



# Effect of Surface Impulsive Thermal Loads on Fatigue Behavior of Constant Volume Propulsion Engine Combustor Materials

Dongming Zhu

U.S. Army Research Laboratory, Glenn Research Center, Cleveland, Ohio

Dennis S. Fox and Robert A. Miller

Glenn Research Center, Cleveland, Ohio

Louis J. Ghosn and Sreeramesh Kalluri

Ohio Aerospace Institute, Brook Park, Ohio

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Dongming Zhu  
U.S. Army Research Laboratory  
Glenn Research Center  
Cleveland, Ohio 44135

Dennis S. Fox and Robert A. Miller  
National Aeronautics and Space Administration  
Glenn Research Center  
Cleveland, Ohio 44135

Louis J. Ghosn and Sreeramesh Kalluri  
Ohio Aerospace Institute  
Brook Park, Ohio 44142

## **Summary**

The development of advanced high performance constant-volume-combustion-cycle engines (CVCCE) requires robust design of the engine components that are capable of enduring harsh combustion environments under high frequency thermal and mechanical fatigue conditions. In this study, a simulated engine test rig has been established to evaluate thermal fatigue behavior of a candidate engine combustor material, Haynes 188, under superimposed CO<sub>2</sub> laser surface impulsive thermal loads (30 to 100 Hz) in conjunction of the mechanical fatigue loads (10 Hz). The mechanical high cycle fatigue (HCF) testing of some laser pre-exposed specimens has also been conducted under a frequency of 100 Hz to determine the laser surface damage effect. The test results have indicated that material surface oxidation and creep-enhanced fatigue is an important mechanism for the surface crack initiation and propagation under the simulated CVCCE engine conditions.

## **Introduction**

Constant-volume-combustion-cycle engines (CVCCE) based on the pulsed detonation engine (PDE) concept have received increasing attention for future aerospace propulsion applications. Because the CVCCE is designed for a high frequency, intermittent detonation combustion process, extremely high gas temperature and pressure can be realized under the nearly constant-volume combustion environment. The CVCCEs can potentially achieve higher thermodynamic cycle efficiency and thrust density as compared to traditional constant-pressure combustion gas turbine engines [1]. However, the development of these engines requires robust design of the engine components that are capable of enduring harsh detonation environments. In particular, the detonation combustor chamber, which is designed to sustain and confine the detonation combustion process, will experience high pressure and temperature pulses with a very short duration [2,3]. Therefore, it is of great importance to evaluate engine combustor materials and components under simulated engine temperature and stress conditions in the laboratory. In this paper, a laser impulsive thermal and thermomechanical fatigue testing approach for evaluating materials to be used in CVCCE combustor applications is described. The failure mechanisms of a cobalt-base Haynes 188 combustor material under the simulated engine conditions are also presented.

## Experimental

A high cycle thermal fatigue test rig for evaluating CVCCE combustor materials has been established using a 1.5 kW CO<sub>2</sub> enhanced pulsed laser [4]. A diagram showing the three laser rig testing approaches employed is shown in fig. 1. The high power laser, when operating in the pulsed mode, can be controlled at various pulse energy levels and waveform distributions. The enhanced laser pulses can be used to mimic the time-dependent temperature and pressure waves encountered in a pulsed detonation engine. Under the enhanced laser pulse condition, a maximum 7.5 kW peak power with duration of approximately 0.1 to 0.2 ms (a spike) can be achieved, followed by a plateau region that has about 1/5 of the maximum power level with several ms duration. The laser thermal fatigue rig has also been developed to adopt flat and rotating tubular specimen configurations for the simulated engine tests [4]. More sophisticated laser optic systems can be used to simulate the spatial distributions of the temperature and shock waves in the engine.

In this study, the pulse laser thermal high cycle fatigue (HCF) behavior has been investigated for the cobalt-base superalloy Haynes 188 specimens (dimension 50 by 50 by 1.0 mm, with mechanically polished surfaces), under the test condition of 30 Hz cycle frequency [4]. In this laser thermal fatigue test, a Gaussian laser beam (with a radius of 16 mm and the above mentioned pulse characteristics) was used to provide the specimen heating and room temperature air was used for specimen backside cooling. Specimen temperatures were measured by two-color pyrometers. The specimens were tested under the high frequency laser pulses at an average surface temperature of 800 °C and the back temperature of 650 °C. Besides the laser thermal high cycle fatigue (HCF) testing, the specimens were also thermally cycled between the test temperatures and room temperature using 30 min hot cycles with 3 min cooling (low cycle fatigue or LCF).

