

NASA/TM-2008-215551



# Guidance and Control Software Project Data

## *Volume 2: Development Documents*

*Edited by*  
*Kelly J. Hayhurst*  
*Langley Research Center, Hampton, Virginia*

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December 2008

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National Aeronautics and  
Space Administration

Langley Research Center  
Hampton, Virginia 23681-2199

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## Abstract

*The Guidance and Control Software (GCS) project was the last in a series of software reliability studies conducted at Langley Research Center between 1977 and 1994. The technical results of the GCS project were recorded after the experiment was completed. Some of the support documentation produced as part of the experiment, however, is serving an unexpected role far beyond its original project context. Some of the software used as part of the GCS project was developed to conform to the RTCA/DO-178B software standard, "Software Considerations in Airborne Systems and Equipment Certification," used in the civil aviation industry. That standard requires extensive documentation throughout the software development life cycle, including plans, software requirements, design and source code, verification cases and results, and configuration management and quality control data. The project documentation that includes this information is open for public scrutiny without the legal or safety implications associated with comparable data from an avionics manufacturer. This public availability has afforded an opportunity to use the GCS project documents for DO-178B training. This report provides a brief overview of the GCS project, describes the 4-volume set of documents and the role they are playing in training, and includes the development documents from the GCS project.*

## 1 Introduction and Background on Software Error Studies

As the pervasiveness of computer systems has increased, so has the desire and obligation to establish the reliability of these systems. Reliability estimation and prediction are standard activities in many engineering projects. For the software aspects of computer systems, however, reliability estimation and prediction have been topics of dispute, especially for safety-critical systems. A primary challenge is how to accurately model the failure behavior of software such that numerical estimates of reliability have sufficient credibility for systems where the probability of failure needs to be quite small, such as in commercial avionics systems (ref. 1). A second challenge is how to gather sufficient data to make such estimates. Software reliability models are not used in the civil aviation industry, for example, because "currently available methods do not provide results in which confidence can be placed to the level required for this purpose." (ref. 2)

In an effort to develop methods to credibly assess the reliability of software for safety-critical avionics applications, Langley Research Center initiated a Software Error Studies program in 1977 (ref. 3). A major focus of those studies was on generating significant quantities of software failure data through controlled experimentation to better understand software failure processes. The intent of the Software Error Studies program was to incrementally increase complexity and realism in a series of experiments so that the final study would have statistically valid results, representative of actual software development processes.

The Software Error Studies program started with initial investigations by the Aerospace Corporation to define software reliability measures and data collection requirements (ref. 4-6).

Next, Boeing Computer Services (BCS) and the Research Triangle Institute (RTI) conducted several simple software experiments with aerospace applications including missile tracking, launch interception, spline function interpolation, Earth satellite calculation, and pitch axis control (refs. 7-11). The experiment design used in these studies generally involved a number of programmers (denoted  $n$ ) who independently generated computer code from a given specification of the problem to produce  $n$  versions of a program. In these experiments, no particular software development standards or life-cycle models were followed. Because the problems were relatively small and simple, the versions were compared to a known error-free version of the program to obtain information on software errors.

Although the initial experiments were small and simplistic compared with real-world avionics development, they yielded some interesting results that have influenced software reliability modeling. The BCS and RTI studies showed widely varying error rates for faults. This finding refuted a common assumption in early software reliability growth models that faults produced errors at equal rates. These studies also provided evidence of fault interaction where one fault could mask potentially erroneous behavior from another fault, or where two or more faults together cause errors when alone they would not. (ref. 12) Additional investigations with  $n$ -version programs (ref. 13) found that points in the input space that cause an error can cluster and form "error crystals". Extrapolating this finding to aerospace applications, where input signals tend to be continuous in nature, the error crystals may manifest themselves as clusters of successive faults that could have unintended consequences. (ref. 14)

The last project in the Software Error Studies program was the Guidance and Control Software (GCS) project. It built on the previous experiments in two ways: (1) by requiring that the software specimens for the experiment be developed in compliance with current software development standards, and (2) by increasing the complexity of the application problem (ref. 15). At the time of the GCS project, the RTCA/DO-178B guidelines, "Software Considerations in Airborne Systems and Equipment Certification," (ref. 2) were the primary standard sanctioned by the Federal Aviation Administration (FAA) for developing software to be approved for use in commercial aircraft equipment (ref. 16). The DO-178B document describes objectives and design considerations to be used for the development of software as well as verification, configuration management, and quality assurance activities to be performed throughout the development process. The DO-178B guidelines were selected as the software development standard to be used for the GCS specimens.

The software application selected for the GCS project, as the title indicates, is a guidance and control function for controlling the terminal descent trajectory of a planetary lander vehicle. This terminal descent trajectory is the same fundamental trajectory referred to as the "seven minutes of terror" in the entry, descent, and landing phase of a planetary mission, such as the recent Phoenix Mars Lander (ref. 17). For the GCS project, the software requirements were reverse engineered from a simulation program used to study the probability of success of the original NASA Viking Lander mission to Mars in the 1970s (ref. 18). It is important to emphasize that the software requirements documented for the GCS project, while realistic, are not the actual software requirements used for NASA's Viking Lander or any other planetary landers.

For the GCS experiment, two<sup>1</sup> teams of software engineers were each tasked to independently design, code, and verify a GCS program, following the software development guidance in DO-178B, as closely as possible. In addition to those teams, another GCS version was produced, without the constraint of compliance with DO-178B, to aid development and verification of the requirements and simulation environment. Once all versions were complete, data on residual

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<sup>1</sup> The original plan for the GCS project called for three independent teams. Due to funding constraints, only two teams were able to complete the project.



errors was supposed to be collected by running all the versions simultaneously in a simulation environment, and using any discrepancies among the results of the versions as possible indications of errors.

Results of the operational simulations and data collection are described in (ref. 15). The purpose of this report is not to repeat those results, but to disseminate some of the project documentation that has an unanticipated utility beyond its original project context. The project documentation of interest is the documentation developed by the teams required to comply with the DO-178B standard. That standard requires extensive records of all of the software development life cycle activities. For the GCS project, those records included 18 documents consisting of life cycle plans, development products including requirements and source code, verification cases and results, and configuration management and quality control data. Comparable data from a commercial avionics system would not be available for public review because of proprietary and other legal considerations. The GCS project documentation is not subject to those considerations because it is not data from an actual operational, or even prototype, system. But, the data has sufficient realism to provide a window into the types of activities and data involved in the production of DO-178 compliant software, which makes the GCS documentation desirable from a training perspective.

The remainder of this report provides a brief overview of aspects of the GCS project relevant to using the documentation for training. This information includes a description of the GCS application, a synopsis of the software development processes used to follow the DO-178B guidance, and the data that was generated as a result. Because the complete set of compliance documents is large, the documents have been divided into four sets (planning, development, verification, and other integral process documents) contained in separate volumes of this report. Volume 2 includes in Appendices A-C the requirements, design, and source code generated as part of the development processes.

## **2 Guidance and Control Software Application**

The requirements for the GCS application focus on two primary functions: (1) to provide guidance and engine control of the lander vehicle during its terminal phase of descent onto the planet's surface, and (2) to communicate sensory information to an orbiting platform about the vehicle and its descent. Figure 1 shows a sketch of the lander vehicle, taken from (ref. 18), noting the location of the terminal descent propulsion systems.

The guidance package for the lander vehicle contains sensors that obtain information about the vehicle state and environment, a guidance and control computer, and actuators providing the thrust necessary for maintaining a safe descent. The vehicle has three accelerometers (one for each body axis), one Doppler radar with four beams, one altimeter radar, two temperature sensors, three strapped-down gyroscopes, three opposed pairs of roll engines, three axial thrust engines, one parachute release actuator, and a touch down sensor. The vehicle has a hexagonal, box-like shape; three legs and a surface sensing rod protrude from its undersurface.

In general, the requirements for the planetary lander only concern the final descent to the surface. Figure 2 shows a sketch of the phases of the terminal descent trajectory.

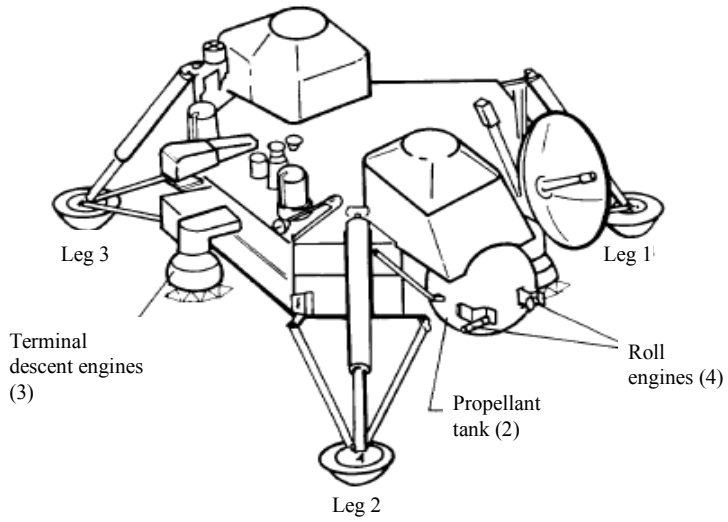


Figure 1. Lander with Terminal Descent Propulsion Systems

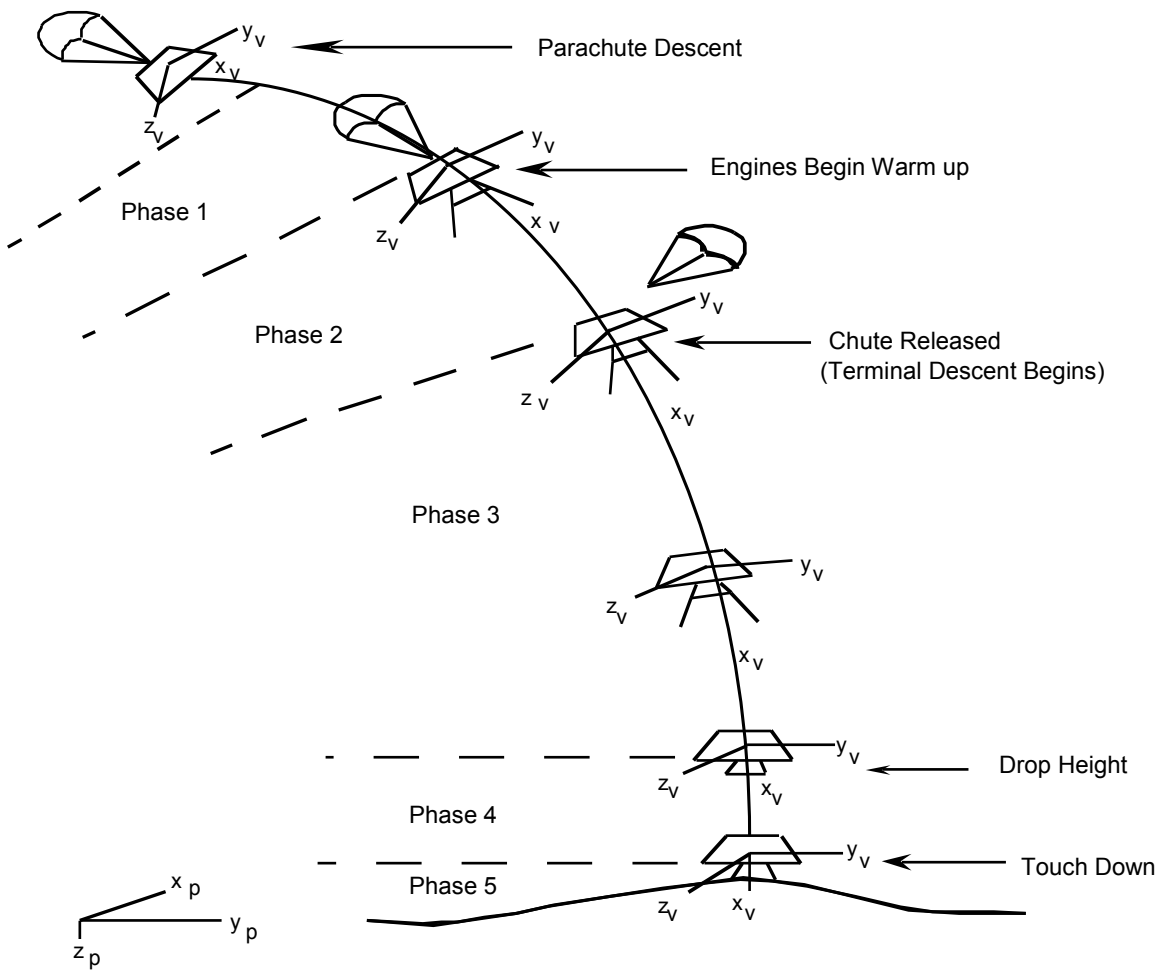


Figure 2. A Typical Terminal Descent Trajectory

After the lander has dropped from orbit, the software controls the engines of the vehicle to the surface of a planet. The initialization of the GCS starts the sensing of vehicle altitude. When a predefined engine ignition altitude is sensed by the altimeter radar, the GCS begins guidance and control of the lander. The axial and roll engines are ignited; while the axial engines are warming up, the parachute remains connected to the vehicle. During this engine warm-up phase, the aerodynamics of the parachute dictate the vehicle's trajectory. Vehicle attitude is maintained by firing the engines in a throttled-down condition. Once the main engines become hot, the parachute is released and the GCS performs an attitude correction maneuver and then follows a controlled acceleration descent until a predetermined velocity-altitude contour is crossed. The GCS then attempts to maintain the descent of the lander along this predetermined velocity-altitude contour. The lander descends along this contour until a predefined engine shut off altitude is reached or touchdown is sensed. After all engines are shut off, the lander free-falls to the surface.

The software requirements for this guidance and control application are contained in a document called the *Guidance and Control Development Specification* (in Volume 2). As mentioned earlier, the initial requirements for this application were reverse engineered from a simulation program used to study the probability of success of the original NASA Viking Lander mission to Mars. Prior to use in the experiment, the requirements were revised to make them suitable for use in an *n*-version software experiment. Each of the GCS programs for the experiment were developed from the same requirements document.

### **3 Software Life Cycle Processes and Documentation**

Having some of the project teams adhere to the DO-178B guidelines as they created a software version for the experiment was a significant element of the GCS project, requiring the development and tracking of numerous software engineering artifacts not normally associated with a software engineering experiment. The purpose of DO-178B is to provide guidelines for the production of software such that the completed implementation performs its intended function with a level of confidence in safety satisfactory for airworthiness. Along with the production of software is the generation of an extensive set of documents recording the production activities.

DO-178B defines software development activities and objectives for the development life cycle of the software, and the evidence that is needed to show compliance. The life-cycle processes are divided into planning, development, and integral processes. The planning process defines and coordinates the software development processes and the integral processes. The software development processes involve identification of software requirements, software design and coding, and integration; that is, the development processes directly result in the software product. Finally, the integral processes function throughout the software development processes to ensure integrity of the software products. The integral processes include software verification, configuration management, and quality assurance processes. Section 11 of DO-178B describes data that should be produced as evidence of performing all of the life cycle process activities.

For the GCS project, some of this data was common for all of the teams, and other data was intended to be specific to each team. For example, each team worked with the same plans, standards, and requirements. Then, each individual team was responsible for independently developing their own design, code, and corresponding verification data. To distinguish the versions, each team was assigned a planetary name: Mercury, Venus, and Pluto<sup>2</sup>.

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<sup>2</sup> At the time the GCS experiment was conducted, Pluto had not yet been relegated to non-planet status.

Table 1. Life Cycle Data

Planning Process Documents	Development Process Documents	Integral Process Documents
<ul style="list-style-type: none"> <li>• <b>Plan for Software Aspects of Certification</b></li> <li>• <b>Software Development Plan</b></li> <li>• <b>Software Verification Plan</b></li> <li>• <b>Software Configuration Management Plan</b></li> <li>• <b>Software Quality Assurance Plan</b></li> <li>• <b>Software Requirements Standards</b></li> <li>• <b>Software Design Standards</b></li> <li>• <b>Software Code Standards</b></li> </ul>	<ul style="list-style-type: none"> <li>• <b>Software Requirements Data</b></li> <li>• <b>Design Description</b></li> <li>• <b>Source Code</b></li> <li>• <b>Executable Object Code</b></li> </ul>	<ul style="list-style-type: none"> <li>• <b>Software Verification Cases and Procedures</b></li> <li>• <b>Software Verification Results</b></li> <li>• <b>Software Life Cycle Environment Configuration Index</b></li> <li>• <b>Software Configuration Index</b></li> <li>• <b>Problem Reports</b></li> <li>• <b>Software Configuration Management Records</b></li> <li>• <b>Software Quality Assurance Records</b></li> <li>• <b>Software Accomplishment Summary</b></li> </ul>

The DO-178B data associated with the development of the Pluto version of the GCS was selected for publication. For dissemination purposes, the Pluto data was divided into the following 4 subsets:

Volume 1: Planning Documents

- *Plan for Software Aspects of Certification of the Guidance and Control Software Project*
- *Software Configuration Management Plan for the Guidance and Control Software Project*
- *Software Quality Assurance Plan for the Guidance and Control Software Project*
- *Software Verification Plan for the Guidance and Control Software Project*
- *Software Development Standards for the Guidance and Control Software Project*

Volume 2: Development Documents

- *Guidance and Control Software Development Specification*
- *Design Description for the Pluto Implementation of the Guidance and Control Software*
- *Source Code for the Pluto Implementation of the Guidance and Control Software*

Volume 3: Verification Documents

- *Software Verification Cases and Procedures for the Guidance and Control Software Project*
- *Software Verification Results for the Pluto Implementation of GCS*
- *Review Records for the Pluto Implementation of the Guidance and Control Software*
- *Test Results Logs for the Pluto Implementation of the Guidance and Control Software*

#### Volume 4: Other Integral Processes Documents

- *Software Accomplishment Summary for the Guidance and Control Software Project*
- *Software Configuration Index for the Guidance and Control Software Project*
- *Problem Reports for the Pluto Implementation of the Guidance and Control Software*
- *Support Documentation Change Reports for the Guidance and Control Software Project*
- *Configuration Management Records for the Guidance and Control Software Project*
- *Software Quality Assurance Records for the Guidance and Control Software Project*

Appendices A-C contain the original development documents for the GCS project. The *Guidance and Control Software Development Specification*, in Appendix A, contains all of the high-level requirements for the guidance and control application, as well as instructions for interfacing with the experiment's simulator. The low-level requirements and architecture are contained in the *Design Description for the Pluto Implementation of the Guidance and Control Software* in Appendix B. The design was developed using a structured analysis tool called *Teamwork* from Cadre Technologies. Finally, Appendix C contains the *Source Code for the Pluto Implementation of the Guidance and Control Software* with the Fortran source code for the Pluto implementation.

The content of the documents in the appendices has not been altered from the original versions produced during the project.

## 4 Role in Training

At the time of the GCS project, there was no publicly available information, such as templates, or examples, or training courses, to help a novice developer generate the type of evidence that a certifying authority would expect to see to demonstrate compliance with DO-178B. As mentioned earlier, compliance data from a real avionics system is not typically available for public review because of various legal and safety considerations. For example, an avionics manufacturer would likely consider the design and implementation of a system to be proprietary. Those considerations do not apply to the data from the GCS project, because neither the requirements nor the software versions represent an actual system with safety, liability, or other considerations.

In addition to the availability of data, the GCS requirements and DO-178B compliance data are sufficiently realistic to serve as an example of a DO-178B project: one that is small enough in scale to be studied in a training course. The GCS documentation provides a window into the activities and data produced throughout the development life cycle to comply with DO-178B. Because the Federal Aviation Administration (FAA) was aware of the GCS project, they recognized the potential value of the documentation for training. The FAA has designed software training to include a case study portion that addresses avionics software issues that arise from the application of the DO-178B guidelines. The case study gives students the opportunity to use auditing techniques to identify flaws in lifecycle data. Because the GCS data was produced by novices, there are plenty of flaws to find.

## 5 Summary

From 1977-1994, NASA Langley Research Center conducted a Software Error Studies program that generated data that provided insights into the software failure process and into conducting software engineering experiments as well. The GCS project was the final experiment in that program. A unique feature of the GCS project was the requirement for some of the

software specimens used in the experiment to conform to the RTCA/DO-178B software standard, "Software Considerations in Airborne Systems and Equipment Certification," used in the civil aviation industry. The project documentation produced to meet that requirement has had the unanticipated benefit of serving as case study material in software certification training long after the conclusion of the original experiment. Volume 2 of this report contains all of the development artifacts from the GCS project.: requirements, design, and source code Other volumes of this report contain the rest of the GCS compliance data including planning, verification, and configuration management and quality assurance documents.

## 6 References

1. Littlewood, Bev, and Strigini, Lorenzo, Software Reliability and Dependability: a Roadmap, 22nd International Conference on Software Engineering, Future of Software Engineering Track, June 4-11, 2000, Limerick Ireland, pp. 175 – 188.
2. Software Considerations in Airborne Systems and Equipment Certification. Doc. No. RTCA/DO-178B, RTCA, Inc., Dec. 1, 1992.
3. Finelli, George B.: NASA Software Failure Characterization Experiments. Reliability Engineering & System Safety, vol. 32, pp. 155–169, 1991.
4. Hecht, H.; Sturm, W. A.; and Tratner, S.: Reliability Measurement During Software Development. NASA CR-145205, 1977.
5. Hecht, H.: Measurement Estimation and Prediction of Software Reliability. NASA CR-145135, 1977.
6. Maxwell, F. D.: The Determination of Measures of Software Reliability. NASA CR-158960, 1978.
7. Nagel, Phyllis M.; and Skrivan, James A.: Software Reliability: Repetitive Run Experimentation and Modeling. NASA CR-165836, 1982.
8. Nagel, P. M.; Scholz, F. W.; and Skrivan, J. A.: Software Reliability: Additional Investigation Into Modeling With Replicated Experiments. NASA CR-172378, 1984.
9. Dunham, Janet R.: Experiments in Software Reliability: Life-Critical Applications. IEEE Transactions on Software Engineering, vol. SE-12, no. 1, Jan. 1986, pp. 110–123.
10. Dunham, J. R.; and Lauterbach, L. A.: An Experiment in Software Reliability Additional Analyses Using Data From Automated Replications. NASA CR-178395, 1987.
11. Dunham, Janet R.; and Pierce, John L.: An Empirical Study of Flight Control Software Reliability. NASA CR-178058, 1986.
12. Dunham, Janet R.; and Finelli, George B., Real-Time Software Failure Characterization, IEE Aerospace and Electronic Systems Magazine, pp. 38-44, November 1990.
13. Ammann, P. and Knight, J.: "Data Diversity: An Approach To Software Fault Tolerance", Digest of Papers FTCS-17: The 17th Annual International Symposium on Fault Tolerant Computing, Pittsburg, Pennsylvania, July 1987.
14. Finelli, George B, Results of Software Error-Data Experiments, AIAA/AHS/ASEE Aircraft Design, Systems and Operations Conference, September 7-9, 1988, Atlanta, Georgia, AIAA-88-4436.

15. Hayhurst, Kelly J., Framework for Small-Scale Experiments in Software Engineering, Guidance and Control Software Project: Software Engineering Case Study, NASA/TM-1998-207666, May 1998.
16. Federal Aviation Administration, Advisory Circular, 20-115B, January 11, 1993.
17. Tobin, Kate, NASA Preps for '7 Minutes of Terror' on Mars, May 23, 2008, <http://www.cnn.com/2008/TECH/space/05/23/mars.lander/index.html>.
18. Holmberg, Neil A.; Faust, Robert P.; and Holt, H. Milton: Viking '75 Spacecraft Design and Test Summary. Volume I—Lander Design. NASA RP-1027, 1980.

## **Appendix A: Guidance and Control Software Development Specification**

Version 2.3 with Formal Modifications 2.3-1 through 2.3-7

Authors: B. Edward Withers, Research Triangle Institute  
Bernice Becher, Lockheed Engineering & Sciences Corp.

This document was produced as part of Guidance and Control Software (GCS) Project conducted at NASA Langley Research Center. Although some of the requirements for the Guidance and Control Software application were derived from the NASA Viking Mission to Mars, this document does not contain data from an actual NASA mission.



## **A. ACKNOWLEDGEMENTS**

We wish to acknowledge Peter Padilla for his guidance and assistance in reviewing the requirements for this document and in recommending revisions so that the requirements might more accurately reflect those of an actual lander. We wish to acknowledge Earle Migneault for his work on earlier experiments of this type and for his vision in suggesting the application to be used in this experiment. We also wish to acknowledge Don C. Rich, Douglas S. Lowman, R. C. Buckland, Anita M. Shagnea, and Janet R. Dunham, all of Research Triangle Institute, for their earlier work on this project.

## **A. FOREWORD**

This specification defines a guidance and control system for a planetary landing vehicle during its terminal phase of descent. It is written for an experienced programmer with two or more years of full-time industrial programming experience using a scientific programming language. The programmer should have an adequate background, either through college courses or job training in mathematics, physics, differential equations, and numerical integration. The specification was written with the assumption that the implementation would be coded in FORTRAN; however, other languages can be used.

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## **A.1 INTRODUCTION**

### **PURPOSE OF THE GUIDANCE AND CONTROL SOFTWARE**

The Guidance and Control Software (GCS) represents the Viking lander (ref. A.20) on-board navigational software. The purpose of this software is to:

1. provide guidance and engine control of the vehicle (shown in Figure A.1.1) during its terminal phase of descent onto a surface and
2. communicate sensory information about the vehicle and its descent to some other receiving device.

A typical descent trajectory is shown in Figure A.1.2.

The initialization of the GCS starts the sensing of vehicle altitude. When a predefined engine ignition altitude is sensed by the altimeter radar, the GCS begins guidance and control of the vehicle. The axial engines are ignited; while the axial engines are warming up, the parachute remains connected to the vehicle. During this engine warm-up phase, the aerodynamics of the parachute dictate the trajectory followed by the vehicle. Vehicle attitude is maintained by firing the engines in a throttled-down condition. Once the main engines become hot, the parachute is released and the GCS performs an attitude correction maneuver and then follows a controlled acceleration descent until a predetermined velocity-altitude contour is crossed (see Figure A.5.1). The GCS then attempts to maintain the descent of the vehicle along this predetermined velocity-altitude contour. The vehicle descends along this contour until a predefined engine shut off altitude is reached or touchdown is sensed. After all engines are shut off, the vehicle free-falls to the surface.

### **VEHICLE CONFIGURATION**

The vehicle to be controlled is a guidance package containing sensors which obtain information about the vehicle state, a guidance and control computer, and actuators providing the thrust necessary for maintaining a safe descent. The vehicle has three accelerometers (one for each body axis), one doppler radar with four beams, one altimeter radar, two temperature sensors, three strapped-down gyroscopes, three opposed pairs of roll engines, three axial thrust engines, one parachute release actuator, and a touch down sensor. The vehicle has a hexagonal, box-like shape with three legs and a surface sensing rod protruding from its undersurface.

Figure A.1.1 THE LANDING VEHICLE DURING DESCENT

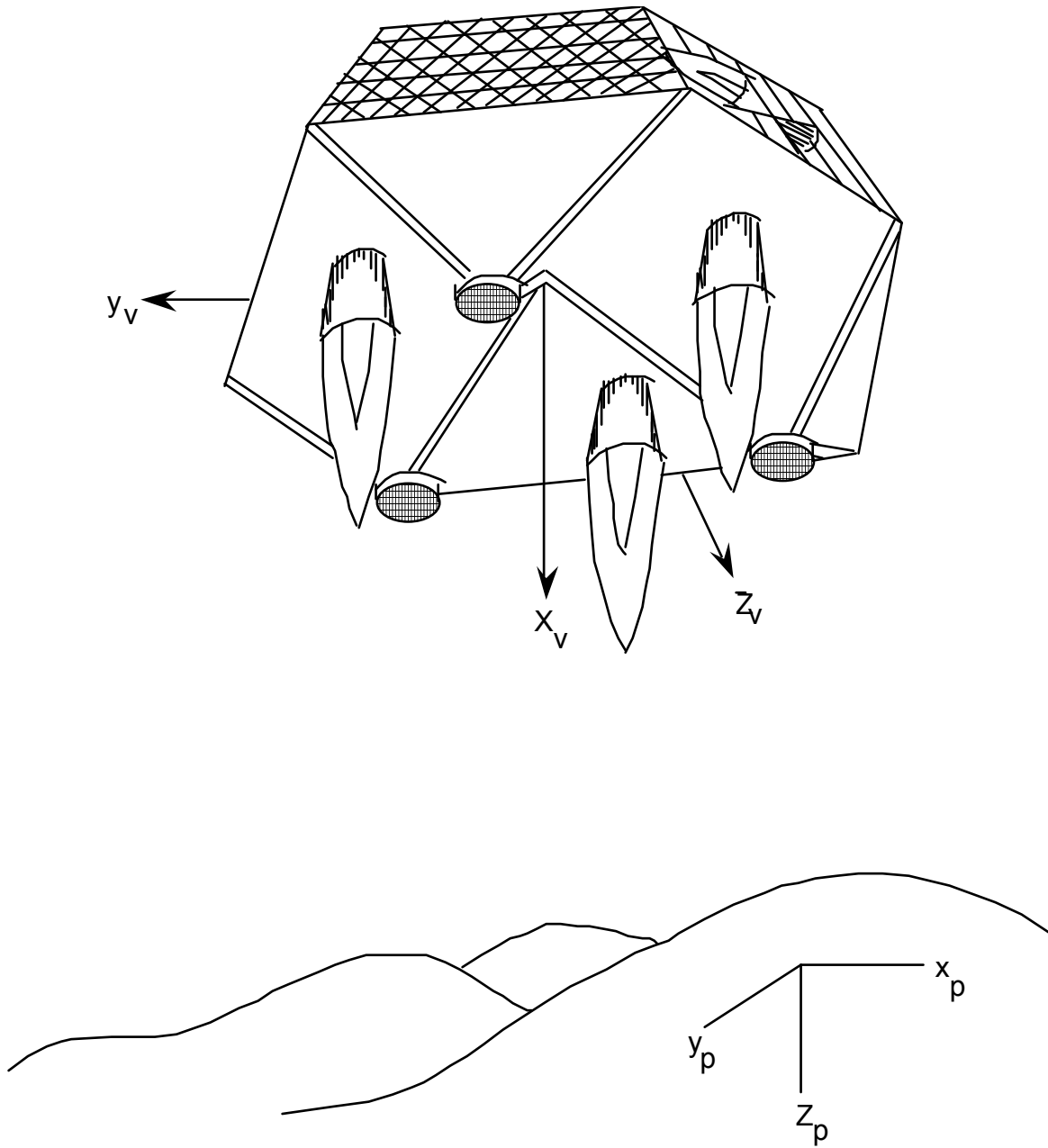
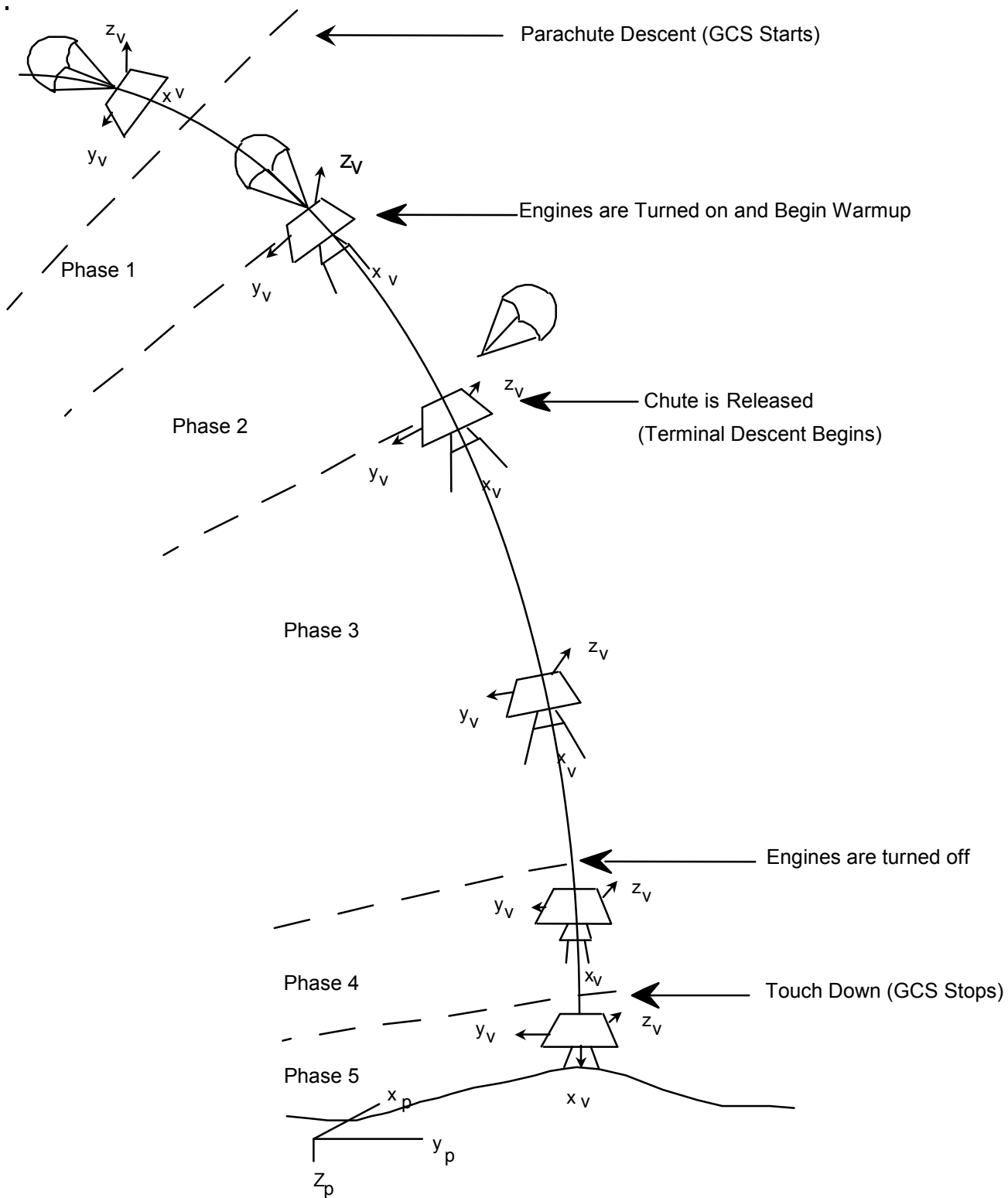


Figure A.1.2 A TYPICAL TERMINAL DESCENT TRAJECTORY





## TERMINAL DESCENT

Prior to the terminal descent phase, the vehicle falls with a parachute attached. This parachute is released seconds after the engines ignite, and terminal descent begins. During terminal descent, the vehicle follows a modified gravity-turn guidance law until a predetermined altitude is reached. The atmosphere introduces drag forces, including the random effects of wind. Independently throttled engines slow the vehicle down. These engines can control the vehicle's orientation, and roll engines control the vehicle's roll rate. Roll control is necessary to keep the doppler radars in lock and insure that the desired touch down attitude (land on two legs prior to the third) is maintained.

The velocity during descent follows the predetermined velocity-altitude contour. At a specific altitude above the planet surface, the vehicle is maintained at a constant descent velocity. Once the surface is sensed, all engines are shut down and the vehicle free falls to the surface.

## VEHICLE DYNAMICS

### Frames of Reference

Terminal descent is described in terms of two coordinate systems:

1. the surface-oriented coordinate system, and
2. the vehicle-oriented coordinate system.

In the surface coordinate system, the  $\bar{z}_p$  axis is viewed as normal to the surface and points down as shown in Figure A.1.2. The  $\bar{x}_p$  axis points north, and the  $\bar{y}_p$  points east.

By defining a *unit vector* as a vector of length equal to one unit along each axis in both the planetary and vehicular frames of reference, a relation between these two frames of reference may be established. Any vector can then be defined as a multiple of the unit vector along each of the axes defined in the frame of reference. Thus, the velocity of the vehicle  $\vec{V}$  may be defined in the vehicle's frame of reference as:  $V_{x_v}\hat{i}_v + V_{y_v}\hat{j}_v + V_{z_v}\hat{k}_v$ , where  $\hat{i}_v, \hat{j}_v,$  and  $\hat{k}_v$  are the unit vectors in the  $x, y,$  and  $z$  directions of the vehicles coordinate system (unit vectors are usually represented by lower case  $i, j,$  or  $k$  with a hat to show that they are unit vectors).  $V_{x_v}, V_{y_v},$  and  $V_{z_v}$  represent the components of the vehicle velocity in the given direction. At the same time, the velocity of the vehicle may be described in the planetary coordinate system as:  $V_{x_p}\hat{i}_p + V_{y_p}\hat{j}_p + V_{z_p}\hat{k}_p$ , where the subscript  $p$  represents planetary rather than vehicle coordinates. Note, since the two coordinate systems are not oriented in the same direction, the values of  $V_{x_v}$  will not be equal to  $V_{x_p}$ , but the magnitude of the total vector  $\vec{V}$  will be the same in both systems.

Also the difference in the magnitudes of individual components represents the difference in relative orientation between the two coordinate systems.

The *dot product*  $(\vec{a} \cdot \vec{b})$  is defined as the magnitude of  $\vec{a}$  multiplied by the magnitude of  $\vec{b}$  and then by the cosine of the angle between the vectors,

$$\vec{a} \cdot \vec{b} = |\vec{a}| |\vec{b}| \cos \angle \vec{a} \vec{b}$$

The dot product is used to project  $\vec{a}$  onto  $\vec{b}$  and can be used to project a vector in one frame of reference onto another one. Rather than calculate the needed cosines each time a vector must be transformed from one frame of reference into another, the cosines of the angles between each unit vector of the vehicular and planetary coordinate systems are computed and placed into a *direction cosine matrix*. This matrix is then used along with the vector's magnitude in each dimension of the original frame of reference to compute a dot product. This product gives the vector's magnitude in each dimension of the new frame of reference.

The transformation between the vehicle and the surface coordinate systems at time  $t$  is specified by a matrix of direction cosines,

$$\begin{pmatrix} l_1 & l_2 & l_3 \\ m_1 & m_2 & m_3 \\ n_1 & n_2 & n_3 \end{pmatrix}_t = \begin{pmatrix} \cos \theta(\hat{i}_v, \hat{i}_p) & \cos \theta(\hat{i}_v, \hat{j}_p) & \cos \theta(\hat{i}_v, \hat{k}_p) \\ \cos \theta(\hat{j}_v, \hat{i}_p) & \cos \theta(\hat{j}_v, \hat{j}_p) & \cos \theta(\hat{j}_v, \hat{k}_p) \\ \cos \theta(\hat{k}_v, \hat{i}_p) & \cos \theta(\hat{k}_v, \hat{j}_p) & \cos \theta(\hat{k}_v, \hat{k}_p) \end{pmatrix}_t$$

where  $\theta(\hat{i}, \hat{j})$  denotes the angle between vectors  $\hat{i}$  and  $\hat{j}$ , etc.

The change in orientation of the vehicle during descent makes the update of the direction cosine matrix necessary at each time step. This update is specified in the following equation:

$$d/dt \begin{pmatrix} l_1 & l_2 & l_3 \\ m_1 & m_2 & m_3 \\ n_1 & n_2 & n_3 \end{pmatrix}_t = \begin{pmatrix} 0 & r_v & -q_v \\ -r_v & 0 & p_v \\ q_v & -p_v & 0 \end{pmatrix}_t \begin{pmatrix} l_1 & l_2 & l_3 \\ m_1 & m_2 & m_3 \\ n_1 & n_2 & n_3 \end{pmatrix}_t$$

where the matrix containing the  $p_v$ ,  $q_v$ , and  $r_v$  terms is the rate of rotation about the axes of the vehicle which may be obtained from sensor values.

### Linear Velocity

The linear components of velocity for the vehicle during terminal descent are denoted by  $\dot{x}_v$ ,  $\dot{y}_v$ , and  $\dot{z}_v$  in the vehicle coordinate system and by  $\dot{x}_p$ ,  $\dot{y}_p$ , and  $\dot{z}_p$  in the

surface coordinate system, where the dot ( $\dot{\phantom{x}}$ ) notation indicates derivatives with respect to time.

### Vehicle Position

Vehicle position is expressed in terms of the surface coordinate system by transforming change in position (velocity) in the vehicle coordinate system into change in position in the surface frame and integrating as follows:

$$\begin{pmatrix} \dot{x}_p \\ \dot{y}_p \\ \dot{z}_p \end{pmatrix}_t = \begin{pmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{pmatrix}_t \begin{pmatrix} \dot{x}_v \\ \dot{y}_v \\ \dot{z}_v \end{pmatrix}_t$$

and

$$\begin{pmatrix} x_p \\ y_p \\ z_p \end{pmatrix}_t = \int \begin{pmatrix} \dot{x}_p \\ \dot{y}_p \\ \dot{z}_p \end{pmatrix} d\tau \Big|_t$$

### Angular Velocity

Roll, pitch, and yaw angular velocities are represented by the quantities  $p_v$ ,  $q_v$ , and  $r_v$  in the vehicle frame of reference only. Roll is about the  $\bar{x}_v$  axis, pitch is about the  $\bar{y}_v$  axis, and yaw is about the  $\bar{z}_v$  axis, as shown in Figure A.1.3. A more in-depth explanation of angular velocity naming conventions and other related material may be found in section II, part B of Reference (ref. A.3).

### Vehicle Attitude

The vehicle attitude at time  $t$  is a function of the vehicle attitude (known by reference to celestial objects) at the start of descent at time  $t_0$  and the cumulative changes in attitude from time  $t_0$  to time  $t$ .

### Acceleration

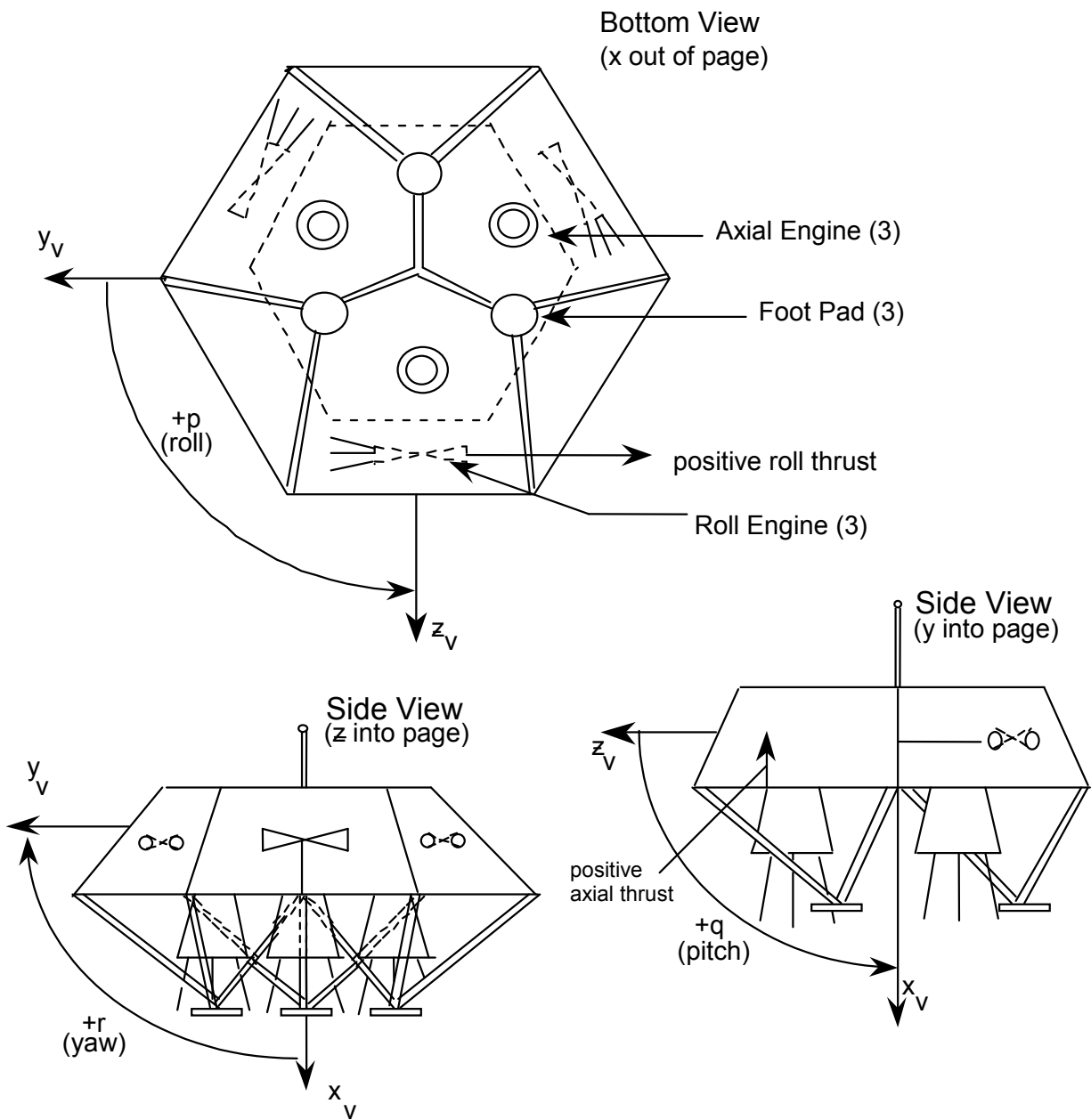
The linear components of acceleration for the vehicle in the vehicle frame of reference during terminal descent are denoted by  $\ddot{x}_v$ ,  $\ddot{y}_v$ , and  $\ddot{z}_v$ , respectively.

### Further Reading

The subjects of vector mathematics, transformations between frames of references, vector calculus, and rotating coordinate systems may not be sufficiently covered here for the user; however, such depth is not intended for this document. Chapter 4 of *Classical Mechanics* (ref. A.4) contains a detailed explanation of rigid body motion and transformation of vectors into multiple frames of reference or coordinate systems. Chapters 15 and 16 of *Engineering Mechanics* (ref. A.5) contains a more basic approach

to the same ideas of multiple frames of reference and vector mechanics. Chapter 14 of (ref. A.6) and Chapter 5 of (ref. A.7) also discuss rotational motion and multiple frames of reference, as well as vector mechanics and calculus. Two other books of possible interest are (ref. A.8) and (ref. A.9). Both cover the mechanics of particles and dynamics, with strong references to particle trajectories and rocket dynamics. Also, these texts are basic in nature and require only a rudimentary knowledge of physics, math, or engineering.

Figure A.1.3 ENGINEERING ILLUSTRATION OF VEHICLE



## **VEHICLE GUIDANCE**

Vehicle guidance is accomplished by varying the engine thrust so that the vehicle follows a single predetermined velocity-altitude contour. This contour is made available during GCS initialization. Applying too great a deceleration early in the descent brings the vehicle velocity to its terminal value too high above the surface, resulting in insufficient propellant for final descent. Applying too small a thrust lets the vehicle impact the surface with too great a velocity. Either condition could be disastrous. As soon as the touch down sensor touches the surface, the engines are shut off. Approximately ninety percent of propellant or thrust is used to minimize gravity losses; the remaining ten percent is used for steering.

A gravity-turn steering law is mechanized by rotating the vehicle in pitch and yaw until the body's lateral axis velocities are zero (causing the thrust axis to point along the total velocity vector). The action of gravity causes the thrust axis to rotate toward the vertical as the total velocity is reduced. An arbitrary roll orientation is maintained with an attitude hold mode during the descent.

## **ENGINES**

The vehicle has three axial engines that supply the force necessary to slow the vehicle and allow it to safely land. Roll is controlled by three pairs of roll engines on the lander supplying rotational thrust. Figure A.1.3 shows the axial and roll engines and the resulting thrust forces they impart to the vehicle.

### **Axial Engine (Thrust) Control**

Three thrust engines first orient the vehicle so that their combined thrust vector opposes the vehicle's velocity vector. Thrust (axial direction) engine control is a function of pitch error, yaw error, thrust error, and deviation from the velocity-altitude contour. A combination of proportional and integral control (PI) logic is applied to pitch and yaw control. The integral portion helps to reduce the steady-state pitch and yaw error.

If no thrust error or velocity-altitude contour deviation occurs, then axial engine response provides only pitch and yaw control via the PI control law. Use of this control law implies that the overshoot problem for pitch-yaw control is probably small.

Thrust control is implemented by a proportional-integral-derivative (PID) control law. The derivative control added here damps out overshoot.

### **Roll Engine Control**

Roll control is attained by pulsing the three pairs of roll engines and is a function of roll angle deviation and roll rate ( $p_V$ ) about the  $x$  axis. Roll engine specific impulse and

thrust per unit time are constant with the integrated thrust controlled by pulse rate. Angle deviations are controlled within a very small range of 0.25 to 0.35 degrees.

## GENERAL INFORMATION

### NOTATION

#### Matrices and Arrays

It should be noted that throughout this specification, the words matrix and array are often interchanged. No significance should be placed upon the use of one word as opposed to use of the other.

All matrices are referenced with the row index first and the column index second. In the cases where there is a time history (see definition of history variable below), the last index is the time index.

When the name of an array which contains a time history is given without any index for the time history being specified, the most recent value is implied.

#### Operators

Throughout this specification, matrix operations (particularly multiplication) are required, and on some occasions, non-standard operations are used upon matrices. The following symbols are used to denote the types of multiplication to be applied.

**Dots (·)** Small dots are used to denote scalar multiplication. For example:

$$3 \cdot 4 = 12$$

**Multiplication sign (×)** This symbol is used to denote standard matrix multiplication.

This does NOT imply a cross product, nor strictly a dot product. The definition of this type of operation is given below:

$$A \times B = C$$

where

$$\forall i \text{ and } \forall j, C_{ij} = \sum_{\forall k} A_{ik} \cdot B_{kj}$$

**Asterisks (\*)** Asterisks are used in conjunction with index markers to show that the operations are to be conducted on individual elements of arrays or vectors as if they were scalars. This is often the case when calculating sensor values or other similar functions when multiple scalars are grouped together for convenience. For example, the following equation is listed in ASP:

$$A\_ACCELERATION\_M(i) = A\_BIAS(i) + A\_GAIN(i) * A\_COUNTER(i)$$

where  $i$  ranges from 1 to 3 and represents the three directions x, y, and z. In this case, the first element of A\_ACCELERATION\_M would be calculated as follows:

$$A\_ACCELERATION\_M(1) = A\_BIAS(1) + A\_GAIN(1) \cdot A\_COUNTER(1)$$

**No Operator** In those cases where variables, matrices, or scalars are located directly beside each other with no operator between, standard multiplication is implied. Thus two matrices collocated would be multiplied as if they had the  $\times$  operator between them, while two scalars would be multiplied as if they had the  $\cdot$  operator between them. Also, if a scalar and a matrix (of one or more dimensions) were collocated, then the scalar would be multiplied by each element of the matrix and a new matrix of equal dimensions would be generated.

## DEFINITIONS

### **Implementation**

Computer code which fulfills all of the requirements outlined in the GCS Development Specification.

### **Functional Unit**

Section A.5 is divided into eleven subsections, each of which describes the requirements for a particular function to be performed by the GCS software. Throughout this specification, the term "functional unit" will be used to refer to one of these eleven functions. Note that there is not necessarily a one-to-one correspondence between a "functional unit" and a distinct unit or module of software code in an implementation.

### **Frame**

A frame is the length of time necessary to execute all scheduled functional units. Each frame has two different time values associated with it. The first is the actual c.p.u. time that it takes to execute the GCS software on the simulation host computer, while the second is the allotted time for a frame on the actual lander. The global variable DELTA\_T represents the time for one frame on the actual lander and is needed in the GCS code for the integration of the dynamic equations for the lander.



### **Subframe**

A subframe is one of the three individual units of time which together make up a frame. The three subframes are named the Sensor Processing subframe (subframe 1), the Guidance Processing subframe (subframe 2), and the Control Law Processing subframe (subframe 3). In each frame, subframe 1 is executed first, subframe 2 is executed second, and subframe 3 is the last subframe executed.

### **Data Store**

The definition for a data or control store given in Hatley (ref. A.13) is "A data or control store is simply a data or control flow frozen in time. The data or control information it contains may be used any time after that information is stored and in any order." In this specification, all stores contain data, while some also contain data conditions. For the purposes of this specification, the term "data store" will be used to refer to any store which contains some combination of data and data conditions. Thus, all four stores listed in the Data Requirements Dictionary part II will be referred to as "data stores".

### **Global Data Store Variable**

A global data store variable is any variable listed in any of the four global data stores in Section A.6, namely GUIDANCE\_STATE data store (Table A.6.1), EXTERNAL data store (Table A.6.2), SENSOR\_OUTPUT data store (Table A.6.3), or RUN\_PARAMETERS data store (Table A.6.4).

### **History Variable**

Within this specification, a particular array, hereafter referred to as a "history variable" is one which contains a time history dimension; that is, it contains values for the current frame as well as for previous frames. The history variables are the following:

A\_ACCELERATION (1:3,0:4)  
A\_STATUS (1:3,0:3)  
AR\_ALTITUDE (0:4)  
AR\_STATUS (0:4)  
G\_ROTATION (1:3,0:4)  
GP\_ALTITUDE (0:4)  
GP\_ATTITUDE (1:3,1:3,0:4)  
GP\_VELOCITY (1:3,0:4)  
K\_ALT (0:4)  
K\_MATRIX (1:3,1:3,0:4)  
TDLR\_VELOCITY (1:3,0:4)

In each case, the last dimension is the time dimension. The first subscript in a time history dimension is always declared to be zero. The time dimension contains a set of

scalars, vectors, or arrays, depending on whether the total number of dimensions is one, two, or three, respectively. Let the term "object" denote a scalar, vector, or array, as appropriate for the particular variable. Each of these variables contains either four or five objects, depending on whether the last dimension is declared to be 0:3 or 0:4 respectively. The variable A\_STATUS contains four objects, while each of the other time history variables contains five objects.

Each of the variables listed contains a most recent object and either three or four previous objects. The object with a time subscript of zero is the most recent object; the object with a time subscript of one is the object which is one frame older; the object with a time subscript of two is the object which is two frames older, etc.; the object with the largest time subscript (three or four) is the oldest object.

## **CONVENTIONS**

### **FORTRAN Convention**

This specification was written with the assumption that the implementation would be coded in FORTRAN. If the development language used is something other than FORTRAN, the programmer must investigate the possibility of differences between FORTRAN and the development language chosen.

## **REQUIREMENTS**

### **Order of Processing**

Within each functional unit in Chapter 5, the processing steps are given in a particular order. If the implementation uses the same order as that given in the specification, then correct results should be obtained; however, the programmer is free to use a different order as long as the change in order does not affect the outputs.

### **Calls to GCS\_SIM\_RENDEZVOUS**

There must be a call to GCS\_SIM\_RENDEZVOUS prior to the execution of each subframe. See section A.2 and section A.8 for discussions regarding GCS\_SIM\_RENDEZVOUS.

### **Control Signals**

The control signals listed in Table A.6.5 in Part III of the Data Requirements Dictionary may be implemented by the programmer in any form desired, or they may be completely ignored and the control of the program may be conducted through other means.



### **Number Representations**

When variables are given in sign-magnitude or other unusual formats, conversion or manipulation may be necessary.

### **Conversion of Units**

It is the responsibility of the programmer to be sure that any implied conversion of units is performed.

### **Global Data Store Organization**

Part II of the Data Requirements Dictionary contains descriptions of four required data stores. Each of these data stores is to be located in a separate, globally accessible data region. The division of the global data stores into four separate regions illustrates the fact these regions have a direct mapping to a specific implementation of GCS on hardware components of an actual lander. (See Figure A.B.1).

If the implementation is being written in FORTRAN, four labeled common blocks should be declared with the labels `GUIDANCE_STATE`, `EXTERNAL`, `SENSOR_OUTPUT`, and `RUN_PARAMETERS`, respectively (See Tables 6.1, 6.2, 6.3, and 6.4). The variables declared in each labeled common block must be in the same order as those in the corresponding table.

### **Use of Variables That Are Not in the Global Data Stores**

A programmer may use variables in addition to the global data store variables; however, if the value of such a variable is dependent upon the values of any global data store variable(s), then the programmer should only use the value of such a variable in the same subframe of the same frame in which it was calculated.

### **Use of Tables**

Some tables have the heading "CURRENT STATE" and "ACTIONS". If the actual state of the variables appears under the "CURRENT STATE" section in the table, then the actions listed in the same line are to be performed. If the actions in one line of the table are performed, then none of the actions in any other line of the table should be performed in the same subframe. If the actual current state is not represented in any line under the "CURRENT STATE" section of the table, then no action is to be taken.

### **Rotation of History Variables**

In Chapter 5, in certain functional units, an instruction is given to "rotate" specific variables. Table A.1.1 illustrates what is meant by rotation. The table is given for a variable with a time dimension of 0:4. For a variable with a time dimension of 0:3, the

last line of the table should be ignored. Note that after the variable has been rotated, the new or current object is calculated and placed into the zeroth time history position.

Table A.1.1 ROTATION OF VARIABLES

TIME HISTORY SUBSCRIPT	VALUES BEFORE ROTATION	VALUES AFTER ROTATION	VALUE AFTER CALCULATIONS FOR CURRENT FRAME
0	$O_{n-1}$	X	$O_n$
1	$O_{n-2}$	$O_{n-1}$	$O_{n-1}$
2	$O_{n-3}$	$O_{n-2}$	$O_{n-2}$
3	$O_{n-4}$	$O_{n-3}$	$O_{n-3}$
4	$O_{n-5}$	$O_{n-4}$	$O_{n-4}$

Note:  $O_i$  denotes object that was calculated in frame  $i$

$n$  = current frame number

X = denotes that any value is acceptable

### Precision

All calculations involving floating point variables should be done with precision equivalent to that of FORTRAN D-floating (REAL\*8).

### EXCEPTION HANDLING

During the execution of a computer program, exception conditions may sometimes occur. The implementation should anticipate or detect certain types of exception conditions and take specific actions. The relevant exception conditions and the actions to be taken are listed below.

#### Exception Conditions

##### ***DIVIDE BY ZERO***

A division is performed, but the divisor is equal to zero.

##### ***NEGATIVE SQUARE ROOT***

A square root is taken, but the argument for the square root is negative.

##### ***UPPER OR LOWER LIMIT EXCEEDED***

The current value for a data element exceeds its upper or lower limit as specified in the range section in the Data Requirements Dictionary Part I.

Only certain data elements under certain conditions are to be checked for limits exceeded. The criteria for which elements are to be checked, in what context they are to be checked, and when they must be checked is as follows:

Which data elements:

A particular data element is to be checked for limits exceeded only if it is of data type REAL\*8, and is in either of the two global data stores GUIDANCE\_STATE or SENSOR\_OUTPUT.

Context for check:

A data element is to be checked only when it is being used as an input. Rotation of a data element is not considered to be a use as an input for the purposes of limit checking. If the data element is a vector or array, then each element in the vector or array that is being used as input must be checked, including history values. It is not necessary for the functional unit CP to check any of its input data elements for limit exceeded.

When data element must be checked:

When an input data element is to be used or processed in a given subframe, then it must be checked sometime within that same subframe before it is used. If the data element is also being updated or changed in the same subframe before it is being used as an input, then it must be checked sometime between the time it is updated and the time it is used.

### **Action to be Taken for Each Specified Exception Condition**

Write the appropriate output as specified below to the FORTRAN Logical Unit Number 6 and then continue. In the case of UPPER/LOWER LIMIT EXCEEDED, do not modify the data element. Note that to "continue" implies that the divide will be executed, or the square root will be taken, or the data element with exceeded limit will be used.

### **Output to be Generated for Each Exception Condition**

The first line of the exception message should appear as follows:  
" %EXCEPTIONAL-CONDITION-GCS-"<insert specific condition here>  
where the specific condition is one of the following:  
"DIVIDE\_BY\_ZERO"  
"NEGATIVE\_SQUARE\_ROOT"  
"LOWER\_LIMIT\_EXCEEDED"  
"UPPER\_LIMIT\_EXCEEDED"

The second line of the exception message should contain the name of the functional unit where the exception condition occurred (i.e. AECLP, ASP, etc.), the name of the actual subroutine where the exception condition occurred, and the current value of the frame counter. Implementations that are coded in FORTRAN should use the following FORTRAN format statement:

FORMAT (x, a6, x, a32, x, i4)

A third line of the exception message containing information that is specific to the individual error type may be required as specified below.

*Divide By Zero*

No additional output necessary.

*Negative Square Root*

Display the value of the argument to the square root operation.

Use FORTRAN format statement FORMAT (x, e23.14).

*Lower Limit Exceeded*

Display the name of the data element in question and the value of the data element.

Use FORTRAN format statement FORMAT (x, a32, e23.14) for type real elements.

*Upper Limit Exceeded*

Display the name of the data element in question and the value of the data element.

Use FORTRAN format statement FORMAT (x, a32, e23.14) for type real elements.

## **A.2 LEVELS 0 AND 1 SPECIFICATION**

### **LEVEL 0 SPECIFICATION**

The GCS will provide an interface between the sensors (rate of descent, attitude, etc.) and the engines (roll and axial). The purpose of the GCS is to keep the vehicle descending along the predetermined velocity-altitude contour which has been chosen to conserve enough fuel to effect a safe attitude and touch down.

The GCS effects this control by:

- processing the following sensor information:
  - acceleration data from the three accelerometers -- one for each vehicle axis,
  - range rate data from four splayed doppler radar beams,
  - altitude data from one altimeter radar,
  - temperature data from a solid-state temperature sensor and a thermocouple pair temperature sensor,
  - rates of rotation from three strapped-down gyroscopes -- one for each vehicle axis, and
  - sensing of touch down by the touch down sensor.

- determining the appropriate commands for the axial and roll engines and the chute release mechanism and issuing them to keep the vehicle on a predetermined velocity-altitude contour.

The GCS also transmits telemetry data and synchronizes through a rendezvous routine (GCS\_SIM\_RENDEZVOUS) with GCS\_SIM (ref. A.10), the simulator and controller.

Note that implementations of the GCS developed from this specification may be executed singly or in parallel. Consequently, only specific system services can be used in an implementation. In particular, a rendezvous routine will be provided and should be invoked, as specified in the implementation notes in section A.8. In addition, FORTRAN Intrinsic Functions may be used. Other system services and library routines are explicitly excluded from use by the programmer.

Figures 2.2 through 2.5, 3.1, 3.2, and 4.1 through 4.4, and Tables 2.1, 3.1, 4.1, and 4.2 follow Hatley's extension to Structured Analysis (see section A.7), with the following exceptions and assumptions.

Exceptions:

1. Any data store may appear at more than one level because the processes specified do not communicate directly but only through data stores.
2. Any unlabeled flow between a process and a data store may not necessarily carry all the information in the data store (the actual flow content is defined by the process specification and the Data Requirements Dictionary Part II).

Assumptions:

1. The initial value for control signals is assumed to be "FALSE".
2. In a process activation table (PAT), an empty process cell indicates the process is deactivated.
3. In a PAT, an empty output cell indicates the control signal value remains unchanged.
4. In a PAT, output control signals receive values before any processes are activated and therefore may delay the activation of processes by deactivating their parent process.



An example of assumption 4 is Table A.3.1 where setting RENDEZVOUS to "TRUE" delays the activation of the processes of which RUN\_GCS is composed until GCS\_SIM sets RENDEZVOUS to "FALSE".

Figure A.2.1 STRUCTURE OF THE GCS SPECIFICATION

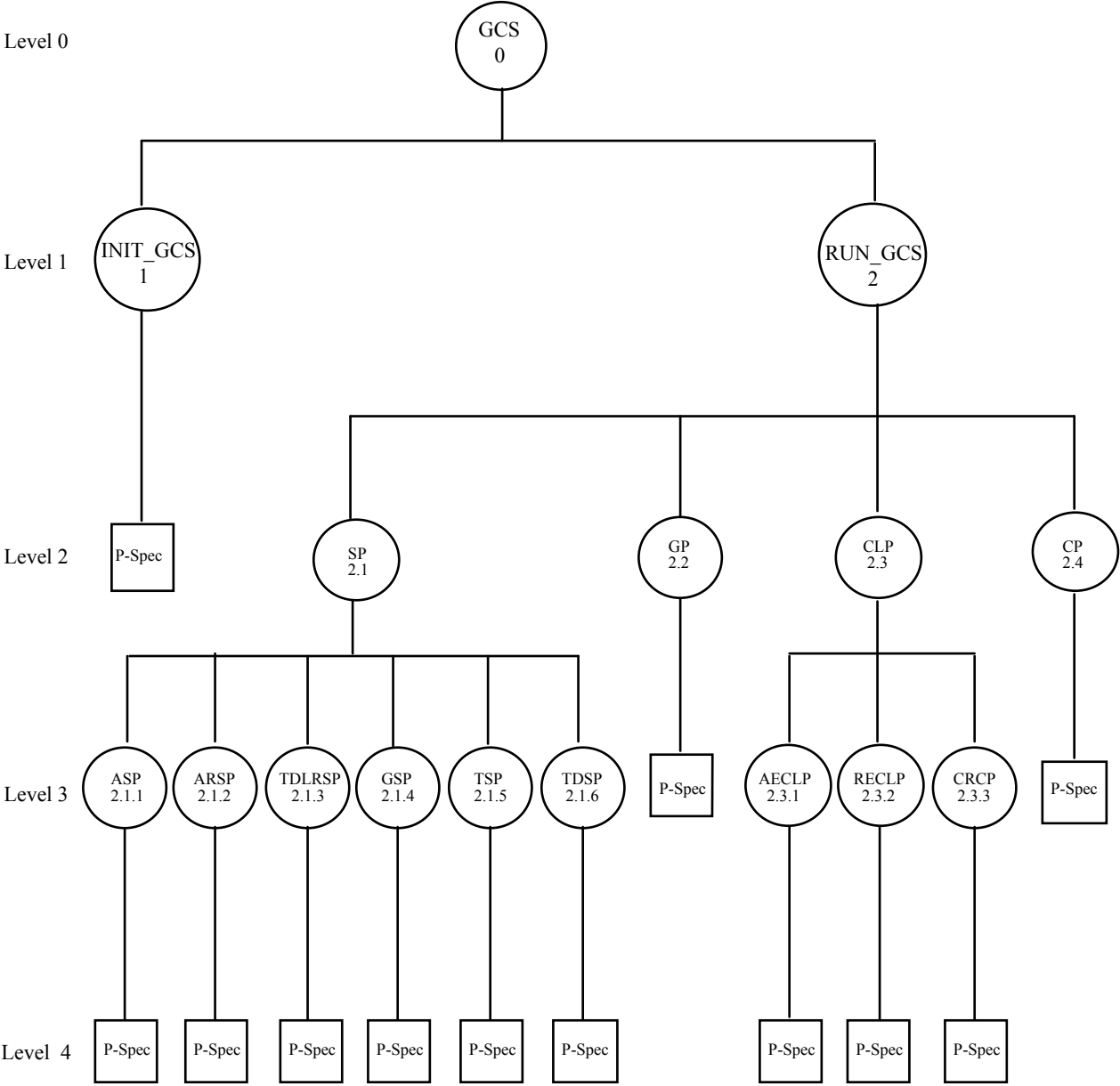


Figure A.2.2 DATA CONTEXT DIAGRAM: LANDER

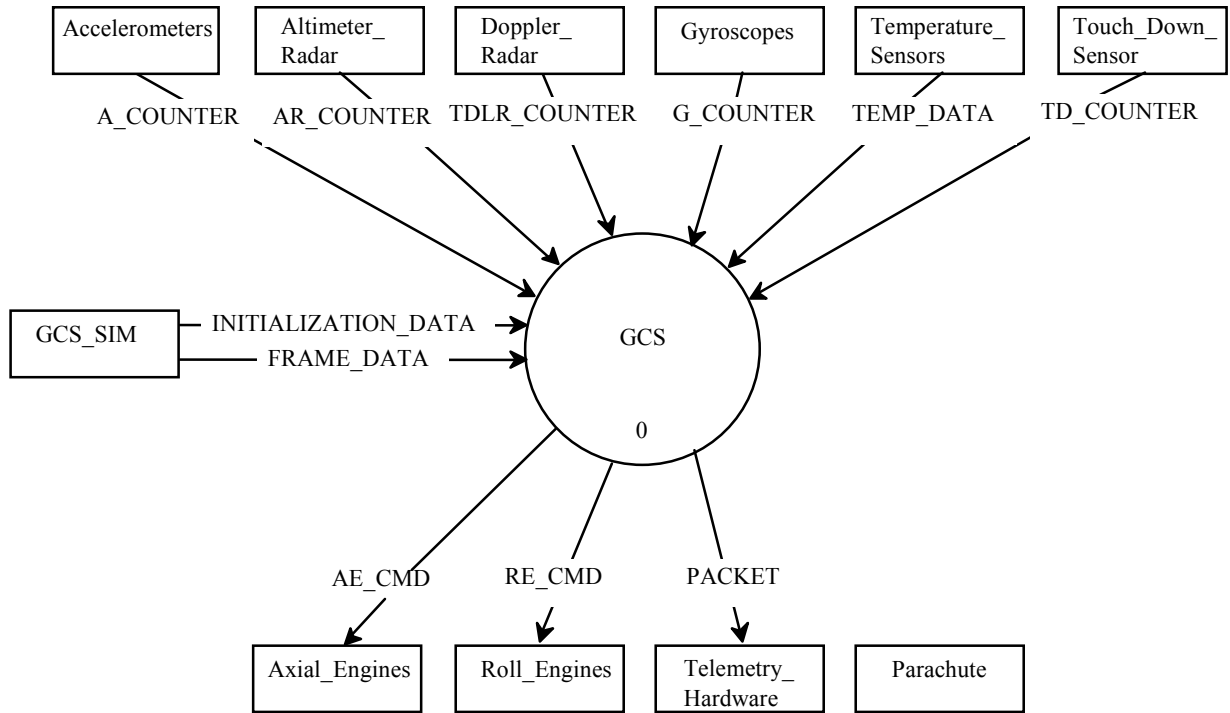
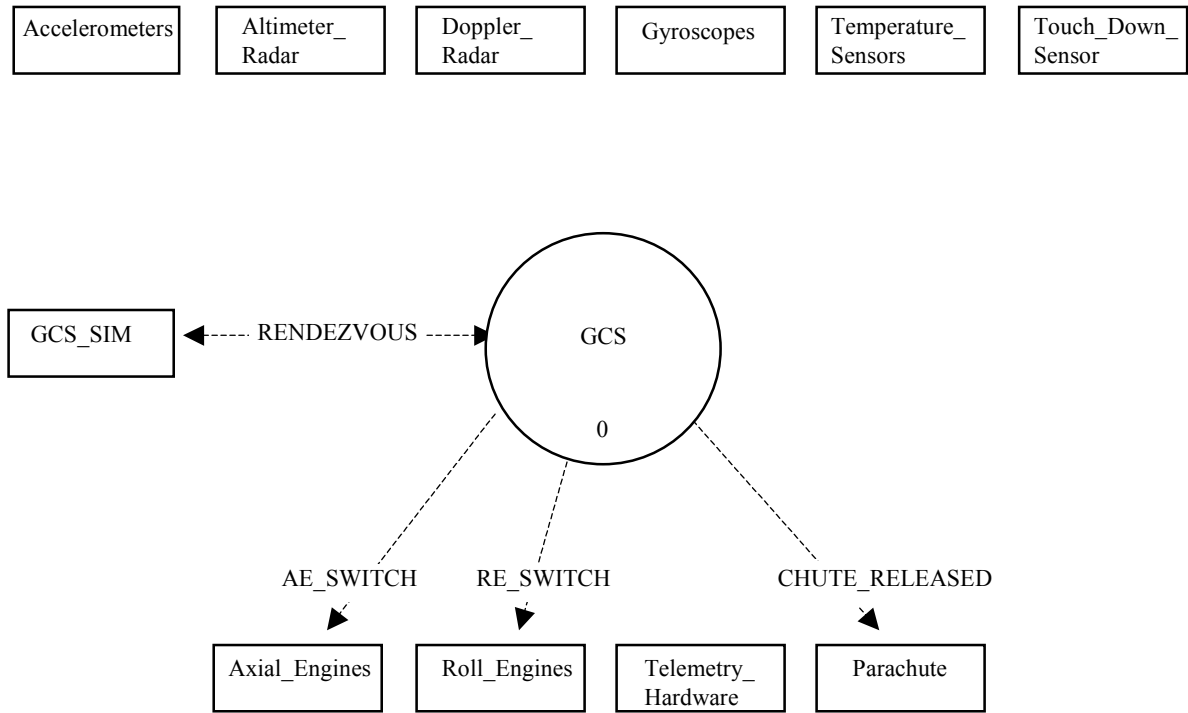


Figure A.2.3 CONTROL CONTEXT DIAGRAM: LANDER



# LEVEL 1 SPECIFICATION

Figure A.2.4 DATA FLOW DIAGRAM (DFD) 0: GCS

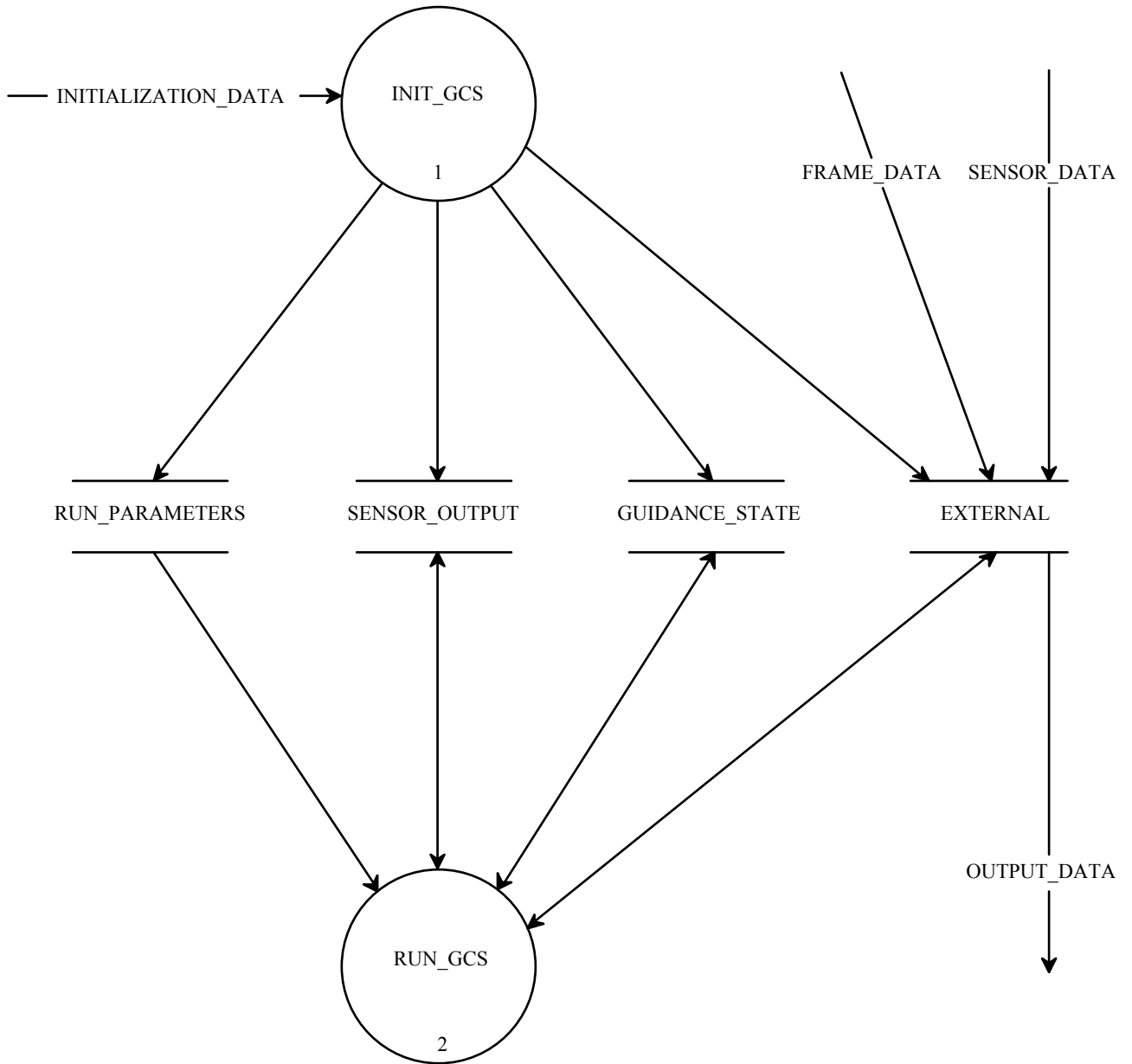
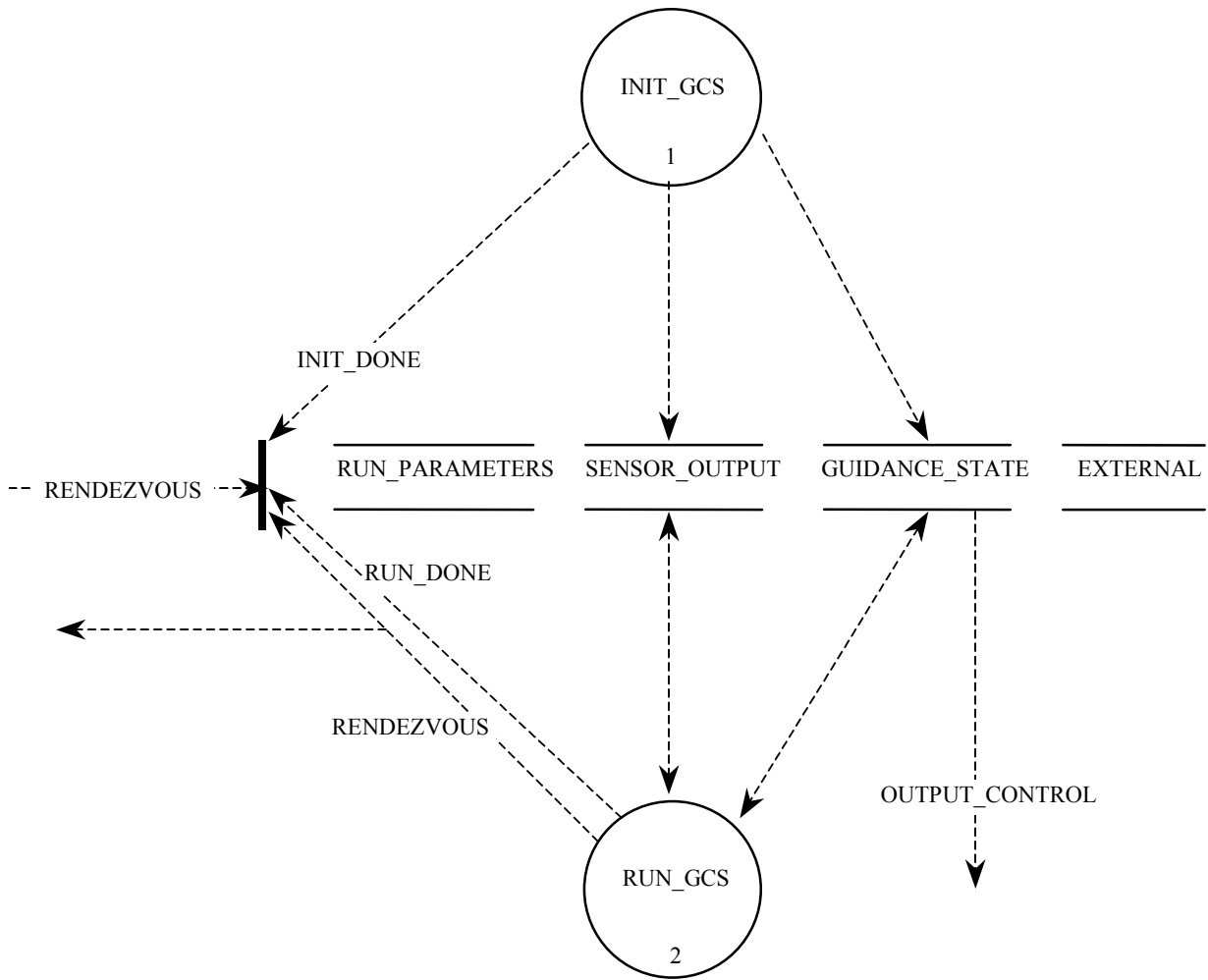


Figure A.2.5 CONTROL FLOW DIAGRAM (CFD) 0: GCS



RENDEZVOUS is only set to "TRUE" by RUN\_GCS and it is only set to "FALSE" by GCS\_SIM.

