



## **AIAA 2000-2386**

### **Aeroelastic Deformation Measurements of Flap, Gap, and Overhang on a Semispan Model**

A. W. Burner, Tianshu Liu  
NASA Langley Research Center  
Hampton, VA

Sanjay Garg  
High Technology Corporation  
Hampton, VA

Terence A. Ghee  
NAVAIR  
Patuxent River, MD

Nigel J. Taylor  
DERA Farnborough  
Farnborough Hampshire, UK

**21st AIAA Aerodynamic  
Measurement Technology  
and Ground Testing Conference  
19-22 June 2000 / Denver, CO**



# AEROELASTIC DEFORMATION MEASUREMENTS OF FLAP, GAP, AND OVERHANG ON A SEMISPAN MODEL

A. W. Burner<sup>\*</sup>, Tianshu Liu<sup>‡</sup>  
NASA Langley Research Center  
Hampton, VA 23681-2199

Sanjay Garg<sup>‡</sup>  
High Technology Corporation  
28 Research Drive  
Hampton, VA 23666

Terence A. Ghee<sup>\*</sup>  
NAVAIR, Code 4321  
Bldg. 2187, Suite 1320B  
Patuxent River, MD 20670-1906

Nigel J. Taylor<sup>†¶</sup>  
DERA Farnborough  
Kuchemann Building X80, Ively Road  
Farnborough Hampshire GU 14 0LX, UK

## ABSTRACT

Single-camera, single-view videogrammetry has been used to determine static aeroelastic deformation of a slotted flap configuration on a semispan model at the National Transonic Facility (NTF). Deformation was determined by comparing wind-off to wind-on spatial data from targets placed on the main element, shroud, and flap of the model. Digitized video images from a camera were recorded and processed to automatically determine target image plane locations that were then corrected for sensor, lens, and frame grabber spatial errors. The videogrammetric technique has been established at NASA facilities as the technique of choice when high-volume static aeroelastic data with minimum impact on data taking is required. The primary measurement at the NTF with this technique in the past has been the measurement of static aeroelastic wing twist on full span models. The first results using the videogrammetric technique for the measurement of

component deformation during semispan testing at the NTF are presented.

## INTRODUCTION

On modern military air vehicles, high-lift systems are used to improve take-off and landing performance. For naval air vehicles, an improvement in the lift coefficient in a landing or approach configuration allows for arrested landings at reduced speeds and/or increased payloads. In addition, reduced landing speeds have been shown to improve safety and reduce stress on the airframe. For conventional take-off or landing (CTOL), improved lift-to-drag ratios allow for shorter take-off runs and/or greater payload capacity. For these reasons, it is imperative to quantify and improve the performance of high-lift systems including trailing edge flap (TEF), gap, and shroud geometry.

An effort has been initiated to develop procedures using the videogrammetric model deformation (VMD) measurement technique to measure TEF gap and flap and shroud geometry changes induced by aerodynamic loading. VMD measurement technique development with multiple cameras was initiated in the 1980s<sup>1</sup>, based on earlier successful wind tunnel tests conducted in the 1970s using film cameras<sup>2</sup>. The introduction of image processing routines coupled with the development of a simplified single-camera, single-view photogrammetric technique permitted automated data acquisition and

<sup>\*</sup> Research Scientist, Senior Member

<sup>†</sup> Research Scientist, Member

<sup>‡</sup> Currently with Hypertherm, Inc., Hanover, NH

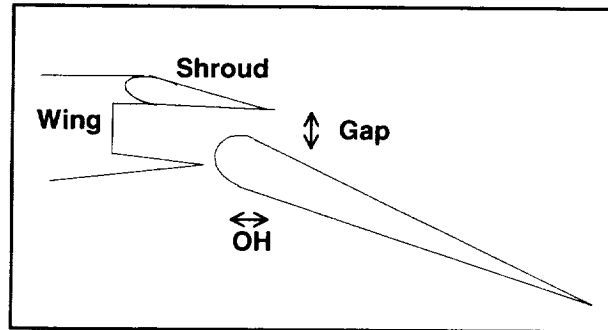
<sup>¶</sup> Currently with Matra BAe Dynamics (UK) Ltd, Bristol, UK  
Copyright © 2000 by the American Institute of Aeronautics and Astronautics, Inc. No copyright is asserted in the United States under Title 17, U.S. Code. The U.S. Government has a royalty-free license to exercise all rights under the copyright claimed herein for Governmental purposes. All other rights are reserved by the copyright owner.

reduction. These developments facilitated near routine use in production wind tunnels<sup>3</sup>. The target-tracking version of VMD developed under NASA contract and used for this test is discussed in reference 4. A review of the VMD measurement technique can be found in reference 5.

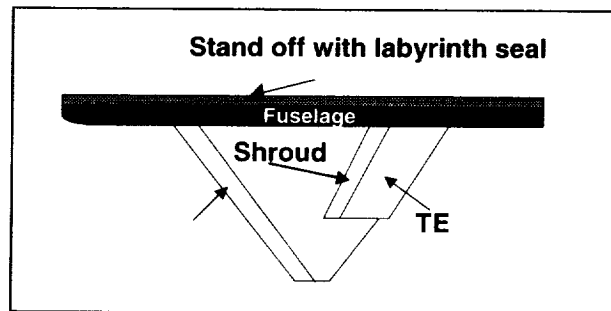
Component deformation measurements are especially troublesome due to difficulty in imaging the area of interest, limited target placement options, and the need to measure small deformation levels that are very sensitive to small errors in pitch angle (dependent on the radius from the center of rotation of the model). Although a few preliminary tests have been conducted during which flap angle changes with flow were measured at other non-cryogenic facilities<sup>6</sup>, this paper will address the first application of the technique for the combined measurement of trailing edge flap and shroud geometry changes under aerodynamic loading at the NTF. In addition, this was the first application of the technique at the NTF with a semispan model and the first optical measurements of component deformation at the facility. Deformation measurements, including the deformation of control surfaces and associated components, are of particular importance in high Reynolds number facilities such as the NTF since high dynamic pressures ( $Q$ ), with accompanying deformation, are typically associated with high Reynolds number testing. For CFD evaluation, it is important to quantify the gap and overhang differences from the static condition due to shroud and/or trailing edge flap deflections under load.

The intent of this paper is not to present extensive data on gap and flap deformation, so only representative data will be presented. Rather, this paper relates experiences using videogrammetry in a large production wind tunnel for such measurements in order to aid potential users of the technique at the NTF and other facilities. Issues related to targeting such as location, application, contrast, surface quality and target thickness will be addressed. Camera installation will be described along with initial camera calibration to establish camera calibration coefficients and camera location in the test section coordinate system. A major concern for high-productivity facilities is that calibration time be kept to a minimum so as not to negatively impact productivity. Techniques employed to significantly reduce tunnel downtime for calibration will be described. The data acquisition procedure and interaction with the facility data acquisition system will be described. The advantages and disadvantages of a commercial prototype target-tracking image acquisition system will be discussed. The data reduction procedure to determine gap and flap deformation due to aerodynamic loading will also be described. The

relation of centroid repeatability to the precision of the measurements will be addressed along with estimates of uncertainty.



