

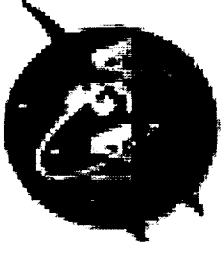
A Regeneratively-Cooled Thrust Chamber for the Fastrac Engine

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Huntsville, Alabama



Overview



- Introduction and Background
- Design
 - Requirements
 - Integrated Engine Concepts
 - Test Article Design
 - Analyses
- Fabrication
 - Fabrication Processes
 - Fabrication
- Test Program
- Status



Introduction



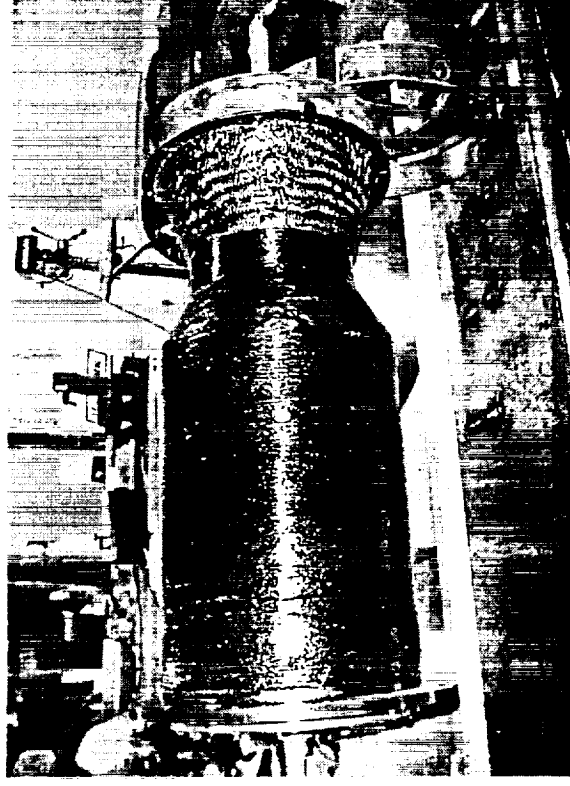
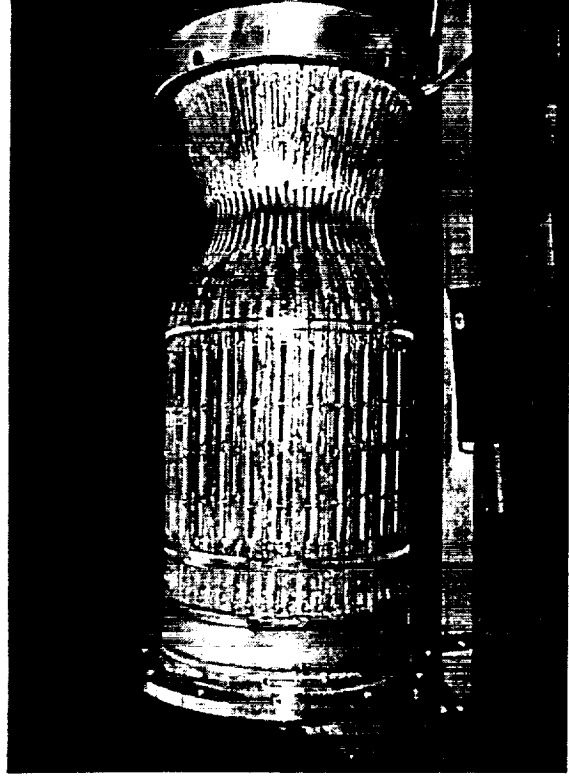
- Fastrac engine was developed to demonstrate low cost design and fabrication methods
- Originally intended for an expendable booster
- NRA 8-21, Cycle 2 solicited low-cost, reusable rocket engine technologies
 - Space America, Inc. proposed and was selected to develop a regeneratively-cooled thrust chamber for the Fastrac engine based on their commercial engine development program
 - Contract ATP 30 August 99
 - Rapid, firm/fixed price contract
- Regen thrust chamber enables more cost efficient test program

