

# Free Space Laser Communications

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## Outline of Presentation

- Fundamentals
- Spacecraft Technology
- Ground Reception Systems
- Simplified Link Calculation
- Recent Demonstrations
- Future Demonstrations

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## Fundamentals

### Free Space Propagation

- Electromagnetic beams diverge at rates at least as fast as  $\lambda/d$  (Diffraction-limit)
  - $\lambda$  is the wavelength of the radiation
  - $d$  is the diameter of the transmitting aperture
- RF wavelengths usually in the cm-m range
- Optical wavelengths are in the  $\mu\text{m}$  range
- The more wavelengths across the aperture, the more narrow the beam divergence

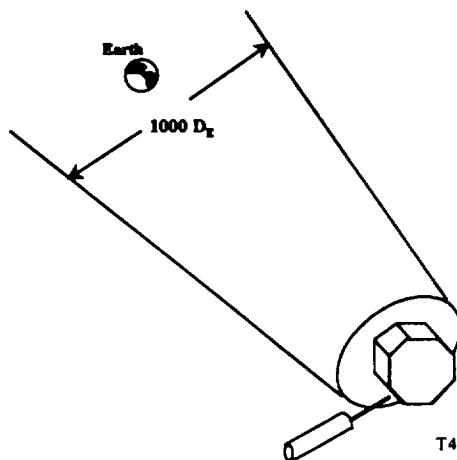
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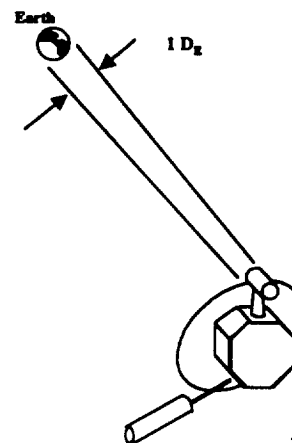
## Deep Space Communications

### Beam Spread

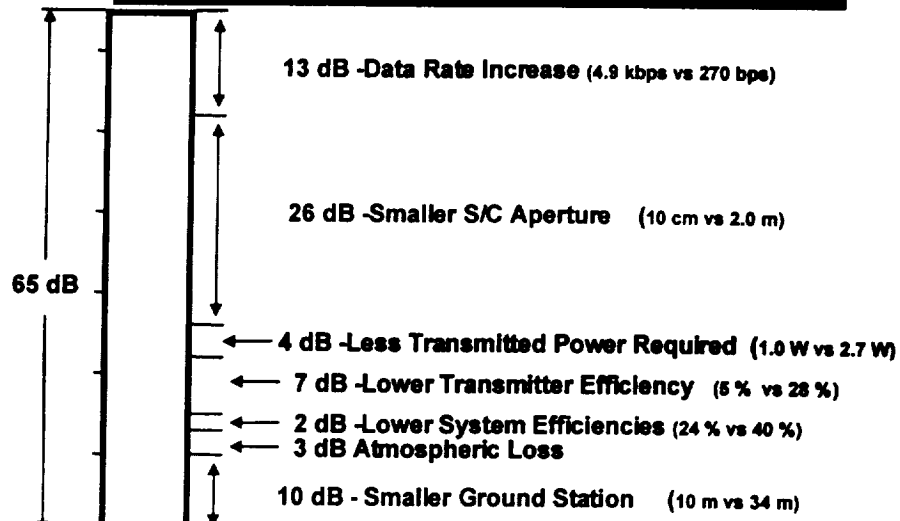
**Voyager (X-Band) at Saturn**  
(3.8m S/C Antenna)



**Optical at Saturn**  
(10 cm Telescope)



## Optical Advantage Relative to Ka-Band (Based on a Pluto FB Example)\*



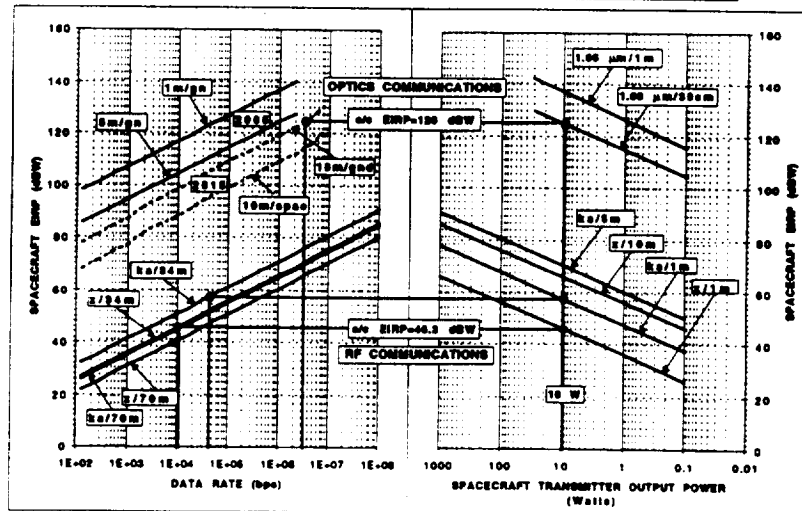
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\* Same Input Electrical Power

