Magnetic and Electrical Characteristics of Cobalt-Based Amorphous Materials and Comparison to a Permalloy Type Polycrystalline Material

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Magnetic component designers are always looking for improved soft magnetic core materials to increase the efficiency, temperature rating and power density of transformers, motors, generators and alternators, and energy density of inductors. In this paper, we report on the experimental investigation of commercially available cobalt-based amorphous alloys which, in their processing, were subjected to two different types of magnetic field anneals: A longitudinal magnetic field anneal or a transverse magnetic field anneal. The longitudinal field annealed material investigated was Metglas® 2714A. The electrical and magnetic characteristics of this material were investigated over the frequency range of 1 to 200 kHz and temperature range of 23 to 150 °C for both sine and square wave voltage excitation. The specific core loss was lower for the square than the sine wave voltage excitation for the same maximum flux density, frequency and temperature. The transverse magnetic field annealed core materials include Metglas® 2714AF and Vacuumschmelze 6025F. These two materials were experimentally characterized over the frequency range of 10 to 200 kHz for sine wave voltage excitation and 23 °C only. A comparison of the 2174A to 2714AF found that 2714AF always had lower specific core loss than 2714A for any given magnetic flux density and frequency and the ratio of specific core loss of 2714A to 2714AF was dependent on both magnetic flux density and frequency. A comparison was also made of the 2714A, 2714AF, and 6025F materials to two different tape thicknesses of the polycrystalline Supermalloy material and the results show that 2714AF and 6025F have the lowest specific core loss at 100 kHz over the magnetic flux density range of 0.1 to 0.4 Tesla.

Nomenclature

I^2R	winding power losses measured in Watts
B-H	hysteresis plot of magnetic flux density B versus magnetic field intensity H
SCL	specific core loss measured in Watts per pound, Watts per cubic meter, or Watts per cubic centimeter
B_M	maximum magnetic flux density measured in Tesla
f	electrical frequency measured in Hertz
$i_p(t)$	the primary excitation current measured in Amperes
$e_s(t)$	the secondary induced voltage measured in volts
T	the core temperature measured in Celsius

I.   Introduction

Almost all power electronic circuits, such as inverters and converters, require power magnetic components. These magnetic components function as either power transfer or energy storage devices, and in some cases fulfill both needs. Increasing the operating frequency of the power magnetic components will reduce their mass and size[1]. Increasing their operating temperature will admit smaller cooling radiators or heat sinks and also reduce the complexity of the heat transport system.

Magnetic components designers are always looking for improved soft ferromagnetic core materials to increase the efficiency, temperature rating and power density of transformers, motors, generators and alternators, and energy density of inductors. The primary means to increase the transformer's efficiency is to decrease the loss in the magnetic core material and the I^2R or Joulean loss in the windings. The primary means to increase the transformer's power density is to increase the frequency. But increasing the frequency without a decrease in the magnetic flux density will increase the core loss. So in most instances, the trade-off between power density, efficiency, and temperature rise comes down to a trade between operating frequency and magnetic flux density of the magnetic core material and current density in the windings. It should be noted that increasing the frequency will also increase the AC I^2R loss in the windings.

A very essential element in the design of power magnetic components is the knowledge of the electrical and magnetic properties and characteristics of available soft magnetic core materials. Properties such as saturation induction, Curie temperature, and thermal conductivity can generally be obtained from the product literature provided by the manufactures and fabricators of soft magnetic materials. However, experimental characterization data such as the effect of temperature, frequency, flux density, lamination or tape thickness, and excitation waveform on the core loss and dynamic *B-H* hysteresis loop are not always readily available. In many instances neither the manufacturer's product literature nor the technical literature provide the required information. This almost total lack of information is particularly true for non-sinusoidal excitation core loss data. In most power electronic circuits such as switched mode power supplies, the excitation voltage impressed on the converter's transformer is non-sinusoidal, and in *DC-DC* converters such as the push-pull and bridge converters, voltage excitation waveform is a square wave. Because of this lack of non-sinusoidal excitation core loss data, the transformer designer for switched mode power supplies, must generally fall back to using core loss data obtained for sine wave voltage excitation, assuming that even this data exists. Because of this lack of design data, the NASA Glenn Research Center initiated an experimental program to investigate the electrical and magnetic characteristics of candidate soft magnetic materials for temperatures up to 300 °C and frequencies up to 1 MHz for both sine and square wave voltage excitations.

The core loss, that is, the power loss, of soft magnetic materials is a function of the excitation frequency, magnetic flux density, temperature, type of excitation (voltage or current), excitation waveform (sine, square, etc.), and lamination or tape thickness. A summary of core loss theory is given in Reference 8. In previously published papers[2,3,4,5,6,7,8] we have reported on the specific core loss, *SCL,* and dynamic *B-H* hysteresis loop behavior for several polycrystalline, nanocrystalline, and amorphous soft magnetic materials. In this previous research we investigated the effects of magnetic flux density, frequency, temperature, tape thickness, and excitation waveform for voltage excitation on the *SCL* and dynamic *B-H* hysteresis loops. The soft magnetic materials investigated included an 80Ni-Fe polycrystalline alloy[2,3,6,8], two 50Ni-Fe polycrystalline alloys[4], a 2V-49Fe-49Co polycrystalline alloy[5], a grain oriented 3Si-Fe polycrystalline alloy[5], two iron-based amorphous alloys[3,4], two cobalt-based amorphous alloys[7], and an iron-based nanocrystalline alloy[7].

The difference in core loss and *B-H* loop behavior resulting from either a sine or square wave voltage excitation was previously investigated by C.H. Chen[9], T. Sato and Y. Sakaki[10], and G.E. Schwarze, W.R. Wieserman, and J.M. Niedra[6]. Chen investigated several materials and depending on material and flux density, the test frequencies ranged between 10 and 100 kHz. Chen found for like conditions of maximum magnetic flux density, B_M, and frequency, f, that the core loss was larger for sine wave than for square wave voltage excitation. Sato and Sakaki tested materials similar to those investigated by Chen, but extended the test frequency up to 1 MHz. Their results were similar to those reported by Chen. In these papers there is no indication that their tests were conducted for temperatures beyond 50 °C. Schwarze, Wieserman, and Niedra did extensive experimental tests on an 80Ni-Fe alloy known in the trade as Supermalloy. Their investigation covered the frequency range of 1 kHz to 50 kHz and temperature range of 23 to 300 °C. An analytical investigation of the sine and square wave *SCL* always found that the sine wave *SCL* for the same B_M, f, and T was always greater than the square wave *SCL*. It was also found that the ratio of sine-to-square *SCL* varied up to 22 percent[6] depending on B_M, f, and T.

In this paper, we will report on an experimental investigation of commercially available cobalt-based amorphous alloys which, in their processing, were subjected to two different types of magnetic anneals: a longitudinal or transverse magnetic field anneal. The longitudinal magnetic field anneal is applied parallel to the rolling direction and in the plane of the magnetic tape while the transverse magnetic field anneal is applied perpendicular to the rolling direction and in the plane of the tape.

We previously investigated very thin tape Permalloy (80Ni-20Fe-4Mo) type polycrystalline material and found the ¼-mil thick tape to have very low core loss. The Permalloy type materials are relatively "old" technology materials compared to the relatively "new" amorphous magnetic materials. The *SCL* for this ¼-mil thick tape will be included in a comparison to several amorphous materials.

In addition, dynamic *B-H* loops for the materials investigated in this paper will be presented to show the effects of frequency and excitation waveform on the size and shape of these loops.

II.   Materials and Test Core Description

The amorphous longitudinal magnetic field annealed Metglas® 2714A test cores were wound by Magnetics, a Division of Spang and Company, in the form of a toroid with nominal tape thickness of 20 μm. The width of the tape was 0.25 inch and nominal core dimensions were OD = 1.25 inches and ID = 1.0 inch. The amorphous transverse magnetic field annealed Metglas® 2714AF, also known as MAGNAPERM®, test core was provided to NASA Glenn Research Center as a sample toroid core by Allied Signal, Inc., Parsippany, NY. The tape thickness of the toroid was also a nominal 20 μm with core dimensions of OD = 1.75 inches, ID = 0.875 inches and height = 0.375 inches.

The manufacturer's literature[11] for the 2714A and 2714AF gives a saturation flux density of 0.57 T, saturation magnetostriction of less than 1 ppm, Curie temperature of 225C, crystallization temperature of 550 °C, continuous operating temperature of 90 °C, and mass density of 7.59 gm/cm^3. The composition of 2714A and 2714AF according to the manufacturer's Material Safety Data Sheet[12] in weight percent is Cobalt (75 – 90), Iron (7 - 13), Nickel (1 – 5), Silicon (7 – 13), and Boron (1 – 5).

III.   Experimental Description

The measurement system used to measure, compute, plot, and display the electrical and magnetic characteristics of the test core material is shown in Figure 1. A key element of the measurement system is the power amplifier used to excite the core material. The introduction of amplitude or phase distortion by the amplifier, and this is particularly true for square wave voltage excitation, will produce erroneous core loss and *B-H* dynamic loops. The method used to obtain the *SCL* and *B-H* dynamic loops from the primary excitation current, $i_p(t)$, and the secondary induced voltage, $e_s(t)$, waveforms is described and discussed in Reference 2.

The electrical and magnetic characteristics of the 2714A material were tested over the frequency range of 1 to 200 kHz and temperature range of 23 to 150 °C for both sine and square wave voltage excitation. The electrical and magnetic characteristics of the 2714AF material were tested over the frequency range of 10 to 100 kHz for sine wave voltage excitation and 23 °C only. B_M was either the saturation flux density for the low frequencies or that B_M for which the *SCL* remained less than 100 W/lb. Particular attention was given to capturing the required waveforms in the minimum length of time.

