during October and November 1995, at BHTI's test site near Waxahachie, Texas. NASA-Langley Research Center was responsible for overall test direction as well as acoustic and meteorological measurements. NASA-Ames provided aircraft position tracking. BHTI supported the tests by providing the XV-15 aircraft and test site coordination under contract NAS1-20094, Task 3. As an additional effort under this contract, BHTI also developed a computerized visualization tool to display instantaneous noise contours concurrently with XV-15 position and nacelle angle.

This report documents the test setup and procedures used during this program. Acoustic and flight profile data are not included, since these were recorded and analyzed by NASA. Questions concerning the complete database generated during this test should be addressed to Mike Marcolini of NASA-LaRC.

#### **1.1 PURPOSE OF TEST**

Noise impact is currently considered to be a major obstacle to developing the tiltrotor's full potential within the civil transportation system. If this potential is to be realized, noise reduction must be considered in each new tiltrotor design, and low-noise operating techniques must be defined for all tiltrotors. The purpose of this test was to support the noise reduction design and operation of future tiltrotors. The stated objectives were to:

- provide a comprehensive acoustic database for NASA and U.S. industry
- validate noise prediction methodologies, and
- develop and demonstrate low-noise flight profiles.

This is the latest in a series of XV-15 noise tests aimed at understanding the noise characteristics of the relatively new tiltrotor aircraft (References 1 through 4). The timeline shown in Figure 1 illustrates the history leading up to the current test. Primary emphasis was given to the approach flight condition where blade-vortex interaction (BVI) dominates the noise signature. Since this flight condition influences community noise impact more than any other, an understanding of the noise generating processes is required to guide the development of low noise flight operations. This, in turn, can substantially reduce the tiltrotor's impact on the community.



Figure 1. XV-15 Noise Test History Leading Up to the Present Test

#### 2. TEST DESCRIPTION

The test consisted of two distinct phases: Phase 1 provided an acoustic database for validating analytical noise prediction techniques, and Phase 2 directly measured large area noise impact over a broad range of operating profiles.

#### 2.1 TEST SITE

Testing was performed in a rural area near the town of Waxahachie, Texas, on an available tract of land that had been the site of the former Superconducting Super Collider (SSC). The site is sufficiently remote that the ambient noise levels were low, 35-40 dBA, yet near enough to the Dallas-Fort Worth area to allow flight operations out of BHTI's Arlington flight facility. The terrain is flat with few trees, and during the test the ground was covered with short, mowed grass.

Since the XV-15 is not equipped with a particle separator, a helipad was constructed for hovering flight. Figure 2 shows the XV-15 hovering above this pad. The terrain in the background is typical of the topography at this site.



Figure 2. XV-15 Over Helipad Constructed for Tests

#### 2.2 PERSONNEL/ CREW ASSIGNMENTS

As stated earlier, NASA-LaRC was responsible for the overall test direction and for selecting test points and flight procedures that would receive the highest priority. These selections were made with the assistance from BHTI and other industry members and from NASA-Ames/Army handling qualities/simulation personnel, notably Mr. Bill Decker. Handling qualities were

considered an integral part of the program to ensure that any "low noise" flight operations were practical ones which could actually be used in a commercial tiltrotor.

NASA-LaRC provided equipment and personnel for acoustical (30 microphone stations) and meteorological measurements during the test, and for overnight analysis of each dataset. The NASA-LaRC team included personnel under contract from Wyle and Lockheed.

NASA-Ames supported the test by providing the XV-15 position tracking. A laser optical tracking system, discussed later (Section 2.3.3) provided precision readouts of x, y, and z position. This system required a substantial support team headed by NASA-Ames and assisted by personnel from Recom and Stering.

BHTI provided the XV-15 aircraft and flight support, as well as test site coordination. BHTI monitored and recorded acoustically influential aircraft parameters, including rotor RPM, nacelle angle, flap angle, airspeed, and radar altitude.

A list of personnel involved in the test is given in Appendix A. Each individual's responsibilities during the test are given, along with his company affiliation.

#### Aircraft Description

The XV-15 tiltrotor has a design gross weight of 13,200 pounds, and was built by BHTI as a proof-of-concept aircraft and technology demonstrator with first flight in May 1977. The aircraft has a fuselage, empennage, and fixed wings similar to those of a conventional airplane, with an engine/nacelle/rotor assembly mounted on each wingtip. Each nacelle houses a main transmission and a Lycoming T-53 turboshaft engine capable of generating 1800 shaft horsepower. A cross-shaft connects the two transmissions for transient power transfer and one-engine-out operation. Rotor orientation is changed by pivoting the nacelles with respect to the wings. The wings are swept forward 6.5 degrees to provide clearance for rotor flapping during forward flight in the airplane mode. Figure 3 shows the XV-15 in transitional flight, with nacelles tilted approximately 60 degrees. Only two flight aircraft were built, Tail Numbers N702NA and N703NA. Both have been extensively tested to define the capabilities and limitations of the tiltrotor concept, and have successfully demonstrated the practicality of this new aircraft type. Aircraft #2 (Tail Number N703NA) was used in the tests described in this report.

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The XV-15 test aircraft, shown in Figure 3, has two 25-foot diameter rotors mounted on wingtip nacelles that are capable of tilting from approximately 95 degrees (helicopter mode) to 0 degrees (airplane mode). Each rotor has three highly twisted, square-tip metal blades. The XV-15 rotors typically operate at 589 RPM during the hover mode and transition, but are reduced to 517 RPM for high speed forward flight. The RPM's correspond to 98% and 86% of rotor design speed. Major XV-15 aircraft parameters are listed in Table 1. A more detailed description of the XV-15 is available in Reference 5.



Figure 3. XV-15 Aircraft #2 (N703NA) Used in Noise Tests

TABLE 1.	XV-15	TILTROTOR	<b>DESIGN AND</b>	<b>OPERATING</b>	<b>PARAMETERS</b>
----------	-------	-----------	-------------------	------------------	-------------------

GROSS WEIGHT	13,200 lb.
PROPS/ROTORS (2)	
NUMBER OF BLADES	3
DIAMETER	25 feet
ROTATIONAL SPEED	601 RPM @ 100%
	589 RPM @ 98% (HELICOPTER MODE)
	517 RPM @ 86% (AIRPLANE MODE)
ROTATIONAL TIPSPEED	771 FEET PER SECOND @ 98%
	677 FEET PER SECOND @ 86%
ENGINES (2)	LYCOMING T53

The XV-15 flight envelope, shown in Figure 4, illustrates the combinations of nacelle angle and airspeeds for stabilized flight. It should be noted that a fairly broad range of nacelle angles and airspeeds is possible within this operating envelope. The acoustic effects of avoiding certain portions of this envelope can guide flight operations of the XV-15 (and presumably other tiltrotors) in minimizing external noise. The present test was designed to extend the body of information available to define these effects.



Figure 4. XV-15 Flight Envelope

#### 2.3 TEST SETUP

The general layout of the test site is shown in Figure 5. The flight track was selected so the microphone array would be in the flattest portion of the terrain, away from trees and easily accessible by vehicle. NASA-LaRC acoustic recording equipment was housed in instrumentation vans, with 10 microphone sites being supported by each van. A trailer was set up south of the flight track to serve as control headquarters for the test. The optical tracker site, north of the flight track and offset by about 4700 feet, was on a rise which commanded a view of the entire flight track, allowing for early acquisition of the aircraft. A weather balloon was deployed near the tracker site to acquire layered atmosphere data, and ground-based meteorological data was recorded at the BHTI van and at one of the NASA vans. Aircraft parameters were recorded onboard the XV-15.



Figure 5. XV-15 Noise Test Setup (Phase 1 Test)

All datasets were recorded in parallel with a satellite-synchronized time code signal. Prior to each flight, the XV-15's onboard timecode generator was synchronized with a satellite time code unit at the BHTI Flight Test Center to provide time correlation between airborne and ground based recordings. During the test, safety of flight data was telemetered from the XV-15 to the ground station at the test site command post, where it was monitored continuously.

#### 2.3.1 Acoustic Measurements

During "Phase 1" testing, noise was measured with microphones arranged as shown in Figure 6. This is a fairly linear array oriented perpendicular to the flight track, and extending about 2300 feet to each side. The exact positions are given in Appendix B. The purpose of this phase was to provide data to support noise prediction efforts and to document tiltrotor sound characteristics at specific points in the flight envelope. XV-15 flight conditions consisted of descents, level flights, takeoffs, and hover.

In "Phase 2" testing, the microphones were re-deployed over a large ground area near a simulated "vertiport", as shown in Figure 7. The purpose was to define maximum and minimum noise contours for civil vertiport land use planning. As in the initial Phase 1 testing, the flight conditions consisted of descents, level flights, takeoffs, and hover.



Bell Microphones

Figure 6. Phase 1 Testing: Linear Microphone Array



Bell Microphones



The sequence of testing, along with field notes made by the author, is listed in Appendix C.

#### 2.3.2 Meteorological Measurements

Acoustic testing was generally conducted when weather conditions met the following criteria:

- average surface (10 meter above ground level) winds less than 10 knots
- relative humidity less than 95%
- no precipitation present
- visibility greater than 3 miles
- ceiling greater than 1500 feet.

Because of the low wind requirements, early morning flights were scheduled. Based on weather information available at 3:00 PM prior to each potential test day, plans for the next day's testing were made.

During testing, meteorological data was recorded at the BHTI acoustics van, where monitor instrumentation was located on a 10-meter tower. These data are presented graphically in Appendix D. In addition, NASA monitored meteorological conditions at a ground tower and aloft on an airborne weather balloon positioned near the flight track. Figure 8 shows NASA's ground tower.

#### 2.3.3 Position Tracking System

Aircraft position was monitored and recorded during the test by an optical tracking system provided by NASA Ames. A photo of the tracker support vans is shown in Figure 9. This system provided a continuous, real-time display of longitudinal (x), lateral (y), and vertical (z) aircraft position to a display in the XV-15 (Figure 10) and to a monitor in the control trailer (Figure 11). The tracker's ground station generates and directs a laser beam toward the aircraft, where an aircraft-mounted retro-reflector reflects the beam back to the ground station. The retro-reflector mounted on the XV-15 is shown in Figure 12. The ground station was stabilized at a known, pre-surveyed position with respect to the flight track, and the measured return time of the beam, along with precise knowledge of the its azimuth and elevation, provided a very accurate ( $\pm 1$  meter) measure of x,y, and z position at a sample rate of 10 per second. The ground station was located approximately 4700 feet north of the flight track (see Figure 13).