Table A.2.1 CONTROL SPECIFICATION (C-SPEC) 0: GCS

	"INIT_GCS"	"RUN_GCS"
~RENDEZVOUS & ~RUN_DONE		1
RENDEZVOUS & ~INIT_DONE & ~RUN_DONE	1	
(RENDEZVOUS & INIT_DONE)   RUN_DONE		

### A.3 LEVEL 2 SPECIFICATION PROCESS SPECIFICATION (P-Spec) 1:

#### INIT\_GCS

**PURPOSE** INIT\_GCS initializes the guidance and control software.

#### INPUT

INITIALIZATION_DATA
---------------------

#### OUTPUT

INITIALIZATION_DATA
---------------------

**PROCESS** INIT\_GCS is actually a part of GCS\_SIM\_RENDEZVOUS, which will be supplied to the programmer; thus the functions performed by INIT\_GCS are listed here for information only, but are not the responsibility of the programmer. There should be a call to GCS\_SIM\_RENDEZVOUS, prior to executing each subframe. The first call to GCS\_SIM\_RENDEZVOUS will cause INIT\_GCS to automatically be executed. INIT\_GCS will initialize all variables in the group flow INITIALIZATION\_DATA, which is defined in Table A.6.7 in the Data Requirements Dictionary Part III. Since the variables FRAME\_COUNTER and SUBFRAME\_COUNTER are part of INITIALIZATION\_DATA, they will be initialized at this time. FRAME\_COUNTER will be initialized to a value representing the next frame to be executed, while SUBFRAME\_COUNTER will always be initialized to the value one, which implies that the first subframe of the first frame to be executed will always be the sensor processing subframe. Although a terminal descent trajectory begins with FRAME\_COUNTER initialized to the value one, the option exists for starting execution at some point other than at the beginning of the trajectory, i.e., FRAME\_COUNTER may be initialized to a value greater than one.



Figure A.3.1 DFD 2: RUN\_GCS

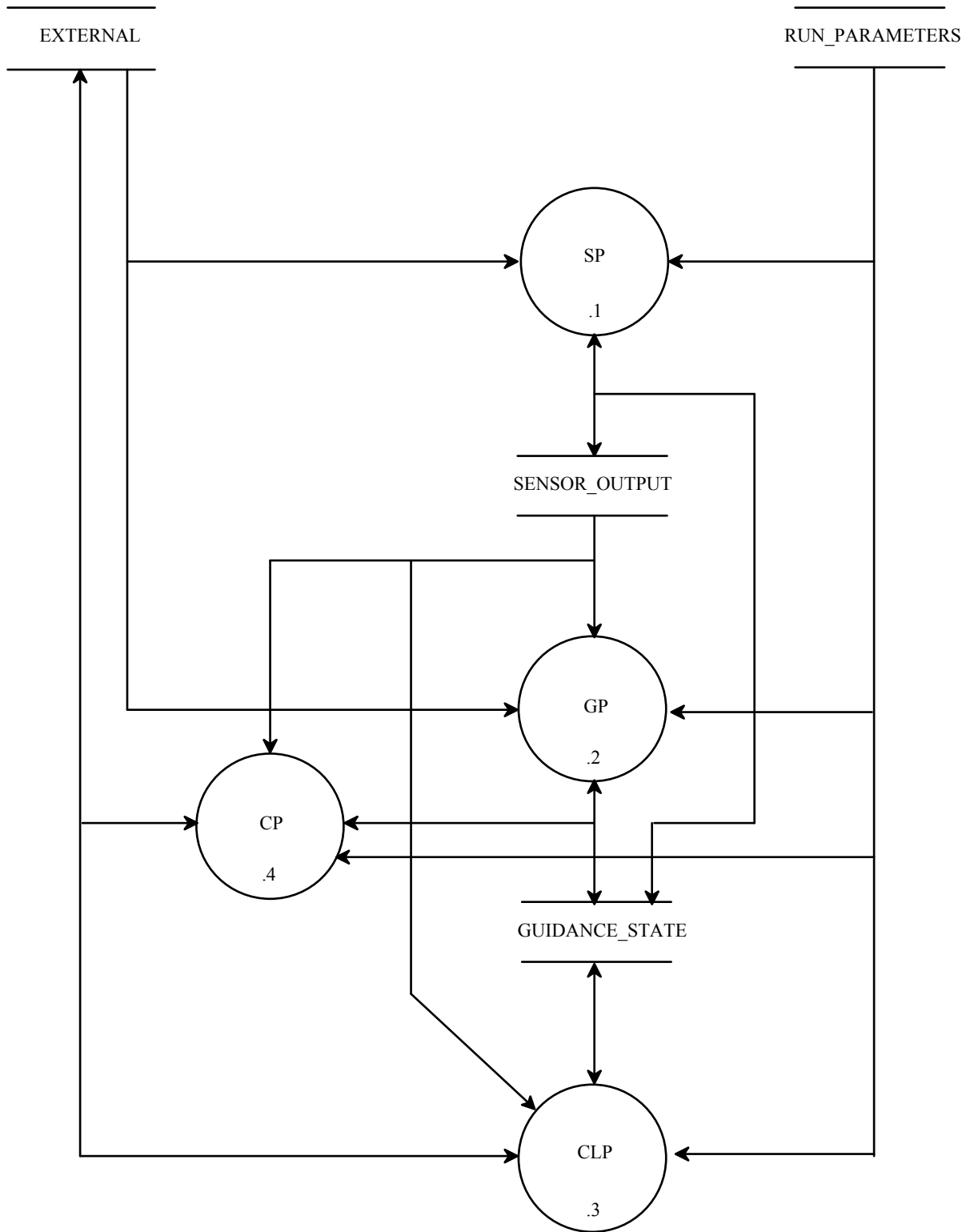


Figure A.3.2 CFD 2: RUN\_GCS

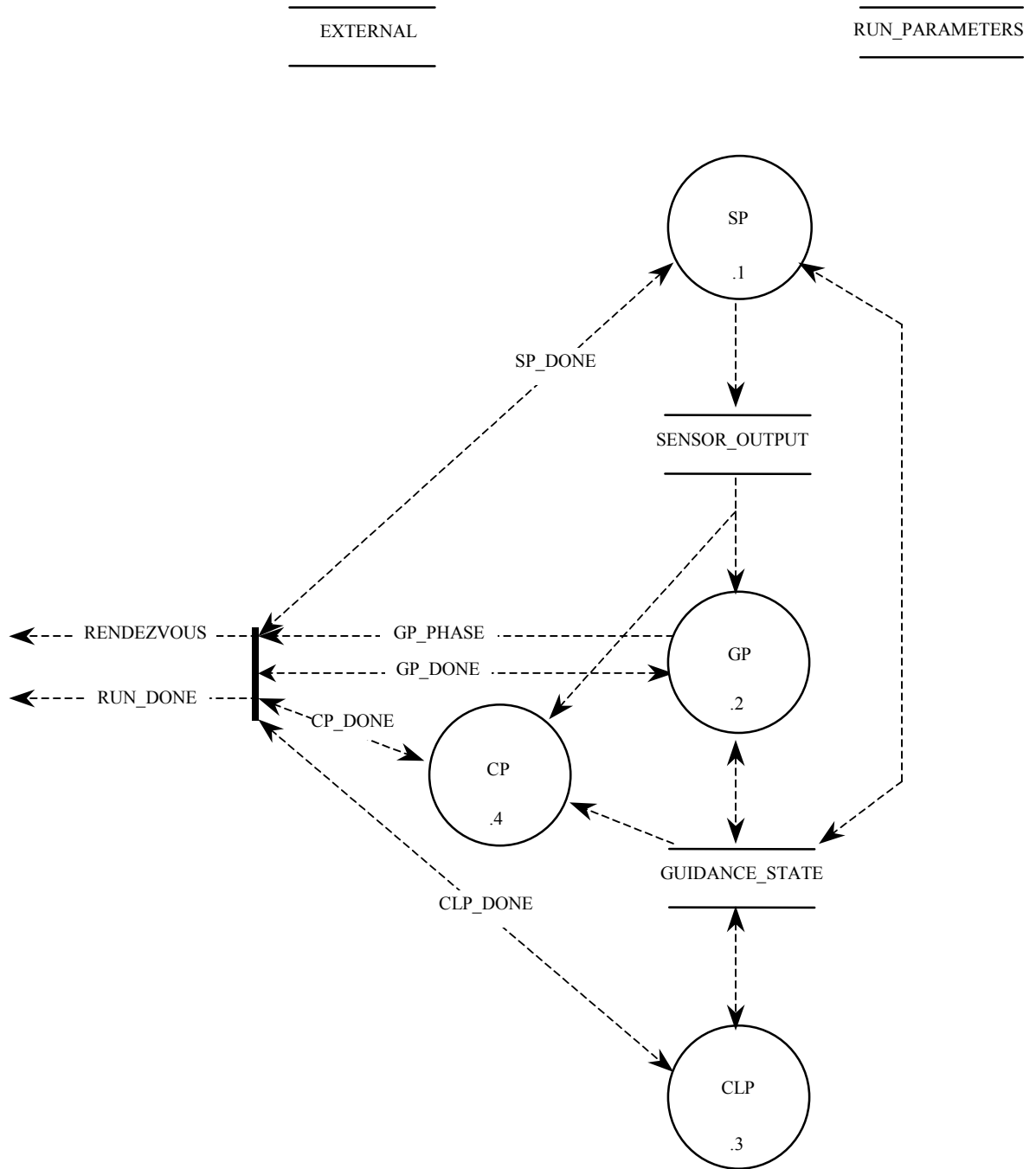


Table A.3.1 C-Spec 2: RUN\_GCS

	"SP"	"GP"	"CLP"	"CP"	SP_DONE	GP_DONE	CLP_DONE	CP_DONE	RENDEZVOUS	RUN_DONE
~SP_DONE & ~GP_DONE & ~CLP_DONE & ~CP_DONE	1			2					"TRUE"	
SP_DONE & CP_DONE		1		2	"FALSE"			"FALSE"	"TRUE"	
GP_DONE & CP_DONE & GP_PHASE ~= 5			1	2		"FALSE"		"FALSE"	"TRUE"	
CLP_DONE & CP_DONE	1			2			"FALSE"	"FALSE"	"TRUE"	
GP_DONE & CP_DONE & GP_PHASE = 5										"TRUE"

## A.4 LEVEL 3 FLOW DIAGRAMS AND C-SPECS

Figure A.4.1 DFD 2.1: SP -- SENSOR PROCESSING

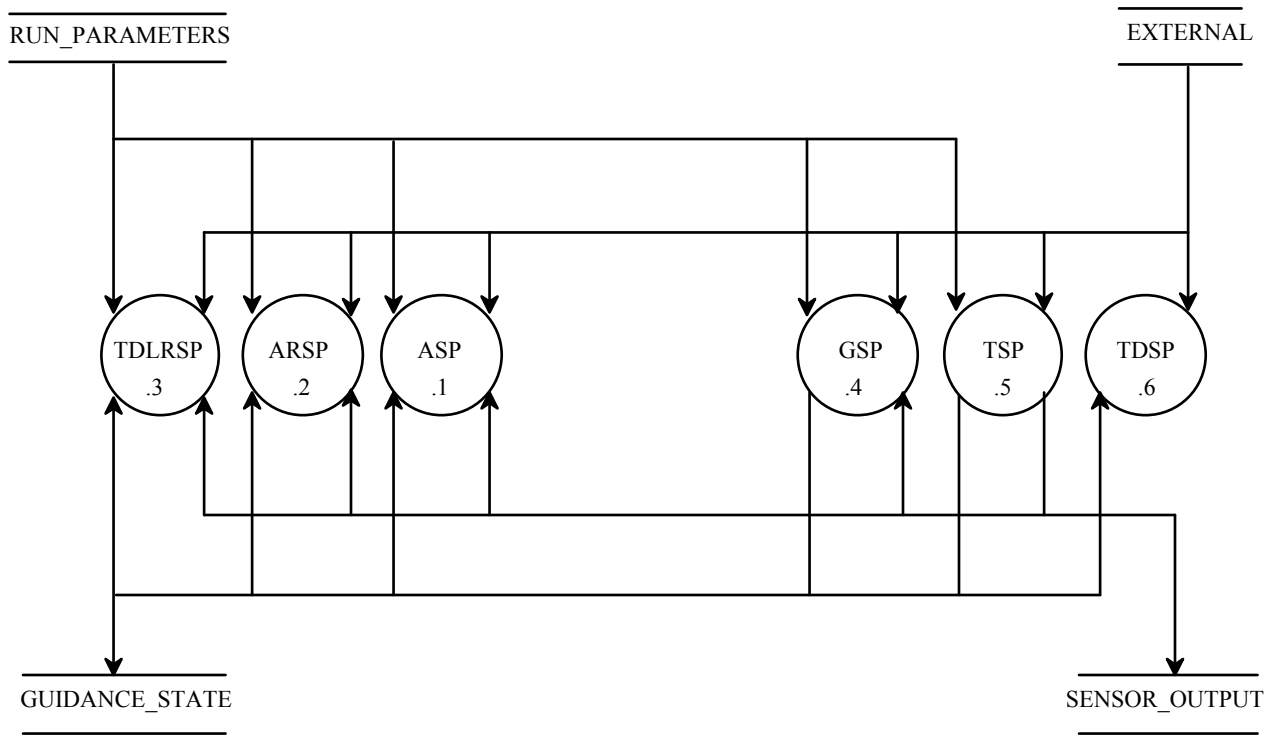


Figure A.4.2 CFD 2.1: SP -- SENSOR PROCESSING

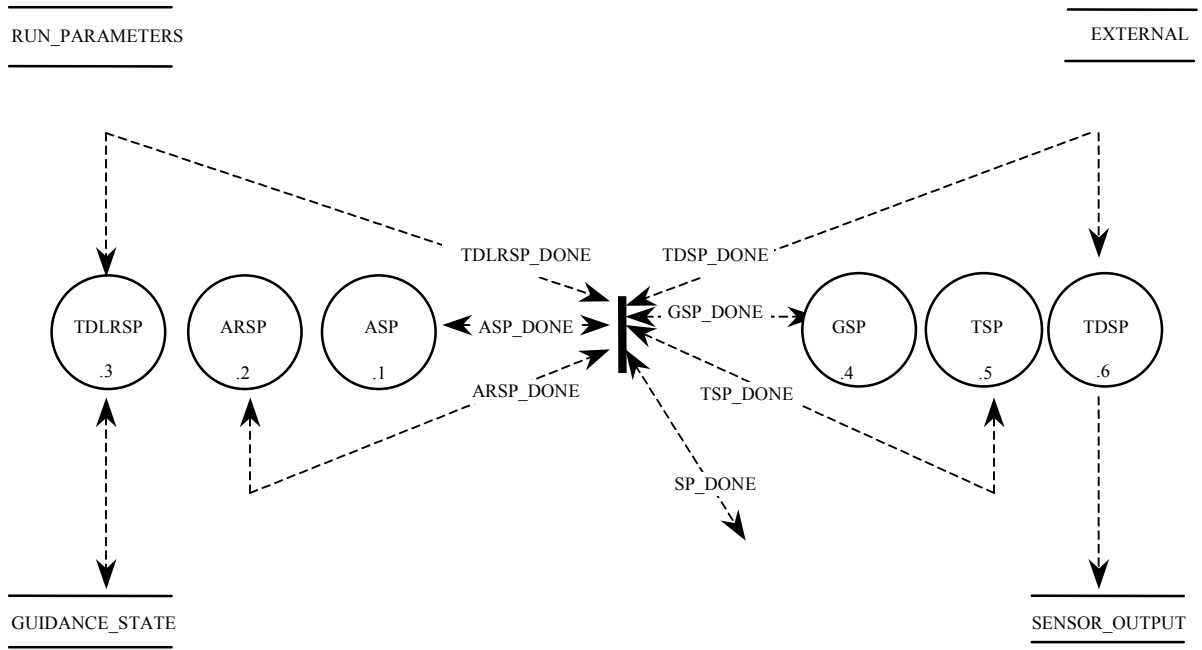


Table A.4.1 C-Spec 2.1: SP -- SENSOR PROCESSING

	"ASP "	ARSP"	"TDLRSP"	"GSP"	"TSP"	"TDSP"	ASP_ DONE	ARSP_ DONE	TDLRSP_ DONE	GSP_ DONE	TSP_ DONE	TDSP_ DONE	SP_ DONE
~ASP_DONE & ~ARSP_DONE & ~TDLRSP_DONE & ~GSP_DONE & ~TSP_DONE & ~TDSP_DONE & ~SP_DONE	2	2	2	2	1	2							
ASP_DONE & ARSP_DONE & TDLRSP_DONE & GSP_DONE & TSP_DONE & TDSP_DONE & ~SP_DONE							"FALSE"	"FALSE"	"FALSE"	"FALSE"	"FALSE"	"FALSE"	"TRUE"

Figure A.4.3 DFD 2.3: CLP -- CONTROL LAW PROCESSING

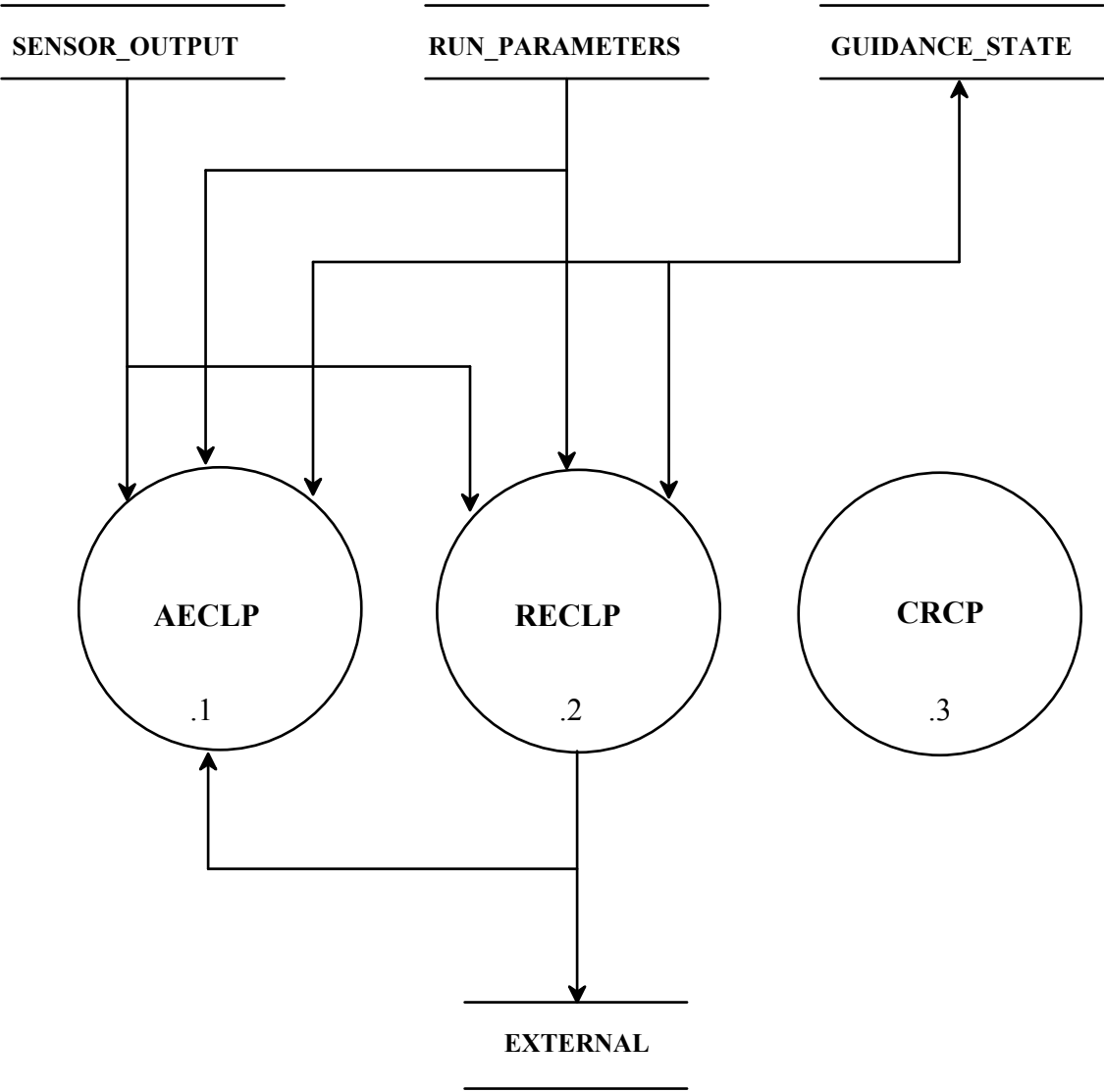


Figure A.4.4 CFD 2.3: CLP -- CONTROL LAW PROCESSING

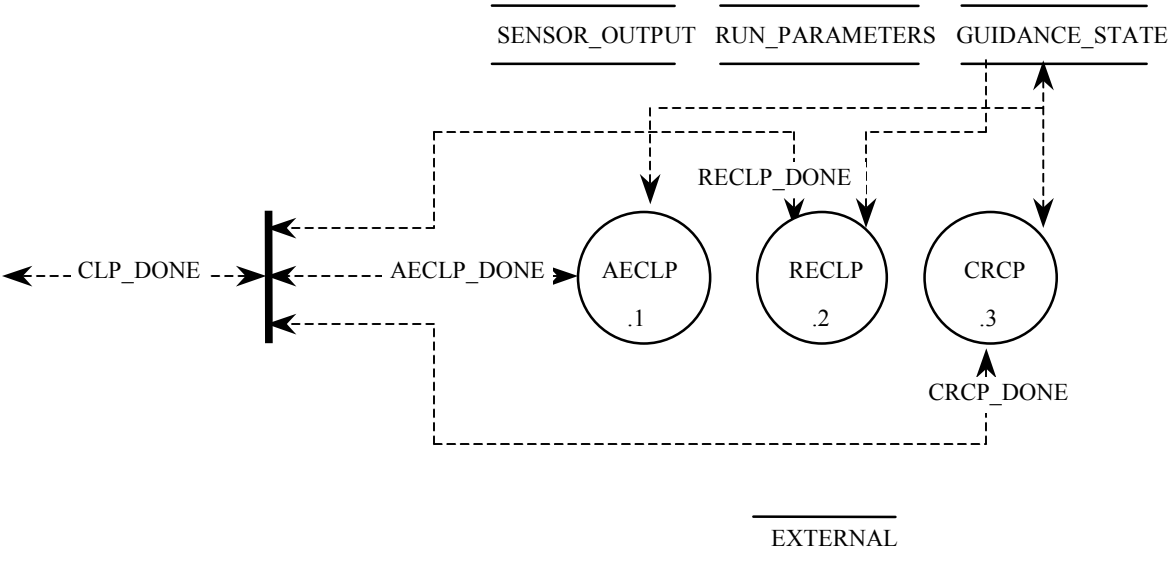




Table A.4.2 C-Spec 2.3: CLP -- CONTROL LAW PROCESSING

	"AECLP"	"RECLP"	"CRCP"	AECLP_DONE	RECLP_DONE	CRCP_DONE	CLP_DONE
~AECLP_DONE & ~RECLP_DONE & ~CRCP_DONE & ~CLP_DONE	1	1					
AECLP_DONE & ~CRCP_DONE & ~CLP_DONE		1	1				
AECLP_DONE & RECLP_DONE & CRCP_DONE & ~CLP_DONE				"FALSE"	"FALSE"	"FALSE"	"TRUE"

## SCHEDULING

The execution of one frame consists of the execution of the Sensor Processing Subframe, the Guidance Processing Subframe, and the Control Law Processing Subframe, in that order. Within each subframe, the functional units which are to be executed are listed in Table A.4.3. Within each of the three subframes, GCS\_SIM\_RENDEZVOUS should be executed before executing any of the functional units, and the functional unit CP should be executed last. In the first and third subframes, there are also some sequencing constraints to be imposed upon certain functional units due to the fact that certain data is output from one unit and input to another unit: In the sensor processing subframe, TSP should be executed before ASP, and TSP should be executed before GSP. In the control law processing subframe, AECLP should be executed before CRCP. Within any given subframe, the order of execution of functional units not specifically mentioned here is immaterial.

Each functional unit will be executed every frame in the particular subframe in which it is included in Table A.4.3. Execution of the GCS may begin at any frame number and should operate as if it had been running from the beginning of the trajectory (frame number 1). On the first, and subsequent, calls to GCS\_SIM\_RENDEZVOUS, FRAME\_COUNTER and SUBFRAME\_COUNTER will be returned to the implementation containing the correct values for operation.

Table A.4.3 FUNCTIONAL UNIT SCHEDULING

Sensor Processing Subframe (Subframe 1)
ARSP
ASP
CP
GSP
TDLRSP
TDSP
TSP
Guidance Processing Subframe (Subframe 2)
CP
GP
Control Law Processing Subframe (Subframe 3)
AECLP
CP
CRCP
RECLP

The GCS software must meet all the requirements for a particular frame for any specific value of the variable FRAME\_COUNTER. The software must be capable of

executing continuously one frame after another until specified termination conditions are met, at which time it must terminate itself according to specified termination procedures.

The termination conditions and procedures are: GCS should check whether to terminate itself in each frame immediately after executing the Control Law Processing subframe. At that time if the value of the variable GP\_PHASE is equal to 5, then GCS should terminate itself gracefully (without any exception conditions). In this case, the implementation should terminate at the end of the present subframe, i.e., it should execute the functional unit Communications Processing and then terminate without calling GCS\_SIM\_RENDEZVOUS.

## 5 P-SPECS FOR LEVELS 3 and 4

### AECLP -- Axial Engine Control Law Processing (P-Spec 2.3.1)

**PURPOSE** The AECLP functional unit computes the valve settings for each of the three main (axial) engines. Measurements of the vehicle's velocity, acceleration, and roll rates are combined to produce error signals for the pitch, yaw, and thrust of the vehicle. These error signals are then mixed to produce the axial engine valve settings.

#### INPUT

AE_SWITCH	AE_TEMP
A_ACCELERATION	CHUTE_RELEASED
CL	CONTOUR_CROSSED
DELTA_T	ENGINES_ON_ALTITUDE
FRAME_COUNTER	FRAME_ENGINES_IGNITED
FULL_UP_TIME	GA
GAX	GP1
GP2	GPY
GP_ALTITUDE	GP_ATTITUDE
GP_ROTATION	GP_VELOCITY
GQ	GR
GRAVITY	GV
GVE	GVEI
GVI	GW
GW1	INTERNAL_CMD
OMEGA	PE_INTEGRAL
PE_MAX	PE_MIN
TE_DROP	TE_INIT
TE_INTEGRAL	TE_LIMIT
TE_MAX	TE_MIN
VELOCITY_ERROR	YE_INTEGRAL
YE_MAX	YE_MIN

#### OUTPUT

AE_CMD	AE_STATUS
AE_TEMP	INTERNAL_CMD
PE_INTEGRAL	TE_INTEGRAL

TE_LIMIT	YE_INTEGRAL
----------	-------------

**PROCESS** The reader should refer to section A.9 for notes on integration. Note that once the correct value of AE\_CMD has been determined, it will automatically be transmitted to the engines during the next call to the GCS\_SIM\_RENDEZVOUS routine provided in the GCS\_SIM rendezvous package. (See section A.8. Implementation Notes). Computation of the axial engine valve settings requires the following steps:

✓ **PROCESSING WHEN AXIAL ENGINES ARE OFF**

- IF AE\_SWITCH is set to OFF, then perform the following steps:
  - Set all elements of AE\_CMD to 0
  - Proceed directly to the step "SET AXIAL ENGINE STATUS TO HEALTHY."

✓ **PROCESSING WHEN AXIAL ENGINES ARE ON**

The variable CL is used here as a subscript. Explanations for the variables CL and VELOCITY\_ERROR are provided in functional unit 2.6 GP. The variables PE\_INTEGRAL, YE\_INTEGRAL, and TE\_INTEGRAL will be initialized by INIT\_GCS.

- **If AE\_SWITCH is set to ON then perform the following steps:**

(Note:  $p_v$ ,  $q_v$ , and  $r_v$  are the current elements of GP\_ROTATION;  $\dot{x}_v$ ,  $\dot{y}_v$ , and  $\dot{z}_v$  are the current elements of GP\_VELOCITY;  $\ddot{x}_v$  is the current x component of A\_ACCELERATION.)

**DETERMINE ENGINE TEMPERATURE**

- Set AE\_TEMP according to Table A.5.1

Table A.5.1 DETERMINATION OF AXIAL ENGINE TEMPERATURE

CURRENT STATE			ACTION
AE_TEMP	GP_ALTITUDE	(FRAME_COUNTER - FRAME_ENGINES_IGNITED) · DELTA_T	AE_TEMP
cold	≤ ENGINES_ON_ALTITUDE	< FULL_UP_TIME	warming-up
warming-up	≤ ENGINES_ON_ALTITUDE	≥ FULL_UP_TIME	hot

**COMPUTE LIMITING ERRORS FOR PITCH**

$$\bullet \bullet \quad PE\_INTEGRAL = PE\_INTEGRAL + \int_{t_0}^t \frac{\dot{z}_v}{|\dot{x}_v|} dt ,$$

where  $t_0$  is the time at the beginning of this frame and  $t$  is the time at the end of this frame.

$$\bullet \bullet \quad P_e^L = GQ(CL) \cdot q_v + GW(CL) \cdot \left( \frac{\dot{z}_v}{|\dot{x}_v|} \right) + GWI(CL) \cdot PE\_INTEGRAL$$

$\bullet \bullet$  If  $P_e^L < PE\_MIN(CL)$  then set  $P_e^L$  to  $PE\_MIN(CL)$ .

$\bullet \bullet$  If  $P_e^L > PE\_MAX(CL)$  then set  $P_e^L$  to  $PE\_MAX(CL)$ .

### COMPUTE LIMITING ERROR FOR YAW

$$\bullet\bullet \quad YE\_INTEGRAL = YE\_INTEGRAL + \int_{t_0}^t \frac{\dot{y}_v}{|\dot{x}_v|} dt,$$

where  $t_0$  is the time at the beginning of this frame and  $t$  is the time at the end of this frame.

$$\bullet\bullet \quad Y_e^L = -GR(CL) \cdot r_v + GV(CL) \cdot \left( \frac{\dot{y}_v}{|\dot{x}_v|} \right) + GVI(CL) \cdot YE\_INTEGRAL$$

$\bullet\bullet$  If  $Y_e^L < YE\_MIN(CL)$  then set  $Y_e^L$  to  $YE\_MIN(CL)$ .

$\bullet\bullet$  If  $Y_e^L > YE\_MAX(CL)$  then set  $Y_e^L$  to  $YE\_MAX(CL)$ .

### COMPUTE LIMITING ERROR FOR THRUST

$\bullet\bullet$  If CONTOUR\_CROSSED is set to "contour not crossed", then proceed directly to the step "COMPUTE PITCH, YAW, AND THRUST ERRORS."

$\bullet\bullet$  If CONTOUR\_CROSSED is set to "contour crossed", then perform the following steps:

$$\bullet\bullet\bullet \quad TE\_INTEGRAL = TE\_INTEGRAL + \int_{t_0}^t (VELOCITY\_ERROR) dt$$

where  $t_0$  is the time at the beginning of this frame and  $t$  is the time at the end of this frame.

$\bullet\bullet\bullet$  Solve the following equation analytically in order to calculate the value for  $TE\_LIMIT$ :

$$\frac{d}{dt}(TE\_LIMIT) + OMEGA \cdot TE\_LIMIT = GA - GAX \cdot (\ddot{x}_v + GRAVITY \cdot GP\_ATTITUDE(1,3,0)) + GVE \cdot VELOCITY\_ERROR + GVEI(CL) \cdot TE\_INTEGRAL$$

$\bullet\bullet\bullet$  If  $TE\_LIMIT < TE\_MIN(CL)$  then set  $TE\_LIMIT$  to  $TE\_MIN(CL)$ .

$\bullet\bullet\bullet$  If  $TE\_LIMIT > TE\_MAX(CL)$  then set  $TE\_LIMIT$  to  $TE\_MAX(CL)$ .

### COMPUTE PITCH, YAW, AND THRUST ERRORS

- Compute pitch error ( $P_e$ ), Yaw Error ( $Y_e$ ), and Thrust Error ( $T_e$ ), according to Table A.5.2

Table A.5.2 DETERMINATION OF ERROR TERMS

CURRENT STATE			ACTIONS		
AE_SWITCH	CHUTE_RELEASED	CONTOUR_CROSSED	$P_e$	$Y_e$	$T_e$
1	1	1	$P_e^L$	$Y_e^L$	TE_LIMIT
1	1	0	$P_e^L$	$Y_e^L$	TE_DROP
1	0	0,1	$GQ(CL) \cdot q_v$	$-GR(CL) \cdot r_v$	TE_INIT

### COMPUTE AXIAL ENGINE VALVE SETTINGS

Given pitch, yaw, and thrust errors, ( $P_e, Y_e, T_e$ ), the valve settings (AE\_CMD) for each of the three main engines are calculated as:

$$\text{INTERNAL\_CMD} = \begin{pmatrix} GP1 & 0 & 1 \\ GP2 & -GPY & 1 \\ GP2 & GPY & 1 \end{pmatrix} \times \begin{pmatrix} P_e \\ Y_e \\ T_e \end{pmatrix}$$

which will result in each element of the INTERNAL\_CMD vector being a real value. This value should be converted into an integer value between 0 and 127 and placed into the appropriate element of the AE\_CMD vector. The mapping for the conversion from real to integer values for each of the three elements should be as follows:

Table A.5.3 DETERMINATION OF AXIAL ENGINE COMMANDS

CURRENT STATE	ACTIONS
INTERNAL_CMD	AE_CMD
$I < 0.0$	$A = 0$
$0.0 \leq I \leq 1.0$	$0 \leq A \leq 127$
$1.0 < I$	$A = 127$

Note: "I" represents the appropriate element of the vector INTERNAL\_CMD  
 "A" represents the appropriate element of the vector AE\_CMD

with INTERNAL\_CMD between 0 and 1.0 being converted *linearly* to a value of AE\_CMD between 0 and 127. Each value for AE\_CMD is to be rounded to the nearest integer, where rounding is defined as follows:

Let  $x$  represent the real value that is to be rounded

Then,  $AE\_CMD = \text{the integer part of } (x+0.5)$

✓ **SET AXIAL ENGINE STATUS TO HEALTHY**

- Set  $AE\_STATUS$  to healthy.



## ARSP -- Altimeter Radar Sensor Processing (P-Spec 2.1.2)

**PURPOSE** The vehicle has one altimeter radar. The ARSP functional unit reads the altimeter counter provided by this radar and converts the data into a measure of distance to the surface.

### INPUT

AR_ALTITUDE	AR_COUNTER
AR_FREQUENCY	AR_STATUS
K_ALT	

### OUTPUT

AR_ALTITUDE	AR_STATUS
K_ALT	

**PROCESS** The processing of the altimeter counter data (AR\_COUNTER) into the vehicle's altitude above the planet's terrain depends on whether or not an echo is received by the altimeter radar for the current time step. The distance covered by the radio pulses emitted from the altimeter radar is directly proportional to the time between transmission and reception of its echo. A digital counter (AR\_COUNTER) is started as the radar pulse is transmitted. The counter increments AR\_FREQUENCY times per second. If an echo is received, the lower order fifteen bits of AR\_COUNTER contain the pulse count, and the sign bit will contain the value zero. If an echo is not received, AR\_COUNTER will contain sixteen one bits.

✓ **ROTATE VARIABLES**

- Rotate AR\_ALTITUDE, AR\_STATUS, AND K\_ALT.

✓ **DETERMINE ALTITUDE**

- If an echo is received, perform the following:
  - Convert the AR\_COUNTER value to a distance to be returned in the variable AR\_ALTITUDE according to the following equation:

$$AR\_ALTITUDE = \frac{AR\_COUNTER \cdot 3 \times 10^8 \frac{m}{sec}}{AR\_FREQUENCY \cdot 2}$$

- If an echo is not received, compute AR\_ALTITUDE as follows:
    - If all four previous values of AR\_STATUS are healthy:
      - In order to smooth the estimate of altitude, fit a third-order polynomial to the previous four values of AR\_ALTITUDE.
      - Use this polynomial to extrapolate a value for AR\_ALTITUDE for the current time step.
    - If any of the previous four values of AR\_STATUS is failed:
      - Set the current value of AR\_ALTITUDE equal to the previous value of AR\_ALTITUDE.
- ✓ **SET ALTIMETER RADAR STATUS**
- Set the current values for AR\_STATUS and K\_ALT according to TABLE A.5.4.

Table A.5.4 DETERMINATION OF ALTITUDE STATUS

CURRENT STATE		ACTIONS	
ECHO RETURNED?	All 4 previous AR_STATUS values healthy?	AR_STATUS	K_ALT
yes	d	healthy	1
no	yes	failed	1
no	no	failed	0

Note: "d" = don't care condition

## ASP -- Accelerometer Sensor Processing (P-Spec 2.1.1)

**PURPOSE** Three accelerometers, located at the vehicle's center of gravity, are slightly misaligned along the vehicle's  $\vec{x}_v$ ,  $\vec{y}_v$ , and  $\vec{z}_v$  axes. Each accelerometer produces a 16-bit binary value (A\_COUNTER), represented as the magnitude portion of a sign magnitude number which is a linear function of the acceleration along its axis. The sign of the counter will always be positive, but the offset given in A\_BIAS will be negative or zero. The Acceleration Sensor Processing (ASP) functional unit provides measures of the vehicle accelerations through the conversion and digital filtering of this raw accelerometer data.

### INPUT

ALPHA_MATRIX	ATMOSPHERIC_TEMP
A_ACCELERATION	A_BIAS
A_COUNTER	A_GAIN_0
A_SCALE	A_STATUS
G1	G2

### OUTPUT

A_ACCELERATION	A_STATUS
----------------	----------

**PROCESS** The processing of the accelerometer data (A\_COUNTER) into vehicle accelerations (A\_ACCELERATION) requires the following steps:

- ✓ **ROTATE VARIABLES**
  - Rotate A\_ACCELERATION and A\_STATUS.

- ✓ **ADJUST GAIN FOR TEMPERATURE**

The standard gain (A\_GAIN\_0) must be adjusted for the effects of temperature prior to the conversion of the raw accelerometer values. The adjusted gain is a quadratic function of the ambient temperature (ATMOSPHERIC\_TEMP) and the standard gain.

- Adjust the gain for temperature as follows:

$$A\_GAIN(i) = A\_GAIN\_0(i) + (G1 \cdot ATMOSPHERIC\_TEMP) + (G2 \cdot ATMOSPHERIC\_TEMP^2)$$

where  $i$  ranges from 1 to 3 and represents the three directions x, y, and z, and where A\_GAIN\_0 is the standard gain.

✓ **REMOVE CHARACTERISTIC BIAS**

Each accelerometer has a characteristic DC bias (A\_BIAS) which must be removed from the signal prior to conversion. The acceleration is a linear function of its A\_COUNTER value where the gain specifies the slope and the offset (A\_BIAS) specifies the intercept.

- Remove the bias as follows:

$$A\_ACCELERATION\_M(i) = A\_BIAS(i) + A\_GAIN(i) * A\_COUNTER(i)$$

where  $i$  ranges from 1 to 3 and represents the three directions x, y, and z.

✓ **CORRECT FOR MISALIGNMENT**

Each accelerometer is slightly misaligned from the true vehicle axes. The multiplier matrix (ALPHA\_MATRIX) which is shown below, is based on small angle approximations and corrects for this misalignment. It is used for transforming the measured acceleration data into the true vehicle accelerations.

$$ALPHA\_MATRIX = \begin{pmatrix} 1 & -\alpha_{xz} & \alpha_{xy} \\ \alpha_{yz} & 1 & -\alpha_{yx} \\ -\alpha_{zy} & \alpha_{zx} & 1 \end{pmatrix}$$

$\alpha_{xy}$  defines the angle of rotation about the vehicle's  $\bar{y}_v$  axis between the  $\bar{x}_v$  axis and the misaligned  $\bar{x}_v$  axis. The other misalignment angles are defined similarly, based upon a right-handed coordinate system.

- Compute preliminary current value of A\_ACCELERATION as follows:

$$A\_ACCELERATION = ALPHA\_MATRIX \times A\_ACCELERATION\_M$$

✓ **DETERMINE ACCELERATIONS AND ACCELEROMETER STATUS**

The variable A\_STATUS is a four-element array in each of the three physical dimensions, and contains the present and previous three values of status for each accelerometer. The variable A\_ACCELERATION is a five-element array in each of the three dimensions (x, y, and z). A\_ACCELERATION contains the present and previous four values of acceleration.

- The following steps are described for the  $x$  axis but should be performed for each axis:
  - If one or more of the previous three values of A\_STATUS is unhealthy, leave the current value of A\_ACCELERATION unchanged, set the current value of A\_STATUS to healthy, and do no further processing for this axis.
  - If all three of the previous values of A\_STATUS are healthy and all three of the previous values of A\_ACCELERATION are equal to each other, leave the current

value of A\_ACCELERATION unchanged, set the current value of A\_STATUS to healthy, and do no further processing for this axis.

- If all three of the previous values of A\_STATUS are healthy, and it is not true that all three of the previous values of A\_ACCELERATION are equal to each other, check for extreme values and set A\_STATUS and A\_ACCELERATION according to the method described below. The accelerometer processing includes filtering of the calculated accelerations along each axis (i.e. filtering of  $(\ddot{x}_v, \ddot{y}_v, \ddot{z}_v)_t$ ), and ignoring or eliminating calculated accelerations which are out of range. To effect this filtering, the means and standard deviations for each component of acceleration are to be computed using the calculated accelerations from the previous three time steps. That is, for the current time step  $t$  and the measurement of acceleration along the  $x$  axis:

- Calculate

$$\hat{\mu} = \sum_{i=t-3}^{t-1} \frac{\ddot{x}_{v(i)}}{3}$$

which is the current sample mean

- Calculate

$$\hat{\sigma} = \sqrt{\frac{\sum_{i=t-3}^{t-1} (\ddot{x}_{v(i)} - \hat{\mu})^2}{3}}$$

which is the current sample standard deviation.

- If  $|\hat{\mu} - \ddot{x}_v(t)| > A\_SCALE \cdot \hat{\sigma}$

set  $\ddot{x}_v(t)$  to  $\hat{\mu}$

set A\_STATUS to unhealthy

where  $\ddot{x}_v(t)$  is the acceleration along the  $x$  axis for the current time step. Similar equations hold for eliminating outliers in the measures of acceleration along the  $y$  and  $z$  axes.

otherwise

set A\_STATUS to healthy

In summary, if the calculated acceleration for the current time step for any component differs from the mean by more than A\_SCALE times the standard

deviation, then that component of acceleration should be replaced by its current mean and A\_STATUS should be set to unhealthy.

If the calculated acceleration for any component is within the specified range of the mean, then the preliminary value of A\_ACCELERATION should remain unchanged and A\_STATUS should be set to healthy.

## CP -- Communications Processing (P-Spec 2.4)

**PURPOSE** Data from the vehicle sensors and guidance processor is relayed back to the orbiting platform for later analysis. The CP functional unit converts the sensed data into a data packet appropriate for radio transmission.

### INPUT

AE_CMD	AE_STATUS
AE_TEMP	AR_ALTITUDE
AR_STATUS	ATMOSPHERIC_TEMP
A_ACCELERATION	A_STATUS
CHUTE_RELEASED	COMM_SYNC_PATTERN
CONTOUR_CROSSED	C_STATUS
FRAME_COUNTER	GP_ALTITUDE
GP_ATTITUDE	GP_PHASE
GP_ROTATION	GP_VELOCITY
G_ROTATION	G_STATUS
K_ALT	K_MATRIX
PE_INTEGRAL	RE_CMD
RE_STATUS	SUBFRAME_COUNTER
TDLR_STATE	TDLR_STATUS
TDLR_VELOCITY	TDS_STATUS
TD_SENSED	TE_INTEGRAL
TS_STATUS	VELOCITY_ERROR
YE_INTEGRAL	

### OUTPUT

C_STATUS	PACKET
----------	--------

**PROCESS** The data packet (PACKET) prepared for transmission is organized to sequentially contain a message and a checksum. The message consists of the synchronization pattern, sequence number, sample mask, and data section. The data packet created will automatically be transmitted during the next call to GCS\_SIM\_RENDEZVOUS.

- ✓ **SET COMMUNICATOR STATUS TO HEALTHY**
  - Set C\_STATUS to healthy.

The construction of the packet requires the following steps:

- ✓ **CONSTRUCT PACKET:**
  - GET SYNCHRONIZATION PATTERN

The synchronization pattern is provided in the variable COMM\_SYNC\_PATTERN. It is a 16-bit pattern dictated by the design of the receiving communications equipment.

- DETERMINE SEQUENCE NUMBER

The sequence number identifies the packet of data that is being sent. It is a byte value in the range 0..255. The sequence number will be 0 during the first subframe of frame number 1. Sequence numbers increase by one every subframe, except that the values repeat after the 256th packet. The sequence number can be calculated based on the values of the variables FRAME\_COUNTER and SUBFRAME\_COUNTER.

- PREPARE SAMPLE MASK

The sample mask is a Boolean vector where "ones" represent variables that have been sampled since the previous transmission. Any variables listed in Table A.5.5 that may have changed during the present subframe should be marked in the mask and transmitted, with one exception. The variable TE\_INTEGRAL may be changed by GP in the second subframe and by AECLP in the third subframe; however, TE\_INTEGRAL should be transmitted by CP only during the third subframe, and not during the second subframe. In the case of any "history variable", that is, one which contains a time dimension, only the object (scalar, vector, or array) with a time subscript of zero should be transmitted. Each bit position in the mask represents a particular variable listed in Table A.5.5. The leftmost bit of the mask corresponds to AE\_CMD, and moving across the mask from left to right, the next mask bit corresponds to the next variable in Table A.5.5 (in row order).

- PREPARE DATA SECTION

The data section of the packet contains the sixteen bit values for the elements of the variables in Table A.5.5 that may have new samples available. Once it has been determined which variables should be transmitted for this particular subframe, those variables should be packed into the data section. Although the length of the variable PACKET is fixed, the number of bytes of PACKET which contain actual variables to be transmitted will vary depending on the values of FRAME\_COUNTER and SUBFRAME\_COUNTER. The variables to be transmitted should be concatenated so that there are no unused bytes between the data to be transmitted. There may however be unused bytes following the checksum. The data are concatenated in the order given by the sample mask, starting with the most significant bit (i.e. left most bit). Variables should be packed to the nearest byte boundary; thus, a single element of PACKET could contain a logical\*1 and the first byte of the variable that follows it. Arrays should be sent with the first index changing most rapidly. It should be noted that some arrays have



terms that are constant (e.g. the off-diagonal terms of K\_MATRIX and the diagonal terms of GP\_ROTATION) and since these terms can never have "new" values, they should not be transmitted. The values in Table A.5.5 should be sent in row order, starting at the top of the table. The first value in alphabetical order goes next to the mask in the packet.

- CALCULATE CHECKSUM

The checksum is calculated for the message using the standard CRC-16 polynomial as defined in (ref. A.11). Table A.5.7 illustrates the byte structure of the packet. The unused part of PACKET should be ignored in the calculation of the checksum. The checksum should be placed in the two bytes immediately following the message for this subframe. Refer to Appendix D for a detailed description of the packet and for specific instructions on the checksum calculation.

Table A.5.5 PACKET VARIABLES

AE_CMD	AE_STATUS	AE_TEMP
AR_ALTITUDE	AR_STATUS	ATMOSPHERIC_TEMP
A_ACCELERATION	A_STATUS	CHUTE_RELEASED
CONTOUR_CROSSED	C_STATUS	GP_ALTITUDE
GP_ATTITUDE	GP_PHASE	GP_ROTATION
GP_VELOCITY	G_ROTATION	G_STATUS
K_ALT	K_MATRIX	PE_INTEGRAL
RE_CMD	RE_STATUS	TDLR_STATE
TDLR_STATUS	TDLR_VELOCITY	TDS_STATUS
TD_SENSED	TE_INTEGRAL	TS_STATUS
VELOCITY_ERROR	YE_INTEGRAL	

Note: when read by rows, this table represents the alphabetical listing of variables that are to appear in the data section of the packet.

Table A.5.6 SAMPLE MASK

INFORMATION SENT	A	B	C	...	Z
EXAMPLE MASK	1	1	0	...	1

Note: this table gives information only on the order of the packet. The packet should be packed to a byte-boundary limit into integer\*2 elements.

Table A.5.7 PACKET BYTE STRUCTURE

Subframe 1 Byte Positions	Subframe 2 Byte Positions	Subframe 3 Byte Positions	CONTENTS (Cells in bold italics with double-line border constitute the	
1	1	1	<b><i>SYNCHRONIZATION PATTERN</i></b>	
2	2	2		
3	3	3	<b><i>SEQUENCE NUMBER</i></b>	
4	4	4	<b><i>SAMPLE MASK</i></b>	
5	5	5		
6	6	6		
7	7	7		
8	8	8	<b><i>DATA SECTION</i></b>	
.	.	.		
.	.	.		
.	.	.		
129	173	45		
130	174	46		CHECKSUM
131	175	47		
132	176	48		NOT USED
.	.	.		
.	.	.		
512	512	512		

Note: The variables inserted into PACKET are inserted in the VAX standard byte order.

### CRCP -- Chute Release Control Processing (P-Spec 2.3.3)

**PURPOSE** The CRCP functional unit implements the release of the parachute which is attached prior to the beginning of the terminal descent phase.

**INPUT**

AE_TEMP	CHUTE_RELEASED
---------	----------------

**OUTPUT**

CHUTE_RELEASED
----------------

**PROCESS** If the chute has been released, leave CHUTE\_RELEASED unchanged and this signal will be automatically transmitted to the chute release mechanism during the next call to GCS\_SIM\_RENDEZVOUS. If the chute has not been released, the engine temperature will determine whether or not to release the chute. If the chute has not been released and the engines are hot (i.e. AE\_TEMP is HOT), then release the chute by setting CHUTE\_RELEASED to "chute released."

## GP -- Guidance Processing (P-Spec 2.2)

**PURPOSE** GP uses the information available from ASP, ARSP, CRCP, GSP, TDLRSP, and TDSP and the results of its previous computations to control the vehicle's state during terminal descent.

### INPUT

AE_SWITCH	AE_TEMP
AR_ALTITUDE	A_ACCELERATION
CHUTE_RELEASED	CL
CONTOUR_ALTITUDE	CONTOUR_CROSSED
CONTOUR_VELOCITY	DELTA_T
DROP_HEIGHT	DROP_SPEED
ENGINES_ON_ALTITUDE	FRAME_COUNTER
GP_ALTITUDE	GP_ATTITUDE
GP_PHASE	GP_VELOCITY
GRAVITY	G_ROTATION
K_ALT	K_MATRIX
MAX_NORMAL_VELOCITY	RE_SWITCH
TDLR_VELOCITY	TDS_STATUS
TD_SENSED	

### OUTPUT

AE_SWITCH	CL
CONTOUR_CROSSED	FRAME_ENGINES_IGNITED
GP_ALTITUDE	GP_ATTITUDE
GP_PHASE	GP_ROTATION
GP_VELOCITY	RE_SWITCH
TE_INTEGRAL	VELOCITY_ERROR

**ARRAYS** The variables GP\_ATTITUDE, GP\_ALTITUDE, and GP\_VELOCITY are five element arrays in each of their history dimensions and contain enough previous values to provide the required history for integration in updating the vehicle and guidance states.

**PROCESS** The Guidance Processor computes the velocity, altitude, and attitude to be used in controlling the engines.

✓ **ROTATE VARIABLES**

- Rotate GP\_ATTITUDE, GP\_ALTITUDE, and GP\_VELOCITY.

✓ **SET UP THE GP\_ROTATION MATRIX**

G\_ROTATION contains three values: p, q, and r, in that order. These values must be placed into a 3 x 3 matrix (GP\_ROTATION) in the correct positions for later calculations. Note that GP\_ROTATION does not include any time histories; thus it may be convenient to use a temporary variable during calculation to hold the time histories of GP\_ROTATION or to use

elements directly from G\_ROTATION; however, GP\_ROTATION does describe the correct matrix orientation for operations and upon exiting from GP should contain the correct values for the present time step.

- Place the values from G\_ROTATION into GP\_ROTATION as shown:

$$GP\_ROTATION = \begin{pmatrix} 0 & r_v & -q_v \\ -r_v & 0 & p_v \\ q_v & -p_v & 0 \end{pmatrix}$$

✓ **CALCULATE NEW VALUES OF ATTITUDE, VELOCITY, AND ALTITUDE**

The attitude, velocity, and altitude are each calculated by:

1. finding a rate of change from known values, and then
2. integrating this rate of change through one time step by some method of integration providing the accuracy specified. That is:

$$X_t = X_{t-1} + \int_{t-1}^t \dot{X} dt$$

where  $\dot{X}$  represents the rate of change of attitude, velocity, or altitude.

Table A.5.8 gives the equations for the rates of change for each of the variables GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE.

- Solve for the current values of GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE using the equation for  $X_t$  given above, Table A.5.8, and an appropriate integration method (see section A.9 *Numerical Integration Instructions*).

Table A.5.8 DIFFERENTIAL EQUATIONS

$\frac{d(GP\_ATTITUDE)}{dt} = GP\_ROTATION \times GP\_ATTITUDE$
$\frac{d(GP\_VELOCITY)}{dt} = GP\_ROTATION \times GP\_VELOCITY$ $+ GP\_ATTITUDE \times \begin{pmatrix} 0 \\ 0 \\ GRAVITY \end{pmatrix} + A\_ACCELERATION + K\_MATRIX \times (TDLR\_VELOCITY - GP\_VELOCITY)$
$\frac{d(GP\_ALTITUDE)}{dt} = - \left( GP\_ATTITUDE \times \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \right)^T \times GP\_VELOCITY + K\_ALT \cdot (AR\_ALTITUDE - GP\_ALTITUDE)$

✓ **DETERMINE IF ENGINES SHOULD BE ON OR OFF**

Note that RE\_SWITCH is initialized to on, while AE\_SWITCH is initialized to off, and FRAME\_ENGINES\_IGNITED is initialized by INIT\_GCS. Use Table A.5.9 to determine whether to turn axial engines on (set AE\_SWITCH to on and set FRAME\_ENGINES\_IGNITED) or whether to turn axial and roll engines off (set AE\_SWITCH and RE\_SWITCH to off).

TABLE A.5.9 DETERMINATION OF AXIAL AND ROLL ENGINE ON/OFF SWITCHES

CURRENT STATE					ACTIONS		
AE_SWITCH	GP_ALTITUDE	$(\sqrt{\text{velocity\_expression}^1 + \text{xcomponent of GP\_VELOCITY}}) \leq \text{MAX\_NORMAL\_VELOCITY} ?$	Have engines been turned off in any prior frame?	TD_SENSED	FRAME_ENGINES_IGNITED	AE_SWITCH	RE_SWITCH
off	$\leq \text{ENGINES\_ON\_ALTITUDE}$	d	no	not sensed	current FRAME_COUNTER	on	
on	$\leq \text{DROP\_HEIGHT}$	yes	d	not sensed		off	off
on	d	d	d	sensed		off	off

$$^1 \text{velocity\_expression} = 2 \cdot \text{GRAVITY} \cdot \text{maximum}(\text{GP\_ALTITUDE}, 0)$$

Note: A blank box under "ACTIONS" indicates no action is to be taken

"d" = don't care condition

✓ **DETERMINE VELOCITY ERROR**

The velocity-altitude contour consists of a set of points of which one coordinate is the altitude of the craft and the other coordinate is the optimal x component of velocity at the altitude given by the first coordinate. The altitude and optimal velocity coordinates are held in the CONTOUR\_ALTITUDE and CONTOUR\_VELOCITY arrays respectively. The altitude coordinates are in the CONTOUR\_ALTITUDE array contiguous to each other, in ascending numerical order, beginning with the first element of the array. Any unused elements of the array have been filled with zeroes (the value of zero will not be used as an actual value for altitude). There are at least two valid non-zero altitude values in the table. The two arrays are related such that for a given value of altitude in CONTOUR\_ALTITUDE, the corresponding value in CONTOUR\_VELOCITY is the optimal velocity x component at that altitude. For any altitude that is not explicitly listed in CONTOUR\_ALTITUDE, the value for optimal velocity can be found by linear interpolation (or extrapolation if the value is outside the range of the altitude array). The velocity error (VELOCITY\_ERROR) is the difference between

the actual x component of the velocity of the craft (GP\_VELOCITY) and the optimal velocity x component at the vehicle altitude. Figure A.5.1 illustrates the velocity-altitude contour.

- The optimal velocity should be calculated by finding the present altitude in CONTOUR\_ALTITUDE and then locating the corresponding velocity in CONTOUR\_VELOCITY, using interpolation or extrapolation if necessary. Let *optimal\_velocity* represent the value obtained from the contour arrays, whether extracted, interpolated, or extrapolated.
- Calculate VELOCITY\_ERROR as follows:  
$$\text{VELOCITY\_ERROR} = \text{x component of GP\_VELOCITY} - \textit{optimal\_velocity}$$

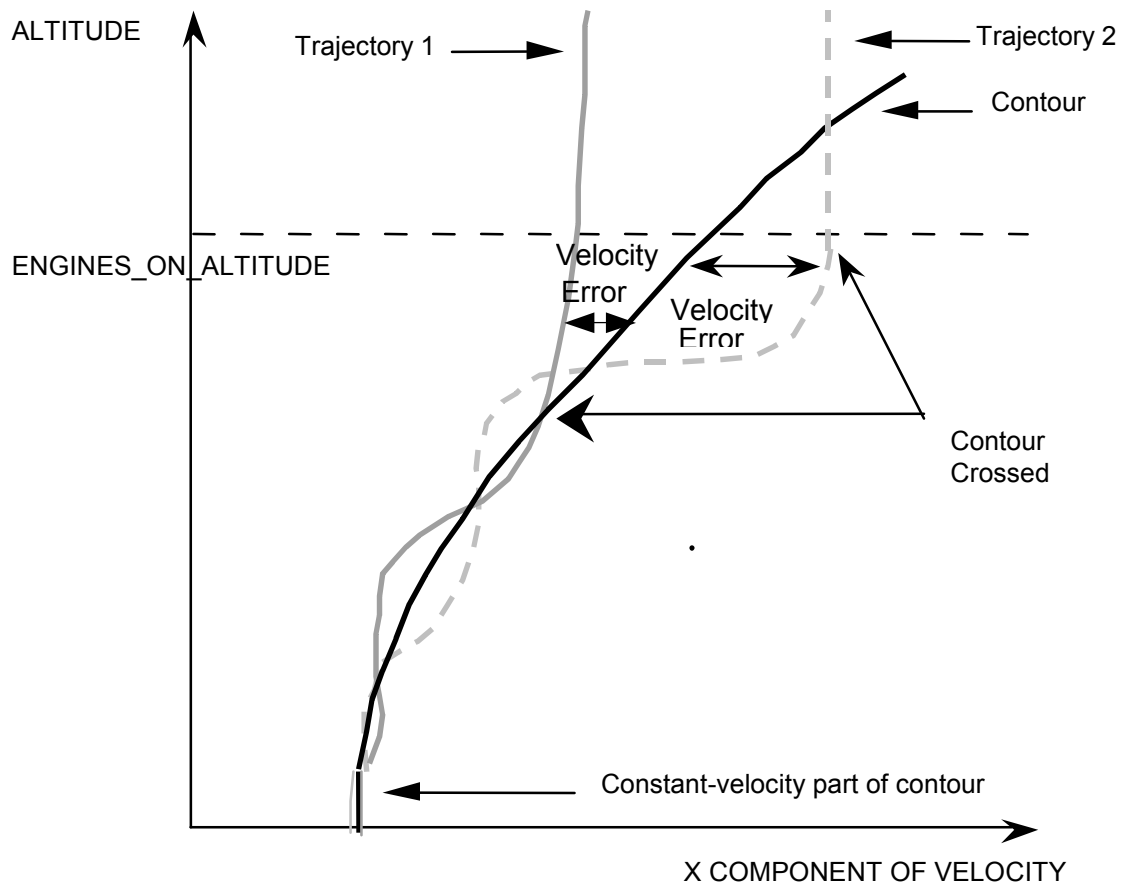
✓ **DETERMINE IF CONTOUR HAS BEEN CROSSED**

- If GP\_ALTITUDE ≤ ENGINES\_ON\_ALTITUDE, then check whether the contour has been crossed as follows:
  - If CONTOUR\_CROSSED = "contour not crossed" and VELOCITY\_ERROR ≥ 0, then set CONTOUR\_CROSSED to "contour crossed". Otherwise CONTOUR\_CROSSED should remain unchanged.

Figure A.5.1 shows two possible trajectories, with the point along each where the contour is first sensed and also an example of VELOCITY\_ERROR. Note: the altitude where the engines are turned on should be the earliest point to check crossing the contour, even though the trajectory may have crossed the contour at some greater altitude.



Figure A.5.1 VELOCITY-ALTITUDE CONTOUR



✓ **DETERMINE GUIDANCE PHASE**

- The guidance phase (GP\_PHASE) is determined according to the events in Table A.5.10. These phases are based upon information that may be provided by processes other than the guidance processor.

The current phase (GP\_PHASE) and the event are to be used where appropriate to reset GP\_PHASE to the next phase. If there is no combination of current phase and event from the table that is true, then GP\_PHASE should not be changed. Note that the two columns labeled "CURRENT STATE DESCRIPTION" and "NEXT STATE DESCRIPTION" are for informational purposes only, and are not used in the setting of GP\_PHASE.

Table A.5.10 DETERMINATION OF GUIDANCE PHASE

CURRENT STATE			NEXT STATE	
GP_PHASE	CURRENT STATE DESCRIPTION	EVENT	ACTION	NEXT STATE DESCRIPTION
1	Chute attached Engines off Touch Down not sensed	Altitude for turning engines on is sensed	2	Chute attached Engines on Touch down not sensed
2	Chute attached Engines on Touch down not sensed	Axial Engines become hot and the chute is released	3	Chute released Axial Engines Hot Touch down not sensed
2	Chute attached Engines on Touch down not sensed	Touched down is sensed	5	Chute attached Engines off Touch down sensed
3	Chute released Axial Engines Hot Touch down not sensed	Altitude $\leq$ DROP_HEIGHT and TDS_STATUS = healthy and Touch down not sensed and $(\sqrt{\text{velocity\_expression}}^1 + \text{xcomponentofGP\_VELOCITY}) \leq \text{MAX\_NORMAL\_VELOCITY}$	4	Chute released Engines off Touch down not sensed
3	Chute released Axial Engines Hot Touch down not sensed	Altitude $\leq$ DROP_HEIGHT and TDS_STATUS = failed	5	Chute released Engines off Touch down not sensed
3	Chute released Axial Engines Hot Touch down not sensed	Touch down is sensed	5	Chute released Engines off Touch down sensed
4	Chute released Engines off Touch down not sensed	Touch down is sensed	5	Chute released Engines off Touch down sensed
4	Chute released Engines off Touch down not sensed	TDS_STATUS = failed	5	Chute released Engines off Touch down not sensed

$$^1 \text{velocity\_expression} = 2 \cdot \text{GRAVITY} \cdot \text{maximum}(\text{GP\_ALTITUDE}, 0)$$

- PHASE 1: If the altitude provided by the guidance processor is less than or equal to the ENGINES\_ON\_ALTITUDE, set GP\_PHASE = 2.
- PHASE 2: If the axial engines have become hot and the parachute has been released, set GP\_PHASE = 3. If touch down is sensed, set GP\_PHASE = 5.
- PHASE 3: If touch down has not been sensed and DROP\_HEIGHT has not been reached, then control the axial and roll engines to cause the lander to follow a gravity-turn steering descent. If DROP\_HEIGHT is reached and touch down is not sensed and

$$\sqrt{2 \cdot GRAVITY \cdot \text{maximum}(GP\_ALTITUDE, 0)} + x \text{ component of } GP\_VELOCITY \leq MAX\_NORMAL\_VELOCITY$$

and TDS\_STATUS = healthy, then set GP\_PHASE = 4. If DROP\_HEIGHT is reached, and TDS\_STATUS = failed, then set GP\_PHASE = 5. If touch down is sensed, then set GP\_PHASE = 5.

- PHASE 4: If touch down has not been sensed and TDS\_STATUS is healthy, then take no action. If TDS\_STATUS is failed, then set GP\_PHASE to 5. If touch down has been sensed, set GP\_PHASE to 5.

✓ **DETERMINE WHICH SET OF CONTROL LAW PARAMETERS TO USE**

The "Control Law Parameters" are a subset of the variables in the global data store named "RUN\_PARAMETERS." This subset consists of the following variables: GVEI, GV, GVI, GR, GW, GWI, GQ, PE\_MIN, PE\_MAX, TE\_MIN, TE\_MAX, YE\_MIN, and YE\_MAX. Note that each one of these variables is an array of two elements. The elements with a subscript of one will be referred to as the "first" set of Control Law Parameters, while the elements with a subscript of two will be referred to as the "second" set of Control Law Parameters.

The variable CL is used to control which set of Control Law Parameters is used in the control laws at any given time by the functional unit AECLP. The functional unit GP must determine the value of CL for use by AECLP. The variable CL has two valid values, namely "first" which means that the first set of Control Law Parameters should be used by AECLP, and "second" which means that the second set of Control Law Parameters should be used by AECLP in the equations for  $P_e$ ,  $Y_e$ ,  $P_e^L$ ,  $Y_e^L$ , and TE\_LIMIT. See the Data Requirements Dictionary for the actual numeric values for CL which correspond to "first" and "second." The variable CL is initialized to the value "first" by INIT\_GCS, and thus the first set of parameters will be used by AECLP until CL is changed. The second set of Control Law Parameters should be used by AECLP at the first point where the lander crosses the constant-velocity part of the Velocity-Altitude contour. The constant-velocity part of the contour consists of the four sets of coordinates with the smallest altitudes and for which the CONTOUR\_VELOCITY elements are exactly equal to the value DROP\_SPEED. The GUIDANCE PROCESSOR (GP) must determine when to begin using the second set of Control Law Parameters, as follows:

- If the following conditions are true:
  - CL = first, and
  - optimal\_velocity = DROP\_SPEED, and
  - x component of GP\_VELOCITY < DROP\_SPEED

Then

Set CL = second

Set TE\_INTEGRAL = 0.0

## GSP -- Gyroscope Sensor Processing (P-Spec 2.1.4)

**PURPOSE** Three fiber-optic ring gyroscopes are located on the lander, one for each of the *x*, *y*, and *z* axes. The Gyroscope Sensor Processing (GSP) functional unit provides a measure of the vehicle's rotation rates through the conversion and filtering of the raw gyroscope data.

### INPUT

ATMOSPHERIC_TEMP	G3
G4	G_COUNTER
G_GAIN_0	G_OFFSET
G_ROTATION	

### OUTPUT

G_ROTATION	G_STATUS
------------	----------

**PROCESS** The output from each of the gyroscopes is a 16-bit quantity (G\_COUNTER) divided into 2 parts: the lower 14 bits represent the vehicle's rate of rotation about that axis and the high-order bit represents the direction of this rotation. This is a sign-magnitude representation of the counter value that only uses the lower 14 bits of the magnitude portion of the number. Following is a map of G\_COUNTER:

15	14	13	12	11	...	0
D	X	MAGNITUDE				

where D = direction, and X = unused. The high bit set to 1 indicates a negative rotation consistent with a right-handed coordinate system.

#### ✓ ROTATE VARIABLES

- Rotate G\_ROTATION.

#### ✓ ADJUST GAIN

The standard gain (G\_GAIN\_0) must be adjusted for the effects of temperature prior to the conversion of the raw gyroscope values. The adjusted gain is a quadratic function of the ambient temperature (ATMOSPHERIC\_TEMP) and the standard gain.

That is,

$$G\_GAIN(i) = G\_GAIN\_0(i) + (G3 \cdot ATMOSPHERIC\_TEMP) + (G4 \cdot ATMOSPHERIC\_TEMP^2)$$

where *i* ranges from 1 to 3 and represents the three directions *x*, *y*, and *z*.

✓ **CONVERT G\_COUNTER**

The rotation rate is linear with respect to the unprocessed gyroscope values, i.e. the lower 14 bits must be converted. G\_GAIN is the multiplier for this conversion and G\_OFFSET is the constant offset. The equation for converting counter to rotation then becomes:

$$G\_ROTATION(i) = G\_OFFSET(i) + G\_GAIN(i) * (G\_COUNTER(i))$$

where  $i$  ranges from 1 to 3 and represents the three directions x, y, and z.

✓ **SET GYROSCOPE STATUS TO HEALTHY.**

- Set G\_STATUS to healthy.

## RECLP -- Roll Engine Control Law Processing (P-Spec 2.3.2)

**PURPOSE** RECLP generates the roll engine command which controls the firing pulse and direction of the roll engines.

### INPUT

DELTA_T	G_ROTATION
P1	P2
P3	P4
RE_SWITCH	THETA
THETA1	THETA2

### OUTPUT

RE_CMD	RE_STATUS
THETA	

**PROCESS** Roll control of the lander is achieved by generating the roll commands as functions of the differences between the actual and desirable values for the roll angle and rate. These differences are limited, and the control commands are proportional to them. Note that once the roll command (RE\_CMD) has been set with the correct value, it will automatically be sent to the engines during the next call to GCS\_SIM\_RENDEZVOUS. The steps to be performed are as follows:

- ✓ **DETERMINE IF ENGINES ARE ON**
  - If RE\_SWITCH is off, then set RE\_CMD to 1, and proceed directly to the step "SET ROLL ENGINE STATUS TO HEALTHY."
  
- ✓ **DETERMINE PULSE INTENSITY AND DIRECTION**
  - The pulse intensity and direction are derived from the graph shown in Figure A.5.2 using  $(p_v)_i$ . For each region of the graph, the intensity is given, followed by the direction inside parentheses. Note that the x axis represents the integral of the roll rate. This is really the present angle of roll. This integral should be calculated by Euler's method (see section A.9). As an example, THETA = THETA + (integral of roll rate for this frame). The variable THETA will be initialized by INIT\_GCS. Note that when the vehicle status is located on a boundary between two or more roll command regions, the lowest intensity signal should be used to avoid over-commanding the engines. One should refer to the Data Requirements Dictionary under RE\_CMD for the actual values for intensity and direction.

✓ **DETERMINE ROLL ENGINE COMMAND**

- The pulse intensity and direction are packed into the lowest three lower-order bits of the actual roll engine command (RE\_CMD) as shown:

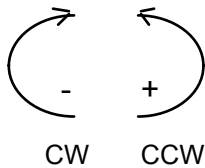
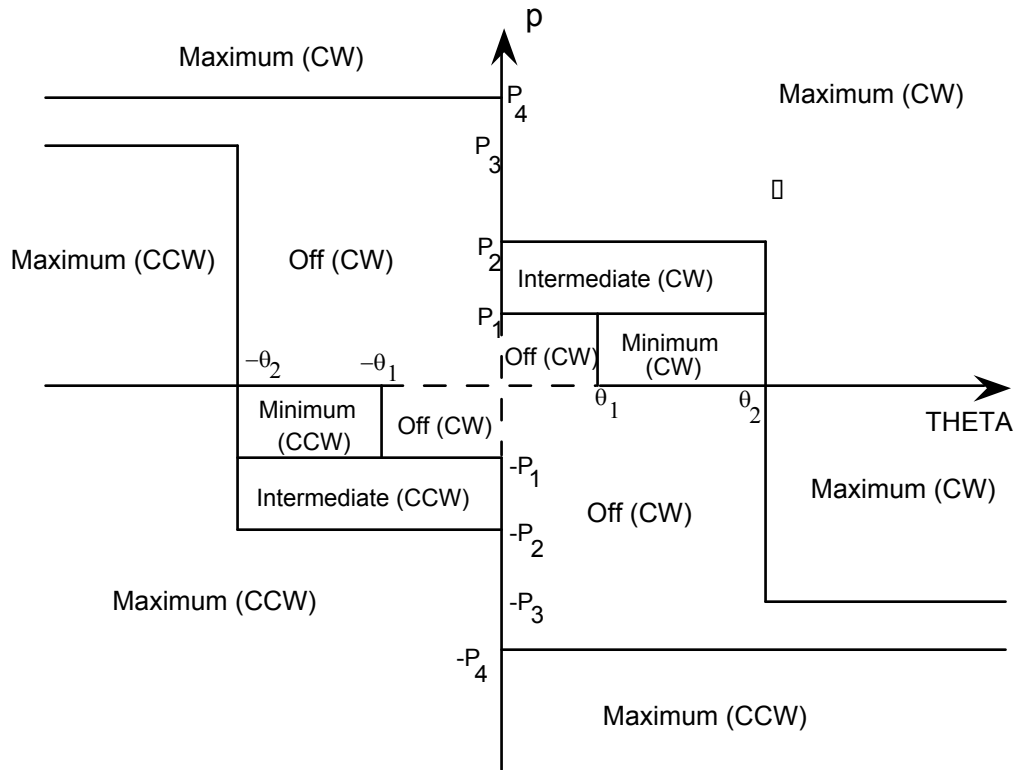
15	14	13	...	3	2	1	0
X	X	X	...	X	I	I	D

where X = unused, I = intensity, and D = direction. The bits marked "X = unused" in RE\_CMD must be left at 0.

