

In House Shock Prediction Tool

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Daniel Kaufman
Mechanical Systems Analysis & Simulation Branch
NASA Goddard Space Flight Center
Greenbelt, MD 20771, USA
Daniel.S.Kaufman@nasa.gov

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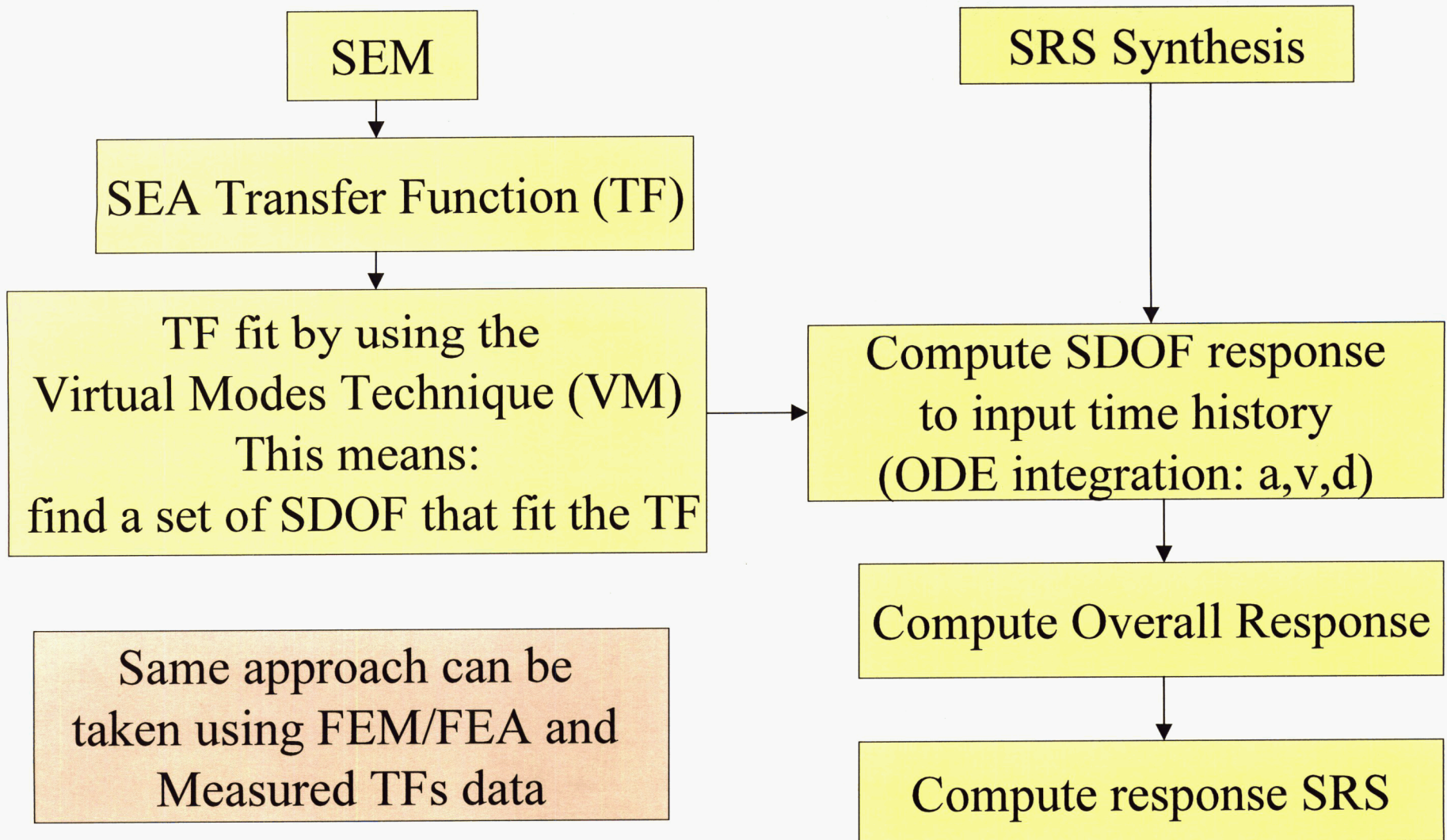
Background

- For decades and still today the preferred tool for shock prediction at NASA GSFC is a semi empirical approach based originally in a study for NASA Goddard NAS5-15208: “Aerospace Systems Pyrotechnic Shock Data”, Ground Test and Flight, March 1970, and subsequent empirical data.
- NASA also sponsored in the past Shock Prediction Technology, for example the TRANSTAR (TRAnsient ANalysis STorage And Retrieval) which is a database management and prediction system. We no longer use it at GSFC although it may still be used by the industry.
- The Mechanical Systems Analysis Branch (Code 542) has an AutoSEA2 license for vibroacoustic analysis. AutoSEA2 is currently owned by the ESI Group.

Background

- The ESI Group has expanded the use of AutoSEA2 by integrating the PowerSurge code which was licensed under an agreement with Military Technology Inc.
- The Shock Module from ESI Group allows to extend the use of AutoSEA2 models to shock prediction.
- Code 542 does not have the Shock Module Expansion due to budget limitations. Swales Aerospace purchased the Module and used it in support of various shock problems at NASA.
- Code 542 decided to use existing in house routines and try to develop the technique. We asked and received from Swales data to benchmark our in house effort.