To assist the pilot in setting up each pass, three 1000-watt lights were stationed along the track. By aligning these lights, the pilot could enter each pass very accurately, so that only small corrections were necessary when the tracker acquired the XV-15 and enabled the onboard position indicator. One of these lights is shown in Figure 14.



Figure 8. NASA's Weather Tower



Figure 9. NASA-Ames Mobile Optical Tracker



Figure 10. XV-15 Cockpit



Figure 11. Headquarters Trailer with Test Personnel



Figure 12. XV-15 Details



Figure 13. Optical Tracking Station

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Figure 14. Flight Track Marker

#### 2.3.4 Aircraft Parameters

An onboard recording system monitored basic aircraft flight and operating parameters. These were recorded in flight, then analyzed and permanently stored. Table 2 is a list of the flight data recorded during these tests.

DATA CODE	ITEM CODE	DESCRIPTION	UNITS
00DV02	P342	BOOM ALTITUDE	FT
00DV04	D327	RADAR ALTIMETER	FT
00QP01	D010	PITCH ATTITUDE	DEG
00QP02	D008	ANGLE OF ATTACK	DEG
00QQ01	D011	YAW ATTITUDE	DEG
00QQ02	D007	ANGLE OF SIDE-SLIP	DEG
00QR01	D009	ROLL ATTITUDE	DEG
00VF03	P002	BOOM AIRSPEED	KNOTS
00VV02	<b>V086</b>	RATE OF CLIMB	FT/MIN
10DF04	DO21	F/A CYC STICK CONTROL POSN	%
10DF05	DO24	RUDDER PEDALS CONTROL POSN	%
10DF06	DO23	POWER LEVER CONTROL POSN	%
10DL02	DO22	LAT CYC STICK CONTROL POSN	%
12DM13	D617	FLAP POSITION	DEG
25DM12	D161	#2 PYLON CONVERSION POSN	DEG
25DM13	D186	#1 PYLON CONVERSION POSN	DEG
30RM03	R106	ROTOR RPM (@ reduced sample rate)	%

#### **TABLE 2. FLIGHT DATA RECORDED DURING TESTS**

#### 2.4 PHASE 1. "LINEAR" MICROPHONE ARRAY TESTING

Phase 1 testing was accomplished on 9 test days during 1995. October 10, 12, 16, 27, 28 and November 1,4,7, and 8.

The linear microphone array consisted of 17 microphones along a line perpendicular to the flight track, and an additional 3 microphones along the flight track. The exact positions are given in Appendix B. An aerial view of a portion of the linear array is shown in Figure 15.

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#### 2.4.1 Flight Conditions

The XV-15 passed over the microphone array at constant airspeed/nacelle angle combinations and constant flight angles. Test conditions consisted of level flights, descents, climbs, and hover as defined in Appendix E. Prior to the test, each condition was assigned a priority classification of 1, 2, or 3. The "priority 1" conditions were considered essential to the overall test objectives. All the Priority 1 conditions was completed first, then the Priority 2 and 3 test conditions were included as flight time permitted. The XV-15's landing gear was up during level flight and during descents at airspeeds greater than 90 knots. During descents less than 90 knots, the landing gear was down.



Figure 15. Linear Microphone Array During Phase 1 Testing

#### 2.4.1.1 Level Flight (Phase 1 testing)

The flight profile for the Phase 1 level flights is sketched in Figure 16a. During each pass, the XV-15 passed over the microphones at a specific altitude and flight condition. The level flight airspeed/nacelle angle combinations tested are shown in Figure 16(b), and listed in Appendix E.

Each level flyover was initiated at a point approximately 2 nautical miles uprange of the line of microphones. From this point, the desired flight condition was maintained while passing over the line of microphones and continuing to a point approximately 1 nautical mile past the microphones. After breakoff, the XV-15 continued in a "racetrack" pattern and set up for the next pass.

#### 2.4.1.2 Descents (Phase 1 testing)

The flight profiles for the Phase 1 descents are sketched in Figure 17a. Flight direction was from East to West. During each pass, the XV-15 passed through a point 394 feet (120 meters) above ground level, an altitude that corresponds to the descent condition currently used in helicopter noise certification. The nacelle angle/airspeed combinations flown during descent are shown in Figure 17b, and listed in Appendix E.

Each descent was initiated at a point about 2 nautical miles uprange of the line of microphones. From this point, the desired flight conditions was maintained while passing over the microphones and continuing as long as practical past them. Specific breakoff altitude was left to the pilot's judgment. After breakoff, the XV-15 went around and set up for the another pass.

Descents received the heaviest emphasis during this test because of the strong influence this condition has upon terminal area noise impact.

#### 2.4.1.3 Takeoffs (Phase 1 testing)

The flight profiles for the Phase 1 takeoffs are sketched in Figure 18(a), patterned after the helicopter noise certification procedure. Flight direction was from East to West. During each pass, the climb was initiated at an uprange position intended to bring the XV-15 through a point 394 feet (120 meters) above ground level. This altitude matches that used in the descent conditions.

Each takeoff was entered by first flying level at 100 feet above ground level toward the line of microphones, then initiating a climb at pre-determined uprange point based on the predicted climb angle for that flight condition. From this climb initiation point, the desired flight condition was maintained while passing over the line of microphones and continuing to a point approximately 1 nautical mile downrange from the microphones. After breakoff, the XV-15 went around and set up for the next pass.



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Figure 16. Phase 1 Level Flight

APPROACH



Figure 17. Phase 1 Approaches



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(Flight Conditions)

Figure 18. Phase 1 Takeoffs

#### 2.4.1.4 Hover (Phase 1 testing)

The XV-15 hovered over the center microphone at an altitude of 394 feet, slowly changing azimuth while maintaining a stationary position. The original intent was to hover at 15 degree incremental headings while taking acoustic data. At this altitude, however, the pilot had no visual landmarks, and station-keeping was a problem for long-duration hovers. For this reason, a brief, continuous-turn hover was performed.

#### 2.4.2 Meteorological Conditions - Phase 1 Testing

The meteorological conditions during each Phase 1 test day, as measured at BHTI's 10-meter tower, are presented graphically in Appendix D, pages 1-9.

The meteorological conditions measured at altitude and at NASA's ground station are not included in this report. These are part of the database acquired and processed by NASA.

#### 2.4.3 XV-15 Position/Aircraft Parameters

Position data and aircraft state data are not included in this report. These have been incorporated in the database processed by NASA in parallel with the noise data for each of the twenty Phase 1 microphone positions.

#### 2.5 PHASE 2. "DISTRIBUTED" MICROPHONE ARRAY TESTING

After completion of the Phase 1 testing, the microphones were re-deployed into the distributed array previously shown in Figure 7. Phase 2 testing was accomplished on 3 test days. November 13, 15 and 16.

The distributed microphone array consisted of 30 microphones covering an area 2000 feet laterally from the flight track, and 7000 feet (-6000 to +1000) along the flight track, as previously shown in Figure 7. The exact measurement positions are given in Appendix B.

#### 2.5.1 Flight Conditions

During Phase 2 testing the XV-15 test conditions included level flights, descents to IGE hover, takeoffs from IGE hover, and flight idle. Details of each flight condition flown are given in Appendix E.

#### 2.5.1.1 Level Flights (Phase 2 Testing)

A limited number of level flights were performed during Phase 2. These consisted of the "housekeeping" pass conducted each test day to allow tracing of day-to-day test condition variations, and a right and a left level turn over the array. A total of 4 level flight conditions were flown.

#### 2.5.1.2 Descents (Phase 2 Testing)

For descents, the XV-15 approached the helipad from the West along a heading of approximately 75 degrees, guided by the optical tracker signal displayed in the cockpit. The approaches were categorized according to their glideslopes. A total of 22 descent conditions were flown during Phase 2.

<u>Fixed Glideslopes to 100 ft Waveoff</u>. These descents were performed in a manner similar to those in Phase 1 testing. The intent was to provide "large-array" data that could be correlated with noise predictions based on the Phase 1 results. During each pass, the XV-15 maintained a fixed glideslope and flight condition while attempting to fly through a point 396 above the helipad. After passing over the pad, the condition was held until a point about 100 feet above the ground, where the XV-15 broke off and climbed out in preparation for the next pass.

#### Fixed Glideslopes to Flare/Hover

During each of these descents, the XV-15 initially maintained a fixed glideslope and flight condition, but it was necessary to bring the nacelles to the full helicopter mode and flare to an IGE hover over the helipad. The point at which the constant flight condition was discontinued was at the discretion of the pilot, and was of course dependent on the target descent angle and airspeed.

#### Segmented Glideslopes to Flare/Hover

This descent was similar to those discussed in the previous paragraph, but included two glideslope segments. The initial segment required a 3 degree glideslope, and the second segment required a 12 degree slope. As in the fixed glideslope tests, the XV-15 maintained a constant flight condition as long as practical, then flared to a hover over the helipad. Only one of these segmented approaches was included in this test.

#### Pilot Discretion to Flare/Hover

During this series of tests, the pilot was constrained only by the requirement to maintain the desired flight track and to approach to a hover over the helipad. The pilot, Roy Hopkins, selected a series of practical approaches which might produce a broad range of noise contours. These were labeled A through G in the test log. This series of approaches was run November 14, and was repeated November 16.

#### 2.5.1.3 Takeoffs (Phase 2 Testing)

For takeoff, the XV-15 hovered over the helipad, then climbed out to the West along a heading of approximately 255 degrees, guided by the optical tracker signal displayed in the cockpit. Except for the requirement to maintain flight track, the takeoff flight parameters were not constrained, but were left to the discretion of the pilot. These were labeled Takeoff "A" through "Q" in the test log.

#### 2.5.1.4 IGE Hover (Phase 2 Testing)

An IGE hover was performed at an approximate wheel height of 15 feet over the helipad as previously shown in the photograph of Figure 2. Measurements were taken at four aircraft headings. Two headings were aligned with the flight track (75 and 255 degrees) and two more were perpendicular to the track (165 and 345 degrees).

#### 2.5.1.5 Flight Idle (Phase 2 Testing)

A brief set of acoustic data was acquired with the XV-15 at flight idle, i.e., the rotors were at flat pitch and turning at approximately 98% RPM. The XV-15 was positioned at the center of the helipad. Two headings (75 and 255 degrees) were included.

#### 2.5.2 Meteorological Conditions

The meteorological conditions during each Phase 2 test day as measured at BHTI's 10-meter tower are presented graphically in Appendix D, pages 10-12.