In order to investigate the combustor cooling hole effect on the fatigue behavior of the candidate material, a combined thermal and mechanical four-point-bend test was also performed under the superimposed laser thermal HCF loads (100 Hz) in conjunction with the mechanical fatigue bending loads (10 Hz). The dimension of the bend test specimens used was 19 by 10 by 1.2 mm, with the cooling hole diameter being 0.38 and 0.76 mm, respectively. The specimen hole arrangement is shown in fig. 2. The specimens were mechanically polished and then tested under the high frequency laser pulses at the average surface temperature of 650 °C and the back temperature of 500 °C. The specimens were also thermally cycled between the test temperatures and room temperature using 30 min hot cycles with 3 min cooling.

The mechanical high cycle fatigue testing was also conducted for laser pulse treated tensile fatigue specimens under a frequency of 100 Hz (mechanical) at 816 °C. The tensile fatigue specimens were mechanically polished so that the final polishing marks were in the longitudinal direction of the specimens to minimized surface roughness effect on the HCF behavior. The tensile fatigue specimens were all subjected to the laser thermal HCF pre-treatment at a surface average temperature ranging from 816 to 1010 °C at 100Hz, with the laser 30 min cycle thermal LCF test conditions. The sequential laser and mechanical HCF tests were used to investigate the prior laser HCF surface damage effect on the subsequent HCF strength of the candidate material Haynes 188 alloy.

The laser induced impulsive temperature profiles, stress distributions and creep response in the test specimens are modeled using finite difference to help understand the thermal fatigue behavior of the materials system under the laser-enhanced HCF and LCF test conditions. The material failure mechanisms under the laser simulated CVCCE conditions are also presented in this paper.

## Experimental Results and Discussion

Figure 3 shows the typical temperature response and distributions calculated using one-dimensional finite difference models for the Haynes 188 alloy specimen under the enhanced laser pulse thermal