✓ **SET ROLL ENGINE STATUS TO HEALTHY**

- Set RE\_STATUS to healthy.

Figure A.5.2 GRAPH FOR DERIVING ROLL ENGINE COMMANDS



Note: "Off", "Minimum", "Intermediate", and "Maximum" are Intensities.

"CW" and "CCW" are Directions, as viewed from below the craft..

"CW" = Clockwise; "CCW" = Counterclockwise

Note: P<sub>1</sub> < P<sub>2</sub> < P<sub>3</sub> < P<sub>4</sub> and θ<sub>1</sub> < θ<sub>2</sub>



## TDLRSP -- Touch Down Landing Radar Sensor Processing (P-Spec 2.1.3)

**PURPOSE** A single touch down landing radar (TDLR) gauges the velocity of the vehicle during terminal descent. This radar is a doppler radar with four radar beams, each of which emanates from the vehicle's center of gravity with a slight offset from the vehicle's  $\vec{x}_v$  axis. The radar beams form the edges of the pyramid as shown in Figure A.5.3.

The Touch Down Landing Radar Sensor Processing (TDLRSP) functional unit converts measurements of the frequency shift of each beams reflection into vehicle velocities; however, the receivers associated with each beam may not find a usable reflection. If no usable reflection is found, the receiver returns a status of beam in search mode (unlocked).

### INPUT

DELTA_T	FRAME_BEAM_UNLOCKED
FRAME_COUNTER	K_MATRIX
TDLR_ANGLES	TDLR_COUNTER
TDLR_GAIN	TDLR_LOCK_TIME
TDLR_OFFSET	TDLR_STATE
TDLR_VELOCITY	

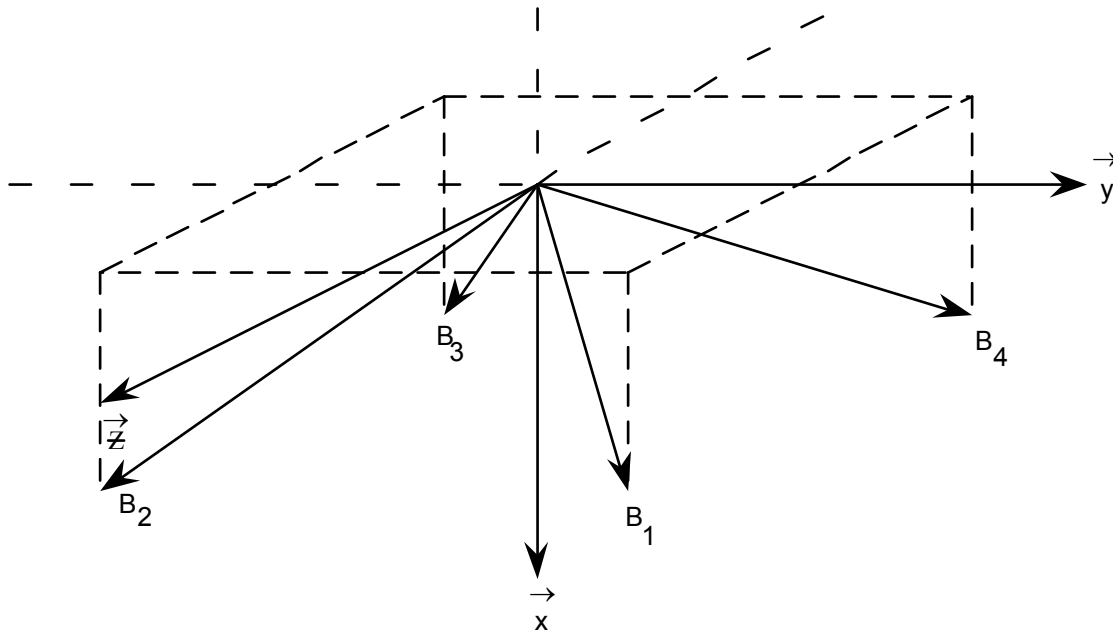
### OUTPUT

FRAME_BEAM_UNLOCKED	K_MATRIX
TDLR_STATE	TDLR_STATUS
TDLR_VELOCITY	

**PROCESS** The value returned by each beam (TDLR\_COUNTER) is proportional to the beam frequency shift down that beam, which is, in turn, proportional to the velocity down that beam. The processing of the TDLR\_COUNTER data into the component velocities along the vehicle's  $\vec{x}$ ,  $\vec{y}$ , and  $\vec{z}$  axes requires the following steps:

- ✓ **ROTATE VARIABLES**
  - Rotate TDLR\_VELOCITY and K\_MATRIX.

Figure A.5.3 DOPPLER RADAR BEAM LOCATIONS



✓ **DETERMINE RADAR BEAM STATES**

The processing of the four radar beams depends on the current state of the radar, i.e. whether or not each of the four beams is searching or in lock, and also upon the previous states of the beams. Note that at the beginning of each trajectory, FRAME\_BEAM\_UNLOCKED will be set to zero, thus meaning that the beam has never been unlocked. If the receiver for a beam does not sense an echo (i.e. the beam is in search mode), the corresponding TDLR\_COUNTER value will be zero. Note that a beam which becomes unlocked will be ignored for TDLR\_LOCK\_TIME seconds.

- Use Table A.5.11 to determine the state (TDLR\_STATE and FRAME\_BEAM\_UNLOCKED) for each of the four beams.

Table A.5.11 DETERMINATION OF RADAR BEAM STATES

CURRENT STATE			ACTIONS	
TDLR_STATE	TDLR_COUNTER	$\frac{DELTA\_T}{(FRAME\_COUNTER - FRAME\_BEAM\_UNLOCKED)} \geq TDLR\_LOCK\_TIME?$	TDLR_STATE	FRAME_BEAM_UNLOCKED
locked	0	d	unlocked	current FRAME_COUNTER
unlocked	$\neq 0$	yes	locked	
unlocked	0	yes		current FRAME_COUNTER

Note: A blank box under "ACTIONS" indicates no action is to be taken  
 "d" = don't care condition

✓ **DETERMINE BEAM VELOCITIES**

A beam velocity is a linear function of its TDLR\_COUNTER value where the gain (TDLR\_GAIN) specifies the slope and the offset (TDLR\_OFFSET) specifies the intercept.

- Calculate the beam velocities as follows:

$$B(i) = TDLR\_OFFSET + TDLR\_GAIN * (TDLR\_COUNTER(i))$$

where  $i$  ranges from 1 to 4 and represents the four radar beams.

✓ **PROCESS THE BEAM VELOCITIES**

- Use Table A.5.12 to calculate values for  $\hat{B}_x$ ,  $\hat{B}_y$ , and  $\hat{B}_z$ , which are the processed beam velocities. Note that in Table A.5.12,  $B_i$  is shorthand for  $B(i)$ , where  $i$  ranges from 1 to 4. Note also that the knowledge of which beams are in lock is used to determine which line of the table to use in order to calculate  $\hat{B}_x$ ,  $\hat{B}_y$ , and  $\hat{B}_z$ .

✓ **CONVERT TO BODY VELOCITIES**

- In order to convert the processed beam velocities to body velocities (TDLR\_VELOCITY), use the following equations, which make use of the angles  $\alpha$ ,  $\beta$  and  $\gamma$  (TDLR\_ANGLES) which are the offsets of the beams from the body axes:

$$TDLR\_VELOCITY(1) = \frac{\hat{B}_x}{\cos\alpha}$$

$$TDLR\_VELOCITY(2) = \frac{\hat{B}_y}{\cos\beta}$$

$$TDLR\_VELOCITY(3) = \frac{\hat{B}_z}{\cos\gamma}$$

✓ **SET VALUES IN K\_MATRIX**

When calculating the vehicle velocity, the Guidance Processor must know which components of the body velocities are usable. A value of one in the diagonal element of the K\_MATRIX indicates that the corresponding velocity should be used, while a value of zero indicates that it should not.

- Use Table A.5.12 to set the values for  $K_x$ ,  $K_y$ , and  $K_z$  in K\_MATRIX, (again on the basis of which beams are in lock), as follows:

$$K\_MATRIX = \begin{pmatrix} K_x & 0 & 0 \\ 0 & K_y & 0 \\ 0 & 0 & K_z \end{pmatrix}$$

The off-diagonal elements of K\_MATRIX should not be updated.

✓ **SET TDLR\_STATUS**

- Set all elements of TDLR\_STATUS to healthy.

Table A.5.12 PROCESSING OF DOPPLER RADAR BEAMS IN LOCK

CURRENT STATE BEAMS IN LOCK	A C T I O N S					
	$\hat{B}_x$	$K_x$	$\hat{B}_y$	$K_y$	$\hat{B}_z$	$K_z$
none	0	0	0	0	0	0
$B_1$	0	0	0	0	0	0
$B_2$	0	0	0	0	0	0
$B_3$	0	0	0	0	0	0
$B_4$	0	0	0	0	0	0
$B_1, B_2$	0	0	$(B_1 - B_2)/2$	1	0	0
$B_1, B_3$	$(B_1 + B_3)/2$	1	0	0	0	0
$B_1, B_4$	0	0	0	0	$(B_1 - B_4)/2$	1
$B_2, B_3$	0	0	0	0	$(B_2 - B_3)/2$	1
$B_2, B_4$	$(B_2 + B_4)/2$	1	0	0	0	0
$B_3, B_4$	0	0	$(B_4 - B_3)/2$	1	0	0
$B_1, B_2, B_3$	$(B_1 + B_3)/2$	1	$(B_1 - B_2)/2$	1	$(B_2 - B_3)/2$	1
$B_1, B_2, B_4$	$(B_2 + B_4)/2$	1	$(B_1 - B_2)/2$	1	$(B_1 - B_4)/2$	1
$B_1, B_3, B_4$	$(B_1 + B_3)/2$	1	$(B_4 - B_3)/2$	1	$(B_1 - B_4)/2$	1
$B_2, B_3, B_4$	$(B_2 + B_4)/2$	1	$(B_4 - B_3)/2$	1	$(B_2 - B_3)/2$	1
$B_1, B_2, B_3, B_4$	$(B_1 + B_2 + B_3 + B_4)/4$	1	$(B_1 - B_2 - B_3 + B_4)/4$	1	$(B_1 + B_2 - B_3 - B_4)/4$	1

## TDSP -- Touch Down Sensor Processing (P-Spec 2.1.6)

**PURPOSE** The touch down sensor is attached to the end of a rod which is attached to the bottom of the vehicle. Its purpose is to trigger engine shutdown when the vehicle is at the correct distance from the surface. This shutdown is necessary to:

- avoid the stirring up of dust and debris and
- avoid scorching immediate area of the experiment site.

### INPUT

TDS_STATUS	TD_COUNTER
------------	------------

### OUTPUT

TDS_STATUS	TD_SENSED
------------	-----------

**PROCESS** The touch down sensor is a simple switch at the end of a pole on the underside of the lander. If the sensor is functioning properly, then TD\_COUNTER will contain one of only two 16-bit values, namely sixteen "ones", which means that touch down has been sensed, or sixteen "zeroes", which means that touch down has not been sensed. If the sensor has failed due to electrical noise, TD\_COUNTER will contain some combination of "ones" and "zeroes" other than all "ones" or all "zeroes".

✓ **DETERMINE STATUS OF TOUCH DOWN SENSOR AND WHETHER TOUCH DOWN HAS BEEN SENSED:**

- Use Table A.5.13 to determine whether the touch down sensor is functioning properly (set TDS\_STATUS), and whether touch down has been sensed (set TD\_SENSED). Note that if the sensor fails, the guidance processor will decide when the vehicle has touched down.

Table A.5.13 DETERMINATION OF TOUCH DOWN SENSOR AND STATUS

CURRENT STATE		ACTIONS	
TDS_STATUS	TD_COUNTER	TD_SENSED	TDS_STATUS
healthy	all zeroes	not sensed	
healthy	all ones	sensed	
healthy	mixture of ones & zeroes	not sensed	failed

Note: A blank block under "ACTIONS" indicates no action is to be taken

## TSP -- Temperature Sensor Processing (P-Spec 2.1.5)

**PURPOSE** A temperature gauge on the vehicle is used to adjust the response of the accelerometers and gyroscopes. The gauge contains two temperature sensing devices, namely a solid-state sensor and a matched pair of thermocouples. The Temperature Sensor Processing (TSP) functional unit determines the ambient temperature, using either the solid-state sensor or the thermocouple pair in a manner maximizing the accuracy of the measurement.

### INPUT

M1	M2
M3	M4
SS_TEMP	T1
T2	T3
T4	THERMO_TEMP

### OUTPUT

ATMOSPHERIC_TEMP	TS_STATUS
------------------	-----------

**PROCESS** The temperature values from the solid-state sensor are highly quantized. The processing of raw temperature data from the solid-state sensor and thermocouple pair, SS\_TEMP and THERMO\_TEMP, is based on the solid-state sensor being less accurate than the thermocouple pair, but having a greater usable operating range.

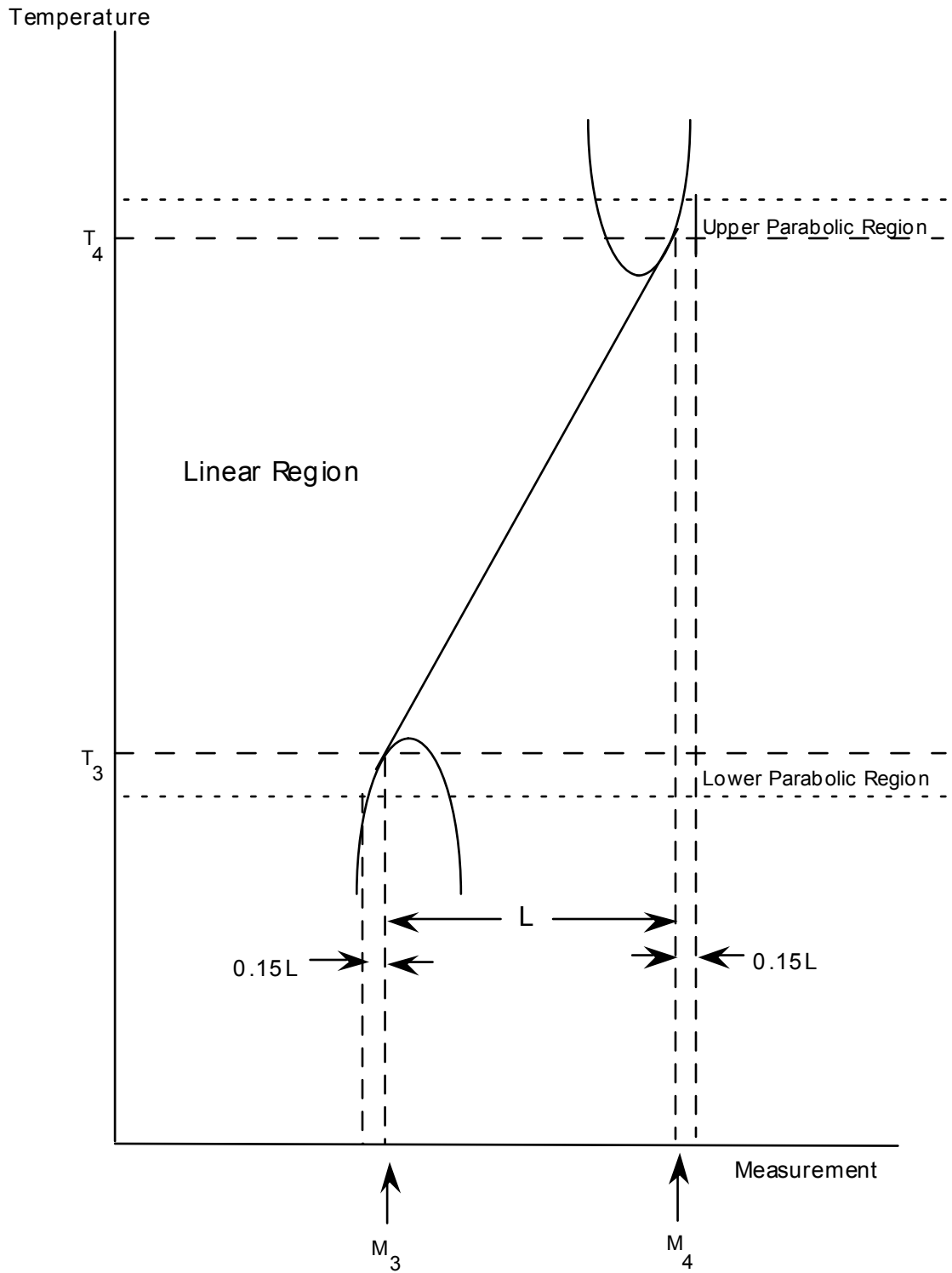
The ambient temperature (ATMOSPHERIC\_TEMP) is to be calculated using either the solid state sensor value (SS\_TEMP) or the thermocouple sensor value (THERMO\_TEMP). Since the thermocouple sensor is more accurate, it should be used whenever possible; the solid state sensor should be used only if the temperature does not lie within the usable range of the thermocouple pair.

The response of the solid-state temperature sensor is linear with respect to the ambient temperature and is computed using the two calibration points (M1, T1) and (M2, T2) which characterize the line.

The response of the thermocouple pair is calibrated differently depending on the region (linear or parabolic) where the measurement lies (see Figure A.5.4):

Thermocouple linear region - The linear region is bounded by the calibration points used by the thermocouple sensor (i.e., [M3, T3] and [M4, T4] inclusive). Temperatures measured within this region are calibrated accordingly.

Figure A.5.4 CALIBRATION OF THERMOCOUPLE PAIR



Note:  $M_3 < M_4$  and  $T_3 < T_4$

Thermocouple parabolic regions - The upper and lower parabolic regions extend plus or minus 15 percent of the difference between the measured calibration points, M4 and M3, respectively. These parabolic regions each intersect the line at the calibration points. The rate of change in temperature, with respect to the thermocouple measurements, is continuous at these intersections. The upper (and lower) parabolas are defined so that the temperature goes up (or down) as the square of the measurement value (THERMO\_TEMP). The parabolas are offset along both the temperature and measurement axes. By using the values of T3, T4, M3, and M4, and the fact that the function is continuous at the endpoints, the offsets for the parabolas may be determined, and the equations for the parabolas may be generated. Note that the line in the linear region in Figure A.5.4 is tangent to both parabolas.

The processing of the values SS\_TEMP and THERMO\_TEMP into an accurate measure of ambient temperature (ATMOSPHERIC\_TEMP) requires several steps, as follows:

- ✓ **CALCULATE THE SOLID STATE TEMPERATURE**
  - Use the value of SS\_TEMP and the equation appropriate to the solid-state linear region to compute the temperature.
- ✓ **DETERMINE WHETHER TO USE SOLID STATE OR THERMOCOUPLE TEMPERATURE**
  - If the temperature derived from SS\_TEMP in the previous step does not fall within the accurate temperature response zone of the thermocouple pair (the linear as well as parabolic regions), then set ATMOSPHERIC\_TEMP to the temperature derived from SS\_TEMP and proceed directly to the step labeled "SET STATUS TO HEALTHY"; otherwise, proceed to the step "CALCULATE THE THERMOCOUPLE TEMPERATURE".
- ✓ **CALCULATE THE THERMOCOUPLE TEMPERATURE**
  - Use the value of THERMO\_TEMP to determine whether the temperature lies in the thermocouple linear or the upper parabolic or the lower parabolic region.
  - Use the value of THERMO\_TEMP and the equation appropriate to the particular thermocouple region (as determined above) to calculate ATMOSPHERIC\_TEMP.
- ✓ **SET STATUS TO HEALTHY**
  - Set the values of both elements of TS\_STATUS to healthy.



## A.6 DATA REQUIREMENTS DICTIONARY

### PART I. DATA ELEMENT DESCRIPTIONS

The following template has been constructed for defining the data elements in the four required global data stores and the optional variables shown in Table A.6.5:

NAME: DESCRIPTION: USED IN: UNITS: RANGE: DATA TYPE: ATTRIBUTE: DATA STORE LOCATION: ACCURACY:
--

**NAME** This field gives the name of the variable used in the specification. The variable name used during coding must be the same as specified.

**DESCRIPTION** This field gives a brief description of the variable.

**USED IN** This field provides a reference to the functional units using this variable.

**UNITS** This field indicates the unit of measure for the data contained in the variable being defined.

**RANGE** This field specifies the acceptable range of data values for the variable.

**DATA TYPE** The data type field specifies the data type to be used when declaring the variable during coding.

**ATTRIBUTE** This field indicates whether or not the variable contains data, control information, or a data condition.

**DATA STORE LOCATION** This field references the common region where the variable must be stored.

**ACCURACY** This field dictates the degree of accuracy required for output comparisons to be made between implementations. In the data dictionary, accuracy is listed as N/A where accuracy is not applicable, or TBD where accuracy is (T)o (B)e (D)etermined later. A formal modification will be released when the values of the accuracy requirements have been approved.

NAME: A\_ACCELERATION  
DESCRIPTION: vehicle accelerations  
USED IN: AECLP, ASP, CP, GP  
UNITS:  $\frac{meters}{sec^2}$   
RANGE: [-20, 5]  
DATA TYPE: array (1..3, 0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: TBD

NAME: A\_BIAS  
DESCRIPTION: characteristic bias in the accelerometer measurements  
USED IN: ASP  
UNITS:  $\frac{meters}{sec^2}$   
RANGE: [-30, 0]  
DATA TYPE: array (1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: A\_COUNTER  
DESCRIPTION: accelerations along the  $\bar{x}$ ,  $\bar{y}$ , and  $\bar{z}$  axes  
USED IN: ASP  
UNITS: none  
RANGE: [0, 2<sup>15</sup> -1]  
DATA TYPE: array (1..3) of Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: A\_GAIN\_0  
DESCRIPTION: standard gain in the accelerations  
USED IN: ASP  
UNITS:  $\frac{meters}{sec^2}$   
RANGE: [0, 1]  
DATA TYPE: array (1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: A\_SCALE  
DESCRIPTION: multiplicative constant used to determine limit on deviation accelerometer values.  
USED IN: ASP  
UNITS: none  
RANGE: [0, 3]  
DATA TYPE: Integer\*4  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: A\_STATUS  
DESCRIPTION: Flag indicating whether or not the accelerometers are working properly.  
USED IN: ASP, CP  
UNITS: none  
RANGE: [0 : healthy, 1: unhealthy]  
DATA TYPE: array (1..3, 0..3) of logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: AECLP\_DONE  
DESCRIPTION: Flag indicating completion of AECLP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task AECLP incomplete, TRUE: running of task AECLP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: AE\_CMD  
DESCRIPTION: Valve settings for the axial engines.  
USED IN: AECLP, CP  
UNITS: none  
RANGE: [0, 127]  
DATA TYPE: array (1..3) of Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: TBD

NAME: AE\_STATUS  
DESCRIPTION: Status of axial engines.  
USED IN: AECLP, CP  
UNITS: none  
RANGE: [0: Healthy, 1: Failed.]  
DATA TYPE: logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: AE\_SWITCH  
DESCRIPTION: Flag indicating whether or not axial engines are turned on.  
USED IN: AECLP, GP  
UNITS: none  
RANGE: [0: axial engines are off, 1: axial engines are on.]  
DATA TYPE: logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: AE\_TEMP  
DESCRIPTION: Temperature of axial engines when they are turned on.  
USED IN: AECLP, CP, CRCP, GP  
UNITS: none  
RANGE: [0: Cold, 1: Warming-Up, 2: Hot]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: ALPHA\_MATRIX  
DESCRIPTION: Matrix of misalignment angles  
USED IN: ASP  
UNITS: none  
RANGE:  $[-\pi, \pi]$   
DATA TYPE: array (1..3, 1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: AR\_ALTITUDE  
DESCRIPTION: altimeter radar height above terrain  
USED IN: ARSP, CP, GP  
UNITS: meters  
RANGE: [0, 2000]  
DATA TYPE: array (0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: TBD

NAME: AR\_COUNTER  
DESCRIPTION: counter containing elapsed time since transmission of radar pulse  
USED IN: ARSP  
UNITS: Cycles  
RANGE:  $[-1, 2^{15}-1]$   
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: AR\_FREQUENCY  
DESCRIPTION: increment frequency of AR\_COUNTER  
USED IN: ARSP  
UNITS:  $\frac{cycles}{sec}$   
RANGE:  $[1, 2.45 \times 10^9]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: AR\_STATUS  
DESCRIPTION: status of the altimeter radars  
USED IN: ARSP, CP  
UNITS: none  
RANGE: [0 : healthy, 1: failed]  
DATA TYPE: array (0..4) of logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: ARSP\_DONE  
DESCRIPTION: Flag indicating completion of ARSP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task ARSP incomplete, TRUE: running of task ARSP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: ASP\_DONE  
DESCRIPTION: Flag indicating completion of ASP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task ASP incomplete, TRUE: running of task ASP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: ATMOSPHERIC\_TEMP  
DESCRIPTION: atmospheric temperature  
USED IN: ASP, CP, GSP, TSP  
UNITS: degrees C  
RANGE: [-200, 25]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: TBD

NAME: C\_STATUS  
DESCRIPTION: Flag indicating whether or not the communications processor is working properly.  
USED IN: CP  
UNITS: none  
RANGE: [0 : healthy, 1: failed]  
DATA TYPE: logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: CHUTE\_RELEASED  
DESCRIPTION: signal indicating parachute has been released  
USED IN: AECLP, CP, CRCP, GP  
UNITS: none  
RANGE: [0: Chute Attached, 1: Chute Released]  
DATA TYPE: logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: CL  
DESCRIPTION: Index which specifies which set of Control Law Parameters to use  
USED IN: AECLP, GP  
UNITS: none  
RANGE: [1: first, 2: second]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: CLP\_DONE  
DESCRIPTION: Control signal which indicates whether or not Control Law Processing function has completed.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of Control Law Processing function incomplete, TRUE: running of Control Law Processing function complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: COMM\_SYNC\_PATTERN  
DESCRIPTION: sixteen bit synchronization pattern  
USED IN: CP  
UNITS: none  
RANGE: [1101100110110010] (binary)  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: CONTOUR\_ALTITUDE  
DESCRIPTION: Altitude in velocity-altitude contour.  
USED IN: GP  
UNITS: kilometers  
RANGE: [-.01, 2]  
DATA TYPE: array (1..100) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: CONTOUR\_CROSSED  
DESCRIPTION: Indicates if the velocity-altitude contour has been sensed.  
USED IN: AECLP, CP, GP  
UNITS: none  
RANGE: [0: contour not crossed, 1: contour crossed]

DATA TYPE: logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: CONTOUR\_VELOCITY  
DESCRIPTION: Velocity in velocity-altitude contour.  
USED IN: GP  
UNITS: kilometers  
sec  
RANGE: [0, 0.5]  
DATA TYPE: array (1..100) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: CP\_DONE  
DESCRIPTION: Flag indicating completion of CP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task CP incomplete, TRUE: running of task CP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: CRCP\_DONE  
DESCRIPTION: Flag indicating completion of CRCP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task CRCP incomplete, TRUE: running of task CRCP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: DELTA\_T  
DESCRIPTION: Time step duration.  
USED IN: AECLP, GP, RECLP, TDLRSP  
UNITS: seconds  
RANGE: [0.005, 0.20]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: DROP\_HEIGHT  
DESCRIPTION: Height from which vehicle should free-fall to surface  
USED IN: GP  
UNITS: meters  
RANGE: [0, 100]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: DROP\_SPEED  
 DESCRIPTION: Optimal speed during constant velocity descent.  
 USED IN: GP  
 UNITS:  $\frac{\text{meters}}{\text{sec}}$   
 RANGE: [0, 4.0]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: ENGINES\_ON\_ALTITUDE  
 DESCRIPTION: Altitude at which the axial engines are turned on.  
 USED IN: AECLP, GP  
 UNITS: meters  
 RANGE: [0, 2000]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: FRAME\_BEAM\_UNLOCKED  
 DESCRIPTION: Variable containing the number of the frame during which the radar beam unlocked  
 USED IN: TDLRSP  
 UNITS: none  
 RANGE: [0, 2<sup>31</sup>-1]  
 DATA TYPE: array (1..4) of Integer\*4  
 ATTRIBUTE: data  
 DATA STORE LOCATION: GUIDANCE\_STATE  
 ACCURACY: TBD

NAME: FRAME\_COUNTER  
 DESCRIPTION: Counter containing the number of the present frame  
 USED IN: AECLP, ARSP, CP, GP, TDLRSP  
 UNITS: none  
 RANGE: [1, 2<sup>31</sup>-1]  
 DATA TYPE: Integer\*4  
 ATTRIBUTE: data  
 DATA STORE LOCATION: EXTERNAL  
 ACCURACY: N/A

NAME: FRAME\_ENGINES\_IGNITED  
 DESCRIPTION: Variable containing the number of the frame during which the engines were ignited  
 USED IN: AECLP, GP  
 UNITS: none  
 RANGE: [0, 2<sup>31</sup>-1]  
 DATA TYPE: Integer\*4  
 ATTRIBUTE: data  
 DATA STORE LOCATION: GUIDANCE\_STATE  
 ACCURACY: TBD

NAME: FULL\_UP\_TIME  
 DESCRIPTION: Time for axial engines to reach optimum operational condition  
 USED IN: AECLP  
 UNITS: seconds

RANGE: [0, 60]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: G1  
 DESCRIPTION: coefficient used to adjust A\_GAIN  
 USED IN: ASP  
 UNITS:  $\frac{\text{meters}}{\text{deg} \text{ sec}^2}$

RANGE: [-5, 5]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: G2  
 DESCRIPTION: coefficient used to adjust A\_GAIN  
 USED IN: ASP  
 UNITS:  $\frac{\text{meters}}{\text{deg} \text{ sec}^2}$

RANGE: [-5, 5]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: G3  
 DESCRIPTION: coefficient used to adjust G\_GAIN  
 USED IN: GSP  
 UNITS:  $\frac{\text{radians}}{\text{deg} \text{ sec}}$

RANGE: [-5, 5]  
 DATA TYPE: real\*8  
 ATTRIBUTE: data  
 DATA STORE LOCATION: RUN\_PARAMETERS  
 ACCURACY: N/A

NAME: G4  
DESCRIPTION: coefficient used to adjust G\_GAIN  
USED IN: GSP  
UNITS:  $\frac{\text{radians}}{\text{degree } C^2}$   
RANGE: [-5, 5]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: G\_COUNTER  
DESCRIPTION: gyroscope measurement of vehicle rotation rates  
USED IN: GSP  
UNITS: none  
RANGE:  $[-(2^{14}-1), 2^{14}-1]$   
DATA TYPE: array (1..3) of Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: G\_GAIN\_0  
DESCRIPTION: standard gain in vehicle rotation rates as measured by the gyroscopes  
USED IN: GSP  
UNITS:  $\frac{\text{radians}}{\text{sec}}$   
RANGE: [-1, 1]  
DATA TYPE: array (1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: G\_OFFSET  
DESCRIPTION: standard offset of the rotation raw values  
USED IN: GSP  
UNITS:  $\frac{\text{radians}}{\text{sec}}$   
RANGE: [-0.5, 0.5]  
DATA TYPE: array (1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: G\_ROTATION  
DESCRIPTION: vehicle rotation rates  
USED IN: CP, GSP, GP, RECLP  
UNITS:  $\frac{\text{radians}}{\text{sec}}$   
RANGE: [-1.0, 1.0]  
DATA TYPE: array (1..3, 0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: TBD

NAME: G\_STATUS  
DESCRIPTION: status of the gyroscopes  
USED IN: CP, GSP  
UNITS: none  
RANGE: [0 : healthy, 1: failed]  
DATA TYPE: logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: GA  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS:  $\frac{\text{sec}}{\text{meter}}$   
RANGE: [0, 50]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GAX  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: none  
RANGE: [0, 5]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GP1  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: none  
RANGE: [-5, 5]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GP2  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: none  
RANGE: [-5, 5]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GP\_ALTITUDE  
DESCRIPTION: altitude as seen by guidance processor  
USED IN: AECLP, CP, GP  
UNITS: meters  
RANGE: [0, 2000]  
DATA TYPE: array (0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: GP\_ATTITUDE  
DESCRIPTION: direction cosine matrix  
USED IN: AECLP, CP, GP  
UNITS: none  
RANGE: [-1, 1]  
DATA TYPE: array (1..3, 1..3, 0..4) real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: GP\_DONE  
DESCRIPTION: Flag indicating completion of GP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task GP incomplete, TRUE: running of task GP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: GP\_PHASE  
DESCRIPTION: phase of operation as seen by guidance processor  
USED IN: CP, GP  
UNITS: none  
RANGE: [1, 5]  
DATA TYPE: integer\*4  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: GP\_ROTATION  
DESCRIPTION: rotation rates as determined by the guidance processing functional unit  
USED IN: AECLP, CP, GP  
UNITS:  $\frac{radians}{sec}$   
RANGE: [-1.0, 1.0]  
DATA TYPE: array (1..3, 1..3) real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: GP\_VELOCITY  
DESCRIPTION: Velocity as corrected by the guidance algorithm.  
USED IN: AECLP, CP, GP  
UNITS:  $\frac{meters}{sec}$   
RANGE: [-100, 100]  
DATA TYPE: array ( 1..3, 0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: GPY  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: none  
RANGE: [-5, 5]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GQ  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: seconds  
RANGE: [-5, 8]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GR  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: seconds  
RANGE: [-5, 8]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GRAVITY  
DESCRIPTION: gravity of planet  
USED IN: AECLP, GP  
UNITS:  $\frac{meters}{sec^2}$   
RANGE: [0, 100]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GSP\_DONE  
DESCRIPTION: Flag indicating completion of GSP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task GSP incomplete, TRUE: running of task GSP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: GV  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS:  $\frac{\text{sec}}{\text{meter}}$   
RANGE: [-5, 8]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GVE  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: /second  
RANGE: [0, 500]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GVEI  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: /second<sup>2</sup>  
RANGE: [-5, 40]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GVI  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: /meter  
RANGE: [-5, 5]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GW  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS:  $\frac{\text{sec}}{\text{meter}}$   
RANGE: [-5, 8]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: GWI  
DESCRIPTION: gain  
USED IN: AECLP  
UNITS: /meter  
RANGE: [-5, 5]  
DATA TYPE: array (1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: INIT\_DONE  
DESCRIPTION: Flag indicating completion of GCS initialization.  
USED IN: 0. GCS  
UNITS: none  
RANGE: [FALSE: initialization incomplete, TRUE: initialization complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: INTERNAL\_CMD  
DESCRIPTION: Real vector containing the command to be sent to the axial engines  
USED IN: AECLP  
UNITS: none  
RANGE: [-0.7, 1.7]  
DATA TYPE: array (1..3) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: K\_ALT  
DESCRIPTION: Determines use of altimeter radar by guidance processor  
USED IN: ARSP, CP, GP  
UNITS: none  
RANGE: [0, 1]  
DATA TYPE: array (0..4) of Integer\*4  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A



NAME: K\_MATRIX  
DESCRIPTION: Determines use of doppler radar by guidance processor.  
USED IN: CP, GP, TDLRSP  
UNITS: none  
RANGE: [0, 1]  
DATA TYPE: array (1..3, 1..3, 0..4) Integer\*4  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: M1  
DESCRIPTION: lower measured temperature calibration point for solid state temperature sensor  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: M2  
DESCRIPTION: upper measured temperature calibration point for solid state temperature sensor  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: M3  
DESCRIPTION: lower measured temperature calibration point for thermocouple pair temperature sensor  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: M4  
DESCRIPTION: upper measured temperature calibration point for thermocouple pair temperature sensor  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: MAX\_NORMAL\_VELOCITY  
DESCRIPTION: Maximum vertical velocity for safe landing  
USED IN: GP  
UNITS: meters  
sec  
RANGE: [0, 3.35]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: OMEGA  
DESCRIPTION: gain of angular velocity  
USED IN: AECLP  
UNITS: /second  
RANGE: [-50, 50]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: P1  
DESCRIPTION: pulse rate boundary  
USED IN: RECLP  
UNITS: radians  
sec  
RANGE: [0, 0.05]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: P2  
DESCRIPTION: pulse rate boundary  
USED IN: RECLP  
UNITS: radians  
sec  
RANGE: [0, 0.05]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: P3  
DESCRIPTION: pulse rate boundary  
USED IN: RECLP  
UNITS: radians  
sec  
RANGE: [0, 0.05]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: P4  
DESCRIPTION: pulse rate boundary  
USED IN: RECLP  
UNITS:  $\frac{\text{radians}}{\text{sec}}$   
RANGE: [0, 0.05]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: PACKET  
DESCRIPTION: Packet of telemetry data  
USED IN: CP  
UNITS: N/A  
RANGE: N/A  
DATA TYPE: array (1..256) of Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: PE\_INTEGRAL  
DESCRIPTION: Integral portion of Pitch error equation  
USED IN: AECLP, CP  
UNITS: meters  
RANGE: [-100, 100]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: PE\_MAX  
DESCRIPTION: Maximum pitch error tolerable  
USED IN: AECLP  
UNITS: none  
RANGE: [0, 1]  
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: PE\_MIN  
DESCRIPTION: Minimum pitch error tolerable.  
USED IN: AECLP  
UNITS: none  
RANGE: [-1, 0]  
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: RE\_CMD  
DESCRIPTION: roll engine command  
USED IN: CP, RECLP  
UNITS: none  
RANGE:  
[1: off,  
2: minimum, counterclockwise,  
3: minimum, clockwise,  
4: intermediate, counterclockwise,  
5: intermediate, clockwise,  
6: maximum, counterclockwise,  
7: maximum, clockwise]

note: the values above for Range have been derived from range of intensity and direction as follows:  
Intensity [00:off, 01:minimum, 10:intermediate, 11:maximum](binary)  
Direction [0:counterclockwise (positive), 1:clockwise (negative)] (binary)  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: TBD

NAME: RE\_STATUS  
DESCRIPTION: status of the roll engines  
USED IN: CP, RECLP  
UNITS: none  
RANGE: [0: healthy, 1: failed]  
DATA TYPE: logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: RE\_SWITCH  
DESCRIPTION: Flag indicating whether or not the roll engines are turned on.  
USED IN: GP, RECLP  
UNITS: none  
RANGE: [0: roll engines are off, 1: roll engines are on.]  
DATA TYPE: logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: RECLP\_DONE  
DESCRIPTION: Flag indicating completion of RECLP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task RECLP incomplete, TRUE: running of task RECLP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: RENDEZVOUS  
DESCRIPTION: Control signal which indicates whether or not GCS\_SIM\_RENDEZVOUS is to be activated.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: GCS\_SIM\_RENDEZVOUS is not to be activated, TRUE: GCS\_SIM\_RENDEZVOUS is to be activated]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: RUN\_DONE  
DESCRIPTION: Flag indicating completion of GCS.  
USED IN: 0. GCS  
UNITS: none  
RANGE: [FALSE: running of GCS incomplete, TRUE: running of GCS complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: SP\_DONE  
DESCRIPTION: Control signal which indicates whether or not Sensor Processing function has been completed.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of Sensor Processing function incomplete, TRUE: running of Sensor Processing function complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: SS\_TEMP  
DESCRIPTION: Solid state temperature data  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: SUBFRAME\_COUNTER  
DESCRIPTION: Counter containing the number of the present subframe.  
USED IN: CP  
UNITS: none  
RANGE: [1, 3]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: T1  
DESCRIPTION: lower ambient temperature calibration point for solid state temperature sensor  
USED IN: TSP  
UNITS: degrees C  
RANGE: [-250, 250]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: T2  
DESCRIPTION: upper ambient temperature calibration point for solid state temperature sensor  
USED IN: TSP  
UNITS: degrees C  
RANGE: [-250, 250]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: T3  
DESCRIPTION: lower ambient temperature calibration point for thermocouple pair temperature sensor  
USED IN: TSP  
UNITS: degrees C  
RANGE: [-50, 50]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: T4  
DESCRIPTION: upper ambient temperature calibration point for thermocouple pair temperature sensor  
USED IN: TSP  
UNITS: degrees C  
RANGE: [-50, 50]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TD\_COUNTER  
DESCRIPTION: value returned by Touch Down Sensor  
USED IN: TDSP  
UNITS: none  
RANGE:  $[-2^{15}, 2^{15}-1]$   
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: TD\_SENSED  
DESCRIPTION: Flag indicating whether or not touch down has been sensed.  
USED IN: CP, GP, TDSP  
UNITS: none  
RANGE: [0: touch down not sensed, 1: touch down sensed]  
DATA TYPE: logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: N/A

NAME: TDLR\_ANGLES  
DESCRIPTION: vector of doppler radar beam offset angles (i.e.,  $\alpha$ ,  $\beta$ ,  $\gamma$ )  
USED IN: TDLRSP  
UNITS: radians  
RANGE:  $[0, \frac{\pi}{2})$   
DATA TYPE: array (1..3) real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TDLR\_COUNTER  
DESCRIPTION: value returned by Doppler radar  
USED IN: TDLRSP  
UNITS: none  
RANGE:  $[0, 2^{15}-1]$   
DATA TYPE: array (1..4) Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: TDLR\_GAIN  
DESCRIPTION: gain in doppler radar beam  
USED IN: TDLRSP  
UNITS:  $\frac{meters}{sec}$   
RANGE: [-1, 1]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TDLR\_LOCK\_TIME  
DESCRIPTION: locking time of doppler radar beam  
USED IN: TDLRSP  
UNITS: seconds  
RANGE: [0, 60]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TDLR\_OFFSET  
DESCRIPTION: offset in doppler radar beam  
USED IN: TDLRSP  
UNITS:  $\frac{meters}{sec}$   
RANGE: [-100, 0]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TDLR\_STATE  
DESCRIPTION: state of the touch down landing radar beams.  
USED IN: CP, TDLRSP  
UNITS: none  
RANGE: [0: Beam unlocked, 1: Beam locked]  
DATA TYPE: array (1..4) logical\*1  
ATTRIBUTE: data condition  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: TDLR\_STATUS  
DESCRIPTION: status of the doppler radar  
USED IN: CP, TDLRSP  
UNITS: none  
RANGE: [0 : healthy, 1: failed]  
DATA TYPE: array (1..4) of logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: TDLR\_VELOCITY  
DESCRIPTION: Velocity as computed by the touch down landing radar.  
USED IN: CP, GP, TDLRSP  
UNITS:  $\frac{meters}{sec}$   
RANGE: [-100, 100]  
DATA TYPE: array (1..3, 0..4) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: SENSOR\_OUTPUT  
ACCURACY: TBD

NAME: TDLRSP\_DONE  
DESCRIPTION: Flag indicating completion of TDLRSP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task TDLRSP incomplete, TRUE: running of task TDLRSP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: TDSP\_DONE  
DESCRIPTION: Flag indicating completion of TDSP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE: [FALSE: running of task TDSP incomplete, TRUE: running of task TDSP complete]  
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: TDS\_STATUS  
DESCRIPTION: status of the touch down sensor  
USED IN: CP, GP, TDSP  
UNITS: none  
RANGE: [0 : healthy, 1: failed]  
DATA TYPE: logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: TE\_DROP  
DESCRIPTION: The axial thrust error when axial engines are warm and the velocity altitude contour has not been intersected.  
USED IN: AECLP  
UNITS: none  
RANGE: [-2, 2]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TE\_INIT  
DESCRIPTION: The axial thrust error when the axial engines are cold.  
USED IN: AECLP  
UNITS: none  
RANGE: [-2, 2]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TE\_INTEGRAL  
DESCRIPTION: Integral portion of Thrust error equation  
USED IN: AECLP, CP, GP  
UNITS: meters  
RANGE: [-100, 100]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: TE\_LIMIT  
DESCRIPTION: Limiting thrust error  
USED IN: AECLP  
UNITS: none  
RANGE: [-100, 100]  
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: TE\_MAX  
DESCRIPTION: Maximum thrust error tolerable  
USED IN: AECLP  
UNITS: none  
RANGE: [-2, 2]  
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TE\_MIN  
DESCRIPTION: Minimum thrust error tolerable.  
USED IN: AECLP  
UNITS: none  
RANGE: [-2, 2]  
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: THERMO\_TEMP  
DESCRIPTION: thermocouple pair temperature  
USED IN: TSP  
UNITS: none  
RANGE: [0, 2<sup>15</sup>-1]  
DATA TYPE: Integer\*2  
ATTRIBUTE: data  
DATA STORE LOCATION: EXTERNAL  
ACCURACY: N/A

NAME: THETA  
DESCRIPTION: roll angle  
USED IN: RECLP  
UNITS: radians  
RANGE:  $[-\pi, \pi]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: THETA1  
DESCRIPTION: pulse angle boundary  
USED IN: RECLP  
UNITS: radians  
RANGE:  $[0, 0.05]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: THETA2  
DESCRIPTION: pulse angle boundary  
USED IN: RECLP  
UNITS: radians  
RANGE:  $[0, 0.05]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: TS\_STATUS  
DESCRIPTION: status of the temperature sensors in solid state, then thermocouple pair order  
USED IN: CP, TSP  
UNITS: none  
RANGE:  $[0 : \text{healthy}, 1 : \text{failed}]$   
DATA TYPE: array (1..2) of logical\*1  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: N/A

NAME: TSP\_DONE  
DESCRIPTION: Flag indicating completion of TSP task.  
USED IN: 2. RUN\_GCS  
UNITS: none  
RANGE:  $[\text{FALSE} : \text{running of task TSP incomplete}, \text{TRUE} : \text{running of task TSP complete}]$   
DATA TYPE: logical\*1  
ATTRIBUTE: control  
DATA STORE LOCATION: none  
ACCURACY: N/A

NAME: VELOCITY\_ERROR  
DESCRIPTION: Distance from velocity-altitude contour. (Difference in velocities from actual to desired on contour.)  
USED IN: AECLP, CP, GP  
UNITS:  $\frac{\text{meters}}{\text{sec}}$   
RANGE:  $[-300, 20]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: YE\_INTEGRAL  
DESCRIPTION: Integral portion of Yaw error equation  
USED IN: AECLP, CP  
UNITS: meters  
RANGE:  $[-100, 100]$   
DATA TYPE: real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: GUIDANCE\_STATE  
ACCURACY: TBD

NAME: YE\_MAX  
DESCRIPTION: Maximum yaw error tolerable  
USED IN: AECLP  
UNITS: none  
RANGE:  $[-1, 1]$   
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

NAME: YE\_MIN  
DESCRIPTION: Minimum yaw error tolerable.  
USED IN: AECLP  
UNITS: none  
RANGE:  $[-1, 1]$   
DATA TYPE: array(1..2) of real\*8  
ATTRIBUTE: data  
DATA STORE LOCATION: RUN\_PARAMETERS  
ACCURACY: N/A

## PART II. CONTENTS OF DATA STORES

Table A.6.1 DATA STORE: GUIDANCE\_STATE

VARIABLE NAME	USED BY:
A_STATUS	ASP, CP
AE_STATUS	AECLP, CP
AE_SWITCH	AECLP, GP
AE_TEMP	AECLP, CP, CRCP, GP
AR_STATUS	ARSP, CP
C_STATUS	CP
CL	AECLP, GP
CONTOUR_CROSSED	AECLP, CP, GP
FRAME_BEAM_UNLOCKED	TDLRSP
FRAME_ENGINES_IGNITED	AECLP, GP
G_STATUS	CP, GSP
GP_ALTITUDE	CP, GP, AECLP
GP_ATTITUDE	AECLP, CP, GP
GP_PHASE	CP, GP
GP_ROTATION	AECLP, CP, GP
GP_VELOCITY	AECLP, CP, GP
INTERNAL_CMD	AECLP
K_ALT	ARSP, CP, GP
K_MATRIX	CP, GP, TDLRSP
PE_INTEGRAL	AECLP, CP
RE_STATUS	CP, RECLP
RE_SWITCH	GP, RECLP
TDLR_STATE	CP, TDLRSP
TDLR_STATUS	CP, TDLRSP
TDS_STATUS	CP, GP, TDSP
TE_INTEGRAL	AECLP, CP, GP
TE_LIMIT	AECLP
THETA	RECLP
TS_STATUS	CP, TSP
VELOCITY_ERROR	AECLP, CP, GP
YE_INTEGRAL	AECLP, CP

Table A.6.2 DATA STORE: EXTERNAL

VARIABLE NAME	USED BY
A_COUNTER	ASP
AE_CMD	AECLP, CP
AR_COUNTER	ARSP
CHUTE_RELEASED	AECLP, CP, CRCP, GP
FRAME_COUNTER	AECLP, ARSP, CP, GP, TDLRSP
G_COUNTER	GSP
PACKET	CP
RE_CMD	RECLP, CP
SS_TEMP	TSP
SUBFRAME_COUNTER	CP
TD_COUNTER	TDSP
TDLR_COUNTER	TDLRSP
THERMO_TEMP	TSP

Table A.6.3 DATA STORE: SENSOR\_OUTPUT

VARIABLE NAME	USED BY:
A_ACCELERATION	AECLP, ASP, CP, GP
AR_ALTITUDE	ARSP, CP, GP
ATMOSPHERIC_TEMP	ASP, CP, GSP, TSP
G_ROTATION	CP, GSP, GP, RECLP
TD_SENSED	CP, GP, TDSP
TDLR_VELOCITY	CP, GP, TDLRSP



Table A.6.4 DATA STORE: RUN\_PARAMETERS

VARIABLE NAME	USED BY
A_BIAS	ASP
A_GAIN_0	ASP
A_SCALE	ASP
ALPHA_MATRIX	ASP
AR_FREQUENCY	ARSP
COMM_SYNC_PATTERN	CP
CONTOUR_ALTITUDE	GP
CONTOUR_VELOCITY	GP
DELTA_T	AECLP, GP, RECLP, TDLRSP
DROP_HEIGHT	GP
DROP_SPEED	GP
ENGINES_ON_ALTITUDE	AECLP, GP
FULL_UP_TIME	AECLP
G1	ASP
G2	ASP
G3	GSP
G4	GSP
G_GAIN_0	GSP
G_OFFSET	GSP
GA	AECLP
GAX	AECLP
GP1	AECLP
GP2	AECLP
GPY	AECLP
GQ	AECLP
GR	AECLP
GRAVITY	AECLP, GP
GV	AECLP
GVE	AECLP
GVEI	AECLP
GVI	AECLP
GW	AECLP
GW1	AECLP
M1	TSP
M2	TSP
M3	TSP
M4	TSP
MAX_NORMAL_VELOCITY	GP
OMEGA	AECLP
P1	RECLP
P2	RECLP
P3	RECLP
P4	RECLP
PE_MAX	AECLP
PE_MIN	AECLP
T1	TSP
T2	TSP
T3	TSP
T4	TSP

Table A.6.4 (continued) DATA STORE: RUN\_PARAMETERS

VARIABLE NAME	USED BY
TDLR_ANGLES	TDLRSP
TDLR_GAIN	TDLRSP
TDLR_LOCK_TIME	TDLRSP
TDLR_OFFSET	TDLRSP
TE_DROP	AECLP
TE_INIT	AECLP
TE_MAX	AECLP
TE_MIN	AECLP
THETA1	RECLP
THETA2	RECLP
YE_MAX	AECLP
YE_MIN	AECLP

### PART III. CONTROL SIGNALS, DATA CONDITIONS, AND GROUP FLOWS

Table A.6.5 CONTROL SIGNALS (OPTIONAL USAGE)

CONTROL SIGNAL NAME
AECLP_DONE
ARSP_DONE
ASP_DONE
CLP_DONE
CP_DONE
CRCP_DONE
GP_DONE
GSP_DONE
INIT_DONE
RECLP_DONE
RENDEZVOUS
RUN_DONE
SP_DONE
TDLRSP_DONE
TDSP_DONE
TSP_DONE

Note: These variables are not in the required global data stores.

Table A.6.6 DATA CONDITIONS (REQUIRED USAGE)

DATA CONDITION VARIABLE NAME
AE_SWITCH
AE_TEMP
CHUTE_RELEASED
CONTOUR_CROSSED
GP_PHASE
RE_SWITCH
TD_SENSED
TDLR_STATE

Table A.6.7 INITIALIZATION DATA

VARIABLE NAME	USED BY
A_ACCELERATION	AECLP, ASP, CP, GP
A_BIAS	ASP
A_COUNTER	ASP
A_GAIN_0	ASP
A_SCALE	ASP
A_STATUS	ASP, CP
AE_STATUS	AECLP, CP
AE_SWITCH	AECLP, GP
AE_TEMP	AECLP, CP, CRCP, GP
ALPHA_MATRIX	ASP
AR_ALTITUDE	ARSP, CP, GP
AR_COUNTER	ARSP
AR_FREQUENCY	ARSP
AR_STATUS	ARSP, CP
ATMOSPHERIC_TEMP	ASP, CP, GSP, TSP
C_STATUS	CP
CHUTE_RELEASED	AECLP, CP, CRCP, GP
CL	AECLP, GP
COMM_SYNC_PATTERN	CP
CONTOUR_ALTITUDE	GP
CONTOUR_CROSSED	AECLP, CP, GP
CONTOUR_VELOCITY	GP
DELTA_T	AECLP, GP, RECLP, TDLRSP
DROP_HEIGHT	GP
DROP_SPEED	GP
ENGINES_ON_ALTITUDE	AECLP, GP
FRAME_BEAM_UNLOCKED	TDLRSP
FRAME_COUNTER	AECLP, ARSP, CP, GP, TDLRSP
FRAME_ENGINES_IGNITED	AECLP, GP
FULL_UP_TIME	AECLP
G1	ASP
G2	ASP
G3	GSP
G4	GSP
G_COUNTER	GSP
G_GAIN_0	GSP
G_OFFSET	GSP
G_ROTATION	CP, GSP, GP, RECLP
G_STATUS	CP, GSP
GA	AECLP
GAX	AECLP
GP1	AECLP
GP2	AECLP
GP_ALTITUDE	AECLP, CP, GP
GP_ATTITUDE	AECLP, CP, GP
GP_PHASE	CP, GP
GP_ROTATION	AECLP, CP, GP
GP_VELOCITY	AECLP, CP, GP
GPY	AECLP
GQ	AECLP
GR	AECLP
GRAVITY	AECLP, GP
GV	AECLP

Table A.6.7 (continued) INITIALIZATION DATA

VARIABLE NAME	USED BY
GVE	AECLP
GVEI	AECLP
GVI	AECLP
GW	AECLP
GW1	AECLP
K_ALT	ARSP, CP, GP
K_MATRIX	CP, GP, TDLRSP
M1	TSP
M2	TSP
M3	TSP
M4	TSP
MAX_NORMAL_VELOCITY	GP
OMEGA	AECLP
P1	RECLP
P2	RECLP
P3	RECLP
P4	RECLP
PE_INTEGRAL	AECLP, CP
PE_MAX	AECLP
PE_MIN	AECLP
RE_STATUS	CP, RECLP
RE_SWITCH	GP, RECLP
SS_TEMP	TSP
SUBFRAME_COUNTER	CP
T1	TSP
T2	TSP
T3	TSP
T4	TSP
TD_COUNTER	TDSP
TD_SENSED	CP, GP, TDSP
TDLR_ANGLES	TDLRSP
TDLR_COUNTER	TDLRSP
TDLR_GAIN	TDLRSP
TDLR_LOCK_TIME	TDLRSP
TDLR_OFFSET	TDLRSP
TDLR_STATE	CP, TDLRSP
TDLR_STATUS	CP, TDLRSP
TDLR_VELOCITY	CP, GP, TDLRSP
TDS_STATUS	CP, GP, TDSP
TE_DROP	AECLP
TE_INIT	AECLP
TE_INTEGRAL	AECLP, CP, GP
TE_LIMIT	AECLP
TE_MAX	AECLP
TE_MIN	AECLP
THERMO_TEMP	TSP
THETA	RECLP
THETA1	RECLP
THETA2	RECLP
TS_STATUS	CP, TSP
VELOCITY_ERROR	AECLP, CP, GP
YE_INTEGRAL	AECLP, CP

YE_MAX	AECLP
YE_MIN	AECLP

Table A.6.8 TEMP\_DATA

VARIABLE NAME
SS_TEMP
THERMO_TEMP

Table A.6.9 SENSOR\_DATA

VARIABLE NAME
A_COUNTER
AR_COUNTER
TDLR_COUNTER
G_COUNTER
TEMP_DATA
TD_COUNTER

Table A.6.10 OUTPUT\_DATA

VARIABLE NAME
AE_CMD
RE_CMD
PACKET

Table A.6.11 OUTPUT\_CONTROL

VARIABLE NAME
AE_SWITCH
RE_SWITCH
CHUTE_RELEASED

Table A.6.12 FRAME\_DATA

VARIABLE NAME
FRAME_COUNTER
SUBFRAME_COUNTER

## A.7 NOTATION FOR LEVELS 0, 1, 2, AND 3 SPECIFICATION

This specification was developed using the extended structured analysis method advocated by Hatley (ref. A.12, A.13) and Cadre's *teamwork* (ref. A.19). This method is based on a hierarchical approach to defining processes and the associated data and control flows.

The documents constructed as a part of this specification include data context and flow diagrams, control context and flow diagrams, process and control specifications, and a Data Requirements Dictionary. Figure A.7.1 defines the graphical symbols used in the data flow and control flow diagrams, respectively.

The data flow diagrams describe the processes, data flows, and data stores. The data context diagram is the highest-level data flow diagram and represents the data flow between the system and the external entities.

The control flow diagrams describe processes, control signal and data condition flows, control specifications, and data stores. The control signal and data condition flows are depicted using directed arcs with broken lines. The control signals listed in the data dictionary may be implemented by the programmer in any form desired, or they may be completely ignored and the control of the program conducted through other means. The control flow diagrams show what the process structure must do under all conditions. Signal flows between the control flow diagram and the control specification have a short bar at the end of the directed arc. The control flow diagrams contain duplicate descriptions of the processes represented on the data flow diagrams. The control context diagram representing the most abstract control flow is similar to the data context diagram.

The control specifications describe the control requirements of a system. These specifications contain the conditions under which the processes detailed in the data and control flow diagrams are activated and de-activated, and in some cases also contain output values for control signals.

The Data Requirements Dictionary contains definitions for data, data conditions, control signals, and group flows.

Following is a list of definitions and explanations for the structured analysis diagrams:

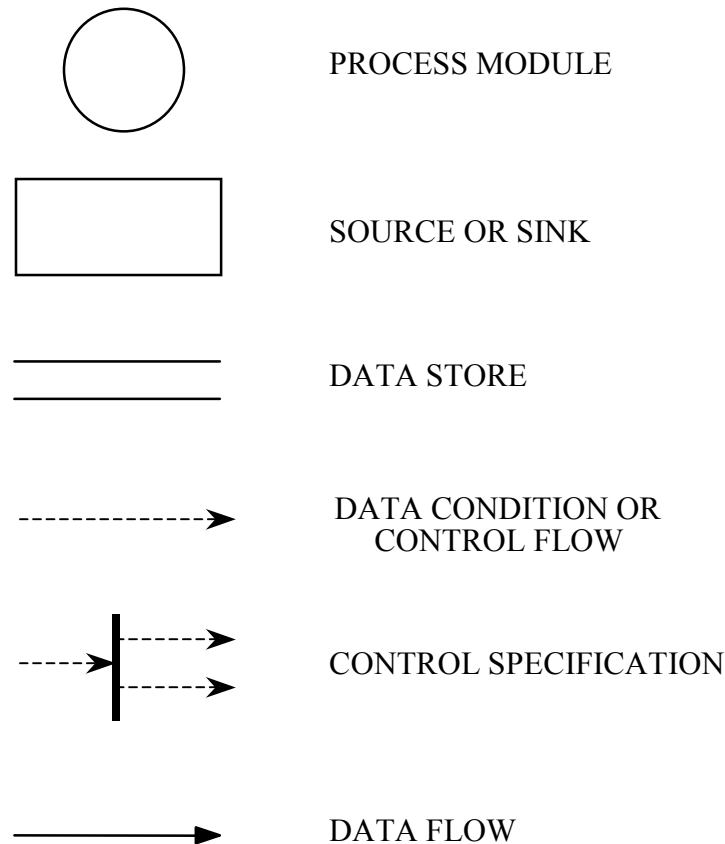
1. The data and control flow names on the directed arcs in the structured analysis figures can be found in the Data Requirements Dictionary Part I, while the group flow names on the arcs can be found in the Data Requirements Dictionary Part III.
2. In the Process Activation Tables, the first column contains the inputs. The second set of columns (separated by two vertical lines) contains the cells which indicate whether a process is to be activated or deactivated. A blank cell indicates that the process is deactivated. An integer indicates that the process is activated. A process whose cell

contains the integer "n" must complete before the process with integer "n+1" is activated. All processes whose cells contain the same integer can be activated in any order. The third set of columns, if present, represents the output values for control signals.

3. The meanings for the symbols used in the expressions for inputs are:

- = equal
- ~= not equal
- ~ logical NOT
- & logical AND
- | logical OR
- () grouping (expression inside parentheses is evaluated first)

Figure A.7.1 GRAPHICAL SYMBOLS USED IN STRUCTURED ANALYSIS DIAGRAMS



## A.8 IMPLEMENTATION NOTES

### INTERFACE

#### Background



For the purposes of this research experiment, each GCS implementation must function as if it were actually controlling a planetary lander. In reality, each GCS implementation will be interacting with a software simulator (GCS\_SIM) that *models* the behavior of a physical lander when exposed to the environmental forces of a planet.

Due to the fact that each GCS implementation must interact with GCS\_SIM as if it were connected to the lander hardware, there are some additional requirements that are placed on a GCS implementation that help define a *software* interface. The software interface to the simulator replaces the physical connection to planetary lander hardware through the use of a simulator support utility and an additional requirement involving the organization of the global data stores.

### **Simulator Support Utility**

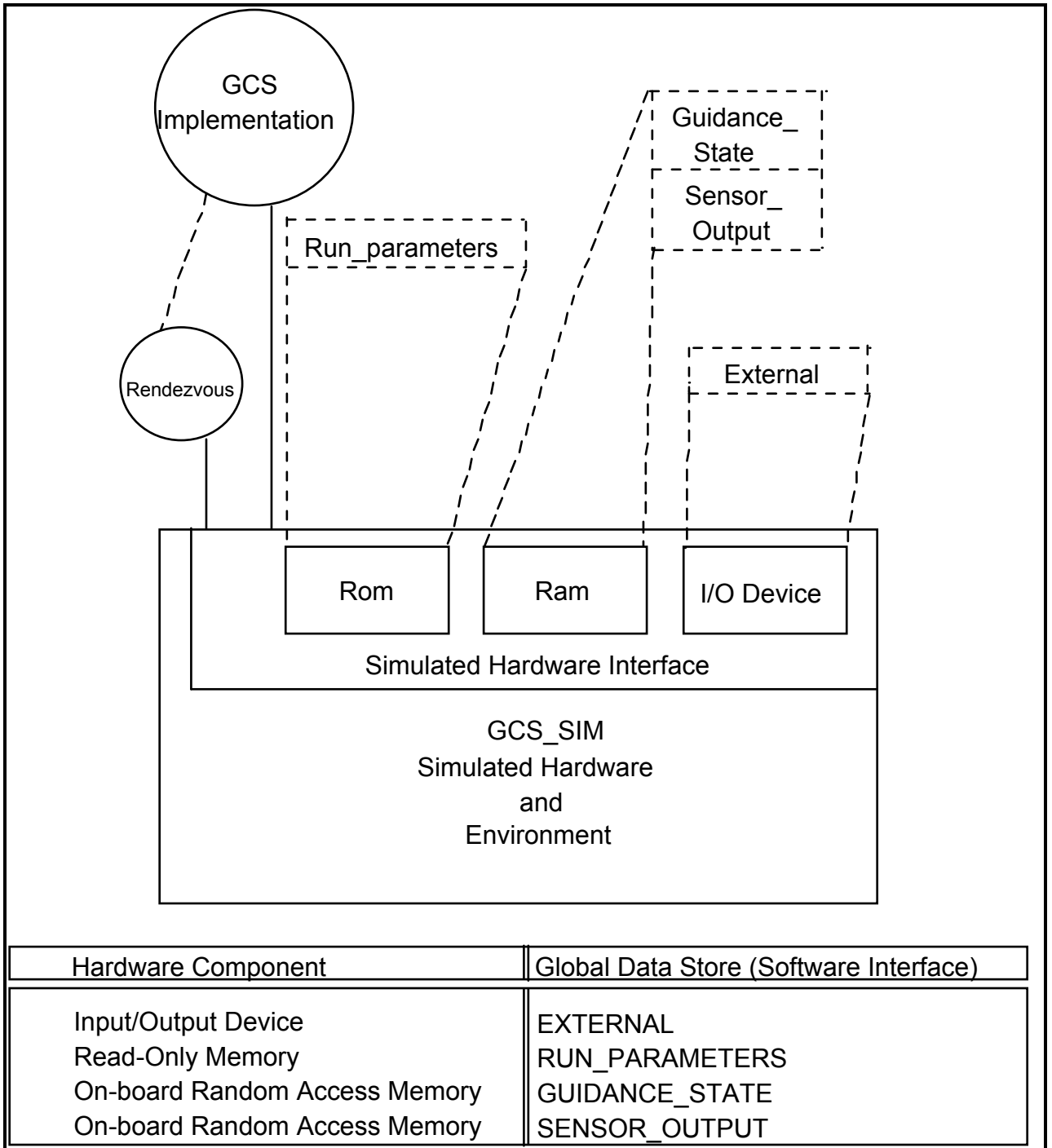
A single simulator support utility (GCS\_SIM\_RENDEZVOUS) is provided to form a uniform interface between the GCS implementation and the simulation environment (GCS\_SIM). This utility is a routine which simplifies the interface between the GCS implementations and the simulation of the vehicle sensing and control mechanisms. This utility also includes a synchronization mechanism for the configurations using more than one version of the GCS. This routine provides the following support functions:

- Initialization for the Beginning of Terminal Descent
- Simulator Rendezvous Synchronization
- GCS Interface for Simulated Reads and Writes

### **Input/Output**

The GCS\_SIM\_RENDEZVOUS routine simulates all of the input/output operations for each GCS implementation. When using the rendezvous routine with a GCS implementation, all data needed by rendezvous is passed via the four global data stores and there are no additional parameters required. All information *read from* or *written to* each GCS implementation will be transferred through the four global data stores defined in the data dictionary.

Figure A.8.1 DIAGRAM OF STORAGE AS SEEN BY GCS IMPLEMENTATIONS



## **Process**

The GCS uses the sensor input values in order to calculate control commands which are used by GCS\_SIM to manipulate the actuators. Since GCS\_SIM handles the *orbit to terminal descent* portion of each trajectory, a rendezvous must be issued at the start of each trajectory to load initial sensor values into each GCS implementation. Following the first call to rendezvous, all GCS implementations will synchronize themselves by calling rendezvous prior to the execution of each subframe. This rendezvous, in effect, suspends the GCS implementations until the other GCS implementations have processed this subframe.

The calling convention for this GCS\_SIM provided support utility is as follows:

- GCS\_SIM\_RENDEZVOUS (*requires no parameters*)

## **GCS Initialization**

During the initialization phase of each GCS trajectory (the first call to GCS\_SIM\_RENDEZVOUS) the frame counter (FRAME\_COUNTER) will be updated with the starting frame number for the particular trajectory, and the subframe counter (SUBFRAME\_COUNTER) will be initialized to the value one. Under *normal* circumstances, the value of the frame counter will be "1," but the programmer should not rely on that.

By using the interface described above, the simulator can be transparent to the implementation.

## **A.9 NUMERICAL INTEGRATION INSTRUCTIONS**

Within the Guidance Processing functional unit, the calculations of GP\_VELOCITY, GP\_ALTITUDE, and GP\_ATTITUDE require the use of a highly accurate integration method. To maintain the necessary degree of accuracy, three methods of numerical integration have been designated as acceptable for coding, namely Adams-Moulton method, Hamming's method, and the Runge-Kutta fourth-order method for simultaneous equations. If the Runge-Kutta method is used, it is required that the three equations be solved as a set of simultaneous equations.

Each method is briefly described in the following paragraphs, and references to numerical analysis texts describing the method are provided. Algorithms specified in either a text listed or another suitable numerical analysis text should be used during coding.

### **Adams-Moulton Method**

The Adams-Moulton Method requires values from the previous four time steps to calculate the value at the next time step. The Adams-Moulton method is a predictor/corrector method. Both (ref. A.14) (pp. 346-7) and (ref. A.16) (pp. 478-81) explain the Adams-Moulton method.

### **Hamming's Method**

The Hamming method uses a predictor/corrector method similar to that of Adams-Moulton. Hamming's method uses the same predictor as Milne's, but uses a much simpler corrector formula. Milne's method of integration was deemed too unstable for use, but Hamming's method with the simpler corrector is sufficiently stable. A description of both Hamming's method and Milne's method can be found in (ref. A.14) (pp. 347-8).

### **Runge-Kutta Fourth-Order Method for Simultaneous Equations**

The well-known Runge-Kutta fourth-order method for simultaneous equations requires only the previous two values to calculate the next value. References can be found in many texts including: (ref. A.15)(pp. 356-60), (ref. A.17) (pp. 240-6; pp. 282-5), (ref. A.18) (pg. 447; pp. 471-3)

During the first time step, using a numerical integration method necessitates some specification of previous values. These values will be provided during initialization for the data elements provided in Table A.9.1.

TABLE A.9.1 INITIAL VALUES PROVIDED FOR USE IN INTEGRATION

A_ACCELERATION (1..3, 0..4)
AR_ALTITUDE (0.4)
GP_ALTITUDE (0.4)
GP_ATTITUDE (1..3, 1..3, 0..4)
GP_VELOCITY (1..3, 0..4)
G_ROTATION (1..3, 0..4)
K_ALT (0.4)
K_MATRIX (1..3, 1..3, 0..4)
TDLR_VELOCITY (1..3, 0..4)

Note that not all integration required by the GCS specification requires the use of one of the methods listed in this appendix. More specifically, in computing THETA, TE\_INTEGRAL, PE\_INTEGRAL, and YE\_INTEGRAL, Euler's method provides sufficient accuracy and simplicity and should be used. Information on Euler's method may be found in: (ref. A.14)(pp. 318-22), (ref. A.15)(pg. 223), and (ref. A.16)(pp. 462-3).

**ADAPTATION OF RUNGE-KUTTE FOURTH-ORDER METHOD FOR SIMULTANEOUS EQUATIONS TO THE GCS SOFTWARE**

In the case where the Runge-Kutte method has been selected for integration in the Guidance Processing functional unit, the following gives information on how it is to be applied to GCS. The notation and formulas presented here are merely one representation of the Runge-Kutte method and its adaptation to GCS. The software designer/implementer may vary the notation and/or the form of the equations as long as the algorithm used is equivalent to the one presented here.

The Runge-Kutte fourth-order method (for one dependent variable only) can be summarized as follows:

Given:

Let  $dy/dx = f(x,y)$

Let h represent the interval between equidistant values of x

Let the initial values for x and y be  $x_0$  and  $y_0$  respectively

Let  $x_1 = x_0 + h$

The problem is to estimate  $y_1$

The solution is:

$y_1 = y_0 + k$

$k = 1/6 \times (k_1 + 2 \times (k_2 + k_3) + k_4)$

where:

$$\begin{aligned}
k_1 &= h \times f(x_0, y_0) \\
k_2 &= h \times f(x_0 + h/2, y_0 + k_1/2) \\
k_3 &= h \times f(x_0 + h/2, y_0 + k_2/2) \\
k_4 &= h \times f(x_0 + h, y_0 + k_3)
\end{aligned}$$

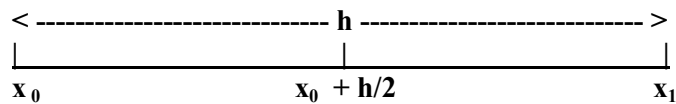
The GCS problem to be solved is as follows:

Simultaneously calculate current values for the variables GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE, using the equations for the corresponding derivatives given in GUIDANCE PROCESSING (P-Spec 2.2), Table A.5.8.

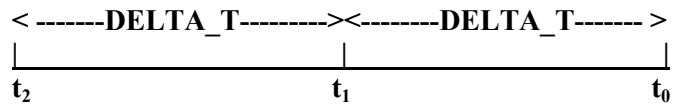
**Adaptation to GCS of the Runge-Kutte fourth-order method for simultaneous equations**

In the discussion that follows, let the "dependent" variables refer to GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE, and let the "sensor" variables refer to G\_ROTATION, A\_ACCELERATION, K\_MATRIX, TDLR\_VELOCITY, K\_ALT, and AR\_ALTITUDE. In the Runge-Kutte method, it is assumed that the derivative for y can be obtained as a function of the dependent and independent variables. In GCS, the derivative for each of the dependent variables is a function of some subset of the dependent variables and some subset of the sensor variables. The values for the sensor variables are only available to GCS at discrete values of time, namely at any time which is an integer multiple of the value of DELTA\_T. It is therefore not possible to calculate derivatives at the midpoint between two frames. The mapping of the Runge-Kutte independent variable to the GCS time interval is shown below. This mapping should be used, as it will ensure that derivatives can be calculated as required.

**Runge-Kutte**



**GCS**



	<b>t<sub>2</sub></b>	<b>t<sub>1</sub></b>	<b>t<sub>0</sub></b>	<b>Time</b>	
	<b>2</b>		<b>1</b>	<b>0</b>	<b>History</b>
<b>Subscript</b>					
	<b>n-2</b>	<b>n-1</b>	<b>n</b>	<b>Frame</b>	
<b>Number</b>					

where:

$$h = 2 \times \text{DELTA\_T}$$

$$t_0 = \text{present time} \quad (\text{time for the current frame})$$

$$t_1 = t_0 - \text{DELTA\_T} \quad (\text{time one frame ago})$$

$$t_2 = t_0 - (2 \times \text{DELTA\_T}) \quad (\text{time two frames ago})$$

### **The Algorithm**

The following is intended to be a conceptual representation of the Runge-Kutte algorithm as applied to GCS. It is not intended to be pseudo code or actual code. In this discussion, the subscripts for arrays have been omitted except for the history subscript which appears as "(j)" where j is 0, 1, or 2. This has been done here in order to present the concepts involved concisely, but without low-level details. The previously calculated values of the dependent variables at  $t_1$ , although available, are not to be used. Also note that the history values of the dependent and sensor variables with subscripts of 3 and 4 are not used in this adaptation of Runge-Kutte to GCS.

### **Notation**

Let  $k_1, k_2, k_3, k_4$  each represent a  $3 \times 3$  array to hold estimate for change in attitude.

Let  $l_1, l_2, l_3, l_4$  each represent a vector of size 3 to hold estimate for change in velocity.

Let  $m_1, m_2, m_3, m_4$  each represent a scalar to hold estimate for change in altitude.

Let SENS\_ATT(j) represent the G\_ROTATION array with time history subscript j, where j is 0, 1, or 2.

Let SENS\_VEL(j) represent the G\_ROTATION, A\_ACCELERATION, K\_MATRIX, and TDLR\_VELOCITY arrays with time history subscript (j), where j = 0, 1, or 2.