Technical Approach



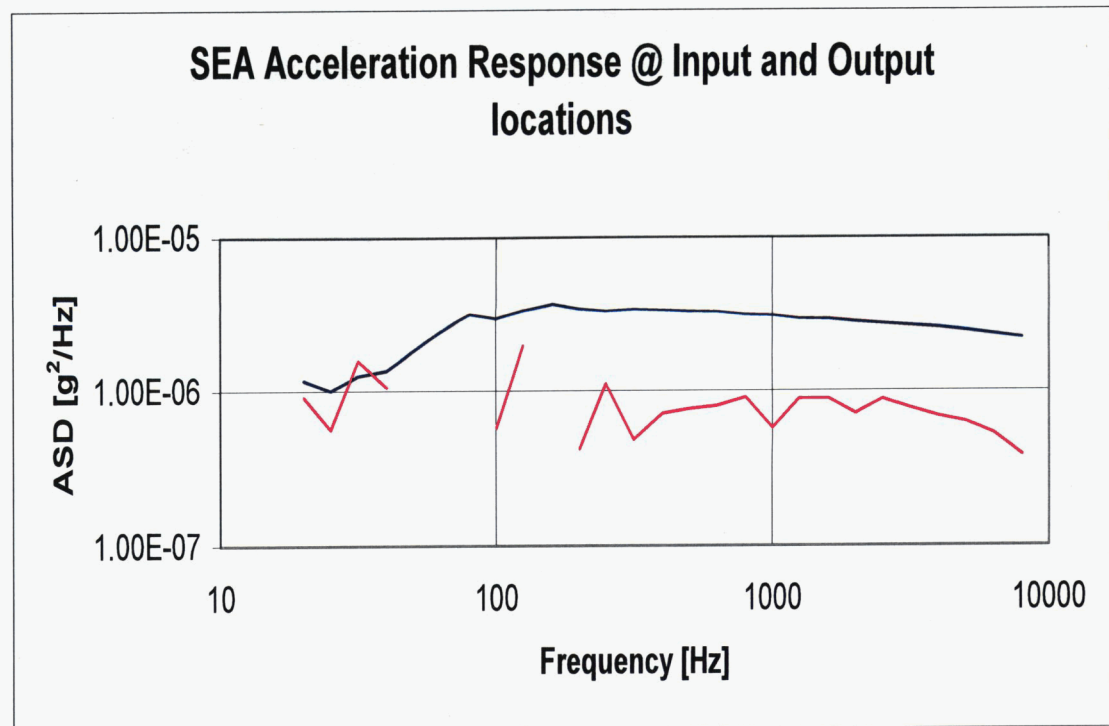
SEA Case

- Swales provided the necessary data to benchmark the problem. This is: Input SRS, SEM, input and output locations and SRS response.
- Code 542 took the SEM, identified input and output locations and computed a psd response (SC shear panel) due to an unitary force at the input location.
- An acceleration TF [g/g] was obtained by:

$$TF = \text{SQRT}(\text{PSDout} / \text{PSDin})$$

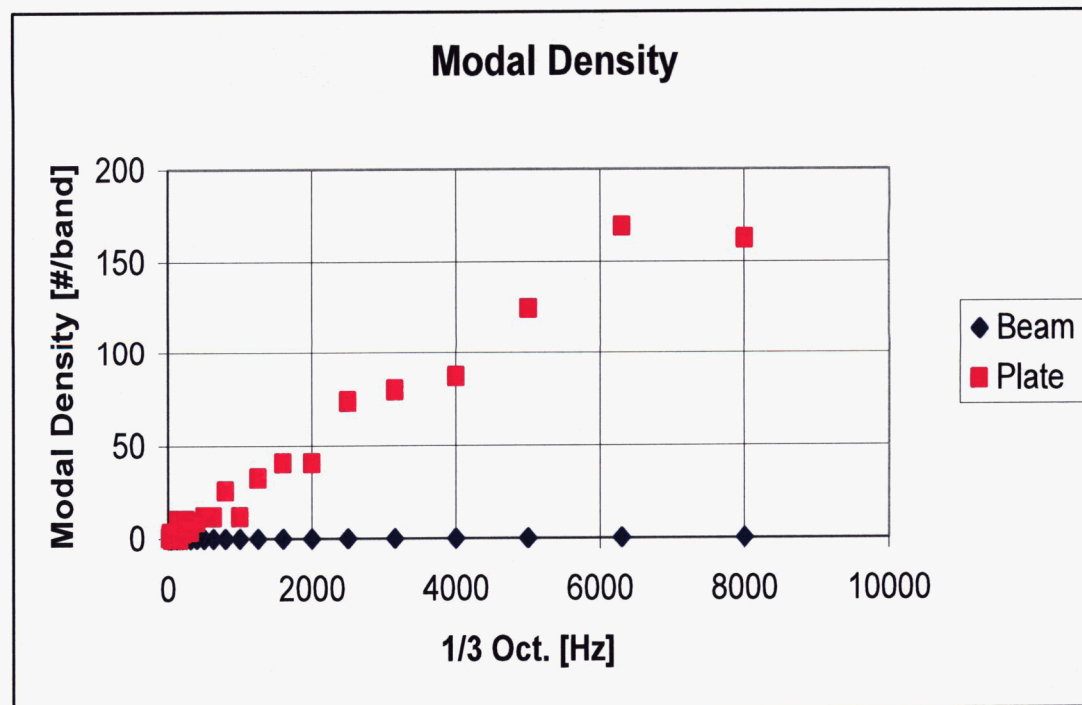
SEA Results

	Beam 990	Plate 936
	Extensional	Flexural
Frequency(Hz)	ASD(g ² /HZ)	ASD(g ² /Hz)
20	1.17E-06	9.11E-07
25	1.00E-06	5.66E-07
31.5	1.25E-06	1.56E-06
40	1.34E-06	1.06E-06
50	1.79E-06	0
63	2.39E-06	0
80	3.12E-06	0
100	2.89E-06	5.78E-07
125	3.32E-06	1.94E-06
160	3.71E-06	0
200	3.42E-06	4.22E-07
250	3.30E-06	1.11E-06
315	3.40E-06	4.84E-07
400	3.34E-06	7.13E-07
500	3.28E-06	7.64E-07
630	3.24E-06	7.93E-07
800	3.09E-06	8.98E-07
1000	3.04E-06	5.72E-07
1250	2.88E-06	8.84E-07
1600	2.84E-06	8.84E-07
2000	2.74E-06	7.08E-07
2500	2.65E-06	8.75E-07
3150	2.57E-06	7.68E-07
4000	2.51E-06	6.77E-07
5000	2.40E-06	6.25E-07
6300	2.28E-06	5.30E-07
8000	2.15E-06	3.84E-07