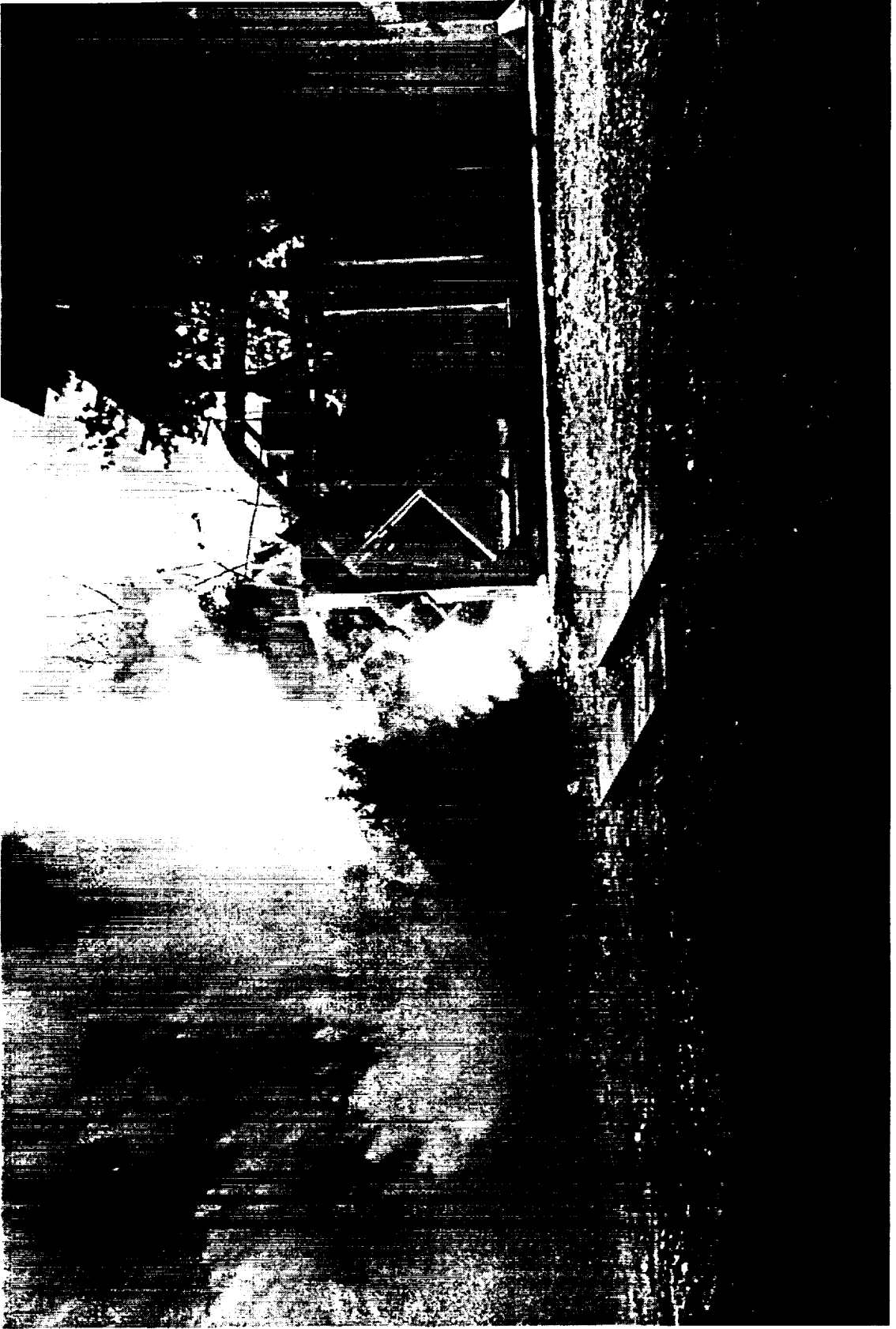
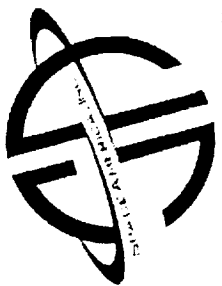


Space America 12K Background



- 12,000 lbf LOX/Kerosene regeneratively-cooled thrust chamber.
- Hydraformed copper tubes, TIG'd together, and brazed to manifolds. Graphite overwrap structural jacket
- 16 starts, 12 to mainstage as-of Nov 99. Still operational
- $P_C=250$ psia, regen-cooled to $\epsilon_e=3:1$, 10.5" ϕ cc, 6.9" ϕ throat
{Fastrac 633 psia, 15:1, 11.3" ϕ cc, 8.25" ϕ throat}







Research Objectives



- Design, develop, and fabricate a regeneratively cooled thrust chamber for the Fastrac engine using the low cost design and fabrication methodology developed by SAI for their 12K regeneratively-cooled chamber.
- Develop conceptual layouts for integrating a regeneratively cooled thrust chamber into the Fastrac engine assembly, with specific application to integration of a regeneratively cooled Fastrac engine into the X-34 flight test program
- Provide a proof-of-concept test article to MSFC for a 3-test series in TS 116.
 - Tested at the same operating conditions.
 - Measure bulk coolant temp increase and the temps at the coolant tube/composite jacket interface.
 - Examine for life limiting hardware issues.



Design Requirements



- Direct comparison to 15:1 ablative nozzle tests, thus 15:1 regeneratively-cooled thrust chamber
 - Interface to MSFC test stand and injector
- Path to integrated engine with regen chamber
- Similar, low-cost fabrication processes as 12K, but modified as needed
 - Single production test article vs production
 - Tube bifurcation required
 - Trade study evaluated 1-pass, 1-1/2 pass, 2 pass
 - 1 pass selected, with 2:1 splice ring



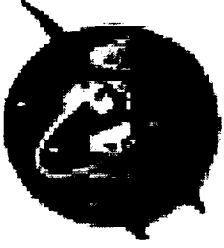
Integrated Engine Concepts



- Turbopump relationships remain unchanged
 - Existing propellant inlets to the engine
 - Existing orientation with respect to the injector
 - Existing MOV position
 - Existing belly band
 - Maintain pressure drop within existing fuel orifice delta-P
- Horizontal start capability
 - Coolant jacket primed at engine start
- MFV can be repositioned
- Existing ignition system
- Maintain injector feed (splitter block and steer horns) as similar to existing as possible
- Use existing TVC actuator bracket
- Ancillary engine components subject to relocation
 - igniter valves, bypass valves, purge valves, TCA igniter assembly, etc.