**Fig. 1. Sketch illustrating shroud, trailing-edge-flap (TEF), gap, and overhang (OH).**

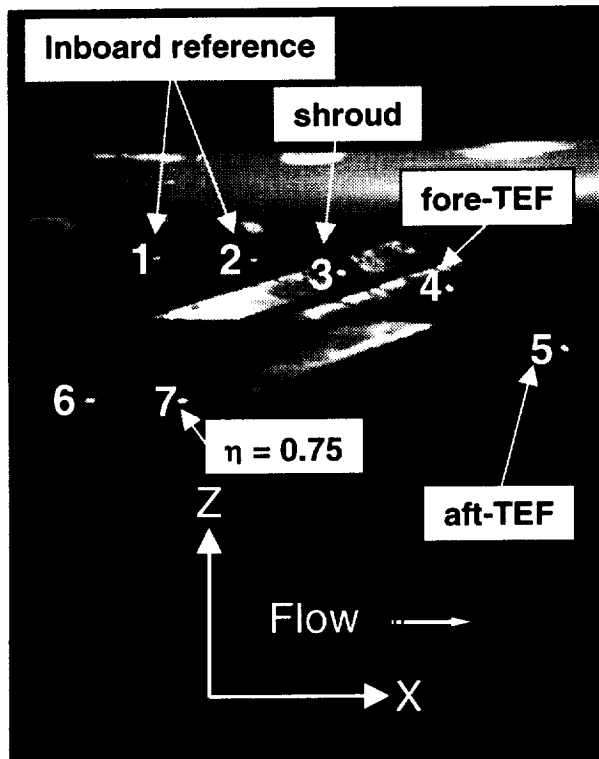


**Fig. 2 - Sketch of Diamond Wing High Lift Model (top view)**

### **TECHNIQUE**

The VMD measurement technique consists of a single-camera, single-view, photogrammetric solution from digital images of targets placed on the wing at known semispan locations. Since only one camera is required, lighting requirements are reduced, which is especially advantageous when using existing test section illumination. The technique is non-intrusive except for the targets, which may have some minor effects on the aerodynamic data. The basic hardware consists of a standard video-rate CCD video camera, a frame grabber board, and a computer with image acquisition and reduction software. A light source is usually located as close to the camera as possible to take advantage of retroreflective targets at all facilities where the technique is used except for the NTF. At the NTF, where stringent model surface finish requirements preclude the use of retroreflective targets, test section lights are used for diffuse illumination of polished paint targets. For measurements at the NTF, the camera is positioned to the side and somewhat above the model, resulting in an oblique view of the model. A target row

is typically placed on or near the fuselage to serve as control in addition to target rows at known semispan locations along the wing. Image processing is used to automatically locate and compute corrected image plane coordinates for each of the targets. Single-view photogrammetry is then used to determine the  $X$  (streamwise) and  $Z$  (vertical) coordinates in object space, given the known  $Y$  (crossflow) coordinates. Vertical displacements at specified chordwise locations and slope angles are computed by linear least squares for each semispan station along the wing<sup>5</sup>.



**Fig. 3 – Model and targets viewed from camera.**

### **FACILITY**

The National Transonic Facility (NTF) is a fan-driven, closed circuit, continuous-flow pressurized wind tunnel<sup>7</sup>. The 8.2 x 8.2 x 25-ft long test-section has a slotted-wall configuration. The wind tunnel can operate in an elevated temperature mode up to  $T = 140^\circ \text{ F}$ , normally using air, and in a cryogenic mode, using liquid nitrogen as a coolant, to obtain a test temperature range down to about  $-250^\circ \text{ F}$ . (However, note that for the test described here the NTF was operated in air mode only at  $95^\circ \text{ F}$ .) Thermal insulation inside the pressure shell minimizes energy consumption. The design total pressure range for the NTF is from 15 psia to 130 psia. The combination of pressure and cold test gas can provide a maximum Reynolds number of

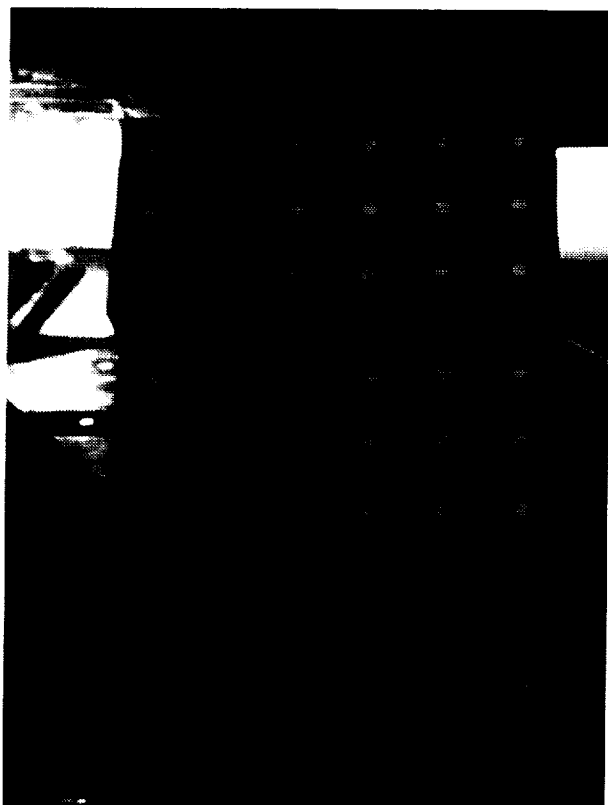
120,000,000 at Mach 1.0, based on a chord length of 9.75 inches. These characteristics afford full-scale Reynolds number testing for a wide range of aircraft. Three types of investigations are possible: Reynolds number effects at constant Mach number and dynamic pressure; model aeroelastic effects at constant Reynolds number and Mach number; and Mach number effects at constant dynamic pressure and Reynolds number.

The constraints imposed by operation in a high-pressure environment over such a wide range of temperatures have had a significant impact on the continuing development, improvement, and optimization of instrumentation at the facility. A major instrumentation challenge at the National Transonic Facility is the requirement to make measurements over the wide range of temperature from  $140^\circ \text{ F}$  down to  $-250^\circ \text{ F}$ . Aeroelastic deformation measurements have been made at the NTF for both High Speed Research (HSR) and Advanced Subsonic Technology (AST) full span models. In all cases before the test described here, the emphasis of the aeroelastic measurements at the NTF was for the determination of the change in main element wing twist due to aerodynamic loading<sup>5</sup>. The results presented here represent the first attempt at the NTF to make aeroelastic measurements on a semispan model and the first attempt to measure the aeroelastics of components in addition to the main wing element.