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## Comm Link Nomograph

Earth-Mars range: 2.5 AU

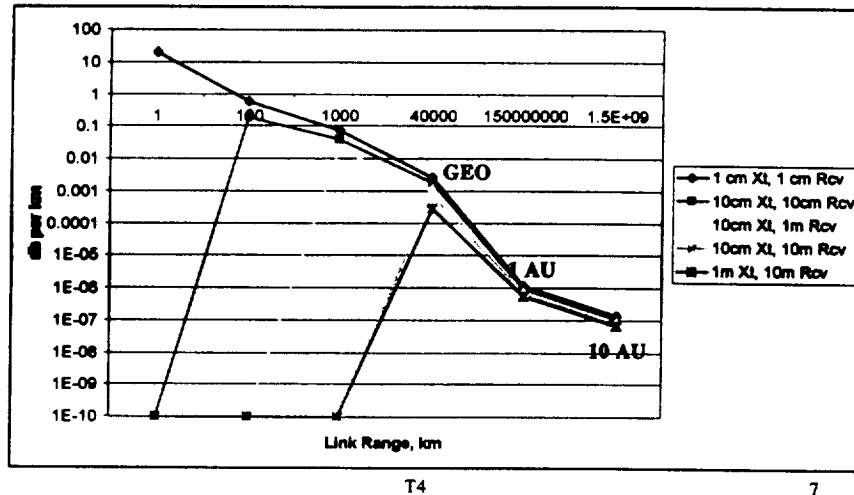


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## Fundamentals

### Equivalent dB/km Loss for Free Space



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## Fundamentals

### Good News/Bad News

- Good News:
  - Optical beams are more narrow
  - Concentrate transmitted energy on target RCVR
- Bad News:
  - Optical beams are more narrow
  - Narrow beams must be more precisely pointed
  - Must track beacon signal from intended receiver

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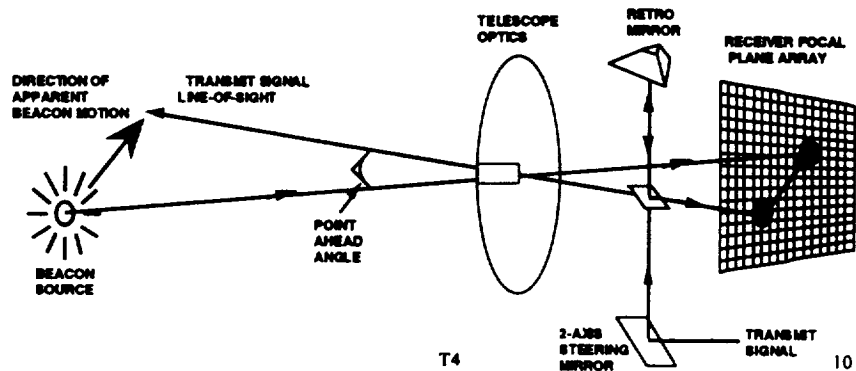
# Spacecraft Technology

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## Optical Communications Demonstrator (OCD) Simplified Optical Design

- Uses only one steering mirror and one detector array for all beam control functions
- Eliminates many beam relay optics and need for large optical bench
- All optics are located on telescope body
- Fiber-coupled laser transmitter signal removes laser heat from optics



# Optical Communications Demonstrator

Telescope Optical Assy (TOA)

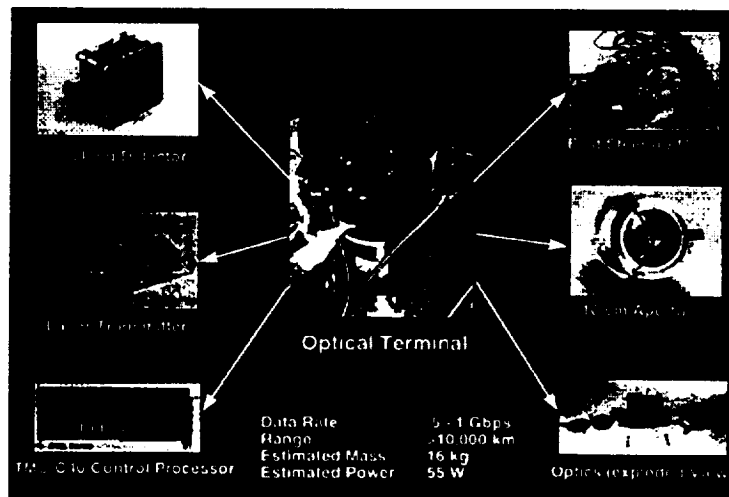


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# Optical Communications Demonstrator