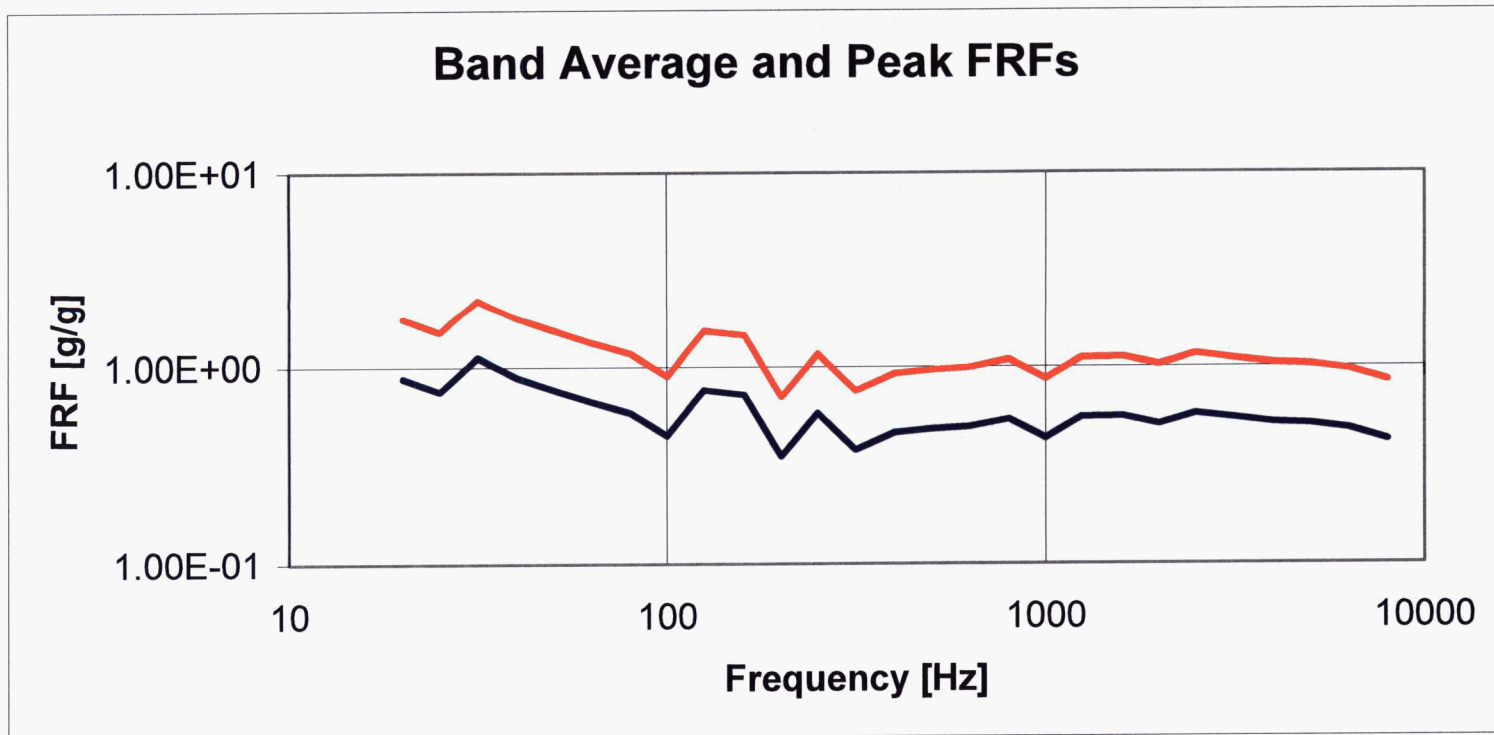


SEA Results

Frequency (Hz)	Modal Density	
	Beam 990	Plate 936
	Extensional Modes	Flexural Modes
20	0	1
25	0	1
32	0	3
40	0	3
50	0	0
63	0	0
80	0	0
100	0	2
125	0	10
160	0	0
200	0	3
250	0	10
315	0	4
400	0	9
500	0	12
630	0	12
800	0	26
1000	0	12
1250	0	33
1600	0	41
2000	0	41
2500	0	74
3150	0	80
4000	0	87
5000	0	125
6300	0	169
8000	0	163
total # modes		921