### **WIND TUNNEL TEST**

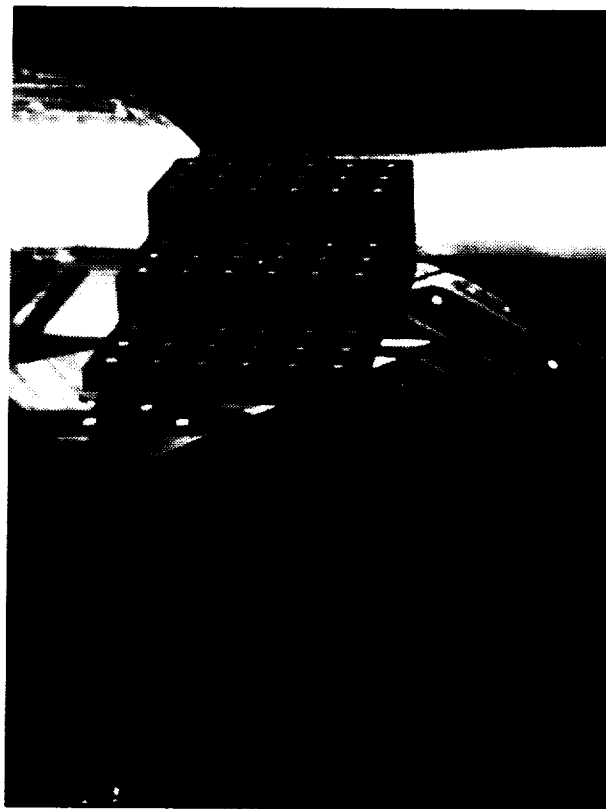
The first evaluation test for trailing edge flap and shroud geometry measurements at the NTF was conducted on a large representative military semispan steel wing during an air mode test at constant Mach number and varying dynamic pressures. Figure 1 illustrates the definition of gap as the distance from the trailing edge of the shroud to a tangent point on the trailing edge flap. Overhang is defined as the distance parallel to the model chordline from the trailing edge of the shroud to the leading edge of the TEF. Figure 2 depicts the entire semispan model with leading-edge-flap (LEF), shroud, TEF, and standoff with labyrinth seal. The labyrinth seal and standoff plate were used to mitigate the effect of the wind tunnel boundary layer on the aerodynamic performance. Uniformly distributed static loads applied pre-test to the wing and shroud indicated relatively stiff wing components with little expected deformation. The air mode test served as an effective means to investigate implementation issues associated with the aeroelastic measurement technique and to evaluate the resolution of the measurement technique, while avoiding the complications that cryogenic operations introduce for optical instrumentation. The semispan wing was tested under the auspices of The Technical Co-operation Program (TTCP), a multi-national test program that includes

NASA, DERA (UK), and US Navy. For this test the angle-of-attack range was  $-5$  to  $24$  degrees, the Mach number fixed at  $0.2$  for the VMD runs, and the dynamic pressure range was  $60$  to  $350$  psf. Parametric studies were conducted on gap and overhang to determine the optimum settings for a configuration with specific angle settings for the shroud and trailing-edge-flap.



**Fig. 4 – View from data camera with 3-stepped plate positioned for determining camera calibration parameters.**

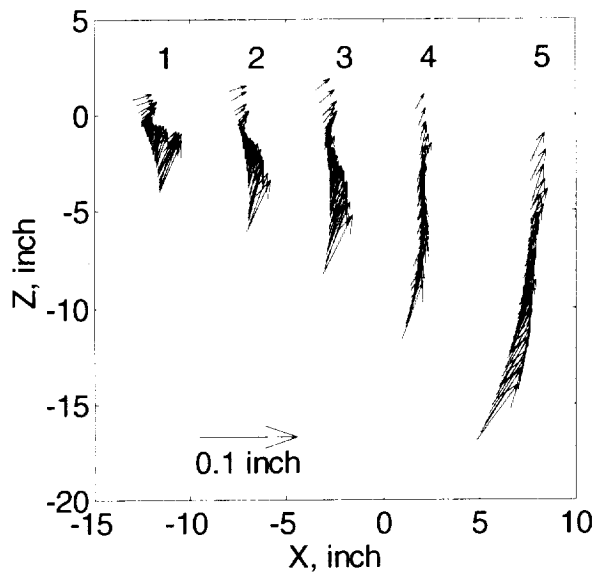
In addition to studying the basic flow physics of military high-lift configurations, the test was also conducted for CFD validation. Results from the test will be used as a bench-mark for future CFD studies to predict high lift system performance and, ultimately, high lift system design. As such, it is critical to gage the extent of deflection of the high lift system under load. The components of the high lift system (trailing edge flap and shroud) act as cantilever beams, which under aerodynamic loading may deflect. Since the gap between the trailing edge flap and the shroud was crucial to the parametric study during the test and is a main parameter for CFD studies, knowledge of the deformation is crucial.



**Fig. 5 – View from data camera with 3-stepped plate positioned for determining camera orientation in test section coordinate system.**

#### **PRE-TEST LOADING OF COMPONENTS**

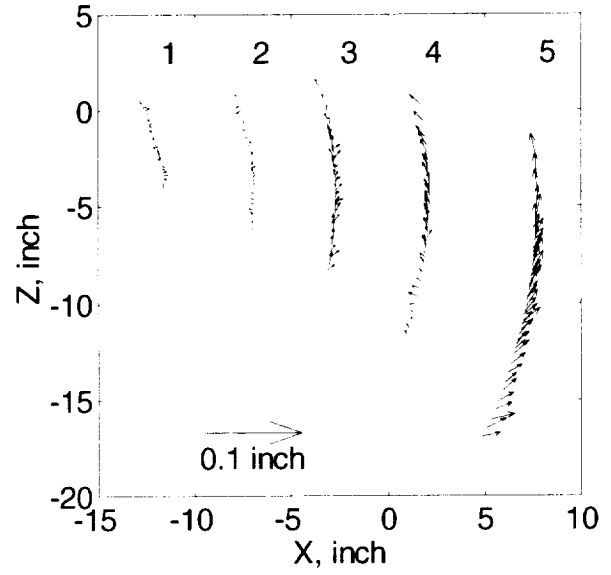
To estimate the potential deflection due to aerodynamic loading prior to testing, static loading tests were conducted. The shroud was uniformly loaded using weighted bags while the trailing edge flap was loaded using point loads attached to the flap ends near the  $\frac{1}{4}$  chord. With the shroud set to a deflection angle of  $23^\circ$  and the trailing edge flap set to  $35^\circ$  (23/35 configuration) a load of  $420$  pounds applied to the trailing edge flap was found to decrease gap a maximum of  $0.008$  inches measured at the bracket location. The shroud, loaded to  $20$  pounds was found to increase gap  $0.0045$  inches. Therefore a pre-test estimate of the maximum change in gap was established to be on the order of  $0.0035$  inches. In the worse case with zero shims corresponding to a gap of  $0.196$  inches (or  $0.5\%$  of the undeflected wing chord located at the mid-span of the flap), the estimated deflection would be  $1.8\%$  of the unloaded gap. The gap and overhang were adjusted using shim plates and serrated teeth, respectively. The gap was variable from  $0.5$  to  $2.5\%$ c and overhang was variable from  $-1.0$  to  $5.0\%$ c in increments of  $0.5\%$ c.