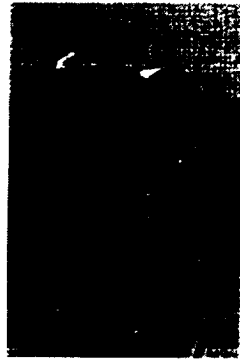
Terminal



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## OCD with Electronic Assy



Telescope Optics Assembly (TOA) on gimbal

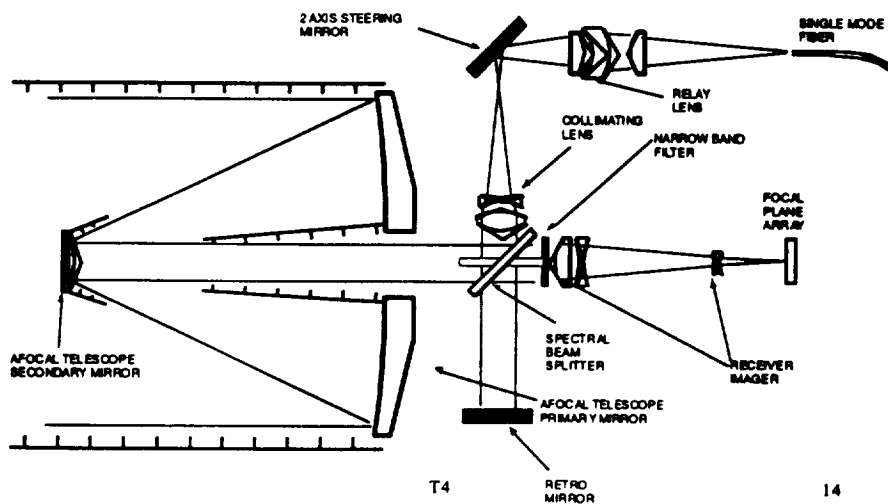
Control Electronics and Enclosure



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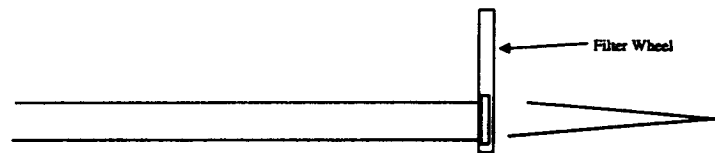
## Optical Communications Demonstrator Optics Layout



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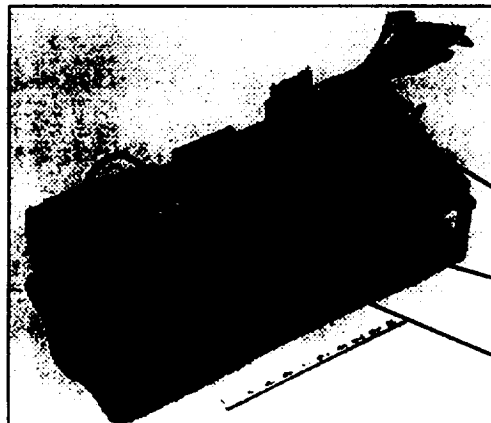
(With Imager)



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## ACLAIM Breadboard Terminal



### ACLAIM

- Laboratory breadboard terminal
- Overall dimensions:  
(4" x 4" x 8")
- Built from COTS parts
- Demonstrates camera/opt comm
- Part of microspacecraft breadboard

2-axis Steering Mirror

APS Detector Array  
(256 x 256)

Fiber Coupled Laser  
(Laser transmitter hidden from view)

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## X2000 Program Optical Comm Subsystem

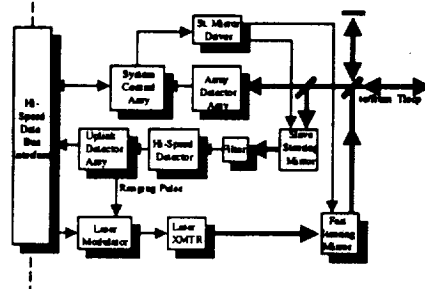


### Multi-Function Uses:

- Optical Comm (uplink and downlink)
- High-Resolution Imaging
  - Science Images
  - Optical (Image-based) Navigation
- Laser Altimeter Reception
- Uplink Ranging Reception
- Downlink Ranging Transmission

