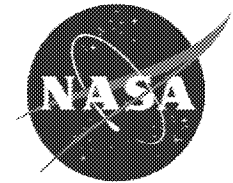
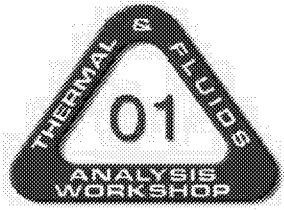


Incorporation of Condensation Heat Transfer in a Flow Network Code

Miranda Anthony & Alok Majumdar

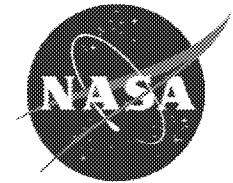
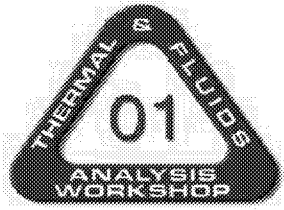
NASA/Marshall Space Flight Center

Huntsville, Alabama



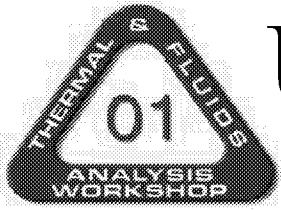
Content

- Introduction
- Problem Description
- Generalized Fluid System Simulation Program
- Condensation Heat Transfer
- Solid to Fluid Heat Transfer
- Numerical Model Results
- Conclusions
- References & Acknowledgements

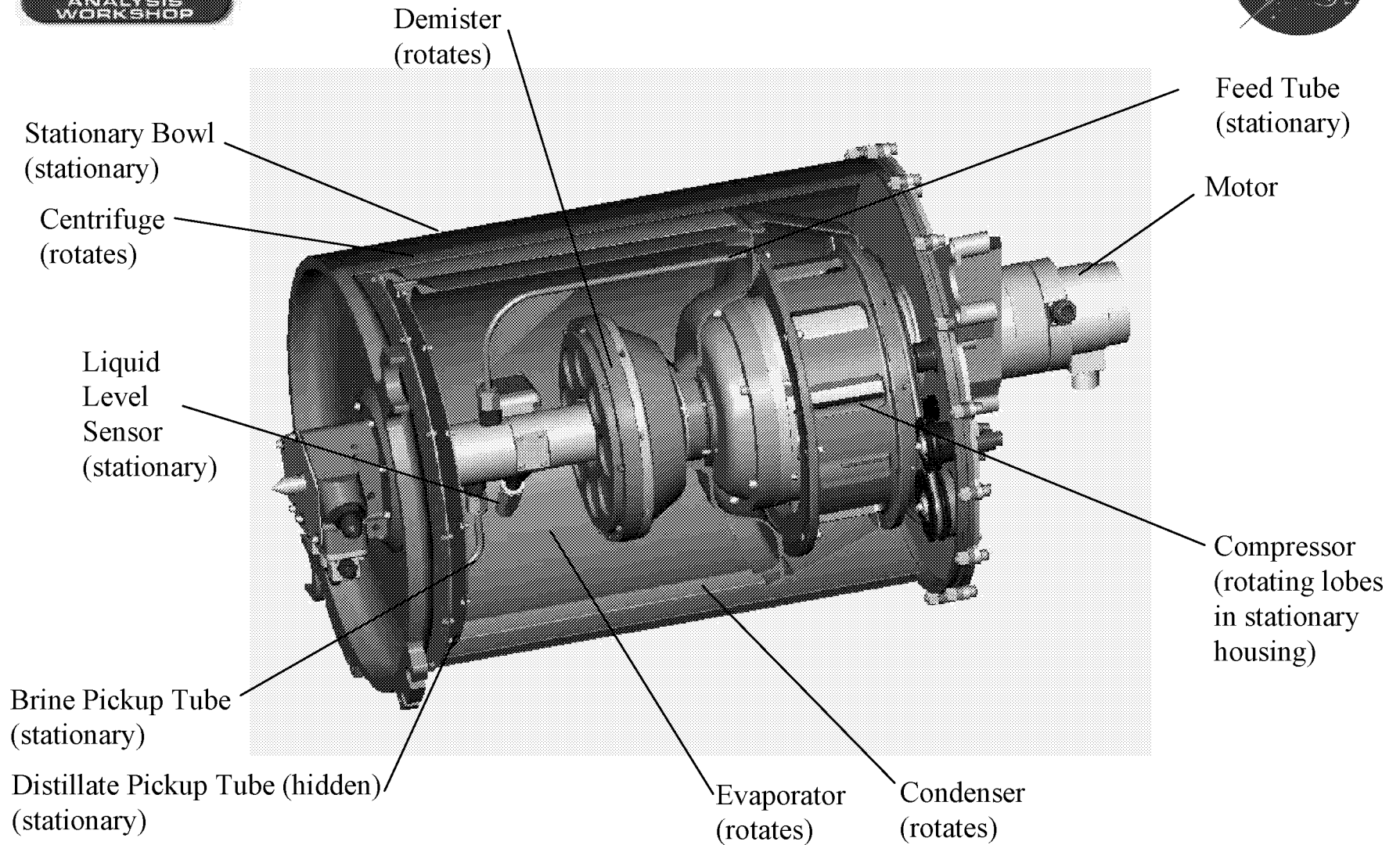
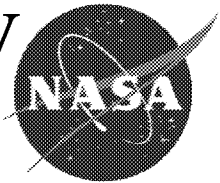


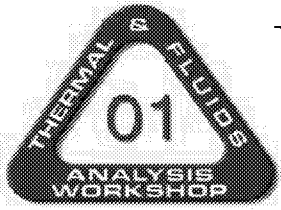
Introduction

- Pure water is distilled from waste water in International Space Station
- Distillation assembly consists of evaporator, compressor and condenser
- Vapor is periodically purged from the condenser to avoid vapor accumulation
- Purged vapor is condensed in a tube by coolant water prior to entering purge pump
- The paper presents a condensation model of purged vapor in a tube