**Fig. 6 - Vector displacements from wind-off to wind-on for a high-Q run without compensation. Target numbers are indicated.**

#### **OPTICAL TARGET LAYOUT & APPLICATION**

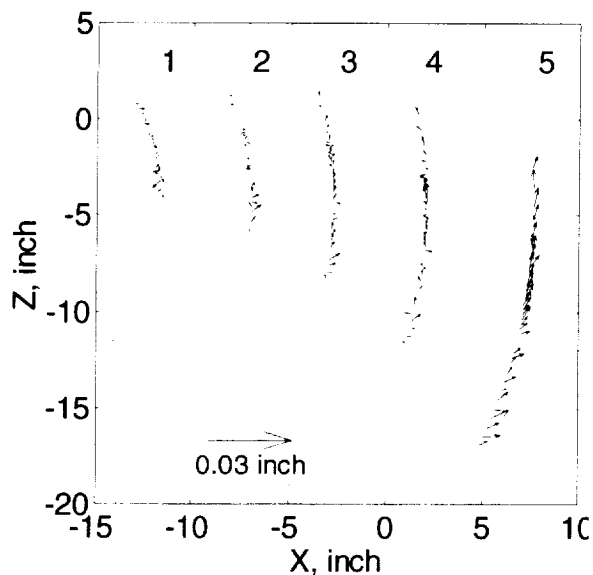
The special illumination technique developed for full-span models at the NTF involves the imaging of a black test-section wall as seen in reflection from the mirror-like wing surface<sup>5</sup>. In such cases good contrast targets are possible with an application of white dots only on the wing and fuselage. A similar illumination technique has not yet been perfected for semi-span testing. Thus to ensure reasonable contrast targets, white dots on a black background were used for this first semi-span test. The targets consisted of polished paint white dots with a 0.5-inch diameter on a black background several diameters wide. The locations of the targets were chosen to minimize interference with pressure taps and generally located away from taps or centered between pressure tap rows. The targets were positioned with aid of precision metal-foil templates that facilitated the target application to model parts that would be used later in the test, especially in one case in which half of two targets would be replaced during a configuration change. The precision metal templates also facilitated the determination of the semi-span ( $Y$ -coordinate) of each target for entry into setup files. All layout, painting, and polishing of the targets was accomplished in a ready bay preparation site before the model was moved to the test section. Some model components were targeted before assembly for use in later configuration changes. The use of precision templates to locate the targets was especially useful since over 90 configuration changes were anticipated for the test.



**Fig. 7 - Vector displacements from wind-off to wind-on for a high-Q run with compensation. Target numbers are indicated.**

The application procedure began with a chemical cleaning of the model to remove any residual oil or film that might hamper adhesion of the paint, which is the standard base-coat used for PSP applications. The circular targets were then masked at the proper locations and painted with an air gun. The masking was removed after an hour or so of drying under IR illumination in order to decrease paint drying time. The masks for the black background stripes were then applied and the black paint applied over the white targets. After drying, the targets and backgrounds were polished with 2000 grit paper and water to yield a thickness of 0.0005 inch and a surface roughness of less than 10  $\mu$ inch as verified by measurements with thickness and roughness gauges.

Two targets were located near the wing root where deformation was expected to be minimum. The wing-root targets were used as reference for computation of the deformation due to aerodynamic loading. Two targets were also placed in a row at a normalized semispan,  $\eta$ , equal to 0.75 in order to determine the change in twist of the main wing element. Targets were placed on the shroud and near the leading and trailing edges of the trailing edge flap. The painted targets with black background can be seen in figure 3 on the trailing edge flap and shroud. The root reference target row can be seen at the top of the figure. This image is from the camera used to make the model

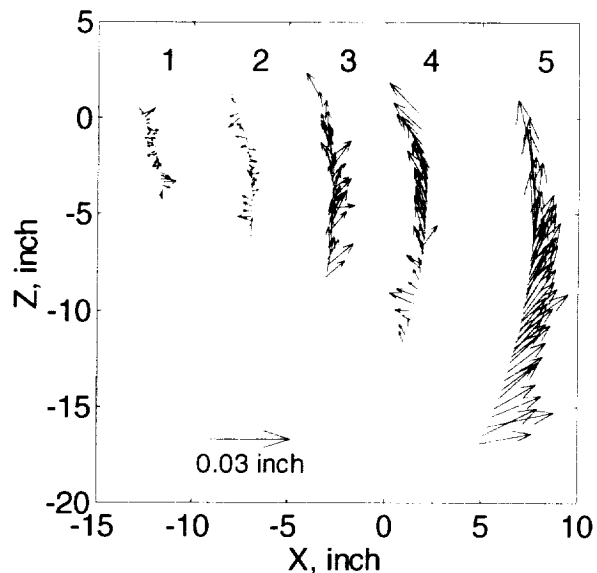


**Fig. 8 - Vector displacements from wind-off to wind-on for a low-Q run (63.5 psf). Target numbers are indicated.**

deformation measurements with targets and coordinate system labeled.

#### **CAMERA SETUP & LIGHTING**

The CCD video camera must be protected from extremes in the operating environment. Temperature and humidity operating requirements for the camera are 0 to 40° C with a relative humidity of 50 to 70%. Environmentally protected pressure housings that can supply heating or cooling are used at the NTF for the VMD cameras due to the large temperature and pressure excursions at the facility. Tests at the NTF have shown that, when possible, it is generally advantageous to mount the camera with a fixed-mount rather than with a pan-tilt unit that may be subject to movement under flow conditions. The interline transfer CCD (charge-coupled device) camera used for this test was an instrumentation grade video-rate camera with a resolution in interlaced mode of 768 pixels horizontal by 493 pixels vertical. The horizontal and vertical pixel spacings are 11.0  $\mu\text{m}$  and 13.0  $\mu\text{m}$  respectively. The target-tracking VMD measurement system digitizes the video image to a resolution of 640 by 480 pixels. A zoom lens was used at a focal setting selected to properly capture the targets of interest throughout the expected pitch range of the test. Standard test-section lighting, also used for surveillance while testing, was used to illuminate the targets. The search for a combination of test-section lights to yield suitable contrast over the entire pitch range was the most time-consuming activity during setup. Often the lighting sett



**Fig. 9 - Vector displacements from wind-off to wind-on for a high-Q run (347.5 psf). Target numbers are indicated.**

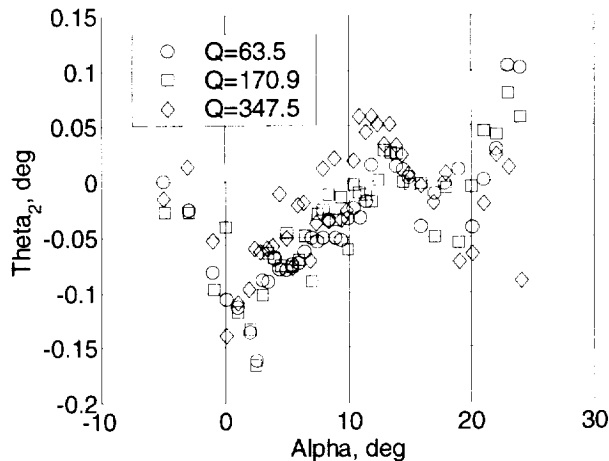
ings used to obtain reasonable contrast at a given pitch angle would be unsuitable for other pitch angles. A compromise in the lighting was finally arrived at that could work over the entire pitch range while still allowing sufficient illumination for the test-section surveillance cameras that are required to be operational during testing.