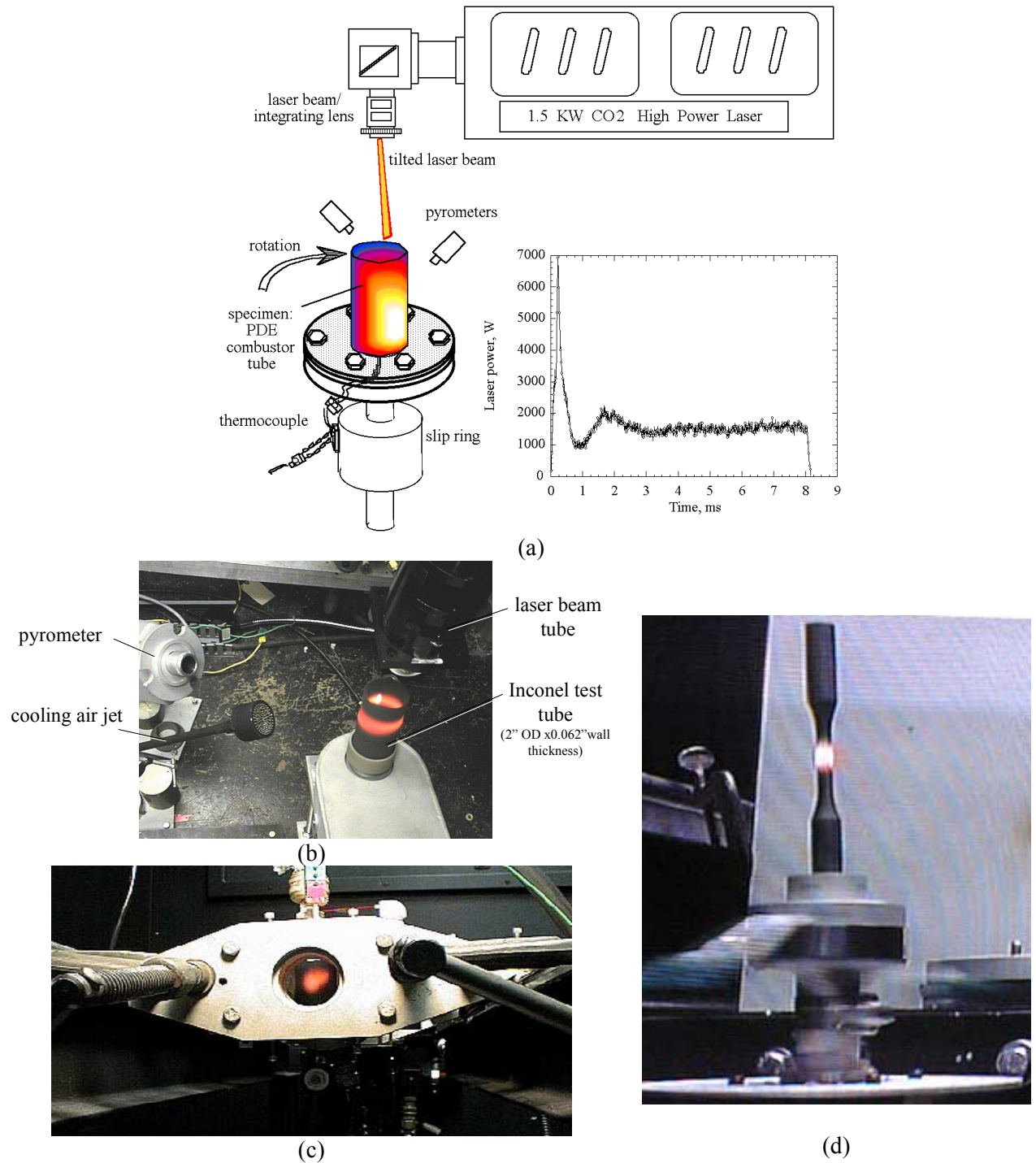


Figure 1.—A high power CO<sub>2</sub> laser rig developed for testing CVCCE combustor materials and components under the simulated engine temperature and stress conditions. (a) Schematic diagram showing a laser test rig, and the measured laser pulse waveform from the pulse signal of a 1.5KW CO<sub>2</sub> laser under the enhanced pulse mode using an oscilloscope. The laser pulse width is 8 ms, and a maximum laser power 7.5KW can be achieved over about 0.2 ms duration at the pulse enhancement mode; (b) and (c) Tubular and flat specimen configurations adopted for the simulated CVCCE engine test, under thermal and/or combined (four point bend) mechanical fatigue thermal fatigue conditions; (d) Pulsed laser pre-testing of a mechanical high cycle fatigue (HCF) specimen.

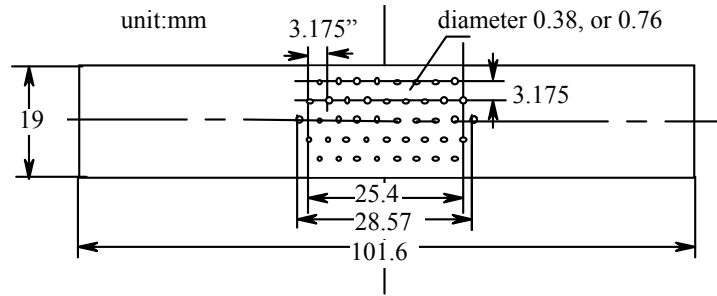


Figure 2.—Four-point-bend test specimen with center holes arrangement for the combined laser thermo-mechanical fatigue test.