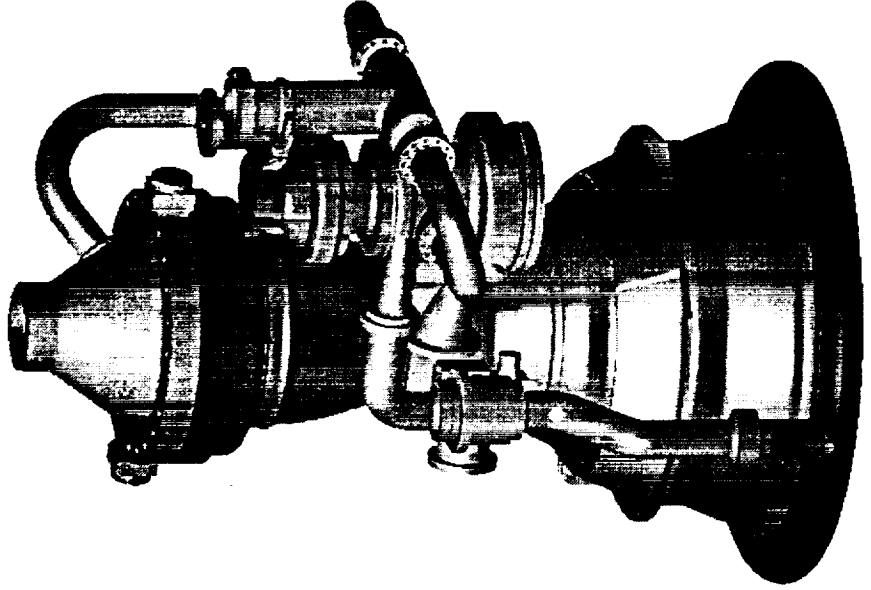
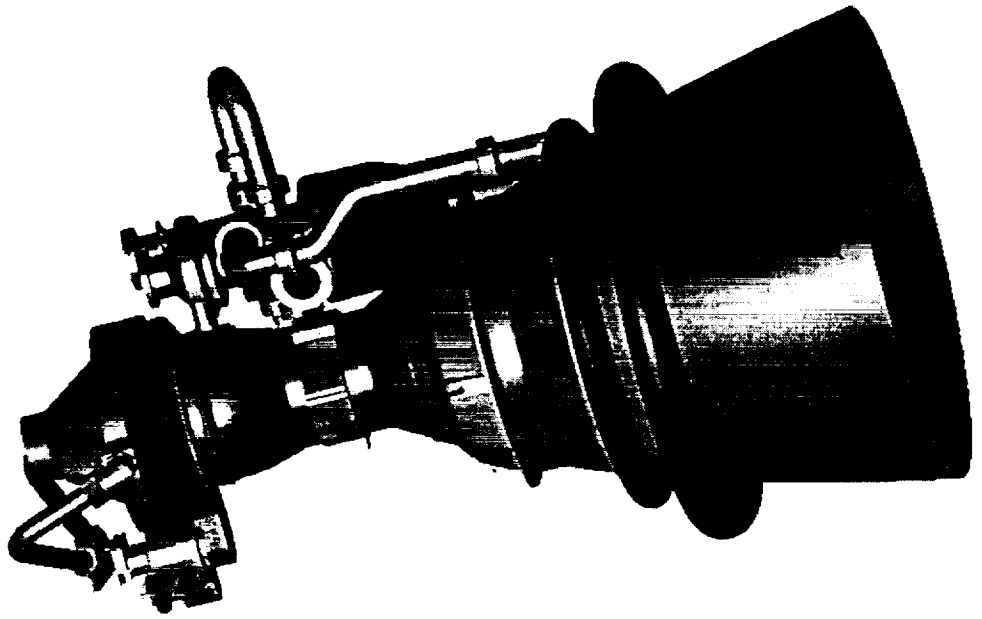