IV.   Experimental Results and Discussion

Effects of the B_M, *f*, and *T* on the *SCL* can best be seen and analyzed for trends by plotting the data as follows:
1.   *SCL* versus B_M with *f* as the parameter for a given *T*.
2.   *SCL* versus *f* with B_M as parameter for a given *T*.
3.   *SCL* versus *T* with *f* as parameter for a given B_M.

The effects of a longitudinal magnetic field anneal (2714A) and transverse magnetic field anneal (2714AF) on the *SCL* can best be seen and analyzed for trends by plotting the data as follows:
1.   Ratio of 2714A to 2714AF *SCL* versus B_M with *f* as the parameter.
2.   Ratio of 2714A to 2714AF *SCL* versus *f* with B_M as the parameter.

A. Longitudinal Magnetic Field Anneal (2714A)

The effects of B_M and *f* on the *SCL* at a temperature of 23 °C for sine and square wave voltage excitation are shown in the Figure 2 and 3 plots, respectively for the 2714A material.

The curve for a given *f* shows that the *SCL* tends to increase nearly linearly with increasing B_M on a log-log scale for both the sine wave excitation (Figure 2a) and the square wave excitation (Figure 2b). Likewise, the plots for a given B_M shows that the *SCL* tends to increase nearly linearly on a log-log scale with *f* for both sine wave excitation (Figure 3a) and square wave excitation (Figure 3b). A comparison of either Figure 2a (sine wave excitation) to Figure 2b (square wave excitation) or Figure 3a (sine wave excitation) to Figure 3b (square wave excitation) shows that the *SCL* is larger for sine wave excitation than for square wave excitation. For example, at B_M = 0.4 Tesla, the ratio of sine-to-square wave *SCL* varies from 1.03 at 1 kHz to 1.09 at 50 kHz. In general, this is the range of variation of the sine-to-square *SCL* ratio for the other B_M values tested. This same comparison of sine-to-square wave *SCL* ratio was previously done for a 1-mil thick tape Supermalloy toroid at B_M = 0.4 Tesla at 23 °C[6]. In this case, the ratio varied between 1.17 and 1.22 over the frequency range of 1 to 50 kHz. This comparison readily shows that the sine-to-square wave *SCL* ratio is greater for the polycrystalline Supermalloy material than for the amorphous

2714A material. The reason for this rather large difference in the ratios is not readily apparent and additional experimentation and analysis will be required to determine the underlying cause. However, these results would imply that the core loss mechanism for a polycrystalline magnetic material is different than that for an amorphous magnetic material when subjected to different types of excitation.

Figure 4a (sine wave excitation) and Figure 4b (square wave excitation) plot the *SCL* as a function of temperature for $B_M = 0.4$ Tesla with f as the parameter for the 2714A material. The "flatness" of the *SCL* versus T curves plotted in these figures is seen to be a function of frequency. For 5 and 10 kHz, the *SCL* curves tend to a slight minimum at 100 °C and then increase in slope from 100 to 150 °C, but the *SCL* value at 150 °C is less than that at 23 °C. For 20 and 50 kHz, the slope of the *SCL* curves decreases slightly from 23 to 100 °C and then the slope increases from 100 to 150 °C, but the *SCL* value at 150 °C is greater than that at 23 °C. The relative increase in *SCL* at 150 °C is greater for 50 kHz than for 20 kHz compared to the *SCL* at 23 °C. For 100 kHz, the slope of the *SCL* curve shows a steady increase over the temperature range of 23 to 150 °C.

Figure 5a (sine wave excitation) and Figure 5b (square wave excitation) give a family of dynamic *B-H* loops for frequencies of 1, 5, 10, 20, and 100 kHz for $B_M = 0.4$ Tesla and $T = 23$ °C for the 2714A material. A comparison of the *B-H* loops in Figure 5a with those in Figure 5b shows that the shape of the loop is excitation dependent. Sine wave voltage excitation gives rounded corners at $\pm B_M$ while square wave voltage excitation gives pointed corners at $\pm B_M$. Both sets of loops give a good visual image of how the size or area of the loop increases with frequency due to eddy current loss. Another observation is that the ac coercive force is less for the square wave than for the sine wave excitation for a given frequency. And finally, it should be noted that loops for both sine and square wave excitation are quite symmetrical about the origin. 2714A is a "square-loop" type of material for which the ratio of remanence to maximum flux density approaches unity. "Square loop" types of materials tend to "ratchet" towards either $\pm B_M$ and thus give non-symmetrical loops.

Figure 6 gives a good visual picture of a comparison of a 2714A *B-H* loop for sine and square wave voltage excitation at $B_M = 0.4$ Tesla, $f = 100$ kHz, and $T = 23$ °C. It is readily seen that the square wave excitation *B-H* loop fits entirely within the area of the sine wave excitation *B-H* loop except for tip areas about $\pm B_M$. If these two tip areas are subtracted from the area of the sine wave excitation *B-H* loop, it is seen that the area (i.e., core loss) enclosed by the sine wave excitation *B-H* loop is larger than the area enclosed by the square wave excitation *B-H* loop.

B. Transverse Magnetic Field Anneal (2714AF)

The effects of B_M and f on the *SCL* at 23 °C for sine wave voltage excitation for the transverse annealed 2714AF material are given in Figures 7 and 8. Just as was observed for the longitudinal annealed 2714A, the curve for any given f in Figure 7 shows that the *SCL* increases nearly linearly with increasing B_M on a log-log scale. Likewise, for any given B_M, Figure 8 shows that the *SCL* increases nearly linearly with f on a log-log scale.

Our primary interest in 2714AF is to compare the *SCL* of the transverse annealed material with the longitudinal annealed 2714A material to determine what advantage 2714A has over 2714AF. Figure 9 gives a comparison of these two material's *SCL* as a function of B_M with f as the parameter at 23 °C; Figure 10 gives this comparison of *SCL* as a function of f with B_M as the parameter at 23 °C. Inspection of the *SCL* versus B_M curves in Figure 10 shows that for any given B_M, the *SCL* is lower for the 2714AF than for the 2714A material for any given frequency. Likewise, inspection of the *SCL* versus f curves in Figure 11 shows that for any given f, the *SCL* is lower for the 2714AF than for the 2714A material for any given B_M.

The results in Figures 9 and 10 clearly show the *SCL* advantages of the transverse anneal compared to the longitudinal anneal for comparable B_M and f. However, Figures 9 and 10 do not quickly show quantifiably how much better the *SCL* is for 2714AF than for 2714A. By plotting the *SCL* ratio of 2714A to 2714AF, the clear advantage of 2714AF is readily seen. Figure 11 is a plot of the *SCL* ratio of 2714A to 2714AF versus B_M for three frequencies at 23 °C. Figure 12 is a plot of this same *SCL* ratio versus f for four B_M values. The *SCL* curves in Figure 11 show that the *SCL* ratio decreases as B_M increases with the lowest frequency giving the largest ratio. The curves in Figure 12 show that the *SCL* ratio decreases as f increases with the lowest B_M giving the largest ratio. The results in the two figures show that the *SCL* advantage of 2714AF over 2714A is greatest at low B_M and low f and that this advantage diminishes as either B_M or f increases. For example, at 20 kHz and $B_M = 0.1$ Tesla, the ratio is 5.4 while for this same frequency and $B_M = 0.5$ Tesla, the ratio now decreases to 1.9. At 100 kHz and $B_M = 0.1$ Tesla the ratio is 2.8 while for this same frequency and for $B_M = 0.4$ Tesla, the ratio drops to 1.4. Even though the *SCL* advantage diminishes with increasing B_M or f, the fact remains that the transverse annealed 2714AF material always has lower losses than the longitudinal annealed 2714A material for the frequencies and flux densities tested.

The 2714AF dynamic *B-H* loops for frequencies 20, 50, and 100 kHz at $B_M = 0.4$ Tesla and 23 °C are drawn in Figure 13. When this family of loops is compared to the family of loops for 2714A in Figure 5(a), the following is

observed: (a) The 2714A loops are more squared, i.e., have a higher remanence than the 2714AF loops, (b) the 2714AF loops are skewed or tilted to the right relative to the 2714A loops, and (c) a 2714A loop has more enclosed area than a 2714AF loop for any given frequency. A more direct comparison of the 2714A and the 2714AF dynamic *B-H* loops for 100 kHz, 0.4 Tesla is displayed in Figure 14. This figure quickly shows that the 2714AF loop is entirely enclosed in the 2714A loop except for the small areas about $\pm B_M$. Figure 14 gives both a good picture of the loss advantage of 2714AF over 2714A and also the tilt of the 2714AF loop relative to the 2714A loop.

C. SCL Comparison of Different Materials

Of special interest and of great help to the magnetic component designer are *SCL* plots comparing various candidate soft magnetic materials over a range of flux densities and frequencies. *SCL* plots of this type reduce design time as they enable the designer to judiciously select the best material for the given design frequency and flux density.

Figure 15 gives a plot of the *SCL* versus B_M at 100 kHz and 23 °C for four different materials which includes not only the 2714A and 2714AF materials reported in this paper, but also the transverse annealed amorphous 6025F material manufactured by Vacuumschmelze, and poly crystalline Supermalloy material. The *SCL* for Supermalloy is given for 1-mil and ¼-mil thick tape. Also, the *SCL* for both sine and square wave voltage excitation are given for 2714A. The curves in Figure 15 show that the *SCL* for the transverse annealed 2714AF and 6025F materials yield the lowest losses with the 6025F material giving slightly lower *SCL* at low flux densities and slightly higher *SCL* at the higher flux densities compared to the 2714AF material. This figure also shows that the *SCL* for the polycrystalline ¼-mil Supermalloy is much better than the longitudinal annealed 2714A for low B_M, but this advantage is almost eliminated as B_M approaches 0.3 Tesla.