#### 2.5.3 XV-15 Position/Aircraft Parameters

Position data and aircraft state data are not included in this report. These have been incorporated in the database processed by NASA in parallel with the noise data for each of the thirty Phase 2 microphone positions. During the final test day, November 16, the optical tracker was not available, so tracking data was acquired using an experimental Differential Global Positioning System (DGPS) installed on the XV-15.

#### 3. <u>RESULTS/CONCLUDING REMARKS</u>

The acoustic results are not included in this report, and no conclusions are drawn as to the optimal operating modes of the XV-15. NASA-Langley is processing and correlating the acoustic, position, aircraft state, and meteorological datasets for Phase 1 and Phase 2 testing. These will be made available to authorized users.

An experimental means of viewing the Phase 2 test results using computer graphics has been developed under the current contract. This display, called the Large Array Noise Data Display (LANDD), simultaneously displays aircraft position, noise data at 30 microphone locations, and limited aircraft state data (heading, roll, pitch, yaw, nacelle position) on a computer screen. Computer interpolation of the noise data allows instantaneous color contours of the time-varying noise to also be displayed. A sample of the on-screen display is shown in Figure 19. This simultaneous viewing of flight path, noise, and aircraft state, provides a tool for visually isolating those flight parameters which most influence total noise.

The LANDD employs the NASA-developed Flow Analysis Software Toolkit (FAST), and was developed on a Silicon Graphics Indigo 2 platform. Currently, 11 approaches and 1 takeoff condition are loaded and available for display. It is recommended that additional Phase 2 approaches and takeoffs be incorporated into LANDD so that comparative studies can be completed.



Figure 19. Bell Helicopter Textron Large Noise Data Display XV-15 Tests at Waxahachie (Oct-Nov 1995)

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## APPENDIX A

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LIST OF TEST PERSONNEL

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## XV-15 NOISE TEST PERSONNEL Oct.-Nov. 1995 @ SSC, Waxahachie, Texas

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TEAM	ASSOCIATION	N	WE	INDIVIDUAL RESPONSIBILITIES
NASA-LaRC ACOUSTICS	NASA-LaRC	DAVED	CONNER	PROJECT ENGINEER
NASA-LARC ACOUSTICS	NASA-LeRC	MICHAEL	MARCOLINI	PROJECT ENGINEER
NASA-LARC ACOUSTICS	NASA-LaRC	JOHN	CLINE	TEST ENGINEER
NASA-LARC ACOUSTICS	NASA-LaRC	KAREN	LYLE	INTERINAL NOISE
NASA-LARC ACOUSTICS	NASA-LaRC	ODILYN	SANTA MARIA	TEST ENGINEER
NASA-LARC ACOUSTICS	LOCKHEED	CHARLES (KEN)	RUTLEDGE	NASA- LARC DATA ANALYSIS
NASA-LARC ACOUSTICS	NASA-LaRC	DAVID (D.C.)	DAVIS	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	LOCKHEED	MARK	WILSON	NASA- LERC DATA ANALYSIS
NASA-LARC ACOUSTICS	WYLE LABS	том	BAXTER	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	WYLE LABS	NICHOLAS	KARANGELEN	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	WYLE LABS	VIRGILIO	MARCELO	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	WYLELABS	KETH	SCUDDER	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	WYLE LABS	JOHN	SWAIN	NASA INSTRUMENTATION
NASA-LARC ACOUSTICS	NASA-LaRC	JAYE	MOEN	METEOROLOGICAL (BALLOON) INSTRUMENTATION
BELL ACOUSTICS	BELL	BRYAN	EDWARDS	PROJECT ENGINEER -ACOUSTICS
BELL ACOUSTICS	BELL	JOHN	BRIEGER	ACOUSTICS
BELL ACOUSTICS	BEL	RICK	RILEY	ACOUSTICS
BELL ACOUSTICS	BELL	CHARLES	cox	ACOUSTICS
BELL FLIGHT	BELL	COLBY	NICKS	PROJECT ENGINEER - FLIGHT
BELL FLIGHT	BELL	ROY	HOPKINS	PILOT
BELL FLIGHT	BELL	DON	BORG	PILOT
BELL FLIGHT	BELL	BILL	MARTIN	FLIGHT TEST
BELL FLIGHT	BELL	JERRY	PICKARD	LOGISTICS
BELL FLIGHT	BELL	ALAN	ADAMSON	INSTRUMENTATION
SELL FLIGHT	BELL	JERRY	WALKER	INSTRUMENTATION
BELL FLIGHT	881.	JIM	WILSON	DYNAMICS
BELL FLIGHT	BELL	MIKE	SHAW	DATA OPERATIONS
BELL FLIGHT	BELL	MARK	STOUFFLET	DATA OPERATIONS
BELL FLIGHT	881.	KELLY	SPIVEY	DATA OPERATIONS
BELL FLIGHT	BELL	KEN	COGDILL	FLIGHT
BELL FLIGHT	BELL	HARRY	DURAND	FUGHT
BELL FLIGHT	BELL	FRED	MAJOR	FLIGHT
BELL FLIGHT	BELL	KEN	MITCHELL	FLIGHT
BELL FLIGHT	BELL	WELDON	RHEA	FLIGHT
NASA- AMES LASER TRACKER	NASA-AMES	FRED	SHIGEMOTO	LASER TRACKER
NASA- AMES LASER TRACKER	RECOM	ED	FARR	LASER TRACKER
NASA- AMES LASER TRACKER	RECOM	JUL	LAWRENCE	LASER TRACKER
NASA- AMES LASER TRACKER	RECOM	RICK	TAYLOR	LASER TRACKER
NASA- AMES LASER TRACKER	STERING	PAM	PFOHL	LASER TRACKER

### APPENDIX B

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#### **MICROPHONE POSITIONS - SURVEYED POINTS**

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			XV-15 SURV	EYED LOC	ATI	ONS	- PH	ASE 1 TES	TIN	G			
SIDELINE ANGLE	LOCATION	1											
FROM VERTICAL	CALLOUT	×	Y	z	<<<	<<<	< N	AD-83 CO(	RC	XNA'	TES :	>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	>
(DEGREES)		(+ is Westerly)	(+ is Southerty)	(+ is up) DISTANCE									· · · · · ·
TARGET ALTITUDE 394 ft.		(ft_)	(ñ.)	(11.)	~~~~	~~~ <b>4</b>	JUTTU	DE>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	~~~	~~~~	d ong	TUDE>>>>>>>	Elevation
	TRACKER SITE			65.7	N	32	20	6.29265	w	96	54	54.36509	723.07
80	M1- 1 -N	0	-5671	17.3	N	32	19	42.72147	w	96	54	48.34208	674.70
70	M1-2 -N	0	-2747	10.8	N	32	19	31.43729	w	96	54	46.44261	668.20
60	M1- 3 -N	0	-1732	6.6	N	32	19	27.51817	w	96	54	45.78267	663.99
50	M1- 4 -N	0	-1192	3.9	N	32	19	25.43206	w	96	54	45.43265	661.28
40	M1-5 -N	0	-839	3.8	N	32	19	24.07174	w	96	54	45.20282	661.17
30	M1-6 -N	0	-577	1.6	N	32	19	23.06127	w	96	54	45.03278	659.04
20	M1-7 -N	0	-364	0.7	N	32	19	22.23797	w	96	54	44.89429	658.09
10	M1-8 -N	0	-176	-0.0	N	32	19	21.51365	w	96	54	44.77243	657.36
0	N1- 9 -N	0	0	-0.0	N	32	19	20.83135	w	96	54	44.65822	657.39
10	M1- 10 -N	0	176	-1.7	N	32	19	20.15273	w	96	54	44.54313	655.66
20	M1-11 -N	0	364	-2.8	N	32	19	19.42834	w	96	54	44.42129	654.63
30	M1- 12 -N	0	577	-3.5	N	32	19	18.60421	w	96	54	44.28276	653.90
40	M1-13 -N	0	839	-3.7	N	32	19	17.59412	w	96	54	44.11269	653.70
50	MT- 14 -N	0	1192	-5.3	N	32	19	16.23299	w	96	54	43.88329	652.14
60	M1- 15 -N	0	1732	-6.8	N	32	19	14.14793	w	96	54	43.53259	650.57
70	M1- 16 -N	0	2747	-7.7	N	32	19	10.22915	w	96	54	42.87306	649.71
80	M1- 17 -N	0	5671	-17.5	N	32	18	58.94370	w	96	54	40.97376	639.92
0	M1- 18 -N	-200	0	-3.6	N	32	19	21.10635	w	96	54	42.34937	653.85
0	M1-19 -N	-400	o	-5.5	N	32	19	21.38039	w	96	54	40.04142	651.93
0	M1-20 -N	-600	o	-6.2	N	32	19	21.65423	w	96	54	37.73286	651.21
VANS	V1- 1 -N	-600	700	-11.9	N	32	19	14.79740	w	96	54	36.57890	645.54
VANS	V1- 2 -N	-600	-700	-1.7	N	32	19	28.51144	w	96	54	38.88704	655.67
VANS	V1- 1-B	-600	600	-11.1	N	32	19	15.77691	w	96	54	36.74315	646.32
BELL MCS	M1- 1-8	-200	492	-3.4	N	32	19	16.28707	w	96	54	41.53812	650.01
BELL MICS	M1- 2-B	-200	0	0.4	N	32	19	21.10635	w	96	54	42.34937	653.85
BELL MICS	M1- 3-B	-200	-492	5.6	N	32	19	25.92615	w	96	54	43.16109	658.97
BELL MICS	M1- 4-B	-200	492	-7.4	N	32	19	16.28707	w	96	54	41.53812	650.01
BELL MCS	M1- 5-B	-200	0	-3.6	N	32	19	21.10635	w	96	54	42.34937	653.85
BELL MICS	M1- 6-B	-200	-492	1.6	N	32	19	25.92615	w	96	54	43.16109	658.97
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M2=MICROPHONE LOCATION, PHASE 2 TESTS N=NASA LOCATION B=BELL LOCATION V=VAN LOCATION

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X - DISTANCES ARE ALONG THE FLIGHT TRACK Y - DISTANCES ARE PERPENDICULAR TO THE FLIGHT PATH Z - DISTANCES ARE VERTICAL HEIGHT ABOVE LANDING PAD FLIGHT PATH RAN ROUGHLY EAST-WEST (75 DEG/255 DEG)