Let SENS\_ALT(j) represent the K\_ALT and AR\_ALTITUDE arrays with time history subscript j, where j = 0, 1, or 2.

Let  $f_{att}$  represent the function for derivative of attitude with respect to time.

Let  $f_{vel}$  represent the function for derivative of velocity with respect to time.

Let  $f_{alt}$  represent the function for derivative of altitude with respect to time.

### **Algorithm**

Do first estimates of changes using derivatives calculated at  $t_2$ .

$$\begin{aligned}
k_1 &= h \times f_{\text{att}}(\text{GP\_ATTITUDE}(2), \text{SENS\_ATT}(2)) \\
l_1 &= h \times f_{\text{vel}}(\text{GP\_ATTITUDE}(2), \text{GP\_VELOCITY}(2), \text{SENS\_VEL}(2)) \\
m_1 &= h \times f_{\text{alt}}(\text{GP\_ATTITUDE}(2), \text{GP\_VELOCITY}(2), \text{GP\_ALTITUDE}(2), \\
&\quad \text{SENS\_ALT}(2))
\end{aligned}$$

Do second estimates of changes using derivatives calculated at  $t_1$ :

$$\begin{aligned}
k_2 &= h \times f_{\text{att}}(\text{GP\_ATTITUDE}(2) + k_1/2, \text{SENS\_ATT}(1)) \\
l_2 &= h \times f_{\text{vel}}(\text{GP\_ATTITUDE}(2) + k_1/2, \text{GP\_VELOCITY}(2) + l_1/2, \text{SENS\_VEL}(1)) \\
m_2 &= h \times f_{\text{alt}}(\text{GP\_ATTITUDE}(2) + k_1/2, \text{GP\_VELOCITY}(2) + l_1/2, \\
&\quad \text{GP\_ALTITUDE}(2) + m_1/2, \text{SENS\_ALT}(1))
\end{aligned}$$

Do third estimates of changes using derivatives calculated at  $t_1$ :

$$\begin{aligned}
k_3 &= h \times f_{\text{att}}(\text{GP\_ATTITUDE}(2) + k_2/2, \text{SENS\_ATT}(1)) \\
l_3 &= h \times f_{\text{vel}}(\text{GP\_ATTITUDE}(2) + k_2/2, \text{GP\_VELOCITY}(2) + l_2/2, \text{SENS\_VEL}(1)) \\
m_3 &= h \times f_{\text{alt}}(\text{GP\_ATTITUDE}(2) + k_2/2, \text{GP\_VELOCITY}(2) + l_2/2, \\
&\quad \text{GP\_ALTITUDE}(2) + m_2/2, \text{SENS\_ALT}(1))
\end{aligned}$$

Do fourth estimates of changes using derivatives calculated at  $t_0$ :

$$\begin{aligned}
k_4 &= h \times f_{\text{att}}(\text{GP\_ATTITUDE}(2) + k_3, \text{SENS\_ATT}(0)) \\
l_4 &= h \times f_{\text{vel}}(\text{GP\_ATTITUDE}(2) + k_3, \text{GP\_VELOCITY}(2) + l_3, \text{SENS\_VEL}(0)) \\
m_4 &= h \times f_{\text{alt}}(\text{GP\_ATTITUDE}(2) + k_3, \text{GP\_VELOCITY}(2) + l_3, \text{GP\_ALTITUDE}(2) + \\
&\quad m_3, \text{SENS\_ALT}(0))
\end{aligned}$$

Add weighted average of four change estimates to previous value of dependent variable to get current dependent variable:

$$\begin{aligned}
\text{GP\_ATTITUDE}(0) &= \text{GP\_ATTITUDE}(2) + 1/6 \times (k_1 + 2 \times (k_2 + k_3) + k_4) \\
\text{GP\_VELOCITY}(0) &= \text{GP\_VELOCITY}(2) + 1/6 \times (l_1 + 2 \times (l_2 + l_3) + l_4) \\
\text{GP\_ALTITUDE}(0) &= \text{GP\_ALTITUDE}(2) + 1/6 \times (m_1 + 2 \times (m_2 + m_3) + m_4)
\end{aligned}$$

## A.10 COMMUNICATIONS PACKET INSTRUCTIONS

### STRUCTURE OF PACKET

The global variable PACKET is defined in the data dictionary as an array of 256 elements of type Integer\*2. The actual memory which holds this array can also be thought of as an array of 512 elements of type Byte. The message to be transmitted can therefore be thought of as a series of contiguous bytes, as illustrated in Table A.5.7. The message on which the checksum is to be calculated consists of the synchronization pattern, the sequence number, the sample mask, and the data section. The data section always begins in the eighth byte, but the position of the last byte of the data section depends upon the particular subframe in which the packet is being transmitted. The checksum is always in the two bytes immediately following the last used byte of the data section for the subframe, or in other words, immediately following the message. The bytes of PACKET following the checksum are unused.



Subframe	Byte Position of Message	Position of Least Significant Byte of Checksum	Position of Most Significant Byte of Checksum
1	1 - 129	130	131
2	1 - 173	174	175
3	1 - 45	46	47

## PROCEDURE FOR CALCULATING THE CHECKSUM

The message polynomial is to be formed as described below, and then is to be multiplied by  $2^{16}$ . This product polynomial is to be divided by the generator polynomial, using modulo 2 arithmetic. The 16-bit remainder obtained from this division (with its bits in reverse order) is the checksum, and is to be placed into the packet immediately following the message.

### Conventions

Byte 1 of the synchronization pattern will be referred to as the first byte of the message, while the last used byte of the data section will be referred to as the last byte of the message. Each number appearing below is given with the most significant digit on the left, and the least significant digit on the right. When bit numbers are referenced, they are the VAX FORTRAN bit numbers (bit 0 is the least significant bit, while bit 7 is the most significant bit of the byte).

#### Form the Message Polynomial

Let  $n$  represent the number of bytes in the message

Let  $\text{pbyte}_i$  represent byte  $i$  of the packet

Let  $\text{bit}_{i,j}$  represent bit  $j$  of byte  $i$  of the packet. Then,

$\langle \text{pbyte}_i \rangle = \langle \text{bit}_{i,7} \rangle \langle \text{bit}_{i,6} \rangle \langle \text{bit}_{i,5} \rangle \langle \text{bit}_{i,4} \rangle \langle \text{bit}_{i,3} \rangle \langle \text{bit}_{i,2} \rangle \langle \text{bit}_{i,1} \rangle \langle \text{bit}_{i,0} \rangle$

$\langle \text{mbyte}_i \rangle = \langle \text{bit}_{i,0} \rangle \langle \text{bit}_{i,1} \rangle \langle \text{bit}_{i,2} \rangle \langle \text{bit}_{i,3} \rangle \langle \text{bit}_{i,4} \rangle \langle \text{bit}_{i,5} \rangle \langle \text{bit}_{i,6} \rangle \langle \text{bit}_{i,7} \rangle$

$\langle \text{Message Polynomial} \rangle = \langle \text{mbyte}_1 \rangle \langle \text{mbyte}_2 \rangle \dots \langle \text{mbyte}_n \rangle$

In other words, the message polynomial is formed by taking the bytes of the message in order from the first to the last, but within each byte, taking the bits in order from the least to the most significant.

#### Form the Dividend

$\langle \text{Dividend} \rangle = \langle \text{Message Polynomial} \rangle \langle 0000000000000000 \rangle$

The dividend is formed by multiplying the message polynomial by  $2^{16}$ , or in other words, by appending 16 zeroes to the end of the polynomial.

#### Form the Divisor

$\langle \text{Divisor} \rangle = \langle 11000000000000101 \rangle$

The divisor is the CRC-16 generator polynomial, which is  $x^{16} + x^{15} + x^2 + x^0$

#### Perform the Long Division

Divide the dividend by the divisor, using modulo two arithmetic.

#### Form the Checksum and Place it into the Packet

Let  $R$  represent the final 16-bit remainder from the long division.

Let  $\langle R_i \rangle$  represent bit  $i$  of  $R$ . Then,

$\langle R \rangle =$

$\langle R_{15} \rangle \langle R_{14} \rangle \langle R_{13} \rangle \langle R_{12} \rangle \langle R_{11} \rangle \langle R_{10} \rangle \langle R_9 \rangle \langle R_8 \rangle \langle R_7 \rangle \langle R_6 \rangle \langle R_5 \rangle \langle R_4 \rangle \langle R_3 \rangle \langle R_2 \rangle \langle R_1 \rangle \langle R_0 \rangle$

$\rangle$

$\langle \text{Checksum} \rangle =$

$\langle R_0 \rangle \langle R_1 \rangle \langle R_2 \rangle \langle R_3 \rangle \langle R_4 \rangle \langle R_5 \rangle \langle R_6 \rangle \langle R_7 \rangle \langle R_8 \rangle \langle R_9 \rangle \langle R_{10} \rangle \langle R_{11} \rangle \langle R_{12} \rangle \langle R_{13} \rangle \langle R_{14} \rangle \langle R_{15} \rangle$

$\rangle$

Thus, the checksum is the final 16-bit remainder, with the bits reversed.  
The checksum is to be placed into the packet in standard VAX byte order, immediately following the last used byte of the message.

### **CHECKSUM ALGORITHMS**

While different algorithms exist for calculating the checksum, any algorithm used in an implementation must be equivalent to, or accomplish the same results as the procedure described above.

### **EXAMPLE OF THE CALCULATION OF A CHECKSUM**

Assume that the message to be sent consists of four bytes (this message is obviously shorter than any message to be sent in any GCS subframe, but it is infeasible to present an example with a message of 45 bytes or more).

Assume the message to be sent is:

Byte Position	Contents in Hexadecimal	Contents in Binary
1	44	01000100
2	4F	01001111
3	56	01010110
4	45	01000101

In this example, the long division(in binary) is as follows:

$$\begin{array}{r}
 \phantom{1100000000000101} \phantom{)0010001011110010011010101010001000000000000000} \phantom{11110010100010011100011110110} \\
 11000000000000101 \phantom{)0010001011110010011010101010001000000000000000} \phantom{11110010100010011100011110110} \\
 \underline{11000000000000101} \\
 10010111100101100 \\
 \underline{11000000000000101} \\
 10101111001010011 \\
 \underline{11000000000000101} \\
 11011110010101100 \\
 \underline{11000000000000101} \\
 11110010101001101 \\
 \underline{11000000000000101} \\
 11001010100100001 \\
 \underline{11000000000000101} \\
 10101001001000001 \\
 \underline{11000000000000101} \\
 11010010010001000 \\
 \underline{11000000000000101} \\
 10010010001101000 \\
 \underline{11000000000000101} \\
 10100100011011010 \\
 \underline{11000000000000101} \\
 11001000110111110 \\
 \underline{11000000000000101} \\
 10001101110110000 \\
 \underline{11000000000000101} \\
 10011011101101010 \\
 \underline{11000000000000101} \\
 10110111011011110 \\
 \underline{11000000000000101} \\
 11101110110110110 \\
 \underline{11000000000000101} \\
 10111011011001100 \\
 \underline{11000000000000101} \\
 11110110110010010 \\
 \underline{11000000000000101} \\
 1101101100101110
 \end{array}$$

The remainder is 1101101100101110

The checksum is then the remainder with the bits reversed, or: 0111010011011011

The two bytes of the checksum will then be placed into the bytes immediately following the data portion, in standard VAX byte order (low order byte first followed by high order byte) as follows:

Byte Position	Contents in Hexadecimal	Contents in Binary
1	44	01000100
2	4F	01001111
3	56	01010110
4	45	01000101
5	DB	11011011
6	74	01110100

## A.11 BIBLIOGRAPHY

- A.1 George B. Finelli. Results of software error-data experiments. In AIAA/AHS/ASEE Aircraft Design, Systems and Operations Conference, Atlanta, GA, September 1988.
- A.2 Special Committee 167 of Requirements and Technical Concepts for Aviation Inc. (RTCA, Inc.). Software Considerations in Airborne Systems and Equipment Certification, DOCUMENT NO. RTCA/DO-178B. RTCA Inc., Washington, D. C., 1992
- A.3 Harm Buning and D. T. Greenwood. Flight mechanics for space and re-entry vehicles. Technical report, The University of Michigan Engineering Summer Conferences, Summer 1964.
- A.4 Herbert Goldstein. Classical Mechanics. Addison-Wesley Publishing Company, Inc., Reading, Massachusetts, USA, 1959.
- A.5 Irving H. Shames. Engineering Mechanics -- Statics and Dynamics. Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1980.
- A.6 Dan Edwin Christie. Vector Mechanics. McGraw-Hill Inc., New York, 1964
- A.7 David Hestenes. New Foundations for Classical Mechanics. D. Reidel Publishing Company, Boston, 1986
- A.8 D. N. Burghes and A. M. Downs. Classical Mechanics and Control. Ellis Horwood Limited, Coll House, Westergate, England, 1975.
- A.9 G. S. Light and J. B. Higham. Theoretical Mechanics. Longman Inc., New York, 1975.
- A.10 Don C. Rich and J. R. Dunham. Guidance and Control Software Simulator (GCS\_SIM) Software Specification. Technical Report NASA Contract NAS1-17964; Task Assignment No. 8, Research Triangle Institute, Research Triangle Park, NC, 1987.
- A.11 Andrew S. Tanenbaum. Computer Networks. Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1981.

- A.12 Derek J. Hatley. The use of structured methods in the development of large, software-based avionics systems. In Proceedings of the AIAA/IEEE 6th Digital Avionics Systems Conference, New York, December 1984.
- A.13 Derek J. Hatley and Imtiaz A. Pirbhai, Strategies for Real-Time System Specification. Dorset House Publishing Company, New York, New York, 1987.
- A.14 W. Allen Smith. Elementary Numerical Analysis. Harper and Row, New York, 1979.
- A.15 J. B. Scarborough. Numerical Mathematical Analysis. The Johns Hopkins Press, Baltimore, 1962
- A.16 Stephen M. Pizer. Numerical Computing and Mathematical Analysis. Science Research Associates, Inc., Chicago, 1975
- A.17 Richard L. Burden and J. Douglas Faires. Numerical Analysis. PWS-KENT Publishing Company, Boston, 1989.
- A.18 Melvin J. Maron and Robert J. Lopez. Numerical Analysis: A Practical Approach. Wadsworth Publishing Company, Belmont, California, 1990.
- A.19 *teamwork/SA teamwork/RT* User's Guide, Cadre Technologies, Inc., Providence, Rhode Island, Release 4.0, 1990.
- A.20 Neil A. Holmberg, Robert P. Faust, and H. Milton Holt, Viking '75 Spacecraft Design and Test Summary, Volume I - Lander Design, NASA Reference Publication 1027, Langley Research Center, Hampton, Virginia, 1980

## **Appendix B: Design Description for the Pluto Implementation of the Guidance and Control Software**

Authors: Philip Morris and Rob Angellatta, Lockheed Martin Engineering and Sciences Corp.

This document was produced as part of Guidance and Control Software (GCS) Project conducted at NASA Langley Research Center. Although some of the requirements for the Guidance and Control Software application were derived from the NASA Viking Mission to Mars, this document does not contain data from an actual NASA mission.

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## **B.1 Introduction to Pluto GCS Design**

This document contains a detailed description of the Pluto software design. The Pluto software design fully encompasses all software requirements as presented in the GCS Guidance and Control Software Development Specification (ref. B.3) defining a GCS implementation. The Pluto design provides full and complete software design specifications suitable for coding a GCS implementation.

### **B.1.1 Top-Level Description**

A GCS implementation represents the guidance and control subsystem of a planetary landing vehicle. The guidance and control subsystem provides navigation, guidance, and attitude control for the lander during the terminal phase of a planetary landing. The Terminal phase of a planetary landing refers to the vehicle events beginning with the separation from the aeroshell to the actual contact with the planet surface.

The overall objective of the guidance and control subsystem is to effect a safe landing and to communicate the lander's telemetry data to a remote receiving station. Pluto implements a velocity-altitude contour (VAC) strategy for fulfilling the guidance and control responsibilities. The VAC strategy consists of attempting to match the vehicle's actual velocity-altitude contour with a predetermined descent contour stored in the flight software.

The communication task consists of preparing the appropriate telemetry data for transmission by the on-board communication gear. Preparing the telemetry data involves building a communications packet containing various vehicle guidance and control information. Periodically, a communications packet is prepared and provided to the communications gear for transmission.

### **B.1.2 Design Methodology**

The Pluto design specification has been developed using the structured analysis with real time extensions (SA/RT) methodology as embodied in Cadre's Teamwork/SA (ref. B.4) and Teamwork/RT software development tools. Cadre's Teamwork/SA implements the Structured Analysis (SA) approach to systems analysis as described by DeMarco (ref. B.5). Cadre's Teamwork/RT is the companion product of Teamwork/SA implementing the real-time extensions to SA as described by Hatley (ref. B.6).

The SA/RT software specification methodology emphasizes data flow between processes. Individual processes are activated when their input data is available. In addition, explicit control specifications are available for describing process sequencing which is often necessary in real-time systems.

Note that both the SA and SA/RT methodologies are intended to describe software development specifications. The Structured Design (SD) methodology, as described by Page-Jones (ref. B.7), is more appropriate for describing the Pluto design specifications. However, the Pluto design was originally developed using SA/RT and during the transition to in-house software development, a decision was made to stay with SA/RT. The potential loss in design description capability directly attributable to the SA/RT methodology as compared with the SD methodology is minimal as compared to the loss of development man-hours it would cost to convert the design from SA/RT to SD during the transition phase.



### B.1.3 Design Syntax Specifications

The main criterion for choosing an algorithm language for describing the Pluto design was that the algorithms should be clear, concise, and easy to read. No specific language was chosen to describe the algorithms of the Pluto design; rather, a “structured English” approach is followed. The language, with a few exceptions, is very similar to the Pascal programming language.

The algorithm description language’s major deviations from Pascal are as follows: First, blocks are not delimited by “BEGIN/END” pairs. Blocks are readily apparent and an “END” appears in a few instances to clarify the end of a block. Semicolons are not used to signify the end of a statement. Again, the end of the statements is quite obvious.

A few conventions were borrowed from the C programming language. Hexadecimal value notation appears as 0xdddd where “0x” identifies “dddd” as a hexadecimal value. A few bitwise binary operators are introduced; “&” signifies bitwise *and* operation, “XOR” signifies bitwise *exclusive or* operation, and “>>” represents the bitwise *shift right* operation.

Two syntax features are peculiar to P-Spec 1.8 CP. The at sign “@” was selected to serve as an indirection operator. It has the same semantics as Pascal’s “^”. The reason for not maintaining the caret “^” for specifying indirection is that it was previously chosen to signify exponentiation. The Modula-2 record syntax was selected for specifying records primarily for its ability to support deviate record structure. Also, when specifying the records, it is necessary to define the size of particular data types. Several terms were introduced for specifying the size of particular data elements: byte - an 8-bit quantity, word - a 16-bit quantity, longword a 32-bit quantity, and quadword a 64-bit quantity.

## B.2 Design Structure

In the Teamwork representation of the Pluto design given in B.4, the SA/RT software specification methodology organizes the design as a top-down functional decomposition. As such, the Pluto design described in this section follows the top-down functional decomposition.

### B.2.1 High-level Software Design

The ultimate goal of the guidance and control subsystem is to safely land the vehicle onto the planet’s surface. Pluto attempts to safely land the vehicle by sensing the vehicle’s position relative to the designated landing surface and commanding the vehicle’s locomotive resources in an effort to maintain a predetermined descent contour. A secondary goal of the guidance and control subsystem is to provide periodic communications of the vehicle’s telemetry data.

The design context diagram depicts Pluto as a process transforming raw sensor data into various output data. The raw sensor data originates from the on-board sensors. As a process, Pluto transforms the incoming raw sensor data into engine data which is passed on to the engine controller and packet data which is passed on to the communications gear, and when appropriate issues the chute\_released signal.

Pluto organizes the vehicle terminal descent as a sequence of time slices. That is, Pluto divides the vehicle’s journey into regular intervals of time. Each “time slice”, or frame, has a well defined time duration as specified by the constant DELTA\_T. During each frame, Pluto first determines the vehicle’s position relative to the planet’s surface and computes the vehicle’s actual descent contour, then Pluto decides how closely the actual descent contour matches the predetermined VAC, and finally computes and issues the necessary corrective action.

As depicted in DFD 0, Pluto processing is partitioned into three processes. Process 1, the Sensor Processing Subframe, is responsible for gathering and transforming, if necessary, the current information available from the vehicle's sensors. Process 2, the Guidance Processing Subframe, is responsible for determining if the vehicle's actual VAC matches the preprogrammed VAC. Process 3, the Control Law Subframe is responsible for maneuvering necessary to put the vehicle closer to the preprogrammed VAC.

Each frame consists of performing the Sensor Processing Subframe processing, followed by the Guidance Processing Subframe processing, followed by the Control Law Subframe processing. This control structure is represented by PAT 0-s1. When Pluto processing is started, the data element GP\_PHASE is initialized to 1. Pluto processing always begins at the beginning of a frame and will always terminate at the completion of a frame. Termination occurs at the completion of Control Law Processing Subframe processing during the frame in which Guidance Processing Subframe processing asserts the signal GP\_PHASE to 5.

The Sensor Processing Subframe is responsible for collecting the information provided by the on-board sensors. The vehicle's sensors include accelerometers, gyroscopes, temperature sensors, an altimeter radar, a four-beam Doppler radar, and a touch-down switch. Sensor Processing Subframe processing is decomposed into eight distinct tasks as represented by the eight processes of DFD 1. The specific responsibilities assigned to each process are detailed in section 2.3 below.

PAT 1-s1 contains the control specification for the processes of DFD 1, Sensor Processing Subframe. It is not immediately obvious why the data element SUBFRAME\_COUNTER was selected as the input to PAT 1-s1. Within each of the three "subframe" processes, a specific order of process activation is required. This particular ordering is necessary when the activation of some process depends upon the completion of another process.

The PAT is a control specification designed specifically for representing the ordering of process activation. The Pat specifies dependencies in the ordering of process activation via the conditions of the input signals. Although in PAT 1-s1, signal conditions are not necessary for determining the sequencing of process activation's, the Teamwork SA/RT implementation of the PAT requires an input signal. So, an input signal, the data element SUBFRAME\_COUNTER, and its value have been selected which always evaluates to "true". This is also the case with PAT 2-s1 and PAT 3-s1.

The major responsibilities of the Guidance Processing Subframe are to determine the current state of the vehicle and to determine how closely the actual vehicle VAC matches the preprogrammed VAC. These tasks are partitioned into three processes as depicted on DFD 2. The process named GCS\_SIM\_RENDEZVOUS appears on DFD 1, DFD 2 and DFD 3. All three "bubbles" represent the same process. At the beginning of each "subframe", Pluto is required to contact the other vehicle subsystems. GCS\_SIM\_RENDEZVOUS processing provides the interface to the other vehicle subsystems. The requirements for GCS\_SIM\_RENDEZVOUS are described in section 2.3 below.

Once Pluto has determined the present vehicle state, it is necessary to command the vehicle's locomotive resources, if available, in an effort to maintain the desired VAC. This responsibility is charged to the Control Law Processing Subframe. This processing is responsible for releasing the parachute and computing the appropriate engine commands. The process named CP appears on DFD 1, DFD 2 and DFD 3. All three "bubbles" represent the same process. At the end of each "subframe", Pluto is required to transmit particular telemetry data to a remote receiving station. CP processing is delegated the task of periodic telemetry communications.

## B.2.2 Data and Control Flow

Consistent with the Software Development Specification, Pluto organizes its global storage into four data stores labeled EXTERNAL, GUIDANCE\_STATE, SENSOR\_OUTPUT, RUN\_PARAMETERS. The data dictionary describes the organization of each data store and describes each of the data elements comprising the data stores.

The data stores are represented on DFD 1, DFD 2, and DFD 3. Each DFD clearly depicts the data flows between the represented processes and the data stores. It is important to note that a non-labeled data flow indicates that all data elements contained in the data store are available in the flow. The data flows originating and terminating in the process GCS\_SIM\_RENDEZVOUS are not labeled. All data elements stored in each of the data stores is available as input and output to the process GCS\_SIM\_RENDEZVOUS. However, GCS\_SIM\_RENDEZVOUS does not necessarily process as input or update as output all of the elements of each data store. The Pluto control flow is described above in section 2.1 High-level software design.

## B.2.3 Module Description

Process specifications, better known as P-Specs, reside at the lowest level of decomposition in the SA/RT development methodology. P-Specs provide a functional description of the necessary processing within a process. A map to the P-Specs found in Pluto is presented below.

The Sensor Processing Subframe provides the guidance and control subsystem with an interface to the vehicle's on-board sensors. The vehicle's sensors provide Pluto with information pertaining to the lander's current state within the terminal descent operation. Sensor Processing Subframe processing is decomposed into eight distinct tasks as described below.

The GCS\_SIM\_RENDEZVOUS process is responsible for the Pluto communications with other vehicle subsystems. GCS\_SIM\_RENDEZVOUS has both read and write access to all four of the global stores. The actual implementation of the GCS\_SIM\_RENDEZVOUS functionality will be provided to the implementer. GCS\_SIM\_RENDEZVOUS is represented in the Sensor Processing subframe by DFD 1.1, in the Guidance Processing subframe by DFD 2.1, and in the Control Law Processing subframe by DFD 3.1. The functional processing of GCS\_SIM\_RENDEZVOUS is represented in P-Spec 1.1.

The ARSP process is responsible for determining the distance from the vehicle to the landing surface. ARSP processes data originating from the on-board altimeter radar sensor and reports the vehicle's altitude above the planet's surface. DFD 1.2 represents the role of ARSP in the Sensor processing subframe and P-Spec 1.2 specifies the ARSP functional processing.

ARSP processing requires an extrapolation algorithm for computing the value of AR\_ALTITUDE. The development specifications calls for extrapolating a value for AR\_ALTITUDE from a third-order polynomial fitted to the previous four values of AR\_ALTITUDE. Given four equally spaced values, we can approximate the third order function representing the polynomial containing the given values. The fifth value in the series may then be extrapolated from this function. The value of DELTA\_T represents the spacing of the values stored in AR\_ALTITUDE.

ARSP employs the divided difference technique for performing the necessary extrapolation. Begin by constructing a difference table for the given values. The first column represents the given values of AR\_ALTITUDE reported in the most recent previous four frames. The second column entries are computed as the difference between adjacent column one entries. Similarly, the third column entries are computed as the difference between adjacent column two entries.

The fourth column is computed as the difference between the column three entries. Letting “A” represent the data element “AR\_ALTITUDE” and “t” represent the current frame, the table appears as:

Frame number	Column			
	1	2	3	4
t-4	A[4]			
		A[3]-A[4]		
t-3	A[3]		(A[2]-A[3])-(A[3]-A[4])	
		A[2]-A[3]	((A[1]-A[2])-(A[2]-A[3]))-((A[2]-A[3])-(A[3]-A[4]))	
t-2	A[2]		(A[1]-A[2])-(A[2]-A[3])	
		A[1]-A[2]		
t-1	A[1]			
t-0				

An extrapolation of the altitude for the current frame is constructed by summing the last element of each column:

$$A[0] = A[1] + A[1]-A[2] + (A[1]-A[2])-(A[2]-A[3]) + ((A[1]-A[2])-(A[2]-A[3]))-((A[2]-A[3])-(A[3]-A[4]))$$

Simplifying the equation yields:

$$A[0] = 4*A[1] - 6*A[2] + 4*A[3] - A[4]$$

The ASP process is responsible for determining the vehicle accelerations along each of its three axes. ASP processes data originating from the on-board accelerometers and reports the vehicle accelerations. DFD 1.3 represents the role of ASP in the Sensor processing subframe and P-Spec 1.3 specifies the ASP functional processing.

The CP process is responsible for preparing a data packet suitable for transmission by the on-board communications gear. CP collects the appropriate data from the four global stores and arranges them into a data packet. CP is represented in the Sensor Processing subframe by DFD 1.8, in the Guidance Processing subframe by DFD 2.3, and in the Control Law Processing subframe by DFD 3.5. The functional processing of CP is described in P-Spec 1.8.

The GSP process is responsible for determining the vehicle’s rotation rates. GSP processes data originating from the on-board gyroscope sensors and reports the vehicle rotation rates. DFD 1.4 represents the role of GSP in the Sensor processing subframe and P-Spec 1.4 specifies the GSP functional processing.

The TDLRSP process is responsible for computing vehicle’s descent velocities. TDLRSP processes data originating from the on-board touch down landing radar sensor and reports the vehicle descent velocities. DFD 1.5 represents the role of TDLRSP in the Sensor processing subframe and P-Spec 1.5 specifies the TDLRSP functional processing.

The TDSP process is responsible for determining the vehicle’s touch down status. TDSP processes data originating from the on-board touch down sensor and reports the vehicle’s touch down status. DFD 1.6 represents the role of TDSP in the Sensor processing subframe and P-Spec 1.6 specifies the TDSP functional processing.

The TSP process is responsible for determining the ambient atmospheric temperature. TSP processes data originating from the two on-board temperature sensors and reports the ambient

atmospheric temperature. DFD 1.7 represents the role of TSP in the Sensor processing subframe and P-Spec 1.7 specifies the TSP functional processing.

TSP contains four algorithms for computing the atmospheric temperature. The algorithm for computing the temperature based on the solid state (SS) sensor has been derived as follows. The task is to determine the linear function specifying the linear equation containing the points (M1, T1) and (M2, T2).

$$y = mx + b$$

where:  $m$  is the slope of the line  
 $b$  is the y intercept

substituting the given point (M1, T1) for (x, y):

$$T1 = m \cdot M1 + b$$

$$b = T1 - m \cdot M1$$

the slope of the line is expressed by the delta y divided by delta x:

$$m = \frac{T2 - T1}{M2 - M1}$$

substituting into the point-slope equation gives:

$$solid\_state\_temp = \frac{T2 - T1}{M2 - M1} \cdot SS\_TEMP + T1 - \frac{T2 - T1}{M2 - M1} \cdot M1$$

The algorithm for converting a sensor measure residing in the lower parabolic region of the thermo-couple (TC) sensor was developed as follows. The first task is to determine the function which describes the lower parabolic region of the TC sensor:

$$y = \frac{1}{4p} \cdot (x - h)^2 + k$$

where:  $(h, k)$  is the vertex  
 $y = (k - p)$  is the directrix

Given that "the temperature goes down as the square of the measurement":

$$y = \frac{1}{4p} \cdot (x - h)^2 + k \quad \text{standard equation of parabola}$$

$$y = -(x - h)^2 + k \quad \text{from spec. "goes down as the square"}$$

$$\frac{1}{4p} = -1$$

$$p = -\frac{1}{4}$$

The derivative of a function at a given point is equivalent to the slope of the line tangent to the function at the given point.

$$f(x) = y = -(x - h)^2 + k$$

$$f'(x) = -2(x - h)$$

The slope of the line tangent to point (M3, T3):

$$m = -2(M3 - h)$$

$$h = M3 + \frac{m}{2}$$

Note, the slope of the line tangent to the point is equivalent to the slope of the line containing the points (M3, T3) and (M4, T4), so:

$$m = \frac{T4 - T3}{M4 - M3}$$

substituting the given point (M3, T3) for (x, y):

$$T3 = -(M3 - (M3 + \frac{m}{2}))^2 + k$$

$$k = T3 + \left(\frac{m}{2}\right)^2$$

The function representing the TC sensor lower parabolic region:

$$y = \frac{1}{4p} \cdot (x - h)^2 + k$$

$$\text{where: } p = -\frac{1}{4}, \quad h = M3 + \frac{m}{2}, \quad k = T3 + \left(\frac{m}{2}\right)^2, \quad \text{and } m = \frac{T4 - T3}{M4 - M3}$$

$$\text{lower\_parabolic\_function} = -\left[ x - \left( M3 + \left( \frac{T4 - T3}{M4 - M3} \right) \right) \right]^2 + T3 + \left( \frac{T4 - T3}{M4 - M3} \right)^2$$

Similarly, the algorithm for converting a sensor measure residing in the upper parabolic region of the thermo-couple sensor was developed as follows. The function which describes the upper parabolic region of the TC sensor:

$$y = \frac{1}{4p} \cdot (x - h)^2 + k$$

$$\text{where: } (h, k) \text{ is the vertex}$$

$$y = (k - p) \text{ is the directrix}$$

Given "the temp. goes up as the square of the measurement":

$$y = \frac{1}{4p} \cdot (x - h)^2 + k \quad \text{standard equation of parabola}$$

$$y = (x - h)^2 + k \quad \text{from spec. "goes up as the square"}$$

$$\frac{1}{4p} = 1$$

$$p = \frac{1}{4}$$

The derivative of a function at a given point is equivalent to the slope of the line tangent to the function at the given point.

$$f(x) = y = (x - h)^2 + k$$

$$f'(x) = 2(x - h)$$

The slope of the line tangent to point (M4, T4):

$$m = 2(M4 - h)$$

$$h = M4 - \frac{m}{2}$$

Note, the slope of the line tangent to the point is equivalent to the slope of the line containing the points (M3, T3) and (M4, T4), so:

$$m = \frac{T4 - T3}{M4 - M3}$$

substituting the given point (M4, T4) for (x, y):

$$T4 = (M4 - (M4 + \frac{m}{2}))^2 + k$$

$$k = T4 - \left(\frac{m}{2}\right)^2$$

The function representing the TC sensor upper parabolic region:

$$y = \frac{1}{4p} \cdot (x - h)^2 + k$$

$$\text{where: } p = \frac{1}{4}, \quad h = M4 - \frac{m}{2}, \quad k = T4 - \left(\frac{m}{2}\right)^2, \quad \text{and } m = \frac{T4 - T3}{M4 - M3}$$

$$\text{upper\_parabolic\_function} = \left( x - \left( M4 - \left( \frac{T4 - T3}{M4 - M3} \right) \right) \right)^2 + T4 - \left( \frac{T4 - T3}{M4 - M3} \right)^2$$

And finally, the algorithm for converting a sensor measure residing in the linear region of the thermo-couple sensor was developed as follows. The task is to determine the linear function specifying the linear equation containing the points (M3, T3) and (M4, T4).

$$y = mx + b$$

where: *m* is the slope of the line  
*b* is the y intercept

substituting the given point (M3, T3) for (x, y):

$$T3 = m \cdot M3 + b$$

$$b = T3 - m \cdot M3$$

the slope of the line is expressed by the delta y divided by delta x:

$$m = \frac{T4 - T3}{M4 - M3}$$

substituting into the point-slope equation gives:

$$tc\_linear\_temp = \frac{T4 - T3}{M4 - M3} \cdot THERMO\_TEMP + T3 - \frac{T4 - T3}{M4 - M3} \cdot M3$$

The GP process is responsible for the guidance tasks of the vehicle. Guidance tasks include determining the current vehicle VAC, determining how closely the actual vehicle VAC matches the preprogrammed VAC, determining which set of engine control law should be in effect, and determining the appropriate state for the engines. GP processes data originating in the Sensor Processing Subframe, the preprogrammed run parameters, and the engine state data in performing the various guidance tasks. DFD 2.2 represents the role of GP in the Sensor processing subframe and P-Spec 2.2 specifies the GP functional processing.

When computing the optimal velocity during the GP processing, there is one case where interpolation is necessary and two cases where extrapolation is required. Note, in order to implement the following routines, it is assumed that the velocity altitude array data contains at least two valid entries.

Given the point (x<sub>0</sub>, f(x<sub>0</sub>)), the point (x<sub>1</sub>, f(x<sub>1</sub>)), and the x value of the desired point (x, f(x)) where x<sub>0</sub> < x < x<sub>1</sub>, interpolate to find f(x)

$$\frac{f(x) - f(x_0)}{x - x_0} = \frac{f(x_1) - f(x_0)}{x_1 - x_0}$$

$$f(x) = f(x_0) + \frac{f(x_1) - f(x_0)}{x_1 - x_0} \cdot (x - x_0)$$

There are two cases for extrapolation. First, if the desired value is greater than the largest value stored in the velocity-altitude contour table, then a value must be extrapolated above the largest value stored in the table. Letting  $(x_0, f(x_0))$  refer to the second largest value stored in the velocity-altitude contour table and  $(x_1, f(x_1))$  refer to the largest value stored in the velocity-altitude contour table, the formula for extrapolation is:

$$\frac{f(x) - f(x_0)}{x - x_0} = \frac{f(x_1) - f(x_0)}{x_1 - x_0}$$

$$f(x) = f(x_0) + \frac{f(x_1) - f(x_0)}{x_1 - x_0} \cdot (x - x_0)$$

This is not misprinted, it is indeed the same formula displayed above describing the interpolation.

In the case where the desired value is less than the smallest value stored in the velocity-altitude contour table, then a value must be extrapolated below the smallest value stored in the table. Letting  $(x_0, f(x_0))$  refer to the smallest value stored in the velocity-altitude contour table and  $(x_1, f(x_1))$  refer to the second smallest value stored in the velocity-altitude contour table, the formula for extrapolation is:

$$\frac{f(x_0) - f(x)}{x_0 - x} = \frac{f(x_1) - f(x_0)}{x_1 - x_0}$$

$$f(x) = f(x_0) - \frac{f(x_1) - f(x_0)}{x_1 - x_0} \cdot (x_0 - x)$$

GP is responsible for computing the current values of the data elements GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE. The current value of GP\_ATTITUDE is expressed by the following formula:



$$GP\_ATTITUDE_t = GP\_ATTITUDE_{t-2} + \int_{t-2}^t (GP\_ATTITUDE)\dot{dt}$$

where

$$GP\_ATTITUDE = GP\_ROTATION \times GP\_ATTITUDE$$

The current value of GP\_VELOCITY is expressed by the following formula:

$$GP\_VELOCITY_t = GP\_VELOCITY_{t-2} + \int_{t-2}^t (GP\_VELOCITY)\dot{dt}$$

where

$$GP\_VELOCITY = GP\_ROTATION \times GP\_VELOCITY + ACCEL + (K\_MATRIX \times (TDLR\_VELOCITY - GP\_VELOCITY))$$

where ACCEL is a 3x1 matrix specified as:

do i = 1 to 3

$$ACCEL[i] = GRAVITY \cdot GP\_ATTITUDE[i,3] + A\_ACCELERATION[i]$$

end do

The current value of GP\_ALTITUDE is expressed by the following formula:

$$GP\_ALTITUDE_t = GP\_ALTITUDE_{t-2} + \int_{t-2}^t (GP\_ALTITUDE)\dot{dt}$$

where

$$GP\_ALTITUDE = (-GP\_ATTITUDE[1,3] \cdot GP\_VELOCITY[1] + -GP\_ATTITUDE[2,3] \cdot GP\_VELOCITY[2] + -GP\_ATTITUDE[3,3] \cdot GP\_VELOCITY[3]) + K\_ALT \cdot (AR\_ALTITUDE - GP\_ALTITUDE)$$

Notice that the formula for computing the rate of change of GP\_ALTITUDE contains references to both GP\_ATTITUDE and GP\_VELOCITY. Because of these references the solution for computing the current values of these data elements must solve these three equations simultaneously -- a system of equations.

The solution to computing this system of equations proposed in Pluto is based on the fourth-order Runge-Kutta (RK) method. Operating on a single equation, the RK method computes four estimates for the incremental value and then uses a weighted average of the four estimates to compute the result. The solution employs the RK method to the three equations simultaneously by computing the first estimate for each equation first, then computing the second estimate for each equation second, and so on, finally performing the weighted averages. In this manner, the intermediately computed estimates are available to the "downstream" computations of other further estimates as necessary.

The typical application of the RK method involves computing the new value of a function given the current value of the function and a step size. The first estimate,  $k_1$ , of the incremental value is determined by multiplying the rate-of-change of the function at the current value by the step size. The second estimate,  $k_2$ , of the incremental value is determined by multiplying the rate-of-change of the function at the midpoint of the line connecting the known value and the estimated new value determined by  $k_1$ . The straight forward application of the RK method to GCS is to treat the value for the current frame as the "new value," the value at the previous frame as the "old value," and the step size as DELTA\_T.

But, there is a problem implementing this straight forward approach. In order to determine the rate-of-change, that is the first derivative of the function, for a specific instance in time, it is necessary to know specific sensor measurements at that point in time. The equations for rate-of-

change presented above depict the necessary sensor measurements. So, if DELTA\_T is chosen as the step-size, it is not possible to compute the rate-of-change at the "midpoint" of the line connecting GP\_VELOCITY<sub>t-1</sub> and the first estimate of GP\_VELOCITY<sub>t</sub>

Likewise in the case of the computation of GP\_ALTITUDE. In order for the necessary sensor information to be available for computations involving the "midpoint," the "midpoint" must coincide with the execution of the sensor processing subframe. Thus, if a step-size of 2 \* DELTA\_T is chosen, the "midpoint" falls on a frame boundary, and the necessary sensor information is available. The Pluto design implements the RK method with 2 \* DELTA\_T as the step-size, the data element value computed two frames previously as the "old value," and the data element current value as the "new value."

P-Spec 2.2 GP, presented in B.4, contains a detailed description of the application of the modified RK method for computing the current values of GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE.

The Control Law Processing Subframe provides the guidance and control subsystem with an interface to the vehicle's locomotive resources, namely the axial engines, the roll engines and the parachute. The vehicle's locomotive resources provide Pluto with the means of maneuvering the lander. Control Law Processing Subframe processing is decomposed into several distinct tasks.

The AECLP process is responsible for generating the appropriate axial engine commands. AECLP processes data originating from the Sensor Processing Subframe and Guidance Processing Subframe processing and computes the axial engine commands. DFD 3.2 represents the role of AECLP in the Control Law Processing Subframe and P-Spec 3.2 specifies the AECLP functional processing.

The development specifications present the following formula as a solution for determining a value for the data element TE\_LIMIT, note that the following data elements are abbreviated GRAVITY as GRAV, GP\_ATTITUDE(1,3,0) as ATT, VELOCITY\_ERROR as VEL\_ERROR, and OMEGA as  $\Omega$ :

$$\frac{d}{dt}(TE\_LIMIT) + \Omega \cdot TE\_LIMIT =$$

$$-GAX \cdot \left( \overset{GA}{\ddot{\chi}_v} + GRAV \cdot ATT \right) + GVE \cdot VEL\_ERROR + GVEI \cdot TE\_INTEGRAL$$

rewriting the equation yields:

$$\frac{d}{dt}(TE\_LIMIT) + \Omega \cdot TE\_LIMIT =$$

$$GA \cdot (-GAX \cdot \left( \ddot{\chi}_v + GRAV \cdot ATT \right) + GVE \cdot VEL\_ERROR + GVEI \cdot TE\_INTEGRAL)$$

Letting  $Q =$

$$GA \cdot (-GAX \cdot \left( \ddot{\chi}_v + GRAV \cdot ATT \right) + GVE \cdot VEL\_ERROR + GVEI \cdot TE\_INTEGRAL)$$

gives:

$$\frac{d}{dt}(TE\_LIMIT) + \Omega \cdot TE\_LIMIT = Q$$

which happens to be a first order linear equation. Multiplying each term by the integrating factor:

$$e^{\int \Omega dt} \cdot \frac{d}{dt}(TE\_LIMIT) + e^{\int \Omega dt} \cdot \Omega \cdot TE\_LIMIT = e^{\int \Omega dt} \cdot Q$$

simplify:

$$\frac{d}{dt} \left( TE\_LIMIT \cdot e^{\int \Omega dt} \right) = e^{\int \Omega dt} \cdot Q$$

integrating both terms:

$$TE\_LIMIT \cdot e^{\int \Omega dt} = \int \left( Q \cdot e^{\int \Omega dt} \right) dt$$

$$TE\_LIMIT = e^{-\int \Omega dt} \cdot Q \cdot \int e^{\int \Omega dt} dt$$

$$e^{\int \Omega dt} = e^{\Omega t}$$

$$\text{let } u = \Omega t \text{ and } du = \Omega dt$$

$$TE\_LIMIT = e^{-\Omega t} \cdot Q \cdot \int e^{\Omega t} dt$$

$$\int e^{\Omega t} dt = \frac{1}{\Omega} \cdot \int (e^{\Omega t} \cdot Q) dt$$

$$= \frac{1}{\Omega} \cdot \int e^u du$$

$$= \frac{1}{\Omega} \cdot e^u + C$$

$$= \frac{1}{\Omega} \cdot e^{\Omega t} + C$$

$$TE\_LIMIT = \frac{Q}{\Omega} + C \cdot Q \cdot e^{-\Omega t}$$

Solving for  $C$  based on the following initial conditions:

$$t = t_0 = 0$$

$$TE\_LIMIT = TE\_LIMIT_0 \quad \text{where } TE\_LIMIT_0 \text{ is the previously computed } TE\_LIMIT$$

$$C = \frac{\left( TE\_LIMIT_0 - \frac{Q}{\Omega} \right)}{Q}$$

The final result is:

$$TE\_LIMIT = \frac{Q}{\Omega} + \left( TE\_LIMIT_0 - \frac{Q}{\Omega} \right) \cdot e^{-\Omega t}$$

where  $Q =$

$$GA \cdot \left( -GAX \cdot \left( \ddot{X}_v + GRAV \cdot ATT \right) + GVE \cdot VEL\_ERROR + GVEI \cdot TE\_INTEGRAL \right)$$

The CRCP process is responsible for determining whether or not to release the parachute. CRCP determines to release the parachute based on the current state of the parachute and the axial engine temperature. DFD 3.3 represents the role of CRCP in the Control Law Processing Subframe and P-Spec 3.2 specifies the CRCP functional processing.

The RECLP process is responsible for generating the appropriate roll engine commands. RECLP processes data originating from the Sensor Processing Subframe and Guidance Processing Subframe processing and computes the roll engine commands. DFD 3.4 represents the role of RECLP in the Control Law Processing Subframe and P-Spec 3.4 specifies the RECLP functional processing.

## **B.2.4 Process scheduling**

The Pluto software design specification contains no explicit process scheduling needs.

## **B.2.5 Data Dictionary**

The data dictionary contains formal definitions of all the data items presented in the data-flow and control-flow diagrams. Teamwork provides an integrated data dictionary for use with the SA/RT software development tools. A copy of Pluto's data dictionary as stored in Teamwork may be found in B.4.

## **B.2.6 Derived Requirements**

According to DO-178B (ref. B.1) derived requirements are those requirements which are not directly traceable to higher level requirements. The GCS Software Development Specification goes to great length in presenting the software specifications for a GCS implementation. As such, it has not been necessary for the Pluto software design specification to create any derived requirements.

## **B.3 References**

- B.1 RTCA Special Committee 152. Software Considerations in Airborne Systems and Equipment Certification. Technical Report RTCA/DO-178B, Requirements and Technical Concepts for Aviation, December 1992.
- B.2 George B. Finelli. Results of software error-data experiments. In AIAA/AHS/ASEE Aircraft Design, Systems and Operations Conference, Atlanta, GA, September 1988.
- B.3 Withers, B. Edward; and Becher, Bernice: *Guidance and Control Software Development Specification*. version 2.3 with formal modifications through 2.3-3, 1994
- B.4 *Teamwork/SA Teamwork/RT User's Guide*. Release 4.0, Cadre Technologies Inc., 1990
- B.5 DeMarco, Tom: *Structured Analysis and System Specification*. Prentice-Hall Inc., 1979.
- B.6 Hatley, Derek J.; and Imtiaz A. Pirbhai: *Strategies for Real-Time System Specification*. Dorset House Publishing Co., 1988
- B.7 Page-Jones, Meilir: *The Practical Guide to Structured Systems Design*. Yourdon Press, 1980

## **B.4 Teamwork Design**

Context-Diagram;22  
PLUTO

\* in \*

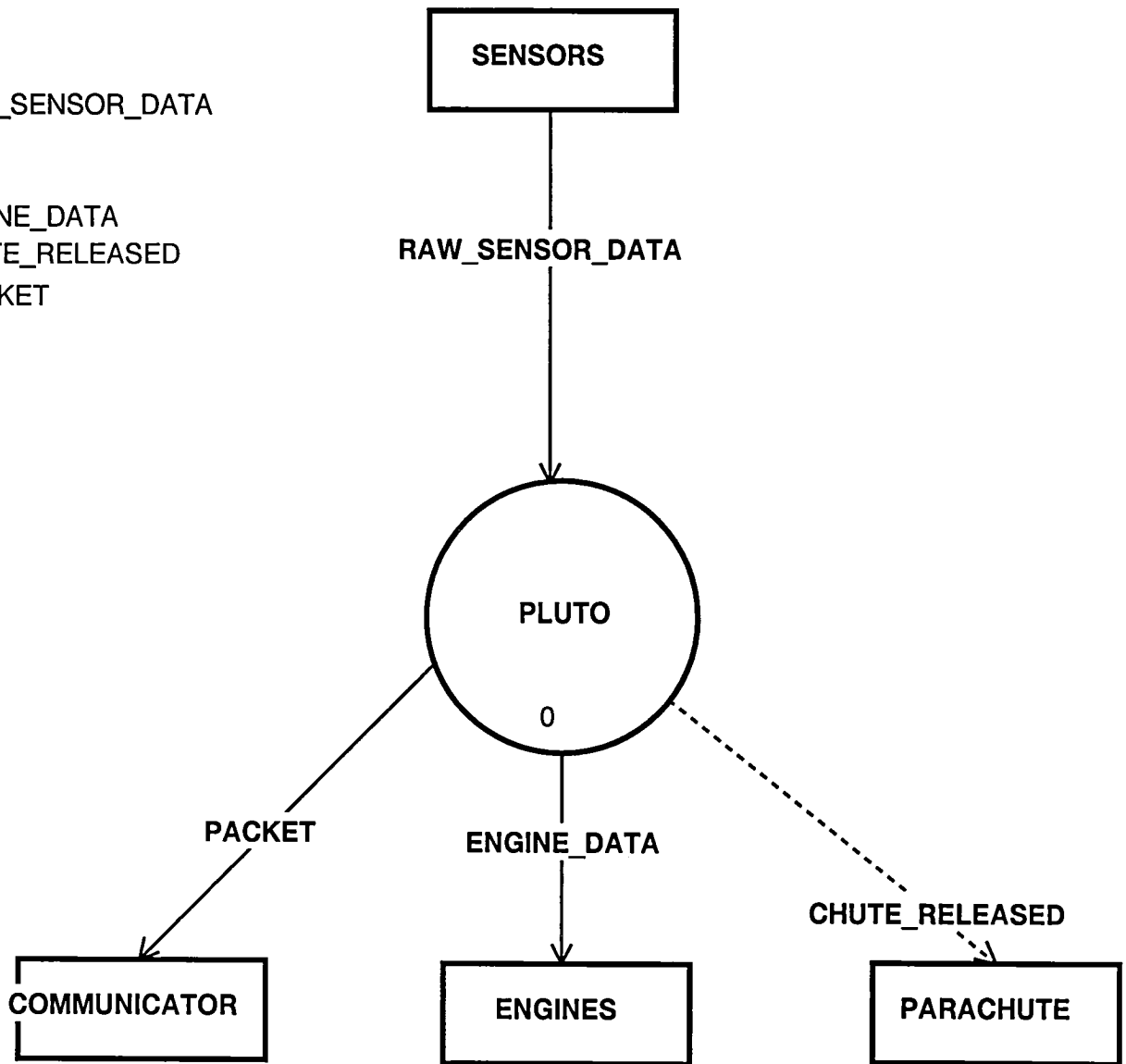
RAW\_SENSOR\_DATA

\* out \*

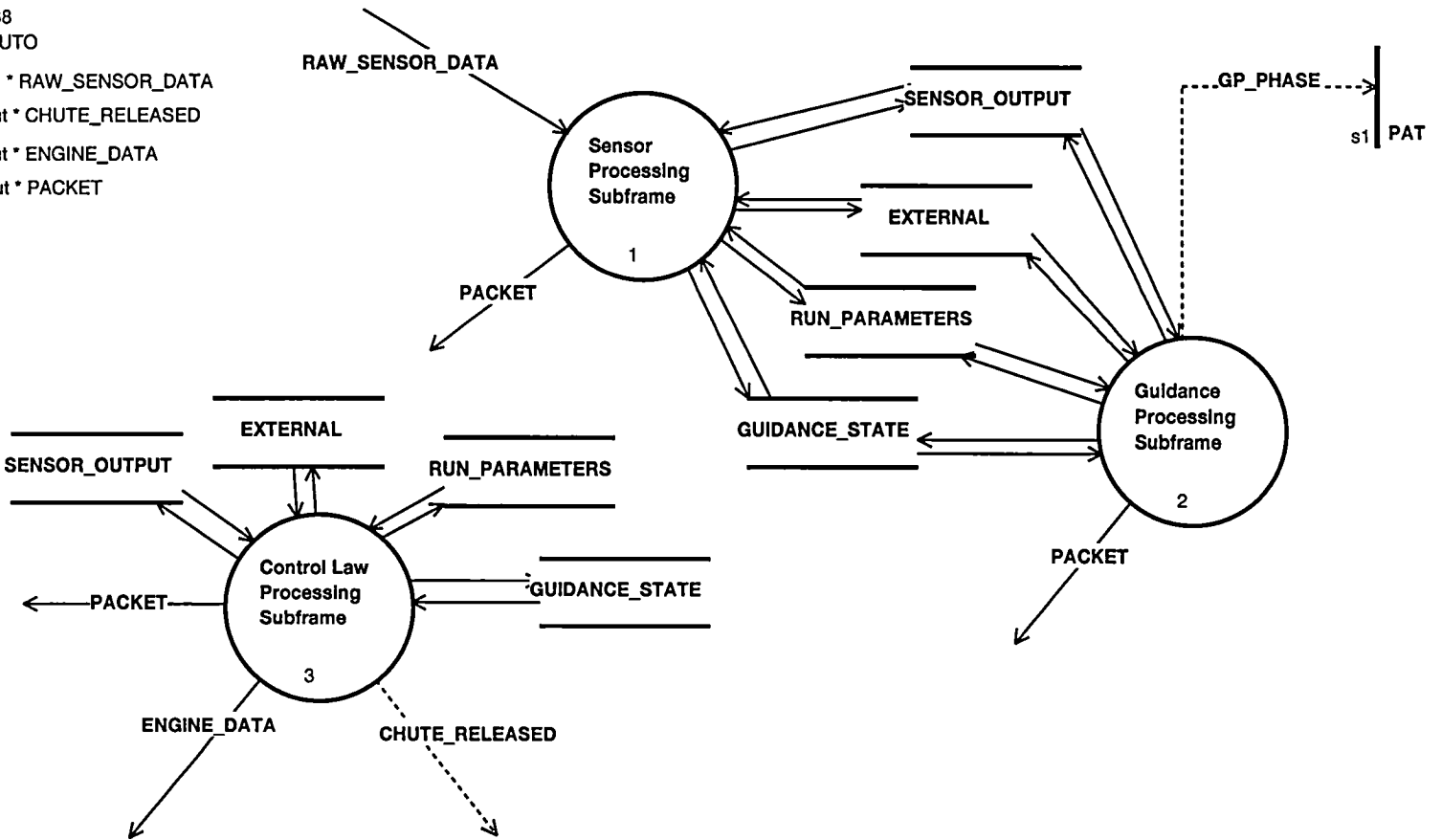
ENGINE\_DATA

CHUTE\_RELEASED

PACKET



0;38  
 PLUTO  
 \* in \* RAW\_SENSOR\_DATA  
 \* out \* CHUTE\_RELEASED  
 \* out \* ENGINE\_DATA  
 \* out \* PACKET



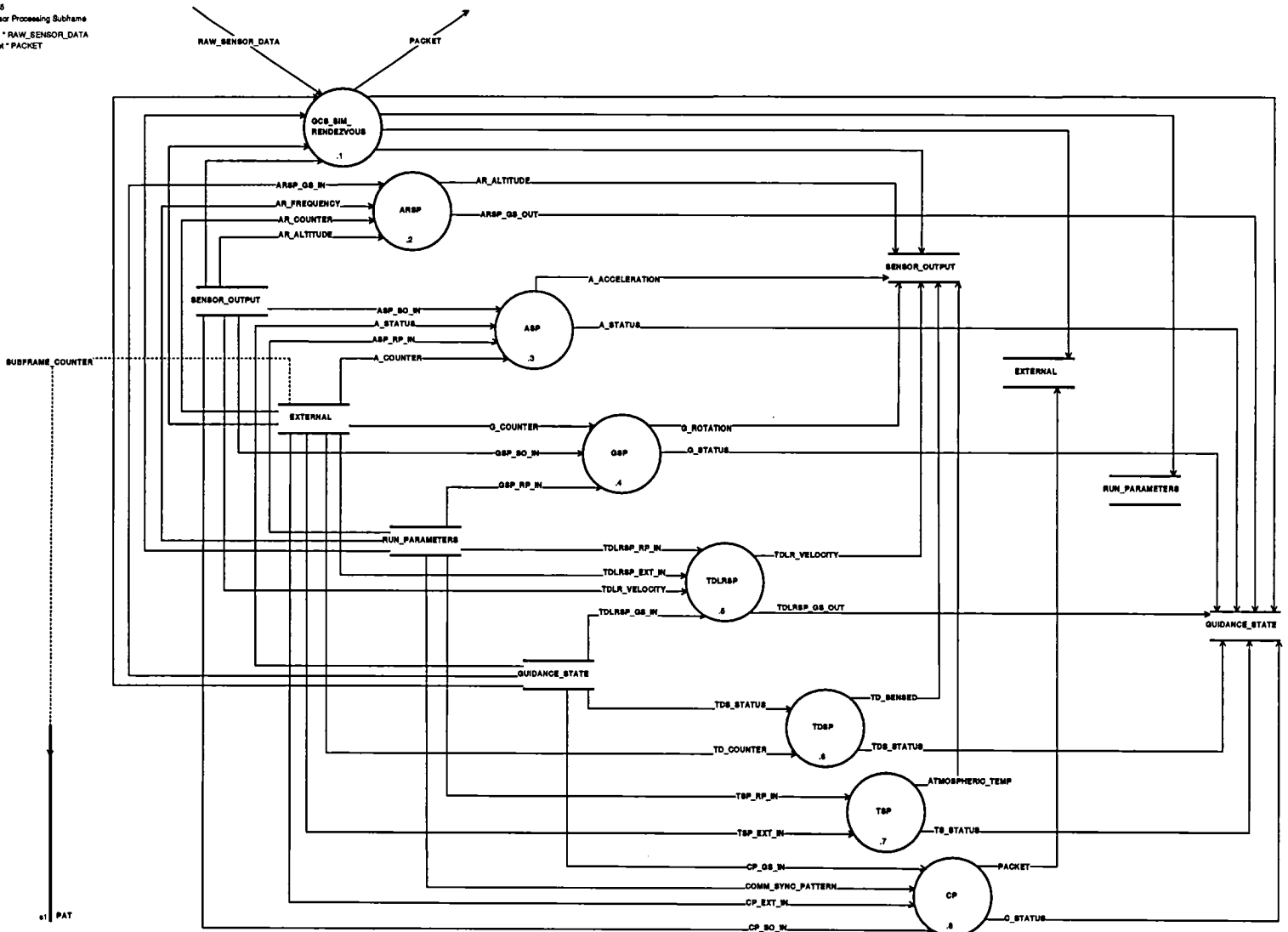


0-s1;23  
PLUTO PAT

<b>GP_PHASE</b>	<b>"Sensor Processing Subframe"</b>	<b>"Guidance Processing Subframe"</b>	<b>"Control Law Processing Subframe"</b>
<b>"5"</b>	<b>0</b>	<b>0</b>	<b>0</b>
<b>Others</b>	<b>1</b>	<b>2</b>	<b>3</b>



1:115  
 Sensor Processing Subframe  
 \* in \* RAW\_SENSOR\_DATA  
 \* out \* PACKET



1-s1,22  
PAT - Sensor Processing Subframe

SUBFRAME_COUNTER	"GCS_SIM_RENDEZVOUS"	"ARSP"	"ASP"	"GSP"	"TDLRSP"	"TDSP"	"TSP"	"CP"
"1"	1	3	3	3	3	3	2	4

**NAME:**

1.1;5

**TITLE:**

GCS\_SIM\_RENDEZVOUS

**INPUT/OUTPUT:**

RAW\_SENSOR\_DATA: data\_in

GUIDANCE\_STATE : data\_in

RUN\_PARAMETERS : data\_in

EXTERNAL : data\_in

SENSOR\_OUTPUT : data\_in

SENSOR\_OUTPUT : data\_out

GUIDANCE\_STATE : data\_out

RUN\_PARAMETERS : data\_out

PACKET: data\_out

EXTERNAL : data\_out

**BODY:**

BEGIN P-Spec

GCS\_SIM\_RENDEZVOUS provides the interface to the vehicle. This module is provided by the systems group.

Bubbles 1.1, 2.1, 3.1 and the associated P-Specs represent a single process.

END P-Spec



**NAME:**

1.2;31

**TITLE:**

ARSP

**INPUT/OUTPUT:**

AR\_ALTITUDE : data\_in

AR\_COUNTER : data\_in

AR\_FREQUENCY : data\_in

AR\_STATUS : data\_in

K\_ALT : data\_in

AR\_ALTITUDE : data\_out

AR\_STATUS : data\_out

K\_ALT : data\_out

**BODY:**

BEGIN P\_SPEC

```

(*****
 * ARSP -- Altimeter Radar Sensor Processing
 *
 * ARSP processing is responsible for:
 * 1) maintaining the history of the altitude and altimeter sensor data
 *    elements,
 * 2) determining the operational status of the altimeter radar sensor, and
 * 3) Reporting the current altitude.
*****)

(*****
 * 1) Maintain the history of the altitude and the sensor status by
 * "rotating variables." Each of the three data elements AR_ALTITUDE,
 * AR_STATUS, and K_ALT are defined as five element arrays. The first
 * element of each array, element zero, holds the most recently computed
 * value. The last element of each array, element four, holds the
 * oldest maintained value. In shifting the values stored in these
 * data elements, a multi-frame history is maintained.
*****)

AR_ALTITUDE[4] := AR_ALTITUDE[3]
AR_ALTITUDE[3] := AR_ALTITUDE[2]
AR_ALTITUDE[2] := AR_ALTITUDE[1]
AR_ALTITUDE[1] := AR_ALTITUDE[0]

AR_STATUS[4] := AR_STATUS[3]
AR_STATUS[3] := AR_STATUS[2]
AR_STATUS[2] := AR_STATUS[1]
AR_STATUS[1] := AR_STATUS[0]

```

```

K_ALT[4] := K_ALT[3]
K_ALT[3] := K_ALT[2]
K_ALT[2] := K_ALT[1]
K_ALT[1] := K_ALT[0]

```

```

(*****
* 2) The data element AR_STATUS represents the operational status
* of the altimeter radar sensor. If an echo has been received,
* then the sensor status is deemed "healthy" (value 0). If an
* echo has not been received, the sensor status is reported as
* "failed" (value 1). The GP process references the data element
* K_ALT to determine which method was used to determine the
* current altitude. If either method A or B, as described below, is
* employed to compute the current altitude, the value for K_ALT is
* reported as "1." If method C is used to compute the altitude,
* the value for K_ALT is reported as "0."
*
* 3) There are three methods for determining the altitude.
*
* A) If an echo has been received, then the altitude will be computed
* from the sensor measurement.
*
* B) If an echo has not been received, and all four of the maintained
* altitude sensor history statuses are "heathly," then the value
* for the current altitude is estimated by fitting a third-order
* polynomial to the altitude history data values (see description
* below).
*
* C) If an echo has not been received, and at least one of the
* maintained altitude sensor history statuses is "failed," then
* the value for the the current altitude is estimated by reporting
* the mostly recently reported value for the altitude.
*****)

```

```

(*****
* If an echo has been recieved, then the lower order fifteen bits of
* AR_COUNTER contain the raw sensor measurement, and the upper bit of
* AR_COUNTER will be clear (ie: 0). When an echo has not been received,
* the AR_COUNTER will contain 16 set bits (ie: 0xFFFF).
*
* It is known that this design will be implemented on VAX/VMS in FORTRAN.
* The data type of AR_COUNTER is integer*2 and the valid value range
* is specified as [-1, 32767]. VAX/VMS uses twos complement method for
* representing negative values. Thus, when an echo has not been recieved,
* the AR_COUNTER will contain the value of -1. Similarly, when an echo
* has been received, AR_COUNTER will contain a non-negative value.
*****)

```

```

if (an echo has been recieved) then [1]

```

```

(** report the sensor status as healthy **)

```

```

AR_STATUS[0] := 0 (* healthy *)
K_ALT[0] := 1 (* method A *)

```

```

(** A) compute the altitude from the sensor measurement **)

```



```

    AR_ALTITUDE := (AR_COUNTER * 3x10^8) / (2 * AR_FREQUENCY)

else      (* no echo received *)                                {1}

(** report the sensor status as failed **)

    AR_STATUS[0]      := 1    (* failed *)

(** if at least one of the history sensor status is "failed" **)

    if (AR_STATUS[1] = 1 OR AR_STATUS[2] = 1 OR                {2}
        AR_STATUS[3] = 1 OR AR_STATUS[4] = 1) then

        K_ALT[0]      := 0    (* method C *)

(** C) return previously computed value **)

(** range check the altitude ****)

    if (AR_ALTITUDE[1] < 0)                                    {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "ARSP ARSP", FRAME_COUNTER,
                      "AR_ALTITUDE", AR_ALTITUDE[1])

    else if (AR_ALTITUDE[1] > 2000)                             {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "ARSP ARSP", FRAME_COUNTER,
                      "AR_ALTITUDE", AR_ALTITUDE[1])

    end if                                                      {3}

    AR_ALTITUDE[0] := AR_ALTITUDE[1]    (* this should already exist *)

else      (* all sensor status histories are "healthy" *)      {2}

(** B) extrapolate the altitude **)

    K_ALT[0] := 1    (* method B *)

(** range check the altitude ****)

    if (AR_ALTITUDE[1] < 0)                                    {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "ARSP ARSP", FRAME_COUNTER,
                      "AR_ALTITUDE", AR_ALTITUDE)

    else if (AR_ALTITUDE[1] > 2000)                             {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "ARSP ARSP", FRAME_COUNTER,
                      "AR_ALTITUDE", AR_ALTITUDE)

    end if                                                      {3}

    if (AR_ALTITUDE[2] < 0)                                    {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "ARSP ARSP", FRAME_COUNTER,
                      "AR_ALTITUDE", AR_ALTITUDE)

```

```
else if (AR_ALTITUDE[2] > 2000) {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "ARSP ARSP", FRAME_COUNTER,
               "AR_ALTITUDE", AR_ALTITUDE)
end if {3}

if (AR_ALTITUDE[3] < 0) {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "ARSP ARSP", FRAME_COUNTER,
               "AR_ALTITUDE", AR_ALTITUDE)

else if (AR_ALTITUDE[3] > 2000) {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "ARSP ARSP", FRAME_COUNTER,
               "AR_ALTITUDE", AR_ALTITUDE)
end if {3}

if (AR_ALTITUDE[4] < 0) {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "ARSP ARSP", FRAME_COUNTER,
               "AR_ALTITUDE", AR_ALTITUDE)

else if (AR_ALTITUDE[4] > 2000) {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "ARSP ARSP", FRAME_COUNTER,
               "AR_ALTITUDE", AR_ALTITUDE)
end if {3}

AR_ALTITUDE[0] := 4*AR_ALTITUDE[1] - 6*AR_ALTITUDE[2] +
                 4*AR_ALTITUDE[3] - AR_ALTITUDE[4]

end if {2}

end if {1}

END P_SPEC
```



**NAME:**

1.3;36

**TITLE:**

ASP

**INPUT/OUTPUT:****A\_ACCELERATION : data\_in****A\_BIAS : data\_in****A\_COUNTER : data\_in****A\_GAIN\_0 : data\_in****A\_SCALE : data\_in****A\_STATUS : data\_in****ALPHA\_MATRIX : data\_in****ATMOSPHERIC\_TEMP : data\_in****G1 : data\_in****G2 : data\_in****A\_ACCELERATION : data\_out****A\_STATUS : data\_out****BODY:**

BEGIN P\_SPEC

```

(*****
 * ASP -- Accelerometer Sensor Processing
 *
 * ASP processing is responsible for:
 * 1) maintaining the history of the accelerations and accelerometer
 *    sensor statuses,
 * 2) determining the operational status of the accelerometer sensors, and
 * 3) Reporting the current vehicle accelerations along each of the
 *    vehicle's three axes.
 *****)

(*****
 * 1) Maintain the history of the vehicle accelerations and
 * accelerometer sensor status by "rotating variables."
 * Both of the data elements A_ACCELERATION and A_STATUS are defined as
 * two dimensional arrays. The first dimension of each array represents
 * a vehicle axis: x-axis (1), y-axis (2), z-axis (3). The second
 * dimension of each data element represents a history. For
 * A_ACCELERATION, the history is five deep and for A_STATUS the history
 * is four deep. The first element of each history, element zero, holds
 * the most recently computed value. The last element of each history,
 * element four or three respectively, holds the oldest maintained value.
 *****)

```

\* In shifting the values stored in these data elements, a multi-frame  
 \* history is maintained.

\*\*\*\*\*)

```
A_ACCELERATION[1, 4] := A_ACCELERATION[1, 3]
A_ACCELERATION[1, 3] := A_ACCELERATION[1, 2]
A_ACCELERATION[1, 2] := A_ACCELERATION[1, 1]
A_ACCELERATION[1, 1] := A_ACCELERATION[1, 0]
```

```
A_ACCELERATION[2, 4] := A_ACCELERATION[2, 3]
A_ACCELERATION[2, 3] := A_ACCELERATION[2, 2]
A_ACCELERATION[2, 2] := A_ACCELERATION[2, 1]
A_ACCELERATION[2, 1] := A_ACCELERATION[2, 0]
```

```
A_ACCELERATION[3, 4] := A_ACCELERATION[3, 3]
A_ACCELERATION[3, 3] := A_ACCELERATION[3, 2]
A_ACCELERATION[3, 2] := A_ACCELERATION[3, 1]
A_ACCELERATION[3, 1] := A_ACCELERATION[3, 0]
```

```
A_STATUS[1, 3] := A_STATUS[1, 2]
A_STATUS[1, 2] := A_STATUS[1, 1]
A_STATUS[1, 1] := A_STATUS[1, 0]
```

```
A_STATUS[2, 3] := A_STATUS[2, 2]
A_STATUS[2, 2] := A_STATUS[2, 1]
A_STATUS[2, 1] := A_STATUS[2, 0]
```

```
A_STATUS[3, 3] := A_STATUS[3, 2]
A_STATUS[3, 2] := A_STATUS[3, 1]
A_STATUS[3, 1] := A_STATUS[3, 0]
```

\*\*\*\*\*)

\* 2) and 3), determine the operational status and the vehicle  
 \* accelerations for each axis.