Figure 16 gives a plot of the *SCL* versus *f* at $B_M = 0.1$ Tesla and 23 °C for the same materials shown in Figure 15. Again it is seen from this figure that the transverse annealed 2714AF and 6025F give the lowest *SCL*, but 6025F shows slightly lower *SCL* compared to 2714AF. Of special interest to note is that the ¼-mil Supermalloy has a lower *SCL* over the entire frequency range compared to the longitudinal annealed amorphous 2714A. Also it is interesting to note that the 1-mil Supermalloy has lower *SCL* than the 2714A up to 20 kHz.

V.   Summary and Conclusion

An experimental study was conducted to investigate the combined effects of temperature and sine or square wave voltage excitation on the *SCL* and dynamic *B-H* hysteresis loops of the longitudinal magnetic field annealed amorphous Metglas® 2714A material. For the same B_M, *f*, and *T*, the *SCL* was always lower for the square than the sine wave voltage excitation. In comparing the polycrystalline Supermalloy to Metglas® 2714A, it was found that the ratio of sine-to-square wave *SCL* was greater for Supermalloy than for 2714A at $B_M = 0.4$ Tesla and $T = 23$ °C. The underlying reason for this is not immediately apparent and needs to be explored if this difference is to be attributed solely to the classical eddy current loss component of the total core loss. The effect of temperature on the *SCL* of 21714A for both sine and square wave voltage excitation was found to be minimal from 23 to 100 °C for $B_M = 0.4$ Tesla, but with a noticeable increase in *SCL* from 100 to 150 °C with the increase being more pronounced with increasing frequency.

An experimental study was also conducted to investigate the effect of a transverse magnetic field annealed material on the S*CL*. A comparison of the *SCL* of 2714A (longitudinal magnetic field anneal) with 2714AF (transverse magnetic field anneal) found that 2714AF always had a lower *SCL* than 2714A for any given B_M and *f*. In particular, it was found that the *SCL* ratio of 2714A to 2714AF was dependent on B_M and *f* and that the highest ratio occurred for the lowest B_M and *f* for decreasing ratio with either increasing B_M or *f*.