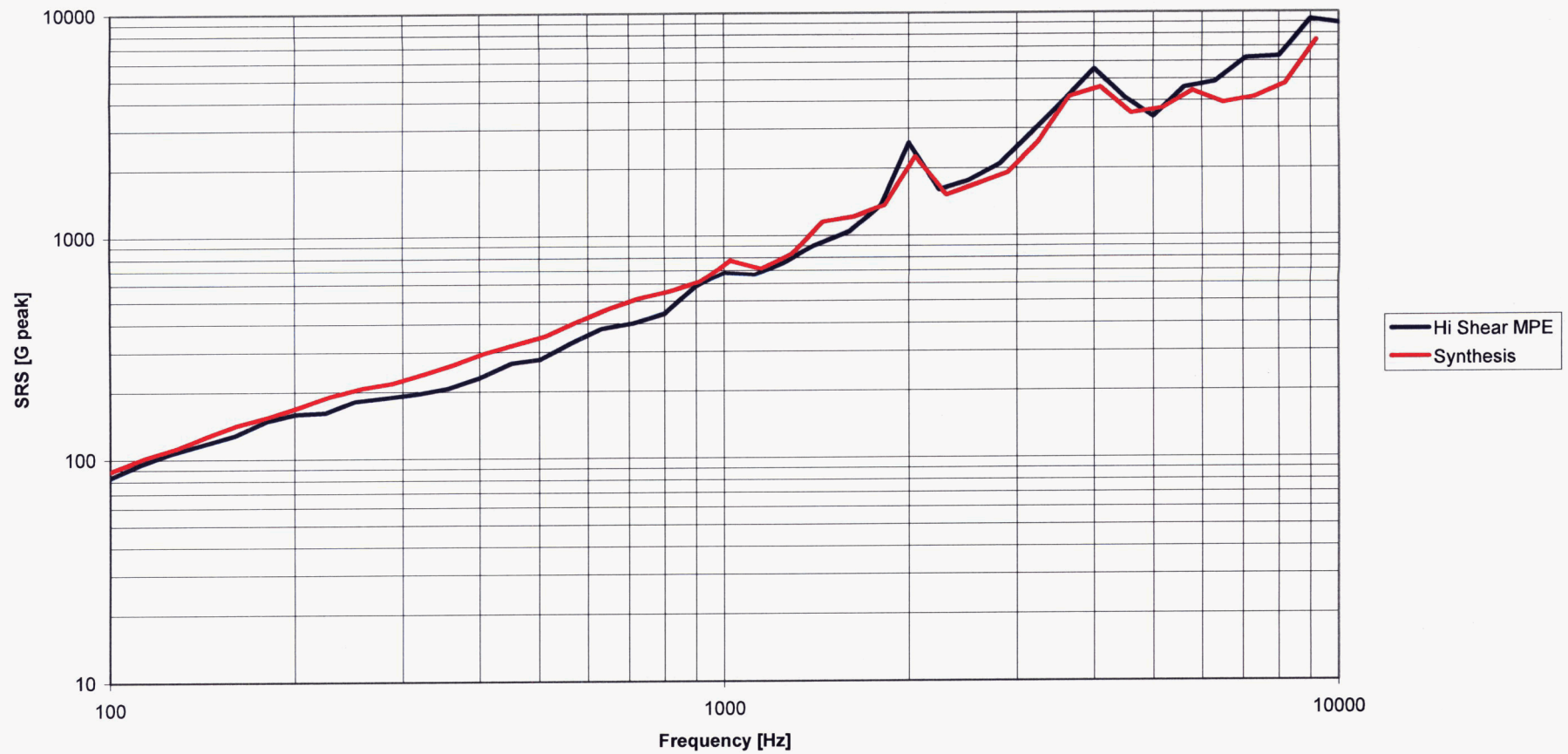


SEA Results



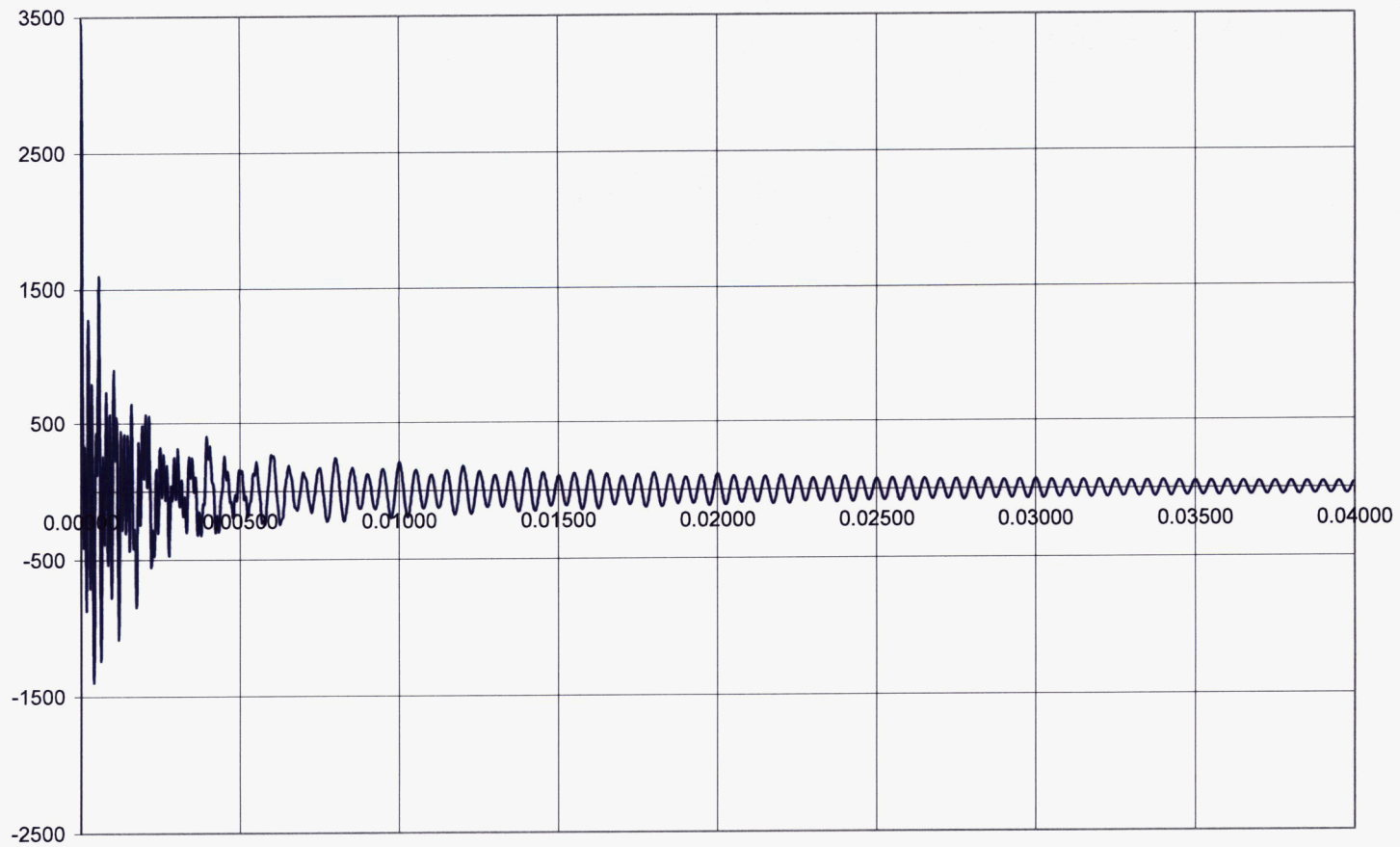
SEA Results

Beam Input: SRS Synthesis