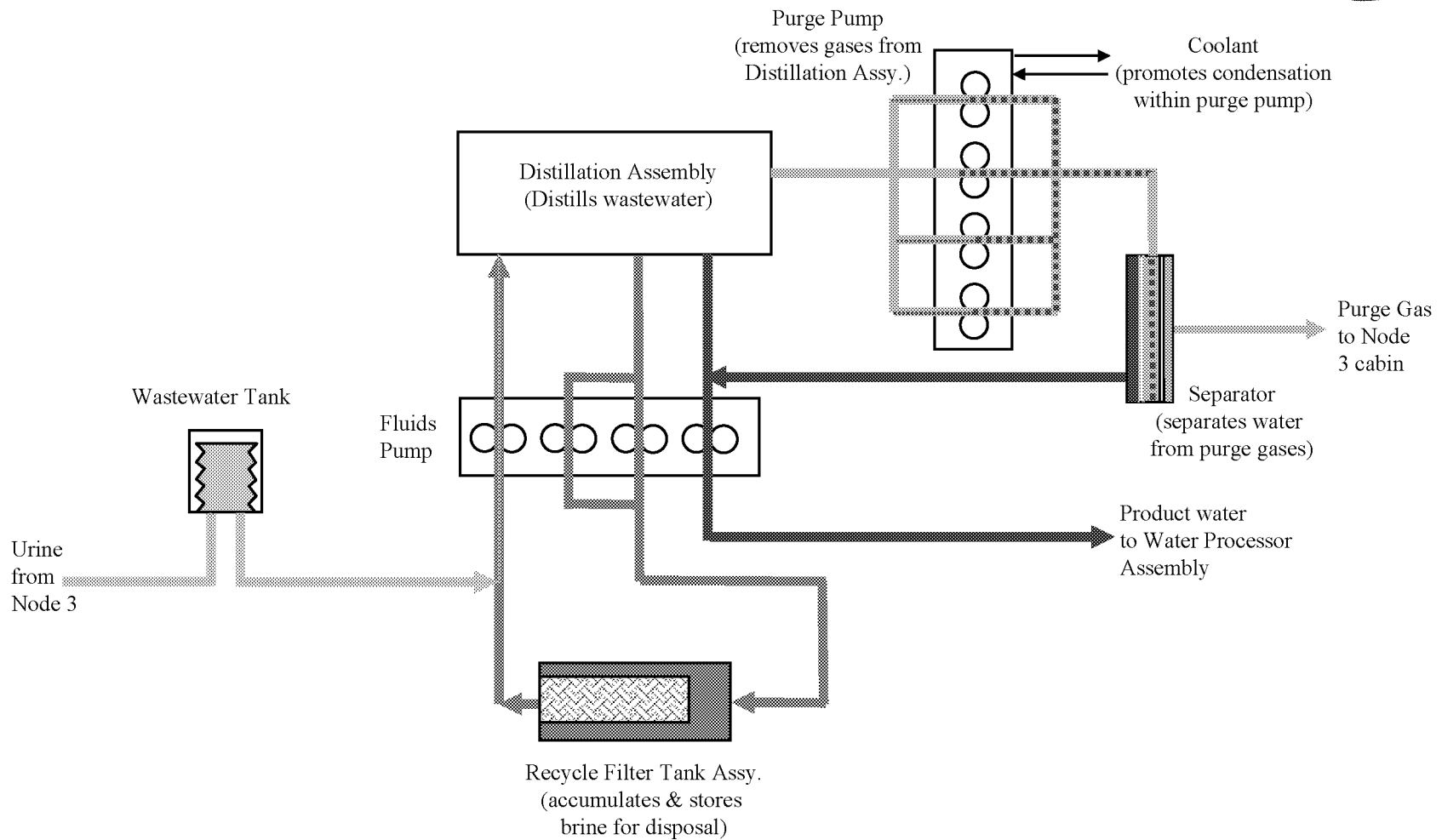
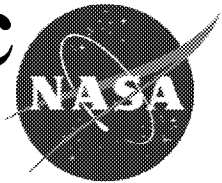


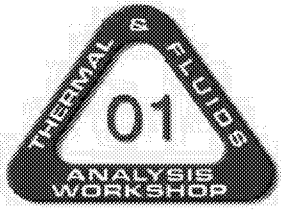
UPA Distillation Assembly



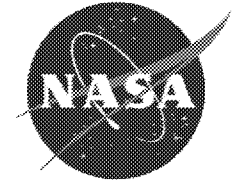


UPA Simplified Schematic

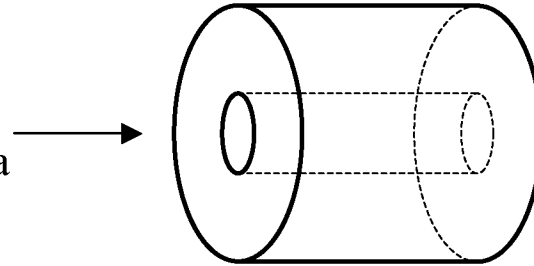




Problem Description



Superheated
Water Vapor
 $P_{\text{inlet}} = 0.95 \text{ psia}$
 $T_{\text{inlet}} = 101^\circ\text{F}$



Saturated
Water Vapor
 $P_{\text{outlet}} = 0.5 \text{ psia}$

$T_{\text{outer wall}} = 65^\circ\text{F}$

Inner Tube Diameter = 0.125 inch

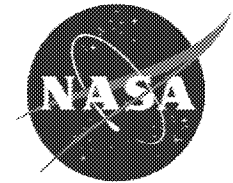
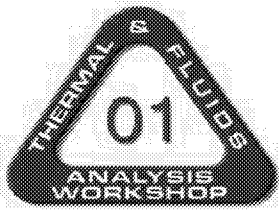
Outer Tube Diameter = 1 inch

Length = 4 inches

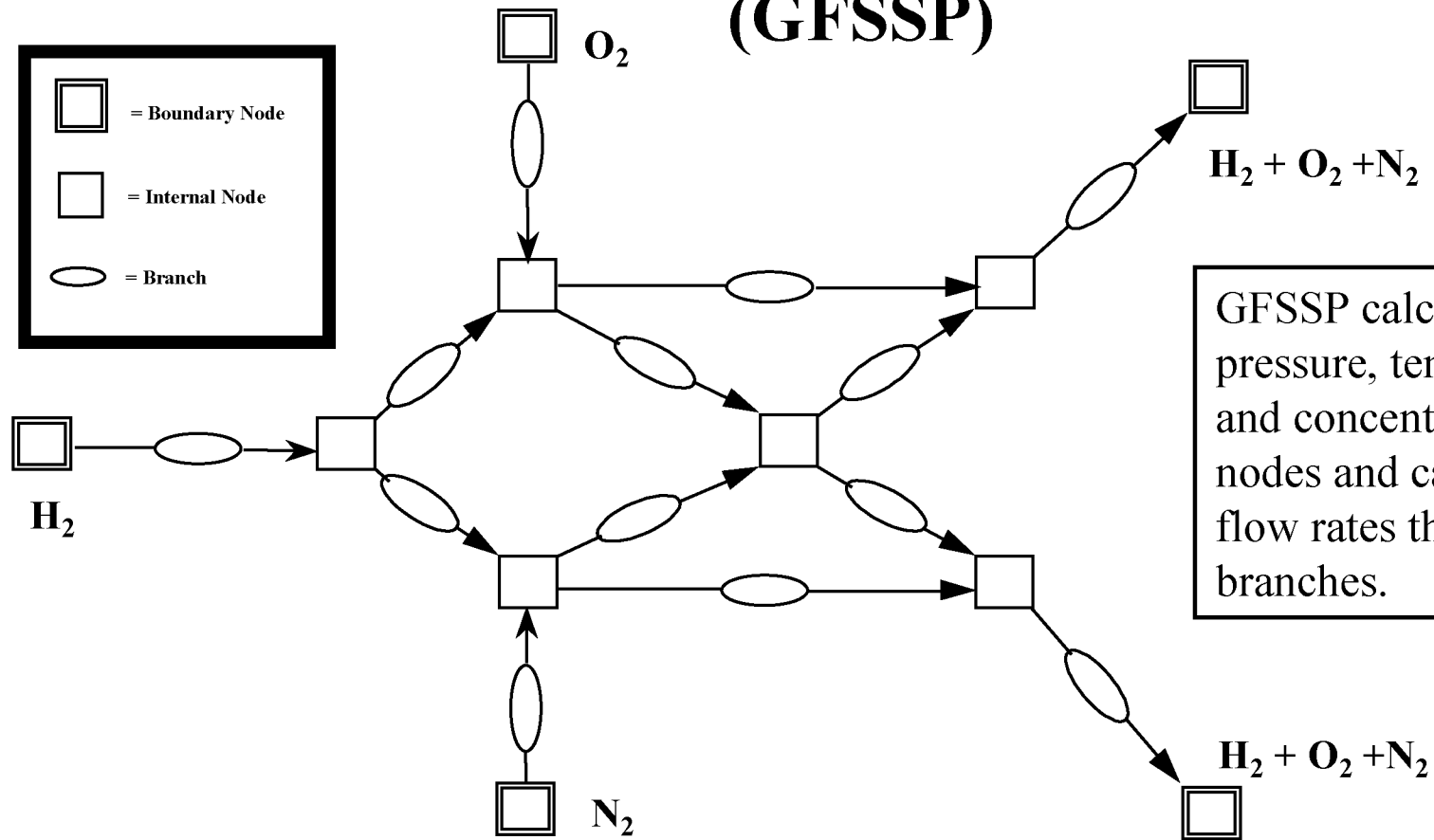
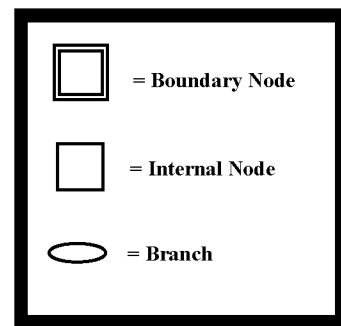
Material is Titanium