B-1

			XV-15 SUR	VEYED LO	CATH	ons	- PH	ASE 2 TES	TIN	G				
	LOCATION CALLOUT	I III	Y	Z	~~~	~~~~	< N/	AD-83 COC	RD	<b>NNA</b>	TE\$ >	·>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>		
Description		(IL)	DISTANCE (IL.)	DISTANCE (R.)	****		LATT	005>>>>>>>			~d.0N	GITUDE>>>>>	Elevation	Description
WEATHER BALLOON		TBO	180	65.7	N	32	20	6.29265	w	96	54	54.36509	723.07	WEATHER BALLOON
OPTICAL TRACKER	1	TBO	TBO	65.7	N	32	20	6.29265	w	96	54	54,36509	723.07	OPTICAL TRACKER
HELIPAD (REF PT.)	M1- 9 -h	0	0	0.0	N	32	19	20.83135	W	96	54	44.65822	657.39	M1-0-N
MICROPHONE	M2-1 +	8000	0	6.0	N	32	19	12.61253	w	96	55	53.90705	<b>663.4</b> 2	M2-1-N
MICROPHONE	M2-2 +	4700	0	-6.8	N	32	19	14.39412	w	96	55	38.90271	650.60	M2-2-N
MICROPHONE	M2-3 +	4700	750	0.0	Ì									
MCROPHONE	M2- 4 -	3850	0	12.2	N	32	19	15.55945	w	96	55	29.09195	669.61	M2-4-N
MCROPHONE	M2- 5 +	3850	500	8.0	N	32	19	10.66187	W	96	55	28.28657	665.42	M2-5-N
MICROPHONE	10- 6 -	3850	1250	10.3	N	32	19	3.31485	W	96	55	27.03007	657.69	M2-6-N
MICROPHONE	M2-7 +	3000	0	12.8	N	32	19	16.72430	W	96	55	19,28244	670.19	M2-7-N
MICROPHONE	M2-8 -	3000	500	4.1	N	32	19	11.82580	W	96	55	18.45775	661.53	M2-8-N
MCDODUONE	MP. 9 J	3000	1000	3.7	N	32	19	6.92827	w	96	55	17.63186	661.1	M2-0-N
MODODUONE	M2 10 .4	3000	1500	5.5	N	32	19	4.47930	w	96	55	17.22040	862.84	M2-10-N
NECONDUCINE	102-10-4	2250	0	4.1	N	32	19	17.75189	w	96	55	10.62660	661.5	M2-11-
MCDODUONE	M2. 12 J	2250	1000	-5.8	N	32	19	7.95591	w	96	55	8.97678	651.63	M2-12-N
MODORIANE	M2 13 A	1500	0	6.9	N	32	19	18.77880	w	96	55	1.97097	664.31	M2-13-N
MONOTIONE	NO. 14 .	1500	1000	-6.3	N	32	19	8.98249	w	96	55	0.32160	651.1	M214-N
MCRODUCKE	M2-15 A	1500	2000	-0.5	N	32	18	59.18746	w	96	54	58.67188	656.92	M2-15-N
MOTOPHONE	100 14 3	1000	0	9.0	N	32	19	19.46339	w	96	54	56.19945	666.34	M2-16-N
ARCHORING	M2-10-4	1000	1000	-2.7	N	32	19	9.66805	w	96	54	54.55068	654.74	M2-17-N
MONOPHONE	100 10 10	500	0	7.6	N	32	19	20.14842	w	96	54	50.42828	664.96	M2-18-N
MONOPTIONE	M2- 10 -	500	1000	-1.0	N	32	19	10.35275	w	96	54	48.78010	656.39	M2-19-N
MICHOPHONE	M2- 10 -	500	2000	0.4	N	32	19	0.55576	w	96	54	47,13017	657.77	M2-20-N
MOTOTIONE	M2- 20 4		500	-5.6	N	32	19	15.93471	w	96	54	43.83354	651.8	M2-21-N
MOTOTIONE	M2- 21 4		1000	-7.7	N	32	19	11.03666	w	96	54	43.00630	649.73	M2-22-N
MICHOPTIONE	102- 22 4		1500	.90	N	32	19	6.13841	w	96	54	42.18471	648.41	M2-23-N
ANCHOPHUNE	M2- 23 -			-6.2	N	32	19	21.5109	w	96	54	38.86731	651.1	M2-24-N
MICHUPTIONE	NO 75 1		500	-0.9	N	32	19	16.61952	w	96	54	38.06308	647.54	M2-25-N
MURUPTURE	M2- 20 -	-500	1000		N	32	19	11.7217	w	96	54	37.23780	645.29	M2-26-N
	100 00 1	500	1500	-14.2	N	32	19	6.82364	w	96	54	35.41449	643.16	M2-27-N
MICHOPHUNE	102- 2/ -			-85	N	32	19	22,20200	W	96	54	33.1161	648.59	M2-28-N
MICHOPHONE	M2- 28 -	-1000	500	-120	N	32	19	17.30387	W	96	54	32.29135	645.38	M2-29-N
MICROPHONE	M2- 20 -	-1000	1000	-15.3	N	32	19	12.40562	w	96	54	31.45783	642.08	M2-30-N
				22.0		30	19	20.51585	w	96	55	28,75024	675.43	M2-1-8
MICROPHONE	M2-1-	3750	-	173		32	10	15 6064	w	96	55	27,93891	670,74	M2-2-8
MICROPHONE	M2- 2 -	3750		17.3		32	10	10 67877		- 94	55	27.12704	666.63	M2-3-8
MICROPHONE	M2-3-	3750	442	13.2		34	46	20 51586				28 75024	675.43	M2-4-B
MICROPHONE	M2- 4 -	3750	-462	10.0			40	16 00000	1		-	27 03801	670 74	M2-5-8
MICROPHONE	M2- 5 -	3 3750	0	13.3		32	10	10.00000	1			27 12704	666 63	M2-6-8
MICROPHONE	M2- 6 -	3 3750	492	9.2		32	10	10.07077	1			A 44283	660.80	M2-7-B
MICROPHONE	M2- 7-	3 7016	883	3.4	N	32	19	2.30H/V	1		50	20 59010	668.80	M2-8-8
MICROPHONE	M2- 8 -	3 8287	'	11.		34	18	9,999,100 100	1	-0	~	20.00010		
	1 10. 1	9500	800	8.6	N	32	19	8,20258	W	96	55	23.73319	666.01	V2-1-8

M2= MICROPHONE LOCATION, PHASE 2 TESTS N= NASA LOCATION B= BELL LOCATION V= VAN LOCATION

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X- DISTANCES ARE ALONG THE FLIGHT TRACK Y- DISTANCES ARE PERPENDICULAR TO THE FLIGHT TRACK Z- DISTANCES ARE VERTICAL HEIGHT ABOYE LANDING PAD FLIGHT PATH RAN ROUGHLY EAST-WEST (75 DEG/255 DEG)

**B-2** 

APPENDIX C

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TEST SEQUENCE

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### TEST SEQUENCE / TEST ENGINEER'S FIELD NOTES

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	LOCAL	XV-15	NASA	BHTI SHIP	BHTI COND'N.	
DATE	TIME	FLT#	RUN #	REC#	NO.	
10/10/95	749	161	101	6	101	question on tracking
10/10/95	/55 802	161	104	9	103A 102	slow condition to check tracking range
10/10/95	802	161	102	11	102	Netinal midance deviation"
10/10/95	815	161	105	12	104	ronce guidence demaning
10/10/95	821	161	106	13	105	
10/10/95	829	161	107	14	106	helicopter interferes - circle XV-15, then come in
10/10/95	835	161	108	15	101	
10/10/95	840	161	109	16	107	
10/10/95	845	161	110	17	306	fibed wing a/c at end of record
	1	1				RTB - fuel
10/10/95	956	161	111	20	306	the state of the same track. Mildle shall do not det
10/10/95	1000	101	112	21	305	tracker set on wong track - XV-15 circled, then good
10/10/95	1012	121	114	<b>1 m</b>	109	abot W/JE too high (100)
10/10/95	1020	161	115	24	109	abortxv-15 too high (100)
10/10/95	1024	161	116	25	110	
10/10/95	1027	161	117	26	111	"tracking drocouts" - posn looked good
10/10/95	1032	161	118	27	112	fored wing jet
10/10/95	1036	161	119	28	113	altitude off - Bell mics overloaded
10/10/95	1041	161	120	29	113	
10/10/95	1047	161	121	·	101	Abort
	<b>.</b>		48-			RTB - fuel
10/12/95	746	162	122	8	101	inned up with lights - pilot indicator shows right of course
10/12/95	/52	162	123		108	Distant page as for
10/12/95	/30	162	124		1064	Querest pass so far
10/12/95	813	162	126	12	301	Blat-Nore high attitude , had , unpatural coodition"
10/12/95	B18	162	127	13	302	FINC. HUSE INg/ attracter - Data - Gringtonal Condition
10/12/95	623	162	128	14	303	
10/12/95	829	162	129	15	315	BVI rating=3. XV-15 got very low to ground
10/12/95	835	162	130	16	314	BVI rating = 4. Tractor on Boz Rd XV-15 circled, then set up for this pass
10/12/95	845	162	131	17	311	BVI rating=2; Pilot: "Bad vibs & handling qualities"
					-	7:30 fit scheduled, but postponed for fuel contamination problem
10/13/95		163				
10/13/95	1350	163				
10/13/95	1405	163	132		101	Phot: - lurbulent"
10110135	1415	100	135	~	312	
10/16/95	745	x	-	-		
10/16/95	750	164	-	-	101	Abort - Housekeeping run
10/16/95	-	164			101	Abort - Housekeeping run
10/16/95	758	164	134	9	101	Housekeeping - still some question on tracking
10/16/95	806	164	135	10	312	BVI rating-1
10/16/95	014	164	130	12	310	BVI rating=3
10/16/95	828	164	138	13	307a	BVI atting=3
10/16/95	834	164	139	14	306	BVI ratinge2
10/16/95	839	164	140	15	309	BVI rating=2
						-
10/27/95	758	168a	141	8	101	Housekeeping
10/27/95	802	168a	142	9	324	Abort - no tracking info.
10/27/95	805	168a	143	10	322	BVI rating=4; went for 90 deg nacelle, got 80deg by mistake
10/27/95	812	1694	144	11	324	SVI reting 2 tracking question: 15.14 headwind also and
10/27/95	836	168-	146	12	325	RVI rating-2, traction question early Plat "confortable anomach"
10/27/95	844	16Ra	147	14	327	BVI rating-4
10/27/95	851	168a	148	15	323	BVI rating-4
10/27/95	857	168a	149	16	320	BVI rating-4
			-		-	RTB- fuel
10/27/95	1000	168b	150	21	101	Housekeeping point
10/27/95	1006	168b	151	22	321	BVI rating=2; high crab angle - nose north of track
10/27/95	1014	1680	152	23	319	BVI rating=4
10/27/95	1021	1580	153	24	316	HIOC: "Can't see ground - nose high"
10/27/95	1026	1680	154	25	317	
10/27/05	1031	1060	135	20 77	318	DVI TELETING
10/27/05	1028	1695		41		nover - nose w 255 dag - checking tracking hover - Nose & 255 dag
10/27/95	1049	1585	156	28	334	ADD CC7 & Deptin - Internet
				~	~~	
10/28/95	852	169	157	2	101	
10/28/95	902	169	158	3	334	
10/28/95	908	169	159	4	334	
10/28/95	914	169	160	5	335	
		400	+	6	335	
10/28/95	919	103	101	<u> </u>		
10/28/95 10/28/95	919 930	169	162	7	336	