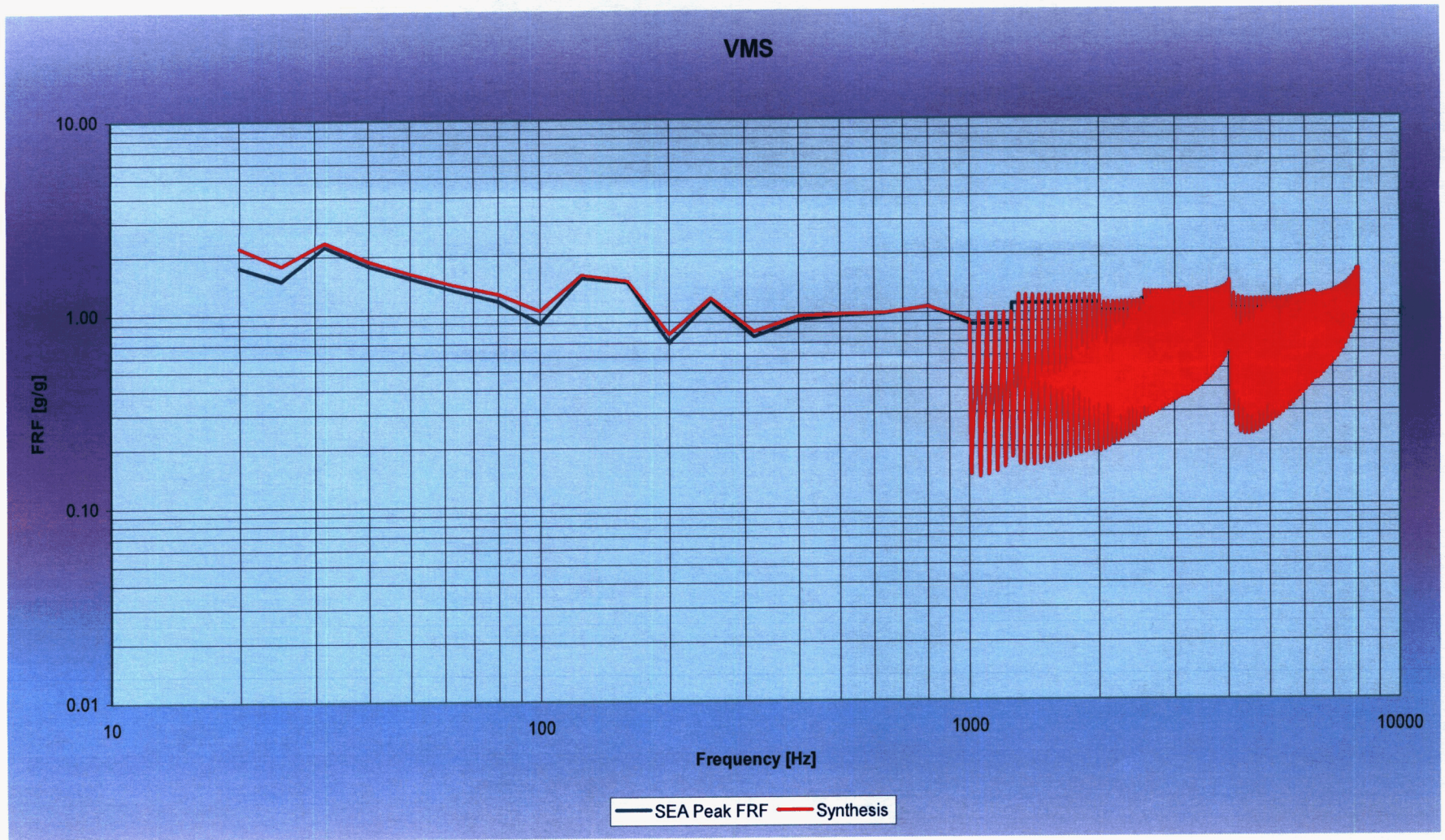


SEA Results

Synthesized Acceleration Input

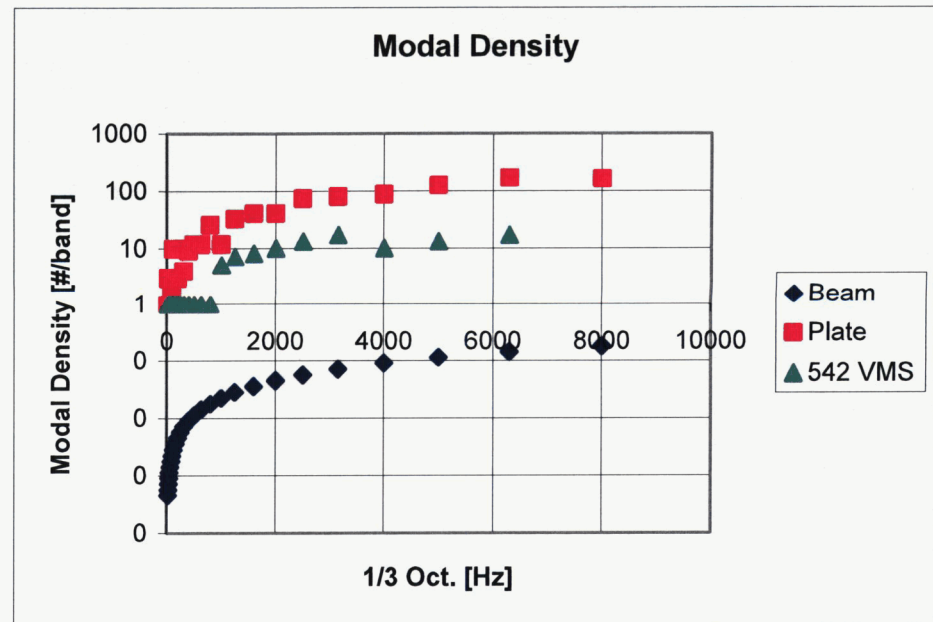


SEA Results