Integrated Engine Concepts



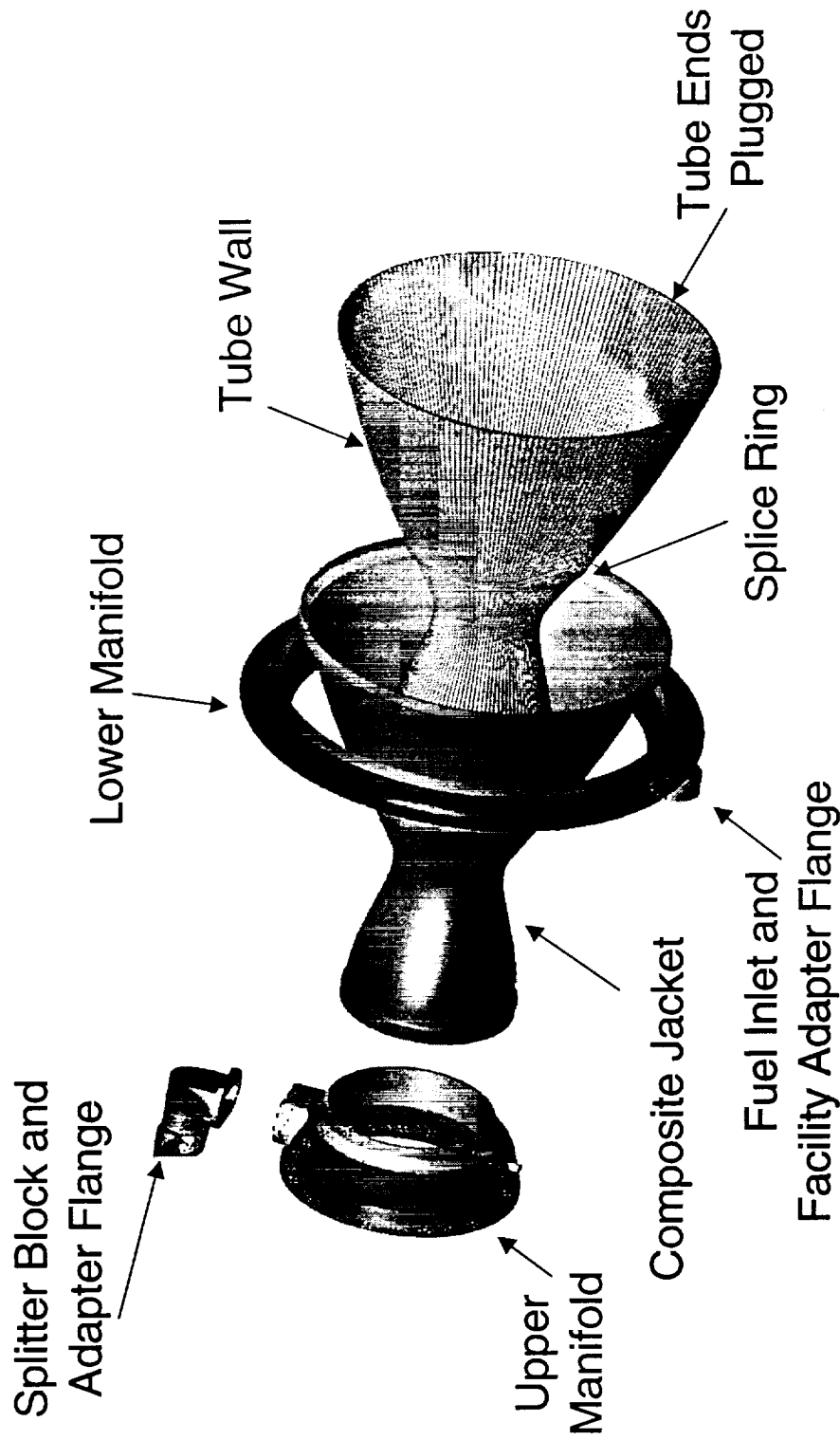
Altitude Application (i.e. X-34)

Booster Application





Test Article Design

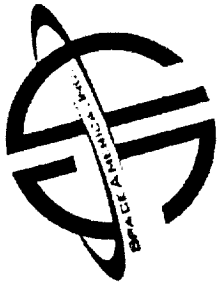




Test Article Design and Fabrication



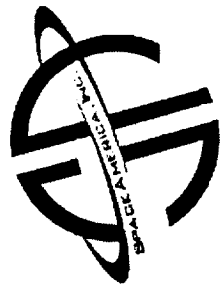
- Coolant tubes
 - Hydraformed C122 Copper tubes
 - Copper selected for high conductivity and formability
- Tubewall assembly
 - Trade study evaluated tube joining processes
 - Welding, torch brazing, furnace brazing, electroplating
 - Selected TIG welding for test article
- Structural jacket
 - Trade evaluated composite jacket
 - Composite jacket vs electroplating
 - Selected composite for test article
 - Fabrication process trade study selected involute method for single production test article
 - Design for TVC actuator loads from X-34