### Communications Characteristics:

- Beacon Laser Tracking out to 1 AU
- Earth-Image Tracking Beyond 1 AU
- Redundant Critical Components
  - Lasers, Detectors, Steering Mirrors, Electronics
- >100 kbps (daytime reception)\*
- >300 kbps (nighttime reception)\*
- Mass < 13kg      • Power < 38W



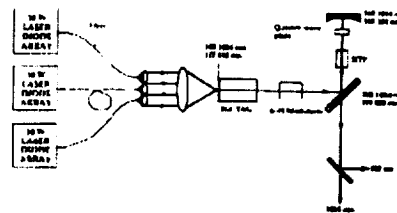
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\* From Europa to a 10-m Photon-beam Receiver

**JPL**

## 2-WATT LASER DEVELOPMENT

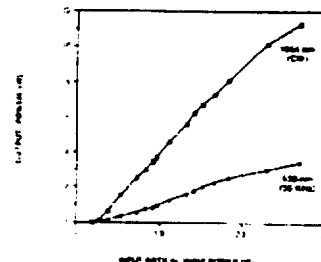
- DESIGNED & DEMONSTRATED A MODULATED, SOLID-STATE GREEN LASER SOURCE
- GOAL: 2 W OF GREEN AT 50 KHz PULSE RATE
- ACHIEVED: 3.5 WATTS (11.7 WATTS CW AT INFRARED WAVELENGTH)
- USES THREE 10-WATT FIBER-COUPLED DIODE-LASER-BARS AS PUMP
- SEVERAL COMMERCIAL COMPANIES INTERESTED IN DESIGN



SCHEMATIC DIAGRAM OF THE SET-UP



PICTURE OF THE SET-UP



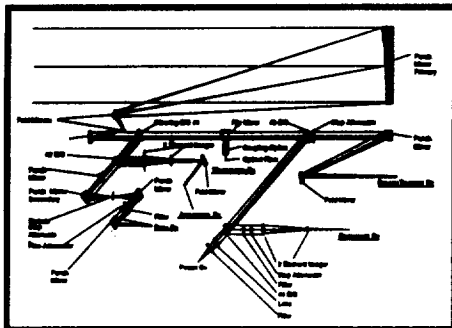
OUTPUT POWER VS. INPUT POWER

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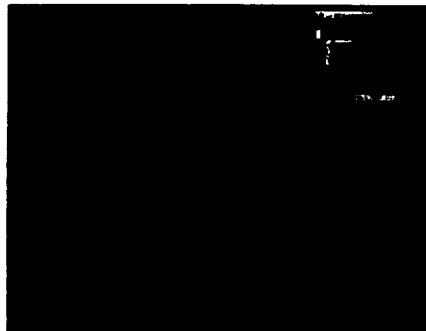
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## Lasercom Test and Eval Station

- LTES is a high optical quality instrument that characterizes the performance of laser communications terminals (LCT's)
  - Measures beam divergence, acquisition and tracking performance, optical output power, and BERs of LCTs up to 1.4 Gbps data rates
  - Appropriate exchange of beamsplitters and detectors allows spectral operating range to extend from 0.5  $\mu\text{m}$  to 2  $\mu\text{m}$



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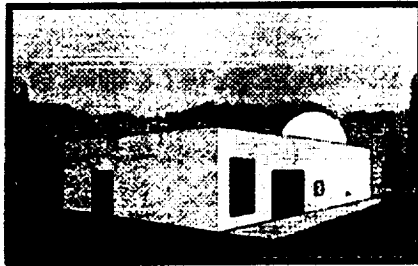
## Ground Reception Systems

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## 1-m Optical Comm R+D Facility

- Optical Comm Telescope Laboratory (OCTL)
- Located at JPL's Table Mountain Facility
  - 2.4 km (7400 ft) elevation
- 1-m diameter aperture
- Fast (Earth-orbit) tracking mount
- Completion at end of 2000