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DATE	LOCAL TIME	XV-15 FLT#	NASA RUN #	BHTI SHIP REC#	BHTI COND'N. NO.	
11/01/95 11/01/95 11/01/95 11/01/95 11/01/95 11/01/95 11/01/95 11/01/95 11/01/95 11/01/95	955 959 1004 1009 1015 1022 1028 1033 1039 1043 1050 1056	170 170 170 170 170 170 170 170 170 170	163 164 165 166 167 168 169 170 171 172 173 174	5 6 7 8 9 10 11 12 13 14 15 16	101 106 108 109 334 501 501 501 501 501 115 115 116 117	
11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95	736 743 752 800 808 816 823 830 836 836 841 846	171a 171a 171a 171a 171a 171a 171a 171a	175 176 177 178 179 180 180 180 181 182 183 184	18 19 20 21 22 23 24 25 26 27 28	101 334 335 336 337 307 307 308 108 109 501	
11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95 11/04/95	955 1000 1005 1012 1017 1021 1027 1033 1038	171b 171b 171b 171b 171b 171b 171b 171b	185 186 187 188 189 190 191 192 193	33 34 35 36 37 38 39 40 41	101 502 344 345 342 342 343 340 341	Abort - No cuidance, no Bell deta
11/04/95 11/04/95 11/04/95	1235	171c 171c 171c	194 195 195	47	195 195	Abort - No guidance <u>Abort - No guidance</u> <u>ATB- Rain moved in</u>
11/07/95 11/07/95 11/07/95 11/07/95 11/07/95	806 815 821 832 840	172 172 172 172 172 172	196 197 198 199 200	10 11 12 13 14	331 333 329 328 101	RTB - Winds too high to continue
11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95	731 738 746 753 759 908 814 819 826 832 838	173a 173a 173a 173a 173a 173a 173a 173a	201 202 203 204 205 206 207 208 209 210 211	8 9 10 11 12 13 14 15 16 17 18	101 354 355 352 353 350 351 347 348 349	
11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95 11/08/95	938 947 1001 1010 1015 1020 1032 1035 1042	173b 173b 173b 173b 173b 173b 173b 173b	212 213 214 215 216 217 218 219 220 221	22 23 24 25 26 27 28 29 30 31	101 332 331 330 330 333 333	hover hover hover

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	LOCAL	XV-15	NASA	BHTI SHIP	BHTI COND'N.	
DATE	TIME	FLTS		REC#	NO.	
UNIE						
11/13/05	825	175	300		200	1
11/13/05	926	176	201	iš	200	
1010000	000		301		200	
11/13/95	845	175	302	10	402	
11/13/95	853	175	303	11	402	
11/13/95	•	175	304	12	410	
11/19/02		175	205	12	471	
11/13/95		1/5	305	13		
11/13/95	920	175	306	14	471	4
						1
44/44/00		470-		_	200	
11/14/95		1/04	307		200	
11/14/95	810	1/68	307	2	200	
11/14/95	817	176a	308	3	402	
11/14/95	- 1	176a	· ·	-	-	
11/14/05	825	1764	309	▲	489	
4414 4805		1.70			400	
11/14/90	833	1/04	310	3	490	
11/14/95	•	176a	1 311	6	492	
11/14/95	843	176a	312	7	601	
11/14/05	946	176.	313		405	
4444400		1.70			200	
11/14/95	052	1/68	314	1 3 1	002	
1	1	1				10.00
	1	I				
11/14/95	1005	176b	315	13	491	1
11/14/06	1014	1765	316		603	
4474 440-	1014	1/00	010		400	
11/14/95	- 1	1760	317	15	483	
11/14/95	1021	176b	318	16	604	
11/14/95	1024	1760	319	17	494	
11/14/95	1030	1765	320	18	805	
4474 4005		1705			400	
11/14/85	1005	1/00	321	19	482	
11/14/95		1/60	322	20	000	
11/14/95	1045	1760	323	21	433	
11/14/95	1052	176b	324	22	422	1
11/14/95	1059	1765	225	21	474	
11/14/05	1000	4700	325		678	
11/14/95	1108	1/60	320	24	4/5	
						RTB - fuel
11/14/95	1252	176c	327	29	469	
11/14/05	101	1760	328	30	470	
11/14/05		1760	320	30		
11/14/95	110	1/60	329	31	000	
11/14/95	-	176c	330	32	471	
11/14/95	-	176c	331	33	607	
11/14/95	116	176c	332	34	472	
11/14/05	120	1780	333	35	A09	
11/14/05	120	170-		~ ~	4300	
11/14/80	123	1760	334	30	4/3	
11/14/95	130	176c	335	37	841	
11/14/95	-	176c	336	38	843	
11/14/95	136	176c	337	40	821	
11/14/95	138	1760	338	ai l	822	
11/14/05		1780	2000	40	844	
11/1-9/80		1760	335	**	02.3	
11/14/95	141	176C	340	43	824	
11/14/95	150	176c	341	44	478	
11/14/95	154	176c	342	45	609	
						RTB - fuel
4440-00					<b></b>	
11/16/95	905	177	343	ð	200	
11/16/95	912	177	344	9	481	
11/16/95	915	177	345	10	610	
11/16/95	<b>91</b> 8	177	346	11	480	1
11/18/05	021	177	347	12	611	
14/10/00	94 I	L	3/1	12	465	
1/16/95	825	14	346	13	462	
11/16/95	928	177	349	14	612	
11/16/95	931	177	350	15	483	
11/16/95	934	177	351	16	613	
11/16/05	838	177	352	17	484	
11/10/06		<del>     </del>	363		614	
11/10/30	3741		333	10	014	
11/16/95	944	177	354	19	485	
11/16/95	947	177	355	20	615	
11/16/95	951	177	356	21	486	
11/16/04	0.00	<del></del>	267	20	616	
10/10/90	CC6		337	~	010	
11/16/95	859	177	358	Z3	486	
11/16/95	1003	177	359	24	617	
11/16/95	1006	177	360	25	251	
11/16/95	1013	177	361	26	253	
		,				
				I		NOTE.
				I		Lanoing gear is up during descents above 90 kt.
						Landing gear is up during level flight passes
						Landing gear is down during descents below 90 kt.

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APPENDIX D

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METEOROLOGICAL CONDITIONS



(LOCAL TIME)



(LOCAL TIME)



#### METEOROLOGICAL RECORDS AT BHTI VAN (10m TOWER) XV-15 PHASE 1 TESTING



METEOROLOGICAL RECORDS AT BHTI VAN (10m TOWER)

D-4



# METEOROLOGICAL RECORDS AT BHTI VAN (10m TOWER)



D-6



D-7



METEOROLOGICAL RECORDS AT BHTI VAN (10m TOWER)



D-9





#### D11



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METEOROLOGICAL RECORDS AT BHTI VAN (10m TOWER) XV-15 PHASE 2 TESTING