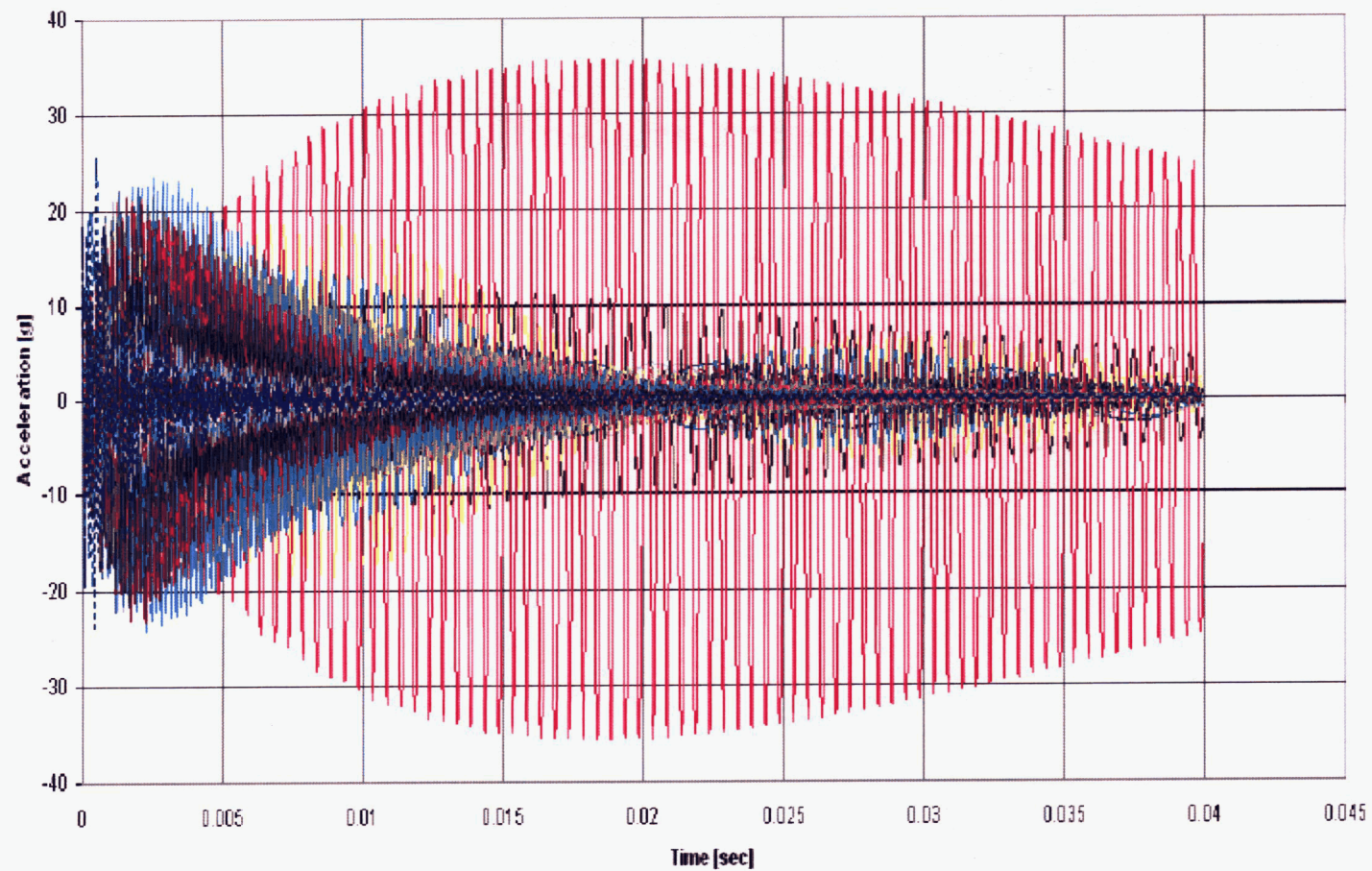
SEA Results

- # Modes Used=118
- Mass Normalized
- Outputs are:
 - Mode#
 - Frequency
 - Damping
 - Effective Weight