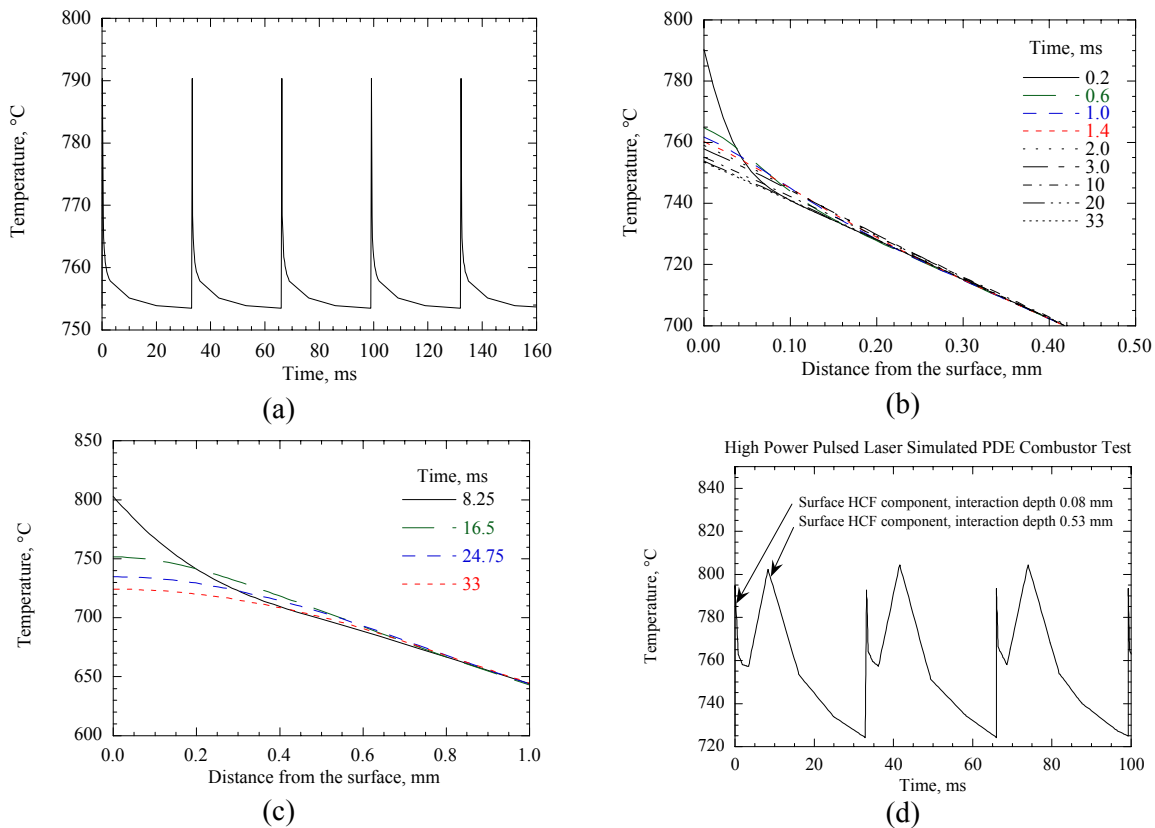


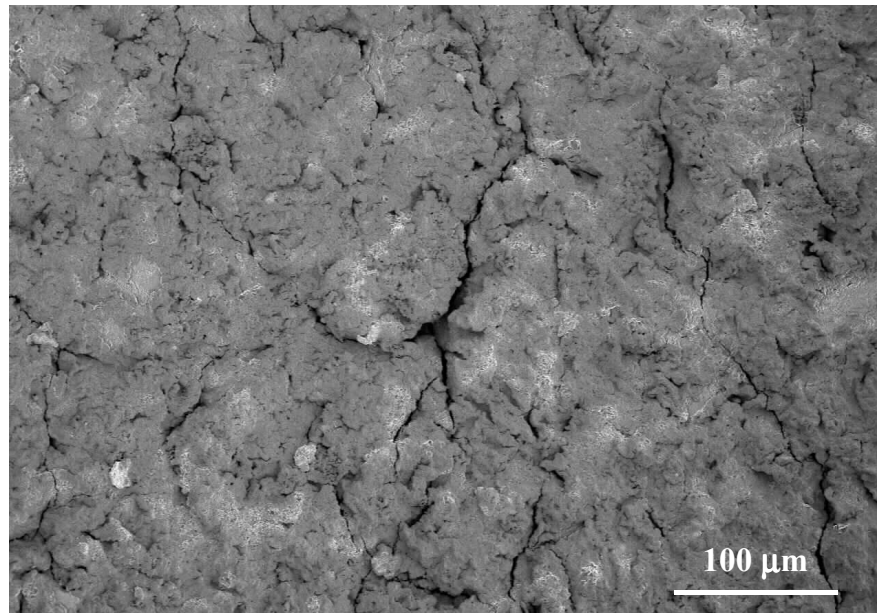
Figure 3.—One-dimensional finite difference modeling results showing the temperature swings on a Haynes 188 specimen under the 30Hz enhanced pulse condition (33 ms pulse period, 10 ms pulse width including 0.2 ms pulse spike). (a) Temperature pulses induced by the high energy laser pulse spike. (b) Temperature swings due to the enhanced, 0.2 ms laser pulse spike. (c) Temperature fluctuations due to the regular 10 ms laser pulse. (d) Superimposed temperature profiles during the enhanced pulse laser testing at the specimen surface.

fatigue test conditions. The numerical calculations show that that the enhanced 0.2 ms laser pulse spikes, which are used to simulate the CVCCE temperature and shockwave pulses, can cause a rapid cyclic temperature swing on the specimen surface, as shown in fig. 3 (a). In addition, an additional 40 °C temperature fluctuation with an interaction depth of 0.08 mm near the specimen surface region will be generated due to the enhanced 0.2 ms laser pulse spikes, as shown in the temperature distribution plot of

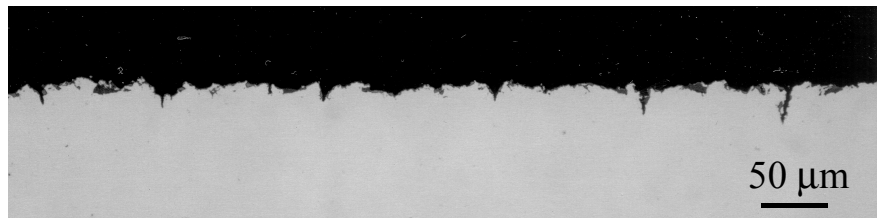


fig. 3 (b). This enhanced pulsed temperature swing will be superimposed onto the temperature swing of 80 °C that is induced by the 10 ms regular laser pulse near the 0.53 mm deep surface interaction region (fig. 3 (c) and fig. 3 (d)).