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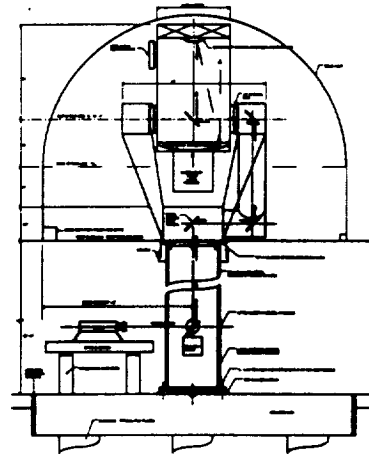
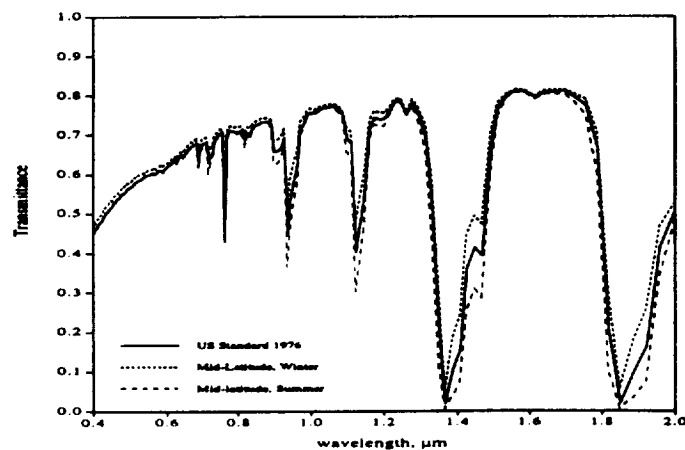


Figure 1a. Telescope Conceptual Drawing (not to scale)

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## Atmospheric Transmission

Clear Weather



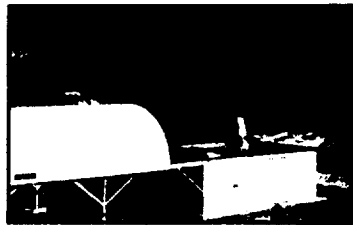
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# Atmospheric Visibility Data

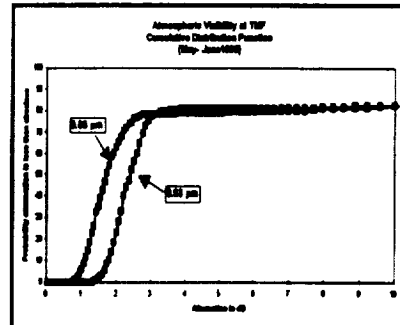


• AVM Observatory at Goldstone, CA



• AVM Observatory at Table Mtn, CA

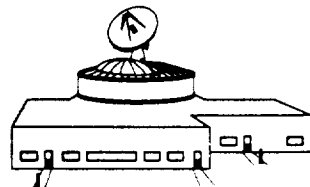
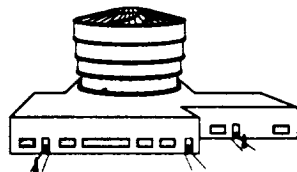
## • Visibility Cumulative Distribution



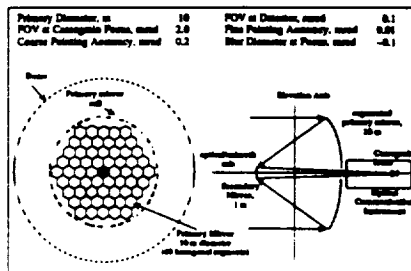
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# Deep Space Reception Station



- 10-m collection aperture
- Photon bucket (non-diffraction-limited)
- Segmented primary mirror



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## Simplified Link Calculation

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## Simplified Link Calculation (Signal Level at Receiver)

- Calculate transmit beam divergence,  $\theta = \lambda/d$
- Calculate spot diameter,  $Z$ , at target  $R$  meters away using  $Z = R * \theta$
- Calculate area of illuminated spot ( $\pi Z^2/4$ )
- Area of receiver =  $\pi D^2/4$  ( $D$ =receiver diameter)
- Propagation loss ( $L_p$ ) is fraction of signal intercepted (receiver area) relative to total spot area =  $D^2/Z^2$
- Received power  $P_r$  (Watts) =  $P_t * L_p * T_a * T_{to} * T_{ro}$ 
  - $P_t$  = Transmitted power
  - $T_a$  = Atmospheric Transmission
  - $T_{to}$  = Transmit Optics Thruput
  - $T_{ro}$  = Receive Optics Thruput
- Received signal rate =  $P_r/(h\nu)$  (photons/sec)

$$h\nu = \frac{2e-19}{\lambda \text{ (in microns)}}$$

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## Simplified Link Calculation (Background Level at Receiver)

- Background Effects
  - Point source interference signals produce a background flux rate over the receive aperture and over a spectral bandwidth (Watts/  $m^2 \cdot nm$ ) if in the detector field-of-view
  - Distributed sources (e.g. daylight) provide a background flux rate over the receive aperture over the entire field-of-view of the receiver (Watts/  $m^2 \cdot nm \cdot Sr$ )
  - Background signals are limited by narrow band filters of BW (in nm) and by detector FPV (in Sr)
  - Received background power ( $P_b$ ) = background flux level \* Receiver area \* filter BW (\*FOV if extended source)
  - Background Noise rate =  $P_b / (h\nu)$  (in photons/sec)

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## Simplified Link Calculation (Detection Performance)