#### **DATA ACQUISITION SYSTEM**

This was the first test at the NTF in which the target-tracking system developed by the High Technology Corporation (HTC) under NASA contract<sup>1</sup> was used as the primary data acquisition system for model deformation measurements. For previous tests at the NTF, all of which were full-span models, an in-house developed automated image acquisition and reduction system had been used<sup>5</sup>. The in-house developed system works well for scenes in which the targets stand out from the background significantly, such as occurs with the special illumination and targeting technique developed for the NTF discussed earlier. In cases where additional glints or spots on the model might be interpreted as false targets, the in-house system may fail. Since the HTC tracking system tracks individually designated targets (by mouse or by selection of a previous centroid file) continuously at a 15 HZ rate, any glints or "false targets" that are more than a few target diameters away from the true targets will not perturb the data acquisition. Since this was the first time model deformation measurements were to be made on a semispan model at the NTF and the quality of the images was expected to be significantly degraded from



that possible with full-span models, the HTC system was selected for primary data acquisition for the model deformation measurements. A number of potential false targets and glints can be seen in figure 3 that would have been very troublesome for the in-house developed system.



**Fig. 10 Aerodynamically induced twist,  $\theta_2$ , for three dynamic pressures,  $Q$  (psf).**

A major difference between the HTC tracking system and the in-house developed system is that the HTC system tracks targets and outputs centroid files upon trigger while the acquisition program is running, but does not do any additional reduction except for a limited quick look capability. On the other hand, the in-house developed system automatically finds targets, does centroiding, target sorting, matching of data with facility point number, all the photogrammetry necessary to determine change in wing twist as each data point is taken, and outputs the reduced data to files. Since the final reduction can not be accomplished until the end of a set of runs for the HTC system, the data turnaround time is increased from that experienced for full-span models when using the in-house developed deformation measurement system. Thus the model deformation data may be transferred to the customer as a separate data file, instead of being merged with the rest of the data shortly after a run series as for full-span testing. However, the improved robustness of the HTC tracking system for this semispan model proved worth this tradeoff.

#### **SYSTEM CALIBRATION**

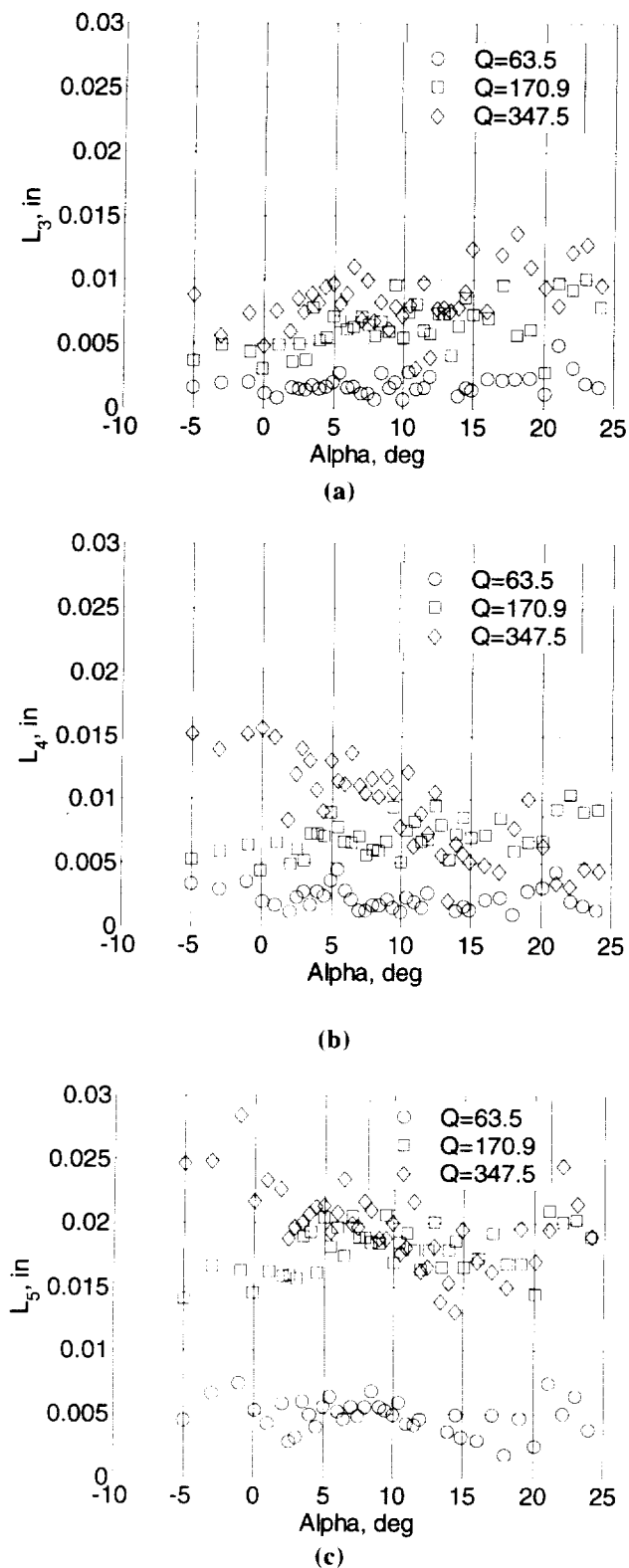
The measurement system calibration is a three-step process. First the camera is calibrated for lens distortion. The location and pointing angles of the camera are then determined in the test section coordinate system. Finally angles and  $X$ ,  $Z$ -coordinates are referenced to a wind-off polar<sup>5</sup> (an alpha sweep over the same pitch range as for a wind-on polar). Figure 4

shows an image from the data camera during the first step. During this phase a calibration fixture consisting of a 3-stepped plate with targets at known locations is positioned to occupy as much of the field-of-view as possible. A centroid file is then recorded from which several camera parameters associated with imaging and needed for the photogrammetric reduction are recovered. The new camera parameters are then used in the subsequent step of the calibration. For the second calibration step, the 3-step calibration plate is aligned to the test section coordinate system so that  $X$  is in the flow direction,  $Z$  is up, and  $Y$  is along the span direction defined by the right-hand rule (figure 5). It is the  $Y$ -value that serves as the known input to enable computations of  $X$  and  $Z$  with a single camera. A row of pressure taps near the root was used to align the calibration plate in the streamwise direction. A precision bubble level was used to establish parallelism to the  $Y$ -axis, which is assumed to be horizontal. It is not necessary to level the plate in the pitch direction (rotation about the  $Y$ -axis) since the offset in pitch is determined by wind-off polars used for final system calibration. The orientation parameters in the test-section coordinate system were then input into the setup file. As a check of the first two steps in calibration and to ensure that the system and setup files are established correctly, the difference in the computed  $X$ -coordinates of targets at the inboard row and outboard row were compared to their known values based on target layout.

The third calibration step begins with a wind-off polar at, or near, the total temperature and pressure that flow data will be taken. A third- to fifth-order polynomial least-squares fit is used to establish correction coefficients based on the onboard accelerometer used to determine the pitch angle of the model. The correction coefficients force the angles measured by the VMD measurement system to agree with the onboard accelerometer and account for slight zero-shifts and changes in system response as a function of time or tunnel conditions. The use of wind-off polars may not be as crucial when conducting tests in air mode such as for this test, but is especially critical when in cryogenic mode due to the larger temperature excursions that are possible, with associated mounting structure movement. For this test the wind-off polars were also used to establish the motion in the  $X$ - $Z$  plane under wind-off conditions. The  $X$ - $Z$  wind-off value at a given alpha (based on the polynomial curve fit) can then be interpolated and subtracted from the flow data to yield differences from wind-off to wind-on.