Calculate the Quality and Heat Transfer Properties
of the Water as it Condenses in the Pipe

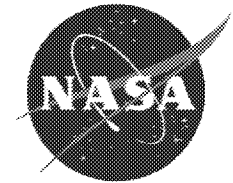
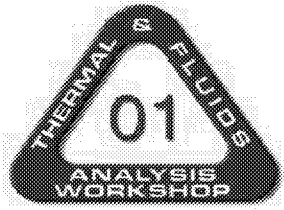
Model consists of 2 Boundary Nodes and 28 Internal Nodes
and Models Conduction through the Tube Wall



Generalized Fluid System Simulation Program (GFSSP)



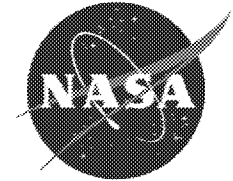
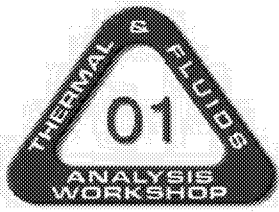
GFSSP calculates pressure, temperature, and concentrations at nodes and calculates flow rates through branches.



GFSSP

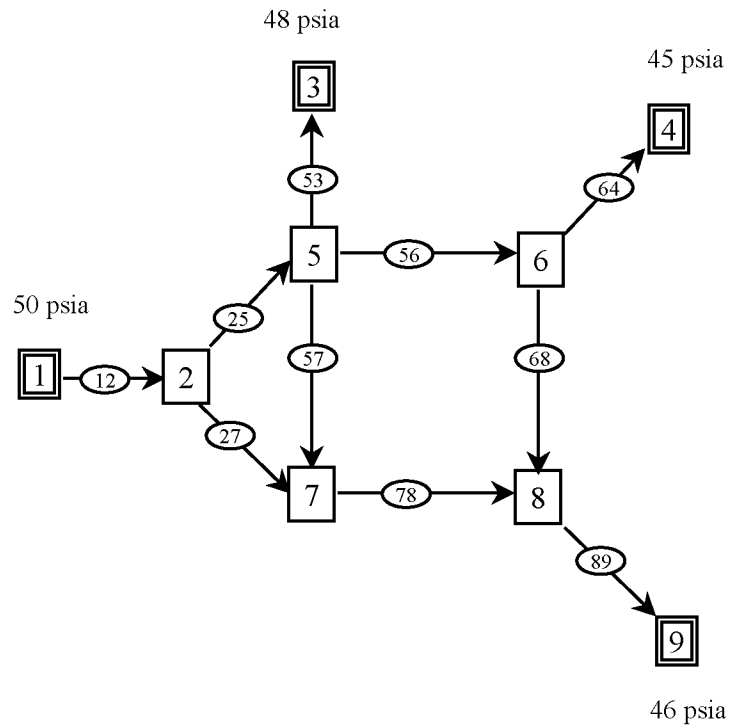
Finite Volume Method

- Finite Volume Method is based on conservation principle of Thermo-Fluid Dynamics
- In Classical Thermodynamics we analyze a single control volume
- In Finite Volume Method, flow domain is discretized into multiple control volumes and a simultaneous analysis is performed
- Finite Volume Method can be classified into two categories:
 - Navier-Stokes Solution (Commonly known as CFD)
 - Network Flow Solution (NFS)

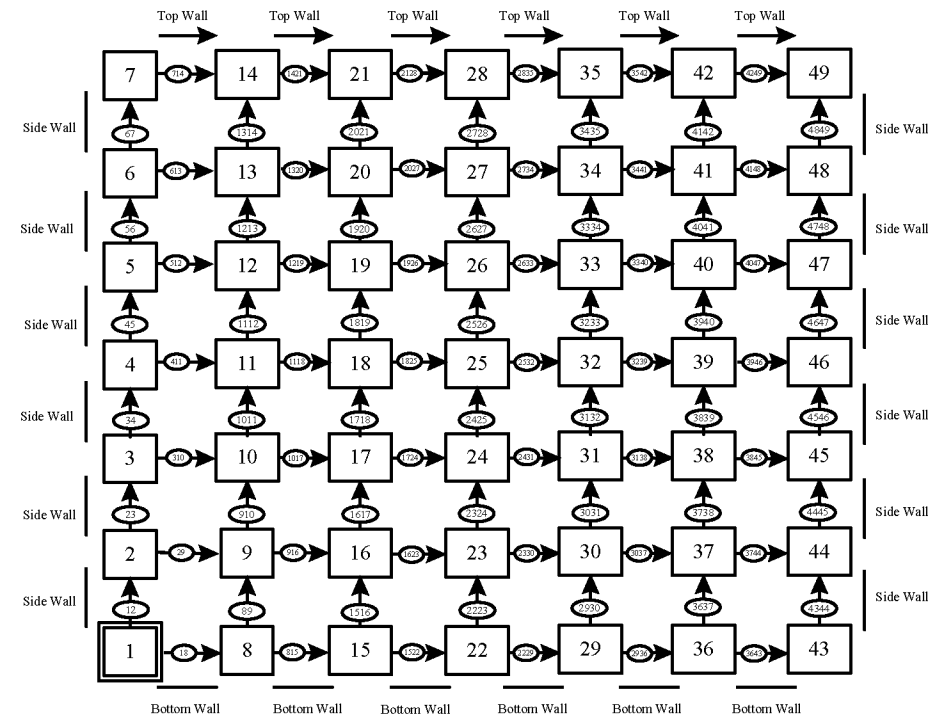


GFSSP

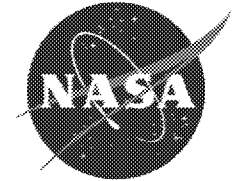
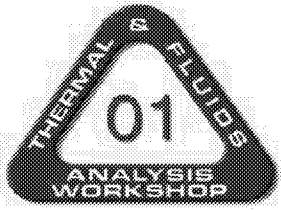
Finite Volume Method



Network Flow Solution (NFS)



Navier-Stokes Solution (CFD)