\*\*\*\*\*)

(\*\*\* range check the atmospheric temperature \*\*\*)

```
if (ATMOSPHERIC_TEMP < -200) then                                [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "ASP ASP", FRAME_COUNTER,
               "ATMOSPHERIC_TEMP", ATMOSPHERIC_TEMP)
```

```
else if (ATMOSPHERIC_TEMP > 25) then                            [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "ASP ASP", FRAME_COUNTER,
               "ATMOSPHERIC_TEMP", ATMOSPHERIC_TEMP)
```

```
end if                                                            [1]
```

(\*\*\* compute the preliminary value for the accelerations \*\*\*)

Let accel\_m be a 3x1 matrix

compute each element (i := 1 to 3) of accel\_m as follows:

```
accel_m[i] := A_BIAS[i] + a_gain * A_COUNTER[i]
```

where

```
a_gain := A_GAIN_0[i] + (G1 * ATMOSPHERIC_TEMP) +
          (G2 * ATMOSPHERIC_TEMP^2)
```

viewing the "current" elements of A\_ACCELERATION as a 3x1 matrix,

```
-
| A_ACCELERATION[1, 0] |
| A_ACCELERATION[2, 0] |
| A_ACCELERATION[3, 0] |
-
```

the preliminary values for A\_ACCELERATION are computed from the matrix multiplication:

```
A_ACCELERATION := ALPHA_MATRIX X accel_m
```

```
(*****
* Determine whether or not the preliminary values for the
* accelerations are reasonable. The preliminary value for an
* acceleration is deemed reasonable: 1) if it differs from the mean
* of the previous three measurements by not more than A_SCALE
* standard deviations; 2) when any of the three accelerometer
* history statuses is "unhealthy" (value 1). If a preliminary
* acceleration value is found to be reasonable,
* then it is reported as the acceleration for it's axis. If a
* preliminary value is not found to be reasonable, then the
* mean of the previous three measurements is reported as the
* acceleration for that axis.
*
* The current value for the sensor status is determined directly
* from the reasonableness of the value of the preliminary
* acceleration. If the preliminary acceleration is reasonable, the
* sensor status is deemed "healthy " (value 0). If the preliminary
* acceleration is not reasonable, the sensor status is deemed
* "unhealthy."
*****)
```

```
do for each axis (i := 1 to 3)
```

```
A_STATUS[i, 0] := 0;      (* set sensor status to "healthy" *)
```

```
if (A_STATUS[i, 1] = 0) AND A_STATUS[i, 2] = 0 AND      {1}
    A_STATUS[i, 3] = 0) then
```

```
if ((A_ACCELERATION[i,1] <> A_ACCELERATION[i,2]) OR    {2}
    (A_ACCELERATION[i,1] <> A_ACCELERATION[i,3])) then
```

```
(** compute the mean of the previous three values **)
```

```
(** range check the acceleration values ***)
```

```
if (A_ACCELERATION[i, 1] < -20) then                    {3}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
```

```

        "ASP ASP", FRAME_COUNTER,
        "A_ACCELERATION", A_ACCELERATION[i, 1])

    else if (A_ACCELERATION[i, 1] > 5) then {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "ASP ASP", FRAME_COUNTER,
            "A_ACCELERATION", A_ACCELERATION[i, 1])
    end if {3}

    if (A_ACCELERATION[i, 2] < -20) then {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
            "ASP ASP", FRAME_COUNTER,
            "A_ACCELERATION", A_ACCELERATION[i, 2])

    else if (A_ACCELERATION[i, 2] > 5) then {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "ASP ASP", FRAME_COUNTER,
            "A_ACCELERATION", A_ACCELERATION[i, 2])
    end if {3}

    if (A_ACCELERATION[i, 3] < -20) then {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
            "ASP ASP", FRAME_COUNTER,
            "A_ACCELERATION", A_ACCELERATION[i, 3])

    else if (A_ACCELERATION[i, 3] > 5) then {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "ASP ASP", FRAME_COUNTER,
            "A_ACCELERATION", A_ACCELERATION[i, 3])
    end if {3}

    mean := ((A_ACCELERATION[i, 1] + A_ACCELERATION[i, 2] +
        A_ACCELERATION[i, 3]) / 3

(***) compute the standard deviation (***)

    temp := ((A_ACCELERATION[i, 1] - mean)^2 +
        (A_ACCELERATION[i, 2] - mean)^2 +
        (A_ACCELERATION[i, 3] - mean)^2) / 3

    sd := SQRT(temp)

    if (ABS(mean - A_ACCELERATION[i, 0]) > A_SCALE * sd) then {3}
        A_ACCELERATION[i, 0] := mean
        A_STATUS[i, 0] := 1 (* set sensor status to "unhealthy" *)
    end if {3}

end if {2}

end if {1}

end do (* for each axis *)

END P_SPECA_STATUS[i, 0] := 0; (* set sensor status to "healthy" *)

```





**NAME:**

1.4;16

**TITLE:**

GSP

**INPUT/OUTPUT:****ATMOSPHERIC\_TEMP : data\_in****G3 : data\_in****G4 : data\_in****G\_COUNTER : data\_in****G\_GAIN\_0 : data\_in****G\_OFFSET : data\_in****G\_ROTATION : data\_in****G\_ROTATION : data\_out****G\_STATUS : data\_out****BODY:**

BEGIN P\_SPEC

```

(*****
 * GSP -- Gyroscopy Sensor Processing
 *
 * GSP processing is responsible for:
 * 1) maintaining the history of the vehicle rotation rates,
 * 2) determining the operational status of the gyroscope sensors, and
 * 3) Reporting the current vehicle rotation rates along each of the
 *    vehicle's three axes.
 *****)

(*****
 * 1) Maintain the history of the vehicle rotation rates by "rotating
 * variables." The data element G_ROTATION is defined as a two
 * dimensional array. The first dimension represents a vehicle axis:
 * x-axis (1), y-axis (2), and z-axis (3). The second dimension
 * represents a five deep history. The first element of the history (0),
 * holds the most recently computed value. The last element of the
 * history (4), holds the oldest maintained value. In shifting the
 * values stored in these data elements, a multi-frame history is
 * maintained.
 *****)

G_ROTATION[1, 4] := G_ROTATION[1, 3]
G_ROTATION[1, 3] := G_ROTATION[1, 2]
G_ROTATION[1, 2] := G_ROTATION[1, 1]
G_ROTATION[1, 1] := G_ROTATION[1, 0]

```

```
G_ROTATION[2, 4] := G_ROTATION[2, 3]
G_ROTATION[2, 3] := G_ROTATION[2, 2]
G_ROTATION[2, 2] := G_ROTATION[2, 1]
G_ROTATION[2, 1] := G_ROTATION[2, 0]
```

```
G_ROTATION[3, 4] := G_ROTATION[3, 3]
G_ROTATION[3, 3] := G_ROTATION[3, 2]
G_ROTATION[3, 2] := G_ROTATION[3, 1]
G_ROTATION[3, 1] := G_ROTATION[3, 0]
```

```
(*****
 * 2) determining the operational status of the gyroscope sensors.
 * The operational status of the gyroscope sensors is always reported
 * as "healthy" (value 0).
 *****)
```

```
G_STATUS      := 0
```

```
(*****
 * 3) Reporting the current vehicle rotation rates along each of the
 * vehicle's three axes.
 *****)
```

```
(** range check the atmospheric temperature **)
```

```
if (ATMOSPHERIC_TEMP < -200) then
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "GSP GSP", FRAME_COUNTER,
               "ATMOSPHERIC_TEMP", ATMOSPHERIC_TEMP)
else if (ATMOSPHERIC_TEMP > 25) then
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "GSP GSP", FRAME_COUNTER,
               "ATMOSPHERIC_TEMP", ATMOSPHERIC_TEMP)
end if
```

```
(*****
 * The raw sensor data stored in G_COUNTER represents the vehicle rate
 * of rotation about a specific axis. The sensor data is
 * stored in a modified sign magnitude format. The lower 14-bits
 * represent the magnitude of the rotation and the most significant
 * bit (bit 15) represents the sign. Bit 14 is not used. A
 * positive value of G_COUNTER indicates a positive rotation about
 * the vehicle axis consistent with a right handed coordinate system,
 * while a negative value indicates a negative rotation consistent
 * with a right handed coordinate system.
 *****)
```

```
do for each axis (i := 1 to 3)
```

```
(** convert the raw sensor ... **)
```

```
(*****
 * Convert the raw sensor data from the modified sign magnitude
 * format into an appropriate format for use by the target CPU, in
 * this case two's complement. Positive values are represented in
```

```

* the same fashion in sign magnitude and two's complement, however,
* negative sensor values must be massaged.
*
* Transfer the magnitude of the rotation from G_COUNTER to the local
* data element named counter by masking bits 14 and 15 from
* G_COUNTER. If G_COUNTER bit 15 is clear, the data element counter
* now contains the properly converted value. If G_COUNTER bit 15 is
* set, the value of data element counter must be negated.
*****)

(*****
* The symbol '&' represents a bitwise AND operation
* the notation '0xdddd' represents a hexadecimal value
*****)

    counter    := G_COUNTER[i] & 0x3FFF

    if ((G_COUNTER[i] & 0x8000) = 1)
        counter    := 0 - counter
    end if

(***) compute the vehicle rotation from the sensor data (***)

    G_ROTATION[i, 0] := G_OFFSET[i] + g_gain * counter

    where
        g_gain := G_GAIN_0[i] + (G3 * ATMOSPHERIC_TEMP) +
                    (G4 * ATMOSPHERIC_TEMP^2)

    end do      (* for each axis *)

END P_SPEC

```



**NAME:**

1.5;27

**TITLE:**

TDLRSP

**INPUT/OUTPUT:****DELTA\_T** : data\_in**FRAME\_BEAM\_UNLOCKED** : data\_in**FRAME\_COUNTER** : data\_in**K\_MATRIX** : data\_in**TDLR\_ANGLES** : data\_in**TDLR\_COUNTER** : data\_in**TDLR\_GAIN** : data\_in**TDLR\_LOCK\_TIME** : data\_in**TDLR\_OFFSET** : data\_in**TDLR\_STATE** : data\_in**TDLR\_VELOCITY** : data\_in**FRAME\_BEAM\_UNLOCKED** : data\_out**K\_MATRIX** : data\_out**TDLR\_STATE** : data\_out**TDLR\_STATUS** : data\_out**TDLR\_VELOCITY** : data\_out**BODY:**

BEGIN P\_SPEC

```
(*****
* TDLRSP -- Touch Down Landing Radar Sensor Processing
*
* TDLRSP processing is responsible for:
* 1) Maintaining the history of the vehicle velocities and the
*    velocity computation indicator,
* 2) Determining the operational status of touch down landing radar
*    sensor, and
* 3) Reporting the current vehicle velocities along each of the
*    vehicle's three axes, and
* 4) Reporting the velocity computation indicators.
*
*****)
```

```
(*****
* 1) Maintain the history of the vehicle velocities and the
*    velocity computation indicator by "rotating variables." The data
*    element TDLR_VELOCITY is defined as a two dimensional array. The
*    first dimension represents a vehicle axis: x-axis (1), y-axis
*    (2), and z-axis (3). The second dimension represents a five deep
*    history. The data element K_MATRIX is defined as a three
*    dimensional array (1..3, 1..3, 0..4). The velocity computation
*    indicators are arranged as a 3x3 matrix, represented by the first
```

```

* two dimensions of K_MATRIX. The third dimension represents a
* five deep history. The first element of the history, element
* zero, holds the most recently computed value. The last element
* of the history, element four, holds the oldest maintained value.
* In shifting the values stored in these data elements, a
* multi-frame history is maintained.
*****)

TDLR_VELOCITY[1, 4] := TDLR_VELOCITY[1, 3]
TDLR_VELOCITY[1, 3] := TDLR_VELOCITY[1, 2]
TDLR_VELOCITY[1, 2] := TDLR_VELOCITY[1, 1]
TDLR_VELOCITY[1, 1] := TDLR_VELOCITY[1, 0]

TDLR_VELOCITY[2, 4] := TDLR_VELOCITY[2, 3]
TDLR_VELOCITY[2, 3] := TDLR_VELOCITY[2, 2]
TDLR_VELOCITY[2, 2] := TDLR_VELOCITY[2, 1]
TDLR_VELOCITY[2, 1] := TDLR_VELOCITY[2, 0]

TDLR_VELOCITY[3, 4] := TDLR_VELOCITY[3, 3]
TDLR_VELOCITY[3, 3] := TDLR_VELOCITY[3, 2]
TDLR_VELOCITY[3, 2] := TDLR_VELOCITY[3, 1]
TDLR_VELOCITY[3, 1] := TDLR_VELOCITY[3, 0]

K_MATRIX[1, 1, 4] := K_MATRIX[1, 1, 3]
K_MATRIX[1, 2, 4] := K_MATRIX[1, 2, 3]
K_MATRIX[1, 3, 4] := K_MATRIX[1, 3, 3]
K_MATRIX[2, 1, 4] := K_MATRIX[2, 1, 3]
K_MATRIX[2, 2, 4] := K_MATRIX[2, 2, 3]
K_MATRIX[2, 3, 4] := K_MATRIX[2, 3, 3]
K_MATRIX[3, 1, 4] := K_MATRIX[3, 1, 3]
K_MATRIX[3, 2, 4] := K_MATRIX[3, 2, 3]
K_MATRIX[3, 3, 4] := K_MATRIX[3, 3, 3]

K_MATRIX[1, 1, 3] := K_MATRIX[1, 1, 2]
K_MATRIX[1, 2, 3] := K_MATRIX[1, 2, 2]
K_MATRIX[1, 3, 3] := K_MATRIX[1, 3, 2]
K_MATRIX[2, 1, 3] := K_MATRIX[2, 1, 2]
K_MATRIX[2, 2, 3] := K_MATRIX[2, 2, 2]
K_MATRIX[2, 3, 3] := K_MATRIX[2, 3, 2]
K_MATRIX[3, 1, 3] := K_MATRIX[3, 1, 2]
K_MATRIX[3, 2, 3] := K_MATRIX[3, 2, 2]
K_MATRIX[3, 3, 3] := K_MATRIX[3, 3, 2]

K_MATRIX[1, 1, 2] := K_MATRIX[1, 1, 1]
K_MATRIX[1, 2, 2] := K_MATRIX[1, 2, 1]
K_MATRIX[1, 3, 2] := K_MATRIX[1, 3, 1]
K_MATRIX[2, 1, 2] := K_MATRIX[2, 1, 1]
K_MATRIX[2, 2, 2] := K_MATRIX[2, 2, 1]
K_MATRIX[2, 3, 2] := K_MATRIX[2, 3, 1]
K_MATRIX[3, 1, 2] := K_MATRIX[3, 1, 1]
K_MATRIX[3, 2, 2] := K_MATRIX[3, 2, 1]
K_MATRIX[3, 3, 2] := K_MATRIX[3, 3, 1]

K_MATRIX[1, 1, 1] := K_MATRIX[1, 1, 0]
K_MATRIX[1, 2, 1] := K_MATRIX[1, 2, 0]
K_MATRIX[1, 3, 1] := K_MATRIX[1, 3, 0]

```

```
K_MATRIX[2, 1, 1] := K_MATRIX[2, 1, 0]
K_MATRIX[2, 2, 1] := K_MATRIX[2, 2, 0]
K_MATRIX[2, 3, 1] := K_MATRIX[2, 3, 0]
K_MATRIX[3, 1, 1] := K_MATRIX[3, 1, 0]
K_MATRIX[3, 2, 1] := K_MATRIX[3, 2, 0]
K_MATRIX[3, 3, 1] := K_MATRIX[3, 3, 0]
```

```
(*****
* 2) Determine the operational status of touch down landing radar
* sensor.
*
* The operational status of the TDLR sensor is always reported
* as "healthy" (value 0).
*****)
```

```
TDLR_STATUS[1] := 0
TDLR_STATUS[2] := 0
TDLR_STATUS[3] := 0
TDLR_STATUS[4] := 0
```

```
(*****
* 3) Reporting the current vehicle velocities along each of the
* vehicle's three axes and reporting the velocity computation
* indicators.
*****)
```

```
(*****
* 3A) Determine the state of the four radar beams.
*
* The data element TDLR_STATE contains the state of the radar
* beams.
*
* Valid radar beam states are "locked" (value 1) and "unlocked"
* (value 0). The present state of a radar beam is determined from
* the current value of the sensor data and the previous state of
* the radar beam. A sensor measurement of zero indicates that the
* radar beam echo was not received and the radar beam is considered
* to be "unlocked." A non-zero sensor measurement indicates that a
* radar beam echo was received, but does not imply a radar beam
* state of "locked." Because, once a radar beam is declared
* "unlocked," it is rendered unusable (remains "unlocked"
* regardless of the sensor data value) for a specified period of
* time. This waiting period must be implemented in the software.
*
* A beam is deemed "locked" when 1) the current sensor value
* contains a non-zero value and the beam's previous state was
* "locked"; or 2) the current sensor value contains a non-zero
* value and the beam's previous state was "unlocked" and the
* elapsed time since the beam was determined "unlocked" is greater
* than or equal to the sensor recovery period.
*
* The data element TDLR_LOCK_TIME specifies the unlocked sensor
* recovery (waiting) period. The data element FRAME_BEAM_UNLOCKED
* is updated with the value of the FRAME_COUNTER during the frame
* in which a radar beam state is first determined as "unlocked."
* The data element DELTA_T specifies in seconds the duration of a
```

```

* single frame. Thus the elapsed time since a radar beam was
* declared "unlocked" can be determined by subtracting the present
* value of FRAME_COUNTER from the value of FRAME_BEAM_UNLOCKED and
* multiplying the result by the value of DELTA_T.
*****)

do (for each radar beam i :=(1 to 4))                                {1}

  if (TDLR_COUNTER[i] = 0) then      (* beam is unlocked *)        {2}

    if (TDLR_STATE[i] = 1) then      (* beam was locked *)        {3}
      TDLR_STATE[i] := 0             (* set unlocked *)
      FRAME_BEAM_UNLOCKED[i] := FRAME_COUNTER

    else (* the beam was unlocked *)                                    {3}

      elapsed_time := DELTA_T * (FRAME_COUNTER - FRAME_BEAM_UNLOCKED[i])

      if (elapsed_time >= TDLR_LOCK_TIME) then                      {4}
        FRAME_BEAM_UNLOCKED[i] := FRAME_COUNTER
      end if                                                         {4}

    end if                                                           {3}

  else (* the sensor measurement != 0 *)                             {2}

    if (TDLR_STATE[i] = 0) then      (* beam was unlocked *)        {3}

      elapsed_time := DELTA_T * (FRAME_COUNTER - FRAME_BEAM_UNLOCKED[i])

      if (elapsed_time >= TDLR_LOCK_TIME) then                      {4}
        TDLR_STATE[i] := 1      (* set locked *)
      end if                                                         {4}

    end if                                                           {3}

  end if                                                             {2}

end do (* for each beam i *)                                         {1}

(*****)
* 3B) Determine the beam velocities.
*****)

do (for each radar beam i := (1 to 4))
  b[i] := TDLR_OFFSET + TDLR_GAIN * TDLR_COUNTER[i]
end do (* for each beam *)

(*****)
* 3C) Determine the "processed" beam velocities, and
* 4) Determine the velocity computation indicators.
*****)
(*****)
* Compute a "processed" beam velocity for each of the three axes as
* specified by the following table:

```



```

*
* Beams |          PROCESSED BEAM VELOCITIES          | K-MATRIX | Case
* in lock |          pbvX          pbvY          pbvZ          | X  Y  Z | Number
* -----|-----|-----|-----|-----|-----|-----|-----
* none |          0          |          0          |          0          | 0 | 0 | 0 | 0
* 1 |          0          |          0          |          0          | 0 | 0 | 0 | 1
* 2 |          0          |          0          |          0          | 0 | 0 | 0 | 2
* 3 |          0          |          0          |          0          | 0 | 0 | 0 | 4
* 4 |          0          |          0          |          0          | 0 | 0 | 0 | 8
* -----|-----|-----|-----|-----|-----|-----|-----
* 1,2 |          0          | (b[1]-b[2])/2 |          0          | 0 | 1 | 0 | 3
* 1,3 | (b[1]+b[3])/2 |          0          |          0          | 1 | 0 | 0 | 5
* 1,4 |          0          |          0          | (b[1]-b[4])/2 | 0 | 0 | 1 | 9
* 2,3 |          0          |          0          | (b[2]-b[3])/2 | 0 | 0 | 1 | 6
* 2,4 | (b[2]+b[4])/2 |          0          |          0          | 1 | 0 | 0 | 10
* 3,4 |          0          | (b[4]-b[3])/2 |          0          | 0 | 1 | 0 | 12
* -----|-----|-----|-----|-----|-----|-----|-----
* 1,2,3 | (b[1]+b[3])/2 | (b[1]-b[2])/2 | (b[2]-b[3])/2 | 1 | 1 | 1 | 7
* 1,2,4 | (b[2]+b[4])/2 | (b[1]-b[2])/2 | (b[1]-b[4])/2 | 1 | 1 | 1 | 11
* 1,3,4 | (b[1]+b[3])/2 | (b[4]-b[3])/2 | (b[1]-b[4])/2 | 1 | 1 | 1 | 13
* 2,3,4 | (b[2]+b[4])/2 | (b[4]-b[3])/2 | (b[2]-b[3])/2 | 1 | 1 | 1 | 14
* -----|-----|-----|-----|-----|-----|-----|-----
* 1,2,3,4 |          a          |          b          |          c          | 1 | 1 | 1 | 15

```

```

* a) (b[1]+b[2]+b[3]+b[4])/4
* b) (b[1]-b[2]-b[3]+b[4])/4
* c) (b[1]+b[2]-b[3]-b[4])/4

```

```

* Each of the 16 possible cases has been assigned a case number to
* facilitate the description of the necessary processing. The case
* number is found in the column labeled "Case Number" in the table
* above.

```

```

* Determine the case number value for the current processing.
* Each of the four radar beams' state has been assigned a weight
* value: beam 1: 1, beam 2: 2, beam 3: 4, beam 4: 8. The "case
* number" is computed by summing the radar beams multiplied by their
* their weight factors.

```

```

*****)

```

```

state_case := TDLR_STATE[1] + 2*TDLR_STATE[2] +
              4*TDLR_STATE[3] + 8*TDLR_STATE[4]

```

```

case state_case of
  0, 1, 2, 4, 8:
    pbvX := 0
    pbvY := 0
    pbvZ := 0

    K_MATRIX[1, 1, 0] := 0
    K_MATRIX[2, 2, 0] := 0
    K_MATRIX[3, 3, 0] := 0
  end

```

```

3:  pbvX := 0
    pbvY := (b1-b2)/2

```

```
    pbvZ := 0

    K_MATRIX[1, 1, 0] := 0
    K_MATRIX[2, 2, 0] := 1
    K_MATRIX[3, 3, 0] := 0
end

5:  pbvX := (b1+b3)/2
    pbvY := 0
    pbvZ := 0

    K_MATRIX[1, 1, 0] := 1
    K_MATRIX[2, 2, 0] := 0
    K_MATRIX[3, 3, 0] := 0
end

9:  pbvX := 0
    pbvY := 0
    pbvZ := (b1-b4)/2

    K_MATRIX[1, 1, 0] := 0
    K_MATRIX[2, 2, 0] := 0
    K_MATRIX[3, 3, 0] := 1
end

6:  pbvX := 0
    pbvY := 0
    pbvZ := (b2-b3)/2

    K_MATRIX[1, 1, 0] := 0
    K_MATRIX[2, 2, 0] := 0
    K_MATRIX[3, 3, 0] := 1
end

10: pbvX := (b2+b4)/2
    pbvY := 0
    pbvZ := 0

    K_MATRIX[1, 1, 0] := 1
    K_MATRIX[2, 2, 0] := 0
    K_MATRIX[3, 3, 0] := 0
end

12: pbvX := 0
    pbvY := (b4-b3)/2
    pbvZ := 0

    K_MATRIX[1, 1, 0] := 0
    K_MATRIX[2, 2, 0] := 1
    K_MATRIX[3, 3, 0] := 0
end

7:  pbvX := (b1+b3)/2
    pbvY := (b1-b2)/2
    pbvZ := (b2-b3)/2
```

```

      K_MATRIX[1, 1, 0] := 1
      K_MATRIX[2, 2, 0] := 1
      K_MATRIX[3, 3, 0] := 1
end

```

```

11: pbvX := (b2+b4)/2
    pbvY := (b1-b2)/2
    pbvZ := (b1-b4)/2

```

```

      K_MATRIX[1, 1, 0] := 1
      K_MATRIX[2, 2, 0] := 1
      K_MATRIX[3, 3, 0] := 1
end

```

```

13: pbvX := (b1+b3)/2
    pbvY := (b4-b3)/2
    pbvZ := (b1-b4)/2

```

```

      K_MATRIX[1, 1, 0] := 1
      K_MATRIX[2, 2, 0] := 1
      K_MATRIX[3, 3, 0] := 1
end

```

```

14: pbvX := (b2+b4)/2
    pbvY := (b4-b3)/2
    pbvZ := (b2-b3)/2

```

```

      K_MATRIX[1, 1, 0] := 1
      K_MATRIX[2, 2, 0] := 1
      K_MATRIX[3, 3, 0] := 1
end

```

```

15: pbvX := (b1+b2+b3+b4)/4
    pbvY := (b1-b2-b3+b4)/4
    pbvZ := (b1+b2-b3-b4)/4

```

```

      K_MATRIX[1, 1, 0] := 1
      K_MATRIX[2, 2, 0] := 1
      K_MATRIX[3, 3, 0] := 1
end

```

```

(*****
 * 3D) Convert "processed" beam velocities into body velocities.
*****)

```

```

TDLR_VELOCITY[1] := pbvX / cos(TDLR_ANGLES[1])
TDLR_VELOCITY[2] := pbvY / cos(TDLR_ANGLES[2])
TDLR_VELOCITY[3] := pbvZ / cos(TDLR_ANGLES[3])

```

```

(** where cos represents the cosine function. **)

```

```

END P_SPEC

```



**NAME:**

1.6;18

**TITLE:**

TDSP

**INPUT/OUTPUT:**

TD\_COUNTER : data\_in

TDS\_STATUS : data\_in

TD\_SENSED :data\_out

**TDS\_STATUS : data\_out****BODY:**

BEGIN P\_SPEC

```

(*****
* TDSP -- Touch Down Sensor Processing
*
* TDSP processing is responsible for:
* 1) Determining the operational status of the touch down sensor, and
* 2) determining if touch down has been sensed.
*****)

(*****
* 1) Determining the operational status of the touch down sensor.
* and 2) determining if touch down has been sensed.
*
* The data element TD_COUNTER represents the sensor's measurement.
* There are only two valid sensor measurements: A) all bits set
* which indicates touch down is sensed, and B) all bits clear which
* indicates touch down is not sensed. If a valid sensor value
* exists, then the operation status of the touch down sensor is
* reported as "healthy" (value 0). Any other value of TD_COUNTER
* indicates a faulty sensor in which case the touch down sensor
* status is reported as "failed" (value 1).
*
* Note, once the touch down sensor has been determined to be
* faulty, it is considered to be failed for the duration of the
* mission -- no processing occurs once the sensor has failed.
*
* The notation '0xdddd' represents a hexadecimal value
*****)

if (TDS_STATUS = 0) then      (* healthy sensor *)

    if (TD_COUNTER = 0) then
        TD_SENSED := 0      (* TD not sensed *)

    else if (TD_COUNTER = 0xFFFF) then
        TD_SENSED := 1      (* TD sensed *)

    else
        (* faulty sensor *)
        TD_SENSED := 0
        TDS_STATUS := 1      (* failed sensor *)

```

end if

end if

END P\_SPEC



**NAME:**

1.7;21

**TITLE:**

TSP

**INPUT/OUTPUT:**

M1 : data\_in

M2 : data\_in

M3 : data\_in

M4 : data\_in

SS\_TEMP : data\_in

T1 : data\_in

T2 : data\_in

T3 : data\_in

T4 : data\_in

THERMO\_TEMP : data\_in

ATMOSPHERIC\_TEMP : data\_out

TS\_STATUS : data\_out

**BODY:**

BEGIN P\_SPEC

```

(*****
 * TSP -- Temperature Sensor Processing
 *
 * TSP is responsible for:
 * 1) Ascertaining the operational status of the temperature sensors, and
 * 2) Determining the current atmospheric temperature based on the
 *    measurements provided by two on-board temperature sensors.
 *
 * Notes:
 * o The constants associated with the solid state temperature sensor
 *    and the thermocouple pair would normally be calculated once and
 *    re-used in subsequent calls to this routine. However, the GCS
 *    experiment methodology requires it to be calculated each call.
 *****)

(*****
 * 1) Determine the operational status of the temperature sensors
 *****)

(***) The status of both sensors is always reported as HEALTHY (***)

```



```

TS_STATUS[1] := 0
TS_STATUS[2] := 0

```

```

(*****
 * 2A) Compute the temperature based on the solid state sensor
 *****)

```

```

solid-state-temp :=
  ((T2 - T1)/(M2 - M1)) * SS_TEMP + T1 - ((T2 - T1)/(M2 - M1)) * M1

```

Implementation note, if M1 := M2 a divide by zero exception must be handled.

```

(*****
 * 2B) Determine if the temperature is within the valid range of the
 * TC sensor;
 *****)

```

```

lower-parabolic-function :=
  -(x - (M3 + (((T4 - T3)/(M4 - M3))/2)))^2 + (T3 + (((T4 - T3)/(M4 - M3))/2))^2

```

```

(*****
 * Once the function describing the parabola has been determined, the
 * temperature representing the lower limit of the parabolic region can
 * be determined. The lower limit of the lower parabolic region is
 * specified as 15% of the difference of the two calibration
 * measurements less than the lower calibration point.
 *****)

```

```

lower-parabolic-temp-limit := lower-parabolic-function(M3 - 0.15*(M4 - M3))

```

```

(***) define the upper parabolic function (***)

```

```

upper-parabolic-function :=
  (x - (M4 - (((T4 - T3)/(M4 - M3))/2)))^2 + (T4 - (((T4 - T3)/(M4 - M3))/2))^2

```

```

(*****
 * Once the function describing the parabola has been determined, the
 * temperature representing the upper limit of the parabolic region can
 * be determined. The upper limit of the upper parabolic region is
 * specified as 15% of the difference of the two calibration
 * measurements greater than the upper calibration point.
 *****)

```

```

upper-parabolic-temp-limit := upper-parabolic-function(M4 + 0.15*(M4 - M3))

```

```

(*****
 * Now determine sensor temperature measurement to report
 *****)

```

```

if (solid-state-temp < lower-parabolic-temp-limit) OR           {1}
    (solid-state-temp > upper-parabolic-temp-limit) then

```

```

(***) the atmospheric temp is beyond the valid range of the TC sensor
    so return the solid-state-temp                               (***)

```

```

ATMOSPHERIC_TEMP := solid-state-temp

```

```
else {1}

(*****
 * 2C) Compute the temperature based on the TC sensor
 *****)

    if (THERMO_TEMP < M3) then {2}

(** the atmospheric temp resides within the TC lower parabolic region **)

        ATMOSPHERIC_TEMP := lower-parbolic-function(THERMO_TEMP)

    else if (THERMO_TEMP > M4) then {2}

(** the atmospheric temp resides within the TC upper parabolic region **)

        ATMOSPHERIC_TEMP := upper-parabolic-function(THERMO_TEMP)

    else {2}

(** The temperature resides within the TC sensor linear region **)

(** compute the temperature from the TC linear region **)

        ATMOSPHERIC_TEMP :=
        ((T4 - T3)/(M4 - M3)) * THERMO_TEMP + T3 - ((T4 - T3)/(M4 - M3)) * M3

    end if {2}

end if {1}

END P_SPEC
```



**NAME:**

1.8;51

**TITLE:**

CP

**INPUT/OUTPUT:**

AE\_CMD : data\_in

AE\_STATUS : data\_in

AE\_TEMP : data\_in

AR\_ALTITUDE : data\_in

AR\_STATUS: data\_in

ATMOSPHERIC\_TEMP : data\_in

A\_ACCELERATION : data\_in

A\_STATUS : data\_in

CHUTE\_RELEASED : data\_in

COMM\_SYNC\_PATTERN : data\_in

CONTOUR\_CROSSED : data\_in

C\_STATUS : data\_in

FRAME\_COUNTER : data\_in

GP\_ALTITUDE : data\_in

GP\_ATTITUDE : data\_in

GP\_PHASE : data\_in

GP\_ROTATION : data\_in

GP\_VELOCITY : data\_in

G\_ROTATION : data\_in

G\_STATUS : data\_in

K\_ALT : data\_in

K\_MATRIX : data\_in

PE\_INTEGRAL : data\_in

RE\_CMD : data\_in

RE\_STATUS : data\_in

**SUBFRAME\_COUNTER : data\_in**

**TDLR\_STATE : data\_in**

**TDLR\_STATUS : data\_in**

**TDLR\_VELOCITY : data\_in**

**TDS\_STATUS : data\_in**

**TD\_SENSED : data\_in**

**TE\_INTEGRAL : data\_in**

**TS\_STATUS : data\_in**

**VELOCITY\_ERROR : data\_in**

**YE\_INTEGRAL : data\_in**

**C\_STATUS : data\_out**

**PACKET :data\_out**

**BODY:**

BEGIN P\_SPEC

Note, bubbles 1.8, 2.3, 3.5 and the associated P-Specs represent a single process, CP described below.

```
(*****  
* CP -- Communications Processing  
*  
* CP processing is responsible for:  
* 1) determining the current operational status of the communicator, and  
* 2) constructing a telemetry data packet.  
*  
* CP processing is responsible for constructing a data packet  
* suitable for transmission via the on-board communications  
* equipment. The data element PACKET contains 512 bytes of storage  
* in which to construct the data packet. Conceptually, the data  
* packet is merely the organization of particular data into the  
* storage defined by PACKET.  
*  
* A data packet is organized into five fields arranged in the  
* following sequence: a synchronization pattern, a sequence number,  
* a data mask, a data field, and a checksum. Constructing a data  
* packet consists of updating the five fields with the appropriate  
* data.  
*  
* CP has the capability to construct three specific types of  
* data packets, one each for reporting the completion of each  
* subframe. The distinguishing element of each packet type is  
* the contents of the data field and indirectly the value of the  
* data mask. The data field is a composite
```

\* field consisting of the values of specific data elements which  
 \* were potentially altered during the processing of the specified  
 \* subframe.

\*  
 \* The contents of the data field of a specific data packet is  
 \* indicated by the data packet's data mask. The data mask is a  
 \* 32-bit field. Each of the 32 data elements which may be reported  
 \* in the data packet has an associated bit in the data mask. A set  
 \* bit in the data mask indicates that the associated data element  
 \* is stored in the data field portion of the data packet.

\*  
 \* At the completion of sensor processing subframe, the data field  
 \* contains the data elements listed below in the order listed.  
 \* Note the list of data elements below contains the derivation  
 \* of the data mask value and derivation of the data field length,  
 \* in bytes, which is used in constructing the packet. The  
 \* synchronization pattern, sequence number, and data mask  
 \* consume 7 bytes.

* data element	data	field length	
* name	bit mask	in bytes	
* AR_ALTITUDE	0x10000000	8	
* AR_STATUS	0x08000000	1	
* ATMOSPHERIC_TEMP	0x04000000	8	122 bytes in this field
* A_ACCELERATION	0x02000000	24	+ 7 bytes in preceding fields
* A_STATUS	0x01000000	3	---
* C_STATUS	0x00200000	1	129 bytes not including
* G_ROTATION	0x00008000	24	the checksum
* G_STATUS	0x00004000	1	
* K_ALT	0x00002000	4	
* K_MATRIX	0x00001000	12	
* TDLR_STATE	0x00000100	4	
* TDLR_STATUS	0x00000080	4	
* TDLR_VELOCITY	0x00000040	24	
* TDS_STATUS	0x00000020	1	
* TD_SENSED	0x00000010	1	
* TS_STATUS	0x00000004	2	
			122 bytes

\*  
 \*  
 \* 0x1F20F1F4 data mask value for subframe #1

\* At the completion of guidance processing subframe, the data field  
 \* contains the following data elements:

* data element	data	field length	
* name	bit mask	in bytes	
* CONTOUR_CROSSED	0x00400000	1	
* C_STATUS	0x00200000	1	
* GP_ALTITUDE	0x00100000	8	166 bytes in this field
* GP_ATTITUDE	0x00080000	72	+ 7 bytes in preceding fields
* GP_PHASE	0x00040000	4	---
* GP_ROTATION	0x00020000	48	173 bytes not including
* GP_VELOCITY	0x00010000	24	the checksum
* VELOCITY_ERROR	0x00000002	8	

```

*                                     166 bytes
*
*                                     0x007F0002 data mask value for subframe #2
*
* At the completion of control law processing subframe, the data field
* contains the following data elements:
*
* data element      data      field length
*   name           bit mask   in bytes
*
* AE_CMD           0x80000000    6
* AE_STATUS        0x40000000    1
* AE_TEMP          0x20000000    2      38 bytes in this field
* CHUTE_RELEASED  0x00800000    1      + 7 bytes in preceding fields
* C_STATUS         0x00200000    1      ---
* PE_INTEGRAL     0x00000800    8      45 bytes not including
* RE_CMD          0x00000400    2      the checksum
* RE_STATUS       0x00000200    1
* TE_INTEGRAL     0x00000008    8
* YE_INTEGRAL     0x00000001    8
*
*                                     38 bytes
*
*                                     0xE0A00E09 data mask value for subframe #3
*
* It is not obvious why the checksum field is defined in three
* places in the data structures presented below. Notice that the
* data field is variable in length. The organization of the data
* packet demands that the checksum field immediately follow the
* last byte of the data field. In order to satisfy this
* requirement, storage for the checksum field is defined as the
* last element in each of the data field specifications.
*
* A function for computing the CRC-16 for a data packet is defined
* below. The function takes two arguments, the address of the byte
* stream to process and integer specifying the length of the byte
* stream. The function returns an integer value which is the
* CRC-16 of the specified byte stream.
*****

```

(\*\* the Sensor Processing subframe data field and checksum \*\*)

```

type sp_data_t Record
  AR_ALTITUDE      : quadword
  AR_STATUS        : byte
  ATMOSPHERIC_TEMP : quadword
  A_ACCELERATION   : array[1..3] of quadword
  A_STATUS         : array[1..3] of byte
  C_STATUS         : byte
  G_ROTATION       : array[1..3] of quadword
  G_STATUS         : byte
  K_ALT            : longword
  K_MATRIX         : array[1..3] of longword
  TDLR_STATE       : array[1..4] of byte
  TDLR_STATUS      : array[1..4] of byte
  TDLR_VELOCITY    : array[1..3] of quadword
  TDS_STATUS       : byte

```

```

    TD_SENSED      : byte
    TS_STATUS      : array[1..2] of byte
    CHECKSUM       : word
end {record}

```

(\*\* the Guidance Processing subframe data field and checksum \*\*)

```

type gp_data_t record
    CONTOUR_CROSSED : byte
    C_STATUS        : byte
    GP_ALTITUDE     : quadword
    GP_ATTITUDE     : array[1..9] of quadword
    GP_PHASE        : longword
    GP_ROTATION     : array[1..6] of quadword
    GP_VELOCITY     : array[1..3] of quadword
    VELOCITY_ERROR  : quadword
    CHECKSUM        : word
end {record}

```

(\*\* the Control Law Processing subframe data field and checksum \*\*)

```

type clp_data_t record
    AE_CMD          : array [1..3] of word
    AE_STATUS       : byte
    AE_TEMP         : word
    CHUTE_RELEASED : byte
    C_STATUS        : byte
    PE_INTEGRAL    : quadword
    RE_CMD          : word
    RE_STATUS       : byte
    TE_INTEGRAL    : quadword
    YE_INTEGRAL    : quadword
    CHECKSUM        : word
end {record}

```

(\*\* the data packet structure \*\*)

```

type subframe_t = (sp_data_t, gp_data_t, clp_data_t)

```

```

type data_packet_t = record
    SYNC_PATTERN    : word
    SEQ_NUMBER      : byte
    DATA_MASK      : longword
    case subframe_t of
        sp          : sp_data_t
        | gp        : gp_data_t
        | clp       : clp_data_t
    end
end {record}

```

```

(*****
 * Overlay the data element PACKET with the data structure data_packet_t
 * and refer to it as "data_packet" for local processing.
 *****)

```

(\*\* declare a variable of type pointer to data\_packet\_t \*\*)



```

var data_packet: @data_packet_t

data_packet@ := PACKET      (* new variable "points to" PACKET *)

(*****
 * 1) Determine the current operational status of the communicator.
 *
 * The operational status of the communicator is always reported
 * as "healthy" (value 0).
 *****)

C_STATUS := 0

(*****
 * 2) Construct a telemetry data packet.
 *****)

(*****
 * 2A) Get synchronization pattern.
 *
 * The leading field is the synchronization pattern. This 16-bit
 * pattern allows the receiving communications gear to recognize
 * the beginning of the data packet. The bit pattern is stored in
 * the data element COMM_SYNC_PATTERN.
 *****)

data_packet.SYNC_PATTERN := COMM_SYNC_PATTERN

(*****
 * 2B) Determine the sequence number.
 *
 * The sequence number is an unsigned 8-bit value. Conceptually,
 * the sequence number performs as an 8-bit counter. The initial
 * packet is assigned a value of zero and the counter incremented
 * for each packet thereafter. However, an implementation does not
 * have access to its own inter-subframe static storage, so the
 * "counter" is implemented as a function of the current frame
 * number and subframe number.
 *****)

data_packet.SEQ_NUMBER := (3*(FRAME_COUNTER-1)+(SUBFRAME_COUNTER-1)) MOD 256

where MOD represents modulo division operation

(*****
 * 2C) Prepare the data mask,
 * 2D) Prepare the data, and
 * 2E) Compute the checksum.
 *****)

if (SUBFRAME_COUNTER == 1) then      (* sp *)
  data_packet.DATA_MASK := 0x1F20F1F4

  data_packet.DATA.SP.AR_ALTITUDE := AR_ALTITUDE[0]

```

```

data_packet.DATA.SP.AR_STATUS      := AR_STATUS[0]
data_packet.DATA.SP.ATMOSPHERIC_TEMP := ATMOSPHERIC_TEMP
data_packet.DATA.SP.A_ACCELERATION[1] := A_ACCELERATION[1,0]
data_packet.DATA.SP.A_ACCELERATION[2] := A_ACCELERATION[2,0]
data_packet.DATA.SP.A_ACCELERATION[3] := A_ACCELERATION[3,0]
data_packet.DATA.SP.A_STATUS[1]      := A_STATUS[1,0]
data_packet.DATA.SP.A_STATUS[2]      := A_STATUS[2,0]
data_packet.DATA.SP.A_STATUS[3]      := A_STATUS[3,0]
data_packet.DATA.SP.C_STATUS         := C_STATUS
data_packet.DATA.SP.G_ROTATION[1]    := G_ROTATION[1,0]
data_packet.DATA.SP.G_ROTATION[2]    := G_ROTATION[2,0]
data_packet.DATA.SP.G_ROTATION[3]    := G_ROTATION[3,0]
data_packet.DATA.SP.G_STATUS         := G_STATUS
data_packet.DATA.SP.K_ALT            := K_ALT[0]
data_packet.DATA.SP.K_MATRIX[1]     := K_MATRIX[1,1,0]
data_packet.DATA.SP.K_MATRIX[2]     := K_MATRIX[2,2,0]
data_packet.DATA.SP.K_MATRIX[3]     := K_MATRIX[3,3,0]
data_packet.DATA.SP.TDLR_STATE[1]    := TDLR_STATE[1]
data_packet.DATA.SP.TDLR_STATE[2]    := TDLR_STATE[2]
data_packet.DATA.SP.TDLR_STATE[3]    := TDLR_STATE[3]
data_packet.DATA.SP.TDLR_STATE[4]    := TDLR_STATE[4]
data_packet.DATA.SP.TDLR_STATUS[1]   := TDLR_STATUS[1]
data_packet.DATA.SP.TDLR_STATUS[2]   := TDLR_STATUS[2]
data_packet.DATA.SP.TDLR_STATUS[3]   := TDLR_STATUS[3]
data_packet.DATA.SP.TDLR_STATUS[4]   := TDLR_STATUS[4]
data_packet.DATA.SP.TDLR_VELOCITY[1] := TDLR_VELOCITY[1,0]
data_packet.DATA.SP.TDLR_VELOCITY[2] := TDLR_VELOCITY[2,0]
data_packet.DATA.SP.TDLR_VELOCITY[3] := TDLR_VELOCITY[3,0]
data_packet.DATA.SP.TDS_STATUS       := TDS_STATUS
data_packet.DATA.SP.TD_SENSED        := TD_SENSED
data_packet.DATA.SP.TS_STATUS[1]     := TS_STATUS[1]
data_packet.DATA.SP.TS_STATUS[2]     := TS_STATUS[2]
data_packet.DATA.SP.CHECKSUM         := CRC16(data_packet.DATA.SP, 129)

```

```

else if (SUBFRAME_COUNTER == 2) then      (* gp *)
  data_packet.DATA_MASK := 0x007F0002

```

```

data_packet.DATA.GP.CONTOUR_CROSSED := CONTOUR_CROSSED
data_packet.DATA.GP.C_STATUS        := C_STATUS
data_packet.DATA.GP.GP_ALTITUDE     := GP_ALTITUDE[0]

```

(\*\*\* first element of array changes most rapidly \*\*\*)

```

data_packet.DATA.GP.GP_ATTITUDE[1] := GP_ATTITUDE[1, 1, 0]
data_packet.DATA.GP.GP_ATTITUDE[2] := GP_ATTITUDE[2, 1, 0]
data_packet.DATA.GP.GP_ATTITUDE[3] := GP_ATTITUDE[3, 1, 0]
data_packet.DATA.GP.GP_ATTITUDE[4] := GP_ATTITUDE[1, 2, 0]
data_packet.DATA.GP.GP_ATTITUDE[5] := GP_ATTITUDE[2, 2, 0]
data_packet.DATA.GP.GP_ATTITUDE[6] := GP_ATTITUDE[3, 2, 0]
data_packet.DATA.GP.GP_ATTITUDE[7] := GP_ATTITUDE[1, 3, 0]
data_packet.DATA.GP.GP_ATTITUDE[8] := GP_ATTITUDE[2, 3, 0]
data_packet.DATA.GP.GP_ATTITUDE[9] := GP_ATTITUDE[3, 3, 0]

```

```

data_packet.DATA.GP.GP_PHASE        := GP_PHASE

```

```

data_packet.DATA.GP.GP_ROTATION[1] := GP_ROTATION[2, 1]

```

```

data_packet.DATA.GP.GP_ROTATION[2] := GP_ROTATION[3, 1]
data_packet.DATA.GP.GP_ROTATION[3] := GP_ROTATION[1, 2]
data_packet.DATA.GP.GP_ROTATION[4] := GP_ROTATION[3, 2]
data_packet.DATA.GP.GP_ROTATION[5] := GP_ROTATION[1, 3]
data_packet.DATA.GP.GP_ROTATION[6] := GP_ROTATION[2, 3]

data_packet.DATA.GP.GP_VELOCITY[1] := GP_VELOCITY[1, 0]
data_packet.DATA.GP.GP_VELOCITY[2] := GP_VELOCITY[2, 0]
data_packet.DATA.GP.GP_VELOCITY[3] := GP_VELOCITY[3, 0]

data_packet.DATA.GP.VELOCITY_ERROR := VELOCITY_ERROR
data_packet.DATA.GP.checksum      := CRC16(data_packet.DATA.GP, 173)

```

```
else (* clp *)
```

```
data_packet.DATA_MASK := 0xE0A00E09
```

```

data_packet.DATA.CLP.AE_CMD[1] := AE_CMD[1]
data_packet.DATA.CLP.AE_CMD[2] := AE_CMD[2]
data_packet.DATA.CLP.AE_CMD[3] := AE_CMD[3]
data_packet.DATA.CLP.AE_STATUS := AE_STATUS
data_packet.DATA.CLP.AE_TEMP := AE_TEMP
data_packet.DATA.CLP.CHUTE_RELEASED := CHUTE_RELEASED
data_packet.DATA.CLP.C_STATUS := C_STATUS
data_packet.DATA.CLP.PE_INTEGRAL := PE_INTEGRAL
data_packet.DATA.CLP.RE_CMD := RE_CMD
data_packet.DATA.CLP.RE_STATUS := RE_STATUS
data_packet.DATA.CLP.TE_INTEGRAL := TE_INTEGRAL
data_packet.DATA.CLP.YE_INTEGRAL := YE_INTEGRAL
data_packet.DATA.CLP.CHECKSUM := CRC16(data_packet.DATA.CLP, 45)

```

```
end if
```

```
return
```

```

(*****
* Title: CRC16
* Description:
*   Compute the Cyclic Redundancy Code of the specified buffer using
*   CRC-16 as the generator polynomial.
* Arguments:
*   byte pointer buffer - address of first byte of message.
*   longword   length - count of bytes in message.
*
* Returns:
*   word   crc   - the CRC-16 of the specified message.
*****)

```

```

(*****
* The following CRC generation algorithm is described by Perez in
* IEEE Micro, Volume 3, Number 3 (june 1983).
*
* The algorithm computes the CRC of the specified messages by
* operating on a byte at a time. Beginning with an initial value
* for the CRC, each byte of the message in sequence is applied to
* the computation of the new CRC value.
*

```

\* In the bitwise approach to generating a CRC, Each bit within the  
 \* message is operated on individually. Note, that after performing the  
 \* necessary bitwise operations on 8 successive bits, there are only  
 \* 256 possible distinct results. This algorithm takes advantage of  
 \* this fact and operates on a single byte (8-bits) at time.

\*

\* For a given 17-bit generator polynomial a 256 (16-bits) entry  
 \* table is constructed for storing the polynomial "signature."  
 \* The contents of this table is used for processing the message.  
 \* An algorithm for constructing the table is presented in the reference  
 \* cited above.

\*\*\*\*\*)

(\*\* The "signature" table for the CRC-16 generator polynomial 0x1A001 \*\*)

```
word crc16_table[0..255] :=
    0x0000, 0xc0c1, 0xc181, 0x0140, 0xc301, 0x03c0, 0x0280, 0xc241,
    0xc601, 0x06c0, 0x0780, 0xc741, 0x0500, 0xc5c1, 0xc481, 0x0440,
    0xcc01, 0x0cc0, 0x0d80, 0xcd41, 0x0f00, 0xcf41, 0xce81, 0x0e40,
    0x0a00, 0xca41, 0xcb81, 0x0b40, 0xc901, 0x09c0, 0x0880, 0xc841,
    0xd801, 0x18c0, 0x1980, 0xd941, 0x1b00, 0xdb41, 0xda81, 0x1a40,
    0x1e00, 0xde41, 0xdf81, 0x1f40, 0xdd01, 0x1dc0, 0x1c80, 0xdc41,
    0x1400, 0xd441, 0xd581, 0x1540, 0xd701, 0x17c0, 0x1680, 0xd641,
    0xd201, 0x12c0, 0x1380, 0xd341, 0x1100, 0xd141, 0xd081, 0x1040,
    0xf001, 0x30c0, 0x3180, 0xf141, 0x3300, 0xf341, 0xf281, 0x3240,
    0x3600, 0xf641, 0xf781, 0x3740, 0xf501, 0x35c0, 0x3480, 0xf441,
    0x3c00, 0xfc41, 0xfd81, 0x3d40, 0xff01, 0x3fc0, 0x3e80, 0xfe41,
    0xfa01, 0x3ac0, 0x3b80, 0xfb41, 0x3900, 0xf941, 0xf881, 0x3840,
    0x2800, 0xe841, 0xe981, 0x2940, 0xeb01, 0x2bc0, 0x2a80, 0xea41,
    0xee01, 0x2ec0, 0x2f80, 0xef41, 0x2d00, 0xed41, 0xec81, 0x2c40,
    0xe401, 0x24c0, 0x2580, 0xe541, 0x2700, 0xe741, 0xe681, 0x2640,
    0x2200, 0xe241, 0xe381, 0x2340, 0xe101, 0x21c0, 0x2080, 0xe041,
    0xa001, 0x60c0, 0x6180, 0xa141, 0x6300, 0xa341, 0xa281, 0x6240,
    0x6600, 0xa641, 0xa781, 0x6740, 0xa501, 0xa5c0, 0xa480, 0xa441,
    0x6c00, 0xac41, 0xad81, 0x6d40, 0xaf01, 0x6fc0, 0x6e80, 0xae41,
    0xaa01, 0x6ac0, 0x6b80, 0xab41, 0x6900, 0xa941, 0xa881, 0x6840,
    0x7800, 0xb841, 0xb981, 0x7940, 0xbb01, 0x7bc0, 0x7a80, 0xba41,
    0xbe01, 0x7ec0, 0x7f80, 0xbf41, 0x7d00, 0xbd41, 0x7c81, 0x7c40,
    0xb401, 0x74c0, 0x7580, 0xb541, 0x7700, 0xb741, 0xb681, 0x7640,
    0x7200, 0xb241, 0xb381, 0x7340, 0xb101, 0x71c0, 0x7080, 0xb041,
    0x5000, 0x90c1, 0x9181, 0x5140, 0x9301, 0x53c0, 0x5280, 0x9241,
    0x9601, 0x56c0, 0x5780, 0x9741, 0x5500, 0x95c1, 0x9481, 0x5440,
    0x9c01, 0x5cc0, 0x5d80, 0x9d41, 0x5f00, 0x9fc1, 0x9e81, 0x5e40,
    0x5a00, 0x9ac1, 0x9b81, 0x5b40, 0x9901, 0x99c0, 0x9880, 0x9841,
    0x8801, 0x48c0, 0x4980, 0x8941, 0x4b00, 0x8b41, 0x8a81, 0x4a40,
    0x4e00, 0x8ec1, 0x8f81, 0x4f40, 0x8d01, 0x4dc0, 0x4c80, 0x8c41,
    0x4400, 0x84c1, 0x8581, 0x4540, 0x8701, 0x47c0, 0x4680, 0x8641,
    0x8201, 0x42c0, 0x4380, 0x8341, 0x4100, 0x81c1, 0x8081, 0x4040
```

(\*\* crc is a 16-bit unsigned integer value \*\*)

```
    crc := 0 (* initial crc value *)
```

(\*\* process every byte in the message \*\*)

```
    do next_byte := 1 to bytecount
```

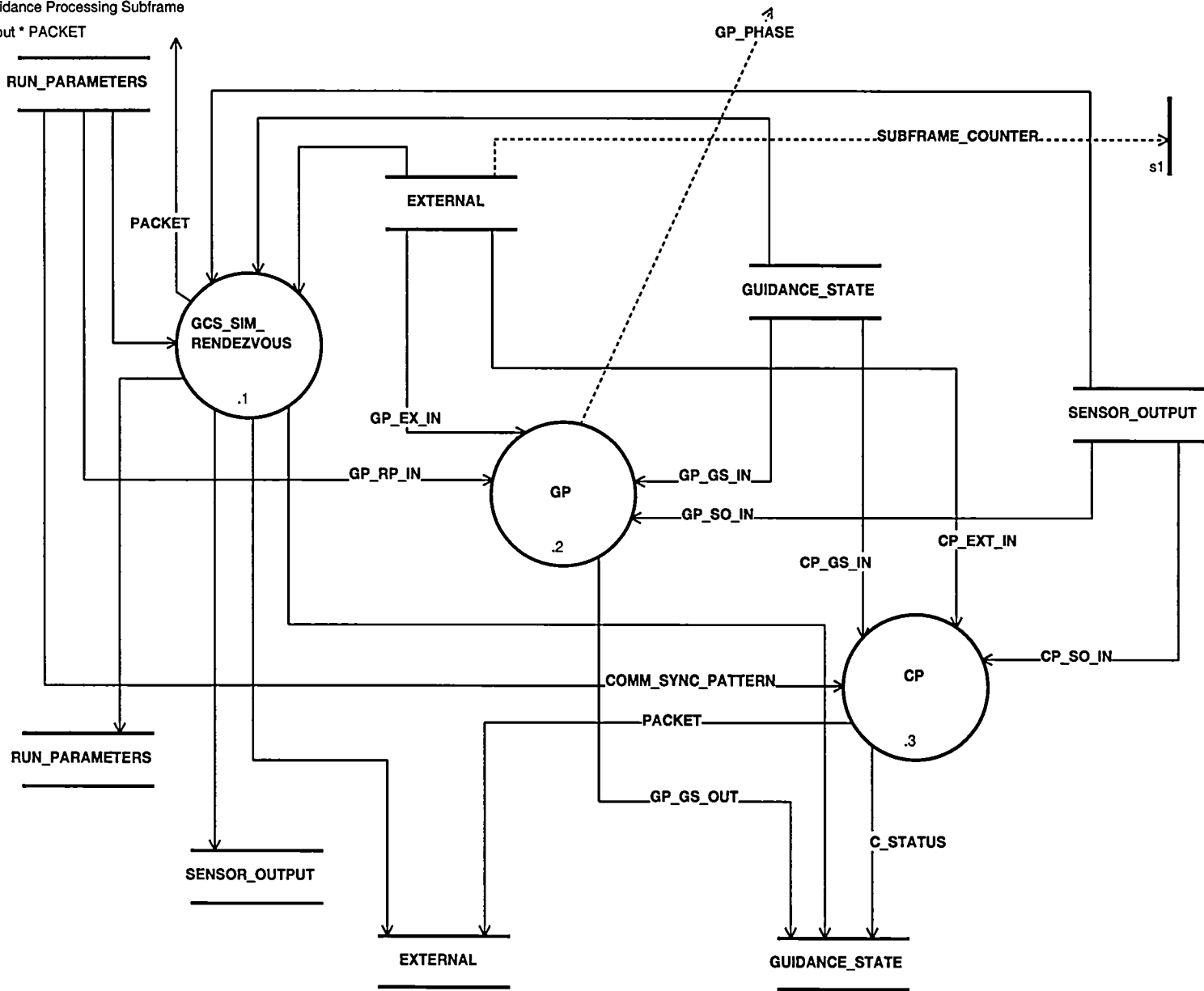
```
    index := crc XOR next_byte (* bitwise exclusive OR the lower 8 bits of crc *)
    crc   := crc >> 8          (* bitwise right shift crc 8 times *)
    crc   := crc XOR crcl6_table[index](* bitwise exclusive OR all 16 bits of crc *)
end do

return crc

END P_SPEC
```



2;10  
 Guidance Processing Subframe  
 \* out \* PACKET



2-s1;3  
PAT - Guidance Processing Subframe

SUBFRAME_COUNTER	"GCS_SIM_RENDEZVOUS"	"GP"	"CP"
"2"	1	2	3



**NAME:**

2.1;4

**TITLE:**

GCS\_SIM\_RENDEZVOUS

**INPUT/OUTPUT:**

**SENSOR\_OUTPUT** : data\_in

**GUIDANCE\_STATE** : data\_in

**EXTERNAL** : data\_in

**RUN\_PARAMETERS** : data\_in

**RUN\_PARAMETERS** : data\_out

**SENSOR\_OUTPUT** : data\_out

**EXTERNAL** : data\_out

**PACKET**: data\_out

**GUIDANCE\_STATE** : data\_out

**BODY:**

BEGIN P-Spec

GCS\_SIM\_RENDEZVOUS provides the interface to the vehicle. This module is provided by the systems group.

Bubbles 1.1, 2.1, 3.1 and the associated P-Specs represent a single process.

END P-Spec



**NAME:**

2.2;47

**TITLE:**

GP

**INPUT/OUTPUT:****A\_ACCELERATION : data\_in****AE\_SWITCH : data\_in****AE\_TEMP : data\_in****AR\_ALTITUDE : data\_in****CHUTE\_RELEASED : data\_in****CL : data\_in****CONTOUR\_ALTITUDE : data\_in****CONTOUR\_CROSSED : data\_in****CONTOUR\_VELOCITY : data\_in****DELTA\_T : data\_in****DROP\_HEIGHT : data\_in****DROP\_SPEED : data\_in****ENGINES\_ON\_ALTITUDE : data\_in****FRAME\_COUNTER : data\_in****GP\_ALTITUDE : data\_in****GP\_ATTITUDE : data\_in****GP\_PHASE : data\_in****GP\_VELOCITY : data\_in****GRAVITY : data\_in****G\_ROTATION : data\_in****K\_ALT : data\_in****K\_MATRIX : data\_in****MAX\_NORMAL\_VELOCITY : data\_in****RE\_SWITCH : data\_in****TD\_SENSED : data\_in**

**TDLR\_VELOCITY : data\_in**

**TDS\_STATUS : data\_in**

**AE\_SWITCH : data\_out**

**CL : data\_out**

**CONTOUR\_CROSSED : data\_out**

**FRAME\_ENGINES\_IGNITED : data\_out**

**GP\_ALTITUDE : data\_out**

**GP\_ATTITUDE : data\_out**

**GP\_PHASE : data\_out**

**GP\_ROTATION : data\_out**

**GP\_VELOCITY : data\_out**

**RE\_SWITCH : data\_out**

**TE\_INTEGRAL : data\_out**

**VELOCITY\_ERROR : data\_out**

**BODY:**

BEGIN P\_SPEC

```
(*****  
* GP -- Guidance Processing  
*  
* GP is responsible for:  
* 1) Maintaining the history of the vehicle's altitude, velocities,  
*    and attitude,  
* 2) Computing the current vehicle altitude, velocities and attitude,  
* 3) Determining if the engines should be switched on or off,  
* 4) Computing the current velocity error,  
* 5) Determining if the predetermined velocity-altitude contour has  
*    been crossed,  
* 6) Determining the current guidance phase, and  
* 7) Determining the appropriate axial engine control law parameters.  
*****)  
  
(*****  
* 1) Maintain the history of the vehicle altitude, velocities,  
*    and attitude by "rotating variables."  
*  
* The data element GP_ALTITUDE is defined as a single dimensional  
* array. The data element GP_VELOCITY is defined as a two  
* dimensional array. The first dimension of GP_VELOCITY represents  
* a vehicle axis: x-axis (1), y-axis (2), z-axis (3). The data
```

```

* element GP_ATTITUDE is defined as a three dimensional array
* (1..3, 1..3, 0..4). The vehicle attitudes are arranged as a 3x3
* matrix, represented by the first two dimensions of GP_ATTITUDE.
* The first dimension of GP_ATTITUDE, the second dimension of
* GP_VELOCITY and the third dimension of GP_ATTITUDE represent a
* history. Each history is five deep. The first element of each
* history, element zero, holds the most recently computed value.
* The last element of each history, element four holds the oldest
* maintained value. In shifting the values stored in these data
* elements, a multi-frame history is maintained.
*****
GP_ALTITUDE[4] := GP_ALTITUDE[3]
GP_ALTITUDE[3] := GP_ALTITUDE[2]
GP_ALTITUDE[2] := GP_ALTITUDE[1]
GP_ALTITUDE[1] := GP_ALTITUDE[0]

GP_VELOCITY[1, 4] := GP_VELOCITY[1, 3]
GP_VELOCITY[1, 3] := GP_VELOCITY[1, 2]
GP_VELOCITY[1, 2] := GP_VELOCITY[1, 1]
GP_VELOCITY[1, 1] := GP_VELOCITY[1, 0]

GP_VELOCITY[2, 4] := GP_VELOCITY[2, 3]
GP_VELOCITY[2, 3] := GP_VELOCITY[2, 2]
GP_VELOCITY[2, 2] := GP_VELOCITY[2, 1]
GP_VELOCITY[2, 1] := GP_VELOCITY[2, 0]

GP_VELOCITY[3, 4] := GP_VELOCITY[3, 3]
GP_VELOCITY[3, 3] := GP_VELOCITY[3, 2]
GP_VELOCITY[3, 2] := GP_VELOCITY[3, 1]
GP_VELOCITY[3, 1] := GP_VELOCITY[3, 0]

GP_ATTITUDE[1, 1, 4] := GP_ATTITUDE[1, 1, 3]
GP_ATTITUDE[1, 2, 4] := GP_ATTITUDE[1, 2, 3]
GP_ATTITUDE[1, 3, 4] := GP_ATTITUDE[1, 3, 3]
GP_ATTITUDE[2, 1, 4] := GP_ATTITUDE[2, 1, 3]
GP_ATTITUDE[2, 2, 4] := GP_ATTITUDE[2, 2, 3]
GP_ATTITUDE[2, 3, 4] := GP_ATTITUDE[2, 3, 3]
GP_ATTITUDE[3, 1, 4] := GP_ATTITUDE[3, 1, 3]
GP_ATTITUDE[3, 2, 4] := GP_ATTITUDE[3, 2, 3]
GP_ATTITUDE[3, 3, 4] := GP_ATTITUDE[3, 3, 3]

GP_ATTITUDE[1, 1, 3] := GP_ATTITUDE[1, 1, 2]
GP_ATTITUDE[1, 2, 3] := GP_ATTITUDE[1, 2, 2]
GP_ATTITUDE[1, 3, 3] := GP_ATTITUDE[1, 3, 2]
GP_ATTITUDE[2, 1, 3] := GP_ATTITUDE[2, 1, 2]
GP_ATTITUDE[2, 2, 3] := GP_ATTITUDE[2, 2, 2]
GP_ATTITUDE[2, 3, 3] := GP_ATTITUDE[2, 3, 2]
GP_ATTITUDE[3, 1, 3] := GP_ATTITUDE[3, 1, 2]
GP_ATTITUDE[3, 2, 3] := GP_ATTITUDE[3, 2, 2]
GP_ATTITUDE[3, 3, 3] := GP_ATTITUDE[3, 3, 2]

GP_ATTITUDE[1, 1, 2] := GP_ATTITUDE[1, 1, 1]
GP_ATTITUDE[1, 2, 2] := GP_ATTITUDE[1, 2, 1]
GP_ATTITUDE[1, 3, 2] := GP_ATTITUDE[1, 3, 1]
GP_ATTITUDE[2, 1, 2] := GP_ATTITUDE[2, 1, 1]

```

```

GP_ATTITUDE[2, 2, 2] := GP_ATTITUDE[2, 2, 1]
GP_ATTITUDE[2, 3, 2] := GP_ATTITUDE[2, 3, 1]
GP_ATTITUDE[3, 1, 2] := GP_ATTITUDE[3, 1, 1]
GP_ATTITUDE[3, 2, 2] := GP_ATTITUDE[3, 2, 1]
GP_ATTITUDE[3, 3, 2] := GP_ATTITUDE[3, 3, 1]

```

```

GP_ATTITUDE[1, 1, 1] := GP_ATTITUDE[1, 1, 0]
GP_ATTITUDE[1, 2, 1] := GP_ATTITUDE[1, 2, 0]
GP_ATTITUDE[1, 3, 1] := GP_ATTITUDE[1, 3, 0]
GP_ATTITUDE[2, 1, 1] := GP_ATTITUDE[2, 1, 0]
GP_ATTITUDE[2, 2, 1] := GP_ATTITUDE[2, 2, 0]
GP_ATTITUDE[2, 3, 1] := GP_ATTITUDE[2, 3, 0]
GP_ATTITUDE[3, 1, 1] := GP_ATTITUDE[3, 1, 0]
GP_ATTITUDE[3, 2, 1] := GP_ATTITUDE[3, 2, 0]
GP_ATTITUDE[3, 3, 1] := GP_ATTITUDE[3, 3, 0]

```

```

(*****
* 2) Compute the current vehicle altitude, velocities and attitude.
*
* For a more detailed description of this processing, see the section
* 2.3 of the design introduction.
*****)

```

```

(***) simultaneously compute the current vehicle attitude, velocities
and altitude (***)

```

```

(***) range check the following data elements (***)

```

```

(*****
* In all other instances of range checking, the actual range checking
* has been written out. Here, however, writing out all of the range
* checking is prohibitively long. So, it should be sufficient to say,
* range check the following data elements:
*
* element lower upper
*****)

```

```

GP_ATTITUDE[1, 1, 2] -1 1
GP_ATTITUDE[1, 2, 2] -1 1
GP_ATTITUDE[1, 3, 2] -1 1
GP_ATTITUDE[2, 1, 2] -1 1
GP_ATTITUDE[2, 2, 2] -1 1
GP_ATTITUDE[2, 3, 2] -1 1
GP_ATTITUDE[3, 1, 2] -1 1
GP_ATTITUDE[3, 2, 2] -1 1
GP_ATTITUDE[3, 3, 2] -1 1

```

```

GP_VELOCITY[1, 2] -100 100
GP_VELOCITY[2, 2] -100 100
GP_VELOCITY[3, 2] -100 100

```

```

GP_ALTITUDE[2] 0 2000

```

```

(***) sensor data (***)

```

```

G_ROTATION[1, 0] -1 1

```

```

G_ROTATION[2, 0]      -1      1
G_ROTATION[3, 0]      -1      1
G_ROTATION[1, 1]      -1      1
G_ROTATION[2, 1]      -1      1
G_ROTATION[3, 1]      -1      1
G_ROTATION[1, 2]      -1      1
G_ROTATION[2, 2]      -1      1
G_ROTATION[3, 2]      -1      1

```

```

A_ACCELERATION[1, 0]  -20      5
A_ACCELERATION[2, 0]  -20      5
A_ACCELERATION[3, 0]  -20      5
A_ACCELERATION[1, 1]  -20      5
A_ACCELERATION[2, 1]  -20      5
A_ACCELERATION[3, 1]  -20      5
A_ACCELERATION[1, 2]  -20      5
A_ACCELERATION[2, 2]  -20      5
A_ACCELERATION[3, 2]  -20      5

```

```

TDLR_VELOCITY[1, 0]   -100     100
TDLR_VELOCITY[2, 0]   -100     100
TDLR_VELOCITY[3, 0]   -100     100
TDLR_VELOCITY[1, 1]   -100     100
TDLR_VELOCITY[2, 1]   -100     100
TDLR_VELOCITY[3, 1]   -100     100
TDLR_VELOCITY[1, 2]   -100     100
TDLR_VELOCITY[2, 2]   -100     100
TDLR_VELOCITY[3, 2]   -100     100

```

```

AR_ALTITUDE[0]        0      2000
AR_ALTITUDE[1]        0      2000
AR_ALTITUDE[2]        0      2000

```

```

(*****

```

```

*   A five step implementation of the RK method. The functions
*   deriv_att(), deriv_vel(), and deriv_alt() are described below.
*

```

```

*   The interval begins at the current frame minus 2 frames.
*

```

```

*   1. Compute the first estimate of the incremental value for
*       GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
*       rate of change at the beginning of the interval
*       (2 frames ago):
*

```

```

*       estimate      := rate_of_change * step_size

```

```

*****

```

```

att_k1 := deriv_att(GP_ATTITUDE[1, 1, 2], 2) * 2*DELTA_T
vel_k1 := deriv_vel(GP_VELOCITY[1, 2],
                    GP_ATTITUDE[1, 1, 2], 2) * 2*DELTA_T
alt_k1 := deriv_alt(GP_ALTITUDE[2],
                    GP_VELOCITY[1, 2],
                    GP_ATTITUDE[1, 1, 2], 2) * 2*DELTA_T

```

```

(*****

```

```

*   2. Compute the second estimate of the incremental value for

```

```

*      GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
*      rate of change at the midpoint of the first estimate k1:
*****)

att_k2 := deriv_att((GP_ATTITUDE[1, 1, 2] + att_k1/2), 1) * 2*DELTA_T
vel_k2 := deriv_vel((GP_VELOCITY[1, 2] + vel_k1/2),
                    (GP_ATTITUDE[1, 1, 2] + att_k1/2), 1) * 2*DELTA_T
alt_k2 := deriv_alt((GP_ALTITUDE[2] + alt_k1/2),
                    (GP_VELOCITY[1, 2] + vel_k1/2),
                    (GP_ATTITUDE[1, 1, 2] + att_k1/2), 1) * 2*DELTA_T

(*****
* 3. Compute the third estimate of the incremental value for
*      GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
*      rate of change at the midpoint of the second estimate k2:
*****)

att_k3 := deriv_att((GP_ATTITUDE[1, 1, 2] + att_k2/2), 1) * 2*DELTA_T
vel_k3 := deriv_vel((GP_VELOCITY[1, 2] + vel_k2/2),
                    (GP_ATTITUDE[1, 1, 2] + att_k2/2), 1) * 2*DELTA_T
alt_k3 := deriv_alt((GP_ALTITUDE[2] + alt_k2/2),
                    (GP_VELOCITY[1, 2] + vel_k2/2),
                    (GP_ATTITUDE[1, 1, 2] + att_k2/2), 1) * 2*DELTA_T

(*****
* 4. Compute the fourth estimate of the incremental value for
*      GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
*      the rate-of-change at the third estimate k3:
*****)

att_k4 := deriv_att((GP_ATTITUDE[1, 1, 2] + att_k3), 0) * 2*DELTA_T
vel_k4 := deriv_vel((GP_VELOCITY[1, 2] + vel_k3),
                    (GP_ATTITUDE[1, 1, 2] + att_k3), 0) * 2*DELTA_T
alt_k4 := deriv_alt((GP_ALTITUDE[2] + alt_k3),
                    (GP_VELOCITY[1, 2] + vel_k3),
                    (GP_ATTITUDE[1, 1, 2] + att_k3), 0) * 2*DELTA_T

(*****
* 5. Perform a weighted average of the four previously computed
*      estimates of the new value for GP_ATTITUDE, GP_VELOCITY, and
*      GP_ALTITUDE.
*
* Note, the syntax [* , x] and [* , *, x] represent the xth history of
* the data element.
*****)

GP_ATTITUDE[* , *, 0] := GP_ATTITUDE[* , *, 2] +
                        (1/6)(att_k1 + 2*(att_k2 + att_k3) + att_k4)

GP_VELOCITY[* , 0] := GP_VELOCITY[* , 2] +
                      (1/6)(vel_k1 + 2*(vel_k2 + vel_k3) + vel_k4)

GP_ALTITUDE[0] := GP_ALTITUDE[2] +
                  (1/6)(alt_k1 + 2*(alt_k2 + alt_k3) + alt_k4)

(** establish the "final" rotation matrix **)

```



```

GP_ROTATION[1, 1] := 0
GP_ROTATION[1, 2] := G_ROTATION[3, 0]
GP_ROTATION[1, 3] := -G_ROTATION[2, 0]
GP_ROTATION[2, 1] := -G_ROTATION[3, 0]
GP_ROTATION[2, 2] := 0
GP_ROTATION[2, 3] := G_ROTATION[1, 0]
GP_ROTATION[3, 1] := G_ROTATION[2, 0]
GP_ROTATION[3, 2] := -G_ROTATION[1, 0]
GP_ROTATION[3, 3] := 0

```

```

(*****
* 3) Determine if the engines should be switched on or off.
*****)

```

```

(*****
* At the beginning of the trajectory, the axial engines are "off"
* and the roll engines are "on." During the course of the
* trajectory the axial engines are "switched on." Further along
* the course of the trajectory, the axial engines and the roll
* engines are "switched off." These engine "switching" decisions
* are made here.
*****)

```

```

(** range check the current altitude **)

```

```

if (GP_ALTITUDE[0] < 0) [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
    "GP GP", FRAME_COUNTER,
    "GP_ALTITUDE", GP_ALTITUDE[0])
else if (GP_ALTITUDE[0] > 2000) [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
    "GP GP", FRAME_COUNTER,
    "GP_ALTITUDE", GP_ALTITUDE[0])
end if [1]

```

```

(** range check the current x-axis vehicle velocity **)

```

```

if (GP_VELOCITY[1, 0] < -100) [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
    "GP GP", FRAME_COUNTER,
    "GP_VELOCITY", GP_VELOCITY[1, 0])
else if (GP_VELOCITY[1, 0] > 100) [1]
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
    "GP GP", FRAME_COUNTER,
    "GP_VELOCITY", GP_VELOCITY[1, 0])
end if [1]

```

```

(** **)

```

```

if (AE_SWITCH = 0) then (* axial engines are "off" *) [1]
  if (RE_SWITCH = 1) then (* engines not prev. "off" *) [2]
    if (TD_SENSED = 0) then (* touch down "not sensed" *) [3]
      if (GP_ALTITUDE[0] <= ENGINES_ON_ALTITUDE) then [4]

```

```

        AE_SWITCH := 1          (* switch axial engines "on" *)
        FRAME_ENGINES_IGNITED := FRAME_COUNTER
    end if                                {4}
end if                                    {3}
end if                                    {2}

else                                       (* axial engines are "on" *) {1}
    if (TD_SENSED = 1) then                (* touch down "sensed" *) {2}
        AE_SWITCH := 0                    (* switch axial engines "off"*)
        RE_SWITCH := 0                    (* switch roll engines "off" *)

    else                                    (* touch down "not sensed" *) {2}
        if (GP_ALTITUDE[0] <= DROP_HEIGHT) then {3}
            temp := 2*GRAVITY*maximum(GP_ALTITUDE[0],0)

            if (temp < 0) then              {4}
                display-error("%EXCEPTIONAL-CONDITION-GCS-NEGATIVE_SQUARE_ROOT",
                    "GP GP", FRAME_COUNTER,
                    temp)
            end if                          {4}

            if (sqrt(temp)+GP_VELOCITY[1,0] <= MAX_NORMAL_VELOCITY) then {4}
                AE_SWITCH := 0              (* switch axial engines "off"*)
                RE_SWITCH := 0              (* switch roll engines "off" *)
            end if                          {4}
        end if                              {3}
    end if                                  {2}
end if                                     {1}

(*****
* 4) Compute the current velocity error.
*
* For a more detailed description of the interpolation and extrapolation
* algorithms, see the section labeled "" in the design overview.
*****)

(***) compute the optimal velocity (***)

(***) convert GP_ALTITUDE from meters to kilometers (***)

    cur_altitude := GP_ALTITUDE[0] / 1000

    do for i := 1 to 100                    {1}
        if (CONTOUR_ALTITUDE[i] = cur_altitude) then {2}

(***) found an exact match in the table (***)

            optimal_velocity := CONTOUR_VELOCITY(i)

            i := 101                        (* early do loop exit *)

        else if (CONTOUR_ALTITUDE[i] > cur_altitude) then {2}
            if (i > 1) then {3}

(***) interpolate between i-1 and i (***)

```

```

(** check for potential divide by zero condition **)

    if (CONTOUR_ALTITUDE[i] = CONTOUR_ALTITUDE[i-1]) then      {4}
        display-error("%EXCEPTIONAL-CONDITION-GCS-DIVIDE_BY_ZERO",
                      "GP GP", FRAME_COUNTER)
    end if                                                         {4}

(** interpolation formula **)

    optimal_velocity := CONTOUR_VELOCITY[i-1] +
        ((CONTOUR_VELOCITY[i] - CONTOUR_VELOCITY[i-1]) /
         (CONTOUR_ALTITUDE[i] - CONTOUR_ALTITUDE[i-1])) *
        (cur_altitude - CONTOUR_ALTITUDE[i-1])

    i := 101                                                         (* early do loop exit *)

    else (* i = 1 and altitude < table entry *)                    {3}

(** Extrapolate for altitude < smallest value in table entries **)

(** check for potential divide by zero condition **)

    if (CONTOUR_ALTITUDE[2] = CONTOUR_ALTITUDE[1]) then      {4}
        display-error("%EXCEPTIONAL-CONDITION-GCS-DIVIDE_BY_ZERO",
                      "GP GP", FRAME_COUNTER)
    end if                                                         {4}

(** Extrapolation formula **)

    optimal_velocity := CONTOUR_VELOCITY[1] -
        ((CONTOUR_VELOCITY[2] - CONTOUR_VELOCITY[1]) /
         (CONTOUR_ALTITUDE[2] - CONTOUR_ALTITUDE[1])) *
        (CONTOUR_ALTITUDE[1] - cur_altitude)

    i := 101                                                         (* early do loop exit *)

    end if                                                         {3}

    else (* CONTOUR_ALTITUDE[i] < cur_altitude *)                {2}

        if ((CONTOUR_ALTITUDE[i] = 0) OR (i = 100)) then        {3}

(** Extrapolate for altitude > largest value in table entries **)
(** note, i points to first (lowest) "0" entry in the table **)

(** check for potential divide by zero condition **)

            if (CONTOUR_ALTITUDE[i-1] = CONTOUR_ALTITUDE[i-2]) then {4}
                display-error("%EXCEPTIONAL-CONDITION-GCS-DIVIDE_BY_ZERO",
                              "GP GP", FRAME_COUNTER)
            end if                                                         {4}

(** Extrapolation formula **)

            optimal_velocity := CONTOUR_VELOCITY[i-1] +
                ((CONTOUR_VELOCITY[i-1] - CONTOUR_VELOCITY[i-2]) /

```

```

                (CONTOUR_ALTITUDE[i-1] - CONTOUR_ALTITUDE[i-2]) *
                (cur_altitude - CONTOUR_ALTITUDE[i-1])

        i := 101                                (* early do loop exit *)

    end if                                     {3}

end if                                       {2}
end do                                       {1}

(** convert optimal_velocity from km/sec to m/sec **)

    optimal_velocity := optimal_velocity * 1000

(** compute the velocity error **)

    VELOCITY_ERROR := GP_VELOCITY[1, 0] - optimal_velocity

(*****
 * 5) Determine if the predetermined velocity-altitude contour has
 *   been crossed.
 *****)

(** range check the VELOCITY_ERROR ****)

    if (VELOCITY_ERROR < -300)                {1}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "GP GP", FRAME_COUNTER,
                      "VELOCITY_ERROR", VELOCITY_ERROR)

    else if (VELOCITY_ERROR > 20)             {1}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "GP GP", FRAME_COUNTER,
                      "VELOCITY_ERROR", VELOCITY_ERROR)

    end if                                    {1}

    if (GP_ALTITUDE[0] <= ENGINES_ON_ALTITUDE) then {1}
        if (CONTOUR_CROSSED = 0) then (* "contour not crossed" *) {2}
            if (VELOCITY_ERROR >= 0) then {3}
                CONTOUR_CROSSED := 1 (* set "contour crossed" *)
            end if {3}
        end if {2}
    end if {1}

(*****
 * 6) Determine the current guidance phase.
 *****)

    case GP_PHASE of

(** trans from 1 to 2 when the "engines on altitude" is reached **)

        1:   if (GP_ALTITUDE[0] <= ENGINES_ON_ALTITUDE) then {1}
                GP_PHASE := 2
            end if {1}
        end {of case 1}

```

(\*\*\* trans from 2 to 5 when touch down is sensed \*\*\*)

```

2:   if (TD_SENSED = 1) then      (* "touch down sensed" *)      {1}
      GP_PHASE := 5
    else                          {1}

```

(\*\*\* trans from 2 to 3 when the engines are hot and the chute is released \*\*\*)

```

      if (AE_TEMP = 2) then        (* a-engines are "hot" *) {2}
        if (CHUTE_RELEASED = 1) then (* "chute released" *) {3}
          GP_PHASE := 3
        end if                      {3}
      end if                          {2}
    end if                              {1}

```

end [of case 2]

(\*\*\* trans from 3 to 5 when touch down is sensed \*\*\*)

```

3:   if (TD_SENSED = 1) then      (* touch down "sensed" *)      {1}
      GP_PHASE := 5
    else                          (* touch down "not sensed" *) {1}

```

(\*\*\* trans from 3 to 5 when the TD sensor fails and altitude too low \*\*\*)

(\*\*\* trans from 3 to 4 when the TD sensor healthy and altitude too low \*\*\*)

```

      if (GP_ALTITUDE[0] =< DROP_HEIGHT) then (* too low *) {2}
        if (TDS_STATUS = 1) then          (* sensor "failed"*) {3}
          GP_PHASE := 5
        else                              (* sensor "healthy" *) {3}
          temp := 2*GRAVITY*maximum(GP_ALTITUDE[0],0)
          if (temp < 0) then                {4}
            display-error("%EXCEPTIONAL-CONDITION-GCS-NEGATIVE_SQUARE_ROOT",
              "GP GP", FRAME_COUNTER,
              temp)
          end if                            {4}
          if (sqrt(temp)+GP_VELOCITY[1,0] <=
            MAX_NORMAL_VELOCITY) then      {4}
            GP_PHASE := 4
          end if                            {4}
        end if                              {3}
      end if                              {2}
    end if                                  {1}

```

end [of case 3]

(\*\*\* trans from 4 to 5 when touch down is sensed \*\*\*)

```

4:   if (TD_SENSED = 1) then      (* touch down "sensed" *)      {1}
      GP_PHASE := 5

```

```

        else                                (* touch down "not sensed" *)  {1}

(** trans from 4 to 5 when the TD sensor fails **)

        if (TDS_STATUS = 1) then          (* sensor "failed"*)          {2}
            GP_PHASE := 5
        end if                             {2}
    end if                                 {1}

    end {of case 4}

end of case statement

(*****
 * 7) Determine the appropriate axial engine control law parameter index.
 *****)

(** Note, the optimal_velocity is computed above during the computing of
    the current velocity error.          ***)

    if (CL = 1) then                       {1}
        if (optimal_velocity = DROP_SPEED) then {2}
            if (GP_VELOCITY[1, 0] < DROP_SPEED) then {3}
                CL := 2
                TE_INTEGRAL := 0
            end if                             {3}
        end if                               {2}
    end if                                 {1}

return

(*****
 * Title: deriv_att
 * Description:
 *     Compute the derivative of the vehicle attitude.
 *
 * Usage:
 *     rate-of-change := deriv_att(attitude, i)
 *
 * Arguments:
 *     attitude input pointer to longword array[1..3, 1..3]
 *     i         input          longword integer    - time history index
 *
 *     where
 *         pv := G_ROTATION[1, i]
 *         qv := G_ROTATION[2, i]
 *         rv := G_ROTATION[3, i]
 *****)

    deriv_att :=
        -      -
        |  0   rv  -qv |
        | -rv   0   pv | x attitude
        |  qv  -pv   0  |
        -      -

return

```

```

(*****
* Title: deriv_vel
* Description:
*   Compute the derivative of the vehicle velocity.
*
* Usage:
*   rate-of-change := deriv_vel(velocity, attitude, i)
*
* Arguments:
*   velocity input pointer to longword array[1..3]
*   attitude input pointer to longword array[1..3, 1..3]
*   i       input          longword integer    - time history index
*****)

```

$$\text{deriv\_vel} := \begin{bmatrix} 0 & rv & -qv \\ -rv & 0 & pv \\ qv & -pv & 0 \end{bmatrix} \times \text{velocity} +$$

$$\begin{bmatrix} \text{GRAVITY} * \text{attitude}[1,3] + \text{A\_ACCELERATION}[1,i] \\ \text{GRAVITY} * \text{attitude}[2,3] + \text{A\_ACCELERATION}[2,i] \\ \text{GRAVITY} * \text{attitude}[3,3] + \text{A\_ACCELERATION}[3,i] \end{bmatrix} +$$

$$\text{K\_MATRIX}[i] \times \begin{bmatrix} \text{TDLR\_VELOCITY}[1,i] - \text{velocity}[1] \\ \text{TDLR\_VELOCITY}[2,i] - \text{velocity}[2] \\ \text{TDLR\_VELOCITY}[3,i] - \text{velocity}[3] \end{bmatrix}$$

where

```

pv := G_ROTATION[1, i]
qv := G_ROTATION[2, i]
rv := G_ROTATION[3, i]

```

(\* note that "K\_MATRIX[i]" represents the "i" history of the 3x3 matrix \*)

return

```

(*****
* Title: deriv_alt
* Description:
*   Compute the derivative of the vehicle altitude.
*
* Usage:
*   rate-of-change := deriv_att(attitude, i)
*
* Arguments:
*   altitude input          longword real
*   velocity input pointer to longword array[1..3]
*   attitude input pointer to longword array[1..3, 1..3]
*   i       input          longword integer    - time history index
*****)

```

deriv\_alt =

$$\begin{array}{c} - \\ | -attitude[1,3] \ -attitude[2,3] \ -attitude[3,3] | \\ - \end{array} \times \text{velocity} +$$

K\_ALT[i] \* (AR\_ALTITUDE[i] - altitude)

END P\_SPEC



**NAME:**

2.3;2

**TITLE:**

CP

**INPUT/OUTPUT:**

CP\_EXT\_IN : data\_in

CP\_SO\_IN : data\_in

CP\_GS\_IN : data\_in

COMM\_SYNC\_PATTERN : data\_in

PACKET : data\_out

C\_STATUS : data\_out

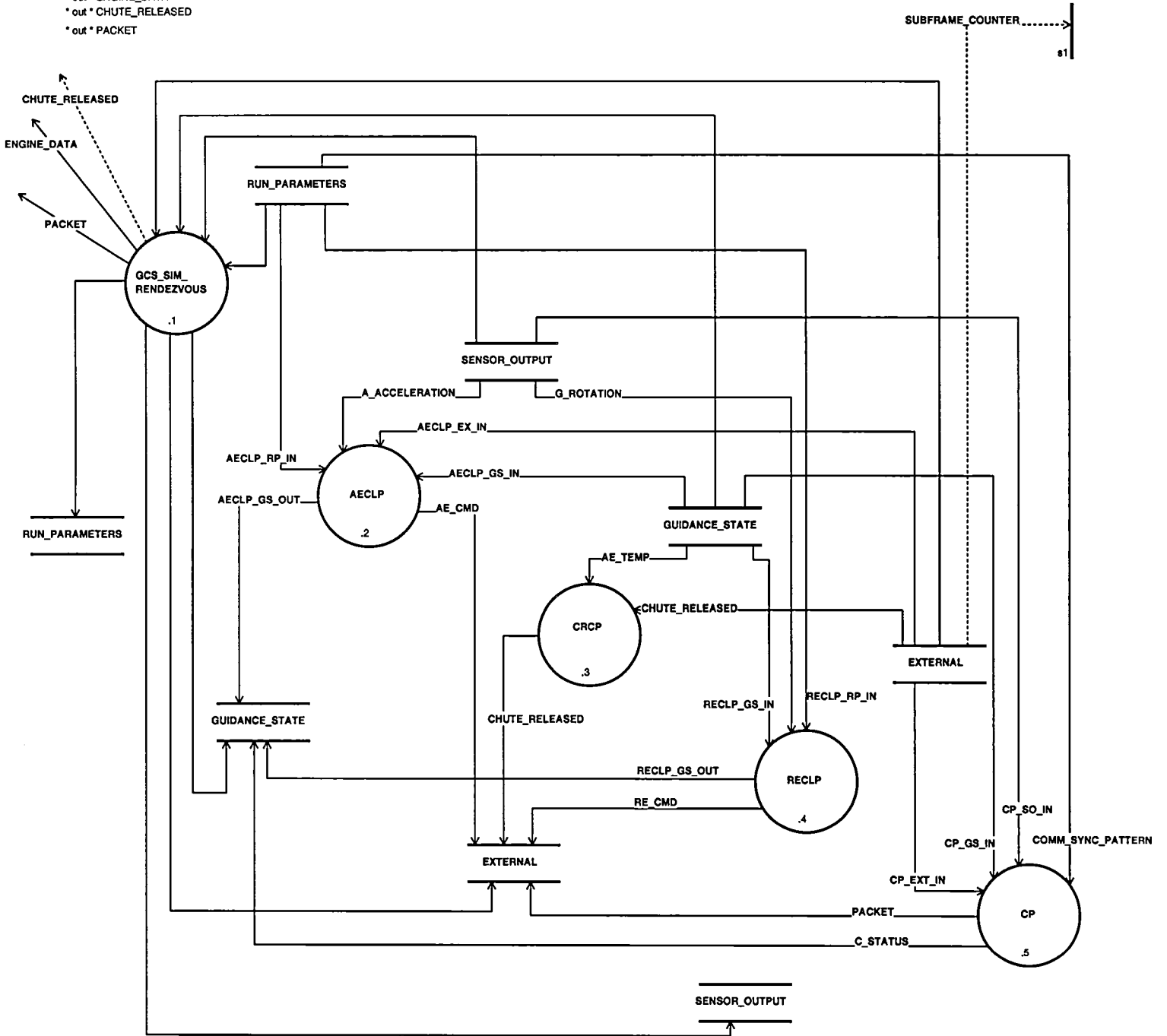
**BODY:**

Bubbles 1.8, 2.3, 3.5 and the associated P-Specs represent a single process, CP as described in P-Spec 1.8.