Specimen failure modes were investigated after the laser thermal high cycle fatigue testing. As shown in fig. 4, extensive surface cracking with the crack depths of approximately 30 μm was observed on the tested specimens under the enhanced laser pulses and thermal cycling. The surface crack morphologies of the specimen are further shown in fig. 5. As can be seen from fig. 5, under the oxidizing environments, oxide scales (typically Cr<sub>2</sub>O<sub>3</sub> and Ni,Cr spinel oxides) were formed on the Haynes 188 specimen surfaces. The carbide inclusions, which can initiate intergranular cracks [5], will also facilitate the fatigue crack propagation under the surface impulsive thermal loading. Significant alloy creep and fatigue, as indicated by the deformation, cracking and various length scale fatigue striations in the substrate near the oxide/alloy interfaces, were observed under the laser test conditions. The stresses originating from the large thermal gradients across the specimen, as well as the thermal expansion mismatch between the oxide scales and substrate under the laser HCF and LCF test conditions, resulted in the alloy creep deformation and later the surface cracking due to the oxidation-creep interaction under the complex cyclic stresses.



(a)



(b)

Figure 4.—Surface cracking patterns of the Haynes 188 superalloy after the 30 Hz enhanced laser pulses and thermal cycling (10.8 million 30 Hz high cycle fatigue cycles, and 200 30 min-heating-cooling cycles). (b) Cross-section of tested specimen showing surface cracking penetration into the alloy.