Finally, a comparison of the 2714A and 2714AF materials was made to another transverse magnetic annealed amorphous material, 6025F, manufactured by Vacuumschmelze and two different tape thicknesses of the polycrystalline material, Supermalloy. From the magnetic component designer's viewpoint, the best material to use from this comparison in terms of *SCL* is either 2714AF or 6025F which have comparable losses at 100 kHz from $B_M = 0.1$ to 0.4 Tesla. This comparison also shows that the ¼-mil thick tape Supermalloy has a lower *SCL* than the longitudinal annealed 2714A over the entire frequency range and magnetic flux density range investigated. The comparison also shows that the *SCL* of the 1-mil thick tape Supermalloy is competitive with the 2714A at low B_M and *f*.
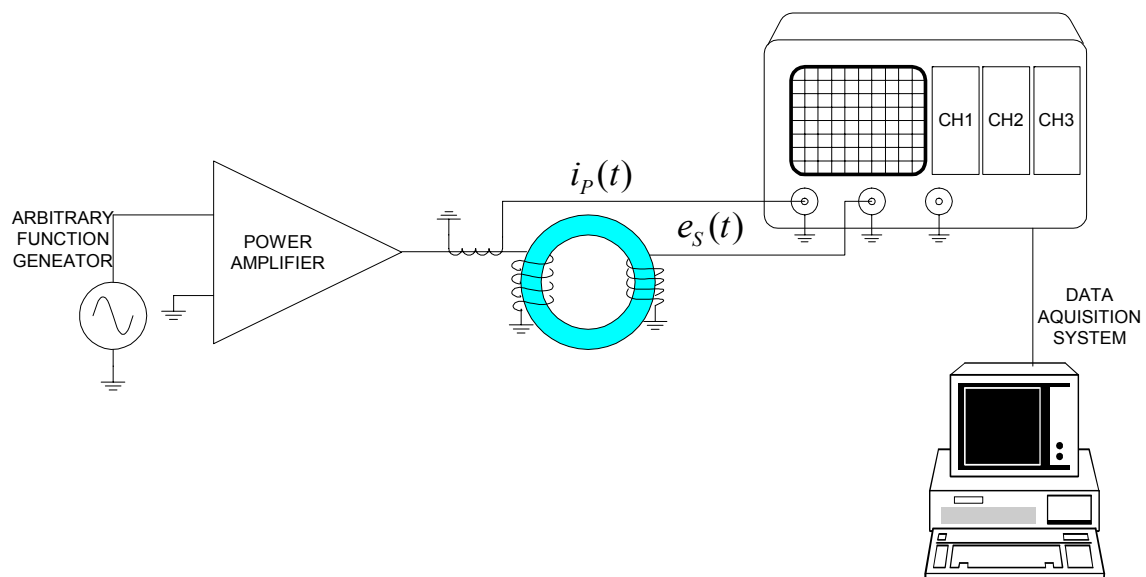
Figure 1.—Specific loss and dynamic *B-H* hysteresis loop measurement system.
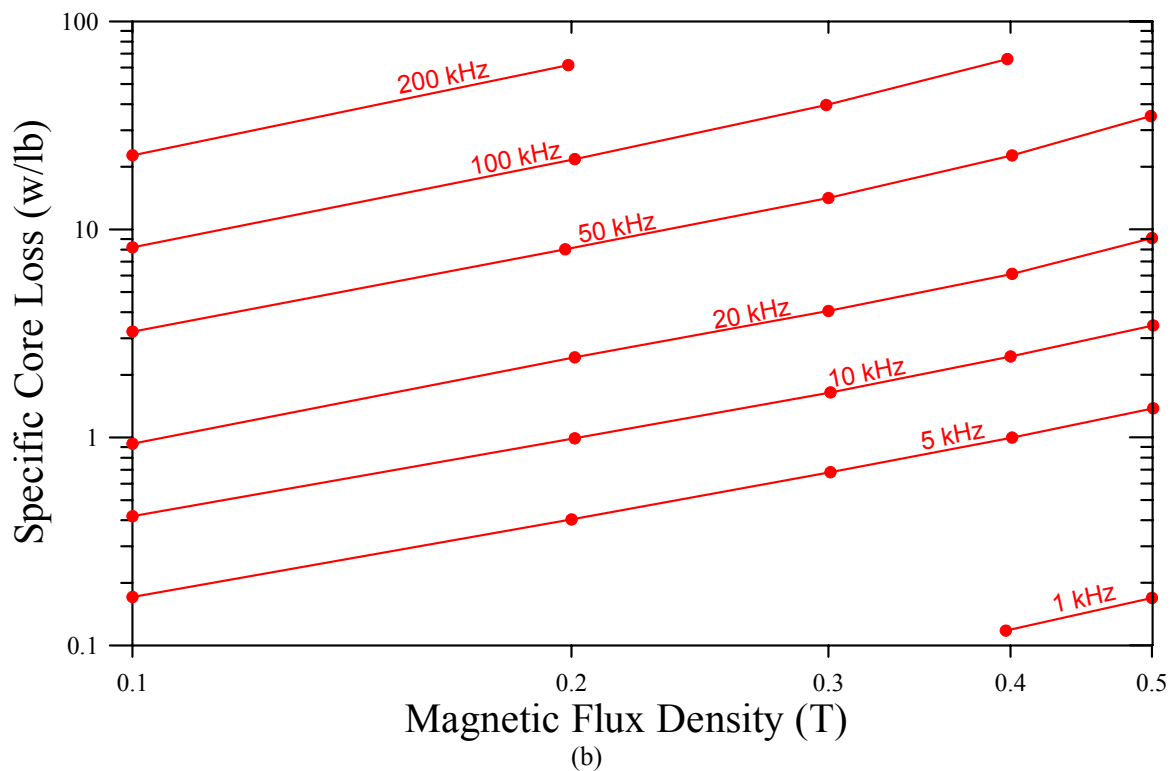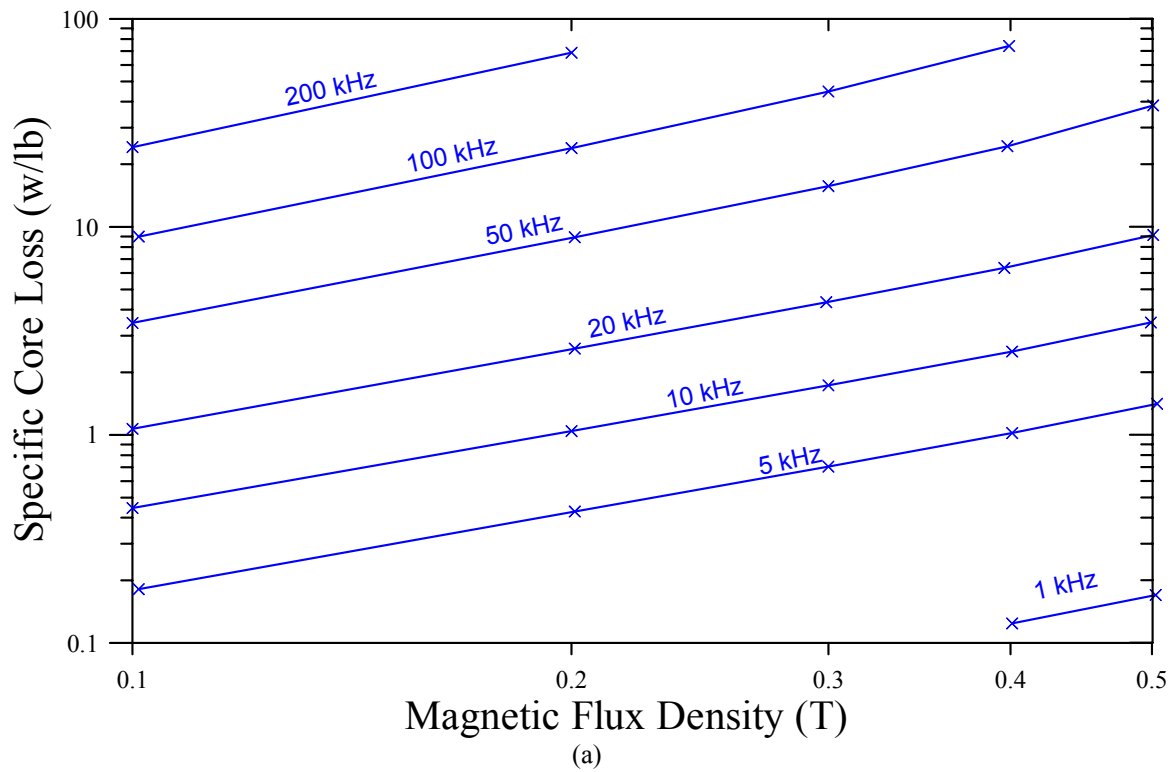
Figure 2.—Metglas® 2714A specific core loss versus maximum flux density at 23 °C with frequency as parameter for nominal 20 μm thick tape toroid. (a) Sine wave voltage excitation, (b) Square wave voltage excitation.
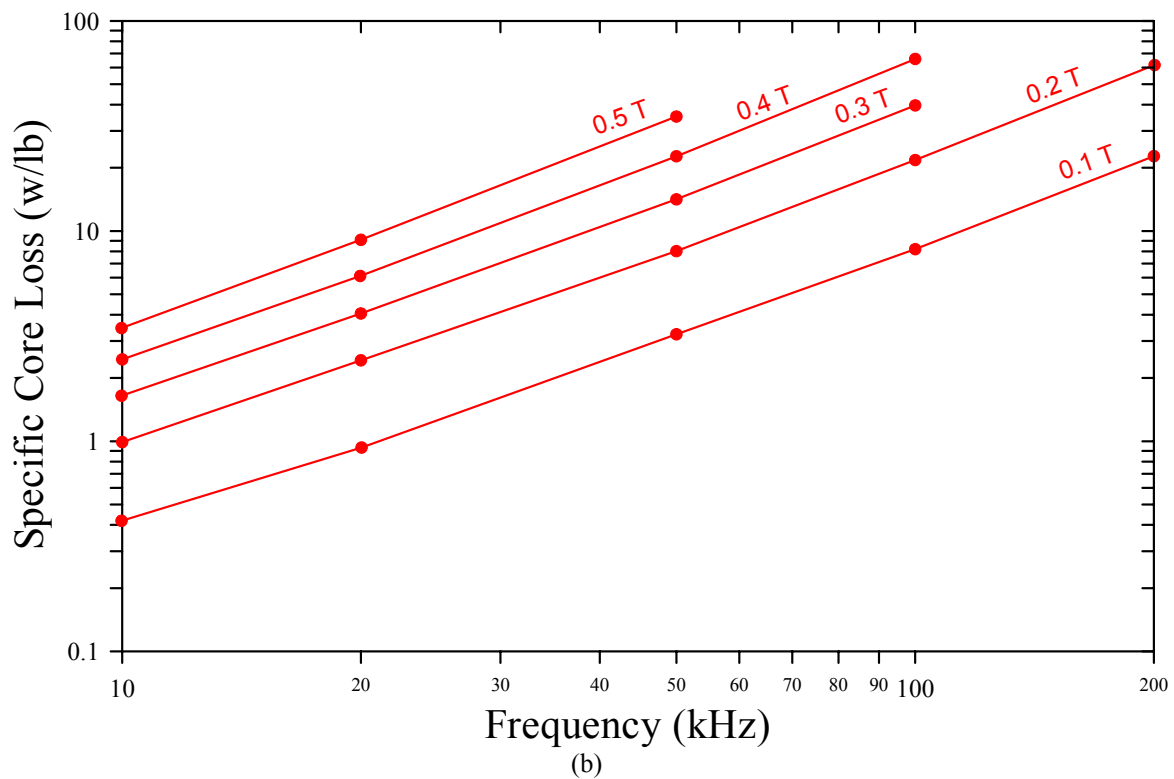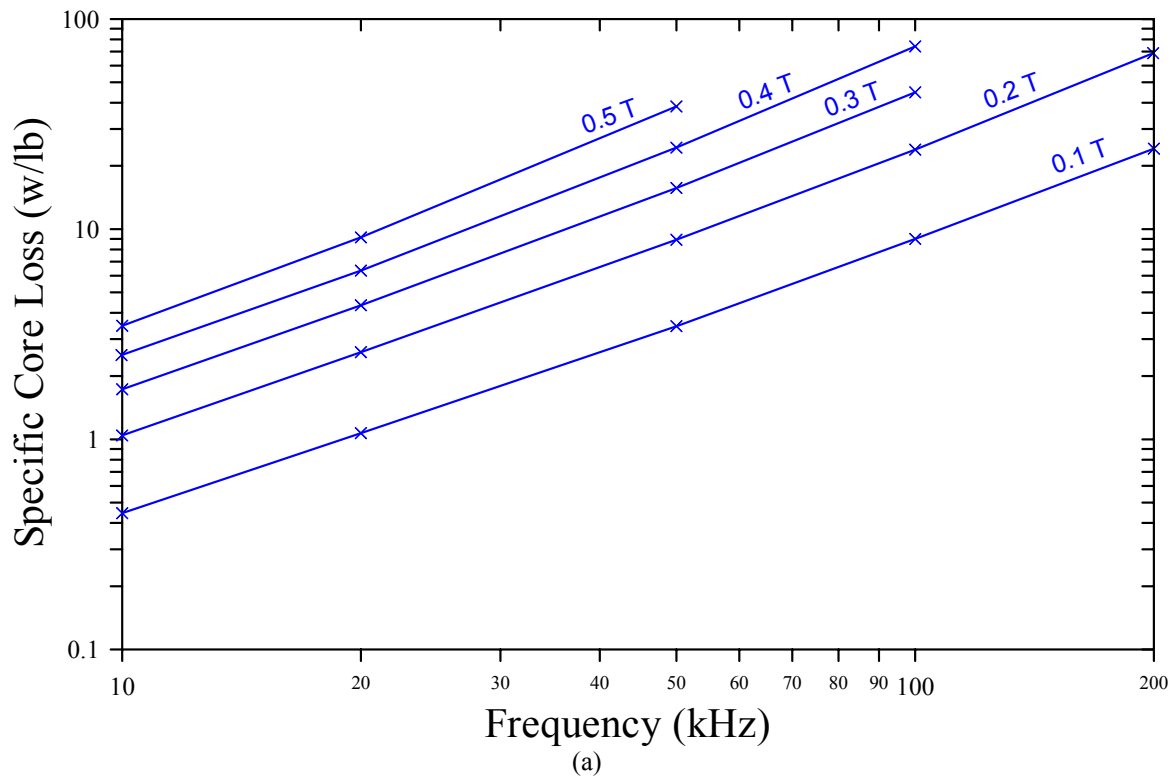
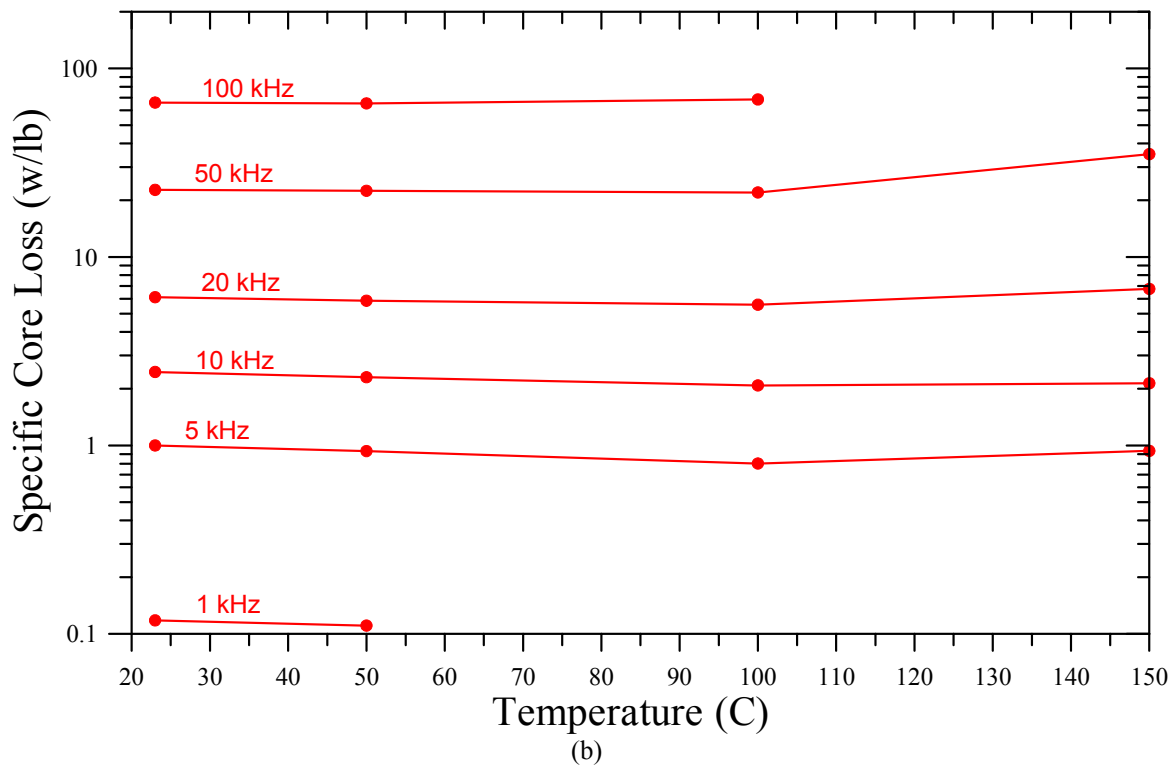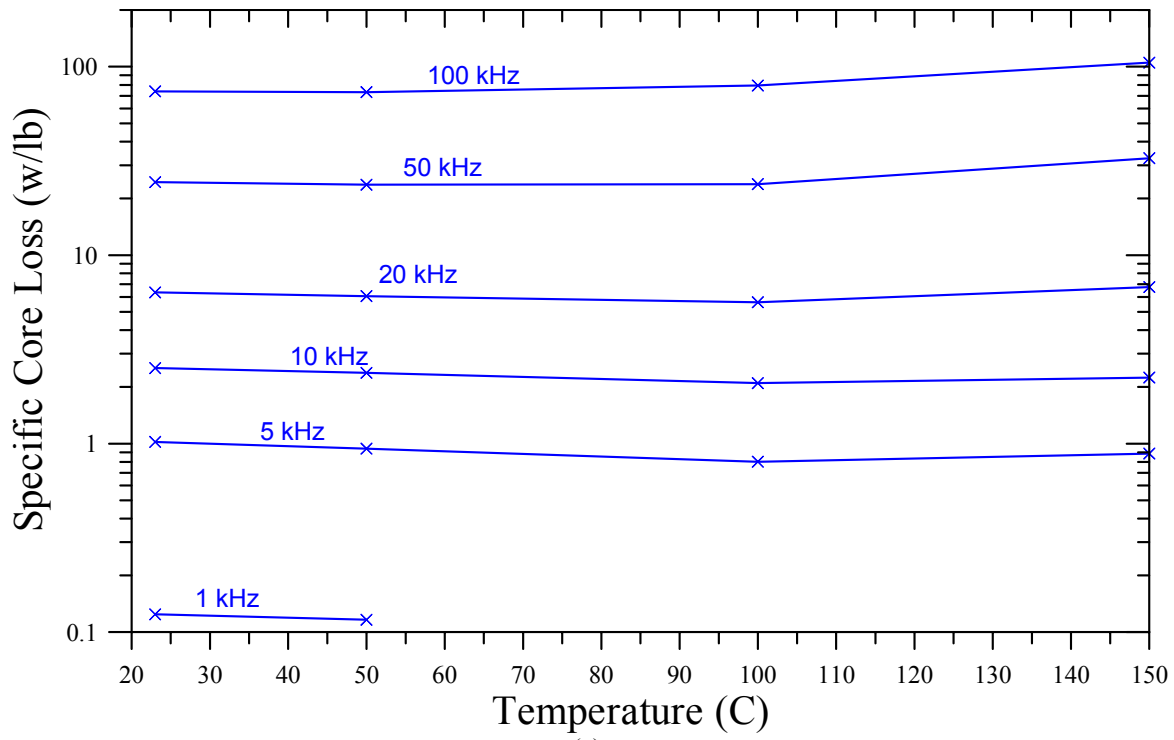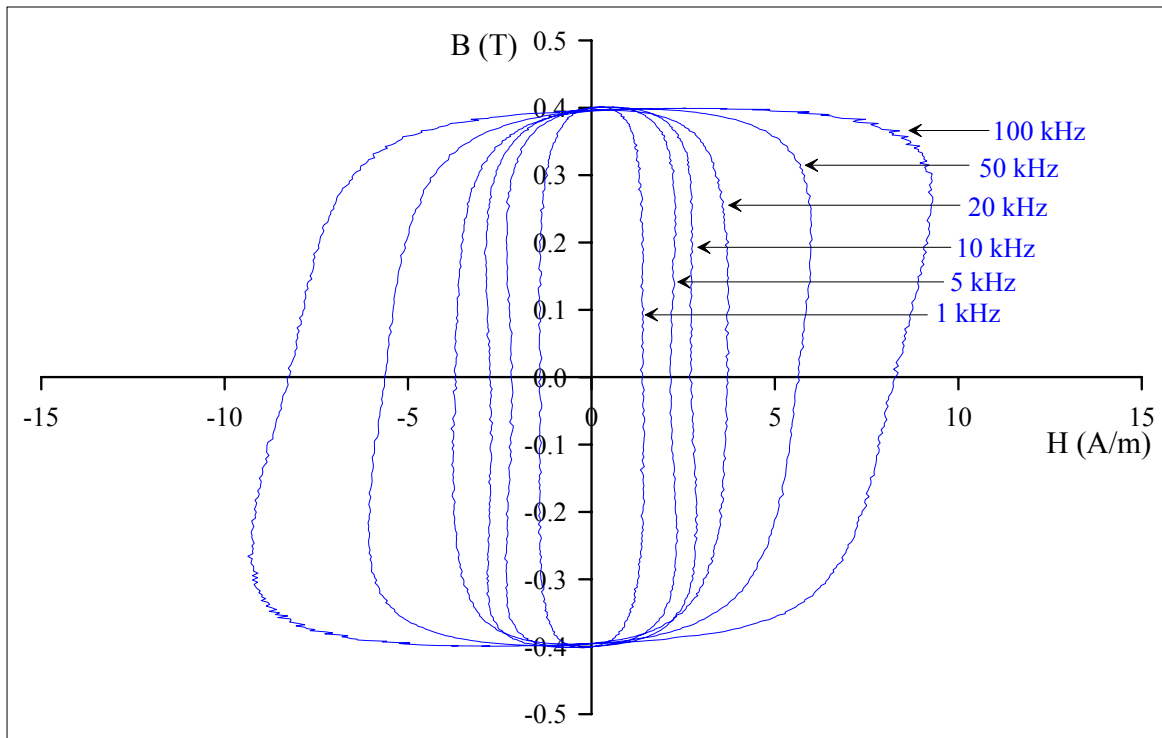