3:9  
Control Law Processing Subframe

\* out \* ENGINE\_DATA  
\* out \* CHUTE\_RELEASED  
\* out \* PACKET



3-s1;2

PAT - Control Law Processing Subframe

SUBFRAME_COUNTER	"GCS_SIM_RENDEZVOUS"	"AECLP"	"CRCP"	"RECLP"	"CP"
"3"	1	2	3	2	4

**NAME:**

3.1;4

**TITLE:**

GCS\_SIM\_RENDEZVOUS

**INPUT/OUTPUT:**

**EXTERNAL : data\_in**

**GUIDANCE\_STATE : data\_in**

**SENSOR\_OUTPUT : data\_in**

**RUN\_PARAMETERS : data\_in**

**GUIDANCE\_STATE : data\_out**

**EXTERNAL : data\_out**

**SENSOR\_OUTPUT : data\_out**

**RUN\_PARAMETERS : data\_out**

**ENGINE\_DATA: data\_out**

**PACKET: data\_out**

**CHUTE\_RELEASED : data\_out**

**BODY:**

BEGIN P-Spec

GCS\_SIM\_RENDEZVOUS provides the interface to the vehicle. This module is provided by the systems group.

Bubbles 1.1, 2.1, 3.1 and the associated P-Specs represent a single process.

END P-Spec

**NAME:**

3.1;4

**TITLE:**

GCS\_SIM\_RENDEZVOUS

**INPUT/OUTPUT:**

**EXTERNAL : data\_in**

**GUIDANCE\_STATE : data\_in**

**SENSOR\_OUTPUT : data\_in**

**RUN\_PARAMETERS : data\_in**

**GUIDANCE\_STATE : data\_out**

**EXTERNAL : data\_out**

**SENSOR\_OUTPUT : data\_out**

**RUN\_PARAMETERS : data\_out**

**ENGINE\_DATA : data\_out**

**PACKET : data\_out**

**CHUTE\_RELEASED : data\_out**

**BODY:**

BEGIN P-Spec

GCS\_SIM\_RENDEZVOUS provides the interface to the vehicle. This module is provided by the systems group.

Bubbles 1.1, 2.1, 3.1 and the associated P-Specs represent a single process.

END P-Spec



**NAME:**

3.2;40

**TITLE:**

AECLP

**INPUT/OUTPUT:****AE\_SWITCH :data\_in****AE\_TEMP :data\_in****A\_ACCELERATION :data\_in****CHUTE\_RELEASED :data\_in****CL :data\_in****CONTOUR\_CROSSED :data\_in****DELTA\_T :data\_in****ENGINES\_ON\_ALTITUDE :data\_in****FRAME\_COUNTER :data\_in****FRAME\_ENGINES\_IGNITED :data\_in****FULL\_UP\_TIME :data\_in****GA :data\_in****GAX :data\_in****GP1 :data\_in****GP2 :data\_in****GPY :data\_in****GP\_ALTITUDE :data\_in****GP\_ATTITUDE :data\_in****GP\_ROTATION :data\_in****GP\_VELOCITY :data\_in****GQ :data\_in****GR :data\_in****GRAVITY :data\_in****GV :data\_in****GVE :data\_in**



**GVEI :data\_in**

**GVI :data\_in**

**GW :data\_in**

**GW I :data\_in**

**INTERNAL\_CMD: data\_in**

**OMEGA :data\_in**

**PE\_INTEGRAL :data\_in**

**PE\_MAX :data\_in**

**PE\_MIN :data\_in**

**TE\_DROP :data\_in**

**TE\_INIT :data\_in**

**TE\_INTEGRAL :data\_in**

**TE\_LIMIT :data\_in**

**TE\_MAX :data\_in**

**TE\_MIN :data\_in**

**VELOCITY\_ERROR :data\_in**

**YE\_INTEGRAL :data\_in**

**YE\_MAX :data\_in**

**YE\_MIN :data\_in**

**AE\_CMD :data\_out**

**AE\_STATUS :data\_out**

**AE\_TEMP :data\_out**

**INTERNAL\_CMD :data\_out**

**PE\_INTEGRAL :data\_out**

**TE\_INTEGRAL :data\_out**

**TE\_LIMIT :data\_out**

**YE\_INTEGRAL :data\_out**

**BODY:**

BEGIN P\_SPEC

```

(*****
* AECLP -- Axial Engine Control Law Processing
*
* AECLP processing is responsible for:
* 1) determining the current operational status of the axial engines, and
* 2) generating the appropriate axial engine commands.
*****)

(*****
* 1) Determine the current operational status of the axial engines.
*
* The operational status of the axial engines is always reported
* as "Healthy" (value 0).
*****)

    AE_STATUS := 0

(*****
* 2) Generate the appropriate axial engine commands.
*
* Determine if the axial engines are on. If the axial engines
* are "off" (value 0) then the axial engine commands are "0".
* Otherwise, further processing is required in order to determine
* the appropriate axial engine commands.
*****)

    if (AE_SWITCH = 0) then          (* axial engines are off *)    {1}
        AE_CMD[1] := 0
        AE_CMD[2] := 0
        AE_CMD[3] := 0

    else                               {1}

(*****
* The axial engines are "on" so further processing is required.
*
* 2A) determine the axial engine temperature.
*****)

(** range check the current altitude **)

    if (GP_ALTITUDE[0] < 0) then      {2}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "GP_ALTITUDE", GP_ALTITUDE[0])

    else if (GP_ALTITUDE[0] > 2000) then {2}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "GP_ALTITUDE", GP_ALTITUDE[0])

    end if                               {2}

(*****

```

```

* The three possible engine temperature states are: "Cold" (value 0),
* "Warming up" (value 1), and "Hot" (value 2). The current temperature
* of the axial engines is stored in the data element AE_TEMP.
*****)

    if (GP_ALTITUDE[0] <= ENGINES_ON_ALTITUDE) then           [2]

        if (AE_TEMP = 0) then                                [3]
            (* engines are "Cold" *)

            if ((FRAME_COUNTER - FRAME_ENGINES_IGNITED) * DELTA_T <
                FULL_UP_TIME) then                           [4]
                AE_TEMP := 1                                (* "Warming up" *)
            end if                                           [4]

        else if (AE_TEMP = 1) then                            [3]
            (* engines are "Warming up" *)

            if ((FRAME_COUNTER - FRAME_ENGINES_IGNITED) * DELTA_T >=
                FULL_UP_TIME) then                           [4]
                AE_TEMP := 2                                (* "Hot" *)
            end if                                           [4]

        end if                                               [3]

    end if                                                    [2]

(*****
* 2B) Compute the pitch error limit.
*****)

(***) range check the pitch error integral (***)

    if (PE_INTEGRAL < -100) then                             [2]
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "PE_INTEGRAL", PE_INTEGRAL)

    else if (PE_INTEGRAL > 100) then                         [2]
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "PE_INTEGRAL", PE_INTEGRAL)

    end if                                                    [2]

(***) range check the x-axis roll rate (***)

    if (GP_VELOCITY[1, 0] < -100) then                      [2]
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "x-axis GP_VELOCITY", GP_VELOCITY[1, 0])

    else if (GP_VELOCITY[1, 0] > 100) then                  [2]
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
            "AECLP AECLP", FRAME_COUNTER,
            "x-axis GP_VELOCITY", GP_VELOCITY[1, 0])

    end if                                                    [2]

(***) range check the z-axis roll rate (***)

```

```

if (GP_VELOCITY[3, 0] < -100) then                                {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "z-axis GP_VELOCITY", GP_VELOCITY[3, 0])

else if (GP_VELOCITY[3, 0] > 100) then                          {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "z-axis GP_VELOCITY", GP_VELOCITY[3, 0])
end if                                                            {2}

(** check for potential divide by zero condition **)

if (GP_VELOCITY[1, 0] = 0) then                                  {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-DIVIDE_BY_ZERO",
               "AECLP AECLP", FRAME_COUNTER,
               "x-axis GP_VELOCITY")
end if                                                            {2}

(** compute the current value for PE_INTEGRAL **)

PE_INTEGRAL := PE_INTEGRAL +
              (GP_VELOCITY[3, 0] / ABS(GP_VELOCITY[1, 0])) * DELTA_T

  where "ABS()" represents the absolute value operation

(** range check the pitch error integral (again) **)

if (PE_INTEGRAL < -100) then                                    {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "PE_INTEGRAL", PE_INTEGRAL)

else if (PE_INTEGRAL > 100) then                                {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "PE_INTEGRAL", PE_INTEGRAL)
end if                                                            {2}

(** range check the pitch rotational displacement **)

if (GP_ROTATION[3, 1] < -1) then                                 {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "GP_ROTATION", GP_ROTATION[3, 1])

else if (GP_ROTATION[3, 1] > 1) then                             {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "GP_ROTATION", GP_ROTATION[3, 1])
end if                                                            {2}

(** compute the pitch error limit **)

pitch_error_limit := GQ[CL] * GP_ROTATION[3, 1] +

```

```

        GW[CL] * (GP_VELOCITY[3, 0] / ABS(GP_VELOCITY[1, 0])) +
        GWI[CL] * PE_INTEGRAL

if (pitch_error_limit < PE_MIN[CL]) then                                {2}
    pitch_error_limit := PE_MIN[CL]

else if (pitch_error_limit > PE_MAX[CL]) then                          {2}
    pitch_error_limit := PE_MAX[CL]

end if                                                                    {2}

(*****
* 2C) Compute the yaw error limit.
*****)

(***) range check the yaw error integral (***)

if (YE_INTEGRAL < -100) then                                            {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "YE_INTEGRAL", YE_INTEGRAL)

else if (YE_INTEGRAL > 100) then                                        {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "YE_INTEGRAL", YE_INTEGRAL)

end if                                                                    {2}

(***) range check the y-axis roll rate (***)

if (GP_VELOCITY[2, 0] < -100) then                                      {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "y-axis GP_VELOCITY", GP_VELOCITY[2, 0])

else if (GP_VELOCITY[2, 0] > 100) then                                  {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "y-axis GP_VELOCITY", GP_VELOCITY[2, 0])

end if                                                                    {2}

(***) check for potential divide by zero condition (***)

if (GP_VELOCITY[1, 0] = 0) then                                        {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-DIVIDE_BY_ZERO",
                  "AECLP AECLP", FRAME_COUNTER,
                  GP_VELOCITY[1, 0])

end if                                                                    {2}

(***) Compute the current value for YE_INTEGRAL (***)

YE_INTEGRAL := YE_INTEGRAL +
              (GP_VELOCITY[2, 0] / ABS(GP_VELOCITY[1, 0])) * DELTA_T

(***) range check the yaw error integral (again) (***)

```

```

if (YE_INTEGRAL < -100) then                                {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "YE_INTEGRAL", YE_INTEGRAL)

else if (YE_INTEGRAL > 100) then                            {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "YE_INTEGRAL", YE_INTEGRAL)

end if                                                       {2}

(** range check the yaw rotational displacement **)

if (GP_ROTATION[1, 2] < -1) then                             {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "GP_ROTATION", GP_ROTATION[1, 2])

else if (GP_ROTATION[1, 2] > 1) then                         {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "GP_ROTATION", GP_ROTATION[1, 2])

end if                                                       {2}

(** compute the yaw error limit **)

yaw_error_limit := -GR[CL] * GP_ROTATION[1, 2] +
                  GV[CL] * (GP_VELOCITY[2, 0] / ABS(GP_VELOCITY[1, 0])) +
                  GVI[CL] * YE_INTEGRAL

if (yaw_error_limit < YE_MIN[CL]) then                       {2}
  yaw_error_limit := YE_MIN[CL]

else if (yaw_error_limit > YE_MAX[CL]) then                 {2}
  yaw_error_limit := YE_MAX[CL]

end if                                                       {2}

(*****
 * 2D) Compute the thrust limiting error.
 *****)

if (CONTOUR_CROSSED = 1)      (* "contour crossed" *)      {2}

(** range check the thrust error integral **)

if (TE_INTEGRAL < -100) then                                {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "TE_INTEGRAL", TE_INTEGRAL)

else if (TE_INTEGRAL > 100) then                            {3}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "AECLP AECLP", FRAME_COUNTER,
               "TE_INTEGRAL", TE_INTEGRAL)

end if                                                       {3}

```

```
(** range check the velocity error **)

    if (VELOCITY_ERROR < -300) then                                {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "VELOCITY_ERROR", VELOCITY_ERROR)

    else if (VELOCITY_ERROR > 20) then                            {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "VELOCITY_ERROR", VELOCITY_ERROR)
    end if                                                         {3}

(** Compute the current value for TE_INTEGRAL **)

    TE_INTEGRAL := TE_INTEGRAL + VELOCITY_ERROR * DELTA_T

(** range check the thrust error integral (again) **)

    if (TE_INTEGRAL < -100) then                                  {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "TE_INTEGRAL", TE_INTEGRAL)

    else if (TE_INTEGRAL > 100) then                              {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "TE_INTEGRAL", TE_INTEGRAL)
    end if                                                         {3}

(** range check the attitude component **)

    if (GP_ATTITUDE[1, 3, 0] < -1) then                           {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "GP_ATTITUDE", GP_ATTITUDE[1, 3, 0])

    else if (GP_ATTITUDE[1, 3, 0] > 1) then                       {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "GP_ATTITUDE", GP_ATTITUDE[1, 3, 0])
    end if                                                         {3}

(** range check the x-axis acceleration **)

    if (A_ACCELERATION[1, 0] < -20) then                          {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "x-axis A_ACCELERATION", A_ACCELERATION[1, 0])

    else if (A_ACCELERATION[1, 0] > 5) then                       {3}
        display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                      "AECLP AECLP", FRAME_COUNTER,
                      "x-axis A_ACCELERATION", A_ACCELERATION[1, 0])
    end if                                                         {3}
```

```

(** range check the thrust error limit **)

  if (TE_LIMIT < -100) then                                     {3}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "TE_LIMIT", TE_LIMIT)

  else if (TE_LIMIT > 100) then                                {3}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "TE_LIMIT", TE_LIMIT)

  end if                                                       {3}

(*****
 * Section "Algorithms not specified in GCS Development
 * Specification" of the Design Overview contains a derivation of
 * the following equation used to compute TE_LIMIT.
 *****)

  let e := 2.718281828459045                                  { the number "e" }

  TE_LIMIT := (q / OMEGA) +
              (TE_LIMIT - (q / OMEGA)) * e^(-OMEGA * DELTA_T)

  where q := GA * (-GAX * (A_ACCELERATION[1, 0] + GRAVITY *
                        GP_ATTITUDE[1, 3, 0]) + GVE * VELOCITY_ERROR +
              GVEI[CL] * TE_INTEGRAL)

(** range check the current value of for the thrust error limit **)

  if (TE_LIMIT < -100) then                                     {3}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "TE_LIMIT", TE_LIMIT)

  else if (TE_LIMIT > 100) then                                {3}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "TE_LIMIT", TE_LIMIT)

  end if                                                       {3}

  if (TE_LIMIT < TE_MIN[CL]) then                              {3}
    TE_LIMIT := TE_MIN[CL]

  else if (TE_LIMIT > TE_MAX[CL]) then                          {3}
    TE_LIMIT := TE_MAX[CL]

  end if                                                       {3}

end if                                                         {2}

(*****
 * 2E) Compute the pitch, yaw and thrust errors.
 *****)

```



```

(** Note, to get here (AE_SWITCH = 1) **)

  if (CHUTE_RELEASED = 1) then      (* "Chute Released" *)      {2}

    if (CONTOUR_CROSSED = 0) then  (* "contour not crossed" *)  {3}
      pitch_error := pitch_limiting_error
      yaw_error   := yaw_limiting_error
      thrust_error := TE_DROP

    else                            (* "contour crossed" *)      {3}
      pitch_error := pitch_limiting_error
      yaw_error   := yaw_limiting_error
      thrust_error := TE_LIMIT

    end if                            {3}

  else                                (* "Chute Attached" *)
    pitch_error := GQ[CL] * GP_ROTATION[3, 1]
    yaw_error   := -GR[CL] * GP_ROTATION[1, 2]
    thrust_error := TE_INIT

  end if                                {2}

(*****
* 2F) Compute the axial engine value settings.
*****)

INTERNAL_CMD[1] := GP1 * pitch_error          + thrust_error
INTERNAL_CMD[2] := GP2 * pitch_error - GPY * yaw_error + thrust_error
INTERNAL_CMD[3] := GP2 * pitch_error + GPY * yaw_error + thrust_error

(*****
* 2G) Convert the axial engine value settings to engine commands.
*****)

(** range check the internal command **)

  if (INTERNAL_CMD[1] < -0.7) then      {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "INTERNAL_CMD[1]", INTERNAL_CMD[1])

  else if (INTERNAL_CMD[1] > 1.7) then  {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "INTERNAL_CMD[1]", INTERNAL_CMD[1])

  end if                                {2}

  if (INTERNAL_CMD[2] < -0.7) then      {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "INTERNAL_CMD[2]", INTERNAL_CMD[2])

  else if (INTERNAL_CMD[2] > 1.7) then  {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "AECLP AECLP", FRAME_COUNTER,
                  "INTERNAL_CMD[2]", INTERNAL_CMD[2])

```

```
end if {2}

if (INTERNAL_CMD[3] < -0.7) then {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
    "AECLP AECLP", FRAME_COUNTER,
    "INTERNAL_CMD[3]", INTERNAL_CMD[3])

else if (INTERNAL_CMD[3] > 1.7) then {2}
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
    "AECLP AECLP", FRAME_COUNTER,
    "INTERNAL_CMD[3]", INTERNAL_CMD[3])

end if {2}

(** first engine **)

if (INTERNAL_CMD[1] < 0) then {2}
  AE_CMD[1] := 0

else if (INTERNAL_CMD[1] <= 1) then {2}
  AE_CMD[1] := TRUNC(127 * INTERNAL_CMD[1] + 0.5)

  where TRUNC() represents the truncation operation
else {2}
  AE_CMD[1] := 127

end if {2}

(** second engine **)

if (INTERNAL_CMD[2] < 0) then {2}
  AE_CMD[2] := 0

else if (INTERNAL_CMD[2] <= 1) then {2}
  AE_CMD[2] := TRUNC(127 * INTERNAL_CMD[2] + 0.5)

else {2}
  AE_CMD[2] := 127

end if {2}

(** third engine **)

if (INTERNAL_CMD[3] < 0) then {2}
  AE_CMD[3] := 0

else if (INTERNAL_CMD[3] <= 1) then {2}
  AE_CMD[3] := TRUNC(127 * INTERNAL_CMD[3] + 0.5)

else {2}
  AE_CMD[3] := 127

end if {2}

end if {1}

END P_SPEC
```



**NAME:**

3.3;24

**TITLE:**

CRCP

**INPUT/OUTPUT:****AE\_TEMP** : data\_in**CHUTE\_RELEASED** :data\_in**CHUTE\_RELEASED**:data\_out**BODY:**

BEGIN P\_SPEC

```
(*****
* CRCP -- Chute Release Control Processing
*
* CRCP processing is responsible for:
* 1) Determining whether or not to release the parachute.
*****)

(*****
* The parachute is to be released during the same frame in which the
* axial engine temperature becomes "HOT" (2). Valid states for
* CHUTE_RELEASED are "Chute Attached" (0) and "Chute Released" (1).
*****)

(***) 1) Determine whether or not to release the parachute. (***)

    if (CHUTE_RELEASED = 0) then          (* Chute Attached *)          {1}

        if (AE_TEMP = 2) then            (* engines are "HOT" *)        {2}
            CHUTE_RELEASED := 1          (* release the chute *)        {2}
        end if                            {2}

    end if                                 {1}

END P_SPEC
```



**NAME:**

3.4;23

**TITLE:**

RECLP

**INPUT/OUTPUT:**

DELTA\_T : data\_in

G\_ROTATION : data\_in

P1 : data\_in

P2 : data\_in

P3 : data\_in

P4 : data\_in

RE\_SWITCH : data\_in

THETA : data\_in

THETA1 : data\_in

THETA2 : data\_in

RE\_CMD : data\_out

RE\_STATUS : data\_out

THETA : data\_out

**BODY:**

BEGIN P\_SPEC

```
(*****
* RECLP -- Roll Engine Control Law Processing
*
* RECLP processing is responsible for:
* 1) determining the current operational status of the roll engines, and
* 2) generating the appropriate roll engine command.
*****)

(*****
* 1) Determine the current operational status of the roll engines.
*
* The operational status of the roll engines is always reported
* as "healthy" (value 0).
*****)

    RE_STATUS := 0

(*****
* 2) Generate the appropriate roll engine command.
*
*****)
```

```

* Determine if the roll engines are on.  If the roll engines
* are "switched off" (value 0) then the roll engine command is "1".
*****)

if (RE_SWITCH = 0) then      (* roll engines are switched off *)      {1}
  RE_CMD := 1                (* off + cw *)
else                                                                    {1}

(** range check the x-axis vehicle rotation rate **)

  if (G_ROTATION[1 ,0] < -1.0) then                                     {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "RECLP RECLP", FRAME_COUNTER,
                  "x-axis G_ROTATION", G_ROTATION[1 ,0])

  else if (G_ROTATION[1 ,0] > 1.0) then                                 {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "RECLP RECLP", FRAME_COUNTER,
                  "x-axis G_ROTATION", G_ROTATION[1 ,0])
  end if                                                                {2}

(** range check the x-axis vehicle rotation displacement **)

  let pi := 3.14159265358979

  if (THETA < (0 - pi)) then                                          {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
                  "RECLP RECLP", FRAME_COUNTER,
                  "THETA", THETA)

  else if (THETA > pi) then                                           {2}
    display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
                  "RECLP RECLP", FRAME_COUNTER,
                  "THETA", THETA)
  end if                                                                {2}

(*****
* The roll engine command consists of two components: an
* intensity, and a direction.  Taking into account the command data
* encoding, the possible intensities are: Off (0), Minimum (2),
* Intermediate (4), and Maximum (6), and the possible directions
* are CounterClockwise (0) and Clockwise (1).
*
* Both roll engine command components are determined from the
* current value of the vehicle's roll rate and rotational
* displacement about the x-axis.
*
* Employing Euler's method for differential equations, compute the
* current x-axis angular displacement, theta.
*****)

  THETA      := THETA + G_ROTATION[1 ,0] * DELTA_T

(** range check the theta again before use **)

```

```

if (THETA < (0 - pi)) then                                     [2]
  display-error("%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED",
               "RECLP RECLP", FRAME_COUNTER,
               "THETA", THETA)

else if (THETA > pi) then                                     [2]
  display-error("%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED",
               "RECLP RECLP", FRAME_COUNTER,
               "THETA", THETA)
end if                                                         [2]

(*****
 * From figure 5.2 "Graph for Deriving Roll Engine Commands" of the
 * GCS development specifications, determine the appropriate roll
 * engine intensity and direction.
 *****)

(***) check case when theta = 0 (***)

  if (THETA = 0) then                                         [2]

    if (G_ROTATION[1 ,0] > P4) then                             [3]
      RE_CMD := 6 + 1                                         (* max + cw *)
    else if (G_ROTATION[1 ,0] < -P4) then                       [3]
      RE_CMD := 6 + 0                                         (* max + ccw *)
    else                                                         [3]
      RE_CMD := 0 + 1                                         (* off + cw *)
    end if                                                       [3]

(***) check first and fourth quadrants (***)

  else if (THETA > 0) then                                     [2]

    if (THETA <= THETA1) then                                   [3]

      if (G_ROTATION[1 ,0] > P2) then                             [4]
        RE_CMD := 6 + 1                                         (* max + cw *)
      else if (G_ROTATION[1 ,0] > P1) then                       [4]
        RE_CMD := 4 + 1                                         (* inter + cw *)
      else if (G_ROTATION[1 ,0] >= -P4) then                     [4]
        RE_CMD := 0 + 1                                         (* off + cw *)
      else                                                         [4]
        RE_CMD := 6 + 0                                         (* max + ccw *)
      end if                                                       [4]

    else if (THETA <= THETA2) then                               [3]

      if (G_ROTATION[1 ,0] > P2) then                             [4]
        RE_CMD := 6 + 1                                         (* max + cw *)
      else if (G_ROTATION[1 ,0] > P1) then                       [4]
        RE_CMD := 4 + 1                                         (* inter + cw *)
      else if (G_ROTATION[1 ,0] > 0.0) then                      [4]
        RE_CMD := 2 + 1                                         (* min + cw *)
      else if (G_ROTATION[1 ,0] >= -P4) then                     [4]
        RE_CMD := 0 + 1                                         (* off + cw *)
      else                                                         [4]

```



```

        RE_CMD := 6 + 0                                (* max + ccw *)
    end if                                             [4]

else (* THETA > THETA2 *)                             [3]

    if (G_ROTATION[1 ,0] > -P3) then                 [4]
        RE_CMD := 6 + 1                                (* max + cw *)
    else if (G_ROTATION[1 ,0] >= -P4) then           [4]
        RE_CMD := 0 + 1                                (* off + cw *)
    else                                             [4]
        RE_CMD := 6 + 0                                (* max + ccw *)
    end if                                           [4]

end if                                             [3]

(***) check second and third quadrants (***)

else (* THETA < 0 *)                                 [2]

    if (THETA >= -THETA1) then                       [3]

        if (G_ROTATION[1 ,0] > p4) then             [4]
            RE_CMD := 6 + 1                                (* max + cw *)
        else if (G_ROTATION[1 ,0] >= -P1) then       [4]
            RE_CMD := 0 + 1                                (* off + cw *)
        else if (G_ROTATION[1 ,0] >= -P2) then       [4]
            RE_CMD := 4 + 0                                (* inter + ccw *)
        else                                         [4]
            RE_CMD = 6 + 0                                (* max + ccw *)
        end if                                       [4]

    else if (THETA >= -THETA2) then                 [3]

        if (G_ROTATION[1 ,0] > P4) then             [4]
            RE_CMD := 6 + 1                                (* max + cw *)
        else if (G_ROTATION[1 ,0] >= 0.0) then       [4]
            RE_CMD = 0 + 1                                (* off + cw *)
        else if (G_ROTATION[1 ,0] >= -P1) then       [4]
            RE_CMD := 2 + 0                                (* min + ccw *)
        else if (G_ROTATION[1 ,0] >= -P2) then       [4]
            RE_CMD := 4 + 0                                (* inter + ccw *)
        else                                         [4]
            RE_CMD := 6 + 0                                (* max + ccw *)
        end if                                       [4]

    else (* THETA < -THETA2 *)                       [3]

        if (G_ROTATION[1 ,0] > P4) then             [4]
            RE_CMD := 6 + 1                                (* max + cw *)
        else if (G_ROTATION[1 ,0] >= P3) then       [4]
            RE_CMD := 0 + 1                                (* off + cw *)
        else                                         [4]
            RE_CMD = 6 + 0                                (* max + ccw *)
        end if                                       [4]

end if                                             [3]

```

end if

{2}

end if

{1}

END P\_SPEC

**NAME:**

3.5;2

**TITLE:**

CP

**INPUT/OUTPUT:****COMM\_SYNC\_PATTERN : data\_in****CP\_SO\_IN : data\_in****CP\_GS\_IN : data\_in****CP\_EXT\_IN : data\_in****PACKET : data\_out****C\_STATUS : data\_out****BODY:**

Bubbles 1.8, 2.3, 3.5 and the associated P-Specs represent a single process, CP described in P-Spec 1.8.



**A\_ACCELERATION (data flow, cel) =****\*A\_ACCELERATION\***

-----

DESCRIPTION: vehicle accelerations  
USED IN: AECLP, ASP, CP, GP  
UNITS: meters/sec^2  
RANGE: [-20, 5]  
DATA TYPE: array(1..3, 0..4) of real-8  
ATTRIBUTE: data  
DATA STORE: SENSOR\_OUTPUT  
ACCURACY: TBD

**A\_BIAS (data flow, cel) =****\*A\_BIAS\***

-----

DESCRIPTION: characteristic bias in the accelerometer measurements.  
USED IN: ASP  
UNITS: meters/sec^2  
RANGE: [-30, 0]  
DATA TYPE: array (1..3) of real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**A\_COUNTER (data flow, del) =****\*A\_COUNTER\***

-----

DESCRIPTION: accelerating along the x ,y and z axes  
USED IN: ASP  
UNITS: none  
RANGE: [0, (2^15)-1]  
DATA TYPE: array(1..3) of Integer-2  
ATTRIBUTE: data  
DATA STORE: EXTERNAL  
ACCURACY: N/A

**A\_GAIN\_0 (data flow, cel) =****\*A\_GAIN\_0\***

-----

DESCRIPTION: standard gain in the accelerations  
USED IN: ASP  
UNITS: meters/sec^2

RANGE: [0, 1]  
DATA TYPE: array(1..3) of Real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**A\_SCALE (data flow, del) =**

\*A\_SCALE\*

-----

DESCRIPTION: multiplicative constant used to determine limit on deviation accelerometer values  
USED IN: ASP  
UNITS: none  
RANGE: [0, 3]  
DATA TYPE: Integer-4  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**A\_STATUS (data flow, del) =**

[ "0"  
 | "1"  
 ]  
\*A\_STATUS\*

-----

DESCRIPTION: flag indicating whether or not the accelerometers are working properly  
USED IN: ASP, CP  
UNITS: none  
RANGE: [0:healthy, 1:unhealthy]  
DATA TYPE: array(1..3, 0..3) of Logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**AE\_CMD (data flow, del) =**

\*AE\_CMD\*

-----

DESCRIPTION: valve settings for the axial engines  
USED IN: AECLP, CP  
UNITS: none  
RANGE: [0, 127]  
DATA TYPE: array(1..3) of Integer-2  
ATTRIBUTE: data  
DATA STORE: EXTERNAL  
ACCURACY: TBD

**AE\_STATUS (data flow, del) =**

```
[ "0"  
  | "1"  
]  
*AE_STATUS*
```

-----

DESCRIPTION: status of axial engines  
USED IN: AECLP, CP  
UNITS: none  
RANGE: [0:healthy, 1:failed]  
DATA TYPE: Logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**AE\_SWITCH (data flow, del) =**

```
[ "0"  
  | "1"  
]  
*AE_SWITCH*
```

-----

DESCRIPTION: flag indicating whether or not axial engines are turned on  
USED IN: AECLP, GP  
UNITS: none  
RANGE: [0:AXIAL\_ENGINES\_ARE\_OFF, 1:AXIAL\_ENGINES\_ARE\_ON]  
DATA TYPE: Logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**AE\_TEMP (data flow, del) =**

```
[ "0"  
  | "1"  
  | "2"  
]  
*AE_TEMP*
```

-----

DESCRIPTION: temperature of axial engines when they are turned on  
USED IN: AECLP, CP, CRCP, GP  
UNITS: none  
RANGE: [0:cold, 1:warming\_up, 2:hot]  
DATA TYPE: Integer-2  
ATTRIBUTE: data

DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**AECLP\_EX\_IN (data flow) =**

CHUTE\_RELEASED  
+ FRAME\_COUNTER

**AECLP\_GS\_IN (data flow) =**

AE\_SWITCH  
+ AE\_TEMP  
+ FRAME\_ENGINES\_IGNITED  
+ CONTOUR\_CROSSED  
+ GP\_ALTITUDE  
+ GP\_ATTITUDE  
+ GP\_ROTATION  
+ GP\_VELOCITY  
+ INTERNAL\_CMD  
+ PE\_INTEGRAL  
+ TE\_INTEGRAL  
+ TE\_LIMIT  
+ VELOCITY\_ERROR  
+ YE\_INTEGRAL  
+ CL

**AECLP\_GS\_OUT (data flow) =**

AE\_STATUS  
+ AE\_TEMP  
+ INTERNAL\_CMD  
+ PE\_INTEGRAL  
+ TE\_INTEGRAL  
+ TE\_LIMIT  
+ YE\_INTEGRAL

**AECLP\_RP\_IN (data flow) =**

ENGINES\_ON\_ALTITUDE  
+ DELTA\_T  
+ FULL\_UP\_TIME  
+ GAX  
+ GP2  
+ GQ  
+ GRAVITY  
+ GVE  
+ GVI  
+ GWI  
+ PE\_MIN  
+ TE\_INIT  
+ TE\_MIN  
+ YE\_MIN  
+ GA  
+ GP1



+ GPY  
 + GR  
 + GV  
 + GVEI  
 + GW  
 + OMEGA  
 + PE\_MAX  
 + TE\_DROP  
 + TE\_MAX  
 + YE\_MAX

### ALPHA\_MATRIX (data flow, cel) =

\*ALPHA\_MATRIX\*

-----

DESCRIPTION: matrix of misalignment angles  
 USED IN: ASP  
 UNITS: none  
 RANGE: [-PI, PI] where PI = 3.141592653589793  
 DATA TYPE: array (1..3, 1..3) of Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMENTERS  
 ACCURACY: N/A

### AR\_ALTITUDE (data flow, cel) =

\*AR\_ALTITUDE\*

-----

DESCRIPTION: altimeter radar height above terrain  
 USED IN: ARSP, CP, GP  
 UNITS: meters  
 RANGE: [0, 2000]  
 DATA TYPE: array(0..4) of Real-8  
 ATTRIBUTE: data  
 DATA STORE: SENSOR\_OUTPUT  
 ACCURACY: TBD

### AR\_COUNTER (data flow, del) =

\*AR\_COUNTER\*

-----

DESCRIPTION: counter containing elapsed time since transmission of radar pulse  
 USED IN: ARSP  
 UNITS: cycles  
 RANGE: [-1, (2<sup>15</sup>)-1]  
 DATA TYPE: Integer-2  
 ATTRIBUTE: data

DATA STORE: EXTERNAL  
 ACCURACY: N/A

### AR\_FREQUENCY (data flow) =

\*AR\_FREQUENCY\*

-----

DESCRIPTION: increment frequency of AR\_COUNTER  
 USED IN: ARSP  
 UNITS: cycles/sec  
 RANGE: [1, 2.45x10<sup>9</sup>]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### AR\_STATUS (data flow, del) =

[ "0"  
 | "1"  
 ]  
 \*AR\_STATUS\*

-----

DESCRIPTION: status of the altimeter radars  
 USED IN: ARSP, CP  
 UNITS: none  
 RANGE: [0:healthy, 1:failed]  
 DATA TYPE: array(0..4) of Logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### ARSP\_GS\_IN (data flow) =

AR\_STATUS  
 + K\_ALT

### ARSP\_GS\_OUT (data flow) =

AR\_STATUS  
 + K\_ALT

### ASP\_RP\_IN (data flow) =

A\_BIAS  
 + A\_GAIN\_0  
 + A\_SCALE  
 + ALPHA\_MATRIX  
 + G1

+ G2

**ASP\_SO\_IN (data flow) =**

A\_ACCELERATION  
+ ATMOSPHERIC\_TEMP

**ATMOSPHERIC\_TEMP (data flow, cel) =**

\*ATMOSPHERIC\_TEMP\*

-----

DESCRIPTION: atmospheric temperature  
USED IN: ASP, CP, GSP, TSP  
UNITS: degrees C  
RANGE: [-200, 25]  
DATA TYPE: Real-8  
ATTRIBUTE: data  
DATA STORE: SENSOR\_OUTPUT  
ACCURACY: TBD

**C\_STATUS (data flow, del) =**

[ "0"  
 | "1"  
 ]  
\*C\_STATUS\*

-----

DESCRIPTION: flag indicating whether or not the communications processor is working properly  
USED IN: CP  
UNITS: none  
RANGE: [0:healthy, 1:failed]  
DATA TYPE: Logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**CHUTE\_RELEASED (data/control flow, del) =**

[ "0"  
 | "1"  
 ]  
\*CHUTE\_RELEASED\*

-----

DESCRIPTION: signal indicating parachute has been released  
USED IN: AECLP, CP, CRCP, GP  
UNITS: none  
RANGE: [0:chute\_attached, 1:chute\_released]  
DATA TYPE: Logical-1

ATTRIBUTE: data condition  
 DATA STORE: EXTERNAL  
 ACCURACY: N/A

### CL (data flow, del) =

```
[ "1"
  | "2"
]
```

\*CL\*

- - DESCRIPTION : index which specifies which set of control law parameters to use USED IN : AECLP , GP UNITS

RANGE : [ 1 : first , 2 : second

] DATA TYPE : Integer-2 ATTRIBUTE : data DATA STORE : GUIDANCE\_STATE ACCURACY : N / A

### COMM\_SYNC\_PATTERN (data flow, pel) =

\*COMM\_SYNC\_PATTERN\*

-----

DESCRIPTION: sixteen bit synchronization pattern

USED IN: CP

UNITS: none

RANGE: [0xD9B2] \* hexadecimal notation \*

DATA TYPE: Integer-2

ATTRIBUTE: data

DATA STORE: RUN\_PARAMETERS

ACCURACY: N/A

### CONTOUR\_ALTITUDE (data flow, cel) =

\*CONTOUR\_ALTITUDE\*

-----

DESCRIPTION: altitude in velocity-altitude contour

USED IN: GP

UNITS: kilometers

RANGE: [-.01, 2]

DATA TYPE: array (1..100) of Real-8

ATTRIBUTE: data

DATA STORE: RUN\_PARAMETERS

ACCURACY: N/A

### CONTOUR\_CROSSED (data flow, del) =

```
[ "0"
  | "1"
]
```

\*contour\_crossed\*

-----

DESCRIPTION: indicates if the velocity-altitude contour has been sensed  
 USED IN: AECLP, CP, GP  
 UNITS: none  
 RANGE: [0:contour\_not\_crossed, 1:contour\_crossed]  
 DATA TYPE: logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### CONTOUR\_VELOCITY (data flow, cel) =

\*CONTOUR\_VELOCITY\*

-----

DESCRIPTION: velocity in velocity-altitude contour  
 USED IN: GP  
 UNITS: kilometers/sec  
 RANGE: [0, 0.5]  
 DATA TYPE: array(1..100) of Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### CP\_EXT\_IN (data flow) =

AE\_CMD  
 + CHUTE\_RELEASED  
 + FRAME\_COUNTER  
 + RE\_CMD  
 + SUBFRAME\_COUNTER

### CP\_GS\_IN (data flow) =

A\_STATUS  
 + AE\_STATUS  
 + AE\_TEMP  
 + AR\_STATUS  
 + C\_STATUS  
 + CONTOUR\_CROSSED  
 + G\_STATUS  
 + GP\_ALTITUDE  
 + GP\_ATTITUDE  
 + GP\_PHASE

+ GP\_ROTATION  
 + GP\_VELOCITY  
 + K\_ALT  
 + K\_MATRIX  
 + PE\_INTEGRAL  
 + RE\_STATUS  
 + TDLR\_STATE  
 + TDLR\_STATUS  
 + TDS\_STATUS  
 + TE\_INTEGRAL  
 + TS\_STATUS  
 + VELOCITY\_ERROR  
 + YE\_INTEGRAL

### CP\_SO\_IN (data flow) =

AR\_ALTITUDE  
 + ATMOSPHERIC\_TEMP  
 + A\_ACCELERATION  
 + G\_ROTATION  
 + TDLR\_VELOCITY  
 + TD\_SENSED

### DELTA\_T (data flow, del) =

\*DELTA\_T\*

-----

DESCRIPTION: time step duration  
 USED IN: AECLP, GP, RECLP, TDLRSP  
 UNITS: seconds  
 RANGE: [0.005, 0.20]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### DROP\_HEIGHT (data flow, del) =

\*DROP\_HEIGHT\*

-----

DESCRIPTION: height from which vehicle should free-fall to surface  
 USED IN: GP  
 UNITS: meters  
 RANGE: [0, 100]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A.

**DROP\_SPEED (data flow, del) =**

\*DROP\_SPEED\*

-----

DESCRIPTION: optimal speed during constant velocity descent  
 USED IN: GP  
 UNITS: meters/sec  
 RANGE: [0, 4.0]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**ENGINE\_DATA (data flow) =**

AE\_CMD  
 + RE\_CMD

**ENGINES\_ON\_ALTITUDE (data flow, del) =**

\*ENGINES\_ON\_ALTITUDE\*

-----

DESCRIPTION: altitude at which the axial engines are turned on;  
 USED IN: AECLP, GP  
 UNITS: meters  
 RANGE: [0, 2000]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**EXTERNAL (store) =**

\*-----\*

Implementaion of the data elements in the data store EXTERNAL must be  
 arranged in the order specified below.

\*-----\*

A\_COUNTER  
 + AE\_CMD  
 + AR\_COUNTER  
 + CHUTE\_RELEASED  
 + FRAME\_COUNTER  
 + G\_COUNTER  
 + PACKET  
 + RE\_CMD  
 + SS\_TEMP

+ SUBFRAME\_COUNTER  
 + TD\_COUNTER  
 + TDLR\_COUNTER  
 + THERMO\_TEMP

### FRAME\_BEAM\_UNLOCKED (data flow, del) =

\*FRAME\_BEAM\_UNLOCKED\*

-----

DESCRIPTION: variable containing the number of the frame during which the radar beam unlocked  
 USED IN: TDLRSP  
 UNITS: none  
 RANGE: [0, (2<sup>31</sup>)-1]  
 DATA TYPE: array(1..4) of Integer-4  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

### FRAME\_COUNTER (data flow) =

\*FRAME\_COUNTER\*

-----

DESCRIPTION: counter containing the number of the present frame;  
 USED IN: AECLP, CP, GP, TDLRSP, ARSP  
 UNITS: none  
 RANGE: [1, (2<sup>31</sup>)-1]  
 DATA TYPE: Integer-4  
 ATTRIBUTE: data  
 DATA STORE: EXTERNAL  
 ACCURACY: N/A

### FRAME\_ENGINES\_IGNITED (data flow, del) =

\*FRAME\_ENGINES\_IGNITED\*

-----

DESCRIPTION: variable containing the number of the frame during which the engines were ignited  
 USED IN: AECLP, GP  
 UNITS: none  
 RANGE: [0, (2<sup>31</sup>)-1]  
 DATA TYPE: Integer-4  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD



**FULL\_UP\_TIME (data flow, del) =**

\*FULL\_UP\_TIME\*

-----

DESCRIPTION: time for axial engines to reach optimum operational condition  
 USED IN: AECLP  
 UNITS: seconds  
 RANGE: [0, 60]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**G1 (data flow, del) =**

\*G1\*

- - DESCRIPTION : coefficient used to adjust A\_GAIN USED IN : ASP UNITS : ( meters / sec ^ 2 ) / ( degree\_C ) R  
 ] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**G2 (data flow, del) =**

\*G2\*

- - DESCRIPTION : coefficient used to adjust A\_GAIN USED IN : ASP UNITS : ( meters / sec ^ 2 ) / degree\_C ^ 2 R  
 ] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A .

**G3 (data flow, del) =**

\*G3\*

- - DESCRIPTION : coefficient used to adjust G\_GAIN USED IN : GSP UNITS : ( radians / sec ) / degree\_C RANGE :  
 ] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**G4 (data flow, del) =**

\*G4\*

- - DESCRIPTION : coefficient used to adjust G\_GAIN USED IN : GSP UNITS : ( radians / sec ) / degree\_C ^ 2 RAN  
 ] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**G\_COUNTER (data flow, del) =**

\*G\_COUNTER\*

-----

DESCRIPTION: gyroscope measurement of vehicle rotation rates;  
 USED IN: GSP  
 UNITS: none  
 RANGE: [-(2^14)-1, (2^14)-1]  
 DATA TYPE: array (1..3) of Integer-2  
 ATTRIBUTE: data;

DATA STORE: EXTERNAL  
ACCURACY: N/A

**G\_GAIN\_0 (data flow, del) =**

\*G\_GAIN\_0\*

-----

DESCRIPTION: standard gain in vehicle rotation rates as measured by the gyroscopes  
USED IN: GSP  
UNITS: radians/sec  
RANGE: [-1, 1]  
DATA TYPE: array (1..3) of Real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**G\_OFFSET (data flow, del) =**

\*G\_OFFSET\*

-----

DESCRIPTION: standard offset of the rotation raw values  
USED IN: GSP  
UNITS: radians/sec  
RANGE: [-0.5, 0.5]  
DATA TYPE: array (1..3) of Real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**G\_ROTATION (data flow, cel) =**

\*G\_ROTATION\*

-----

DESCRIPTION: vehicle rotation rates  
USED IN: CP, GSP, GP, RECLP  
UNITS: radians/sec  
RANGE: [-1.0, 1.0]  
DATA TYPE: array (1..3, 0..4) of Real-8  
ATTRIBUTE: data  
DATA STORE: SENSOR\_OUTPUT  
ACCURACY: TBD

**G\_STATUS (data flow, del) =**

[ "0"

| "1"  
]  
\*G\_STATUS\*

-----

DESCRIPTION: status of the gyroscopes  
USED IN: CP, GSP  
UNITS: none  
RANGE: [0:healthy, 1:failed]  
DATA TYPE: Logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**GA (data flow) =**

\*GA\*

- - DESCRIPTION : gain USED IN : AECLP UNITS : sec / meter RANGE : [ 0 , 50  
] DATA TYPE : Real-8 ATTRIBUTE : data DATA  
RUN\_PARAMETERS ACCURACY : N / A

**GAX (data flow) =**

\*GAX\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : none RANGE : [ 0 , 5  
] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE  
RUN\_PARAMETERS ACCURACY : N / A

**GP1 (data flow) =**

\*GP1\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : none RANGE : [ - , 5  
] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE  
RUN\_PARAMETERS ACCURACY : N / A

**GP2 (data flow) =**

\*GP2\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : none RANGE : [ - , 5  
] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE  
RUN\_PARAMETERS ACCURACY : N / A

**GP\_ALTITUDE (data flow) =**

\*GP\_ALTITUDE\*

-----

DESCRIPTION: altitude as seen by guidance processor  
USED IN: AECLP, CP, GP

UNITS: meters  
RANGE: [0, 2000]  
DATA TYPE: array (0..4) of Real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD

**GP\_ATTITUDE (data flow) =**

\*GP\_ATTITUDE\*

-----

DESCRIPTION: direction cosine matrix  
USED IN: AECLP, CP, GP  
UNITS: none  
RANGE: [-1, 1]  
DATA TYPE: array (1..3, 1..3, 0..4) Real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD

**GP\_EX\_IN (data flow) =**

CHUTE\_RELEASED  
+ FRAME\_COUNTER

**GP\_GS\_IN (data flow) =**

AE\_SWITCH  
+ AE\_TEMP  
+ CL  
+ CONTOUR\_CROSSED  
+ GP\_ALTITUDE  
+ GP\_ATTITUDE  
+ GP\_PHASE  
+ GP\_VELOCITY  
+ K\_ALT  
+ K\_MATRIX  
+ RE\_SWITCH  
+ TDS\_STATUS

**GP\_GS\_OUT (data flow) =**

AE\_SWITCH  
+ CONTOUR\_CROSSED  
+ CL  
+ FRAME\_ENGINES\_IGNITED  
+ GP\_ALTITUDE  
+ GP\_ATTITUDE  
+ GP\_PHASE  
+ GP\_ROTATION  
+ GP\_VELOCITY

+ RE\_SWITCH  
 + TE\_INTEGRAL  
 + VELOCITY\_ERROR

### GP\_PHASE (data/control flow, del) =

```
[ "1"
  | "2"
  | "3"
  | "4"
  | "5"
]
*GP_PHASE*
```

-----

DESCRIPTION: phase of operation as seen by guidance processor  
 USED IN: CP, GP  
 UNITS: none  
 RANGE: [1, 5]  
 DATA TYPE: Integer-4  
 ATTRIBUTE: data condition  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

### GP\_ROTATION (data flow) =

\*GP\_ROTATION\*

-----

DESCRIPTION: rotation rates as determined by the guidance processing functional unit  
 USED IN: AECLP, CP, GP  
 UNITS: radians/sec  
 RANGE: [-1.0, 1.0]  
 DATA TYPE: array (1..3, 1..3) Real-8  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

### GP\_RP\_IN (data flow) =

CONTOUR\_ALTITUDE  
 + CONTOUR\_VELOCITY  
 + DELTA\_T  
 + DROP\_HEIGHT  
 + ENGINES\_ON\_ALTITUDE  
 + GRAVITY  
 + DROP\_SPEED  
 + MAX\_NORMAL\_VELOCITY

### GP\_SO\_IN (data flow) =

A\_ACCELERATION  
 + AR\_ALTITUDE

+ G\_ROTATION  
 + TD\_SENSED  
 + TDLR\_VELOCITY

**GP\_VELOCITY (data flow) =**

\*GP\_VELOCITY\*

-----

DESCRIPTION: velocity as corrected by the guidance algorithm  
 USED IN: AECLP, CP, GP  
 UNITS: meters/sec  
 RANGE: [-100, 100]  
 DATA TYPE: array (1..3, 0..4) of Real-8  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

**GPY (data flow) =**

\*GPY\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : none RANGE : [ - , 5  
 ] DATA TYPE : Real-8 ATTRIBUTE : data DATA STORE  
 RUN\_PARAMETERS ACCURACY : N / A

**GQ (data flow) =**

\*GQ\*

- - DESCRIPTION : gain USED IN : AECLP UNITS : seconds RANGE : [ - , 8  
 ] DATA TYPE : array ( 1 ..2 ) of Real-8 ATTRIBU

**GR (data flow) =**

\*GR\*

- - DESCRIPTION : gain USED IN : AECLP UNITS : seconds RANGE : [ - , 8  
 ] DATA TYPE : array ( 1 ..2 ) of Real-8 ATTRIBU

**GRAVITY (data flow) =**

\*GRAVITY\*

-----

DESCRIPTION: gravity of planet  
 USED IN: AECLP, GP  
 UNITS: meters/sec^2  
 RANGE: [0, 100]  
 DATA TYPE: Real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS

ACCURACY: N/A

**GSP\_RP\_IN (data flow) =**

G3  
 + G4  
 + G\_GAIN\_0  
 + G\_OFFSET

**GSP\_SO\_IN (data flow) =**

ATMOSPHERIC\_TEMP  
 + G\_ROTATION

**GUIDANCE\_STATE (store) =**

\*-----\*  
 Implementaion of the data elements in the data store GUIDANCE\_STATE  
 must be arranged in the order specified below.  
 \*-----\*

A\_STATUS  
 + AE\_STATUS  
 + AE\_SWITCH  
 + AE\_TEMP  
 + AR\_STATUS  
 + C\_STATUS  
 + CL  
 + CONTOUR\_CROSSED  
 + FRAME\_BEAM\_UNLOCKED  
 + FRAME\_ENGINES\_IGNITED  
 + G\_STATUS  
 + GP\_ALTITUDE  
 + GP\_ATTITUDE  
 + GP\_PHASE  
 + GP\_ROTATION  
 + GP\_VELOCITY  
 + INTERNAL\_CMD  
 + K\_ALT  
 + K\_MATRIX  
 + PE\_INTEGRAL  
 + RE\_STATUS  
 + RE\_SWITCH  
 + TDLR\_STATE  
 + TDLR\_STATUS  
 + TDS\_STATUS  
 + TE\_INTEGRAL  
 + TE\_LIMIT  
 + THETA  
 + TS\_STATUS  
 + VELOCITY\_ERROR  
 + YE\_INTEGRAL

**GV (data flow) =**

\*GV\*

- - DESCRIPTION : gain USED IN : AECLP UNITS : sec / meter RANGE : [ - , 8  
] DATA TYPE : array ( 1 ..2 ) of Real-8 ATT

### GVE (data flow) =

\*GVE\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : / second RANGE : [ 0 , 500  
] DATA TYPE : Real-8 ATTRIBUTE : data DATA S  
RUN\_PARAMETERS ACCURACY : N / A

### GVEI (data flow) =

\*GVEI\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : / sec ^ 2 RANGE : [ - , 40  
] DATA TYPE : array ( 1 ..2 ) of Real-8 ATT

### GVI (data flow) =

\*GVI\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : / meter RANGE : [ - , 5  
] DATA TYPE : array ( 1 ..2 ) of Real-8 ATTRI

### GW (data flow) =

\*GW\*

- - DESCRIPTION : gain USED IN : AECLP UNITS : sec / meter RANGE : [ - , 8  
] DATA TYPE : array ( 1 ..2 ) of Real-8 ATT

### GWI (data flow) =

\*GWI\*

- - - DESCRIPTION : gain USED IN : AECLP UNITS : / meter RANGE : [ - , 5  
] DATA TYPE : array ( 1 ..2 ) of Real-8 ATTRI

### INTERNAL\_CMD (data flow) =

\*INTERNAL\_CMD\*

-----

DESCRIPTION: real vector containing the command to be sent to the axial engines  
USED IN: AECLP  
UNITS: none  
RANGE: [-0.7, 1.7]  
DATA TYPE: array (1..3) of Real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD



**K\_ALT (data flow) =**

\*K\_ALT\*

- - - DESCRIPTION : determines use of altimeter radar by guidance processor USED BY : ARSP , CP , GP UNITS :  
 RANGE : [ 0 , 1  
 ] DATA TYPE : array ( 0 ..4 ) of integer-4 ATTRIBUTE : data DATA STORE : GUIDANCE\_STATE ACCURACY : N /

**K\_MATRIX (data flow) =**

\*K\_MATRIX\*

-----

DESCRIPTION: determines use of the doppler radar by guidance processor.  
 USED IN: CP, GP, TDLRSP  
 UNITS: none  
 RANGE: [0, 1]  
 DATA TYPE: array (1..3, 1..3, 0..4) integer-4  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

**M1 (data flow) =**

\*M1\*

- - DESCRIPTION : lower measured temperature calibration point for solid state temperature sensor .USED IN : T  
 none RANGE : { 0 , ( 2 ^ 15 ) -  
 ] DATA TYPE : interger-2 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**M2 (data flow) =**

\*M2\*

- - DESCRIPTION : upper measured temperature calibration point for solid state temperature sensor .USED IN : T  
 none RANGE : [ 0 , ( 2 ^ 15 ) -  
 ] DATA TYPE : integer-2 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A .

**M3 (data flow) =**

\*M3\*

- - DESCRIPTION : lower measured temperature calibration point for thermocouple pair temperature sensor USED I  
 UNITS : none RANGE : [ 0 , ( 2 ^ 15 ) -  
 ] DATA TYPE : integer-2 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**M4 (data flow) =**

\*M4\*

- - DESCRIPTION : upper measured temperature calibration point for thermocouple pair temperature sensor USED I

UNITS : none RANGE : [ 0 , ( 2 ^ 15 ) -  
 ] DATA TYPE : integer-2 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

### MAX\_NORMAL\_VELOCITY (data flow) =

\*MAX\_NORMAL\_VELOCITY\*

-----

DESCRIPTION: maximum vertical velocity for safe landing  
 USED IN: GP  
 UNITS: meters/sec  
 RANGE: [0, 3.35]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### OMEGA (data flow) =

\*OMEGA\*

- - - DESCRIPTION : gain of angular velocity USED IN : AECLP UNITS : / second RANGE : [ - 0 , 50  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

### P1 (data flow) =

\*P1\*

- - DESCRIPTION : pulse rate boundary USED IN : RECLP UNITS : radians / sec RANGE : [ 0 , 0 .05  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

### P2 (data flow) =

\*P2\*

- - DESCRIPTION : pulse rate boundary USED IN : RECLP UNITS : radians / sec RANGE : [ 0 , 0 .05  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

### P3 (data flow) =

\*P3\*

- - DESCRIPTION : pulse rate boundary USED IN : RECLP UNITS : radians / sec RANGE : [ 0 , 0 .05  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

### P4 (data flow) =

\*P4\*

- - DESCRIPTION : pulse rate boundary USED IN : RECLP UNITS : radians / sec RANGE : [ 0 , 0 .05  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**PACKET (data flow) =**

\*PACKET\*

-----

DESCRIPTION: packet of telemetry data  
USED IN: CP  
UNITS: N/A  
RANGE: N/A  
DATA TYPE: array (1..256) of integer-2  
ATTRIBUTE: data  
DATA STORE: EXTERNAL  
ACCURACY: N/A

**PE\_INTEGRAL (data flow) =**

\*PE\_INTEGRAL\*

-----

DESCRIPTION: integral portion of pitch error equation  
USED IN: AECLP, CP  
UNITS: meters  
RANGE: [-100, 100]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD

**PE\_MAX (data flow) =**

\*PE\_MAX\*

-----

DESCRIPTION: maximum pitch error tolerable  
USED IN: AECLP  
UNITS: none  
RANGE: [0, 1]  
DATA TYPE: array (1..2) of real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**PE\_MIN (data flow) =**

\*PE\_MIN\*

-----

DESCRIPTION: minimum pitch error tolerable  
USED IN: AECLP

UNITS: none  
 RANGE: [-1, 0]  
 DATA TYPE: array (1..2) of real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### RAW\_SENSOR\_DATA (data flow) =

A\_COUNTER  
 + AR\_COUNTER  
 + G\_COUNTER  
 + SS\_TEMP  
 + TD\_COUNTER  
 + TDLR\_COUNTER  
 + THERMO\_TEMP

### RE\_CMD (data flow) =

```

[ "1"
  | "2"
  | "3"
  | "4"
  | "5"
  | "6"
  | "7"
]
*RE_CMD*
  
```

-----

DESCRIPTION: roll engine command  
 USED IN: CP,RECLP  
 UNITS: none  
 RANGE: [1, 7]  
         1 off  
         2 minimum, counterclockwise  
         3 minimum, clockwise  
         4 intermediate, counterclockwise  
         5 intermediate, clockwise  
         6 maximum, counterclockwise  
         7 maximum, clockwise  
 DATA TYPE: integer-2  
 ATTRIBUTE: data  
 DATA STORE: EXTERNAL  
 ACCURACY: TBD

### RE\_STATUS (data flow) =

```

[ "0"
  | "1"
]
  
```

\*RE\_STATUS\*

-----

DESCRIPTION: status of the roll engines  
 USED IN: CP, RECLP  
 UNITS: none  
 RANGE: [0:healthy, 1:failed]  
 DATA TYPE: logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### RE\_SWITCH (data flow) =

[ "0"  
 | "1"  
 ]

\*RE\_SWITCH\*

-----

DESCRIPTION: flag indicating whether or not the roll engines are turned on  
 USED IN: GP, RECLP  
 UNITS: none  
 RANGE: {0:roll\_engines\_are\_off, 1:roll\_engines\_are\_on]  
 DATA TYPE: logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### RECLP\_GS\_IN (data flow) =

RE\_SWITCH  
 + THETA

### RECLP\_GS\_OUT (data flow) =

RE\_STATUS  
 + THETA

### RECLP\_RP\_IN (data flow) =

DELTA\_T  
 + P1  
 + P2  
 + P3  
 + P4  
 + THETA1  
 + THETA2

**RUN\_PARAMETERS (store) =**

-----  
Implementaion of the data elements in the data store RUN\_PARAMETERS  
must be arranged in the order specified below.  
-----\*

A\_BIAS  
+ A\_GAIN\_0  
+ A\_SCALE  
+ ALPHA\_MATRIX  
+ AR\_FREQUENCY  
+ COMM\_SYNC\_PATTERN  
+ CONTOUR\_ALTITUDE  
+ CONTOUR\_VELOCITY  
+ DELTA\_T  
+ DROP\_HEIGHT  
+ DROP\_SPEED  
+ ENGINES\_ON\_ALTITUDE  
+ FULL\_UP\_TIME  
+ G1  
+ G2  
+ G3  
+ G4  
+ G\_GAIN\_0  
+ G\_OFFSET  
+ GA  
+ GAX  
+ GP1  
+ GP2  
+ GPY  
+ GQ  
+ GR  
+ GRAVITY  
+ GV  
+ GVE  
+ GVEI  
+ GVI  
+ GW  
+ GWI  
+ M1  
+ M2  
+ M3  
+ M4  
+ MAX\_NORMAL\_VELOCITY  
+ OMEGA  
+ P1  
+ P2  
+ P3  
+ P4  
+ PE\_MAX  
+ PE\_MIN  
+ T1  
+ T2  
+ T3  
+ T4

```

+ TDLR_ANGLES
+ TDLR_GAIN
+ TDLR_LOCK_TIME
+ TDLR_OFFSET
+ TE_DROP
+ TE_INIT
+ TE_MAX
+ TE_MIN
+ THETA1
+ THETA2
+ YE_MAX
+ YE_MIN

```

### SENSOR\_OUTPUT (store) =

```

*-----*
Implementaion of the data elements in the data store SENSOR_OUTPUT
must be arranged in the order specified below.
*-----*
```

```

A_ACCELERATION
+ AR_ALTITUDE
+ ATMOSPHERIC_TEMP
+ G_ROTATION
+ TD_SENSED
+ TDLR_VELOCITY

```

### SS\_TEMP (data flow) =

```
*SS_TEMP*
```

```
-----
```

```

DESCRIPTION: solid state temperature data
USED IN:      TSP
UNITS:        none
RANGE:        [0, (2^15)-1]
DATA TYPE:    integer-2
ATTRIBUTE:    data
DATA STORE:   EXTERNAL
ACCURACY:     N/A

```

### SUBFRAME\_COUNTER (control flow, del) =

```

[ "1"
  | "2"
  | "3"
]
*SUBFRAME_COUNTER*

```

```
-----
```

```

DESCRIPTION: Counter containing the number of the present subframe.
USED IN:     CP

```

UNITS: none  
 RANGE: [1,3]  
 DATA TYPE: Integer-2  
 ATTRIBUTE: data  
 DATA STORE: EXTERNAL  
 ACCURACY: N/A

**T1 (data flow) =**

\*T1\*

- - DESCRIPTION : lower ambient temperature calibration point for solid state temperature sensor USED IN : TSP  
 degrees C RANGE : [ - 50 , 250  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**T2 (data flow) =**

\*T2\*

- - DESCRIPTION : upper ambient temperature calibration point for solid state temperature sensor USED IN : TSP  
 degrees C RANGE : [ - 50 , 250  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**T3 (data flow) =**

\*T3\*

- - DESCRIPTION : lower ambient temperature calibration point for thermocouple pair temperature sensor USED IN  
 UNITS : degrees C RANGE : [ - 0 , 50  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**T4 (data flow) =**

\*T4\*

- - DESCRIPTION : upper ambient temperature calibration point for thermocouple pair temperature sensor USED IN  
 UNITS : degrees C RANGE : [ - 0 , 50  
 ] DATA TYPE : real-8 ATTRIBUTE : data DATA STORE : RUN\_PARAMETERS ACCURACY : N / A

**TD\_COUNTER (data flow) =**

\*TD\_COUNTER\*

-----

DESCRIPTION: value returned by touch down sensor  
 USED IN: TDSP  
 UNITS: none  
 RANGE: [(-2<sup>15</sup>), (2<sup>15</sup>)-1]  
 DATA TYPE: integer-2  
 ATTRIBUTE: data  
 DATA STORE: EXTERNAL  
 ACCURACY: N/A



**TD\_SENSED (data flow) =**

```
[ "0"  
  | "1"  
]  
*TD_SENSED*
```

-----

DESCRIPTION: flag indicating whether or not touch down has been sensed  
USED IN: CP, GP, TDSP  
UNITS: none  
RANGE: [0:touch\_down\_not\_sensed, 1:touch\_down\_sensed]  
DATA TYPE: logical-1  
ATTRIBUTE: data  
DATA STORE: SENSOR\_OUTPUT  
ACCURACY: N/A

**TDLR\_ANGLES (data flow) =**

```
*TDLR_ANGLES*
```

-----

DESCRIPTION: vector of doppler radar beam offset angles (i.e.,alpha ,beta ,gamma)  
USED IN: TDLRSP  
UNITS: radians  
RANGE: [0, PI/2) where PI = 3.141592653589793  
DATA TYPE: array (1..3) of real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**TDLR\_COUNTER (data flow) =**

```
*TDLR_COUNTER*
```

-----

DESCRIPTION: value returned by doppler radar  
USED IN: TDLRSP  
UNITS: none  
RANGE: [0, (2<sup>15</sup>)-1]  
DATA TYPE: array (1..4) of integer-2  
ATTRIBUTE: data  
DATA STORE: EXTERNAL  
ACCURACY: N/A

**TDLR\_GAIN (data flow) =**

```
*TDLR_GAIN*
```

-----

DESCRIPTION: gain in doppler radar beam  
USED IN: TDLRSP  
UNITS: meters/sec  
RANGE: [-1, 1]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**TDLR\_LOCK\_TIME (data flow) =**

\*TDLR\_LOCK\_TIME\*

-----

DESCRIPTION: locking time of doppler radar beam  
USED IN: TDLRSP  
UNITS: seconds  
RANGE: [0, 60]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**TDLR\_OFFSET (data flow) =**

\*TDLR\_OFFSET\*

-----

DESCRIPTION: offset in doppler radar beam  
USED IN: TDLRSP  
UNITS: meters/sec  
RANGE: [-100, 0]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**TDLR\_STATE (data flow) =**

```
[ "0"  
  | "1"  
]  
*TDLR_STATE*
```

-----

DESCRIPTION: state of the touch down landing radar beams  
USED IN: CP, TDLRSP

UNITS: none  
 RANGE: [0:beam\_unlocked, 1:beam\_locked]  
 DATA TYPE: array (1..4) logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### **TDLR\_STATUS (data flow) =**

```

[ "0"
  | "1"
]
*TDLR_STATUS*
  
```

-----

DESCRIPTION: status of the doppler radar  
 USED IN: CP, TDLRSP  
 UNITS: none  
 RANGE: [0:healthy, 1:failed]  
 DATA TYPE: array (1..4) of logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

### **TDLR\_VELOCITY (data flow) =**

```

*TDLR_VELOCITY*
  
```

-----

DESCRIPTION: velocity as computed by the touch down landing radar  
 USED IN: CP, GP, TDLRSP  
 UNITS: meters/sec  
 RANGE: [-100, 100]  
 DATA TYPE: array (1..3, 0..4) of real-8  
 ATTRIBUTE: data  
 DATA STORE: SENSOR\_OUTPUT  
 ACCURACY: TBD

### **TDLRSP\_EXT\_IN (data flow) =**

```

FRAME_COUNTER
+ TDLR_COUNTER
  
```

### **TDLRSP\_GS\_IN (data flow) =**

```

FRAME_BEAM_UNLOCKED
+ K_MATRIX
+ TDLR_STATE
  
```

**TDLRSP\_GS\_OUT (data flow) =**

FRAME\_BEAM\_UNLOCKED  
 + K\_MATRIX  
 + TDLR\_STATE  
 + TDLR\_STATUS

**TDLRSP\_RP\_IN (data flow) =**

DELTA\_T  
 + TDLR\_ANGLES  
 + TDLR\_GAIN  
 + TDLR\_LOCK\_TIME  
 + TDLR\_OFFSET

**TDS\_STATUS (data flow) =**

[ "0"  
 | "1"  
 ]  
 \*TDS\_STATUS\*

-----

DESCRIPTION: status of the touch down sensor  
 USED IN: CP, GP, TDSP  
 UNITS: none  
 RANGE: [0:healthy, 1:failed]  
 DATA TYPE: logical-1  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: N/A

**TE\_DROP (data flow) =**

\*TE\_DROP\*

-----

DESCRIPTION: the axial thrust error when axial engines are warm and the velocity altitude contour has not been intersected.  
 USED IN: AECLP  
 UNITS: none  
 RANGE: [-2, 2]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**TE\_INIT (data flow) =**

\*TE\_INIT\*

-----

DESCRIPTION: the axial thrust error when the axial engines are cold  
 USED IN: AECLP  
 UNITS: none  
 RANGE: [-2, 2]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

### TE\_INTEGRAL (data flow) =

\*TE\_INTEGRAL\*

-----

DESCRIPTION: integral portion of thrust error equation  
 USED IN: AECLP, CP, GP  
 UNITS: meters  
 RANGE: [-100, 100]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

### TE\_LIMIT (data flow) =

\*TE\_LIMIT\*

-----

DESCRIPTION: limiting thrust error  
 USED IN: AECLP  
 UNITS: none  
 RANGE: [-100, 100]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: GUIDANCE\_STATE  
 ACCURACY: TBD

### TE\_MAX (data flow) =

\*TE\_MAX\*

-----

DESCRIPTION: maximum thrust error tolerable  
 USED IN: AECLP  
 UNITS: none  
 RANGE: [-2, 2]  
 DATA TYPE: array (1..2) of real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**TE\_MIN (data flow) =**

\*TE\_MIN\*

-----

DESCRIPTION: minimum thrust error tolerable  
 USED IN: AECLP  
 UNITS: none  
 RANGE: [-2, 2]  
 DATA TYPE: array (1..2) of real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**THERMO\_TEMP (data flow) =**

\*THERMO\_TEMP\*

-----

DESCRIPTION: thermocouple pair temperature  
 USED IN: TSP  
 UNITS: none  
 RANGE:  $[0, (2^{15})-1]$   
 DATA TYPE: integer-2  
 ATTRIBUTE: data  
 DATA STORE: EXTERNAL  
 ACCURACY: N/A

**THETA (data flow) =**

\*THETA\*

- - - - DESCRIPTION : roll angle USED IN : RECLP UNITS : radians RANGE : [ - I , PI  
 ] where PI = 3 .141592653589793 DATA  
 real-8 ATTRIBUTE : data DATA STORE : GUIDANCE\_STATE ACCURACY : TBD

**THETA1 (data flow) =**

\*THETA1\*

-----

DESCRIPTION: pulse angle boundary  
 USED IN: RECLP  
 UNITS: radians  
 RANGE: [0, 0.05]  
 DATA TYPE: real-8  
 ATTRIBUTE: data  
 DATA STORE: RUN\_PARAMETERS  
 ACCURACY: N/A

**THETA2 (data flow) =****\*THETA2\***

-----

DESCRIPTION: pulse angle boundary  
USED IN: RECLP  
UNITS: radians  
RANGE: [0, 0.05]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**TS\_STATUS (data flow) =**

[ "0"  
 | "1"  
 ]  
**\*TS\_STATUS\***

-----

DESCRIPTION: status of the temperature sensors in solid state, then thermocouple pair order  
USED IN: CP, TSP  
UNITS: none  
RANGE: [0:healthy, 1:failed]  
DATA TYPE: array (1..2) of logical-1  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: N/A

**TSP\_EXT\_IN (data flow) =**

SS\_TEMP  
+ THERMO\_TEMP

**TSP\_RP\_IN (data flow) =**

M1  
+ M2  
+ M3  
+ M4  
+ T1  
+ T2  
+ T3  
+ T4

**VELOCITY\_ERROR (data flow) =****\*VELOCITY\_ERROR\***

-----

DESCRIPTION: distance from velocity-altitude contour (difference in velocities from actual to desired on contour)  
USED IN: AECLP, CP, GP  
UNITS: meters/sec  
RANGE: [-300, 20]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD

**YE\_INTEGRAL (data flow) =**

\*YE\_INTEGRAL\*

-----

DESCRIPTION: integral portion of yaw error equation  
USED IN: AECLP, CP  
UNITS: meters  
RANGE: [-100, 100]  
DATA TYPE: real-8  
ATTRIBUTE: data  
DATA STORE: GUIDANCE\_STATE  
ACCURACY: TBD

**YE\_MAX (data flow) =**

\*YE\_MAX\*

-----

DESCRIPTION: maximum yaw error tolerable  
USED IN: AECLP  
UNITS: none  
RANGE: [-1, 1]  
DATA TYPE: array (1..2) of real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

**YE\_MIN (data flow) =**

\*YE\_MIN\*

-----

DESCRIPTION: minimum yaw error tolerable  
USED IN: AECLP  
UNITS: none



RANGE: [-1, 1]  
DATA TYPE: array (1..2) of real-8  
ATTRIBUTE: data  
DATA STORE: RUN\_PARAMETERS  
ACCURACY: N/A

## **Appendix C: Source Code for the Pluto Implementation of the Guidance and Control Software**

Author: Philip Morris, Lockheed Martin Engineering and Sciences Corp.