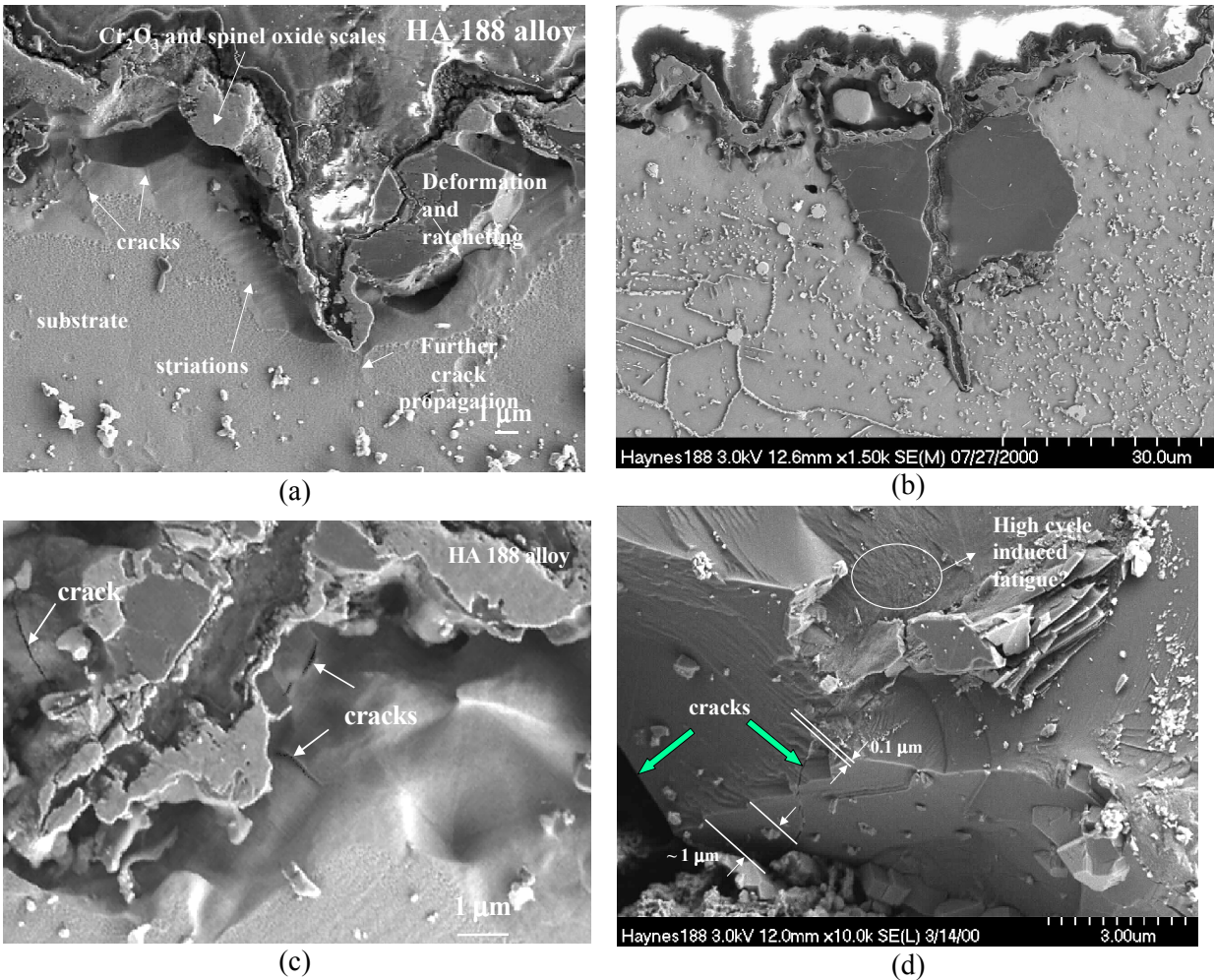


Figure 5.—Micrographs showing significant specimen oxidation, creep deformation and fatigue in the alloy substrate near the oxide scale/alloy interfaces for a Haynes 188 alloy specimen after the laser thermal cyclic testing. Oxide scale initial and further growth is detrimental to the materials fatigue resistance due to the thermal expansion mismatch stress induced creep-oxidation interactions. (a) and (b) Cross-sections of the specimen showing a surface crack penetrating into the alloy and associated oxide scale-alloy substrate fatigue striation and crack initiation. The carbides inclusions can facilitate the surface crack propagation under the surface impulsive thermal loading. (c) and (d) Microcracks and fatigue striations initiated in the alloy at the alloy/oxide interface under the surface cyclic thermal stresses.

As shown in fig. 6, the large induced creep strains, which accumulated at temperature under the thermal and stress gradients, can lead to a large tensile stress state at the surface upon cooling [4]. The specimen surface cracking can be initiated when the creep strain is high enough, and especially when the surface layer is greatly weakened by the presence of the oxidation scales, oxide and carbide inclusions, and grain boundary oxide decorations. As shown schematically in fig. 7, the cracks initiated can be further propagated under the enhanced laser thermal surface impulsive fatigue conditions because of the thermal expansion mismatch and thermal stress induced creep-oxidation interactions. The test results

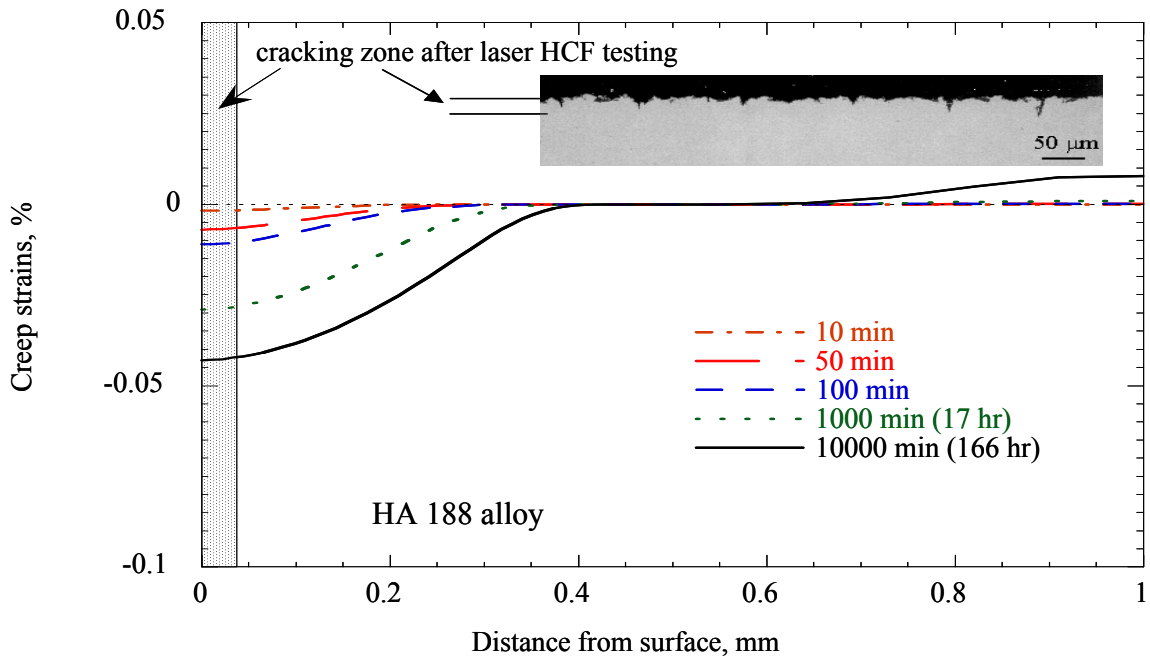


Figure 6.—Modeled creep strain distributions accumulated at temperature as a function of time under the laser thermal gradient testing. Also shown is the surface cracking morphology after the laser testing. Large compressive creep strains will occur at the specimen surface, which can lead to a large tensile stress state upon cooling. The specimen surface cracking can be initiated under high creep strains combined with the surface weakening due to oxidation.