D12

APPENDIX E

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FLIGHT CONDITIONS

#### TEST CONDITIONS, PHASE 1 TEST CONDITIONS RUN WITH THE LINEAR MICROPHONE AREAY

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	XV-15 NOISE TEST - PHASE 1 B T COND						<<<<<<>> PLOT CARD >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>									
I	STEADY									FUG	IT #/D	ATE/CO	UNTE	R #		-
ľ	FLIGHT			FLIGHT				T161	T162	T164	T168	T169	T170	T171	T172	1173
COND.	CONDIN	NACELLE	ARSPEED	ANGLE	RPM	ALTITUDE	<b>HEADING</b>	1000	12007	ност	27007	38007	1-HOV	-	THOY	-
LNO.		(063)	(KT)	(063)	(10791)	(FT)	(080)	CTR #	CTR #	CTR #	CTR #	CTR #	CTR #	CTR	(TR 8	ctae
			-								I					
	LEVEL	<u>rtkin</u>	₽													
	PRIORITY	1 CON	NITIONS													
101	LEVEL MIN	80	80	0	96	394	255	8,15.30	8	XX9	8,21	2	5	18,33	14	8,22
102	LEVEL	90	70	0	96	394	255	10				_				
103	LEVEL	85	70	0	96	394	255	11								
103A		80	50	0	96	394	255	9								
105	LEVEL	80	110	0	96	304	200	12								
106	LEVEL	60	70	o	98	394	255	14								
107	LEVEL	60	110	0	98	394	255	16								
108	LEVEL	60	140	0	98	394	255		9				6,7	26		
1064			120	0	- 00 - 86	394	230	22 23 24	10				8	27		
110	LEVEL		180	ō	86	394	255	25						-		
111	LEVEL	0	220	0	86	394	255	26								
112	LEVEL	0	140	0	86	1500	255	27								
113	LEVEL	° I	220	o	86	1500	255	28,29								
	PRIORITY	2 CON	RITIONS													
114	VOIDED NUM	BER														
115	LEVEL	80	90	0	98	394	255						14			
116	LEVEL	80	110	0	92	394	255						15			
117	LEVEL	80	110	0	95	394	255		ļ			<b> </b>	16			
		1								ł						
		XV-15 NC	NEE TEST	PHASE 1	FLTO	ND.			~~~~		T CA	RD >>	>>>>	~~~~	>>>>	<u> </u>
	STEADY									FUG	T #D/	TE/CO	UNTE	R #		
	FUGHT			FLIGHT				T161	T162	T164	T168	T169	T170	T171	1172	T173
COND.	CONDIN	NACELLE	ARSPEED	ANGLE	RPM	ATTUDE	HEADING	10007	10007	HOCT	270001	BOCT	1-NOV		7HOY	
		(DBG)	(171)	(1983)	(50876)	(FT)	(060)	CTR #	CTRO	CTR #	CTR #	CIRA	CTRA	CTR#	CTR #	CTR #
	DESCE	ITE														
	PRIORITY	1 CON	ITIONS													
301	DESCENTS	60	70	3	98	VAR.	255		12							
302	DESCENTS	60	90 110	3	96 64	VAR.	255		13							
304	DESCENTS	70	70	3	98	VAR.	255		11							
305	DESCENTS	80	70	3	98	VAR.	255	21								
306	DESCENTS	90	70	3	98	VAR.	255	17,20								
307	DESCENTS	80	70	6	98 44	VAR.	255			1.2				23,24		
308	DESCENTS	60	80	6	98	VAR.	255			14				25		
309	DESCENTS	60	110	6	98	VAR.	255			1.6						
310	DESCENTS	70	70	6	04	174.05				13						
311	DESCENTS	80				VAR.	255			12						
313	JESSERIS	80	40	6	98 94	VAR. VAR.	255 285		17	12						8
314	DESCENTS	80 80	40 50 70	6 6	98 98 98	VAR. VAR. VAR. VAR.	256 256 255 255		17	19 12 10 11						
r 1	DESCENTS	80 80 85	40 50 70 70	6 6 6	98 98 98 98	VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255		17 16	19 12 10 11						
315	DESCENTS DESCENTS DESCENTS	80 80 85 90	40 50 70 70 70	6 6 6	98 98 98 98	VAR. VAR. VAR. VAR. VAR. VAR.	256 255 255 255 255 255		17 16 15	13 12 10 11						-
315 316	DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60	40 50 70 70 70	6669	98 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24					-
315 316 317 318	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 60	40 50 70 70 70 90	6 6 6 9 9 9	98 96 96 96 96 96 96 96	VAH. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 265 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 %					31
315 316 317 318 319	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 86 90 60 60 60 70	40 50 70 70 70 90 110 70	6 6 6 9 9 9 9	98 98 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 23					31
315 316 317 318 319 320	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 60 70 80	40 50 70 70 70 90 110 70 40	6 6 6 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 21 16					31
315 316 317 318 319 320 321	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 60 70 80 80 80	40 50 70 70 70 90 110 70 40 50	6 6 6 9 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98 98	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 265 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 23 16 21 1					31
315 316 317 318 319 320 321 322 321	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 80 70 80 80 80 80	40 50 70 70 70 90 110 70 40 50 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98 98	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15					31
315 316 317 318 319 320 321 321 322 323 324	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 80 80 70 80 80 80 85 90	40 50 70 70 70 90 110 70 40 50 70 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 98 98 98 98 96 96 96 96 98 98 98 98 98 98 98 98	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	255 255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15					31
315 316 317 318 319 320 321 323 324 323 324 325	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 80 70 80 80 80 80 80 80 85 95	40 5777779910 117040 5077789	6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98 98 98 9	VAH. VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR	255 255 255 255 255 255 255 255 255 255		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 11 12					31
315 316 317 318 319 320 321 322 323 324 325 326	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 60 60 80 80 80 80 85 95 95 95	40 50 70 70 70 90 110 70 90 10 70 70 70 70 70 70 50	6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98 98 98 9	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.			17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 11 12 13					31
315 316 317 318 319 320 321 323 324 325 325 327 323 324 325 327 327	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 80 80 70 80 80 80 85 95 95 95 95	40 50 70 70 90 110 70 40 50 70 70 70 60 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 98 98 98 98 98 98 98 98 98 98 98 9	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.			17 16 15	19 12 10 11	24 25 26 23 16 20 15 5 11 12 13 14					31
315 316 317 318 319 320 321 323 324 325 325 327 328 329	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 85 90 80 80 80 80 80 80 85 95 95 95 95 95 95 95 95 95 95	40 50 70 70 90 110 70 40 50 70 70 40 50 70 70 60 70 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	266 265 265 265 265 265 265 265 265 265 265		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 11 12 13 14				13	31
315 316 317 318 319 320 321 323 324 325 325 325 325 329 330	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 80 60 60 70 80 80 85 90 95 95 95 95 95 95 95 95 95 95 95 95 95	40 50 70 70 70 90 90 90 90 90 90 90 90 90 90 90 90 90	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	266 265 265 265 265 265 265 265 265 265 265		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 11 12 13 14			x x 48	13 12	31 25,26
315 316 317 318 319 320 31 32 32 32 32 32 32 32 32 32 32 32 32 32	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 80 60 60 70 80 80 85 90 95 95 95 95 95 95 80 70 80 80 80 85 95 95 80 80 80 80 80 80 80 80 80 80 80 80 80	40 50 70 70 70 90 110 70 90 110 70 40 50 70 70 70 70 70 70 70 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR.           VAR.	***		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 15 13 14			x x 48	13 12 10	31 25,26 24
315 316 317 318 319 320 31 32 32 32 32 32 32 32 32 32 32 32 32 32	DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS DESCENTS	80 80 80 60 60 80 80 80 80 85 95 95 95 95 95 95 80 70 80 80 80 80 80 80 80 80 80 80 80 80 80	40 50 70 70 70 90 110 70 40 50 70 70 70 40 50 70 70 70 50 60	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	***		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 3,11 12 13 14			x x 48	13 12 10	31 25,26 24 23
315 316 317 319 321 323 324 325 325 325 325 325 325 325 325 325 325	DESCENTS DESCENTS	80 80 80 60 60 80 80 80 80 85 95 95 95 95 95 80 80 80 80 80 80 80 80 80 80 80 80 80	40 50 70 70 90 110 70 90 110 70 90 110 70 40 50 70 40 50 70 40 50 70 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.			17 16 15	19 12 10 11	24 25 26 23 16 210 15 11 12 13 14			10.	13 12 10 11	31 25,26 24 23 27
	DESCENTS DESCENTS	80 80 80 60 60 70 80 80 80 85 95 95 95 95 95 95 95 95 95 95 95 95 95	40 50 70 70 90 110 70 90 110 70 50 70 40 50 70 40 50 70 40 50 70 40 50 70 40 50 70 40 50 70 70 70 70 70 70 70 70 70 70 70 70 70	6 6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.			17 16 15	19 12 10 11	24 25 26 23 16 210 15 15 11 12 13 14 28	τ.4 5	9	19 20	13 12 10 11	31 25,26 24 23 27
	DESCENTS DESCENTS	80 80 80 60 60 70 80 80 80 80 80 85 95 95 95 95 95 95 95 95 95 95 95 95 95	40 50 70 70 90 110 70 90 110 70 40 50 70 40 50 70 40 50 70 40 50 70 40 50 70 70 40 50 70 70 50 70 70 70 70 70 70 70 70 70 70 70 70 70	6 6 6 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	98 96 96 96 96 96 96 96 96 96 96 96 96 96	<b>VAR.</b> VAR. VAR. VAR. VAR. VAR. VAR. VAR. VAR.	166 16 16 16 16 16 16 16 16 16 16 16 16		17 16 15	19 12 10 11	24 25 26 23 16 22 10 15 11 12 13 14 28	<b>X</b> 456	9	19 20 21	13 12 10 11	31 25,26 24 23 27