This document was produced as part of Guidance and Control Software (GCS) Project conducted at NASA Langley Research Center. Although some of the requirements for the Guidance and Control Software application were derived from the NASA Viking Mission to Mars, this document does not contain data from an actual NASA mission.

```

*****
* Module:      AECLP.FOR
* Facility:    Pluto
* P-Spec:     3.2
* Abstract:
*   This module contains the implementation of the functional
*   requirements for AECLP.
*
* List of Routines:
*   subroutine AECLP
*****

```

```

*****
* Title: AECLP
* Facility: Pluto
* Abstract:
*   1) determine the current operational status of the axial engines.
*   2) generate the appropriate axial engine commands.
*
* Arguments: None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*****

```

```

subroutine AECLP

implicit none

*** include the global common stores ***

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

*** include constant definitions ***

include 'constants.for'

*** declare local variables ***

real*8      q_over_omega
real*8      pitch_error
real*8      pitch_error_limit
real*8      yaw_error
real*8      yaw_error_limit
real*8      thrust_error

integer*4 i

```

```

*****
* 1) Determine the current operational status of the axial engines.
*****

```

```

    AE_STATUS = K$HEALTHY

```

```

*****

```

```

* 2) Generate the appropriate axial engine commands.
*
* Determine if the axial engines are on. If the axial engines
* are "off" (value 0) then the axial engine commands are "0".
* Otherwise, further processing is required in order to determine
* the appropriate axial engine commands.
*****

```

```

    if (AE_SWITCH .EQ. K$AXIAL_ENGINES_ARE_OFF) then
        AE_CMD(1) = 0
        AE_CMD(2) = 0
        AE_CMD(3) = 0
    else

```

```

*****

```

```

* The axial engines are "on" so further processing is required.
*

```

```

* 2A) determine the axial engine temperature.
*****

```

```

*** range check the current altitude ***

```

```

    call RANGE_CHECK(GP_ALTITUDE(0), K$GP_ALTITUDE$LB,
    &                 K$GP_ALTITUDE$UB, 'AECLP', K$GP_ALTITUDE$NAME)

```

```

*****

```

```

* The three possible engine temperature states are: "Cold" (value 0),
* "Warming up" (value 1), and "Hot" (value 2). The current temperature
* of the axial engines is stored in the data element AE_TEMP.
*****

```

```

    if (GP_ALTITUDE(0) .LE. ENGINES_ON_ALTITUDE) then

        if (AE_TEMP .EQ. K$COLD) then

            if ((FRAME_COUNTER - FRAME_ENGINES_IGNITED) *
            &      DELTA_T .LT. FULL_UP_TIME) then
                AE_TEMP = K$WARMING_UP
            end if

            else if (AE_TEMP .EQ. K$WARMING_UP) then
                if ((FRAME_COUNTER - FRAME_ENGINES_IGNITED) *
            &      DELTA_T .GE. FULL_UP_TIME) then

```

```

        AE_TEMP = K$HOT
    end if
end if
end if

```

```

*****

```

```

* 2B) Compute the pitch error limit.

```

```

*****

```

```

*** range check the pitch error integral ***

```

```

    call RANGE_CHECK(PE_INTEGRAL, K$PE_INTEGRAL$LB,
&                K$PE_INTEGRAL$SUB, 'AECLP', K$PE_INTEGRAL$NAME)

```

```

*** range check the x-axis roll rate ***

```

```

    call RANGE_CHECK(GP_VELOCITY(1, 0), K$GP_VELOCITY$LB,
&                K$GP_VELOCITY$SUB, 'AECLP', K$GP_VELOCITY$NAME)

```

```

*** range check the z-axis roll rate ***

```

```

    call RANGE_CHECK(GP_VELOCITY(3, 0), K$GP_VELOCITY$LB,
&                K$GP_VELOCITY$SUB, 'AECLP', K$GP_VELOCITY$NAME)

```

```

*** check for potential divide by zero condition ***

```

```

    call ZERO_CHECK(GP_VELOCITY(1, 0), 'AECLP')

```

```

*** compute the current value for PE_INTEGRAL ***

```

```

    PE_INTEGRAL = PE_INTEGRAL +
&    (GP_VELOCITY(3, 0) / ABS(GP_VELOCITY(1, 0))) * DELTA_T

```

```

*** range check the pitch error integral (again) ***

```

```

    call RANGE_CHECK(PE_INTEGRAL, K$PE_INTEGRAL$LB,
&                K$PE_INTEGRAL$SUB, 'AECLP', K$PE_INTEGRAL$NAME)

```

```

*** range check the pitch rotational displacement ***

```

```

    call RANGE_CHECK(GP_ROTATION(3, 1), K$GP_ROTATION$LB,
&                K$GP_ROTATION$SUB, 'AECLP', K$GP_ROTATION$NAME)

```

```

*** compute the pitch error limit ***

```

```

    pitch_error_limit = GQ(CL) * GP_ROTATION(3, 1) +
&    GW(CL) * (GP_VELOCITY(3, 0) / ABS(GP_VELOCITY(1, 0))) +
&    GWI(CL) * PE_INTEGRAL

```

```

    if (pitch_error_limit .LT. PE_MIN(CL)) then
        pitch_error_limit = PE_MIN(CL)
    end if

```

```

else if (pitch_error_limit .GT. PE_MAX(CL)) then
  pitch_error_limit = PE_MAX(CL)

end if

*****
* 2C) Compute the yaw error limit.
*****

*** range check the yaw error integral ***

  call RANGE_CHECK(YE_INTEGRAL, K$YE_INTEGRAL$LB,
&                 K$YE_INTEGRAL$SUB, 'AECLP', K$YE_INTEGRAL$NAME)

*** range check the y-axis roll rate ***

  call RANGE_CHECK(GP_VELOCITY(2, 0), K$GP_VELOCITY$LB,
&                 K$GP_VELOCITY$SUB, 'AECLP', K$GP_VELOCITY$NAME)

*** check for potential divide by zero condition ***

  call ZERO_CHECK(GP_VELOCITY(1, 0), 'AECLP')

*** Compute the current value for YE_INTEGRAL ***

  YE_INTEGRAL = YE_INTEGRAL +
&             (GP_VELOCITY(2, 0) / ABS(GP_VELOCITY(1, 0))) * DELTA_T

*** range check the yaw error integral (again) ***

  call RANGE_CHECK(YE_INTEGRAL, K$YE_INTEGRAL$LB,
&                 K$YE_INTEGRAL$SUB, 'AECLP', K$YE_INTEGRAL$NAME)

*** range check the yaw rotational displacement ***

  call RANGE_CHECK(GP_ROTATION(1, 2), K$GP_ROTATION$LB,
&                 K$GP_ROTATION$SUB, 'AECLP', K$GP_ROTATION$NAME)

*** compute the yaw error limit ***

  yaw_error_limit = -GR(CL) * GP_ROTATION(1, 2) +
&                 GV(CL) * (GP_VELOCITY(2, 0) / ABS(GP_VELOCITY(1, 0))) +
&                 GVI(CL) * YE_INTEGRAL

  if (yaw_error_limit .LT. YE_MIN(CL)) then
    yaw_error_limit = YE_MIN(CL)

  else if (yaw_error_limit .GT. YE_MAX(CL)) then
    yaw_error_limit = YE_MAX(CL)

```

```

end if

*****
* 2D) Compute the thrust limiting error.
*****

if (CONTOUR_CROSSED .EQ. K$CONTOUR_CROSSED) then

*** range check the thrust error integral ***

    call RANGE_CHECK(TE_INTEGRAL, K$TE_INTEGRAL$LB,
    &                 K$TE_INTEGRAL$SUB, 'AECLP', K$TE_INTEGRAL$NAME)

*** range check the velocity error ***

    call RANGE_CHECK(VELOCITY_ERROR, K$VELOCITY_ERROR$LB,
    &                 K$VELOCITY_ERROR$SUB, 'AECLP', K$VELOCITY_ERROR$NAME)

*** Compute the current value for TE_INTEGRAL ***

    TE_INTEGRAL = TE_INTEGRAL + VELOCITY_ERROR * DELTA_T

*** range check the thrust error integral (again) ***

    call RANGE_CHECK(TE_INTEGRAL, K$TE_INTEGRAL$LB,
    &                 K$TE_INTEGRAL$SUB, 'AECLP', K$TE_INTEGRAL$NAME)

*** range check the attitude component ***

    call RANGE_CHECK(GP_ATTITUDE(1, 3, 0), K$GP_ATTITUDE$LB,
    &                 K$GP_ATTITUDE$SUB, 'AECLP', K$GP_ATTITUDE$NAME)

*** range check the x-axis acceleration ***

    call RANGE_CHECK(A_ACCELERATION(1, 0),
    &                 K$A_ACCELERATION$LB,
    &                 K$A_ACCELERATION$SUB, 'AECLP', K$A_ACCELERATION$NAME)

*** range check the thrust error limit ***

    call RANGE_CHECK(TE_LIMIT, K$TE_LIMIT$LB,
    &                 K$TE_LIMIT$SUB, 'AECLP', K$TE_LIMIT$NAME)

***
* v1 Changes for AR#23. Item 8. Added check for zero.
***

    call ZERO_CHECK(OMEGA, 'AECLP')
    q_over_omega = (GA * (-GAX * (A_ACCELERATION(1,0) +
    &                 GRAVITY * GP_ATTITUDE(1,3,0)) + GVE *
    &                 VELOCITY_ERROR + GVEI(CL) * TE_INTEGRAL)) /
    &                 OMEGA

```

```

***
* v1 Changes for AR#23. End Change.
***
      TE_LIMIT = q_over_omega +
&      (TE_LIMIT - q_over_omega) * EXP(-OMEGA * DELTA_T)

*** range check the current value of for the thrust error limit ***

      call RANGE_CHECK(TE_LIMIT, K$TE_LIMIT$LB,
&      K$TE_LIMIT$UB, 'AECLP', K$TE_LIMIT$NAME)

      if (TE_LIMIT .LT. TE_MIN(CL)) then
        TE_LIMIT = TE_MIN(CL)

      else if (TE_LIMIT .GT. TE_MAX(CL)) then
        TE_LIMIT = TE_MAX(CL)
      end if
    end if

*****
* 2E) Compute the pitch, yaw and thrust errors.
*****

*** Note, to get here (AE_SWITCH = K$AXIAL_ENGINES_ON) ***

      if (CHUTE_RELEASED .EQ. K$CHUTE_RELEASED) then

        if (CONTOUR_CROSSED .EQ. K$CONTOUR_NOT_CROSSED) then
          pitch_error = pitch_error_limit
          yaw_error   = yaw_error_limit
          thrust_error = TE_DROP

        else
          pitch_error = pitch_error_limit
          yaw_error   = yaw_error_limit
          thrust_error = TE_LIMIT
        end if

      else
        ***              "Chute Attached" ***
          pitch_error = GQ(CL) * GP_ROTATION(3, 1)
          yaw_error   = -GR(CL) * GP_ROTATION(1, 2)
          thrust_error = TE_INIT

      end if

*****
* 2F) Compute the axial engine value settings.
*****

```



```

INTERNAL_CMD(1) = GP1 * pitch_error + thrust_error
INTERNAL_CMD(2) = GP2 * pitch_error -
& GPY * yaw_error + thrust_error
INTERNAL_CMD(3) = GP2 * pitch_error +
& GPY * yaw_error + thrust_error

*****
* 2G) Convert the axial engine value settings to engine commands.
*****

*** range check the internal command ***

    call RANGE_CHECK(INTERNAL_CMD(1), K$INTERNAL_CMD$LB,
& K$INTERNAL_CMD$SUB, 'AECLP', K$INTERNAL_CMD$NAME)

    call RANGE_CHECK(INTERNAL_CMD(2), K$INTERNAL_CMD$LB,
& K$INTERNAL_CMD$SUB, 'AECLP', K$INTERNAL_CMD$NAME)

    call RANGE_CHECK(INTERNAL_CMD(3), K$INTERNAL_CMD$LB,
& K$INTERNAL_CMD$SUB, 'AECLP', K$INTERNAL_CMD$NAME)

*** do the conversion for each engine ***

    do i = 1,3

        if (INTERNAL_CMD(i) .LT. 0) then
            AE_CMD(i) = 0

***
* v1 Changes for AR#23. Item 2. Added D0 to 0.5
***

            else if (INTERNAL_CMD(i) .LE. 1) then
                AE_CMD(i) = INT(127 * INTERNAL_CMD(i) + 0.5D0)

***
* v1 Changes for AR#23. End Change.
***

            else
                AE_CMD(i) = 127

            end if
        end do

    end if

    return
end

***** end of module AECLP.FOR *****

```

\*\*\*\*\*

\* Module: ARSP.FOR

\* Facility: Pluto

\* P-Spec: 1.2

\* Abstract:

\* This module contains the implementation of the functional requirements for ARSP.

\*

\* List of Routines:

\* subroutine ARSP

\*\*\*\*\*

\*\*\*\*\*

\* Title: ARSP

\* Facility: Pluto

\* Abstract:

\* 1) maintain the history of the altitude and altimeter sensor data elements

\* 2) determine the operational status of the altimeter radar sensor

\* 3) Report the current altitude.

\*

\* Arguments: None

\*

\* Revision History:

\* v0 15-sep-1994 Rob Angellatta (RKA) Original.

\* v1 10-JAN-1995 Philip Morris (PEM)

\*\*\*\*\*

subroutine ARSP

implicit none

\*\*\* include the global common stores \*\*\*

include 'external.for'

include 'guidance\_state.for'

include 'sensor\_output.for'

include 'run\_parameters.for'

\*\*\* include constant definitions \*\*\*

include 'constants.for'

\*\*\*\*\*

\* 1) Maintain the history of the altitude and the sensor status by

\* "rotating variables."

\*\*\*\*\*

AR\_ALTITUDE(4) = AR\_ALTITUDE(3)

AR\_ALTITUDE(3) = AR\_ALTITUDE(2)

AR\_ALTITUDE(2) = AR\_ALTITUDE(1)

AR\_ALTITUDE(1) = AR\_ALTITUDE(0)

AR\_STATUS(4) = AR\_STATUS(3)  
AR\_STATUS(3) = AR\_STATUS(2)  
AR\_STATUS(2) = AR\_STATUS(1)  
AR\_STATUS(1) = AR\_STATUS(0)

K\_ALT(4) = K\_ALT(3)  
K\_ALT(3) = K\_ALT(2)  
K\_ALT(2) = K\_ALT(1)  
K\_ALT(1) = K\_ALT(0)

\*\*\*\*\*

\* 2) determine the operational status of the altimeter radar sensor.

\*

\* 3) There are three methods for determining the altitude.

\*

\* A) compute altitude from the sensor measurement.

\*

\* B) estimate altitude by fitting a third-order polynomial to the  
\* altitude history data values.

\*

\* C) report the altitude as the most recently reported altitude.

\*\*\*\*\*

\*\*\*\*\*

\* If an echo has been received, then the lower order fifteen bits of  
\* AR\_COUNTER contain the raw sensor measurement, and the upper bit of  
\* AR\_COUNTER will be clear (ie: 0). When an echo has not been received,  
\* the AR\_COUNTER will contain 16 set bits (ie: 0xFFFF).

\*

\* The data type of AR\_COUNTER is integer\*2 and the valid value range  
\* is specified as (-1, 32767). This implementation assumes that integer  
\* values are represented by twos complement. Thus, when an echo has not  
\* been received, the AR\_COUNTER will contain the value of -1. Similarly,  
\* when an echo has been received, AR\_COUNTER will contain a non-negative  
\* value.

\*\*\*\*\*

if (AR\_COUNTER .NE. -1) then  
    AR\_STATUS(0) = K\$HEALTHY  
    K\_ALT(0) = 1

\*\*\* A) compute the altitude from the sensor measurement \*\*\*

\*\*\*

\* v1 Changes for PR#24. Item 8. Changed 3E08 to 3D08.

\*\*\*

\* AR\_ALTITUDE(0) = (AR\_COUNTER \* 3E08) / (2.0 \* AR\_FREQUENCY)  
AR\_ALTITUDE(0) = (AR\_COUNTER \* 3D08) / (2.0 \* AR\_FREQUENCY)

\*\*\*

\* v1 Changes for PR#24. End Change.

\*\*\*

```

else
*           no echo received
  AR_STATUS(0) = K$FAILED

*** if at least one of the history sensor status is "failed" ***

  if ((AR_STATUS(1) .EQ. K$FAILED) .OR.
    &   (AR_STATUS(2) .EQ. K$FAILED) .OR.
    &   (AR_STATUS(3) .EQ. K$FAILED) .OR.
    &   (AR_STATUS(4) .EQ. K$FAILED)) then

    K_ALT(0)    = 0

*** C) return previously computed value ***

*** range check the altitude ****

    call RANGE_CHECK(AR_ALTITUDE(1),K$AR_ALTITUDE$LB,
    &                 K$AR_ALTITUDE$UB,'ARSP', K$AR_ALTITUDE$NAME)

***     the value stored in AR_ALTITUDE(1) is already
***     stored in AR_ALTITUDE(0)!

else
*           all sensor status histories are "healthy"

*** B) extrapolate the altitude ***

    K_ALT(0) = 1

*** range check the altitude ****

***
*   v1 Changes for PR#24. Extra. Changed 'ASP' to 'ARSP'.
***
    call RANGE_CHECK(AR_ALTITUDE(1),K$AR_ALTITUDE$LB,
    &                 K$AR_ALTITUDE$UB,'ARSP', K$AR_ALTITUDE$NAME)

    call RANGE_CHECK(AR_ALTITUDE(2),K$AR_ALTITUDE$LB,
    &                 K$AR_ALTITUDE$UB,'ARSP', K$AR_ALTITUDE$NAME)

    call RANGE_CHECK(AR_ALTITUDE(3),K$AR_ALTITUDE$LB,
    &                 K$AR_ALTITUDE$UB,'ARSP', K$AR_ALTITUDE$NAME)

    call RANGE_CHECK(AR_ALTITUDE(4),K$AR_ALTITUDE$LB,
    &                 K$AR_ALTITUDE$UB,'ARSP', K$AR_ALTITUDE$NAME)

    AR_ALTITUDE(0) = 4*AR_ALTITUDE(1) - 6*AR_ALTITUDE(2) +
    &               4*AR_ALTITUDE(3) - AR_ALTITUDE(4)

***

```

```
*      v1 Changes for PR#24. End Change.  
***
```

```
      end if  
end if
```

```
      return  
end
```

```
***** end of module arsp.for *****
```

```

*****
* Module:    ASP.FOR
* Facility:  Pluto
* P-Spec:   1.3
* Abstract:
*   This module contains the implementation of the functional
*   requirements for ASP.
*
* List of Routines:
*   subroutine ASP
*****

```

```

*****
* Title: ASP
* Facility:  Pluto
* Abstract:
*   1) maintaining the history of the accelerations and accelerometer
*   sensor statuses
*   2) determining the operational status of the accelerometer sensors
*   3) Reporting the current vehicle accelerations along each of the
*   vehicle's three axes.
*
* Arguments:  None
*
* Revision History:
*   v0  15-sep-1994  Rob Angellatta (RKA) Original.
*   v1  16-MAR-1995  Philip Morris (PEM)
*****

```

```

subroutine ASP

implicit none

*** define local constants ***

*** include the global common stores ***

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

*** include constant definitions ***

include 'constants.for'

*** declare local variables ***

real*8      temp
real*8      accel_m(3)

```

integer\*4 i

real\*8            mean  
real\*8            sd

\*\*\*\*\*

\* 1) Maintain the history of the vehicle accelerations and  
\* accelerometer sensor status by "rotating variables."

\*\*\*\*\*

A\_ACCELERATION(1, 4) = A\_ACCELERATION(1, 3)  
A\_ACCELERATION(1, 3) = A\_ACCELERATION(1, 2)  
A\_ACCELERATION(1, 2) = A\_ACCELERATION(1, 1)  
A\_ACCELERATION(1, 1) = A\_ACCELERATION(1, 0)

A\_ACCELERATION(2, 4) = A\_ACCELERATION(2, 3)  
A\_ACCELERATION(2, 3) = A\_ACCELERATION(2, 2)  
A\_ACCELERATION(2, 2) = A\_ACCELERATION(2, 1)  
A\_ACCELERATION(2, 1) = A\_ACCELERATION(2, 0)

A\_ACCELERATION(3, 4) = A\_ACCELERATION(3, 3)  
A\_ACCELERATION(3, 3) = A\_ACCELERATION(3, 2)  
A\_ACCELERATION(3, 2) = A\_ACCELERATION(3, 1)  
A\_ACCELERATION(3, 1) = A\_ACCELERATION(3, 0)

A\_STATUS(1, 3) = A\_STATUS(1, 2)  
A\_STATUS(1, 2) = A\_STATUS(1, 1)  
A\_STATUS(1, 1) = A\_STATUS(1, 0)

A\_STATUS(2, 3) = A\_STATUS(2, 2)  
A\_STATUS(2, 2) = A\_STATUS(2, 1)  
A\_STATUS(2, 1) = A\_STATUS(2, 0)

A\_STATUS(3, 3) = A\_STATUS(3, 2)  
A\_STATUS(3, 2) = A\_STATUS(3, 1)  
A\_STATUS(3, 1) = A\_STATUS(3, 0)

\*\*\*\*\*

\* 2) and 3), determine the operational status and the vehicle  
\* accelerations for each axis.

\*\*\*\*\*

\*\*\* range check the atmospheric temperature \*\*\*

call RANGE\_CHECK(ATMOSPHERIC\_TEMP,K\$ATMOSPHERIC\_TEMP\$LB,  
&            K\$ATMOSPHERIC\_TEMP\$UB,'ASP', K\$ATMOSPHERIC\_TEMP\$NAME)

\*\*\* compute the preliminary value for the accelerations \*\*\*

temp = (G1 \* ATMOSPHERIC\_TEMP) + (G2 \* ATMOSPHERIC\_TEMP\*\*2)

```

accel_m(1) = A_BIAS(1)+ (A_GAIN_0(1) + temp) * A_COUNTER(1)
accel_m(2) = A_BIAS(2)+ (A_GAIN_0(2) + temp) * A_COUNTER(2)
accel_m(3) = A_BIAS(3)+ (A_GAIN_0(3) + temp) * A_COUNTER(3)

```

```

A_ACCELERATION(1, 0) = ALPHA_MATRIX(1, 1) * accel_m(1) +
& ALPHA_MATRIX(1, 2) * accel_m(2) +
& ALPHA_MATRIX(1, 3) * accel_m(3)

```

```

A_ACCELERATION(2, 0) = ALPHA_MATRIX(2, 1) * accel_m(1) +
& ALPHA_MATRIX(2, 2) * accel_m(2) +
& ALPHA_MATRIX(2, 3) * accel_m(3)

```

```

A_ACCELERATION(3, 0) = ALPHA_MATRIX(3, 1) * accel_m(1) +
& ALPHA_MATRIX(3, 2) * accel_m(2) +
& ALPHA_MATRIX(3, 3) * accel_m(3)

```

```

*****

```

```

* Determine whether or not the preliminary values for the
* accelerations are reasonable. The preliminary value for an
* acceleration is deemed reasonable: 1) if it differs from the mean
* of the previous three measurements by not more than A_SCALE
* standard deviations; 2) when any of the three accelerometer
* history statuses is "unhealthy" (value 1). If a preliminary
* acceleration value is found to be reasonable,
* then it is reported as the acceleration for it's axis. If a
* preliminary value is not found to be reasonable, then the
* mean of the previous three measurements is reported as the
* acceleration for that axis.

```

```

*
* The current value for the sensor status is determined directly
* from the reasonableness of the value of the preliminary
* acceleration. If the preliminary acceleration is reasonable, the
* sensor status is deemed "healthy " (value 0). If the preliminary
* acceleration is not reasonable, the sensor status is deemed
* "unhealthy."

```

```

*****

```

```

do i=1,3

```

```

***

```

```

* v1 PR#27 Item 1. Adjust mean calculation.

```

```

***

```

```

* if((A_STATUS(i, 1) .EQ. K$UNHEALTHY) .OR.
* & (A_STATUS(i, 2) .EQ. K$UNHEALTHY) .OR.
* & (A_STATUS(i, 3) .EQ. K$UNHEALTHY)) then

```

```

*

```

```

*** one or more history statuses are "unhealthy" ***

```

```

*

```

```

* A_STATUS(i, 0) = K$HEALTHY

```

```

*

```

```

* else

```



```

*           all history status are "healthy"
  A_STATUS(i, 0) = K$HEALTHY

  if ((A_STATUS(i, 1) .EQ. K$HEALTHY) .AND.
&      (A_STATUS(i, 2) .EQ. K$HEALTHY) .AND.
&      (A_STATUS(i, 3) .EQ. K$HEALTHY)) then

    if ((A_ACCELERATION(i,1) .NE. A_ACCELERATION(i,2)) .OR.
&       (A_ACCELERATION(i,1) .NE. A_ACCELERATION(i,3))) then
***
* v1 PR#27 End Change.
***

*** compute the mean of the previous three values ***

*** range check the acceleration values ****

    call RANGE_CHECK(A_ACCELERATION(i, 1),K$A_ACCELERATION$LB,
&                   K$A_ACCELERATION$SUB,'ASP', K$A_ACCELERATION$NAME)

    call RANGE_CHECK(A_ACCELERATION(i, 2),K$A_ACCELERATION$LB,
&                   K$A_ACCELERATION$SUB,'ASP', K$A_ACCELERATION$NAME)

    call RANGE_CHECK(A_ACCELERATION(i, 3),K$A_ACCELERATION$LB,
&                   K$A_ACCELERATION$SUB,'ASP', K$A_ACCELERATION$NAME)

***
* v1 PR#27 Item 2. Adjust Standard deviation calculation.
***

*** compute the standard deviation ***

    mean = (A_ACCELERATION(i, 1) +
&          A_ACCELERATION(i, 2) +
&          A_ACCELERATION(i, 3)) / 3.0D0

    temp = ((A_ACCELERATION(i,1) - mean)**2 +
&          (A_ACCELERATION(i,2) - mean)**2 +
&          (A_ACCELERATION(i,3) - mean)**2 )
&          / 3.0D0

    sd = SQRT(temp)

    temp = ABS(mean - A_ACCELERATION(i, 0))
    if (temp .GT. A_SCALE * sd) then
      A_ACCELERATION(i, 0) = mean
      A_STATUS(i, 0) = K$UNHEALTHY
    end if

  end if ! close if block for A_ACCELERATION
end if ! close if block for A_STATUS

```

end do

```
*****
* Note, numerical inaccuracies are inherent in the digital
* representation of real numbers. Computing the variance can
* potentially result in a small negative value, when the previous
* accelerations have identical values. Therefore, the following
* algorithm specifies a separate case for computing the standard
* deviation when the previous accelerations have identical values.
*****
*
*   if ((A_ACCELERATION(i,1) .EQ. A_ACCELERATION(i,2)) .AND.
* &     (A_ACCELERATION(i,1) .EQ. A_ACCELERATION(i,3))) then
*     sd = 0.0
*   else
*     temp = ((A_ACCELERATION(i,1)**2 +
* &           A_ACCELERATION(i,2)**2 +
* &           A_ACCELERATION(i,3)**2) / 3.0) - mean**2
*
*     call NEG_VALUE_CHECK(temp, 'ASP')
*
*     sd = SQRT(temp)
*
*   end if
*
*   if (ABS(mean - A_ACCELERATION(i, 0)) .GT.
* &     A_SCALE * sd) then
*     A_ACCELERATION(i, 0) = mean
*     A_STATUS(i, 0) = K$UNHEALTHY
*   else
*     A_STATUS(i, 0) = K$HEALTHY
*   end if
*
* end if
*
* end do
***
* v1 PR#27 End Change.
***
  return
end

***** end of module asp.for *****
```



```

*****
* Module:      CLPSF.FOR
* Facility:    Pluto
* P-Spec:     3.0
* Abstract:
*   This module contains the entry for the control law processing
*   subframe.
*
* List of Routines:
*   subroutine CLPSF
*****

```

```

*****
* Title: CLPSF
* Facility: Pluto
* Abstract:
*   This routine provides control of the Control Law Processing
*   SubFrame processing.
*
* Arguments: None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 15-Feb-1995 Philip Morris (PEM)
*****

```

```

subroutine CLPSF

```

```

implicit none

```

```

*** execution begins here ***

```

```

call GCS_SIM_RENDEZVOUS

```

```

***

```

```

* v1 Changes for AR#26. Item 1. Correct Spelling

```

```

***

```

```

* call AELCP
  call AECLP

```

```

***

```

```

* v1 Changes for AR#26. Item 1. End Cahnge.

```

```

***

```

```

call RECLP
call CRCP
call CP

```

```

return
end

```

```

***** end of module CLPSF.FOR *****

```

\*\*\*\*\*

\* Module:       CONSTANTS.FOR

\* Facility:      Pluto

\* Abstract:

\*       This module contains the constants used in Pluto. The constants  
\*       consist of values for enumerated types, upper and lower  
\*       bounds, and error reporting text.

\*

\* Revision History:

\*       v0  15-sep-1994 Rob Angellatta (RKA) Original.

\*       v1  30-Nov-1994 Philip Morris (PEM)

\*       v2  10-Jan-1995 Philip Morris (PEM)

\*\*\*\*\*

\*\*\* define constant values (for enumerated types) \*\*\*\*\*

\*\*\* AE\_TEMP values \*\*\*

\*\*\*

\* v1 Changes for AR#23. Item 4. Changed logical\*1 to integer\*2

\*\*\*

integer\*2  K\$COLD  
parameter (K\$COLD               = 0)

integer\*2  K\$WARMING\_UP  
parameter (K\$WARMING\_UP       = 1)

integer\*2  K\$HOT  
parameter (K\$HOT               = 2)

\*\*\*

\* v1 Changes for AR#23. End Change.

\*\*\*

\*\*\* AE\_SWITCH values \*\*\*

logical\*1  K\$AXIAL\_ENGINES\_ARE\_OFF  
parameter (K\$AXIAL\_ENGINES\_ARE\_OFF= 0)

logical\*1  K\$AXIAL\_ENGINES\_ARE\_ON  
parameter (K\$AXIAL\_ENGINES\_ARE\_ON   = 1)

\*\*\* CHUTE\_RELEASED values \*\*\*

logical\*1  K\$CHUTE\_ATTACHED  
parameter (K\$CHUTE\_ATTACHED       = 0)

logical\*1  K\$CHUTE\_RELEASED  
parameter (K\$CHUTE\_RELEASED       = 1)

\*\*\* CL values \*\*\*

integer\*2 K\$FIRST  
parameter (K\$FIRST = 1)

integer\*2 K\$SECOND  
parameter (K\$SECOND = 2)

\*\*\* CONTOUR\_CROSSED values \*\*\*

logical\*1 K\$CONTOUR\_NOT\_CROSSED  
parameter (K\$CONTOUR\_NOT\_CROSSED = 0)

logical\*1 K\$CONTOUR\_CROSSED  
parameter (K\$CONTOUR\_CROSSED = 1)

\*\*\* RE\_CMD values \*\*\*

integer\*2 K\$CCW  
parameter (K\$CCW = 0)

integer\*2 K\$CW  
parameter (K\$CW = 1)

integer\*2 K\$OFF  
parameter (K\$OFF = 0)

integer\*2 K\$MINIMUM  
parameter (K\$MINIMUM = 2)

integer\*2 K\$INTERMEDIATE  
parameter (K\$INTERMEDIATE = 4)

integer\*2 K\$MAXIMUM  
parameter (K\$MAXIMUM = 6)

\*\*\* RE\_SWITCH values \*\*\*

logical\*1 K\$ROLL\_ENGINES\_ARE\_OFF  
parameter (K\$ROLL\_ENGINES\_ARE\_OFF = 0)

logical\*1 K\$ROLL\_ENGINES\_ARE\_ON  
parameter (K\$ROLL\_ENGINES\_ARE\_ON = 1)

\*\*\* Sensor statuses \*\*\*

logical\*1 K\$HEALTHY  
parameter (K\$HEALTHY = 0)

logical\*1 K\$UNHEALTHY  
parameter (K\$UNHEALTHY = 1)

```

logical*1 K$FAILED
parameter (K$FAILED = 1)

*** TD_SENSED values ***

logical*1 K$TOUCH_DOWN_NOT_SENSED
parameter (K$TOUCH_DOWN_NOT_SENSED = 0)

logical*1 K$TOUCH_DOWN_SENSED
parameter (K$TOUCH_DOWN_SENSED = 1)

*** TDLR_STATE values ***

logical*1 K$BEAM_UNLOCKED
parameter (K$BEAM_UNLOCKED= 0)

logical*1 K$BEAM_LOCKED
parameter (K$BEAM_LOCKED = 1)

*** define Range checking constants ****

*** upper and lower bounds ***

***
* v1 Changes for AR#23. Item 3. Added D0 to some reals.
***
real*8          K$_ACCELERATION$LB
parameter (K$_ACCELERATION$LB = -20.0)

real*8          K$_ACCELERATION$UB
parameter (K$_ACCELERATION$UB = 5.0)

real*8          K$_ALTITUDE$LB
parameter (K$_ALTITUDE$LB = 0.0)

real*8          K$_ALTITUDE$UB
parameter (K$_ALTITUDE$UB = 2000.0)

real*8          K$ATMOSPHERIC_TEMP$LB
parameter (K$ATMOSPHERIC_TEMP$LB = -200.0)

real*8          K$ATMOSPHERIC_TEMP$UB
parameter (K$ATMOSPHERIC_TEMP$UB = 25.0)

real*8          K$_ROTATION$LB
parameter (K$_ROTATION$LB = -1.0)

real*8          K$_ROTATION$UB
parameter (K$_ROTATION$UB = 1.0)

real*8          K$_ALTITUDE$LB

```

parameter (K\$GP\_ALTITUDE\$LB = 0.0)  
  
 real\*8 K\$GP\_ALTITUDE\$SUB  
 parameter (K\$GP\_ALTITUDE\$SUB = 2000.0)  
  
 real\*8 K\$GP\_ATTITUDE\$LB  
 parameter (K\$GP\_ATTITUDE\$LB = -1.0)  
  
 real\*8 K\$GP\_ATTITUDE\$SUB  
 parameter (K\$GP\_ATTITUDE\$SUB = 1.0)  
  
 real\*8 K\$GP\_ROTATION\$LB  
 parameter (K\$GP\_ROTATION\$LB = -1.0)  
  
 real\*8 K\$GP\_ROTATION\$SUB  
 parameter (K\$GP\_ROTATION\$SUB = 1.0)  
  
 real\*8 K\$GP\_VELOCITY\$LB  
 parameter (K\$GP\_VELOCITY\$LB = -100.0)  
  
 real\*8 K\$GP\_VELOCITY\$SUB  
 parameter (K\$GP\_VELOCITY\$SUB = 100.0)  
  
 real\*8 K\$INTERNAL\_CMD\$LB  
 parameter (K\$INTERNAL\_CMD\$LB = -0.7D0)  
  
 real\*8 K\$INTERNAL\_CMD\$SUB  
 parameter (K\$INTERNAL\_CMD\$SUB = 1.7D0)  
  
 real\*8 K\$PE\_INTEGRAL\$LB  
 parameter (K\$PE\_INTEGRAL\$LB = -100.0)  
  
 real\*8 K\$PE\_INTEGRAL\$SUB  
 parameter (K\$PE\_INTEGRAL\$SUB = 100.0)  
  
 real\*8 K\$TDLR\_VELOCITY\$LB  
 parameter (K\$TDLR\_VELOCITY\$LB = -100.0)  
  
 real\*8 K\$TDLR\_VELOCITY\$SUB  
 parameter (K\$TDLR\_VELOCITY\$SUB = 100.0)  
  
 real\*8 K\$TE\_INTEGRAL\$LB  
 parameter (K\$TE\_INTEGRAL\$LB = -100.0)  
  
 real\*8 K\$TE\_INTEGRAL\$SUB  
 parameter (K\$TE\_INTEGRAL\$SUB = 100.0)  
  
 real\*8 K\$TE\_LIMIT\$LB  
 parameter (K\$TE\_LIMIT\$LB = -100.0)  
  
 real\*8 K\$TE\_LIMIT\$SUB



```

parameter (K$TE_LIMIT$UB          = 100.0)
***
* v2 Changes for AR#24. Item 5. Changed signs.
***
real*8          K$THETA$UB
parameter (K$THETA$UB          = 3.141592653589793)

real*8          K$THETA$LB
parameter (K$THETA$LB          = -3.141592653589793)

*   real*8          K$THETA$UB
*   parameter(K$THETA$UB          = -3.141592653589793)
*
*   real*8          K$THETA$LB
*   parameter(K$THETA$LB          = 3.141592653589793)
***
* v2 Changes for AR#24. End Change.
***

real*8          K$VELOCITY_ERROR$LB
parameter (K$VELOCITY_ERROR$LB = -300.0)

real*8          K$VELOCITY_ERROR$UB
parameter (K$VELOCITY_ERROR$UB = 20.0)

real*8          K$YE_INTEGRAL$LB
parameter (K$YE_INTEGRAL$LB    = -100.0)

real*8          K$YE_INTEGRAL$UB
parameter (K$YE_INTEGRAL$UB    = 100.0)

***
* v1 Changes for AR#23. End Change.
***

*** define constants for data element names used in error messages ****

character*(*)   K$A_ACCELERATION$NAME
parameter (K$A_ACCELERATION$NAME = 'A_ACCELERATION')

character*(*)   K$AR_ALTITUDE$NAME
parameter (K$AR_ALTITUDE$NAME    = 'AR_ALTITUDE')

character*(*)   K$ATMOSPHERIC_TEMP$NAME
parameter (K$ATMOSPHERIC_TEMP$NAME= 'ATMOSPHERIC_TEMP')

character*(*)   K$G_ROTATION$NAME
parameter (K$G_ROTATION$NAME     = 'G_ROTATION')

character*(*)   K$GP_ALTITUDE$NAME
parameter (K$GP_ALTITUDE$NAME    = 'GP_ALTITUDE')

```

character\*(\*) K\$GP\_ATTITUDE\$NAME  
parameter (K\$GP\_ATTITUDE\$NAME = 'GP\_ATTITUDE')

character\*(\*) K\$GP\_ROTATION\$NAME  
parameter (K\$GP\_ROTATION\$NAME = 'GP\_ROTATION')

character\*(\*) K\$GP\_VELOCITY\$NAME  
parameter (K\$GP\_VELOCITY\$NAME = 'GP\_VELOCITY')

character\*(\*) K\$INTERNAL\_CMD\$NAME  
parameter (K\$INTERNAL\_CMD\$NAME = 'INTERNAL\_CMD')

character\*(\*) K\$PE\_INTEGRAL\$NAME  
parameter (K\$PE\_INTEGRAL\$NAME = 'PE\_INTEGRAL')

character\*(\*) K\$TDLR\_VELOCITY\$NAME  
parameter (K\$TDLR\_VELOCITY\$NAME = 'TDLR\_VELOCITY')

character\*(\*) K\$TE\_INTEGRAL\$NAME  
parameter (K\$TE\_INTEGRAL\$NAME = 'TE\_INTEGRAL')

character\*(\*) K\$TE\_LIMIT\$NAME  
parameter (K\$TE\_LIMIT\$NAME = 'TE\_LIMIT')

character\*(\*) K\$THETA\$NAME  
parameter (K\$THETA\$NAME = 'THETA')

character\*(\*) K\$VELOCITY\_ERROR\$NAME  
parameter (K\$VELOCITY\_ERROR\$NAME = 'VELOCITY\_ERROR')

character\*(\*) K\$YE\_INTEGRAL\$NAME  
parameter (K\$YE\_INTEGRAL\$NAME = 'YE\_INTEGRAL')

\*\*\*\*\* end of module CONSTANTS.FOR \*\*\*\*\*

```

*****
* Module:      CP.FOR
* Facility:    Pluto
* P-Spec:     2.3
* Abstract:
*   This module contains the implementation of the functional
*   requirements for CP.
*
* List of Routines:
*   subroutine CP
*   function  CRC16
*****

```

```

*****
* Title: CP
* Facility: Pluto
* Abstract:
*   1) determine the current operational status of the communicator.
*   2) construct a telemetry data packet.
*
* Arguments: None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 13-jan-1995 Philip Morris (PEM)
*****

```

```

subroutine CP

implicit none

*** include the global common stores ***

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

*** include constant definitions ***

include 'constants.for'

*** define local constants ***

*** the byte count (size in bytes) of the three packets ***

integer*4 K$SP_SIZE
parameter (K$SP_SIZE = 129)

integer*4 K$GP_SIZE

```

```

parameter (K$GP_SIZE = 173)

integer*4 K$CLP_SIZE
parameter (K$CLP_SIZE = 45)

*** declare local functions ***

integer*2 CRC16

*** declare local variables ***
integer*2 seq_temp
logical*1 seq_temp_char(2)
equivalence (seq_temp,seq_temp_char(1))

*****
* 1) Determine the current operational status of the communicator.
*****

C_STATUS = 0

*****
* 2) Construct a telemetry data packet.
*****

*****
* 2A) Get synchronization pattern.
*****

PACKET.sync_pattern = COMM_SYNC_PATTERN

*****
* 2B) Determine the sequence number.
*****

seq_temp = MOD(3*(FRAME_COUNTER-1)+
& (SUBFRAME_COUNTER-1), 256)
PACKET.seq_number = seq_temp_char(1)

*****
* 2C) Prepare the data mask,
* 2D) Prepare the data, and
* 2E) Compute the checksum.
*
* The 'PACKET' data structure is defined in module EXTERNAL.FOR
*****

if (SUBFRAME_COUNTER .EQ. 1) then
PACKET.DATA_MASK = '1F20F1F4'X

PACKET.sp.ar_altitude = AR_ALTITUDE(0)
PACKET.sp.ar_status = AR_STATUS(0)

```

```

PACKET.sp.atmospheric_temp = ATMOSPHERIC_TEMP
PACKET.sp.a_acceleration(1)= A_ACCELERATION(1,0)
PACKET.sp.a_acceleration(2)= A_ACCELERATION(2,0)
PACKET.sp.a_acceleration(3)= A_ACCELERATION(3,0)
PACKET.sp.a_status(1)    = A_STATUS(1,0)
PACKET.sp.A_STATUS(2)    = A_STATUS(2,0)
PACKET.sp.a_status(3)    = A_STATUS(3,0)
PACKET.sp.c_status      = C_STATUS
PACKET.sp.g_rotation(1) = G_ROTATION(1,0)
PACKET.sp.g_rotation(2) = G_ROTATION(2,0)
PACKET.sp.g_rotation(3) = G_ROTATION(3,0)
PACKET.sp.g_status      = G_STATUS
PACKET.sp.k_alt         = K_ALT(0)
PACKET.sp.k_matrix(1)   = K_MATRIX(1,1,0)
PACKET.sp.k_matrix(2)   = K_MATRIX(2,2,0)
PACKET.sp.k_matrix(3)   = K_MATRIX(3,3,0)
PACKET.sp.tdlr_state(1) = TDLR_STATE(1)
PACKET.sp.tdlr_state(2) = TDLR_STATE(2)
PACKET.sp.tdlr_state(3) = TDLR_STATE(3)
PACKET.sp.tdlr_state(4) = TDLR_STATE(4)
PACKET.sp.tdlr_status(1) = TDLR_STATUS(1)
PACKET.sp.tdlr_status(2) = TDLR_STATUS(2)
PACKET.sp.tdlr_status(3) = TDLR_STATUS(3)
PACKET.sp.tdlr_status(4) = TDLR_STATUS(4)
PACKET.sp.tdlr_velocity(1) = TDLR_VELOCITY(1,0)
PACKET.sp.tdlr_velocity(2) = TDLR_VELOCITY(2,0)
PACKET.sp.tdlr_velocity(3) = TDLR_VELOCITY(3,0)
PACKET.sp.tds_status    = TDS_STATUS
PACKET.sp.td_sensed     = TD_SENSED
PACKET.sp.ts_status(1)  = TS_STATUS(1)
PACKET.sp.ts_status(2)  = TS_STATUS(2)
***
* v1 PR#25 Item 1. Send whole packet.
***
*   PACKET.sp.checksum    = CRC16(PACKET.sp, K$SP_SIZE)
*   PACKET.sp.checksum    = CRC16(PACKET.PACKET, K$SP_SIZE)
***
* v1 PR#25 End Change.
***

else if (SUBFRAME_COUNTER .EQ. 2) then
  PACKET.data_mask = '007F0002'X

  PACKET.gp.contour_crossed = CONTOUR_CROSSED
  PACKET.gp.c_status      = C_STATUS
  PACKET.gp.gp_altitude   = GP_ALTITUDE(0)

*** first element of array changes most rapidly ***

PACKET.gp.gp_attitude(1) = GP_ATTITUDE(1, 1, 0)
PACKET.gp.gp_attitude(2) = GP_ATTITUDE(2, 1, 0)

```

```

PACKET.gp.gp_attitude(3) = GP_ATTITUDE(3, 1, 0)
PACKET.gp.gp_attitude(4) = GP_ATTITUDE(1, 2, 0)
PACKET.gp.gp_attitude(5) = GP_ATTITUDE(2, 2, 0)
PACKET.gp.gp_attitude(6) = GP_ATTITUDE(3, 2, 0)
PACKET.gp.gp_attitude(7) = GP_ATTITUDE(1, 3, 0)
PACKET.gp.gp_attitude(8) = GP_ATTITUDE(2, 3, 0)
PACKET.gp.gp_attitude(9) = GP_ATTITUDE(3, 3, 0)

PACKET.gp.gp_phase      = GP_PHASE

PACKET.gp.gp_rotation(1) = GP_ROTATION(2, 1)
PACKET.gp.gp_rotation(2) = GP_ROTATION(3, 1)
PACKET.gp.gp_rotation(3) = GP_ROTATION(1, 2)
PACKET.gp.gp_rotation(4) = GP_ROTATION(3, 2)
PACKET.gp.gp_rotation(5) = GP_ROTATION(1, 3)
PACKET.gp.gp_rotation(6) = GP_ROTATION(2, 3)

PACKET.gp.gp_velocity(1) = GP_VELOCITY(1, 0)
PACKET.gp.gp_velocity(2) = GP_VELOCITY(2, 0)
PACKET.gp.gp_velocity(3) = GP_VELOCITY(3, 0)

PACKET.gp.velocity_error = VELOCITY_ERROR
***
* v1 PR#25 Item 1. Send whole packet.
***
*   PACKET.gp.checksum      = CRC16(PACKET.gp, K$GP_SIZE)
*   PACKET.gp.checksum      = CRC16(PACKET.PACKET, K$GP_SIZE)
***
* v1 PR#25 End Change.
***

else
  PACKET.data_mask = 'E0A00E09'X

  PACKET.clp.ae_cmd(1)      = AE_CMD(1)
  PACKET.clp.ae_cmd(2)      = AE_CMD(2)
  PACKET.clp.ae_cmd(3)      = AE_CMD(3)
  PACKET.clp.ae_status      = AE_STATUS
  PACKET.clp.ae_temp        = AE_TEMP
  PACKET.clp.chute_released = CHUTE_RELEASED
  PACKET.clp.c_status       = C_STATUS
  PACKET.clp.pe_integral    = PE_INTEGRAL
  PACKET.clp.re_cmd         = RE_CMD
  PACKET.clp.re_status      = RE_STATUS
  PACKET.clp.te_integral    = TE_INTEGRAL
  PACKET.clp.ye_integral    = YE_INTEGRAL
***
* v1 PR#25 Item 1. Send whole packet.
***
*   PACKET.clp.checksum     = CRC16(PACKET.clp, K$CLP_SIZE)
*   PACKET.clp.checksum     = CRC16(PACKET.PACKET, K$CLP_SIZE)

```

```

***
* v1 PR#25 End Change.
***

    end if

    return
end

***** end of subroutine CP *****

*****
* Title: CRC16
* Facility: Pluto
* Abstract:
* Compute the Cyclic Redundancy Code of the specified buffer using
* CRC-16 as the generator polynomial.
*
* Arguments:
* character*(*) message - address of first byte of message.
* integer*4 bytcount - count of bytes in message.
*
* Returns:
* integer*2 crc16 - the bit checksum of the specified message.
*
* Revision History:
* v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

integer*2 function CRC16(message, bytcount)

implicit none

*** declare the arguments ***

integer*4 bytcount
byte message(bytcount)

*** declare local variables ***

integer*4 i
logical*2 index
integer*2 temp

*** The "signature" table for the CRC-16 generator polynomial 0xA001 ***

integer*2 crc16_table(0:255)

data (crc16_table(i),i= 0, 7)
& /'0000'X, 'c0c1'X, 'c181'X, '0140'X,
& 'c301'X, '03c0'X, '0280'X, 'c241'X/

```

```

data (crc16_table(i),i= 8, 15)
&      /'c601'X, '06c0'X, '0780'X, 'c741'X,
&      '0500'X, 'c5c1'X, 'c481'X, '0440'X/
data (crc16_table(i),i= 16, 23)
&      /'cc01'X, '0cc0'X, '0d80'X, 'cd41'X,
&      '0f00'X, 'cfc1'X, 'ce81'X, '0e40'X/
data (crc16_table(i),i= 24, 31)
&      /'0a00'X, 'cac1'X, 'cb81'X, '0b40'X,
&      'c901'X, '09c0'X, '0880'X, 'c841'X/
data (crc16_table(i),i= 32, 39)
&      /'d801'X, '18c0'X, '1980'X, 'd941'X,
&      '1b00'X, 'dbc1'X, 'da81'X, '1a40'X/
data (crc16_table(i),i= 40, 47)
&      /'1e00'X, 'dec1'X, 'df81'X, '1f40'X,
&      'dd01'X, '1dc0'X, '1c80'X, 'dc41'X/
data (crc16_table(i),i= 48, 55)
&      /'1400'X, 'd4c1'X, 'd581'X, '1540'X,
&      'd701'X, '17c0'X, '1680'X, 'd641'X/
data (crc16_table(i),i= 56, 63)
&      /'d201'X, '12c0'X, '1380'X, 'd341'X,
&      '1100'X, 'd1c1'X, 'd081'X, '1040'X/
data (crc16_table(i),i= 64, 71)
&      /'f001'X, '30c0'X, '3180'X, 'f141'X,
&      '3300'X, 'f3c1'X, 'f281'X, '3240'X/
data (crc16_table(i),i= 72, 79)
&      /'3600'X, 'f6c1'X, 'f781'X, '3740'X,
&      'f501'X, '35c0'X, '3480'X, 'f441'X/
data (crc16_table(i),i= 80, 87)
&      /'3c00'X, 'fcc1'X, 'fd81'X, '3d40'X,
&      'ff01'X, '3fc0'X, '3e80'X, 'fe41'X/
data (crc16_table(i),i= 88, 95)
&      /'fa01'X, '3ac0'X, '3b80'X, 'fb41'X,
&      '3900'X, 'f9c1'X, 'f881'X, '3840'X/
data (crc16_table(i),i= 96,103)
&      /'2800'X, 'e8c1'X, 'e981'X, '2940'X,
&      'eb01'X, '2bc0'X, '2a80'X, 'ea41'X/
data (crc16_table(i),i=104,111)
&      /'ee01'X, '2ec0'X, '2f80'X, 'ef41'X,
&      '2d00'X, 'edc1'X, 'ec81'X, '2c40'X/
data (crc16_table(i),i=112,119)
&      /'e401'X, '24c0'X, '2580'X, 'e541'X,
&      '2700'X, 'e7c1'X, 'e681'X, '2640'X/
data (crc16_table(i),i=120,127)
&      /'2200'X, 'e2c1'X, 'e381'X, '2340'X,
&      'e101'X, '21c0'X, '2080'X, 'e041'X/
data (crc16_table(i),i=128,135)
&      /'a001'X, '60c0'X, '6180'X, 'a141'X,
&      '6300'X, 'a3c1'X, 'a281'X, '6240'X/
data (crc16_table(i),i=136,143)
&      /'6600'X, 'a6c1'X, 'a781'X, '6740'X,
&      'a501'X, '65c0'X, '6480'X, 'a441'X/

```



```

data (crc16_table(i),i=144,151)
&      /'6c00'X, 'acc1'X, 'ad81'X, '6d40'X,
&      'af01'X, '6fc0'X, '6e80'X, 'ae41'X/
data (crc16_table(i),i=152,159)
&      /'aa01'X, '6ac0'X, '6b80'X, 'ab41'X,
&      '6900'X, 'a9c1'X, 'a881'X, '6840'X/
data (crc16_table(i),i=160,167)
&      /'7800'X, 'b8c1'X, 'b981'X, '7940'X,
&      'bb01'X, '7bc0'X, '7a80'X, 'ba41'X/
data (crc16_table(i),i=168,175)
&      /'be01'X, '7ec0'X, '7f80'X, 'bf41'X,
&      '7d00'X, 'bdc1'X, 'bc81'X, '7c40'X/
data (crc16_table(i),i=176,183)
&      /'b401'X, '74c0'X, '7580'X, 'b541'X,
&      '7700'X, 'b7c1'X, 'b681'X, '7640'X/
data (crc16_table(i),i=184,191)
&      /'7200'X, 'b2c1'X, 'b381'X, '7340'X,
&      'b101'X, '71c0'X, '7080'X, 'b041'X/
data (crc16_table(i),i=192,199)
&      /'5000'X, '90c1'X, '9181'X, '5140'X,
&      '9301'X, '53c0'X, '5280'X, '9241'X/
data (crc16_table(i),i=200,207)
&      /'9601'X, '56c0'X, '5780'X, '9741'X,
&      '5500'X, '95c1'X, '9481'X, '5440'X/
data (crc16_table(i),i=208,215)
&      /'9c01'X, '5cc0'X, '5d80'X, '9d41'X,
&      '5f00'X, '9fc1'X, '9e81'X, '5e40'X/
data (crc16_table(i),i=216,223)
&      /'5a00'X, '9ac1'X, '9b81'X, '5b40'X,
&      '9901'X, '59c0'X, '5880'X, '9841'X/
data (crc16_table(i),i=224,231)
&      /'8801'X, '48c0'X, '4980'X, '8941'X,
&      '4b00'X, '8bc1'X, '8a81'X, '4a40'X/
data (crc16_table(i),i=232,239)
&      /'4e00'X, '8ec1'X, '8f81'X, '4f40'X,
&      '8d01'X, '4dc0'X, '4c80'X, '8c41'X/
data (crc16_table(i),i=240,247)
&      /'4400'X, '84c1'X, '8581'X, '4540'X,
&      '8701'X, '47c0'X, '4680'X, '8641'X/
data (crc16_table(i),i=248,255)
&      /'8201'X, '42c0'X, '4380'X, '8341'X,
&      '4100'X, '81c1'X, '8081'X, '4040'X/

```

\*\*\* crc is a 16-bit unsigned integer value \*\*\*

```
CRC16 = 0
```

\*\*\* process every byte in the message \*\*\*

```
do i = 1,bytecount
  temp = message(i)
```

```
index = IEXOR(CRC16, temp)    ! bitwise xOR lower 8 bits of crc
  index = IAND(index,'00FF'X) ! clear top byte of word
CRC16 = ISHFT(CRC16, -8)     ! bitwise right shift crc 8 times
CRC16 = IEXOR(CRC16,crc16_table(index)) ! bitwise XOR 16 bits
end do

return
end
```

```
***** end of function CRC16 *****
```

```
***** end of module CP *****
```

```

*****
* Module:      CRCP.FOR
* Facility:    Pluto
* P-Spec:     3.3
* Abstract:
*   This module contains the implementation of the functional
*   requirements for CRCP.
*
* List of Routines:
*   subroutine CRCP
*****
*****
* Title: CRCP
* Facility:    Pluto
* Abstract:
*   1) Determine whether or not to release the parachute.
*
* Arguments:  None.
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****
      subroutine CRCP

      implicit none

*** include the global common stores ***

      include 'guidance_state.for'
      include 'external.for'

*** include constant definitions ***

      include 'constants.for'

*****
* The parachute is to be released during the same frame in which the
* axial engine temperature becomes "HOT" (2). Valid states for
* CHUTE_RELEASED are "Chute Attached" (0) and "Chute Released" (1).
*****
*** 1) Determine whether or not to release the parachute. ***

      if (CHUTE_RELEASED .eq. K$CHUTE_ATTACHED) then

          if (AE_TEMP .eq. K$HOT) then
              CHUTE_RELEASED = K$CHUTE_RELEASED
          end if

      end if

      return

```

```
end
**** end of module crcp.for ****
```

```

*****
* Module:      EXTERNAL.FOR
* Facility:    Pluto
* Abstract:
*   This module contains the data definitions for the
*   global common data store named EXTERNAL.
*
* Revision History:
*   v0  15-sep-1994 Rob Angellatta (RKA) Original.
*   v1  30-Nov-1994 Philip Morris (PEM)
*****

```

\*\*\* COMMON block definition \*\*\*

```

COMMON      /EXTERNAL/
&          A_COUNTER,
&          AE_CMD,
&          AR_COUNTER,
&          CHUTE_RELEASED,
&          FRAME_COUNTER,
&          G_COUNTER,
&  PACKET,
&          RE_CMD,
&          SS_TEMP,
&          SUBFRAME_COUNTER,
&          TD_COUNTER,
&          TDLR_COUNTER,
&          THERMO_TEMP

```

\*\*\* data type declarations \*\*\*

```

integer*2  A_COUNTER(1:3)
integer*2  AE_CMD(1:3)
integer*2  AR_COUNTER
logical*1  CHUTE_RELEASED
integer*4  FRAME_COUNTER
integer*2  G_COUNTER(1:3)
integer*2  RE_CMD
integer*2  SS_TEMP
integer*2  SUBFRAME_COUNTER
integer*2  TD_COUNTER
integer*2  TDLR_COUNTER(1:4)
integer*2  THERMO_TEMP

```

```

*****
* Although the specifications define 'packet' as an array of
* integer*2's, the functional unit CP treats 'packet' as a
* variant record. The definitions below reserve an array
* of 256 integer*2 data and overlay the area with a variant
* record structure.
*****

```

\*\*\* the Sensor Processing subframe data field and checksum \*\*\*

```
structure /sp_data_t/  
  real*8  ar_altitude  
  logical*1 ar_status  
  real*8  atmospheric_temp  
  real*8  a_acceleration(1:3)  
  logical*1 a_status(1:3)  
  logical*1 c_status  
  real*8  g_rotation(1:3)  
  logical*1 g_status  
  integer*4 k_alt  
  integer*4 k_matrix(1:3)  
  logical*1 tdlr_state(1:4)  
  logical*1 tdlr_status(1:4)  
  real*8  tdlr_velocity(1:3)  
  logical*1 tds_status  
  logical*1 td_sensed  
  logical*1 ts_status(2)  
  integer*2 checksum  
end structure
```

\*\*\* the Guidance Processing subframe data field and checksum \*\*\*

```
structure /gp_data_t/  
  logical*1 contour_crossed  
  logical*1 c_status  
  real*8  gp_altitude  
  real*8  gp_attitude(1:9)  
  integer*4 gp_phase  
  real*8  gp_rotation(1:6)  
  real*8  gp_velocity(1:3)  
  real*8  velocity_error  
  integer*2 checksum  
end structure
```

\*\*\* the Control Law Processing subframe data field and checksum \*\*\*

\*\*\*

\* v1 Changes for AR#23. Item 5. ae\_temp was changed from logical\*1 to integer\*2

\*\*\*

```
structure /clp_data_t/  
  integer*2 ae_cmd(1:3)  
  logical*1 ae_status  
  integer*2 ae_temp  
  logical*1 chute_released  
  logical*1 c_status  
  real*8  pe_integral  
  integer*2 re_cmd  
  logical*1 re_status
```

```
    real*8    te_integral
    real*8    ye_integral
    integer*2 checksum
end structure
```

\*\*\*

\* v1 Changes for AR#23. End Change.

\*\*\*

\*\*\* the data packet structure \*\*\*

```
structure /data_packet_t/
  union
    map
      integer*2    PACKET(1:256)
    end map
    map
      integer*2    sync_pattern
      logical*1    seq_number
      integer*4    data_mask
    union
      map
        record /sp_data_t/ sp
      end map
      map
        record /gp_data_t/ gp
      end map
      map
        record /clp_data_t/ clp
      end map
    end union
  end map
end union
end structure
```

\*\*\* declare a variable of type PACKET \*\*\*

```
record /data_packet_t/ PACKET
```

\*\*\*\*\* end of module EXTERNAL.FOR \*\*\*\*\*

\*\*\*\*\*

\* Module: GP.FOR  
\* Facility: Pluto  
\* P-Spec: 2.2  
\* Abstract:  
\* This module contains the implementation of the functional  
\* requirements for GP.  
\*

\* List of Routines:  
\* subroutine GP  
\* subroutine DERIV\_ALT  
\* subroutine DERIV\_ATT  
\* subroutine DERIV\_VEL  
\* subroutine MULT\_ATT  
\* subroutine MULT\_VEL  
\* subroutine AVG\_ATT  
\* subroutine AVG\_VEL

\*\*\*\*\*

\*\*\*\*\*

\* Title: GP  
\* Facility: Pluto  
\* Abstract:  
\* 1) Maintain the history of the vehicle's altitude, velocities,  
\* and attitude.  
\* 2) Compute the current vehicle altitude, velocities and attitude.  
\* 3) Determine if the engines should be switched on or off.  
\* 4) Compute the current velocity error.  
\* 5) Determine if the predetermined velocity-altitude contour has  
\* been crossed.  
\* 6) Determine the current guidance phase.  
\* 7) Determine the appropriate axial engine control law parameters.  
\*

\* Arguments: None

\*  
\* Revision History:  
\* v0 15-sep-1994 Rob Angellatta (RKA) Original.  
\* v1 01-Dec-1994 Philip Morris (PEM)  
\* v2 10-JAN-1995 Philip Morris (PEM)  
\* v3 16-MAR-1995 Philip Morris (PEM)

\*\*\*\*\*

subroutine GP

implicit none

\*\*\* include the global common stores \*\*\*

include 'external.for'  
include 'guidance\_state.for'  
include 'sensor\_output.for'



```

include 'run_parameters.for'

*** include constant definitions ***

include 'constants.for'

*** declare local variables ***

real*8      temp
real*8      cur_altitude
real*8      optimal_velocity

real*8      att_k1(3,3), att_k2(3,3)
real*8      att_k3(3,3), att_k4(3,3)
real*8      att_tmp(3,3)

real*8      vel_k1(3), vel_k2(3), vel_k3(3), vel_k4(3)
real*8      vel_tmp(3)
real*8      alt_k1, alt_k2, alt_k3, alt_k4

real*8      step_size

integer*4   i, j

*****
* 1) Maintain the history of the vehicle altitude, velocities,
*   and attitude by "rotating variables."
*****

GP_ALTITUDE(4) = GP_ALTITUDE(3)
GP_ALTITUDE(3) = GP_ALTITUDE(2)
GP_ALTITUDE(2) = GP_ALTITUDE(1)
GP_ALTITUDE(1) = GP_ALTITUDE(0)

GP_VELOCITY(1, 4) = GP_VELOCITY(1, 3)
GP_VELOCITY(1, 3) = GP_VELOCITY(1, 2)
GP_VELOCITY(1, 2) = GP_VELOCITY(1, 1)
GP_VELOCITY(1, 1) = GP_VELOCITY(1, 0)

GP_VELOCITY(2, 4) = GP_VELOCITY(2, 3)
GP_VELOCITY(2, 3) = GP_VELOCITY(2, 2)
GP_VELOCITY(2, 2) = GP_VELOCITY(2, 1)
GP_VELOCITY(2, 1) = GP_VELOCITY(2, 0)

GP_VELOCITY(3, 4) = GP_VELOCITY(3, 3)
GP_VELOCITY(3, 3) = GP_VELOCITY(3, 2)
GP_VELOCITY(3, 2) = GP_VELOCITY(3, 1)
GP_VELOCITY(3, 1) = GP_VELOCITY(3, 0)

GP_ATTITUDE(1, 1, 4) = GP_ATTITUDE(1, 1, 3)
GP_ATTITUDE(1, 2, 4) = GP_ATTITUDE(1, 2, 3)

```

GP\_ATTITUDE(1, 3, 4) = GP\_ATTITUDE(1, 3, 3)  
GP\_ATTITUDE(2, 1, 4) = GP\_ATTITUDE(2, 1, 3)  
GP\_ATTITUDE(2, 2, 4) = GP\_ATTITUDE(2, 2, 3)  
GP\_ATTITUDE(2, 3, 4) = GP\_ATTITUDE(2, 3, 3)  
GP\_ATTITUDE(3, 1, 4) = GP\_ATTITUDE(3, 1, 3)  
GP\_ATTITUDE(3, 2, 4) = GP\_ATTITUDE(3, 2, 3)  
GP\_ATTITUDE(3, 3, 4) = GP\_ATTITUDE(3, 3, 3)

GP\_ATTITUDE(1, 1, 3) = GP\_ATTITUDE(1, 1, 2)  
GP\_ATTITUDE(1, 2, 3) = GP\_ATTITUDE(1, 2, 2)  
GP\_ATTITUDE(1, 3, 3) = GP\_ATTITUDE(1, 3, 2)  
GP\_ATTITUDE(2, 1, 3) = GP\_ATTITUDE(2, 1, 2)  
GP\_ATTITUDE(2, 2, 3) = GP\_ATTITUDE(2, 2, 2)  
GP\_ATTITUDE(2, 3, 3) = GP\_ATTITUDE(2, 3, 2)  
GP\_ATTITUDE(3, 1, 3) = GP\_ATTITUDE(3, 1, 2)  
GP\_ATTITUDE(3, 2, 3) = GP\_ATTITUDE(3, 2, 2)  
GP\_ATTITUDE(3, 3, 3) = GP\_ATTITUDE(3, 3, 2)

GP\_ATTITUDE(1, 1, 2) = GP\_ATTITUDE(1, 1, 1)  
GP\_ATTITUDE(1, 2, 2) = GP\_ATTITUDE(1, 2, 1)  
GP\_ATTITUDE(1, 3, 2) = GP\_ATTITUDE(1, 3, 1)  
GP\_ATTITUDE(2, 1, 2) = GP\_ATTITUDE(2, 1, 1)  
GP\_ATTITUDE(2, 2, 2) = GP\_ATTITUDE(2, 2, 1)  
GP\_ATTITUDE(2, 3, 2) = GP\_ATTITUDE(2, 3, 1)  
GP\_ATTITUDE(3, 1, 2) = GP\_ATTITUDE(3, 1, 1)  
GP\_ATTITUDE(3, 2, 2) = GP\_ATTITUDE(3, 2, 1)  
GP\_ATTITUDE(3, 3, 2) = GP\_ATTITUDE(3, 3, 1)

GP\_ATTITUDE(1, 1, 1) = GP\_ATTITUDE(1, 1, 0)  
GP\_ATTITUDE(1, 2, 1) = GP\_ATTITUDE(1, 2, 0)  
GP\_ATTITUDE(1, 3, 1) = GP\_ATTITUDE(1, 3, 0)  
GP\_ATTITUDE(2, 1, 1) = GP\_ATTITUDE(2, 1, 0)  
GP\_ATTITUDE(2, 2, 1) = GP\_ATTITUDE(2, 2, 0)  
GP\_ATTITUDE(2, 3, 1) = GP\_ATTITUDE(2, 3, 0)  
GP\_ATTITUDE(3, 1, 1) = GP\_ATTITUDE(3, 1, 0)  
GP\_ATTITUDE(3, 2, 1) = GP\_ATTITUDE(3, 2, 0)  
GP\_ATTITUDE(3, 3, 1) = GP\_ATTITUDE(3, 3, 0)

\*\*\*\*\*

\* 2) Compute the current vehicle altitude, velocities and attitude.