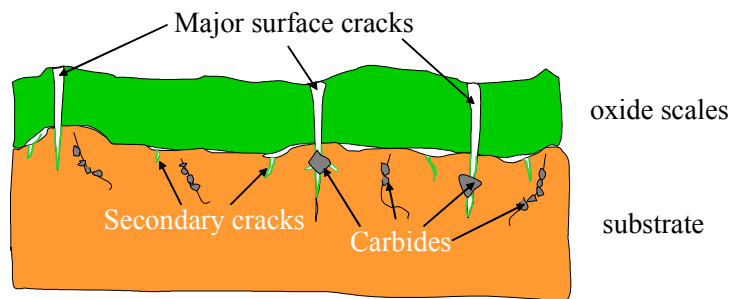


Figure 7.—Surface temperature swings can result in significant thermal cyclic stresses originating not only from the temperature gradient, but also from the CTE mismatch between thermally grown oxide scales and the substrate. The oxidation and creep of the substrate promotes surface crack initiation and propagation under the laser simulated CVCCE thermal HCF and LCF testing.

suggest that oxidation and creep enhanced fatigue can be an important mechanism for materials surface crack initiation and propagation under the simulated impulsive thermal cyclic conditions.

Figure 8 shows the experimental results from the combined laser and four-point-bend thermo-mechanical fatigue tests for the Haynes 188 material. It can be seen that the enhanced fatigue interactions and thus reduced fatigue strength were observed for the material under the laser thermal pulse as compared to traditional mechanical HCF tests. The specimens with the larger sized cooling holes (diameter 0.76 mm also showed somewhat lower fatigue strengths as compared to those with smaller sized cooling holes. The superimposed laser surface impulsive fatigue testing showed a substantially increased fatigue crack initiation and later accelerated fatigue crack propagation due to the complex oxidation, creep and fatigue interactions.

The surface HCF damage also resulted in reductions in the fatigue life of the material under the subsequent mechanical high cycle fatigue tests (100 Hz at 816 °C). As shown in fig. 9 (a), it can be seen that the material fatigue strength was reduced by 10 to 12 percent for the specimens that were subjected to the initial laser pulse testing at the various temperatures and times, as compared to that for the as-machined specimens. Figure 9 (b) shows that the fatigue strength reductions are closely related to the surface temperature and exposure time of the pulsed laser treatment. The higher surface temperature and longer laser exposure time induced increased surface damage, further reducing the HCF Strength. The test results may further demonstrate the detrimental surface impulsive high cycle fatigue effect on the materials fatigue resistance.