#### **DATA ACQUISITION & REDUCTION**

Data acquisition was automatically initiated by a TTL trigger from the facility data acquisition system (DAS). Upon trigger, the centroids of the next 75 images



**Fig. 11 – Magnitude of the displacement for (a) shroud, (b) fore-TEF, and (c) aft-TEF for three dynamic pressures,  $Q$  (psf).**

### **DATA ACQUISITION & REDUCTION**

Data acquisition was automatically initiated by a TTL trigger from the facility data acquisition system (DAS). Upon trigger, the centroids of the next 75 images (representing 5 seconds of image acquisition) were recorded to a data file with a sequential *vmd* point number that was independent of the DAS point number. After the centroid file is stored, a file prepared by DAS containing point number, run number, Mach, alpha, and several other tunnel parameters is retrieved from a shared drive to create a log file with DAS data correlated with *vmd* point numbers for later reductions.

At the conclusion of a set of runs, data reduction is initiated by selecting inclusive *vmd* point numbers for the runs that need to be reduced, with the wind-off run(s) and wind-on runs discriminated. MATLAB scripts are then used for further reductions. The data reduction operations include the following. Centroid coordinates in pixel units are converted to mm units based on horizontal and vertical pixel spacings. The distortion correction parameters found in step 1 of the calibration procedure are then applied for use in the single-camera, single-view photogrammetric determinations of  $X$  and  $Z$  target coordinates based upon known  $Y$  coordinates from setup files. Angle computations in an  $X, Z$ -coordinate plane are then made for targets identified as constituting a given row. Polynomial coefficients are determined based upon the wind-off polar(s) for application to the wind-on data to determine the difference between wind-off and wind-on for angles and  $X$  and  $Z$ -coordinates. For the aeroelastic twist computation at  $\eta = 0.75$  the angle of the inboard row of targets near the root of the main wing element was used as reference and subtracted.

In full-span testing, sting bending causes a displacement of the model during flow. Thus at a given alpha, the model position with and without flow may differ, thus requiring the use of a target row on the body as reference to remove any apparent twist of the body. For semispan testing it was assumed originally that a direct subtraction of interpolated  $X$  and  $Z$  values from the wind-off reference polar would be the best procedure. However, it was found that in some cases displacements (real or apparent) between wind-off and wind-on data were actually larger than the relatively small deformation due to aerodynamic loading. Vector displacements from wind-off to wind-on for one of the high- $Q$  runs are presented in figure 6 for targets 1 through 5, with the target numbers indicated above each arc (caused by the alpha sweep during the polar from  $-5^\circ$  to  $24^\circ$ ). Note the similarity of the displacement vectors for the 5 targets indicating rigid body motion. Targets 1 and 2 were located on the very rigid inboard portion of the main wing element where it is reasonable

to assume no deformation between wind-off and wind-on. However significant displacements were recorded (either real rigid-body displacements or an artifact of the measurement process) that must be removed to properly determine the deformation of the shroud and TEF.

Several methods were investigated to eliminate or reduce the apparent displacement of the inboard targets from wind-off to wind-on. These methods included the subtraction of interpolated (from polynomial fits)  $X$  and  $Z$  values of just target 2. (Interpolation of wind-off data is necessary since the wind-on data may not be at the precise settings used for the wind-off polar). A second method involved the use of a conformal transformation via nonlinear least squares using targets 1 and 2 from the wind-off polar (again from polynomial fits) as reference to yield a pitch correction angle and translations in  $X$  and  $Z$ . However, the angle computed using the conformal transformation was found to have errors in  $\alpha$  that were 2 to 5 times larger than the estimated uncertainty of the precision servo accelerometer used to measure  $\alpha$ . Thus a compromise was made and the means of the interpolated displacements in  $X$  and  $Z$  of targets 1 and 2 from the corresponding wind-off polar were subtracted from the wind-on polar to arrive at the final displacement.

Displacement vectors for the run of figure 6 reduced in this manner are plotted in figure 7 at the same scale as figure 6 for comparison. For figure 7, most of the apparent rigid body bias is removed, leaving the wind-off to wind-on deformation. The displacement vectors for targets 1 and 2 on the inboard portion of the main element of the wing serve as a measure of the noise of the measurement process.

The displacement magnitude  $\Delta X$  was computed as

$$\Delta X_n = (X - X_o)_n - \frac{(X - X_o)_1 + (X - X_o)_2}{2} \quad (1)$$

where  $n = 3, 4$  or  $5$  represents the target number on the shroud, fore TEF, and aft TEF respectively,  $o$  represents interpolated wind-off  $X$ -values from the polynomial fit as a function of model  $\alpha$ , and  $X$  without a subscript represents  $X$ -data from the wind-on polar. A similar expression applied for  $\Delta Z$ .

$$\Delta Z_n = (Z - Z_o)_n - \frac{(Z - Z_o)_1 + (Z - Z_o)_2}{2} \quad (2)$$

The displacement magnitude in  $X$  and  $Z$ , denoted by  $L_n$ , was then found from

$$L_n = \sqrt{(\Delta X_n)^2 + (\Delta Z_n)^2} \quad (3)$$

The angle of the displacement vector,  $\phi_n$  was also computed as

$$\phi_n = \tan^{-1} \left( \frac{\Delta Z_n}{\Delta X_n} \right) \quad (4)$$

The order of the signs of the  $\Delta X$  and the  $\Delta Z$  terms was used to determine the four quadrant inverse tangent with a range of  $\pm 180^\circ$  ( $\text{atan2}[\Delta Z, \Delta X]$  function in MATLAB). With this sign convention, positive angles are found for displacements in the positive  $Z$ -direction and negative angles are found for displacements in the negative  $Z$ -direction.

The change in gap,  $\Delta gap$ , due to aerodynamic loading is approximated by

$$\Delta gap = \frac{(\Delta Z_3 - \Delta Z_4)}{\cos \alpha} \quad (5)$$

where  $\alpha$  is the angle-of-attack of the semispan model. The approximation to the change in gap can also be described in terms of the displacement magnitude and vector angle as

$$\Delta gap = \frac{(L_3 \sin \phi_3 - L_4 \sin \phi_4)}{\cos \alpha} \quad (6)$$

Likewise the change in overhang,  $\Delta OH$ , due to aerodynamic loading is approximated by

$$\Delta OH = \frac{(\Delta X_4 - \Delta X_3)}{\cos \alpha} \quad (7)$$

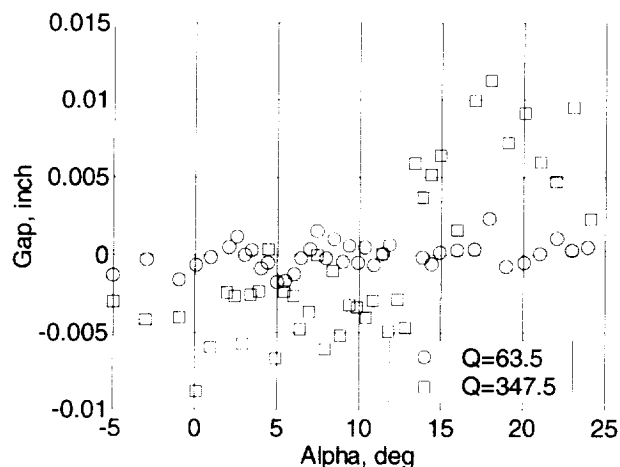
The corresponding relation in terms of the magnitude and angle of the displacement vector for the change in overhang is given by

$$\Delta OH = \frac{(L_4 \cos \phi_4 - L_3 \cos \phi_3)}{\cos \alpha} \quad (8)$$