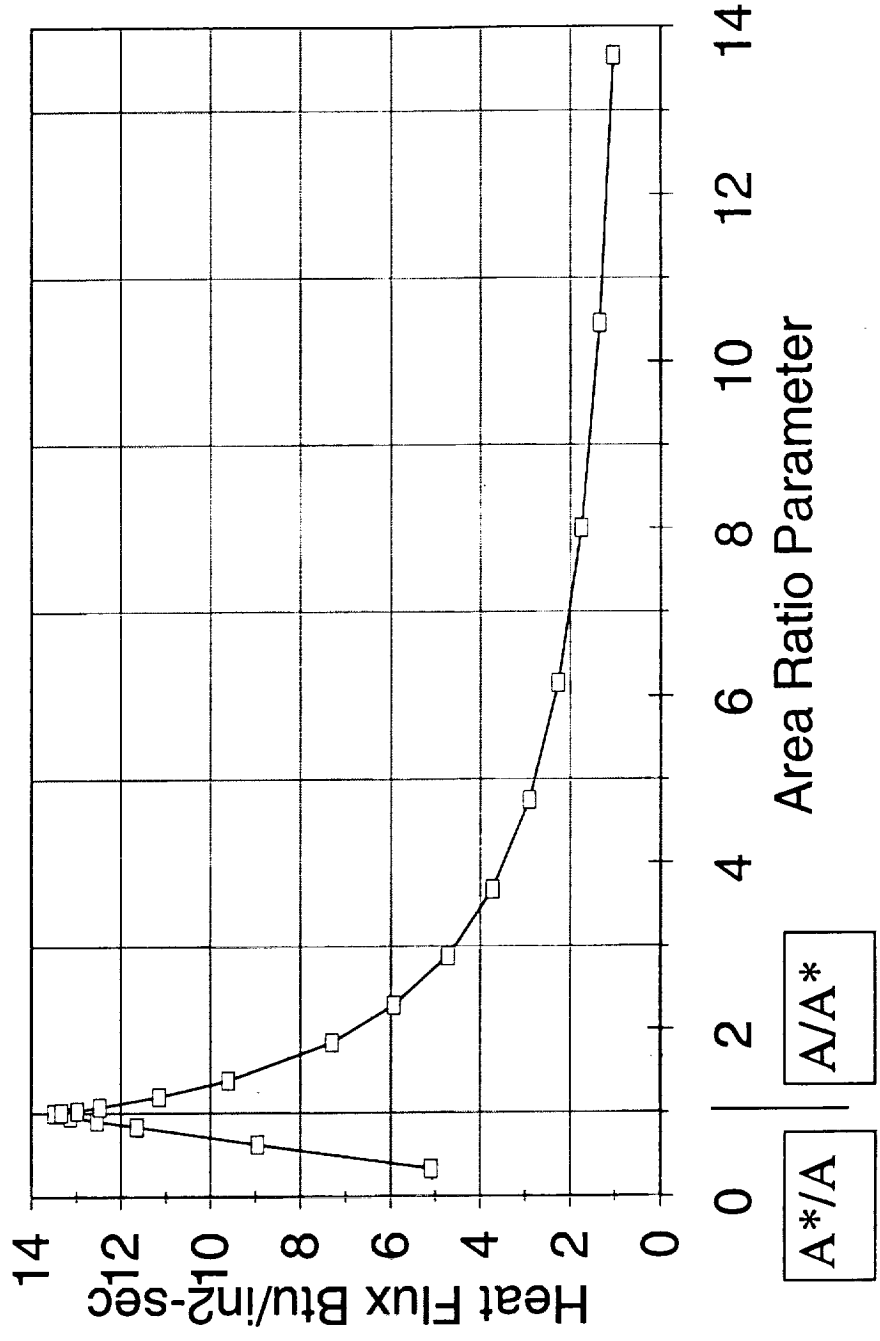
Fluid Dynamic Analyses



- Analytical/Empirical used to begin design
 - Bartz equation to predict heat flux,
 - Correlation to 12K transient and steady-state test data
 - 2-D transient conduction model around tube
 - Pipe flow correlation for coolant flow
 - ΔP and ΔT
- CFD study of hot gas and individual coolant tube followed
 - Hot gas side, with MR gradient for fuel film cooling
 - Liquid side 3-D Navier-Stokes w/variable properties
 - Used predicted tube wall temp from analytical prediction
 - Bulk ΔP and ΔT compared very well with analytical
 - Boundary layer maximum temp less than coking limit