- Signal Detection (performance depends on type of detector, coding, and background levels)

Receiver Type	Sensitivity
Inexpensive Receiver	> 100 photons/bit
State-of-the-Art Receiver	~ 10-20 photons/bit
Low Background/Low Rate Rcvr	< 1 photons/bit

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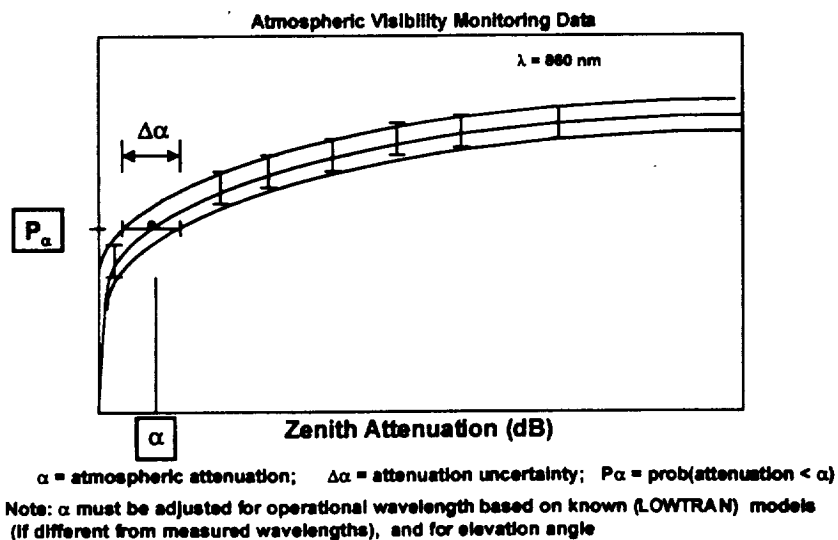
## Comparison of Optical and RF Links

- Optical links are often compared to RF links
  - Need to use a common comparison basis
  - But, optical and RF have some fundamental differences
- Weather affects RF and optical systems differently
  - RF links experience weather fades infrequently
  - Optical must consider spatial diversity reception from the start.
- Need to develop an optical link design methodology that enables comparison with RF but allows for uniqueness of the two technologies

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## Optical Weather Statistics



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## Optical Weather Model

- Atmospheric attenuation ( $\alpha$ ) is a continuous distribution ranging from low values (clear conditions) to very high values (due to clouds)
- Cloud outages impact "Station Availability"
  - Mitigated by station diversity
- Need to define what "outage" means
- Recommendation
  - Use AVM data to define atmospheric model
  - Select a value of  $\alpha$  and the corresponding value of ( $P_\alpha$ )
    - $P_\alpha$  = Probability that attenuation  $< \alpha$
    - Must be corrected for wavelength and elevation angle
  - Approximate the AVM distribution by two states
    - $< \alpha$  means clear (but with some attenuation)
    - $> \alpha$  means (totally) obscured by clouds
  - $P_\alpha$  determines station availability;  $\alpha$  is nominal link attenuation and  $\Delta\alpha$  is weather attenuation uncertainty (when available)

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## Link Analysis Using Weather Model

- Analyze link using  $-\alpha$  (dB) for atmospheric transmission and  $\pm \Delta\alpha/2$  as the favorable and adverse tolerances
- Design link Initially for a "Link Summary" of 0 dB margin using nominal parameter values and calculate the favorable ( $+\sigma_1$ ) and adverse ( $-\sigma_2$ ) uncertainties
- Calculate "Recommended Link Margin" based on the adverse link uncertainty (i.e. margin =  $2\sigma_2$ )
- Redo link design with a nominal link margin equal to the "Recommended Link Margin"
  - Uses visibility data as a basis for link loss and link loss uncertainty
  - Provides a formal basis for establishing value of link margin

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## Link Analysis Example

Link Design Control Table

Parameter	Nominal	Fav	Adv
Transmit laser power	XXX	FFF	AAA
Transmit aperture dia	...	...	...
.	.	.	.
.	.	.	.
.	.	.	.
Atmospheric Trans. (dB)	$-\alpha$	$\Delta\alpha/2$	$-\Delta\alpha/2$
.	.	.	.
Link Summary (0 dB Margin)	0	$\sigma_1$	$-\sigma_2$
Recommended Margin (dB)	$2\sigma_2$		

Note:  $2.2\sigma$  corresponds to 97% confidence

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## Link Availability Analysis

- Optical systems assume spatially-diverse reception
- Assume all ground stations are in independent weather cells (separated by few hundred km)
- Define a station as a "Candidate Station" if it can see spacecraft when atmosphere removed and above some minimum elevation angle (say 20 degrees)
- Define a station as "Available" if it is a candidate station and it has clear weather (i.e. atmospheric attenuation  $< \alpha$ )