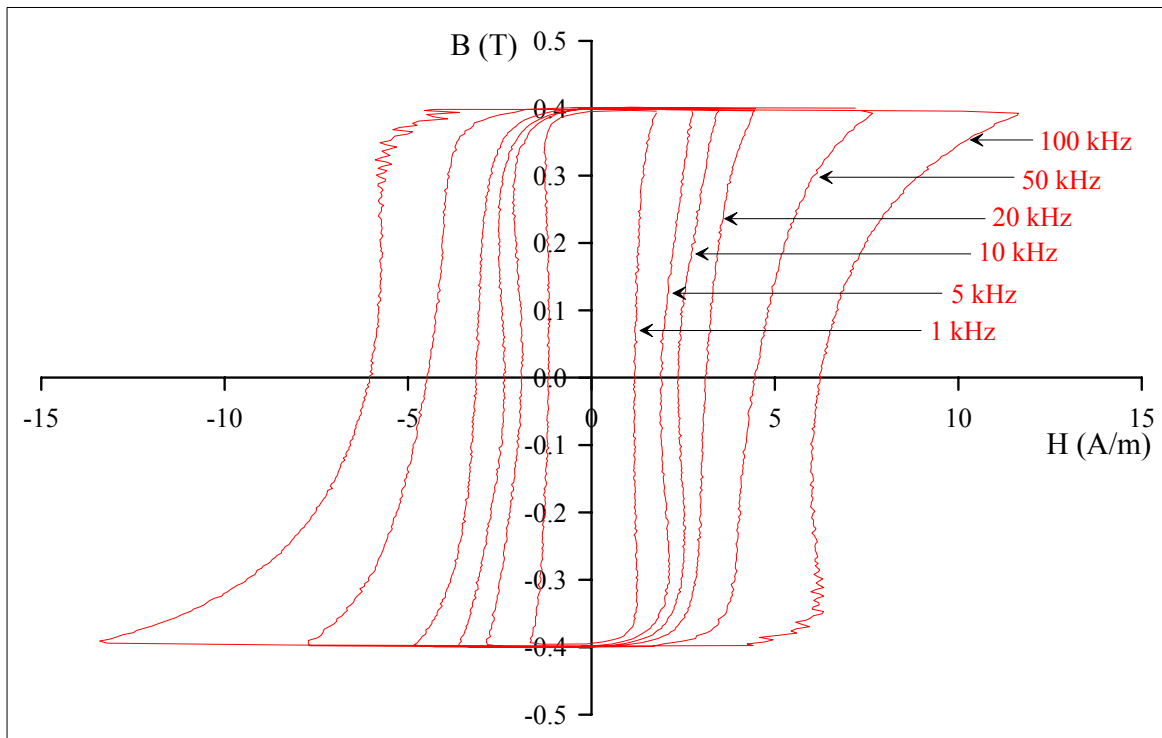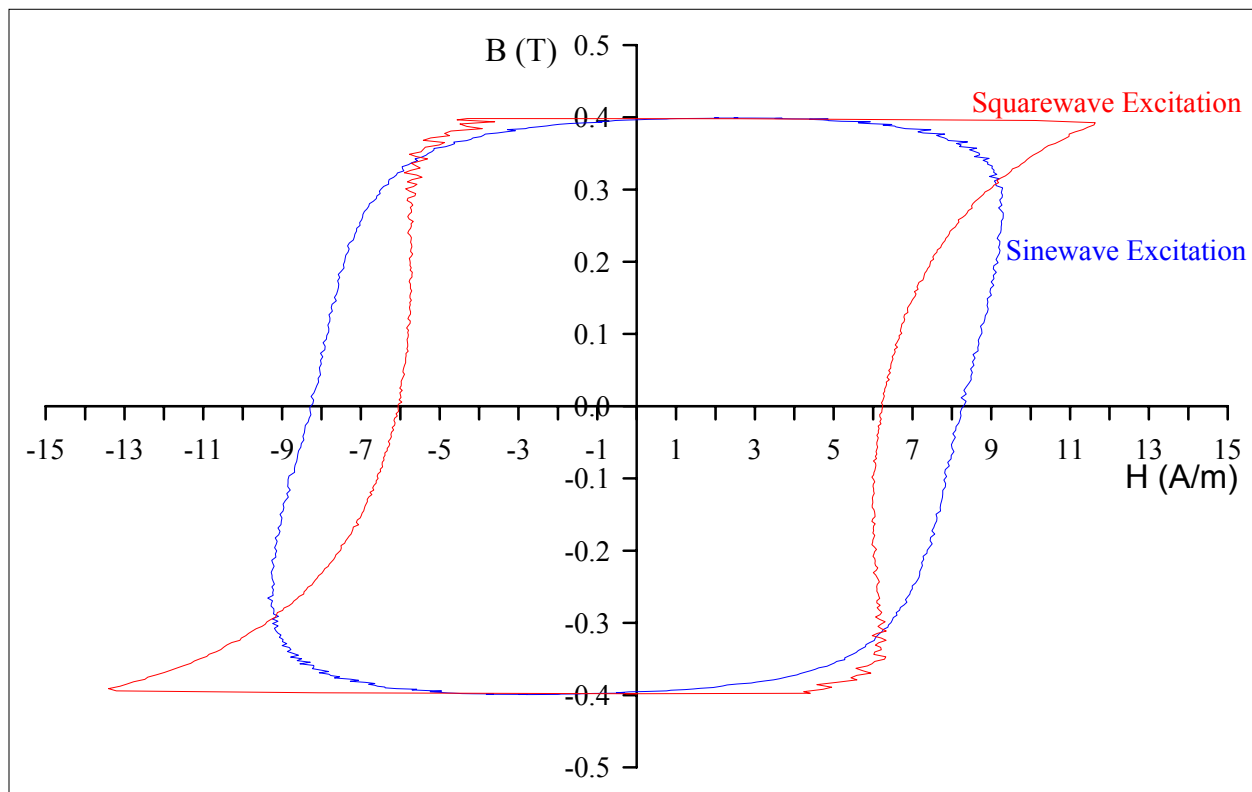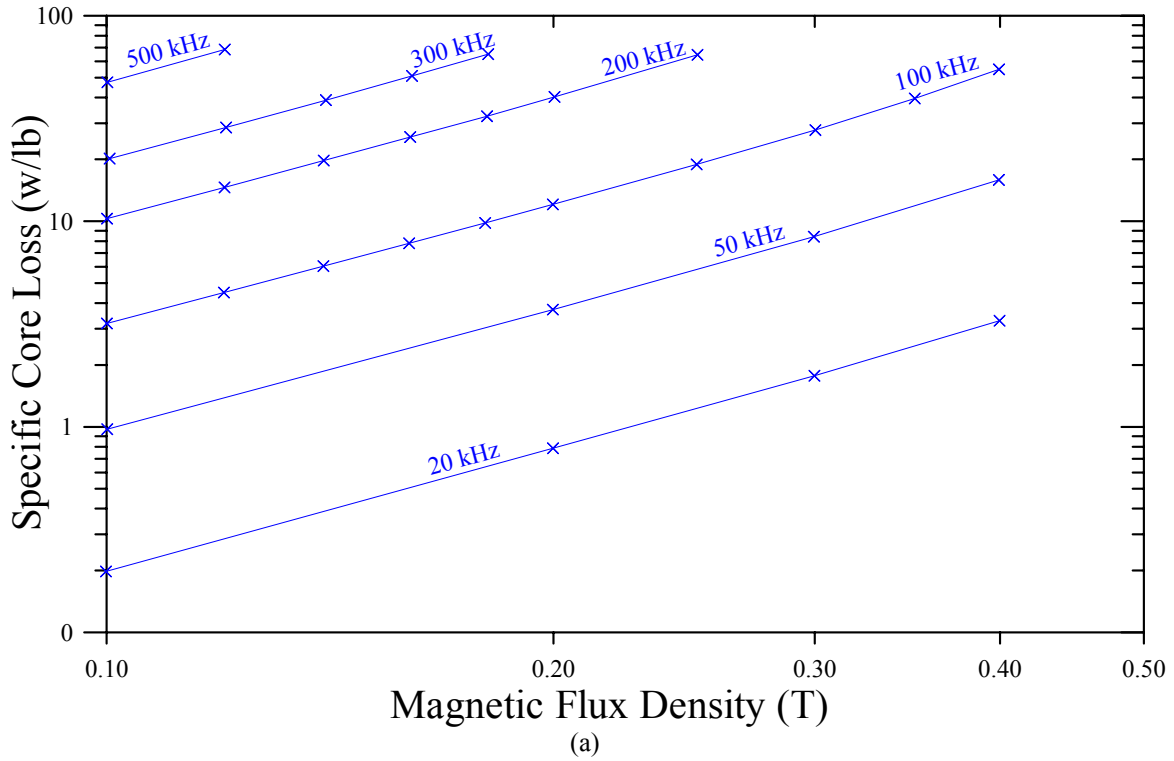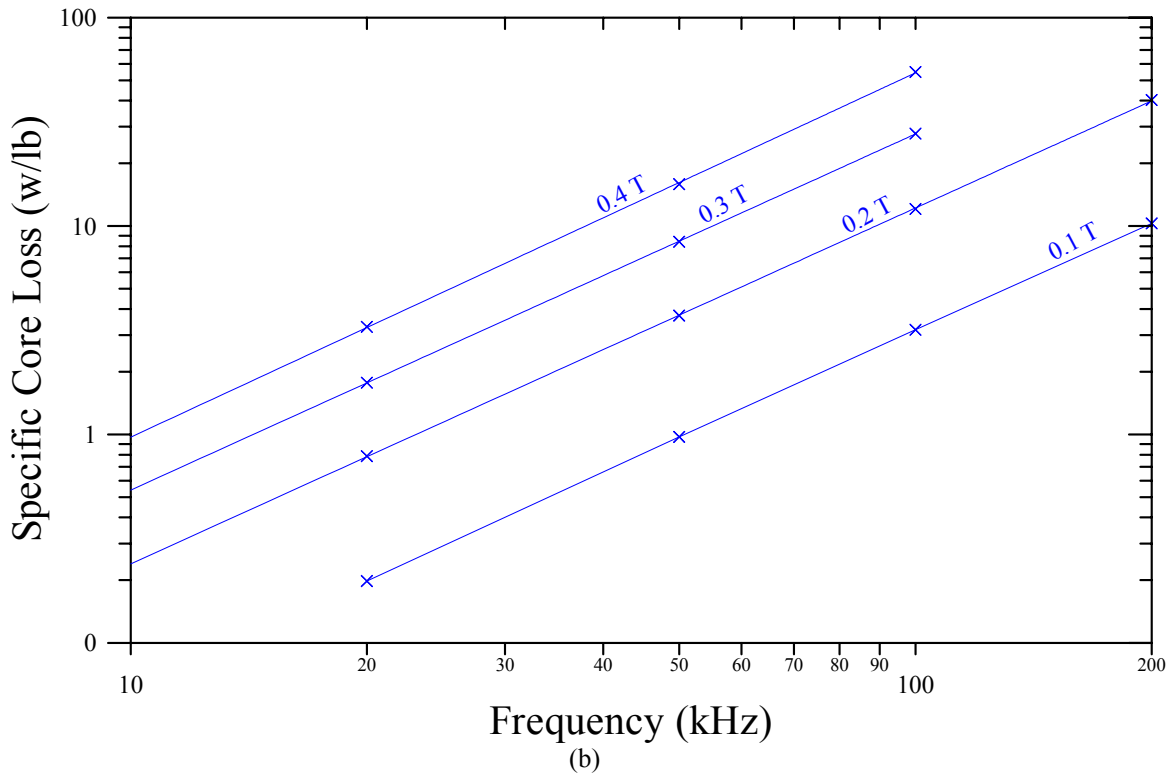Figure 3.—Metglas® 2714A specific core loss versus frequency at 23 °C with maximum flux density as parameter for nominal 20 μm thick tape toroid. (a) Sine wave voltage excitation, (b) Square wave voltage excitation.
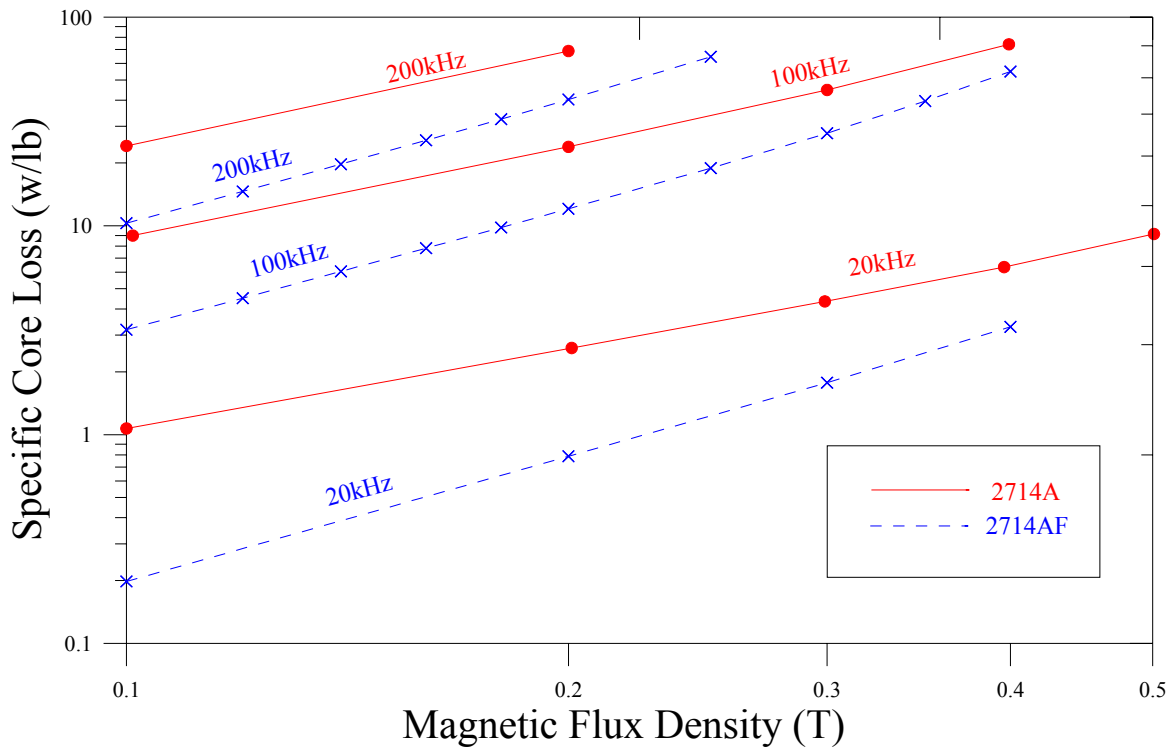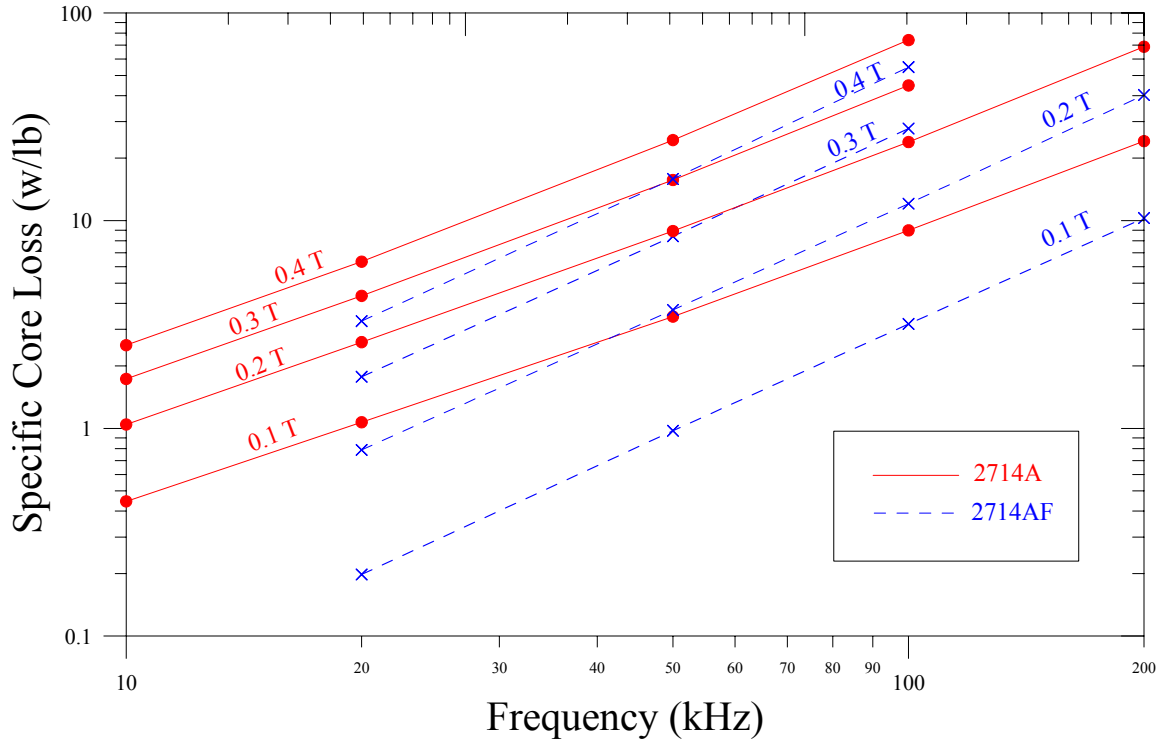
Figure 4.—Metglas® 2714A specific core loss versus temperature at B_M = 0.4 Tesla with frequency as the parameter for a nominal 20 μm thick tape toroid. (a) Sine wave voltage excitation, (b) Square wave voltage excitation.