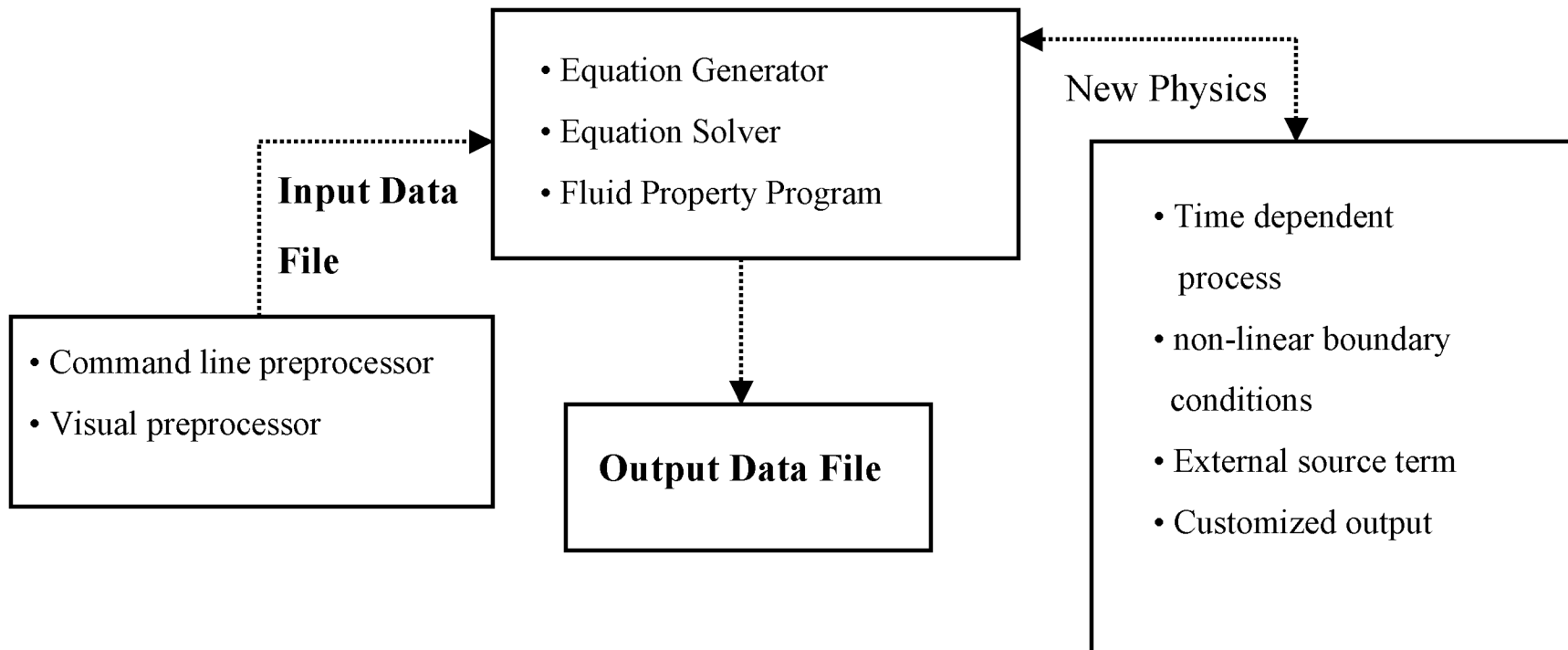
GFSSP Process Flow Diagram

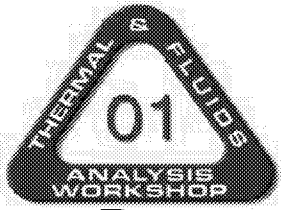
Solver & Property

Preprocessor

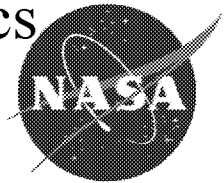
Module

User Subroutines





Coupling of Thermodynamics & Fluid Dynamics



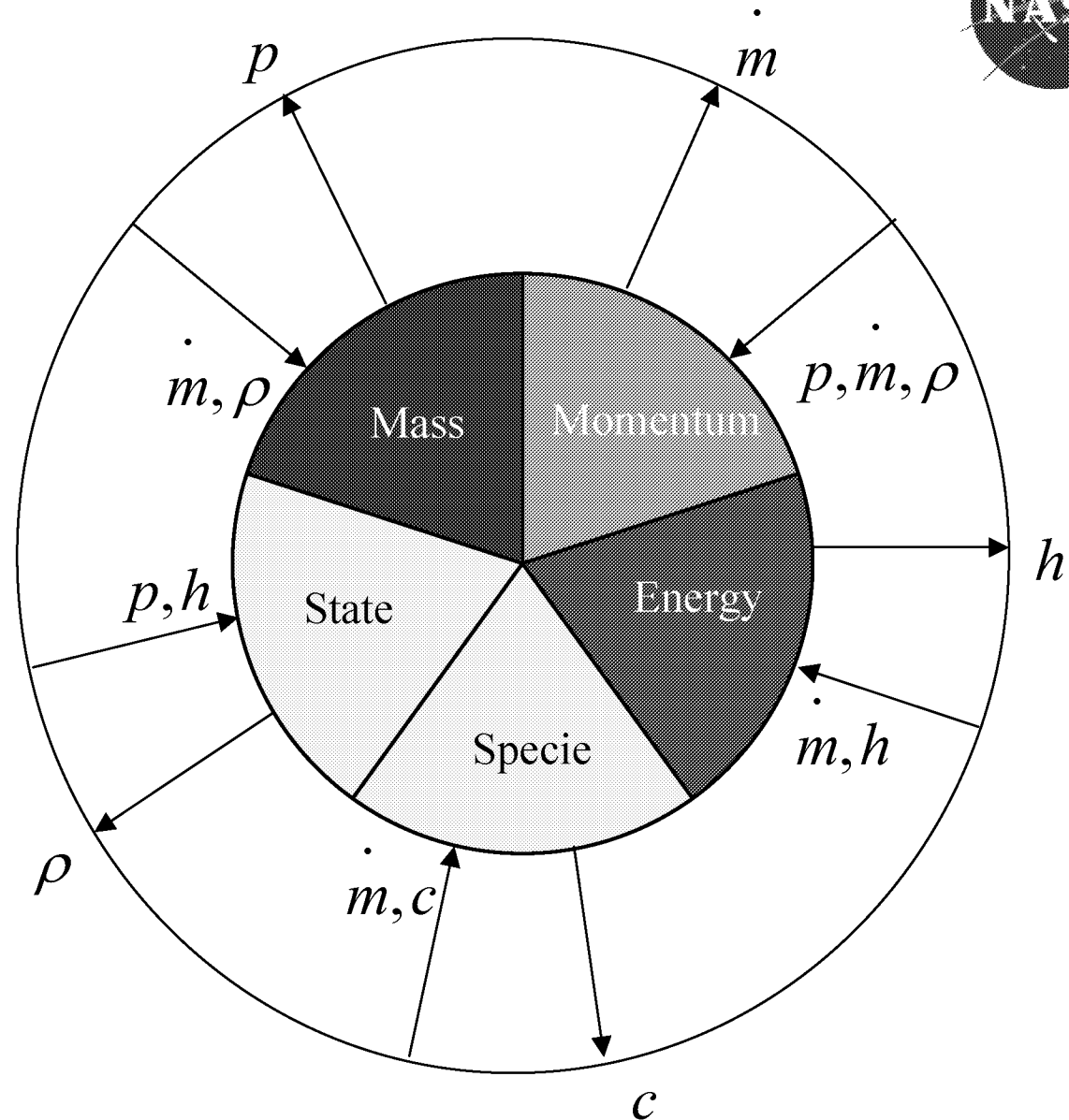
p - Pressure

\dot{m} - Flowrate

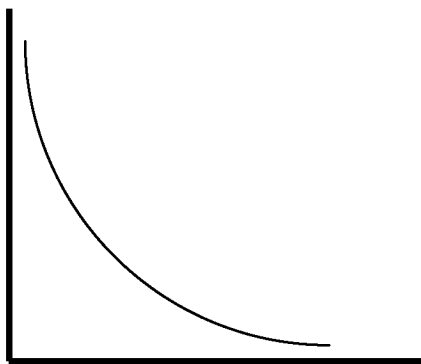
h - Enthalpy

c - Concentration

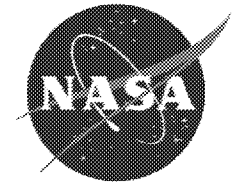
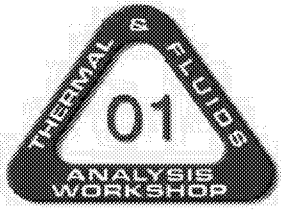
ρ - Density