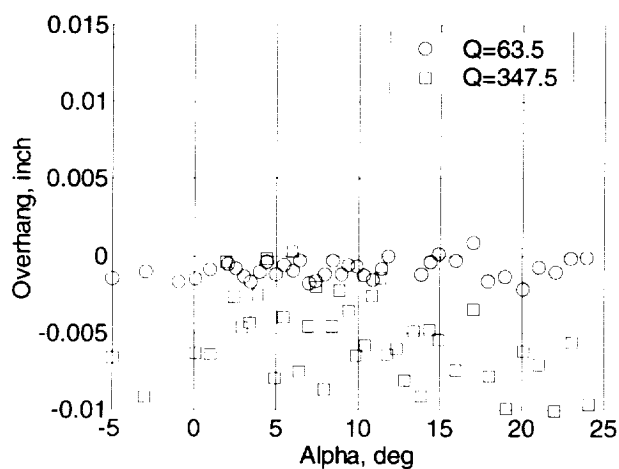
### **REPRESENTATIVE DATA**

Model deformation measurements were not made throughout the test, but rather for selected data sets. All data were taken at Mach 0.2 in air mode at three dynamic pressures of 63.5, 170.9, and 347.5 psf, corresponding to total pressures of 16.2, 43.5, and 88.2 psf. The total temperature was 95° F for all runs. The angle-of-attack range was from  $-5^\circ$  to  $24^\circ$ . Wind-off

reference polars were generally made at pressures of 16.2 and 88.2 psf at the beginning and end of a run series with the 16.2 psf pressure polar used to reduce the 43.5 psf runs. The 43.5 psi runs are thus subject to more error compared to the other pressures.



**Fig. 12 Change in gap induced by Aerodynamic loading for low and high dynamic pressure,  $Q$  (psf), versus alpha.**

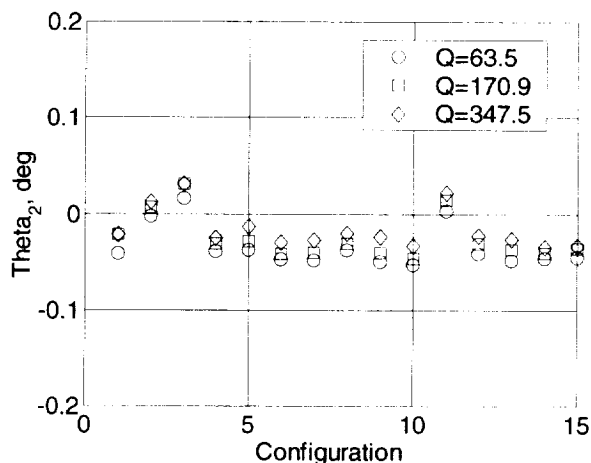


**Fig. 13 Change in overhang induced by Aerodynamic loading for low and high dynamic pressure,  $Q$  (psf), versus alpha.**

Displacement vectors for a low- $Q$  (63.5 psf) and a high- $Q$  (347.5 psf) runs are presented in figures 8 and 9 respectively. (The run presented in figure 9 is the same run used to illustrate the data reduction procedures in figures 6 and 7, but with an increased scale factor for the displacement of 3.3.) For both figures the displacement vectors of targets 1 and 2 serve as a measure of the noise level for the measurement process. For the low- $Q$  run of figure 8 the deformation (except for target 5 on the aft-TEF) is generally within the noise

level of targets 1 and 2. The increased displacements for the high- $Q$  run are obvious, as well as an increase in the noise level. The aft-TEF is seen to generally deflect in a direction influenced by the direction of the aerodynamic loading, with a net reduction in the flap angle. The shroud experiences similar behavior, but with less magnitude and more relative data scatter. The fore-TEF target number 4 actually appears to deflect toward the shroud, which would be consistent with a rotation of the TEF in an upwards sense (+  $Z$ -direction) with the hinge line located below target 4.

The change in twist,  $\theta_2$ , (in degrees) due to aerodynamic loading at a normalized semispan of  $\eta = 0.75$  is plotted versus alpha in figure 10 for each of three dynamic pressures. The low- and high- $Q$  runs are the same runs as plotted in figures 8 and 9. Little direct dependence on  $Q$  is noted and a relatively small amount of twist is indicated. Hence, it is assumed that the values shown in figure 10 are more indicative of the noise level for the twist measurement and serve as an indicator of the maximum twist experienced at the  $\eta = 0.75$  semispan station.



**Fig. 14 Aerodynamically induced twist,  $\theta_2$ , for three dynamic pressures,  $Q$  (psf), versus configuration number.**

The magnitudes of the displacements,  $L_m$ , are plotted versus alpha in figure 11 for low, medium, and high- $Q$  runs. The shroud displacement,  $L_3$ , with the least magnitude of the data plotted, has a definite dependence on the dynamic pressure. At the lowest  $Q$  (63.5 psf) the magnitude of the displacement of the shroud, figure 11 (a), is generally less than 0.003 inch and probably represents the noise level of the measurement system for such measurements. At the highest  $Q$  (347.5 psf), the magnitude of the displacement is generally less than 0.01 inch except at high alpha. A similar behavior is noted for the fore-