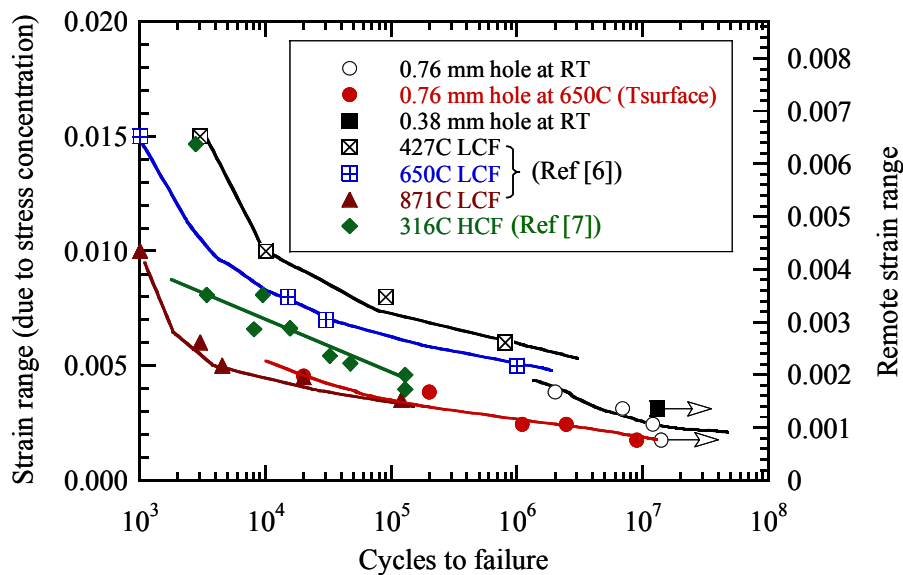
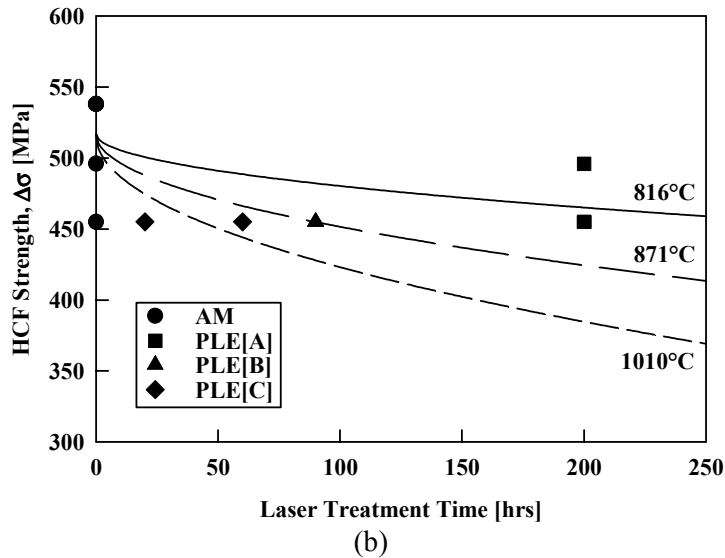
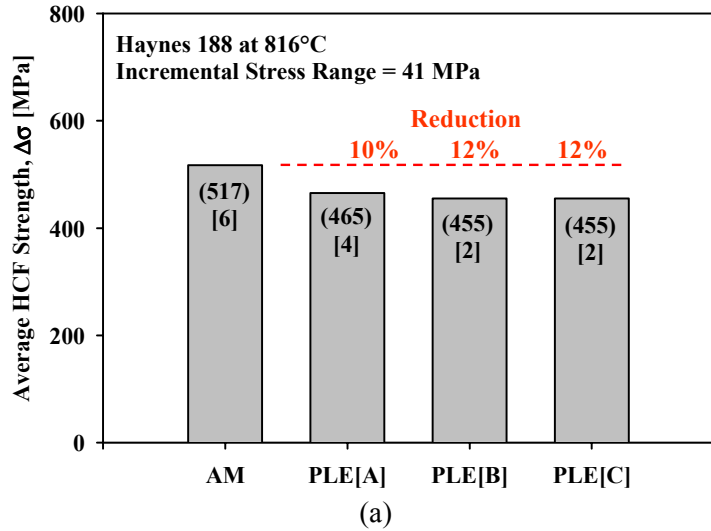


Figure 8.—Fatigue behavior of the Haynes 188 tested under the combined laser surface thermal high cycle fatigue and mechanical four-point bend fatigue test as compared to the conventional low cycle and high cycle fatigue tests.



- AM: As-Machined (6 specimens-[6]):
- PLE[A] (6 specimens-[6]): 400 Cycles; 30 min. Duration; Maximum Temperature: 816 °C (1500 °F);
- PLE[B] (2 specimens-[2]): 180 Cycles; 30 min. Duration; Maximum Temperature: 871 °C (1600 °F);
- PLE[C] (2 specimens-[2]): 40 and 120 Cycles; 30 min. Duration; Maximum Temperature: 1010 °C (1850 °F).

Figure 9.—The mechanical HCF behavior of Haynes 188 after the initial laser pulse thermal HCF treatment. (a) A 10 to 12 percent reduction in the fatigue strength was observed for the laser pretreated specimens as compared to the as-machined specimens. (b) The relationship between the HCF fatigue strength and the exposure time of the pulsed laser treatment as function of laser test temperature.

## Conclusions

A high cycle-enhanced pulse CO<sub>2</sub> laser thermal fatigue approach was developed for evaluating candidate CVCCE combustor materials under simulated engine surface high frequency thermal and mechanical loading conditions. The thermal gradient and temperature swings can result in significant thermal cyclic stresses in the material system, and thus can induce surface cracking under surface oxidation, creep and the thermal cycling conditions. The oxidation- and creep-enhanced fatigue cracking was demonstrated experimentally. Fatigue striations of various sizes were observed at the cracked surfaces and oxide scale/alloy interfaces. Reduced fatigue strength was also demonstrated under combined laser thermo-mechanical fatigue testing for the candidate materials and under the mechanical testing of the laser pulse pre-exposed specimens. The test results indicated that oxidation and creep enhanced fatigue at the oxide scale/alloy interface was an important mechanism for the surface crack initiation and propagation under the laser induced surface impulsive fatigue conditions.

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