Figure 5.—Metglas® 2714A family of dynamic *B-H* loops at 23 °C for various frequencies at B_M = 0.4 Tesla for a nominal 20 μm thick tape toroid. (a) Sine wave voltage excitation, (b) Square wave voltage excitation.

Figure 6.—Comparison of a nominal 20 µm thick tape toroid Metglas® 2714A dynamic *B-H* loops for sine and square wave voltage excitation at 23 °C, B_M = 0.4 Tesla, and f = 100 kHz.

Figure 7.—Metglas® 2714AF specific core loss versus maximum magnetic flux density at 23 °C with frequency as the parameter for sine wave voltage excitation for a nominal 20 µm thick tape toroid.
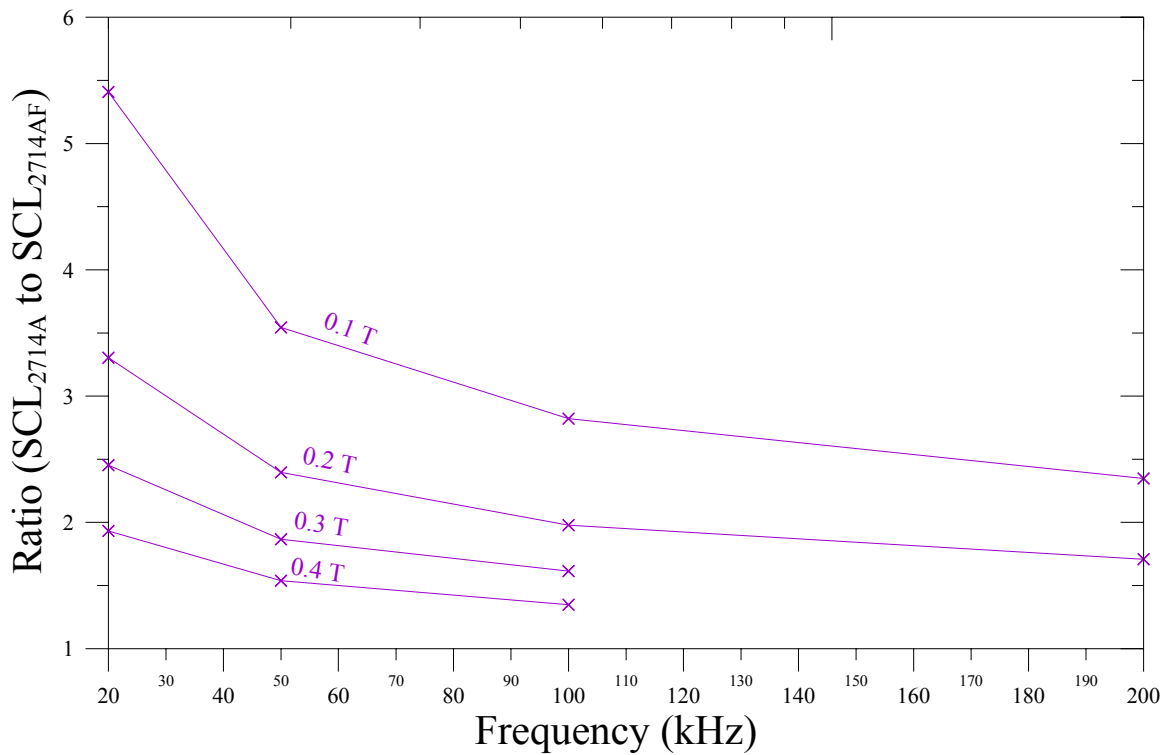

Figure 8.—Metglas® 2714AF specific core loss versus frequency at 23 °C with maximum magnetic flux density as the parameter for a nominal 20 µm thick tape toroid.

Figure 9.—Comparison of Metglas® 2714A to 2714AF specific core loss versus maximum magnetic flux density at 23 °C with frequency as the parameter for sine wave voltage excitation for nominal 20 µm thick tape toroid.

Figure 10.—Comparison of Metglas® 2714A to 2714AF specific core loss versus frequency at 23 °C with maximum flux density as the parameter for sine wave voltage excitation for nominal 20 µm thick tape toroid.

Figure 11.—Specific core loss ratio of Metglas® 2714A to 2714AF material versus maximum magnetic flux density at 23 °C for three frequencies for sine wave voltage excitation for nominal 20 μm thick tape toroids.