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I	XV-15 NOISE TEST + PHASE 1 FLT COND.							<<<<<< PLOT CARD >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>								
1	STEADY									FLIGH	T#/D/	TE/CO	UNTE	R#		
	FLIGHT			FLIGHT				T161	1162	T164	T168	T169	T170	T171	T172	T173
COND.	COND'N	NACELLE	ARSPEED	ANGLE	RPM	ALTITUDE	HEADING	19007	ROCT	SOCT	27007	280CT	1-NOV	4HOV	7NOV	SHOV
NO.		(DEG)	(KT)	(DEG)	(%PPM)	(FT)	(DEG)	CTR	CTR	CTR #	CTR 4	CTR J	CTR	CTR	CTR #	CTR
	DESCE	UTC		ED)												
				ω,												
	PRIORITY	2 CONL	HIONS													
340	DESCENTS	80	90	3	98	VAR.	255							40		
341	DESCENTS	80	110	3	98	VAR.	255							41		
342	DESCENTS	85	70	3	98	VAR.	255							37,38		
343	DESCENTS	85	90	3	98	VAR.	255							39		
344	DESCENTS	90	50	3	98	VAR.	255							35		
345	DESCENTS	90	90	3	98	VAR.	255							36		
346	VOIDED NUM	BER														
347	DESCENTS	70	50	6	98	VAR.	255		1							16
348	DESCENTS	70	90	6	96	VAR.	253		1							17
349	DESCENTS	70	110	6	98	VAR.	255		1							18
350	DESCENTS	80	60	6	98	VAR.	255		1	1						14
351	DESCENTS	80	90	6	98	VAR.	255		1							15
352	DESCENTS	85	40	6	98	VAR.	255		1							12
353	DESCENTS	85	90	6	98	VAR.	255		1							13
354	DESCENTS	90	40	6	98	VAR.	255		1							9
355	DESCENTS	90	50	6	98	VAR.	255									10
356	DESCENTS	90	90	6	96	VAR.	255		l							11
																l
		XV-15 N	XSE TEST	- PHASE 1	<b>FLT CO</b>	ND.		~~~~~	~~~~	< <b>FIL</b> (	OT CA	RD >>	~>>>>	»>>>>	>>>>	
	STEADY	X1 1014								FUGH	IT #/D/	ATE/CO	UNTE	R#		
	FLIGHT			RUGHT				T161	1162	T164	1168	F169	T170	T171	T172	T173
COND	CONDIN	NACELLE		INGLE	RPM	ALTITUDE	HEADING	10001	2007	19001	27001	20007	1-NOV	41101	7NOV	anov
P <sup>ono</sup>																
I NO.		(DEC)	ŝ	(DEG)	(%PPM)	(FT)	(DEG)	CTR	CTR	CTR J	CTR #	CTR	CTR	CTR #	CTR	CTRA
NO.		(060)	( <b>M</b> )	(DEG)	( YURPM)	(17)	(DEG)	CTR	CTR	CTR J	CTR #	CTR #	CTR #	CTR #	CTR	CTRA
NO.		(060)	(TM)	(DE3)	(SURPM)	(17)	(DEG)	CTR #	CTR	CTR J	CTR #	CTR #	CTR .	CTR Ø	CTR	CTRA
NO.	CLIMBS	(063	(T3)	(DEG)	(surphi)	<u>(FT)</u>	(DEG)	CTR	CTR #	CTRA	CTR #	CTR #	CTRO	CTR #	CTR	CTR #
NO.	CLIMBS	(060)		(DEG)	(suaph)	(19)	(083)	CTR	CTR #	CTR #	CTR #	CTR #	CTR	CTR 0	CTR	CTRA
NO.		(060) 1 CONI		(063)	(suaph)	_(FT)	(OEG)	CTR	CTR	CTRA	CTR #	CTR #	CTR	CTR #	CTR	<u>CTR 8</u>
NO. 501		(DEC) 1 CONI 80		(DEG) MAX ROC	(1.49PM) 98	(FT) VAR.	(DEG) 255	CTR	CTR	CTRJ	CTRA	CTR #	CTR.#	CTR #	CTR	CTR 8
NO. 501 501A		(DEG) 1 CONI 80 80	(KT) NTTIONS 65 75	(DES) MAX ROC MAX ROC	(suaph) 96 96	(FT) VAR. VAR.	(DEG) 255 255	CTR	CTR	CTRJ	CTR	CTR #	CTR.	стя. <b>.</b> 28	CTR	CTR 8
NO. 501 501A 502	CLIMBS PRIORITY CUMP CUMP CUMP	(DEG) 1 CONI 80 80 60	(KT) #TTONS 85 75 75 75	(DEG) MAX ROC MAX ROC MAX ROC	(suaph) 96 96 96	VAR. VAR. VAR.	(083) 255 255 255	CTR	CTR #	CTRJ	CTR #	<u>CTR #</u>	CTR.0 10,11 12 13	стп.» 28 34	CTR	CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMP CUMP	(060) 1 CONI 80 90 60	(KT) (KT) (KT) (KT) (KT) (KT) (KT) (KT)	(DEG) MAX ROC MAX ROC MAX ROC	(suaph) 96 96 96	VAR. VAR. VAR.	(063) 255 255 255	CTR	CTR #	CTRJ	CTR #	CTR #	CTR.0 10,11 12 13	стя <b>е</b> 28 34		CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMB <sup>*</sup> CUMB <sup>*</sup>	(060) 1 CONI 80 90 60	(KT) 84TIONS 85 75 75 75	(DEG) MAX ROC MAX ROC MAX ROC	(suaph) 96 96 96	VAR. VAR. VAR. VAR.	(063) 255 255 255	CTR #	CTR #	CTRJ	CTR #	CTR #	CTR #	стп.) 28 34		CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMP CUMP CUMP	(062) 1 CONI 80 80 60	(KT) 81TIONS 85 75 75	(DEO) MAX ROC MAX ROC MAX ROC	(suapau) 98 98 98 98	(FT) VAR. VAR. VAR.	(063) 255 255 255 255	CTR #	CTR #	CTRJ	CTR	CTR	CTR# 10,11 12 13	28 34		CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMB" CUMB" CUMB"	(062) 1 CONI 80 90 60	(KT) 81TIONS 85 75 75 75	(DEO) MAX ROC MAX ROC MAX ROC	(%49M) 98 98 98	(FT) VAR. VAR. VAR.	(063) 255 255 255		CTR #	CTR	CTR	CTR	стве 10,11 12 13	28 34		CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMB <sup>4</sup> CUMB <sup>4</sup>	(060) 1 CONI 80 90 60	(KT) 81TIONS 85 75 75 75	(DEO) MAX ROC MAX ROC MAX ROC	(1.4994) 98 98 98	(FT) VAR. VAR. VAR.	(083) 255 255 255	CTR #	CTR #	CTR	CTR	CTR	10,11 12 13	стп <i>е</i> 28 34		<u>CTR#</u>
NO. 501 501A 502	CLIMBS PRIORITY CUMB* CUMB*	(DEG) 1 CONI 80 90 60	(KT) 85 75 75 75	(DEO) MAX ROC MAX ROC MAX ROC	(11.4994) 98 98 98	(FT) VAR. VAR. VAR.	(063) 255 255 255	CTR #	CTR #	CTAJ	CTR	CTR	стве 10,11 12 13	стп <i>е</i> 28 34		CTR#
NO. 501 501A 502	CLIMBS PRIORITY CUMB" CUMB" CUMB"	(DEG) 1 CONI 50 50 50	(KT) 11TIONS 65 75 75 75	(DEG) MAX ROC MAX ROC MAX ROC	(1,4494) 98 98 98	(F) VAR. VAR. VAR.	(089) 255 255 255		CTR #	CTAJ	CTR	CTR	10,11 12 13	стп. 28 34		CTR#
NO. 501 501A 502	CLIMBS PRIORITY CUMB" CUMB" HOVER	(DEG) 1 CONI 50 50 60	(KT) 11TIONS 65 75 75 75	(DEQ) MAX ROC MAX ROC MAX ROC	(1,4494) 98 98 98	(F) VAR. VAR. VAR.	(083) 255 255 255		GTR #	CTR J	CTA		стве 10,11 12 13	28 34		CTR #
NO. 501 502	CLIMBS PRIORITY CUMB" CUMB" CUMB"	(DEG) 1 CONI 80 80 60	(KT) 11TIONS 65 75 75	(DEG) MAX ROC MAX ROC	98 98 98 98	(FT) VAR. VAR. VAR.	(089) 255 255 255		GTR #	CTR J	CTA		10,11 12 13	28 34		CTR #
NO. 501 501A 502	CLIMBS PRIORITY CUMP CUMP CUMP HOVER	(DEG) 1 CONI 80 80 60	NTIONS 65 75 75	(DEG) MAX ROC MAX ROC	98 98 96 96	(FT) VAR. VAR. VAR.	(089) 255 255 255		GTR #	GTR J			10,11 12 13	28 34		
NO. 501 501A 502 701		(DEG) 1 CONI 80 80 60 1 CONI 90 90	(17) 85 75 75 75 9	(DEG) MAX ROC MAX ROC MAX ROC	98 98 98 98	(FT) VAR. VAR. VAR. 394	255 255 255 255		GTR #	CTR #	<u>27</u>	GRe	10,11 12 13	28 34		CTR #
NO. 501 501A 502 701 702	CLIMBS PRIORITY CUMB* CUMB* CUMB* HOVER HOVER HOVER	(DEG) 1 CONI 50 50 60 1 CONI 90 90 90	(17) 85 75 75 9 1110NS 0 0	(DEG) MAX ROC MAX ROC MAX ROC N.A. N.A.	98 98 96 96 98 98	(FF) VAR. VAR. VAR. 384	255 255 255 255 255 240		GTR #	CTRS	<u>277</u>		10,11 12 13	28 34	1	6,29,30 29,30
NO. 501 501A 502 701 702 703	CLIMBS PRIORITY CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMB* CLIMBS CLIMBS	(DEG) 1 CONI 50 50 60 1 CONI 90 90 90 90	(17) 1110NS 65 75 75 75 75 75	(DEG) MAX ROC MAX ROC MAX ROC N.A. N.A. N.A.	98 98 98 98 98 98 98 98	(FT) VAR. VAR. VAR. 394 394	255 255 255 255 255 240 225			CTRS	277 277		10,11 12 13	28 34		6,29,3 29,30 29,30
NO. 501 501A 502 701 702 703 704	CLIMBS PRIORITY CUMB CUMB CUMB CUMB HOVER HOVER HOVER HOVER HOVER HOVER	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90	(17) 85 75 75 9) TTONS 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC	98 98 98 98 98 98 98 98 98 98	(FT) VAR. VAR. VAR. 384 394 394 394	255 255 255 255 240 225 240 225 210				277 27		10,11 12 13	28 34		6,29,30 29,30 8,29,30 8,29,31
NO. 501 501A 502 701 702 703 704 705	CLIMBS PRIORITY CUMB* CU	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90 90 90 90 90 90 90	(17) 85 75 75 81 10 10 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A.	98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. 394 394 394 394 394	(069) 255 255 255 240 225 210 195				27 27		10,11 12 13	28 34	1	6,29,3 29,30 29,30 8,29,3 29,30
NO. 501 501A 502 701 702 703 704 705 706	CLIMBS PRIORITY CUMB CUMB CUMB CUMB HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90 90 90 90 90 90	(10) 85 75 75 75 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A.	98 98 98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. 394 394 394 394 394 394	255 255 255 255 255 255 240 225 210 196 180				277 27 27		10,11 12 13	28 34	(TR #	6,29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 501A 502 701 702 703 704 705 706 707	CLIMBS PRIORITY CUMB* CU	(DEG) 1 CONI 80 80 80 80 90 90 90 90 90 90 90 90 90 9	(KT) 85 75 75 9 1TIONS 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A. N.A.	98 98 98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. 394 394 394 394 394 394	(069) 255 255 255 255 240 225 210 195 180 165				277 277		10,11 12 13	28 34	1	CTR # 29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 5014 502 701 702 703 704 705 706 707 708	CLIMBS PRIORITY CUMB" CUMB" CUMB" CUMB" HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER	(DEG) 1 CONI 50 50 60 1 CONI 90 90 90 90 90 90 90 90 90 90	(KT) HTIONS 65 75 75 75 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A. N.A. N.A	(1999M) 98 98 98 98 98 98 98 98 98 98 98 98 98	(FT) VAR. VAR. VAR. 394 394 394 394 394 394 394 394 394	(069) 255 255 255 240 225 240 225 240 225 240 185 180 165 150				277 27		10,11 12 13	28 34		6,29,3 29,30 29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 501A 502 701 702 703 704 705 706 706 707 708 709	CLIMBS PRIORITY CUMB CUMB CUMB CUMB HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90 90 90 90 90 90 90	(KT) 85 75 75 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC	98 98 98 98 98 98 98 98 98 98 98 98 98 9	(FF) VAR. VAR. VAR. VAR. 394 394 394 394 394 394 394 394 394 394	(069) 255 255 255 240 225 210 195 180 165 150 155 150				277 27		10,11 12 13	28 34	1	0,29,30 29,30 0,29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 501A 502 701 702 703 704 705 706 707 708 709 710	CLIMBS PRIORITY CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* CUMB* HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER HOVER	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90 90 90 90 90 90 90	(17) 85 75 75 81 110NS 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A. N.A. N.A	(1.449M) 98 98 98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. VAR. 394 394 394 394 394 394 394 394 394 394	(069) 255 255 255 255 240 225 210 195 180 165 150 135 120				27 27		10,11 12 13	28 34		6,29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 501A 502 701 702 703 704 705 706 707 708 709 710 711	CLIMBS PRIORITY CLIMB*	(DEG) 1 CONI 80 80 60 1 CONI 90 90 90 90 90 90 90 90 90 90	(KT) 85 75 75 75 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A. N.A. N.A	(1999M) 98 98 98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. VAR. 394 394 394 394 394 394 394 394 394 394	(069) 255 255 255 255 240 255 240 255 240 255 240 195 180 195 180 195 135 120 155				277 277		10,11 12 13	28 34	1	CTR # 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30
NO. 501 501A 502 701 702 703 704 705 706 707 708 707 708 707 708 707 710 711 711 712	CLIMBS PRIORITY CLIMB*	(DEGA 1 CONI 80 80 80 80 90 90 90 90 90 90 90 90 90 9	(KT) ATTIONS 65 75 75 75 0 0 0 0 0 0 0 0 0 0 0 0 0	(DEG) MAX ROC MAX ROC MAX ROC MAX ROC MAX ROC N.A. N.A. N.A. N.A. N.A. N.A. N.A. N.A	(1999M) 98 98 98 98 98 98 98 98 98 98 98 98 98	(FF) VAR. VAR. VAR. VAR. 394 394 394 394 394 394 394 394 394 394	(069) 255 255 255 255 240 255 240 255 210 195 180 165 150 135 120 105 90 075			CTR #	277 277		10,11 12 13	28 34	5 m s	6,29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30 29,30