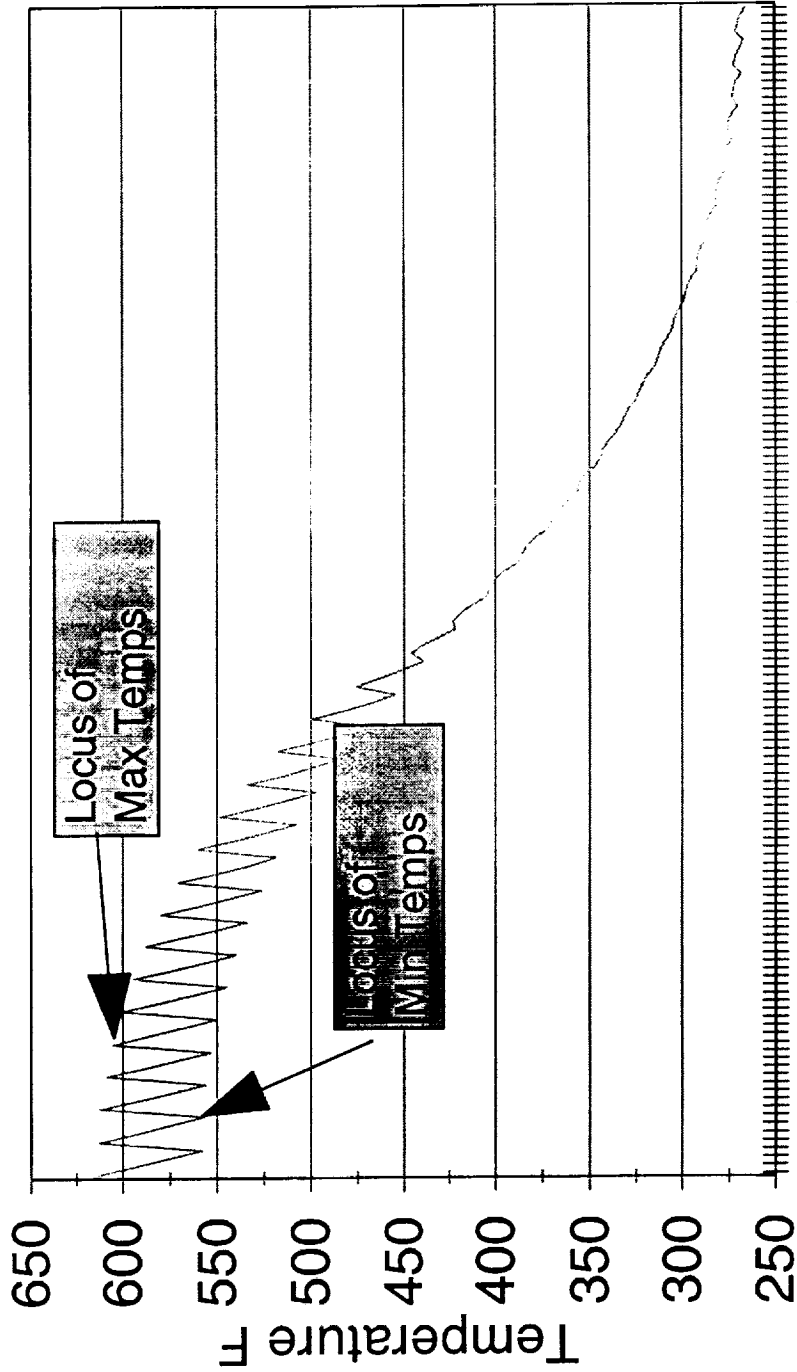
Bartz Equation, Fastrac Engine





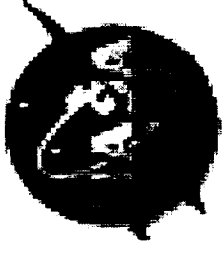
Fastrac Tube Transient Analysis

Steady State Temps





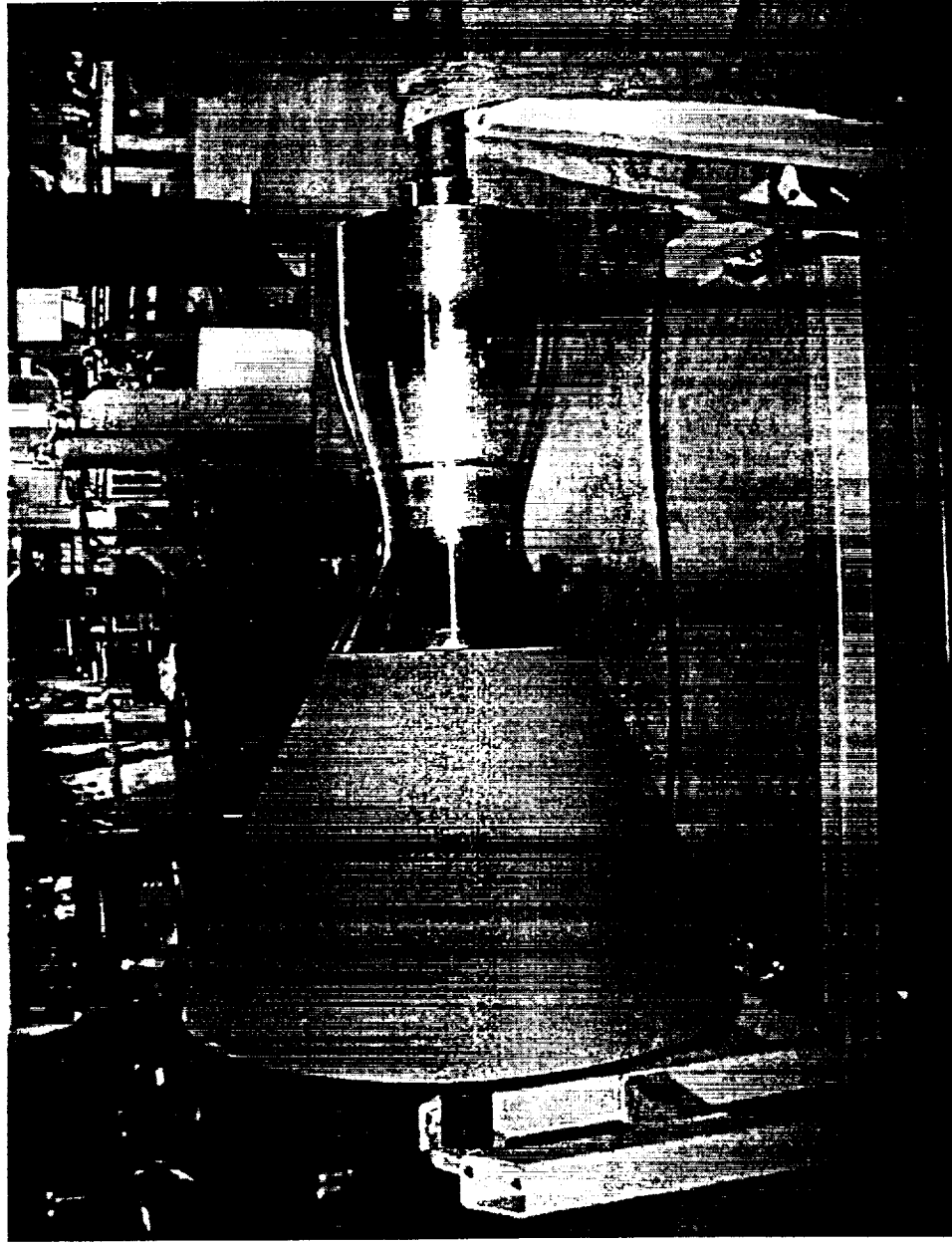
Structural Design and Analysis

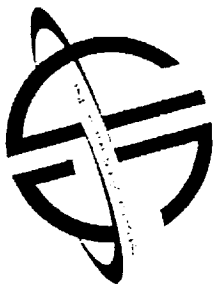


- Two-step design and analysis
 - Hand-calc and CADD add-in FEA program for initial design
 - Composite jacket sized for TVC actuator loads
 - Tube cross-sectional profiles modeled with FEA, and analysis validated against 12K geometries.
 - Detailed Finite Element Analysis
 - Included internal chamber pressure, tube internal pressure, TVC actuator load, and thermal.
 - Showed area of concern between throat and splice ring
 - Test article won't have actuator band or tested with actuator loads
 - Requires further analysis