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## Link Availability Analysis (Cont)

If  $N$  stations are "Candidate Stations", then the probability that  $m$  of them are "Available" is

$$P_N(m) = \binom{N}{m} (P_\alpha)^m (1-P_\alpha)^{N-m}$$

and the probability that at least one of the  $N$  stations is able to receive the link is

$$P_N = \sum_{m=1}^N P_N(m) = 1 - (1-P_\alpha)^N$$

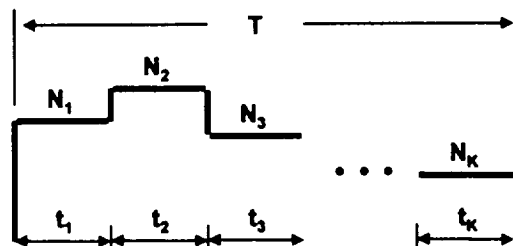
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## Link Availability Analysis (Cont)

Next, consider total time ( $T$ ) of spacecraft support "pass".

Let  $N_1$  be the number of candidate stations at the beginning of this time, and let the number of candidate stations change with time over the pass duration from  $N_1$  (at the beginning) to  $N_K$  at the end of the pass.



Let the corresponding times of  $N_i$  candidate stations be  $t_i$

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## Link Availability Analysis (Cont)

Then, the daily "Expected Data Volume" (EDV) returned for the link considered above, with the weather and station configuration being considered is

$$EDV = R \sum_{i=1}^K t_i P_{Ni}$$

where "R" is the data rate in the link design control table

**RECOMMENDATION : Use EDV for RF/Optical comparisons**

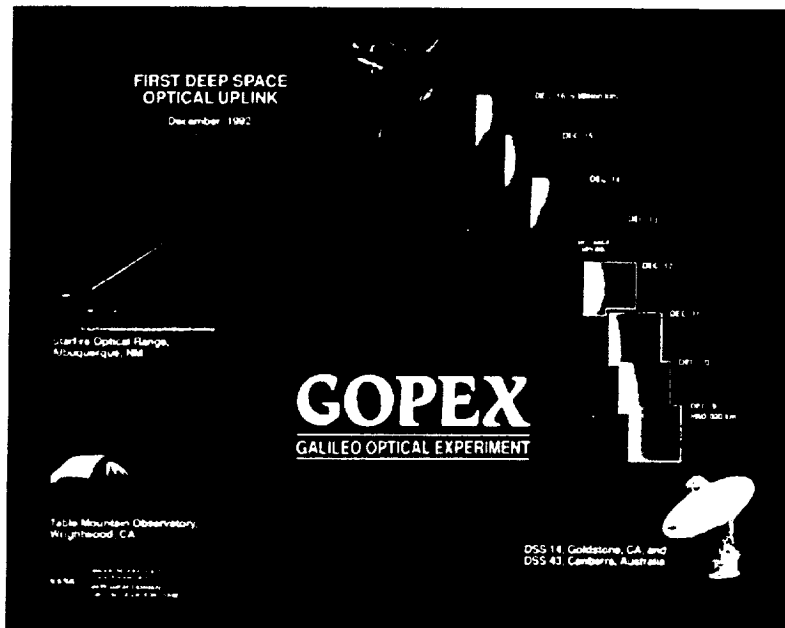
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## Recent Demonstrations

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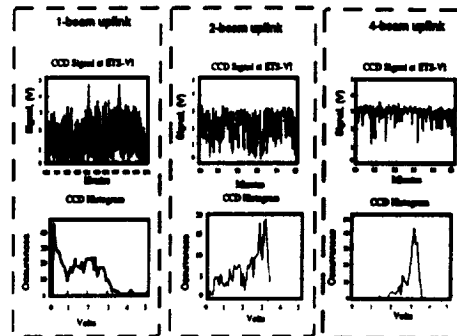
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## Ground-Orbit Lasercom Demo (GOLD) GOLD Multiple-beam Transmission

- Multiple beam uplink mitigates effects of atmospheric scintillation and beam wander
  - Beams are propagated through different atmospheric coherent cells
  - Each beam is delayed relative to the other by greater than laser's coherence length



TMF 0.6-m Transmitter Telescope



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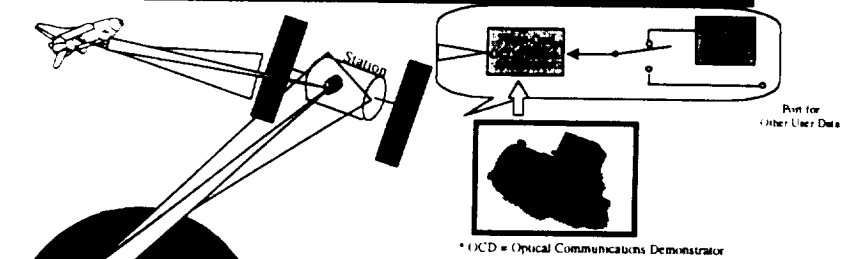
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## Future Demonstrations