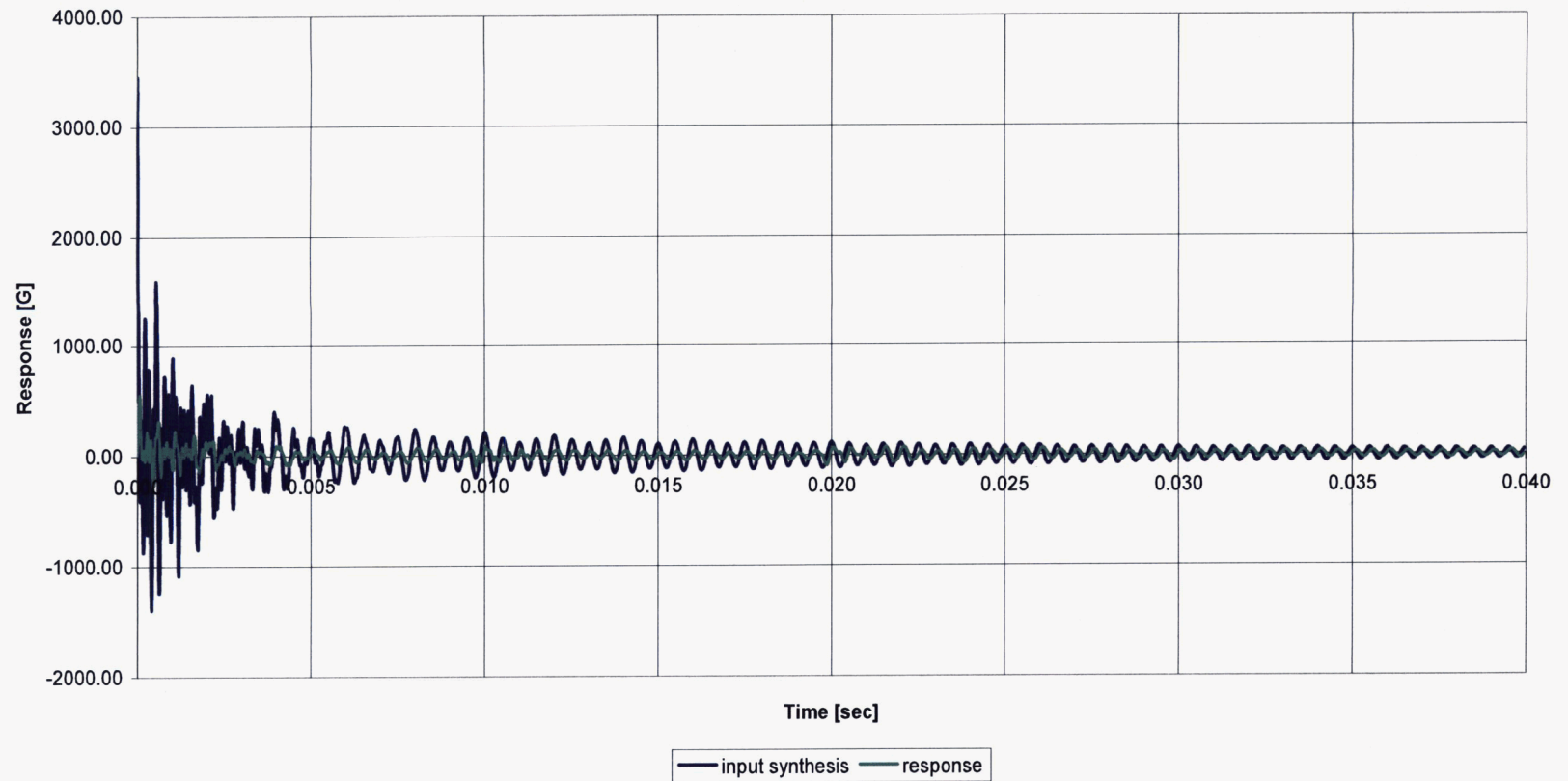
SEA Results

Acceleration Responses



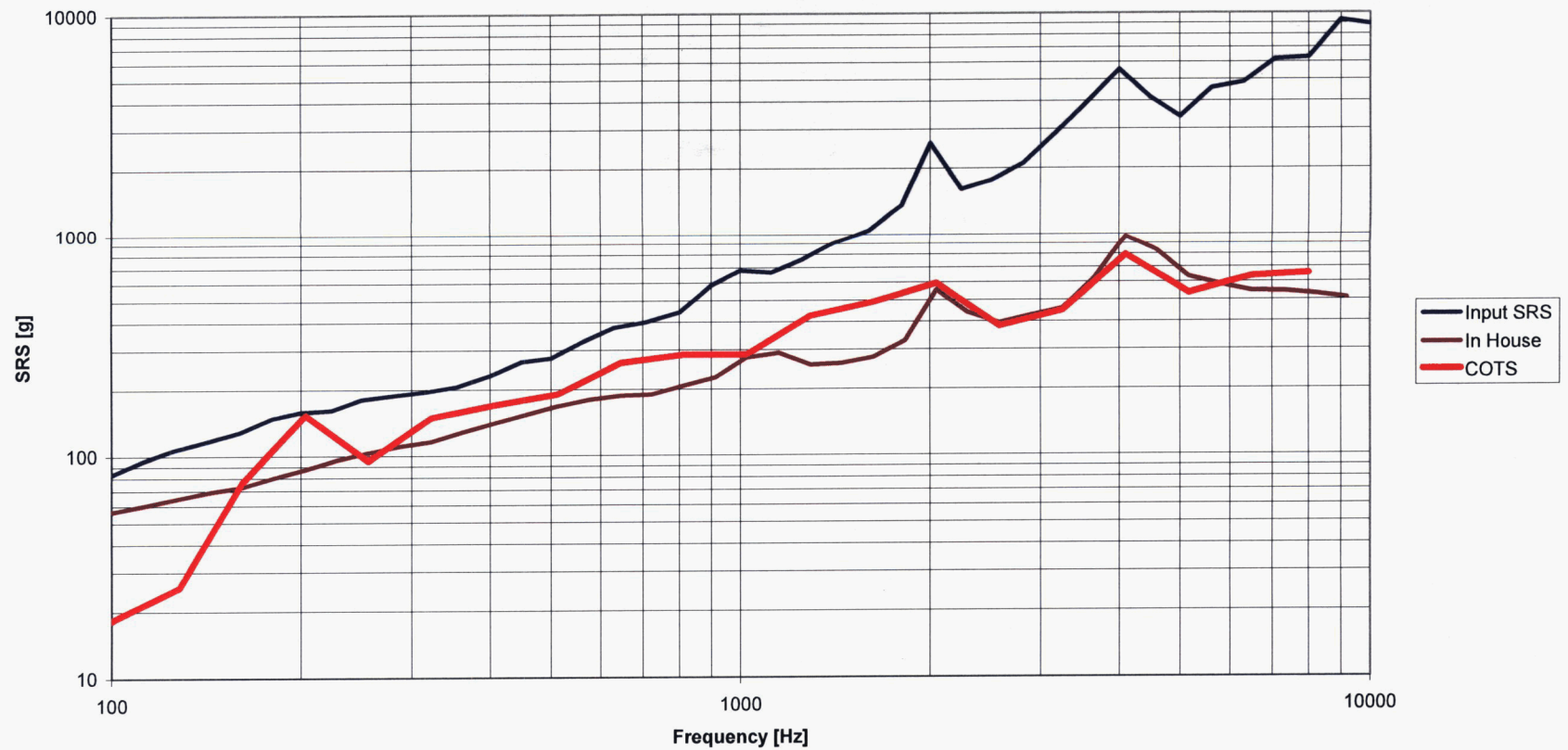
SEA Results

Panel Response, Input at Beam



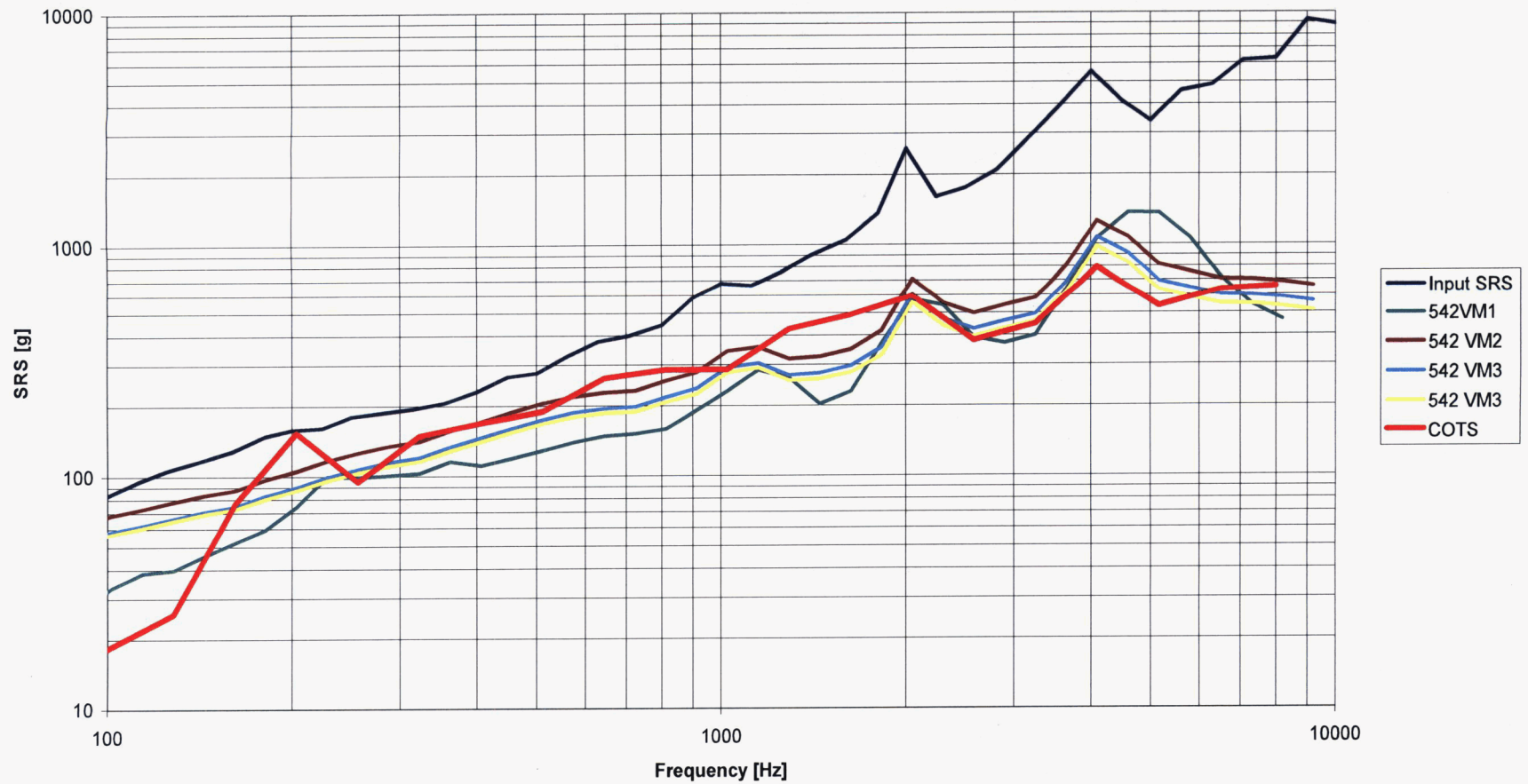
SEA Results

SRS Comparison (COTS and In House)



SEA Results

SRS Comparison (COTS and In House)



Conclusions

- Used existing GSFC in house routines to perform an equivalent solution to the COTS Shock Module.
- The results are very sensitive to the VMS process.
- Responses look good enough to justify the time investment in improving the code.
- The VMS process needs more work and further validation versus COTS code and/or test measurements.
- The in house routines still have to be integrated and automated.
- By applying the method to FEMs and SEMs, results can be combined to get an improved LF/HF solution.