#### TEST CONDITIONS, PHASE 2

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										>>			<b>&gt;&gt;&gt;</b>
	AV-15 NUISE IESI - P	HASE 2 F		105				11/5	11/6	1111	11/5	1170	""
								13NOV	14NOV	16NOV	13NOV	14NOV	18NOV
								CTR#	CTR#	CIR#	CTR#	CTR#	CTR#
	LEVEL FLIGHTS												
COND	R.T.COND	NACELLE	A/S	GLIDESLOPE	RPM	ALTITUDE	HEADING						
200		60	90	<u> </u>	96	364	75	8×	2×		300x	3071	343
200.1		60	90	0	88	394	\$	<u> </u>	<u> </u> 2X		301	30/X	L
	LEVEL TORNS	MODIE			1 1004	LAI TRUE				·····			
251		ANCELLE 60	A/S	GLIUESLOPE		304	75			25			360
				+	- <del>~</del> -	<u>                                     </u>							<u> </u>
253	LEVELLTTURN	60	90	0	98	394	75			26			361
						1							1
		<u></u>			±			<b></b>	•		·		
	FIXED GLIDESLOPES TO 10	OFT WAVE-O	FF			SETUP							
CONDI	FLT COND	NACELLE	AS	GLIDESLOPE	RPM	ALTITUCE	HEADING						T. T. T.
402	DESCENT	60	90	3	98	1048	75	10x	3x		302×	306×	
402.1	DESCENT	60	90	3	98	1048	75	1	3x		303		
410	DESCENT	70	70	6	<u>↓ 98</u>	2100	<u>–</u>	12			304		
622	UESCENT	+	H		H	1 4250	<u>  /*</u>	<b>—</b>	- #			324	<u> </u>
433	UESUBNI		·····	12	- wo	4,000	- <u>^</u>	<b>—</b>	<u></u>			343	
		h	<u> </u>		<b> </b>	+							
		Å	<b></b>		<u></u>	•	<del>ا</del>				· · · · · ·		
	FIXED GLIDESLOPES TO FL	AREMOVER				SETUP							
CONDI	RLT COND	NACELLE	AS	GLIDESLOPE	I FEM	ALTITUDE	HEADING						
469	DESCENT	90 to 95	50 to 0	0/6	98	1665	75		29			327	
470	DESCENT	80 to 95	70 to 0	0/6	98	1665	75		30			328	
471	DESCENT	70 10 95	90 to 0	0/6	98	1665	75	13x	32		305x	330	
471.1	DESCENT	70 10 95	90160	0/6	348	1665	75	14x	32		306x		
472	DESCENT	60 10 95	110100	0/6	98	1665	~~		34			332	
100	access) of			02		87217		<u> </u>	26			224	
4/3	DESCENT	a0 10 95	70 10 0	- 03		2000			23			325	
475	DESCENT	8068	70100	0/12		2000	75		24			326	
		1	1			-							
		1	1			1							
	SEGNENTED GUIDESI ODES					SET D							
COND #	RICOND	NACELLE		GLIDESLOPE		ALTITUDE	HEADING		r			r	
478	DESCENT	70 10 95	90 10 0	0/3/12	96	2000	75		44			341	
		1											
	PILOT DISCRETION TO FLAP	RE/HOVER				SETUP							r
COND#	FLT COND	NACELLE	NS		HPW .	ALTITUDE	HEADING						
480		60	1130, 110 const	<u> </u>	80 10 146	1000							340
400	ARTIONOLO	t	Idecel level at	<u> </u>	861094	1500	<del>  <u>%</u>  </del>	<b>—</b>		13		L	348
483	APPROACHD	60	150, 110 const	<b></b>	86 10 94	1500	75			15			350
484	APHOACHE	60	decel, level att.		98	1500	75			17			352
485	APTHOACHE	75	150, 110 const	steep	86 to 98	1500	75			19			354
486	APPROACHG	8	const	steep	86 to 96	1500	75			21			356
496.1	APPROACHG	95	const	steep	86 to 96	1500	75			23			358
						L	L						
		<u> </u>				1744	<u> </u>			L	J	-	
489	APHOACHA	60	1130, 110 CONST	ł	80.00.96	1000						310	
490		80	Idenal level at		86 to 98	1500	┝╌╬╌┥	<b>—</b>				311	
491.1	APPOACHC	60	decel level at		86 10 94	1500	75		19			321	
492	APPHOACHD	i iii	150, 110 const	1	86 to 96	1500	75		13			315	
493	APPROACHE	60	150, 110 const		86 to 98	1500	75		8			313	
494	APPROACH F	75	150, 110 const	steep	86 to 98	1500	75		15			317	
495	APPROACH G	95	const	steep	86 to 98	1500	75		17			319	

								«« HLO	CARD>	>>		A HUN # >	ə>>
	XV-15 NOISE TEST	- PHASE 2 FL1	CONDIT	ONS				T175	T176	T177	T175	T176	<b>n</b> 77
					REVISED 5/	31/96		13107	14NOV	10NOV	13HOV	1400	1000
								CTR	CIR#	CTR#	CTR#	CTR#	CTR#
	TAKEOFE												
A	TANEUTT	MACHIEL	45	GLIDESLOPE	IPM	ALTITUDE	HEADING						
CORDI	TAVENEA	VAR	PAY	VAR	VAR	VAR	255		7		[	312	
2001	TAKENET	VAR	VAH	VAR	VAR	VAR	255		9			314	L
- AM2	TARECHEC	VAR	VAR	VAR	VAR	VAR	255		1.14			316	
504	TAKEDEED	VAR	VAR	VAR	VAR	VAR	256		16			318	
606	TAKEOFF F	VAR	VAR	VAR	VAR.	VAR	255		18		L	320	
	TAKEDIFE	VAR 1	VAH	VAR	VAR	VAR	255		20			322	
806	TAKEOFF	VAR	VAR	VAR	VAR.	VAR	255		31			329	<u> </u>
807	TAKHTE G	VAR 1	VAR	VAR	VAR	VAR	255		33			331	l
804	TAKENEH	VAR	VAR	VAR	VAR	VAR	255		35			333	L
000	TAXENEL	- VAB T	VAR	VAR	VAR	VAR	255		45			342	
210	TAKE HE	VAR	VAR	VAR	VAR	VAR	256			10			345
211	TAKETHE	VAR	VAH	VAR	VAR	VAR	255			12			34/
610	TAVENEL	VAR	VAR	VAR	VAR	VAR	255			14			349
812	TAKENE	VAR T	VAR	VAR	VAR	VAR	256			16	L		351
214	TAKETEEN		PAY	VAR	VAR	VAR	255			18		L	353
215	TAKHOHO	VAR	PAV	VAR	VAR	VAR	255			20		1	355
- 616	TARBORE	VAB	VAR	VAR	VAR	VAR	255			22			35/
617	TAKEOFF Q	VAR	VAR	VAR	VAR	VAR	255			24			359
	1					I		L		L			
·													
COND.1		MACELLE	AS	GLOSIOFE	<b>FIPM</b>	ALTITULE	HEADING		I				
821	HOVER	90	0	0	98	20	255		40	Į		337	—
822	HOVE	90	0	0	96	20	165		41	L		338	<u> </u>
127	HOVER		0	0	96	20	75		42	L		339	<u> </u>
- 104	HOVER	90	0	0	96	20	345		43	<u> </u>		340	<u> </u>
<b>V</b>									L	<u> </u>		<u> </u>	<u></u>
COND	ALT COND	MACELLE	A/S	GLIDESLOPE	17 <b>7</b> %	ALTITUE	HEADING					-	+
841	ATOLE	90	0	0	17	0	75		37	+		1 330	+
843	ATOLE	90	0	0	77	1 0	255		38	<b></b>		1 330	<b></b>
					1					1		1	1

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Test procedures related to XV- The tests, which took place du of the XV-15 tiltrotor aircraft at -provide a comprehensiv -validate noise prediction -develop and demonstra	<ul> <li>15 noise t</li> <li>15 noise t</li> <li>uring Octob</li> <li>a wide val</li> <li>x a wide val</li> <li>x a coustion</li> <li>n methodo</li> <li>a te low-nois</li> </ul>	ests conducted by Na er and November 19 riety of flight condition c database for NASA logies, and se flight profiles.	ASA-Lar 95, near ns. The and U.S	gley and Bell H Waxahachie, T stated objective . Industry	lelicopte Texas, d es were	er Textron, Inc. are discussed. ocumented the noise signature to:
The test consisted of two distir techniques; Phase 2 directly rr minimizing "approach" noise.	nct phases neasured n	. Phase 1 provided a oise contour informa	an acous tion at a	tic database fo broad range of	r validat operatii	ing analytical noise prediction ng profiles, with emphasis on
This report is limited to a docu conditions, and test personnel	mentation used in th	of the test procedure e test. The acoustic	s, flight results a	conditions, micr re not included	ophone	locations, meteorological
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