Error



Iteration Cycle

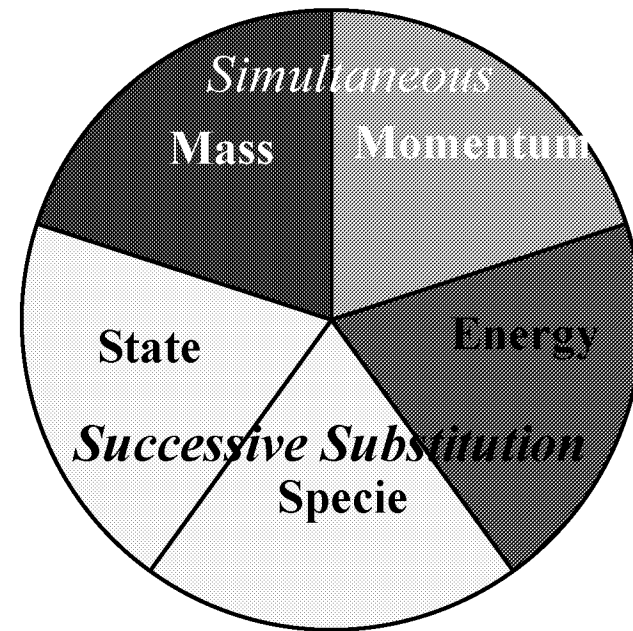


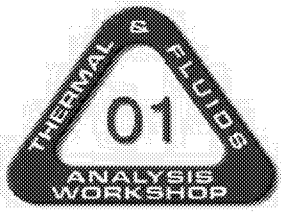
GFSSP Solution Scheme

SASS : Simultaneous Adjustment
with Successive Substitution

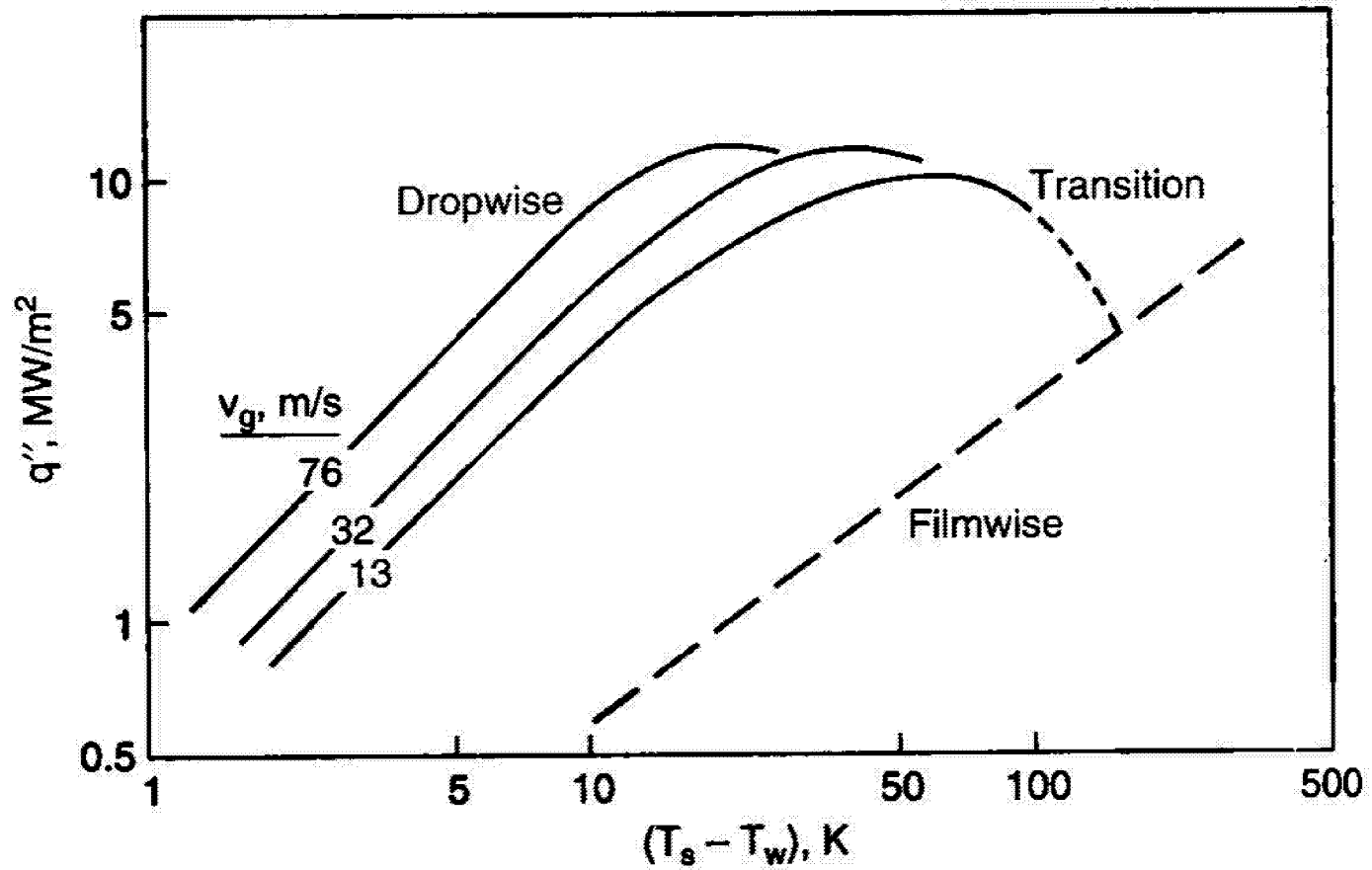
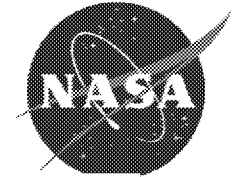
Approach : Solve simultaneously
when equations are strongly
coupled and non-linear

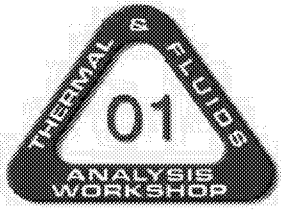
Advantage : Superior
convergence characteristics with
affordable computer memory



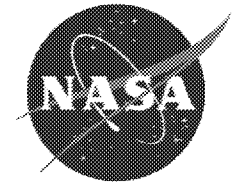


Condensation Heat Transfer





Heat transfer correlations



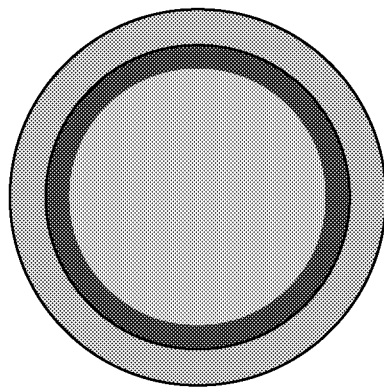
Akers, et al, 1959 – Annular Correlation

Boyko and Kruzhulin, 1967 – Annular Correlation

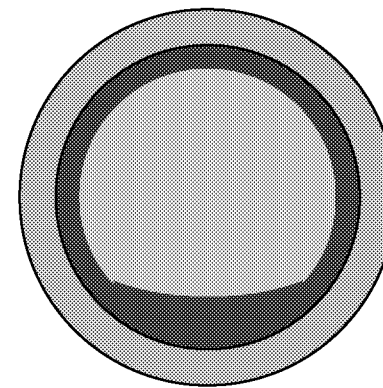
Chato, 1962 – Stratified Correlation

Soliman, et al, 1968 – Generalized Correlation

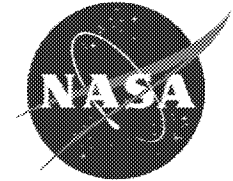
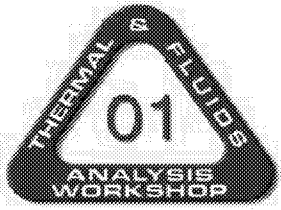
Chose Soliman correlation for its stability and generality



Annular Condensation



Stratified Condensation



Soliman Correlation for Heat Transfer Coefficient for Annular Flow Condensation

$$h = 0.036 \text{Pr}^{0.65} F_0^{0.5} \left[\frac{k_l \rho_l^{0.5}}{\mu_l} \right]$$

$$F_0 = F_f + F_m \pm F_a$$

$$F_f = 0.045 \text{Re}_T^{-0.2} \left[\frac{\pi^2 \rho_v D^4}{8W_T^2} \right] \left[x^{1.8} + 5.70 \left(\frac{\mu_l}{\mu_v} \right)^{0.0523} (1-x)^{0.470} x^{1.33} \left(\frac{\rho_v}{\rho_l} \right)^{0.261} + 8.11 \left(\frac{\mu_l}{\mu_v} \right)^{0.105} (1-x)^{0.940} x^{0.860} \left(\frac{\rho_v}{\rho_l} \right)^{0.522} \right]$$