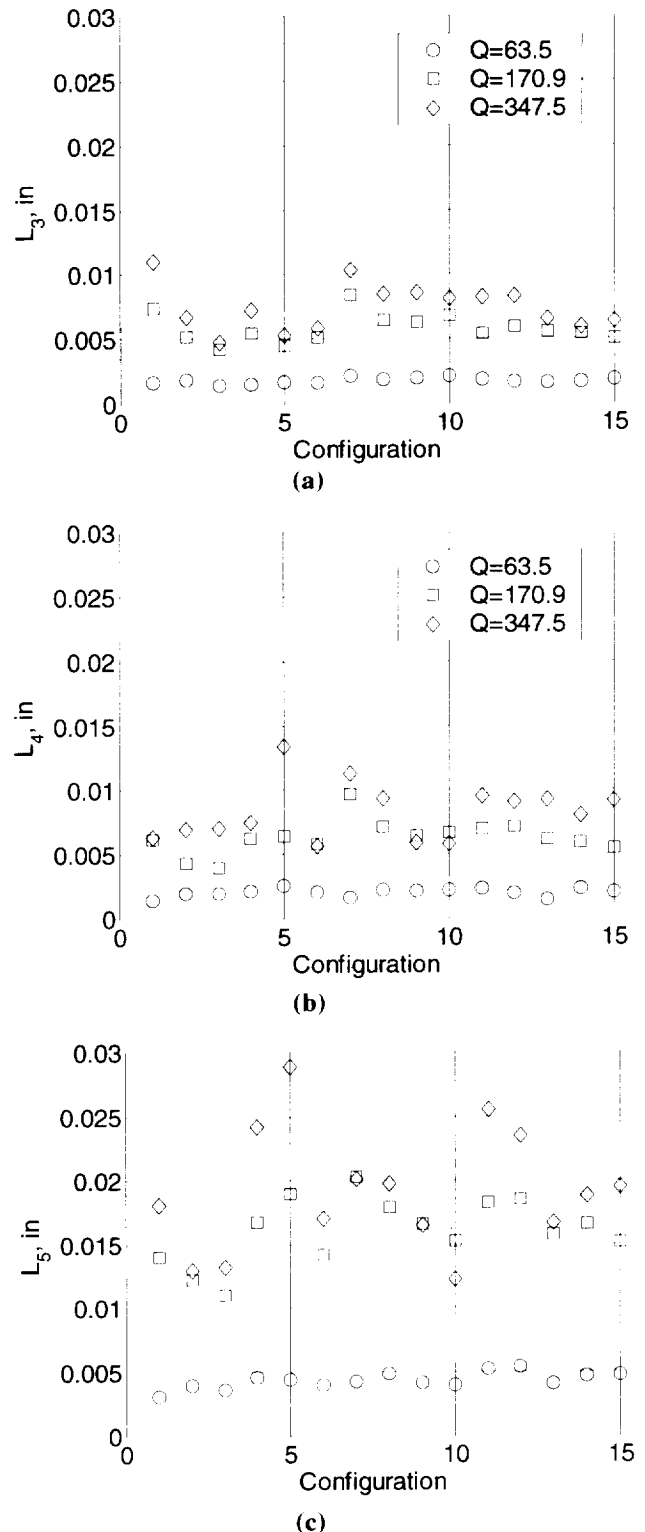
TEF target, figure 11 (b), except that the high-Q data tends to decrease with alpha. The aft-TEF data, figure 11 (c), exceeds considerably the shroud and fore-TEF data and shows little dependence on alpha. The magnitude of the displacement of the aft-TEF approaches 0.03 inch for the high-Q run. The changes in gap and overhang are plotted versus alpha in figures 12 and 13 for the same low and high Q runs of figure 11.

Data for 15 configurations, during which model deformation measurements were made, are summarized in figures 14 and 15. Mean values for all alphas are plotted versus configuration number, to yield a sense of the deformation for a large block of the data set. Data are presented for low, medium, and high-Q runs. The change in twist data,  $\theta_2$ , plotted in figure 14 indicates a noise level for aerodynamically induced twist of about  $0.05^\circ$ , showing little dependence on configuration. The displacement magnitude plots of figure 15 show a clear dependence on Q, but little dependence on configuration.

#### UNCERTAINTY

The VMD measurement system resolution depends on the fraction of the image field that the targets occupy. For cases in which the row of targets span nearly the entire image plane, resolution better than  $0.01^\circ$  is possible in the laboratory. Wind tunnel AoA tests using body targets indicate that  $0.01^\circ$  resolution can be achieved during wind-off tests and may be possible for wind-on tests, provided that the target row(s) occupy nearly the entire image plane and if model translations while changing pitch are not excessive. However, the fraction of the image plane occupied by targets for the test described here is closer to 30% in order to image all segments simultaneously, reducing the resolution considerably from what is possible in a controlled laboratory situation. The targets are also displaced from the center of rotation, especially the aft TEF target, producing relatively large translations in the image plane when pitching the model. The large translations and being located near the edge of the image plane make the measured target locations more susceptible to residual image plane distortion. For similar reasons the displacement measurement precision for this test is of the order of 0.003 inch compared to the 0.0001 inch precision that can be achieved during controlled laboratory experiments.

A change from the standard procedures used for full-span models is that the tunnel alpha was used to determine the correction data from the wind-off curve fit rather than the reference inboard pitch angle determined from VMD measurements. For full-span models, where the change in twist is the primary



**Fig. 15 – Magnitude of the displacement for (a) shroud, (b) fore-TEF, and (c) aft-TEF for three dynamic pressures, Q (psf) versus configuration number.**

measurement and model dynamics can corrupt the onboard accelerometer readings, it has been determined as best practice to use the VMD measured reference angle (usually from targets on the fuselage) instead of tunnel alpha. However, for semispan testing the accelerometer is generally subject to less dynamics, reducing that potential error source. In addition, for situations in which spatial as well as angular data is required, it is advantageous to use the tunnel alpha as reference when the targets are displaced from the center of rotation of the model. In such cases small errors in the reference angle may lead to errors in displacement that are comparable to those due to deformation. For instance, for a target that is displaced from the center-of-rotation by 30 inches, an error of  $0.01^\circ$  causes as error of approximately  $30 \text{ inches} \times 0.17 \text{ milliradians}$ , or 0.005 inch in the displacement.

### **CONCLUDING REMARKS**

During this first use of the videogrammetric deformation measurement technique for semispan testing at the NTF, apparent rigid body motion between the wind-off and wind-on polars was larger than expected. Of the several methods investigated to alleviate this problem, a simple method of removing the mean displacement of the inboard main wing element targets was adopted. As an overall summary, the deformation data were found to be somewhat independent of configuration with little alpha dependence except for the aft-TEF. The aerodynamically induced twist was found to be less than  $0.1^\circ$  overall, which is considered to be the noise floor of the optical measurements for the setup for this test. The noise floor for displacement measurements was found to be about 0.003 inch.

### **ACKNOWLEDGEMENTS**

Luke A. Catella is acknowledged for his innovations in target layout and polished paint application. Harriett Dismond and Kenneth Cate are acknowledged for continuing support in VMD installations, calibration, and operations. The operations and research staff at the NASA Langley NTF are acknowledged for assistance and support in the aeroelastic measurements phase of this test.

### **REFERENCES**

1. Burner, A. W., Snow, W. L., and Goad, W. K., "Model Deformation Measurements at a Cryogenic Wind Tunnel Using Photogrammetry." *31st ISA Symposium*, San Diego, CA, May 1985; published in *Instrumentation in the Aerospace Industry* - vol. 31 ISA pp. 615-622.
2. Brooks, J. D. and Beamish, J. K., "Measurement of Model Aeroelastic Deformations in the Wind Tunnel at

Transonic Speeds Using Stereophotogrammetry", NASA TP 1010, Oct. 1977.

3. Burner, A. W. and Martinson, S. D., "Automated Wing Twist and Bending Measurements Under Aerodynamic Load (Invited)". *presented at the 19th AIAA Advanced Measurement and Ground Testing Technology Conference*, AIAA 96-2253, June 17-20, 1996.

4. Liu, T., Radeztsky, R., Garg, S., and Cattafesta, L., "A Videogrammetric Model Deformation System and its Integration with Pressure Paint". AIAA paper 99-0568, *37<sup>th</sup> AIAA Aerospace Sciences Meeting*, Jan 11-14, 1999.

5. Burner, A. W., "Model Deformation Measurements at NASA Langley Research Center". Presented at the *RTO (formerly AGARD) Symposium on Advanced Aerodynamic Measurement Technology*, Sponsored by NATO 22 - 25 September 1997, Seattle, Washington, published in NATO CP-601, pp. 34-1 to 34-9, May, 1998.

6. Burner, A. W., Liu, T., Garg, S., Bell, J. H., Morgan, D. G., "Unified Model Deformation and Flow Transition Measurements", *Journal of Aircraft*, Vol.36, No.5, Sept-Oct 1999, pp. 898-901.

7. *Research and Technology Highlights 1994*, NASA TM-4708, Dec 1995.