Figure 12.—Specific core loss ratio of Metglas® 2714A to 2714AF material versus frequency at 23 °C for four maximum magnetic flux densities for sine wave voltage excitation for nominal 20 μm thick tape toroids.
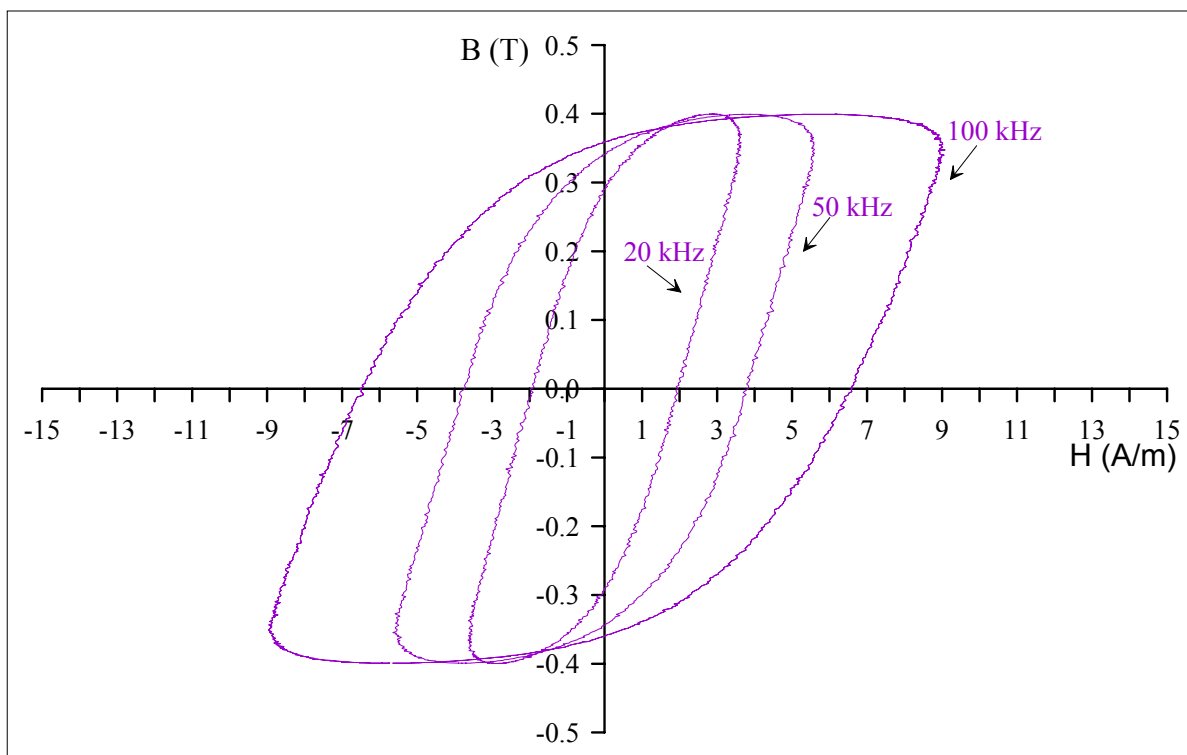
Figure 13.—Metglas® 2714AF family of dynamic *B-H* loops at 23 °C for various frequencies at $B_M = 0.4$ Tesla for sine wave voltage excitation for a nominal 20 μm thick tape toroid.

Figure 14.—Comparison for nominal 20 μm thick tape toroids Metglas® 2714A to 2714AF dynamic *B-H* loops for sine wave voltage excitation at 23 °C, $B_M = 0.4$ Tesla, and $f = 100$ kHz.
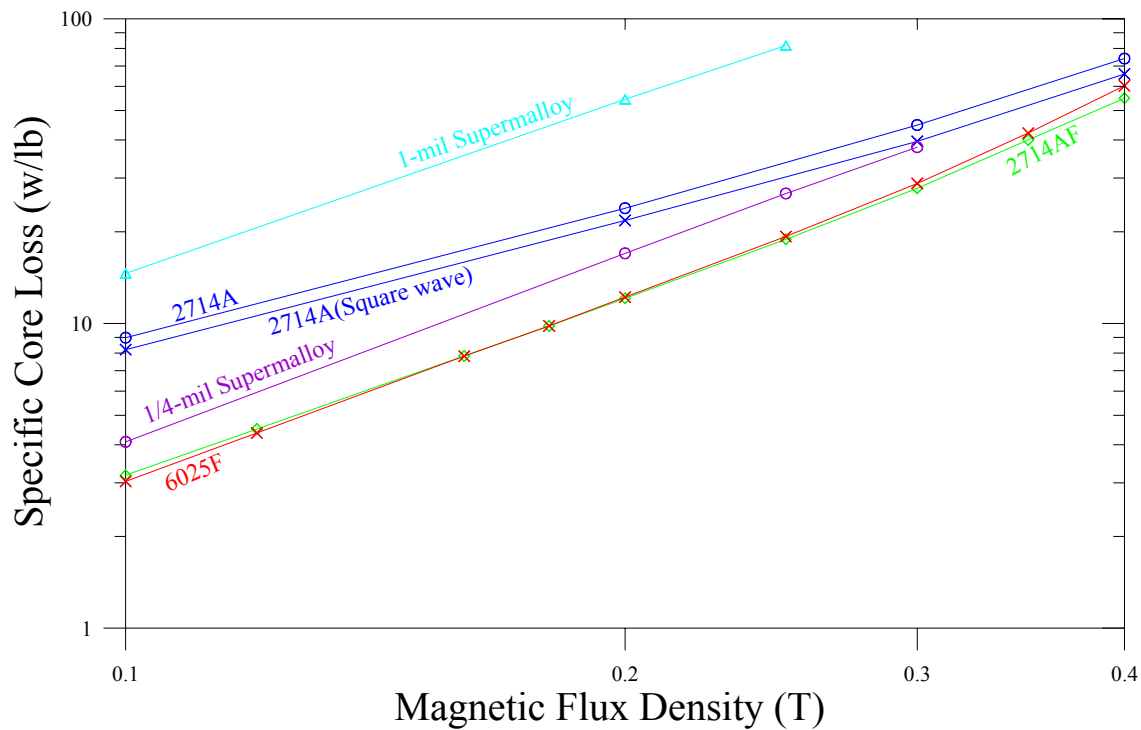
Figure 15.—Comparison of the specific core loss versus maximum magnetic flux density of different magnetic materials for sine wave voltage excitation, except where noted, at 23 °C and 100 kHz.
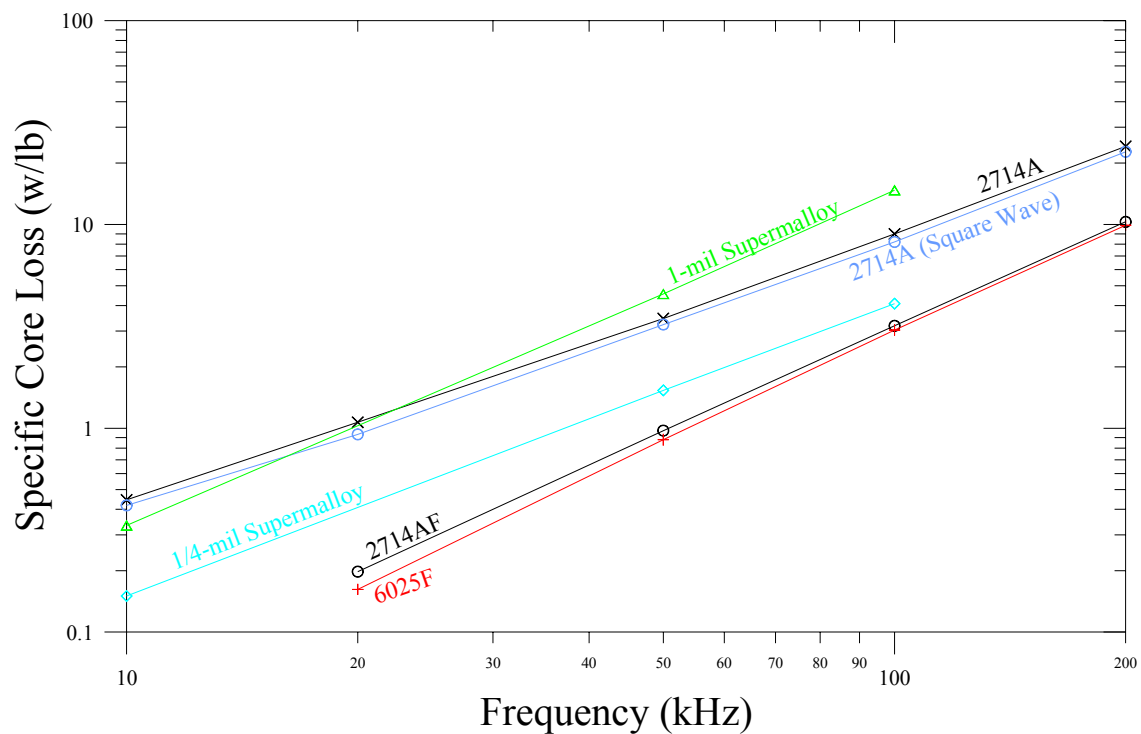

Figure 16.—Comparison of the specific core loss versus frequency of different magnetic materials for sine wave voltage excitation, except where noted, at 23 °C and B_M = 0.1 Tesla.

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13. ABSTRACT (*Maximum 200 words*)

Magnetic component designers are always looking for improved soft magnetic core materials to increase the efficiency, temperature rating and power density of transformers, motors, generators and alternators, and energy density of inductors. In this paper, we report on the experimental investigation of commercially available cobalt-based amorphous alloys which, in their processing, were subjected to two different types of magnetic field anneals: A longitudinal magnetic field anneal or a transverse magnetic field anneal. The longitudinal field annealed material investigated was Metglas® 2714A. The electrical and magnetic characteristics of this material were investigated over the frequency range of 1 to 200 kHz and temperature range of 23 to 150 °C for both sine and square wave voltage excitation. The specific core loss was lower for the square than the sine wave voltage excitation for the same maximum flux density, frequency and temperature. The transverse magnetic field annealed core materials include Metglas® 2714AF and Vacuumschmelze 6025F. These two materials were experimentally characterized over the frequency range of 10 to 200 kHz for sine wave voltage excitation and 23 °C only. A comparison of the 2174A to 2714AF found that 2714AF always had lower specific core loss than 2714A for any given magnetic flux density and frequency and the ratio of specific core loss of 2714A to 2714AF was dependent on both magnetic flux density and frequency. A comparison was also made of the 2714A, 2714AF, and 6025F materials to two different tape thicknesses of the polycrystalline Supermalloy material and the results show that 2714AF and 6025F have the lowest specific core loss at 100 kHz over the magnetic flux density range of 0.1 to 0.4 Tesla.

14. SUBJECT TERMS

Specific core loss; B-H hysteresis loop; Magnetic field anneal; Sine wave voltage excitation; Square wave; Voltage excitation; Permalloy; High frequency; Magnetic measurements; Magnetic cores

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