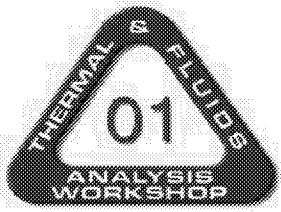
$$F_m = 0.5 \left(D \frac{dx}{dz} \right) \left[\frac{\pi^2 \rho_v D^4}{8W_T^2} \right] \left[2(1-x) \left(\frac{\rho_v}{\rho_l} \right)^{2/3} + \left(\frac{1}{x} - 3 + 2x \right) \left(\frac{\rho_v}{\rho_l} \right)^{4/3} + (2x - 1 + \beta x) \left(\frac{\rho_v}{\rho_l} \right)^{1/3} + \left(2\beta - \frac{\beta}{x} - \beta x \right) \left(\frac{\rho_v}{\rho_l} \right)^{5/3} + 2(1-x-\beta+\beta x) \left(\frac{\rho_v}{\rho_l} \right) \right]$$

$$F_a = 0$$

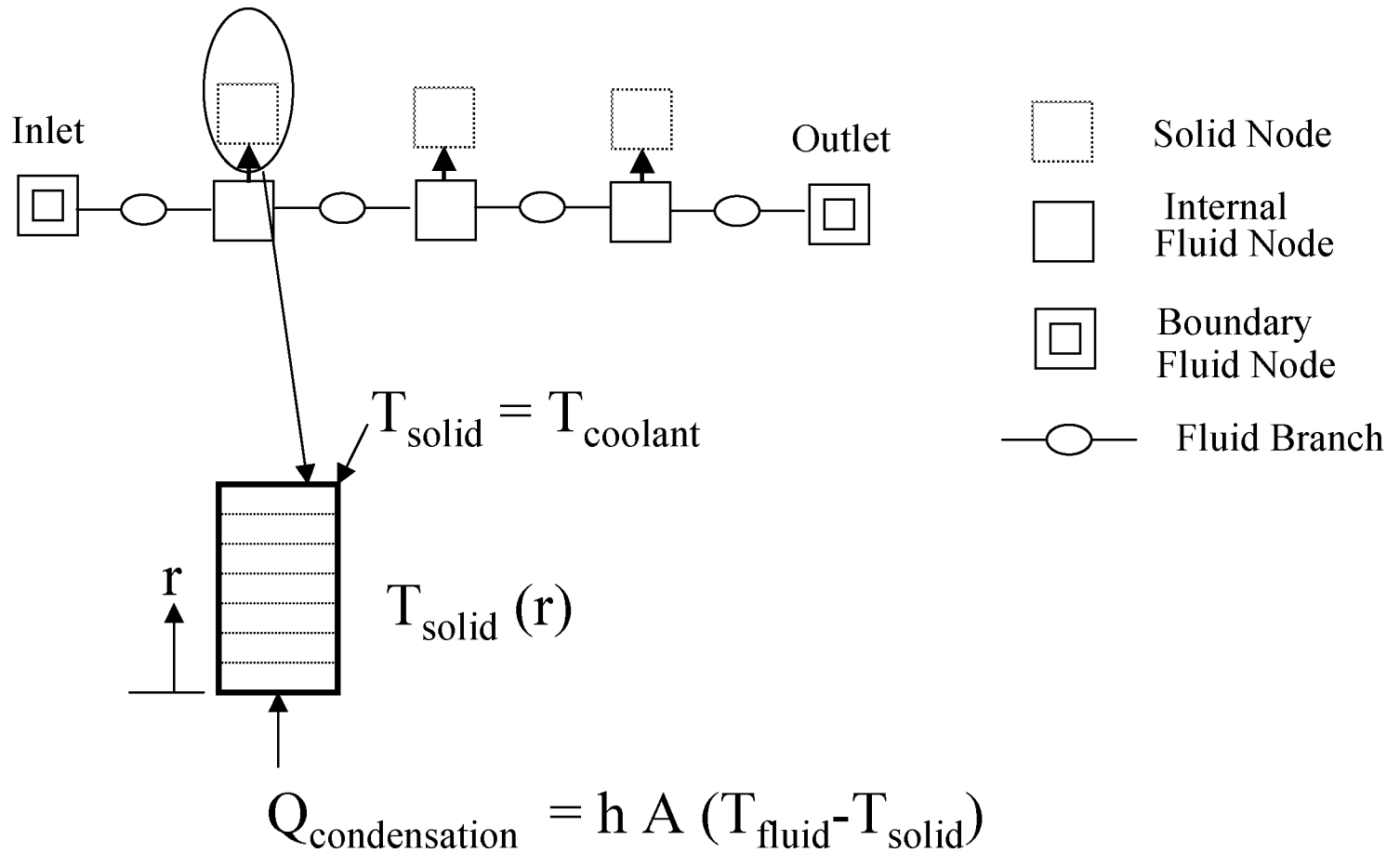
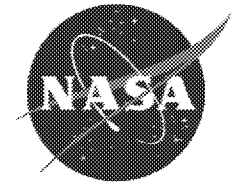
F_f : Effect of two-phase friction

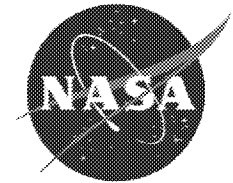
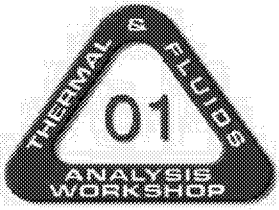
F_m : Effect of momentum changes in the flow