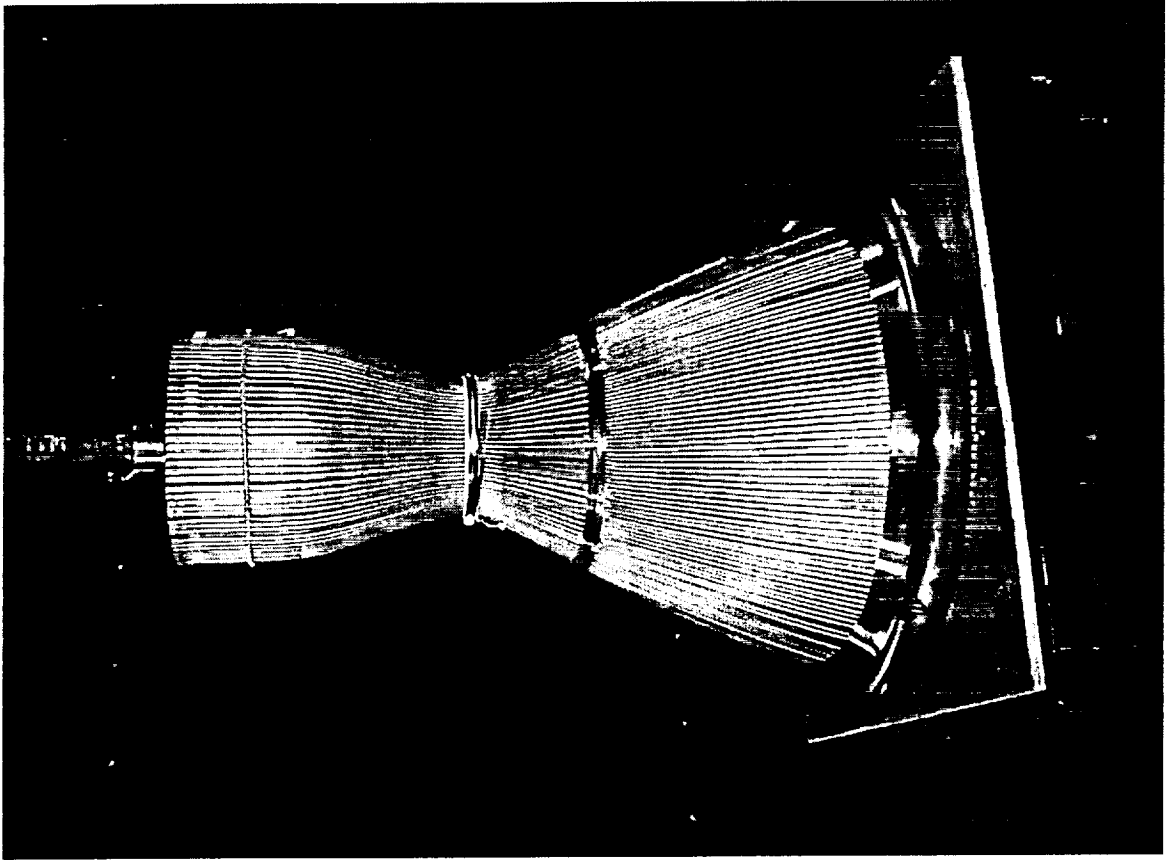


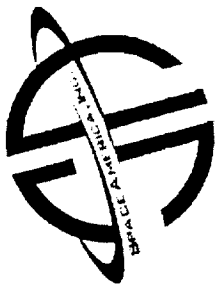
Assembly Mandrel



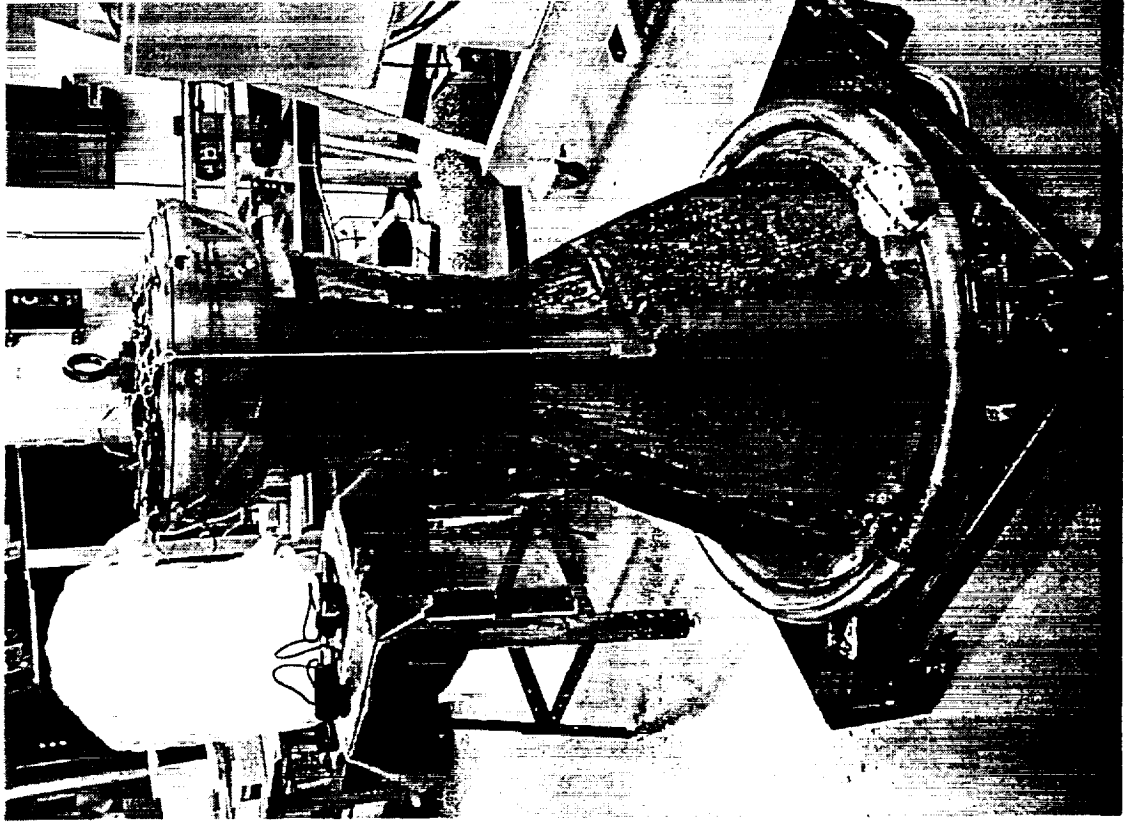


Tubewall Assembly Dry-fit



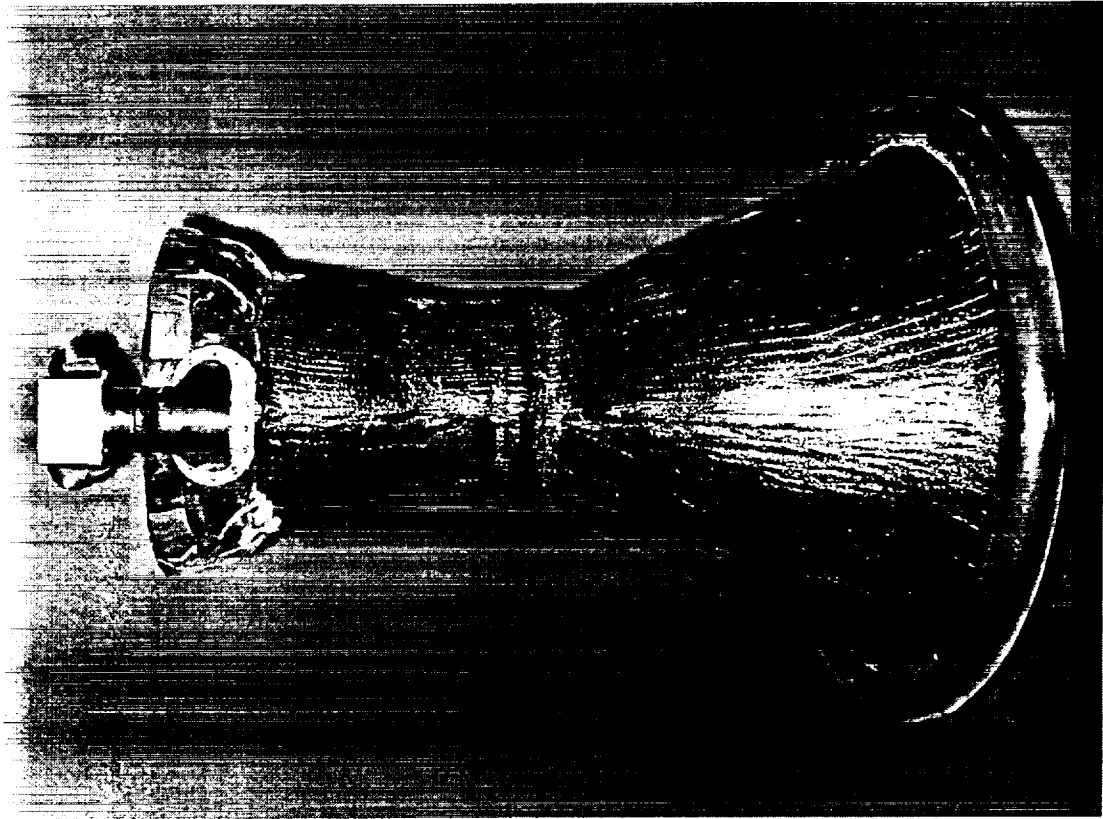


Involute Jacket Assembly





Completed Regen Thrust Chamber





Test Plan



- 3-test test series at MSFC component test stand
 - 10-second test with LOX flow at stage 1 and full fuel flow. Chamber pressure approximately 400 psia.
 - 30-second mainstage test, targeting nominal chamber pressure 633 psia.
 - 150-second (full duration) mainstage test, targeting the same condition.
- Instrumented for manifold pressures, bulk coolant temp, and tubewall/composite jacket interface at 41 pts.
 - Compare to predicted.
- Inspect for signs of life limiting conditions.
- Awaiting test stand availability
 - Testing expected this Fall



Summary



- Project successfully demonstrated ability to fabricate a low-cost regeneratively-cooled thrust chamber
 - Expected production cost 2.5 to 3.5 times the expendable ablative nozzle, but
 - Expected life equal to or exceeding the 7 full duration test requirement of the balance of engine components
- Testing to verify proof-of concept