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## Demonstration from ISS

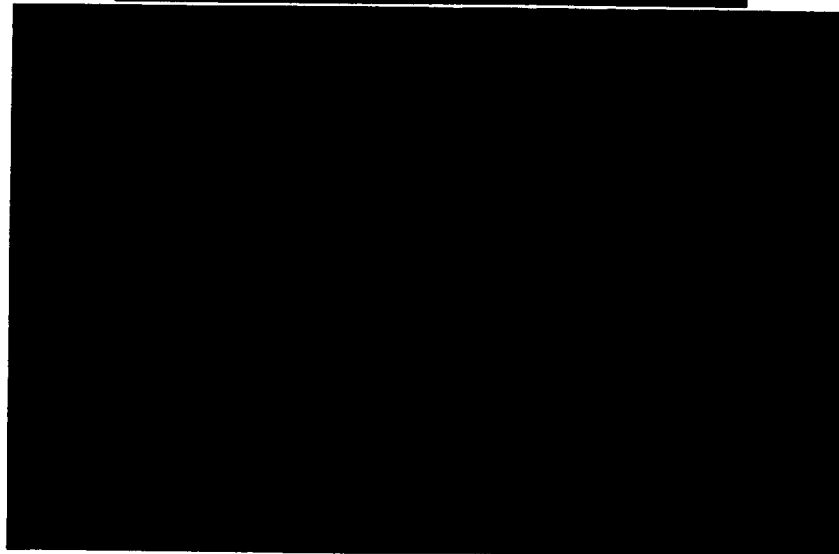


- PN Data dumped to ground at 1 Gbps when over ground site
  - Ground transmits beacon laser to ISS
  - ISS Terminal uses beacon to point downlink
- Station optical comm terminal can also dump other science data to ground
- Can demonstrate space-to-space optical comm if second optical terminal on Shuttle

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## Location of Flight Terminal

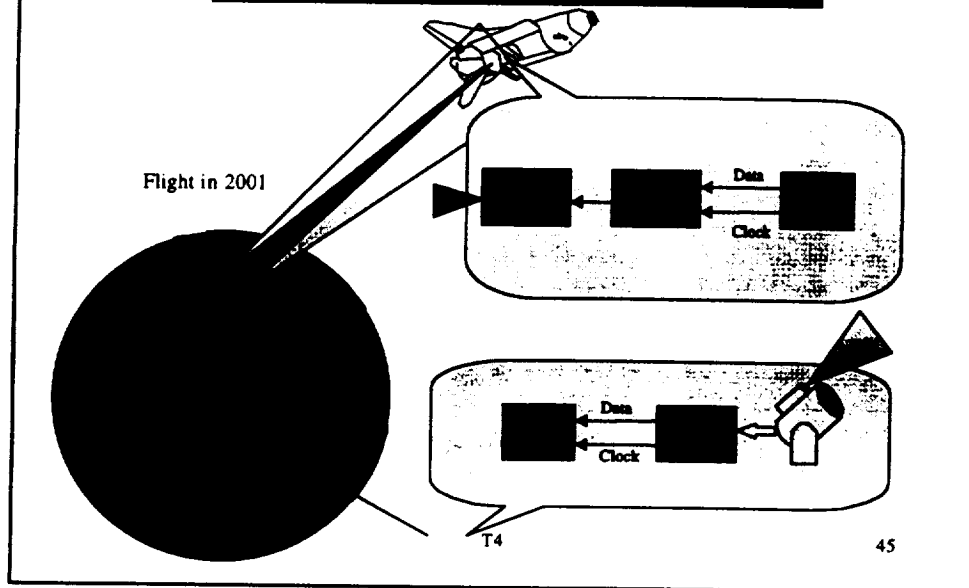


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## FOCAL Demonstration

FOCAL - A Free-space Optical Communications Assessment Link Demo



## Shuttle Link to Ground

1.6 Gbps

Transmit Laser Power	100	mW
Transmit Telescope Dia. (Space)	10	cm
Link Range (Slant range)	1050	km
Receive Telescope Dia. (Ground)	1	m
Atmospheric Losses (space-ground)	7	dB
System Losses	5.2	dB
Detector Efficiency	60	%
Data Rate	1.6	Gbps
Link Margin	21.3	dB

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