F_a : Effect of axial gravitational field on the wall shear stress

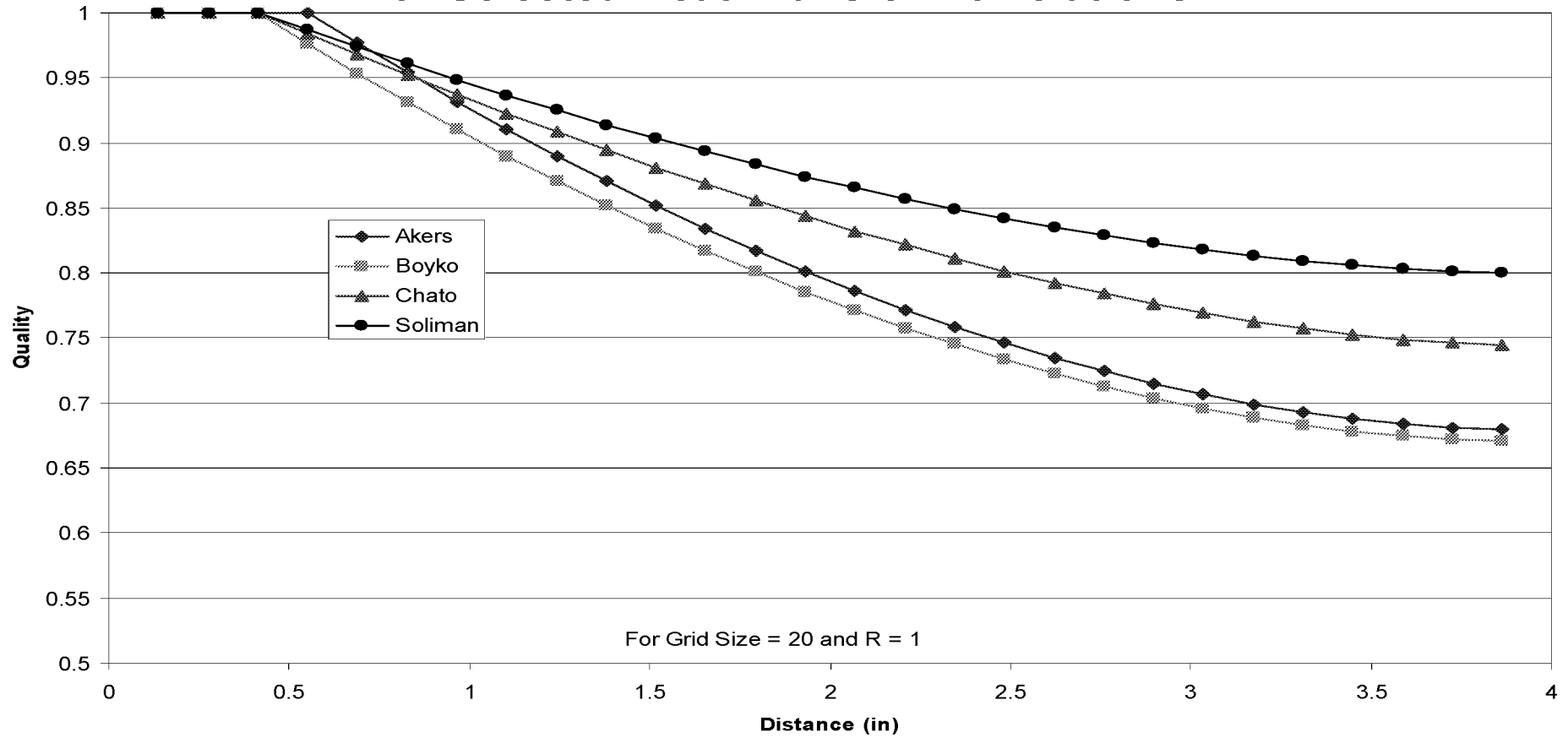


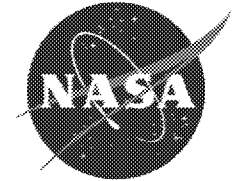
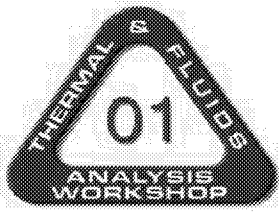
Solid-to-fluid heat transfer



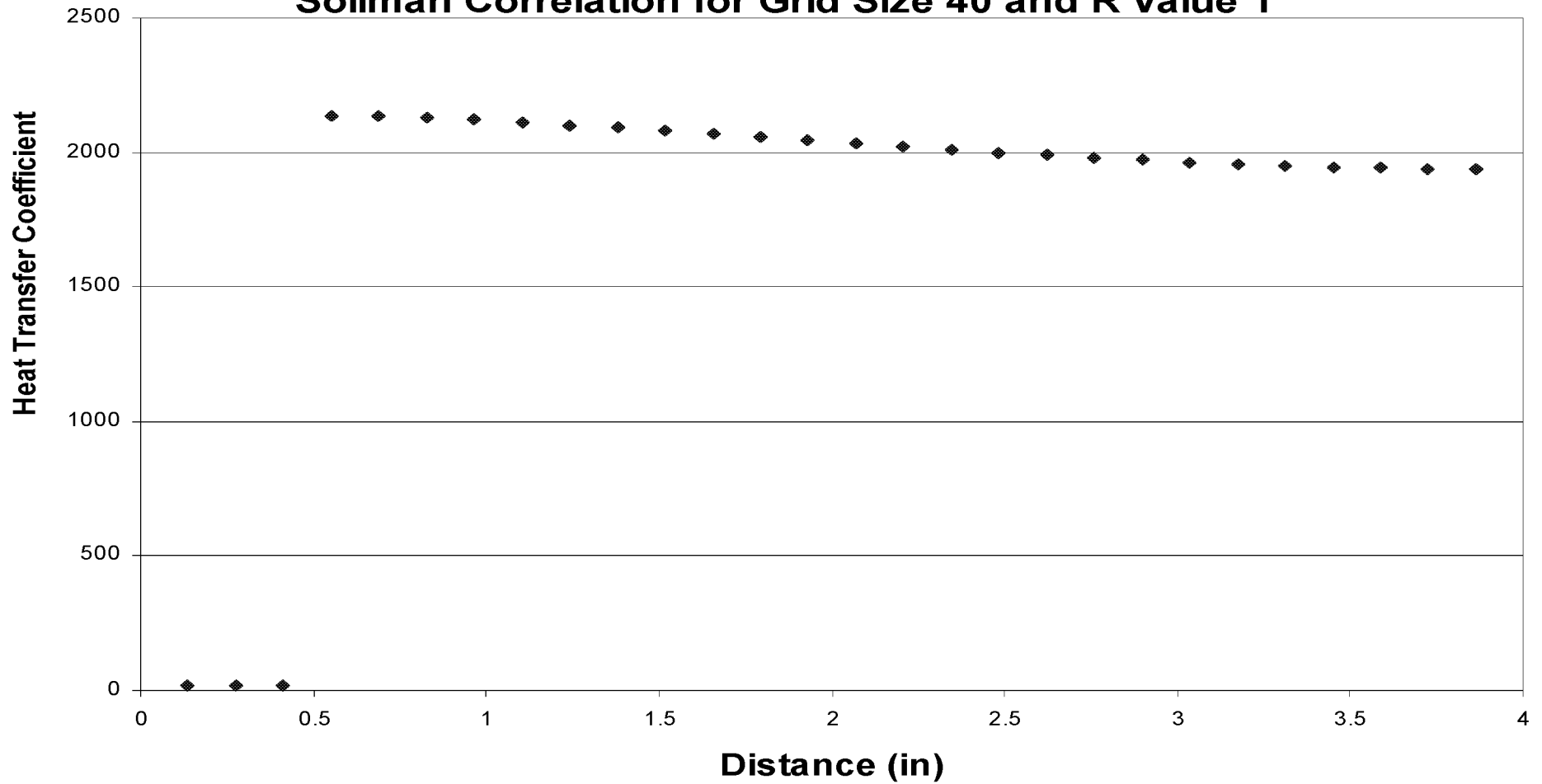


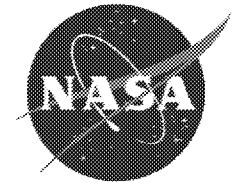
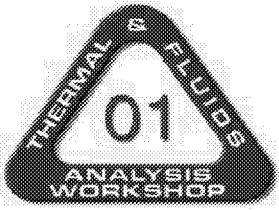
Plot of Quality vs. Pipe Location for Selected Heat Transfer Correlations



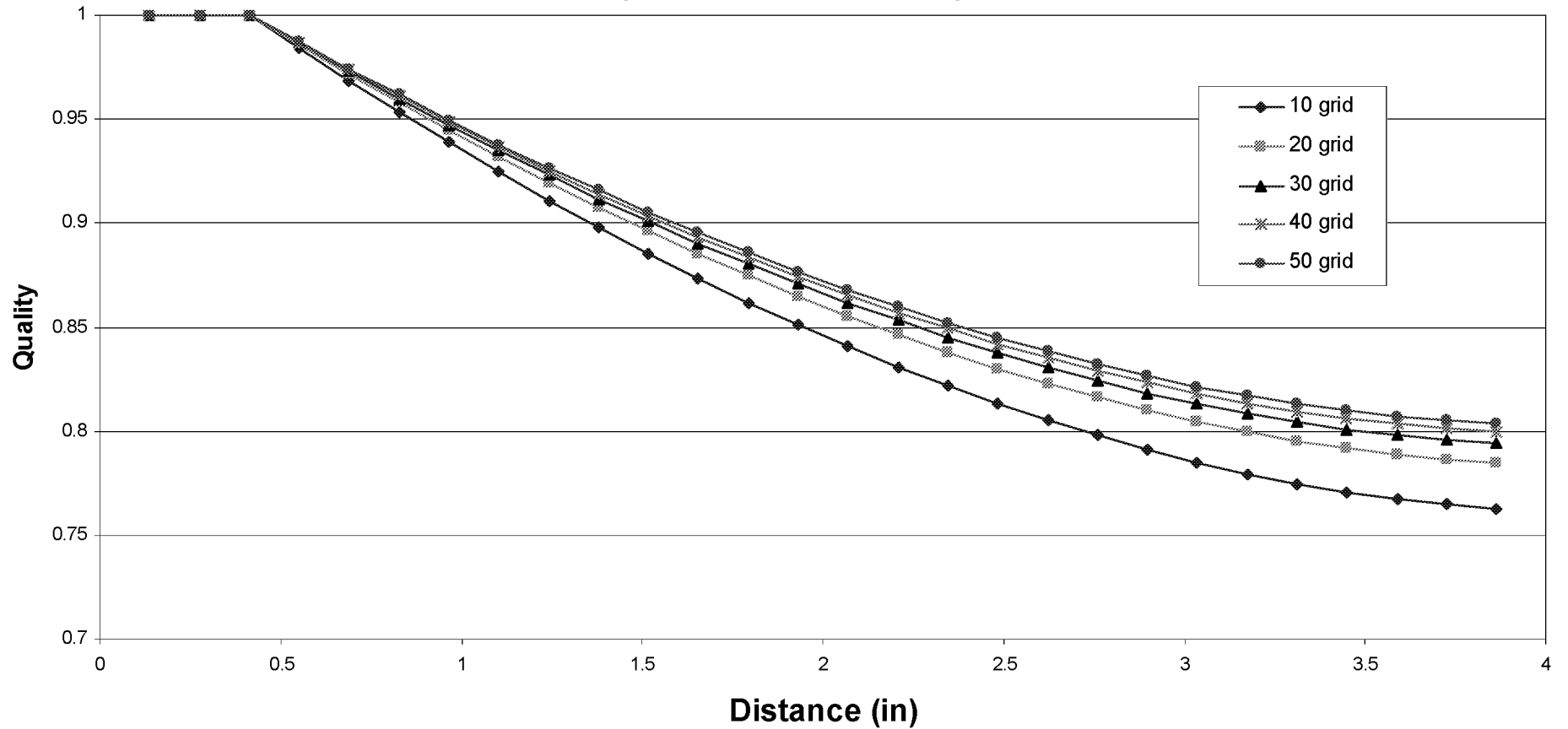


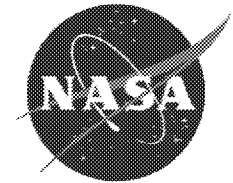
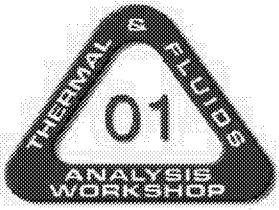
Heat Transfer Coefficient vs. Pipe Location Soliman Correlation for Grid Size 40 and R Value 1



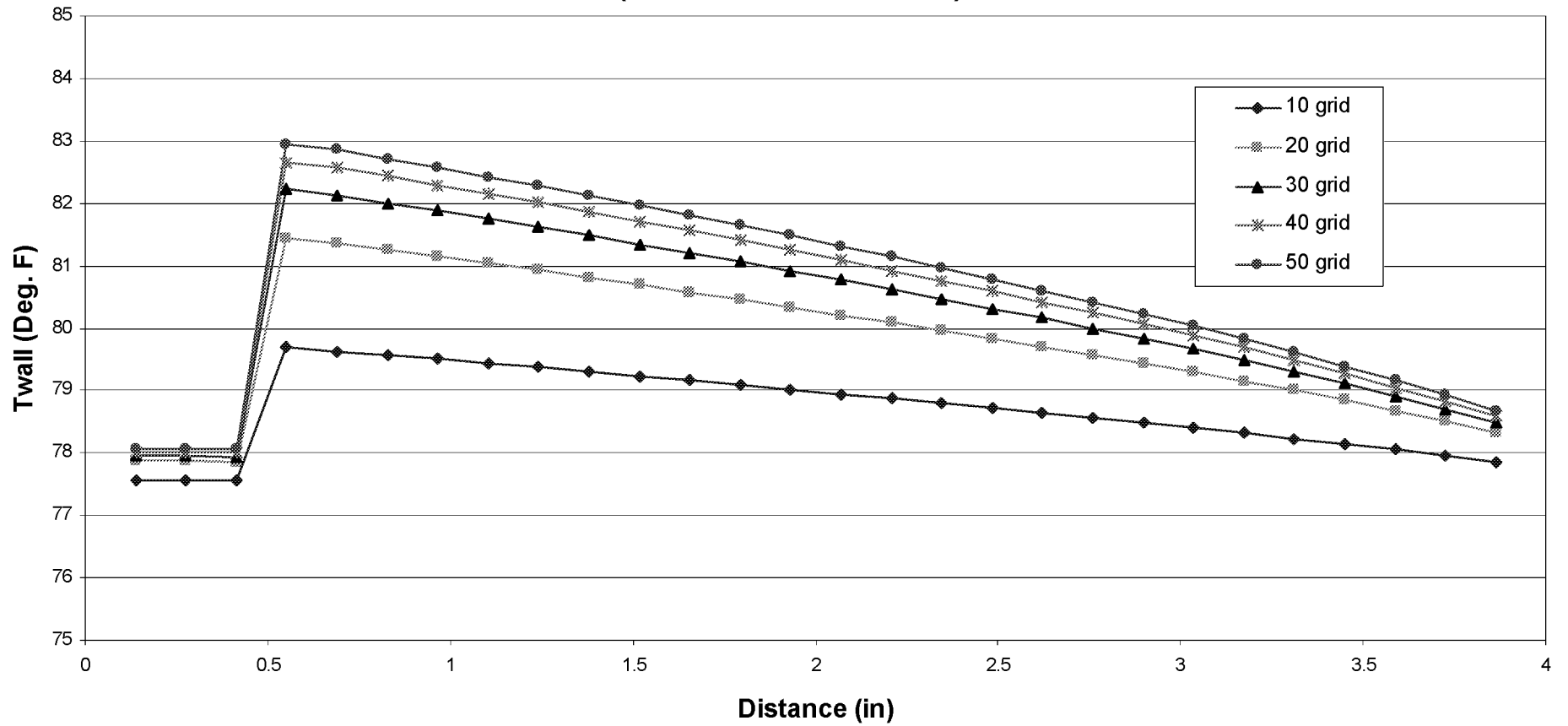


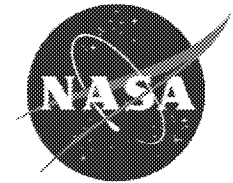
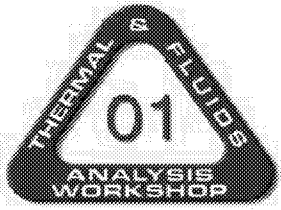
Quality Comparison for Different Tube Grid Resolution (Soliman Correlation)





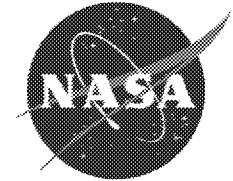
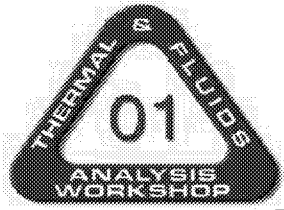
Outer Wall Temperature Comparison for Different Tube Grid Resolution (Soliman Correlation)





Conclusions

- A condensation heat transfer model was successfully incorporated in a general purpose flow network code
- The numerical model considers solid-to-fluid heat transfer
- Soliman et al's correlation of condensation heat transfer is recommended due to its generality and stability



References & Acknowledgements

References:

1. Don Holder, “Urine Processor Assembly Condensate Issue”, NASA/Marshall Space Flight Center, Environmental Control and Life Support System Group, August 31, 2001, Huntsville, Alabama.
1. Rohsenow, W. M., Hartnett, J. P. and Cho, Y. I., “Handbook of Heat Transfer” 3rd Edition, McGraw Hill, 1998
2. Soliman, M., Schuster, J. R. and Berenson, P. J., “A General Heat Transfer Correlation for Annular Flow Condensation”, Journal of Heat Transfer, ASME, May, 1968.
3. Majumdar, A. “Generalized Fluid System Simulation Program (GFSSP) Version 3.0” Sverdrup Technology Report No. MG-99-290, November, 1999.

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