\*\*\*\*\*

\*\*\* range check the following data elements \*\*\*

call RANGE\_CHECK(GP\_ATTITUDE(1, 1, 2), K\$GP\_ATTITUDE\$LB,  
& K\$GP\_ATTITUDE\$SUB, 'GP', K\$GP\_ATTITUDE\$NAME)  
call RANGE\_CHECK(GP\_ATTITUDE(1, 2, 2), K\$GP\_ATTITUDE\$LB,  
& K\$GP\_ATTITUDE\$SUB, 'GP', K\$GP\_ATTITUDE\$NAME)  
call RANGE\_CHECK(GP\_ATTITUDE(1, 3, 2), K\$GP\_ATTITUDE\$LB,  
& K\$GP\_ATTITUDE\$SUB, 'GP', K\$GP\_ATTITUDE\$NAME)  
call RANGE\_CHECK(GP\_ATTITUDE(2, 1, 2), K\$GP\_ATTITUDE\$LB,

```

&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)
call RANGE_CHECK(GP_ATTITUDE(2, 2, 2), K$GP_ATTITUDE$LB,
&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)
call RANGE_CHECK(GP_ATTITUDE(2, 3, 2), K$GP_ATTITUDE$LB,
&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)
call RANGE_CHECK(GP_ATTITUDE(3, 1, 2), K$GP_ATTITUDE$LB,
&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)
call RANGE_CHECK(GP_ATTITUDE(3, 2, 2), K$GP_ATTITUDE$LB,
&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)
call RANGE_CHECK(GP_ATTITUDE(3, 3, 2), K$GP_ATTITUDE$LB,
&      K$GP_ATTITUDE$SUB, 'GP', K$GP_ATTITUDE$NAME)

call RANGE_CHECK(GP_VELOCITY(1, 2), K$GP_VELOCITY$LB,
&      K$GP_VELOCITY$SUB, 'GP', K$GP_VELOCITY$NAME)
call RANGE_CHECK(GP_VELOCITY(2, 2), K$GP_VELOCITY$LB,
&      K$GP_VELOCITY$SUB, 'GP', K$GP_VELOCITY$NAME)
call RANGE_CHECK(GP_VELOCITY(3, 2), K$GP_VELOCITY$LB,
&      K$GP_VELOCITY$SUB, 'GP', K$GP_VELOCITY$NAME)

call RANGE_CHECK(GP_ALTITUDE(2), K$GP_ALTITUDE$LB,
&      K$GP_ALTITUDE$SUB, 'GP', K$GP_ALTITUDE$NAME)

```

\*\*\* sensor data \*\*\*

```

call RANGE_CHECK(G_ROTATION(1, 0), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(2, 0), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(3, 0), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(1, 1), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(2, 1), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(3, 1), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(1, 2), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(2, 2), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)
call RANGE_CHECK(G_ROTATION(3, 2), K$G_ROTATION$LB,
&      K$G_ROTATION$SUB, 'GP', K$G_ROTATION$NAME)

call RANGE_CHECK(A_ACCELERATION(1, 0), K$A_ACCELERATION$LB,
&      K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(2, 0), K$A_ACCELERATION$LB,
&      K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(3, 0), K$A_ACCELERATION$LB,
&      K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(1, 1), K$A_ACCELERATION$LB,
&      K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)

```

```

call RANGE_CHECK(A_ACCELERATION(2, 1), K$A_ACCELERATION$LB,
& K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(3, 1), K$A_ACCELERATION$LB,
& K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(1, 2), K$A_ACCELERATION$LB,
& K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(2, 2), K$A_ACCELERATION$LB,
& K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)
call RANGE_CHECK(A_ACCELERATION(3, 2), K$A_ACCELERATION$LB,
& K$A_ACCELERATION$SUB, 'GP', K$A_ACCELERATION$NAME)

```

```

call RANGE_CHECK(TDLR_VELOCITY(1, 0), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(2, 0), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(3, 0), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(1, 1), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(2, 1), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(3, 1), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(1, 2), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(2, 2), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)
call RANGE_CHECK(TDLR_VELOCITY(3, 2), K$TDLR_VELOCITY$LB,
& K$TDLR_VELOCITY$SUB, 'GP', K$TDLR_VELOCITY$NAME)

```

```

call RANGE_CHECK(AR_ALTITUDE(0), K$AR_ALTITUDE$LB,
& K$AR_ALTITUDE$SUB, 'GP', K$AR_ALTITUDE$NAME)
call RANGE_CHECK(AR_ALTITUDE(1), K$AR_ALTITUDE$LB,
& K$AR_ALTITUDE$SUB, 'GP', K$AR_ALTITUDE$NAME)
call RANGE_CHECK(AR_ALTITUDE(2), K$AR_ALTITUDE$LB,
& K$AR_ALTITUDE$SUB, 'GP', K$AR_ALTITUDE$NAME)

```

\*\*\*\*\*

\* A five step implementation of the RK method. The functions  
\* deriv\_att(), deriv\_vel(), and deriv\_alt() are described below.  
\*

\* The interval begins at the current frame minus 2 frames.  
\*

\* 1. Compute the first estimate of the incremental value for  
\* GP\_ATTITUDE, GP\_VELOCITY, and GP\_ALTITUDE based upon the  
\* rate of change at the beginning of the interval  
\* (2 frames ago):  
\*

\* estimate = rate\_of\_change \* step\_size

\*\*\*\*\*

```

step_size = 2 * DELTA_T

call deriv_att(att_k1, GP_ATTITUDE(1,1,2), 2)
call mult_att(att_k1, step_size)

***
* v1 Changes for AR#23. Item 13. "att_k1" changed to "vel_k1"
***
call deriv_vel(vel_k1, GP_VELOCITY(1,2), GP_ATTITUDE(1,1,2), 2)
call mult_vel(vel_k1, step_size)

***
* v1 Changes for AR#23. End Change.
***
call deriv_alt(alt_k1, GP_ALTITUDE(2), GP_VELOCITY(1,2),
& GP_ATTITUDE(1,1,2), 2)
alt_k1 = alt_k1 * step_size

*****
* 2. Compute the second estimate of the incremental value for
* GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
* rate of change at the midpoint of the first estimate k1:
*****

call avg_att(att_tmp, GP_ATTITUDE(1,1,2), att_k1)
call deriv_att(att_k2, att_tmp, 1)
call mult_att(att_k2, step_size)

call avg_vel(vel_tmp, GP_VELOCITY(1,2), vel_k1)
call deriv_vel(vel_k2, vel_tmp, att_tmp, 1)
***
* v2 Changes for PR#24. Item 2. Changed division placement.
***
* call mult_vel(att_k2, step_size)
call mult_vel(vel_k2, step_size)

* call deriv_alt(alt_k2, (GP_ALTITUDE(2) + alt_k1)/2,
* & vel_tmp, att_tmp, 1)
call deriv_alt(alt_k2, (GP_ALTITUDE(2) + alt_k1)/2,
& vel_tmp, att_tmp, 1)
alt_k2 = alt_k2 * STEP_SIZE
***
* v2 Changes for AR#24. End Change.
***

*****
* 3. Compute the third estimate of the incremental value for
* GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
* rate of change at the midpoint of the second estimate k2:
*****

```

```

call avg_att(att_tmp, GP_ATTITUDE(1,1,2), att_k2)
call deriv_att(att_k3, att_tmp, 1)
call mult_att(att_k3, step_size)

call avg_vel(vel_tmp, GP_VELOCITY(1,2), vel_k2)
call deriv_vel(vel_k3, vel_tmp, att_tmp, 1)
call mult_vel(vel_k3, step_size)

***
* v2 Changes for PR#24. Item 2. Changed division placement.
***
*   call deriv_alt(alt_k3, (GP_ALTITUDE(2) + alt_k2)/2,
*   &               vel_tmp, att_tmp, 1)
*   call deriv_alt(alt_k3, (GP_ALTITUDE(2) + alt_k2)/2,
*   &               vel_tmp, att_tmp, 1)
***
* v2 Changes for AR#24. End Change.
***
    alt_k3 = alt_k3 * STEP_SIZE

*****
* 4. Compute the fourth estimate of the incremental value for
* GP_ATTITUDE, GP_VELOCITY, and GP_ALTITUDE based upon the
* the rate-of-change at the third estimate k3:
*****

do i = 1,3
  do j = 1,3
    att_tmp(i,j) = GP_ATTITUDE(i, j, 2) + att_k3(i, j)
  end do
end do

call deriv_att(att_k4, att_tmp, 0)
call mult_att(att_k4, step_size)

do i = 1,3
  vel_tmp(i) = GP_VELOCITY(i,2) + vel_k3(i)
end do

***
* v1 Changes for AR#23. Item 15. 4th parameter changed to "0"
***
    call deriv_vel(vel_k4, vel_tmp, att_tmp, 0)
***
* v2 Changes for PR#24. Item 4. Changed att_k to vel_k4.
***
*   call mult_vel(att_k4, step_size)
*   call mult_vel(vel_k4, step_size)
***
* v2 Changes for AR#24. End Change.
***

```

```

***
* v1 Changes for AR#23. End Change.
***
    call deriv_alt(alt_k4, (GP_ALTITUDE(2) + alt_k3),
    &                vel_tmp, att_tmp, 0)
    alt_k4 = alt_k4 * STEP_SIZE

*****
* 5. Perform a weighted average of the four previously computed
* estimates of the new value for GP_ATTITUDE, GP_VELOCITY, and
* GP_ALTITUDE.
*
* Note, the syntax (*, x) and (*, *, x) represent the xth history of
* the data element.
*****

*****
* GP_ATTITUDE(*, *, 0) = GP_ATTITUDE(*, *, 2) +
* & (1/6)(att_k1 + 2*(att_k2 + att_k3) + att_k4)
*****

    do i = 1,3
      do j = 1,3
        att_tmp(i,j) = (att_k2(i,j) + att_k3(i,j)) * 2.0
        att_tmp(i,j) = (att_tmp(i,j) + att_k1(i,j) +
        & att_k4(i,j)) / 6.0
        GP_ATTITUDE(i, j, 0) = GP_ATTITUDE(i, j, 2) + att_tmp(i,j)
      end do
    end do

*****
* GP_VELOCITY(*, 0) = GP_VELOCITY(*, 2) +
* & (1/6)(vel_k1 + 2*(vel_k2 + vel_k3) + vel_k4)
*****

    do i = 1,3
      vel_tmp(i) = (vel_k2(i) + vel_k3(i)) * 2.0
      vel_tmp(i) = (vel_tmp(i) + vel_k1(i) + vel_k4(i)) / 6.0
      GP_VELOCITY(i, 0) = GP_VELOCITY(i, 2) + vel_tmp(i)
    end do

*****
* GP_ALTITUDE(0) = GP_ALTITUDE(2) +
* & (1/6)(alt_k1 + 2*(alt_k2 + alt_k3) + alt_k4)
*****

    GP_ALTITUDE(0) = GP_ALTITUDE(2) +
    & (alt_k1 + 2.0*(alt_k2 + alt_k3) + alt_k4) / 6.0

*** establish the "final" rotation matrix ***

```

```

GP_ROTATION(1, 1) = 0
GP_ROTATION(1, 2) = G_ROTATION(3, 0)
GP_ROTATION(1, 3) = -G_ROTATION(2, 0)
GP_ROTATION(2, 1) = -G_ROTATION(3, 0)
GP_ROTATION(2, 2) = 0
GP_ROTATION(2, 3) = G_ROTATION(1, 0)
GP_ROTATION(3, 1) = G_ROTATION(2, 0)
GP_ROTATION(3, 2) = -G_ROTATION(1, 0)
GP_ROTATION(3, 3) = 0

```

\*\*\*\*\*

\* 3) Determine if the engines should be switched on or off.

\*\*\*\*\*

\*\*\* range check the current altitude \*\*\*

```

call RANGE_CHECK(GP_ALTITUDE(0), K$GP_ALTITUDE$LB,
&                K$GP_ALTITUDE$SUB, 'GP', K$GP_ALTITUDE$NAME)

```

\*\*\* range check the current x-axis vehicle velocity \*\*\*

```

call RANGE_CHECK(GP_VELOCITY(1, 0), K$GP_VELOCITY$LB,
&                K$GP_VELOCITY$SUB, 'GP', K$GP_VELOCITY$NAME)

```

\*\*\* \*\*

```

if (AE_SWITCH .EQ. K$AXIAL_ENGINES_ARE_OFF) then
  if (RE_SWITCH .EQ. K$ROLL_ENGINES_ARE_ON) then
    if (TD_SENSED .EQ. K$TOUCH_DOWN_NOT_SENSED) then
      if (GP_ALTITUDE(0) .LE. ENGINES_ON_ALTITUDE) then
        AE_SWITCH = K$AXIAL_ENGINES_ARE_ON
        FRAME_ENGINES_IGNITED = FRAME_COUNTER
      end if
    end if
  end if
end if
else

```

\*\*\* the axial engines are "on" \*\*\*

```

  if (TD_SENSED .EQ. K$TOUCH_DOWN_SENSED) then
    AE_SWITCH = K$AXIAL_ENGINES_ARE_OFF
    RE_SWITCH = K$ROLL_ENGINES_ARE_OFF
  else

```

\*\*\* touch down "not sensed" \*\*\*

\*\*\*

\* v1 PR#27 Item 3. Included a MAX function.

\*\*\*

```

*   if (GP_ALTITUDE(0) .LE. DROP_HEIGHT) then
*     temp = 2*GRAVITY*GP_ALTITUDE(0)
*     call NEG_VALUE_CHECK(temp, 'GP')

```



```

        if (GP_ALTITUDE(0) .LE. DROP_HEIGHT) then
            temp = 2 * GRAVITY * MAX(0.0D0, GP_ALTITUDE(0))
***
* v1 PR#27 End Change
***

        if (sqrt(temp)+GP_VELOCITY(1,0) .LE.
&          MAX_NORMAL_VELOCITY) then
            AE_SWITCH = K$AXIAL_ENGINES_ARE_OFF
            RE_SWITCH = K$ROLL_ENGINES_ARE_OFF
        end if
    end if
end if
end if

*****
* 4) Compute the current velocity error.
*****

*** compute the optimal velocity ***

*** convert GP_ALTITUDE from meters to kilometers ***

    cur_altitude = GP_ALTITUDE(0) / 1000.0

    do i = 1, 100
        if (CONTOUR_ALTITUDE(i) .EQ. cur_altitude) then

*** found an exact match in the table ***

            optimal_velocity = CONTOUR_VELOCITY(i)

            goto 100                ! early exit

        else if (CONTOUR_ALTITUDE(i) .GT. cur_altitude) then
            if (i .GT. 1) then

*** interpolate between i-1 and i ***

*** check for potential divide by zero condition ***

&          call ZERO_CHECK(CONTOUR_ALTITUDE(i)-
&                          CONTOUR_ALTITUDE(i-1), 'GP')

*** interpolation formula ***

            optimal_velocity = CONTOUR_VELOCITY(i-1) +
&          ((CONTOUR_VELOCITY(i) - CONTOUR_VELOCITY(i-1)) /
&          (CONTOUR_ALTITUDE(i) - CONTOUR_ALTITUDE(i-1))) *
&          (cur_altitude - CONTOUR_ALTITUDE(i-1)))

```

```

        goto 100          ! early exit

    else

*** Extrapolate for altitude < smallest value in table entries ***

*** check for potential divide by zero condition ***

        call ZERO_CHECK(CONTOUR_ALTITUDE(2) -
&          CONTOUR_ALTITUDE(1), 'GP')

*** Extrapolation formula ***

        optimal_velocity = CONTOUR_VELOCITY(1) -
&          ((CONTOUR_VELOCITY(2) - CONTOUR_VELOCITY(1)) /
&          (CONTOUR_ALTITUDE(2) - CONTOUR_ALTITUDE(1))) *
&          (CONTOUR_ALTITUDE(1) - cur_altitude)

        goto 100          ! early exit

    end if

    else

***          CONTOUR_ALTITUDE(i) < cur_altitude

        if ((CONTOUR_ALTITUDE(i) .EQ. 0) .OR. (i .EQ. 100)) then

*** Extrapolate for altitude > largest value in table entries ***
*** note, i points to first (lowest) "0" entry in the table ***

*** check for potential divide by zero condition ***

        call ZERO_CHECK(CONTOUR_ALTITUDE(i-1) -
&          CONTOUR_ALTITUDE(i-2), 'GP')

*** Extrapolation formula ***

        optimal_velocity = CONTOUR_VELOCITY(i-1) +
&          ((CONTOUR_VELOCITY(i-1) - CONTOUR_VELOCITY(i-2)) /
&          (CONTOUR_ALTITUDE(i-1) - CONTOUR_ALTITUDE(i-2))) *
&          (cur_altitude - CONTOUR_ALTITUDE(i-1))

        goto 100          ! early exit

        end if
    end if
end do

100 continue

```

```

*** convert optimal_velocity from km/sec to m/sec ***

    optimal_velocity = optimal_velocity * 1000.0

*** compute the velocity error ***

    VELOCITY_ERROR = GP_VELOCITY(1, 0) - optimal_velocity

*****
* 5) Determine if the predetermined velocity-altitude contour has
*   been crossed.
*****

***
* v1 Changes for AR#23. Item 17. >= changed to <=
***
    if (GP_ALTITUDE(0) .LE. ENGINES_ON_ALTITUDE) then
        if (CONTOUR_CROSSED .EQ. K$CONTOUR_NOT_CROSSED) then
            if (VELOCITY_ERROR .GE. 0) then
                CONTOUR_CROSSED = K$CONTOUR_CROSSED
            end if
        end if
    end if

***
* v1 Changes for AR#23. End Change.
***
*****
* 6) Determine the current guidance phase.
*****

    go to (1010, 1020, 1030, 1040, 2000), GP_PHASE

***
* v1 Changes for AR#23. Item 33. Added default goto
***
    go to 2000
***
* v1 Changes for AR#23. End Change.
***

*** GP_PHASE == 1 *****

1010 continue

*** trans from 1 to 2 when the "engines on altitude" is reached ***

    if (GP_ALTITUDE(0) .LE. ENGINES_ON_ALTITUDE) then
        GP_PHASE = 2
    end if

```

```

        goto 2000

*** GP_PHASE == 2 ****

1020  continue

*** trans from 2 to 5 when touch down is sensed ***

        if (TD_SENSED .EQ. K$TOUCH_DOWN_SENSED) then
            GP_PHASE = 5
        else

*** trans from 2 to 3 when the engines are hot and the chute is released ***

            if (AE_TEMP .EQ. K$HOT) then
                if (CHUTE_RELEASED .EQ. K$CHUTE_RELEASED) then
                    GP_PHASE = 3
                end if
            end if
        end if

        goto 2000

*** GP_PHASE == 3 ****

1030  continue

*** trans from 3 to 5 when touch down is sensed ***

        if (TD_SENSED .EQ. K$TOUCH_DOWN_SENSED) then
            GP_PHASE = 5
        else

*** trans from 3 to 5 when the TD sensor fails and altitude too low ***
*** trans from 3 to 4 when the TD sensor healthy and altitude too low ***

            if (GP_ALTITUDE(0) .LE. DROP_HEIGHT) then

                if (TDS_STATUS .EQ. K$FAILED) then
                    GP_PHASE = 5
                else

***
*   v1 PR#27 Item 3. Included a MAX function.
***
*       temp = 2 * GRAVITY * GP_ALTITUDE(0)
*       call NEG_VALUE_CHECK(temp, 'GP')
*       temp = 2 * GRAVITY * MAX(0.0D0, GP_ALTITUDE(0))
***
*   v1 PR#27 End Change
***

```

```

        if (sqrt(temp)+GP_VELOCITY(1,0) .LE.
&          MAX_NORMAL_VELOCITY) then
            GP_PHASE = 4
        end if
    end if
end if
end if

goto 2000

*** GP_PHASE == 4 *****

1040 continue

*** trans from 4 to 5 when touch down is sensed ***

    if (TD_SENSED .EQ. K$TOUCH_DOWN_SENSED) then
        GP_PHASE = 5
    else

*** trans from 4 to 5 when the TD sensor fails ***

        if (TDS_STATUS .EQ. K$FAILED) then
            GP_PHASE = 5
        end if
    end if

2000 continue

*****
* 7) Determine the appropriate axial engine control law parameter index.
*****

*** Note, the optimal_velocity is computed above during the computing of
***   the current velocity error.

    if (CL .EQ. K$FIRST) then
        if (optimal_velocity .EQ. DROP_SPEED) then
            if (GP_VELOCITY(1, 0) .LT. DROP_SPEED) then
                CL = K$SECOND
                TE_INTEGRAL = 0
            end if
        end if
    end if

return
end

*** end of subroutine GP *****

```

```

*****
* Title: DERIV_ATT
* Facility: Pluto
* Abstract:
*   Compute the derivative of the vehicle attitude.
*   rate-of-change = deriv_att(attitude, i)
*
* Arguments:
*   result array (1..3, 1..3) of real*8 The computed derivative.
*   att array (1..3, 1..3) of real*8 The attitude structure
*   index integer*4 The history index
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 01-Dec-1994 Philip Morris (PEM)
*****

```

```

subroutine DERIV_ATT(result, att, index)

```

```

implicit none

```

```

*** define arguments ***

```

```

real*8 att(1:3,1:3)
real*8 result(1:3,1:3)

```

```

integer*4 index

```

```

*** include the global common stores ***

```

```

include 'sensor_output.for'

```

```

***

```

```

* v1 Changes for AR#23. Item 18. Replaced pv, qv, rv with rotation variables
***

```

```

result(1,1) = G_ROTATION(3,index) * att(2,1) +
& (-G_ROTATION(2,index) * att(3,1))
result(1,2) = G_ROTATION(3,index) * att(2,2) +
& (-G_ROTATION(2,index) * att(3,2))
result(1,3) = G_ROTATION(3,index) * att(2,3) +
& (-G_ROTATION(2,index) * att(3,3))

```

```

result(2,1) = (-G_ROTATION(3,index) * att(1,1)) +
& (G_ROTATION(1,index) * att(3,1))
result(2,2) = (-G_ROTATION(3,index) * att(1,2)) +
& (G_ROTATION(1,index) * att(3,2))
result(2,3) = (-G_ROTATION(3,index) * att(1,3)) +
& (G_ROTATION(1,index) * att(3,3))

```

```

    result(3,1) = G_ROTATION(2,index) * att(1,1) +
& (-G_ROTATION(1,index) * att(2,1))
    result(3,2) = G_ROTATION(2,index) * att(1,2) +
& (-G_ROTATION(1,index) * att(2,2))
    result(3,3) = G_ROTATION(2,index) * att(1,3) +
& (-G_ROTATION(1,index) * att(2,3))

***
* v1 Changes for AR#23. End Change.
***
    return
    end

***** end of subroutine DERIV_ATT *****

*****
* Title: DERIV_VEL
* Facility: Pluto
* Abstract:
*   Compute the derivative of the vehicle velocity.
*   rate-of-change = deriv_vel(velocity, attitude, i)
*
* Arguments:
*   result array (1..3) of real*8   The computed derivative.
*   vel    array (1..3) of real*8   The velocity vector
*   att    array (1..3, 1..3) of real*8 The attitude structure
*   index  integer*4               The history index
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 01-Dec-1994 Philip Morris (PEM)
*****

    subroutine DERIV_VEL(result,vel,att,index)

    implicit none

    *** define arguments ***

    real*8      att(1:3,1:3)
    real*8      result(1:3)
    real*8      vel(1:3)
    integer*4   index

    *** include the global common stores ***

    include 'guidance_state.for'
    include 'sensor_output.for'
    include 'run_parameters.for'

    ***

```

\* v1 Changes for AR#23. Item 19. Relpaced pv, qv, rv with rotation variables

\*\*\*

\*\*\* declare local variables \*\*\*

real\*8 temp(3)

\*\*\* execution begins here \*\*\*

\*\*\*

\* v1 Changes for AR#23. Item 20. Changed index values for temp

\*\*\*

temp(1) = TDLR\_VELOCITY(1,index) - vel(1)

temp(2) = TDLR\_VELOCITY(2,index) - vel(2)

temp(3) = TDLR\_VELOCITY(3,index) - vel(3)

result(1) = G\_ROTATION(3,index)\*vel(2) +  
& (-G\_ROTATION(2,index)\*vel(3)) +  
& GRAVITY \* att(1,3) + A\_ACCELERATION(1,index) +  
& K\_MATRIX(1,1,index) \* temp(1) +  
& K\_MATRIX(1,2,index) \* temp(2) +  
& K\_MATRIX(1,3,index) \* temp(3)

result(2) = -G\_ROTATION(3,index)\*vel(1) +  
& G\_ROTATION(1,index)\*vel(3) +  
& GRAVITY \* att(2,3) + A\_ACCELERATION(2,index) +  
& K\_MATRIX(2,1,index) \* temp(1) +  
& K\_MATRIX(2,2,index) \* temp(2) +  
& K\_MATRIX(2,3,index) \* temp(3)

result(3) = G\_ROTATION(2,index)\*vel(1) +  
& (-G\_ROTATION(1,index)\*vel(2)) +  
& GRAVITY \* att(3,3) + A\_ACCELERATION(3,index) +  
& K\_MATRIX(3,1,index) \* temp(1) +  
& K\_MATRIX(3,2,index) \* temp(2) +  
& K\_MATRIX(3,3,index) \* temp(3)

\*\*\*

\* v1 Changes for AR#23. End Change.

\*\*\*

return

end

\*\*\*\*\* end of subroutine DERIV\_VEL \*\*\*\*\*

\*\*\*\*\*

\* Title: DERIV\_ALT

\* Facility: Pluto

\* Abstract:



```

*      Compute the derivative of the vehicle altitude.
*      rate-of-change = deriv_att(attitude, index)
*
* Arguments:
*   result real*8           The computed derivative.
*   alt    real*8           The altitude
*   vel    array (1..3) of real*8   The velocity vector
*   att    array (1..3, 1..3) of real*8 The attitude structure
*   index  integer*4        The history index
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

```

subroutine DERIV_ALT(result,alt,vel,att,index)

```

```

implicit none

```

```

*** define arguments ***

```

```

real*8      alt
real*8      att(1:3,1:3)
real*8      result
real*8      vel(1:3)
integer*4   index

```

```

*** include the global common stores ***

```

```

include 'guidance_state.for'
include 'sensor_output.for'

```

```

*** execution begins here ***

```

```

result = -att(1,3)*vel(1) + (-att(2,3)*vel(2)) +
&        (-att(3,3)*vel(3)) +
&        K_ALT(index)*(AR_ALTITUDE(index) - alt)

```

```

return
end

```

```

***** end of subroutine DERIV_ALT *****

```

```

*****

```

```

* Title: MULT_ATT
* Facility: Pluto
* Abstract:
*   Multiply a 3x3 array by a scaler, result -> 3x3 array.
*   mat = mat * scaler
*
* Arguments:
*   att array (1..3, 1..3) of real*8 The attitude structure

```

```

*   factor      real*8                The scalar multiplier
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 01-Dec-1994 Philip Morris (PEM)
*****

      subroutine MULT_ATT(att,factor)

      implicit none

*** define arguments ***

      real*8      att(1:3,1:3)
      real*8      factor

*** execution begins here ***

***
* v1 Changes for AR#23. Item 22. Changed att index values
***
      att(1,1) = att(1,1) * factor
      att(1,2) = att(1,2) * factor
      att(1,3) = att(1,3) * factor

      att(2,1) = att(2,1) * factor
      att(2,2) = att(2,2) * factor
      att(2,3) = att(2,3) * factor

      att(3,1) = att(3,1) * factor
      att(3,2) = att(3,2) * factor
      att(3,3) = att(3,3) * factor

      return
      end

***
* v1 Changes for AR#23. End Change.
***
***** end of subroutine MULT_ATT *****

*****
* Title: MULT_VEL
* Facility: Pluto
* Abstract:
*   Multiply a 1x3 vector by a scaler, result -> vector
*   vector = vector * scaler
*
* Arguments:
*   att      array (1..3) of real*8      The velocity structure
*   factor   real*8                      The scalar multiplier

```

```

*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

```

subroutine MULT_VEL(vel, factor)

```

```

implicit none

```

```

*** define arguments ***

```

```

real*8      vel(1:3)
real*8      factor

```

```

*** execution begins here ***

```

```

vel(1)      = vel(1) * factor
vel(2)      = vel(2) * factor
vel(3)      = vel(3) * factor

```

```

return
end

```

```

***** end of subroutine MULT_VEL *****

```

```

*****

```

```

* Title: AVG_ATT
* Facility: Pluto
* Abstract:
*   Add two 3x3 array's
*   result = (mat1 + mat2 / 2)
*
* Arguments:
*   result  array (1..3, 1..3) of real*8 the result attitude structure
*   att_1   array (1..3, 1..3) of real*8 an attitude structure
*   att_2   array (1..3, 1..3) of real*8 an attitude structure
*

```

```

* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 01-Dec-1994 Philip Morris (PEM)
*****

```

```

subroutine AVG_ATT(result, att_1, att_2)

```

```

implicit none

```

```

*** define arguments ***

```

```

real*8      result(1:3, 1:3)
real*8      att_1(1:3, 1:3), att_2(1:3, 1:3)

```

\*\*\* execution begins here \*\*\*

\*\*\*

\* v1 Changes for PR#23. Item 14 & 21. Function no longer averages but  
\* divides one element by 2

\*\*\*

\*\*\*

\* v2 Changes for PR#24. Item 1. Changed index values.

\*\*\*

\* result(1,1) = att\_1(1,1) + att\_2(1,1) / 2.0

\* result(1,2) = att\_1(1,1) + att\_2(1,1) / 2.0

\* result(1,3) = att\_1(1,1) + att\_2(1,1) / 2.0

\*

\* result(2,1) = att\_1(2,1) + att\_2(2,1) / 2.0

\* result(2,2) = att\_1(2,1) + att\_2(2,1) / 2.0

\* result(2,3) = att\_1(2,1) + att\_2(2,1) / 2.0

\*

\* result(3,1) = att\_1(3,1) + att\_2(3,1) / 2.0

\* result(3,2) = att\_1(3,1) + att\_2(3,1) / 2.0

\* result(3,3) = att\_1(3,1) + att\_2(3,1) / 2.0

result(1,1) = att\_1(1,1) + att\_2(1,1) / 2.0

result(1,2) = att\_1(1,2) + att\_2(1,2) / 2.0

result(1,3) = att\_1(1,3) + att\_2(1,3) / 2.0

result(2,1) = att\_1(2,1) + att\_2(2,1) / 2.0

result(2,2) = att\_1(2,2) + att\_2(2,2) / 2.0

result(2,3) = att\_1(2,3) + att\_2(2,3) / 2.0

result(3,1) = att\_1(3,1) + att\_2(3,1) / 2.0

result(3,2) = att\_1(3,2) + att\_2(3,2) / 2.0

result(3,3) = att\_1(3,3) + att\_2(3,3) / 2.0

\*\*\*

\* v2 Changes for PR#24. End Change.

\*\*\*

\*\*\*

\* v1 Changes for PR#23. End Change.

\*\*\*

return

end

\*\*\*\*\* end of subroutine AVG\_ATT \*\*\*\*\*

\*\*\*\*\*

\* Title: AVG\_VEL

\* Facility: Pluto

\* Abstract:

\* Add two 1x3 vector's

\* result = (vec1 + vec2 / 2)

\*

\* Arguments:

```

*      result  array (1..3) of real*8 the result velocity structure
*      vel_1   array (1..3) of real*8 an velocity structure
*      vel_2   array (1..3) of real*8 an velocity structure
*
* Revision History:
*      v0  15-sep-1994 Rob Angellatta (RKA) Original.
*      v1  01-Dec-1994 Philip Morris (PEM)
*****

      subroutine AVG_VEL(result, vel_1, vel_2)

      implicit none

      *** define arguments ***

      real*8      result(1:3)
      real*8      vel_1(1:3), vel_2(1:3)

      *** execution begins here ***

      ***
      * v1 Changes for AR#23. Item 14 & 21. Function no longer averages but
      * divides one element by 2
      ***
      result(1) = vel_1(1) + vel_2(1) / 2.0
      result(2) = vel_1(2) + vel_2(2) / 2.0
      result(3) = vel_1(3) + vel_2(3) / 2.0

      ***
      * v1 Changes for AR#23. End Change.
      ***

      return
      end

      ***** end of subroutine AVG_VEL *****

      ***** end of module GP *****

```

```

*****
* Module:      GPSF.FOR
* Facility:    Pluto
* P-Spec:     2
* Abstract:
*   This module contains the entry for the guidance processing
*   subframe.
*
* List of Routines:
*   subroutine GPSF
*****

*****
* Title: GPSF
* Facility:    Pluto
* Abstract:
*   This routine provides control of the Guidance Processing SubFrame
*   processing.
*
* Arguments:   None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

subroutine GPSF

implicit none

*** execution begins here ***

call GCS_SIM_RENDEZVOUS
call GP
call CP

return
end

***** end of module GPSF.FOR *****

```

```

*****
* Module:      GSP.FOR
* Facility:    Pluto
* P-Spec:     1.4
* Abstract:
*   This module contains the implementation of the functional
*   requirements for GSP.
*
* List of Routines:
*   subroutine GSP
*****

```

```

*****
* Title: GSP
* Facility: Pluto
* Abstract:
*   1) maintain the history of the vehicle rotation rates
*   2) determine the operational status of the gyroscope sensors
*   3) Report the current vehicle rotation rates along each of the
*       vehicle's three axes.
*
* Arguments: None
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*****

```

```

subroutine GSP

implicit none

*** include the global common stores ***

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

*** include constant definitions ***

include 'constants.for'

*** declare local variables ***

***
* v1 Changes for AR#23. Item 23. counter type changed from real*8 to integer*2
***
integer*2 counter
real*8      temp

integer*4 i

```

```

***
* v1 Changes for AR#23. End Change.
***
*****
* 1) Maintain the history of the vehicle rotation rates by "rotating
* variables."
*****

```

```

    G_ROTATION(1, 4) = G_ROTATION(1, 3)
    G_ROTATION(1, 3) = G_ROTATION(1, 2)
    G_ROTATION(1, 2) = G_ROTATION(1, 1)
    G_ROTATION(1, 1) = G_ROTATION(1, 0)

```

```

    G_ROTATION(2, 4) = G_ROTATION(2, 3)
    G_ROTATION(2, 3) = G_ROTATION(2, 2)
    G_ROTATION(2, 2) = G_ROTATION(2, 1)
    G_ROTATION(2, 1) = G_ROTATION(2, 0)

```

```

    G_ROTATION(3, 4) = G_ROTATION(3, 3)
    G_ROTATION(3, 3) = G_ROTATION(3, 2)
    G_ROTATION(3, 2) = G_ROTATION(3, 1)
    G_ROTATION(3, 1) = G_ROTATION(3, 0)

```

```

*****
* 2) determine the operational status of the gyroscope sensors.
*****

```

```

    G_STATUS = K$HEALTHY

```

```

*****
* 3) Report the current vehicle rotation rates along each of the
* vehicle's three axes.
*****

```

```

*** range check the atmospheric temperature ***

```

```

    call RANGE_CHECK(ATMOSPHERIC_TEMP,K$ATMOSPHERIC_TEMP$LB,
    &                 K$ATMOSPHERIC_TEMP$UB,'GSP', K$ATMOSPHERIC_TEMP$NAME)

```

```

*****
* The raw sensor data stored in G_COUNTER represents the vehicle rate
* of rotation about a specific axis. The sensor data is
* stored in a modified sign magnitude format. The lower 14-bits
* represent the magnitude of the rotation and the most significant
* bit (bit 15) represents the sign. Bit 14 is not used. A
* positive value of G_COUNTER indicates a positive rotation about
* the vehicle axis consistent with a right handed coordinate system,
* while a negative value indicates a negative rotation consistent
* with a right handed coordinate system.
*****

```



```

temp = (G3 * ATMOSPHERIC_TEMP) + (G4 * ATMOSPHERIC_TEMP**2)

do 100 i = 1, 3

*** convert the raw sensor ***

*****
* Convert the raw sensor data from the modified sign magnitude
* format into an appropriate format for use by the target CPU, in
* this case two's complement. Positive values are represented in
* the same fashion in sign magnitude and two's complement, however,
* negative sensor values must be massaged.
*
* Transfer the magnitude of the rotation from G_COUNTER to the local
* data element named counter by masking bits 14 and 15 from
* G_COUNTER. If G_COUNTER bit 15 is clear, the data element counter
* now contains the properly converted value. If G_COUNTER bit 15 is
* set, the value of data element counter must be negated.
*****

*** clear the two most significant bits (bits 15,14) ***

counter = IAND(G_COUNTER(i), '3FFF'X)

*** if the bit was set, then convert value to two's complement ***

if (BTEST(G_COUNTER(i), 15) .EQ. .TRUE.) then
counter = 0 - counter
end if

*** now, compute the vehicle rotation from the sensor data ***

G_ROTATION(i, 0) = G_OFFSET(i) +
& (G_GAIN_0(i) + temp) * counter

100 continue

return
end

***** end of module GSP.FOR *****

```

```

*****
* Module:    GUIDANCE_STATE.FOR
* Facility:  Pluto
* Abstract:
*   This module contains the data definitions for the
*   global common data store named GUIDANCE_STATE.
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

\*\*\* COMMON block definition \*\*\*

```

COMMON /GUIDANCE_STATE/
&    A_STATUS,
&    AE_STATUS,
&    AE_SWITCH,
&    AE_TEMP,
&    AR_STATUS,
&    C_STATUS,
&    CL,
&    CONTOUR_CROSSED,
&    FRAME_BEAM_UNLOCKED,
&    FRAME_ENGINES_IGNITED,
&    G_STATUS,
&    GP_ALTITUDE,
&    GP_ATTITUDE,
&    GP_PHASE,
&    GP_ROTATION,
&    GP_VELOCITY,
&    INTERNAL_CMD,
&    K_ALT,
&    K_MATRIX,
&    PE_INTEGRAL,
&    RE_STATUS,
&    RE_SWITCH,
&    TDLR_STATE,
&    TDLR_STATUS,
&    TDS_STATUS,
&    TE_INTEGRAL,
&    TE_LIMIT,
&    THETA,
&    TS_STATUS,
&    VELOCITY_ERROR,
&    YE_INTEGRAL

```

\*\*\* data type declarations \*\*\*

```

logical*1 A_STATUS(1:3, 0:3)
logical*1 AE_STATUS
logical*1 AE_SWITCH

```

```

integer*2 AE_TEMP
logical*1 AR_STATUS(0:4)
logical*1 C_STATUS
integer*2 CL
logical*1 CONTOUR_CROSSED
integer*4 FRAME_BEAM_UNLOCKED(1:4)
integer*4 FRAME_ENGINES_IGNITED
logical*1 G_STATUS
real*8      GP_ALTITUDE(0:4)
real*8      GP_ATTITUDE(1:3, 1:3, 0:4)
integer*4 GP_PHASE
real*8      GP_ROTATION(1:3, 1:3)
real*8      GP_VELOCITY(1:3, 0:4)
real*8      INTERNAL_CMD(1:3)
integer*4 K_ALT(0:4)
integer*4 K_MATRIX(1:3, 1:3, 0:4)
real*8      PE_INTEGRAL
logical*1 RE_STATUS
logical*1 RE_SWITCH
logical*1 TDLR_STATE(1:4)
logical*1 TDLR_STATUS(1:4)
logical*1 TDS_STATUS
real*8      TE_INTEGRAL
real*8      TE_LIMIT
real*8      THETA
logical*1 TS_STATUS(1:2)
real*8      VELOCITY_ERROR
real*8      YE_INTEGRAL

```

\*\*\*\*\* end of module GUIDANCE\_STATE.FOR \*\*\*\*\*

```

*****
* Module:    PLUTO.FOR
* Facility:  Pluto
* P-Spec:    0
* Abstract:
*   This module contains the main routine for the Pluto
*   implementation.
*
* List of Routines:
*   program Pluto
*****

```

```

*****
* Title: PLUTO
* Facility:  Pluto
* Abstract:
*   This is the main routine for the Pluto implementation.
*
* Arguments: None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*   v2 15-Feb-1995 Philip Morris (PEM)
*****

```

program PLUTO

implicit none

\*\*\* include the global common stores \*\*\*

include 'guidance\_state.for'

\*\*\* execution begins here \*\*\*

```

*****
* Simply loop through the three subframes until done
*****

```

\*\*\*

\* v2 Changes for AR#26. Item 2. Remove dead code.

\*\*\*

\* 100 continue

\*\*\*

\* v2 Changes for AR#26. End Change.

\*\*\*

\*\*\*

\* v1 Changes for AR#23. Item 6&7. Added DO WHILE loop to remove gotos

\*\*\*

```
*** stop when gp_phase = 5 ***  
  
do while (GP_PHASE .NE. 5)  
  
*** execute the sensor processing subframe ***  
  
    call SPSF  
  
*** execute the guidance processing subframe ***  
  
    call GPSF  
  
*** execute the control law processing subframe ***  
  
    call CLPSF  
  
end do  
  
***  
* v1 Changes for AR#23. End Change.  
***  
    stop  
    end  
  
***** end of module PLUTO.FOR *****
```

```

*****
* Module:      RECLP.FOR
* Facility:    Pluto
* P-Spec:     3.4
* Abstract:
*   This module contains the implementation of the functional
*   requirements for RECLP.
*
* List of Routines:
*   subroutine RECLP
*****

```

```

*****
* Title: RECLP
* Facility:    Pluto
* Abstract:
*   1) determine the current operational status of the roll engines.
*   2) generate the appropriate roll engine command.
*
* Arguments:  None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

subroutine RECLP

implicit none

\*\*\* include the global common stores \*\*\*

```

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

```

\*\*\* include constant definitions \*\*\*

```

include 'constants.for'

```

```

*****
* 1) Determine the current operational status of the roll engines.
*****

```

```

RE_STATUS = K$HEALTHY

```

```

*****
* 2) Generate the appropriate roll engine command.
*****

```

```

if (RE_SWITCH .EQ. K$ROLL_ENGINES_ARE_OFF) then

```

```

    RE_CMD = K$OFF + K$CW
else

*** range check the x-axis vehicle rotation rate ***

    call RANGE_CHECK(G_ROTATION(1, 0), K$G_ROTATION$LB,
&                K$G_ROTATION$UB, 'RECLP', K$G_ROTATION$NAME)

*** range check the x-axis vehicle rotation displacement ***

    call RANGE_CHECK(THETA, K$THETA$LB,
&                K$THETA$UB, 'RECLP', K$THETA$NAME)

*****
* The roll engine command consists of two components: an
* intensity, and a direction. Taking into account the command data
* encoding, the possible intensities are: Off (0), Minimum (2),
* Intermediate (4), and Maximum (6), and the possible directions
* are CounterClockwise (0) and Clockwise (1).
*
* Both roll engine command components are determined from the
* current value of the vehicle's roll rate and rotational
* displacement about the x-axis.
*
* Employing Euler's method for differential equations, compute the
* current x-axis angular displacement, theta.
*****

    THETA = THETA + G_ROTATION(1, 0) * DELTA_T

*** range check the theta again before use ***

    call RANGE_CHECK(THETA, K$THETA$LB,
&                K$THETA$UB, 'RECLP', K$THETA$NAME)

*****
* From figure 5.2 "Graph for Deriving Roll Engine Commands" of the
* GCS development specifications, determine the appropriate roll
* engine intensity and direction.
*****

*** check case when theta = 0 ***

    if (THETA .EQ. 0) then
    if (G_ROTATION(1, 0) .GT. P4) then
        RE_CMD = K$MAXIMUM + K$CW
    else if (G_ROTATION(1, 0) .LT. -P4) then
        RE_CMD = K$MAXIMUM + K$CCW
    else
        RE_CMD = K$OFF + K$CW
    end if

```

\*\*\* check first and fourth quadrants \*\*\*

```
else if (THETA .GT. 0) then
  if (THETA .LE. THETA1) then

    if (G_ROTATION(1, 0) .GT. P2) then
      RE_CMD = K$MAXIMUM + K$CW
    else if (G_ROTATION(1, 0) .GT. P1) then
      RE_CMD = K$INTERMEDIATE + K$CW
    else if (G_ROTATION(1, 0) .GE. -P4) then
      RE_CMD = K$OFF + K$CW
    else
      RE_CMD = K$MAXIMUM + K$CCW
    end if
```

```
else if (THETA .LE. THETA2) then
```

```
  if (G_ROTATION(1, 0) .GT. P2) then
    RE_CMD = K$MAXIMUM + K$CW
  else if (G_ROTATION(1, 0) .GT. P1) then
    RE_CMD = K$INTERMEDIATE + K$CW
  else if (G_ROTATION(1, 0) .GT. 0.0) then
    RE_CMD = K$MINIMUM + K$CW
  else if (G_ROTATION(1, 0) .GE. -P4) then
    RE_CMD = K$OFF + K$CW
  else
    RE_CMD = K$MAXIMUM + K$CCW
  end if
```

```
else
```

```
*           THETA > THETA2
```

```
  if (G_ROTATION(1, 0) .GT. -P3) then
    RE_CMD = K$MAXIMUM + K$CW
  else if (G_ROTATION(1, 0) .GE. -P4) then
    RE_CMD = K$OFF + K$CW
  else
    RE_CMD = K$MAXIMUM + K$CCW
  end if
```

```
end if
```

\*\*\* check second and third quadrants \*\*\*

```
else
```

```
*           THETA .LT. 0
```

```
if (THETA .GE. -THETA1) then
```

```
  if (G_ROTATION(1, 0) .GT. p4) then
    RE_CMD = K$MAXIMUM + K$CW
```



```

else if (G_ROTATION(1, 0) .GE. -P1) then
  RE_CMD = K$OFF + K$CW
else if (G_ROTATION(1, 0) .GE. -P2) then
  RE_CMD = K$INTERMEDIATE + K$CCW
else
  RE_CMD =      K$MAXIMUM + K$CCW
end if

else if (THETA .GE. -THETA2) then

  if (G_ROTATION(1, 0) .GT. P4) then
    RE_CMD = K$MAXIMUM + K$CW
  else if (G_ROTATION(1, 0) .GE. 0.0) then
    RE_CMD =      K$OFF + K$CW
  else if (G_ROTATION(1, 0) .GE. -P1) then
    RE_CMD = K$MINIMUM + K$CCW
  else if (G_ROTATION(1, 0) .GE. -P2) then
    RE_CMD = K$INTERMEDIATE + K$CCW
  else
    RE_CMD = K$MAXIMUM + K$CCW
  end if

else
  *
  THETA < -THETA2

  if (G_ROTATION(1, 0) .GT. P4) then
    RE_CMD = K$MAXIMUM + K$CW
  else if (G_ROTATION(1, 0) .GE. P3) then
    RE_CMD = K$OFF + K$CW
  else
    RE_CMD =      K$MAXIMUM + K$CCW
  end if

  end if
end if
end if

return

end

***** end of module RECLP.FOR *****

```

```

*****
* Module:      RUN_PARAMETERS.FOR
* Facility:    Pluto
* Abstract:
*   This module contains the data definitions for the
*   global common data store named RUN_PARAMETERS.
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

\*\*\* COMMON block definition \*\*\*

```

COMMON      /RUN_PARAMETERS/
&          A_BIAS,
&          A_GAIN_0,
&          A_SCALE,
&          ALPHA_MATRIX,
&          AR_FREQUENCY,
&          COMM_SYNC_PATTERN,
&          CONTOUR_ALTITUDE,
&          CONTOUR_VELOCITY,
&          DELTA_T,
&          DROP_HEIGHT,
&          DROP_SPEED,
&          ENGINES_ON_ALTITUDE,
&          FULL_UP_TIME,
&          G1,
&          G2,
&          G3,
&          G4,
&          G_GAIN_0,
&          G_OFFSET,
&          GA,
&          GAX,
&          GP1,
&          GP2,
&          GPY,
&          GQ,
&          GR,
&          GRAVITY,
&          GV,
&          GVE,
&          GVEI,
&          GVI,
&          GW,
&          GWI,
&          M1,
&          M2,
&          M3,
&          M4,

```

```

&    MAX_NORMAL_VELOCITY,
&    OMEGA,
&    P1,
&    P2,
&    P3,
&    P4,
&    PE_MAX,
&    PE_MIN,
&    T1,
&    T2,
&    T3,
&    T4,
&    TDLR_ANGLES,
&    TDLR_GAIN,
&    TDLR_LOCK_TIME,
&    TDLR_OFFSET,
&    TE_DROP,
&    TE_INIT,
&    TE_MAX,
&    TE_MIN,
&    THETA1,
&    THETA2,
&    YE_MAX,
&    YE_MIN

```

\*\*\* data type declarations \*\*\*

```

real*8    A_BIAS(1:3)
real*8    A_GAIN_0(1:3)
integer*4 A_SCALE
real*8    ALPHA_MATRIX(1:3, 1:3)
real*8    AR_FREQUENCY
integer*2 COMM_SYNC_PATTERN
real*8    CONTOUR_ALTITUDE(1:100)
real*8    CONTOUR_VELOCITY(1:100)
real*8    DELTA_T
real*8    DROP_HEIGHT
real*8    DROP_SPEED
real*8    ENGINES_ON_ALTITUDE
real*8    FULL_UP_TIME
real*8    G1
real*8    G2
real*8    G3
real*8    G4
real*8    G_GAIN_0(1:3)
real*8    G_OFFSET(1:3)
real*8    GA
real*8    GAX
real*8    GP1
real*8    GP2
real*8    GPY

```

```
real*8      GQ(1:2)
real*8      GR(1:2)
real*8      GRAVITY
real*8      GV(1:2)
real*8      GVE
real*8      GVEI(1:2)
real*8      GVI(1:2)
real*8      GW(1:2)
real*8      GWI(1:2)
integer*2   M1
integer*2   M2
integer*2   M3
integer*2   M4
real*8      MAX_NORMAL_VELOCITY
real*8      OMEGA
real*8      P1
real*8      P2
real*8      P3
real*8      P4
real*8      PE_MAX(1:2)
real*8      PE_MIN(1:2)
real*8      T1
real*8      T2
real*8      T3
real*8      T4
real*8      TDLR_ANGLES(1:3)
real*8      TDLR_GAIN
real*8      TDLR_LOCK_TIME
real*8      TDLR_OFFSET
real*8      TE_DROP
real*8      TE_INIT
real*8      TE_MAX(1:2)
real*8      TE_MIN(1:2)
real*8      THETA1
real*8      THETA2
real*8      YE_MAX(1:2)
real*8      YE_MIN(1:2)
```

```
***** end of module RUN_PARAMETERS.FOR *****
```

```

*****
* Module:      SENSOR_OUTPUT.FOR
* Facility:    Pluto
* Abstract:
*   This module contains the data definitions for the
*   global common data store named EXTERNAL.
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

*** COMMON block definition ***

COMMON /SENSOR_OUTPUT/
&      A_ACCELERATION,
&      AR_ALTITUDE,
&      ATMOSPHERIC_TEMP,
&      G_ROTATION,
&      TD_SENSED,
&      TDLR_VELOCITY

*** data type declarations ***

real*8      A_ACCELERATION(1:3, 0:4)
real*8      AR_ALTITUDE(0:4)
real*8      ATMOSPHERIC_TEMP
real*8      G_ROTATION(1:3, 0:4)
logical*1   TD_SENSED
real*8      TDLR_VELOCITY(1:3, 0:4)

***** end of module SENSOR_OUTPUT.FOR *****

```

\*\*\*\*\*

\* Module: SPSF.FOR

\* Facility: Pluto

\* Abstract:

\* This module contains the entry for the sensor processing  
\* subframe.

\*

\* List of Routines:

\* subroutine SPSF

\*\*\*\*\*

\*\*\*\*\*

\* Title: SPSF

\* Facility: Pluto

\* Abstract:

\* This routine provides control of the Sensor Processing SubFrame  
\* processing.

\*

\* Arguments: None

\*

\* Revision History:

\* v0 15-sep-1994 Rob Angellatta (RKA) Original.

\*\*\*\*\*

subroutine SPSF

implicit none

\*\*\* execution begins here \*\*\*

call GCS\_SIM\_RENDEZVOUS

call TSP

call ARSP

call ASP

call GSP

call TDLRSP

call TDSP

call CP

return

end

\*\*\*\*\* end of module SPSF.FOR \*\*\*\*\*

```

*****
* Module:      TDLRSP.FOR
* Facility:    Pluto
* P-Spec:     1.5
* Abstract:
*   This module contains the implementation of the functional
*   requirements for TDLRSP.
*
* List of Routines:
*   subroutine TDLRSP
*****

```

```

*****
* Title: TDLRSP
* Facility: Pluto
* Abstract:
*   1) Maintain the history of the vehicle velocities and the
*       velocity computation indicator
*   2) Determine the operational status of touch down landing radar
*       sensor
*   3) Report the current vehicle velocities along each of the
*       vehicle's three axes
*   4) Report the velocity computation indicators.
*
* Arguments: None
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*   v2 10-JAN-1995 Philip Morris (PEM)
*****

```

```

subroutine TDLRSP

```

```

implicit none

```

```

*** include the global common stores ***

```

```

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'

```

```

*** include constant definitions ***

```

```

include 'constants.for'

```

```

*** declare local variables ***

```

```

integer*4 i

```

```

real*8      b(4)

```

```

real*8      pbvX
real*8      pbvY
real*8      pbvZ

real*8      elapsed_time

```

```

*****
* 1) Maintain the history of the vehicle velocities and the
* velocity computation indicator by "rotating variables." The data
*****

```

```

TDLR_VELOCITY(1, 4) = TDLR_VELOCITY(1, 3)
TDLR_VELOCITY(1, 3) = TDLR_VELOCITY(1, 2)
TDLR_VELOCITY(1, 2) = TDLR_VELOCITY(1, 1)
TDLR_VELOCITY(1, 1) = TDLR_VELOCITY(1, 0)

```

```

TDLR_VELOCITY(2, 4) = TDLR_VELOCITY(2, 3)
TDLR_VELOCITY(2, 3) = TDLR_VELOCITY(2, 2)
TDLR_VELOCITY(2, 2) = TDLR_VELOCITY(2, 1)
TDLR_VELOCITY(2, 1) = TDLR_VELOCITY(2, 0)

```

```

TDLR_VELOCITY(3, 4) = TDLR_VELOCITY(3, 3)
TDLR_VELOCITY(3, 3) = TDLR_VELOCITY(3, 2)
TDLR_VELOCITY(3, 2) = TDLR_VELOCITY(3, 1)
TDLR_VELOCITY(3, 1) = TDLR_VELOCITY(3, 0)

```

```

K_MATRIX(1, 1, 4) = K_MATRIX(1, 1, 3)
K_MATRIX(1, 2, 4) = K_MATRIX(1, 2, 3)
K_MATRIX(1, 3, 4) = K_MATRIX(1, 3, 3)
K_MATRIX(2, 1, 4) = K_MATRIX(2, 1, 3)
K_MATRIX(2, 2, 4) = K_MATRIX(2, 2, 3)
K_MATRIX(2, 3, 4) = K_MATRIX(2, 3, 3)
K_MATRIX(3, 1, 4) = K_MATRIX(3, 1, 3)
K_MATRIX(3, 2, 4) = K_MATRIX(3, 2, 3)
K_MATRIX(3, 3, 4) = K_MATRIX(3, 3, 3)

```

```

K_MATRIX(1, 1, 3) = K_MATRIX(1, 1, 2)
K_MATRIX(1, 2, 3) = K_MATRIX(1, 2, 2)
K_MATRIX(1, 3, 3) = K_MATRIX(1, 3, 2)
K_MATRIX(2, 1, 3) = K_MATRIX(2, 1, 2)
K_MATRIX(2, 2, 3) = K_MATRIX(2, 2, 2)
K_MATRIX(2, 3, 3) = K_MATRIX(2, 3, 2)
K_MATRIX(3, 1, 3) = K_MATRIX(3, 1, 2)
K_MATRIX(3, 2, 3) = K_MATRIX(3, 2, 2)
K_MATRIX(3, 3, 3) = K_MATRIX(3, 3, 2)

```

```

K_MATRIX(1, 1, 2) = K_MATRIX(1, 1, 1)
K_MATRIX(1, 2, 2) = K_MATRIX(1, 2, 1)
K_MATRIX(1, 3, 2) = K_MATRIX(1, 3, 1)
K_MATRIX(2, 1, 2) = K_MATRIX(2, 1, 1)
K_MATRIX(2, 2, 2) = K_MATRIX(2, 2, 1)

```



K\_MATRIX(2, 3, 2) = K\_MATRIX(2, 3, 1)  
K\_MATRIX(3, 1, 2) = K\_MATRIX(3, 1, 1)  
K\_MATRIX(3, 2, 2) = K\_MATRIX(3, 2, 1)  
K\_MATRIX(3, 3, 2) = K\_MATRIX(3, 3, 1)

K\_MATRIX(1, 1, 1) = K\_MATRIX(1, 1, 0)  
K\_MATRIX(1, 2, 1) = K\_MATRIX(1, 2, 0)  
K\_MATRIX(1, 3, 1) = K\_MATRIX(1, 3, 0)  
K\_MATRIX(2, 1, 1) = K\_MATRIX(2, 1, 0)  
K\_MATRIX(2, 2, 1) = K\_MATRIX(2, 2, 0)  
K\_MATRIX(2, 3, 1) = K\_MATRIX(2, 3, 0)  
K\_MATRIX(3, 1, 1) = K\_MATRIX(3, 1, 0)  
K\_MATRIX(3, 2, 1) = K\_MATRIX(3, 2, 0)  
K\_MATRIX(3, 3, 1) = K\_MATRIX(3, 3, 0)

\*\*\*\*\*

\* 2) Determine the operational status of touch down landing radar sensor.

\*\*\*\*\*

TDLR\_STATUS(1) = K\$HEALTHY  
TDLR\_STATUS(2) = K\$HEALTHY  
TDLR\_STATUS(3) = K\$HEALTHY  
TDLR\_STATUS(4) = K\$HEALTHY

\*\*\*\*\*

\* 3) Reporting the current vehicle velocities along each of the  
\* vehicle's three axes and reporting the velocity computation  
\* indicators.

\*\*\*\*\*

\*\*\*\*\*

\* 3A) Determine the state of the four radar beams.

\*

\* The data element TDLR\_STATE contains the state of the radar  
\* beams.

\*

\* Valid radar beam states are "locked" (value 1) and "unlocked"  
\* (value 0). The present state of a radar beam is determined from  
\* the current value of the sensor data and the previous state of  
\* the radar beam. A sensor measurement of zero indicates that the  
\* radar beam echo was not received and the radar beam is considered  
\* to be "unlocked." A non-zero sensor measurement indicates that a  
\* radar beam echo was received, but does not imply a radar beam  
\* state of "locked." Because, once a radar beam is declared  
\* "unlocked," it is rendered unusable (remains "unlocked"  
\* regardless of the sensor data value) for a specified period of  
\* time. This waiting period must be implemented in the software.

\*

\* A beam is deemed "locked" when 1) the current sensor value  
\* contains a non-zero value and the beam's previous state was  
\* "locked"; or 2) the current sensor value contains a non-zero

```

* value and the beam's previous state was "unlocked" and the
* elapsed time since the beam was determined "unlocked" is greater
* than or equal to the sensor recovery period.
*
* The data element TDLR_LOCK_TIME specifies the unlocked sensor
* recovery (waiting) period. The data element FRAME_BEAM_UNLOCKED
* is updated with the value of the FRAME_COUNTER during the frame
* in which a radar beam state is first determined as "unlocked."
* The data element DELTA_T specifies in seconds the duration of a
* single frame. Thus the elapsed time since a radar beam was
* declared "unlocked" can be determined by subtracting the present
* value of FRAME_COUNTER from the value of FRAME_BEAM_UNLOCKED and
* multiplying the result by the value of DELTA_T.
*****

```

```

**** process each radar beam ****

```

```

do 100 i=1,4

  if (TDLR_COUNTER(i) .EQ. 0) then

    if (TDLR_STATE(i) .EQ. K$BEAM_LOCKED) then
      TDLR_STATE(i) = K$BEAM_UNLOCKED
      FRAME_BEAM_UNLOCKED(i) = FRAME_COUNTER
    ***
    * v2 Changes for AR#24. Item 7. Added else if.
    ***
    *
    *     else
    *       elseif (TDLR_STATE(i) .EQ. K$BEAM_UNLOCKED) then
    ***
    * v2 Changes for AR#24. End Change.
    ***
    *
    *           the beam was unlocked
    *     elapsed_time = DELTA_T *
    * &           (FRAME_COUNTER - FRAME_BEAM_UNLOCKED(i))
    *
    *     if (elapsed_time .GE. TDLR_LOCK_TIME) then
    *       FRAME_BEAM_UNLOCKED(i) = FRAME_COUNTER
    *     end if
    *   end if

    *     else
    *           the sensor measurement != 0

    *     if (TDLR_STATE(i) .EQ. K$BEAM_UNLOCKED) then
    *       elapsed_time = DELTA_T *
    * &       (FRAME_COUNTER - FRAME_BEAM_UNLOCKED(i))
    *
    *     if (elapsed_time .GE. TDLR_LOCK_TIME) then
    *       TDLR_STATE(i) = K$BEAM_LOCKED

```

```

        end if
      end if
    end if
100 continue

```

```

*****
* 3B) Determine the beam velocities.
*****

```

```

      do 200 i=1,4
        b(i) = TDLR_OFFSET + TDLR_GAIN * TDLR_COUNTER(i)
      200 continue

```

```

*****
* 3C) Determine the "processed" beam velocities, and
* 4) Determine the velocity computation indicators.
*****

```

```

* Compute a "processed" beam velocity for each of the three axes as
* specified by the following table:

```

```

* Beams |          PROCESSED BEAM VELOCITIES          | K-MATRIX | Case
* in lock | pbvX      pbvY      pbvZ | X Y Z | Number

```

Beams in lock	pbvX	pbvY	pbvZ	X	Y	Z	Case Number
none	0	0	0	0	0	0	0
1	0	0	0	0	0	0	1
2	0	0	0	0	0	0	2
3	0	0	0	0	0	0	4
4	0	0	0	0	0	0	8
1,2	0	$(b(1)-b(2))/2$	0	0	1	0	3
1,3	$(b(1)+b(3))/2$	0	0	1	0	0	5
1,4	0	0	$(b(1)-b(4))/2$	0	0	1	9
2,3	0	0	$(b(2)-b(3))/2$	0	0	1	6
2,4	$(b(2)+b(4))/2$	0	0	1	0	0	10
3,4	0	$(b(4)-b(3))/2$	0	0	1	0	12
1,2,3	$(b(1)+b(3))/2$	$(b(1)-b(2))/2$	$(b(2)-b(3))/2$	1	1	1	7
1,2,4	$(b(2)+b(4))/2$	$(b(1)-b(2))/2$	$(b(1)-b(4))/2$	1	1	1	11
1,3,4	$(b(1)+b(3))/2$	$(b(4)-b(3))/2$	$(b(1)-b(4))/2$	1	1	1	13
2,3,4	$(b(2)+b(4))/2$	$(b(4)-b(3))/2$	$(b(2)-b(3))/2$	1	1	1	14
1,2,3,4	a	b	c	1	1	1	15

```

* a)  $(b(1)+b(2)+b(3)+b(4))/4$ 
* b)  $(b(1)-b(2)-b(3)+b(4))/4$ 
* c)  $(b(1)+b(2)-b(3)-b(4))/4$ 

```

```

* Each of the 16 possible cases has been assigned a case number to
* facilitate the description of the necessary processing. The case
* number is found in the column labeled "Case Number" in the table

```

```

* above.
*
* Determine the case number value for the current processing.
* Each of the four radar beams' state has been assigned a weight
* value: beam 1: 1, beam 2: 2, beam 3: 4, beam 4: 8. The "case
* number" is computed by summing the radar beams multiplied by their
* their weight factors.
*****

***
* v1 Changes for AR#23. Item 24. Default goto 2000 added.
***
      go to (1000,1000,1000,1010,1000,1020,1040,1070,
&      1000,1030,1050,1080,1060,1090,1100,1110),
&      TDLR_STATE(1) + 2*TDLR_STATE(2) +
&      4*TDLR_STATE(3) + 8*TDLR_STATE(4) + 1
      go to 2000
***
* v1 Changes for AR#23. End Change.
***
*** cases 0, 1, 2, 4, 8 ***

1000   pbvX = 0.0
        pbvY = 0.0
        pbvZ = 0.0

        K_MATRIX(1, 1, 0) = 0
        K_MATRIX(2, 2, 0) = 0
        K_MATRIX(3, 3, 0) = 0
        go to 2000

*** case 3 ***

1010   pbvX = 0.0
        pbvY = (b(1) - b(2)) / 2.0
        pbvZ = 0.0

        K_MATRIX(1, 1, 0) = 0
        K_MATRIX(2, 2, 0) = 1
        K_MATRIX(3, 3, 0) = 0
        go to 2000

*** case 5 ***

1020   pbvX = (b(1) + b(3)) / 2.0
        pbvY = 0.0
        pbvZ = 0.0

        K_MATRIX(1, 1, 0) = 1
        K_MATRIX(2, 2, 0) = 0
        K_MATRIX(3, 3, 0) = 0

```

go to 2000

\*\*\* case 9 \*\*\*

1030 pbvX = 0.0  
pbvY = 0.0  
pbvZ = (b(1) - b(4)) / 2.0  
  
K\_MATRIX(1, 1, 0) = 0  
K\_MATRIX(2, 2, 0) = 0  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\* case 6 \*\*\*

\*\*\*

\* v1 Changes for AR#23. Item 25. Goto 2000 added to finish the case properly

\*\*\*

1040 pbvX = 0.0  
pbvY = 0.0  
pbvZ = (b(2) - b(3)) / 2.0  
  
K\_MATRIX(1, 1, 0) = 0  
K\_MATRIX(2, 2, 0) = 0  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\*

\* v1 Changes for AR#23. End Change.

\*\*\*

\*\*\* case 10 \*\*\*

1050 pbvX = (b(2) + b(4)) / 2.0  
pbvY = 0.0  
pbvZ = 0.0  
  
K\_MATRIX(1, 1, 0) = 1  
K\_MATRIX(2, 2, 0) = 0  
K\_MATRIX(3, 3, 0) = 0  
go to 2000

\*\*\* case 12 \*\*\*

1060 pbvX = 0.0  
pbvY = (b(4) - b(3)) / 2.0  
pbvZ = 0.0  
  
K\_MATRIX(1, 1, 0) = 0  
K\_MATRIX(2, 2, 0) = 1  
K\_MATRIX(3, 3, 0) = 0  
go to 2000

\*\*\* case 7 \*\*\*

$$\begin{aligned}1070 \quad \text{pbvX} &= (b(1) + b(3)) / 2.0 \\ \text{pbvY} &= (b(1) - b(2)) / 2.0 \\ \text{pbvZ} &= (b(2) - b(3)) / 2.0\end{aligned}$$

K\_MATRIX(1, 1, 0) = 1  
K\_MATRIX(2, 2, 0) = 1  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\* case 11 \*\*\*

$$\begin{aligned}1080 \quad \text{pbvX} &= (b(2) + b(4)) / 2.0 \\ \text{pbvY} &= (b(1) - b(2)) / 2.0 \\ \text{pbvZ} &= (b(1) - b(4)) / 2.0\end{aligned}$$

K\_MATRIX(1, 1, 0) = 1  
K\_MATRIX(2, 2, 0) = 1  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\* case 13 \*\*\*

$$\begin{aligned}1090 \quad \text{pbvX} &= (b(1) + b(3)) / 2.0 \\ \text{pbvY} &= (b(4) - b(3)) / 2.0 \\ \text{pbvZ} &= (b(1) - b(4)) / 2.0\end{aligned}$$

K\_MATRIX(1, 1, 0) = 1  
K\_MATRIX(2, 2, 0) = 1  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\* case 14 \*\*\*

$$\begin{aligned}1100 \quad \text{pbvX} &= (b(2) + b(4)) / 2.0 \\ \text{pbvY} &= (b(4) - b(3)) / 2.0 \\ \text{pbvZ} &= (b(2) - b(3)) / 2.0\end{aligned}$$

K\_MATRIX(1, 1, 0) = 1  
K\_MATRIX(2, 2, 0) = 1  
K\_MATRIX(3, 3, 0) = 1  
go to 2000

\*\*\* case 15 \*\*\*

$$\begin{aligned}1110 \quad \text{pbvX} &= (b(1) + b(2) + b(3) + b(4)) / 4.0 \\ \text{pbvY} &= (b(1) - b(2) - b(3) + b(4)) / 4.0 \\ \text{pbvZ} &= (b(1) + b(2) - b(3) - b(4)) / 4.0\end{aligned}$$

K\_MATRIX(1, 1, 0) = 1

```
K_MATRIX(2, 2, 0) = 1
K_MATRIX(3, 3, 0) = 1
```

```
2000 continue
```

```
*****
```

```
* 3D) Convert "processed" beam velocities into body velocities.
```

```
*****
```

```
TDLR_VELOCITY(1, 0) = pbvX / COS(TDLR_ANGLES(1))
TDLR_VELOCITY(2, 0) = pbvY / COS(TDLR_ANGLES(2))
TDLR_VELOCITY(3, 0) = pbvZ / COS(TDLR_ANGLES(3))
```

```
return
end
```

```
***** end of module tdlrsp.for *****
```

```

*****
* Module:      TDSP.FOR
* Facility:    Pluto
* P-Spec:     1.6
* Abstract:
*   This module contains the implementation of the functional
*   requirements for CRCP.
*
* List of Routines:
*   subroutine TDSP
*****

```

```

*****
* Title: TDSP
* Facility:    Pluto
* Abstract:
*   1) Determine the operational status of the touch down sensor
*   2) determine if touch down has been sensed.
*
* Arguments:  None
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*****

```

subroutine TDSP

implicit none

\*\*\* include the global common stores \*\*\*

```

include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'

```

\*\*\* include constant definitions \*\*\*

```

include 'constants.for'

```

```

*****
* 1) Determine the operational status of the touch down sensor.
* 2) determine if touch down has been sensed.
*
* The data element TD_COUNTER represents the sensor's measurement.
* There are only two valid sensor measurements: A) all bits set
* (value -1) which indicates touch down is sensed, and B) all bits
* clear (value 0) which indicates touch down is not sensed. If a valid
* sensor value exists, then the operation status of the touch down sensor
* is reported as "healthy" (value 0). Any other value of TD_COUNTER
* indicates a faulty sensor in which case the touch down sensor
* status is reported as "failed" (value 1).

```



```

*
* Note, once the touch down sensor has been determined to be
* faulty, it is considered to be failed for the duration of the
* mission -- no processing occurs once the sensor has failed.
*****

      if (TDS_STATUS .EQ. K$HEALTHY) then

          if (TD_COUNTER .EQ. 0) then
              TD_SENSED = K$TOUCH_DOWN_NOT_SENSED

          else if (TD_COUNTER .EQ. -1) then
              TD_SENSED = K$TOUCH_DOWN_SENSED
*                  faulty sensor
          else
              TD_SENSED = K$TOUCH_DOWN_NOT_SENSED
              TDS_STATUS = K$FAILED

          end if

      end if

      return
      end

***** end of module TDSP.FOR *****

```

\*\*\*\*\*

```
* Module:    TSP.FOR
* Facility:   Pluto
* P-Spec:    1.7
* Abstract:
*   This module contains the implementation of the functional
*   requirements for TSP.
*
* List of Routines:
*   subroutine TSP
*   function LOWER_PARABOLIC_FUNCTION
*   function UPPER_PARABOLIC_FUNCTION
```

\*\*\*\*\*

\*\*\*\*\*

```
* Title: TSP
* Facility:   Pluto
* Abstract:
*
* Purpose:
*   1) Ascertain the operational status of the temperature sensors.
*   2) Determine the current atmospheric temperature based on the
*   measurements provided by two on-board temperature sensors.
*
* Arguments:  None
* Revision History:
*   v0  15-sep-1994  Rob Angellatta (RKA) Original.
*   v1  30-Nov-1994  Philip Morris (PEM)
*   v2  10-JAN-1995  Philip Morris (PEM)
```

\*\*\*\*\*

```
subroutine TSP
```

```
implicit none
```

```
*** include the global common stores ***
```

```
include 'external.for'
include 'guidance_state.for'
include 'sensor_output.for'
include 'run_parameters.for'
```

```
*** include constant definitions ***
```

```
include 'constants.for'
```

```
*** declare local functions ***
```

```
real*8  LOWER_PARABOLIC_FUNCTION
real*8  UPPER_PARABOLIC_FUNCTION
```

```

*** declare local variables ***

real*8    slope
real*8    solid_state_temp
real*8    lower_parabolic_temp_limit
real*8    upper_parabolic_temp_limit
real*8    para_M2_M1
real*8    REAL_THERMO_TEMP

*****

* 1) Determine the operational status of the temperature sensors
*****

    TS_STATUS(1) = K$HEALTHY
    TS_STATUS(2) = K$HEALTHY

*****

* 2A) Compute the temperature based on the solid state sensor
*****

***
* v1 Changes for AR#23. Item 26. Added variable to cast M2-M1 to a real
***
    para_M2_M1 = M2-m1
    call ZERO_CHECK(para_M2_M1, 'TSP')

***
* v1 Changes for AR#23. End Change.
***
    slope      = (T2 - T1)/(M2 - M1)

    solid_state_temp = slope * SS_TEMP + T1 - slope * M1

*****

* 2B) Determine if the temperature is within the valid range of the
* TC sensor;
*****

*****

* Once the function describing the parabola has been determined, the
* temperature representing the lower limit of the parabolic region can
* be determined. The lower limit of the lower parabolic region is
* specified as 15% of the difference of the two calibration
* measurements less than the lower calibration point.
*****

***
* v1 Changes for AR#23. Item 2. "D0" added to 0.15
***
    lower_parabolic_temp_limit =
    &      LOWER_PARABOLIC_FUNCTION(M3 - 0.15D0*(M4 - M3))

```

```

***
* v1 Changes for AR#23. End Change.
***
*****
* Once the function describing the parabola has been determined, the
* temperature representing the upper limit of the parabolic region can
* be determined. The upper limit of the upper parabolic region is
* specified as 15% of the difference of the two calibration
* measurements greater than the upper calibration point.
*****

***
* v1 Changes for AR#23. Item 2. "D0" added to 0.15
***
    upper_parabolic_temp_limit =
    &    UPPER_PARABOLIC_FUNCTION(M4 + 0.15D0*(M4 - M3))

***
* v1 Changes for AR#23. End Change.
***
*****
* Now determine sensor temperature measurement to report
*****

    if ((solid_state_temp .LT. lower_parabolic_temp_limit) .OR.
    &    (solid_state_temp .GT. upper_parabolic_temp_limit)) then

*** the atmospheric temp is beyond the valid range of the TC sensor ***
***   so return the solid_state_temp                                     ***

        ATMOSPHERIC_TEMP = solid_state_temp
    else

*****
* 2C) Compute the temperature based on the TC sensor
*****

        if (THERMO_TEMP .LT. M3) then

*** the atmospheric temp resides within the TC lower parabolic region ***

***
* v2 Changes for AR#24. Item 6. Added variable to cast to a real
***
        REAL_THERMO_TEMP=THERMO_TEMP

        ATMOSPHERIC_TEMP =
LOWER_PARABOLIC_FUNCTION(REAL_THERMO_TEMP)
*    ATMOSPHERIC_TEMP = LOWER_PARABOLIC_FUNCTION(THERMO_TEMP)

```

```

        else if (THERMO_TEMP .GT. M4) then

*** the atmospheric temp resides within the TC upper parabolic region ***

                REAL_THERMO_TEMP=THERMO_TEMP

                ATMOSPHERIC_TEMP =
UPPER_PARABOLIC_FUNCTION(REAL_THERMO_TEMP)
*       ATMOSPHERIC_TEMP = UPPER_PARABOLIC_FUNCTION(THERMO_TEMP)
***
* v2 Changes for AR#24. End Change.
***

        else

*** The temperature resides within the TC sensor linear region ***
*** compute the temperature from the TC linear region ***

                slope  = (T4 - T3)/(M4 - M3)

                ATMOSPHERIC_TEMP =
&       slope * THERMO_TEMP + T3 - slope * M3
                end if
        end if

        return
        end

```

\*\*\*\*\* end of subroutine TSP \*\*\*\*\*

\*\*\*\*\*

```

* Title: LOWER_PARABOLIC_FUNCTION
* Facility: Pluto
* Abstract:
* This routine represents the function of the lower parabolic
* curve of the TC temperature sensor. Given an 'X' value,
* return the corresponding 'Y' value.
*
* Arguments:
* real*8 x -- the 'X' value of interest
*
* Revision History:
* v0 15-sep-1994 Rob Angellatta (RKA) Original.
* v1 30-Nov-1994 Philip Morris (PEM)

```

\*\*\*\*\*

```

real*8 function LOWER_PARABOLIC_FUNCTION(x)

implicit none

```

\*\*\* define the arguments \*\*\*

```

    real*8 x

*** include the global common stores ***

    include 'run_parameters.for'

*** local variables ***

    real*8    half_slope

*** execution begins here ***

    half_slope = ((T4 - T3)/(M4 - M3)) / 2.0

***
* v1 Changes for AR#23. Item 27. "M3 + half" changed "M3 - half"
***
    LOWER_PARABOLIC_FUNCTION =
    &    -(x - M3 - half_slope)**2 + T3 + half_slope**2

***
* v1 Changes for AR#23. End Change.
***

    return
    end

***** end of function LOWER_PARABOLIC_FUNCTION *****

*****
* Title: UPPER_PARABOLIC_FUNCTION
* Facility:    Pluto
* Abstract:
*    This routine represents the function of the upper parabolic
*    curve of the TC temperature sensor. Given an 'X' value,
*    return the corresponding 'Y' value.
*
* Arguments:
*    real*8 x -- the 'X' value of interest
*
* Revision History:
*    v0 15-sep-1994 Rob Angellatta (RKA) Original.
*    v1 30-Nov-1994 Philip Morris (PEM)
*****

    real*8 function UPPER_PARABOLIC_FUNCTION(x)

    implicit none

*** define the arguments ***

```

```

    real*8 x
*** include the global common stores ***

    include 'run_parameters.for'

*** local variables ***

    real*8    half_slope

*** execution begins here ***

    half_slope = ((T4 - T3)/(M4 - M3)) / 2.0

***
* v1 Changes for AR#23. Item 28. Algebra Problem fixed.
***
    UPPER_PARABOLIC_FUNCTION =
&    (x - M4 + half_slope)**2 + T4 - half_slope**2

***
* v1 Changes for AR#23. End Change.
***
    return
    end

***** end of function UPPER_PARABOLIC_FUNCTION ****
***** end of module TSP.FOR ****

```

```

*****
* Module:    UTILITY.FOR
* Facility:  Pluto
* Abstract:
*   A collection of utility routines for Pluto.
*
* List of Routines:
*   subroutine RANGE_CHECK
*   subroutine NEG_VALUE_CHECK
*   subroutine ZERO_CHECK
*****

```

```

*****
* Title: RANGE_CHECK
* Facility:  Pluto
* Abstract:
*   Given a real*8 data element and it's lower and upper bounds,
*   determine if the data element exceeds the lower or upper
*   bound. If the element exceeds one of the bounds, then display
*   an error message.
*
* Arguments:
*   source      real*8           The value to check.
*   lower_bound real*8           The lower bound
*   upper_bound real*8           The upper bound
*   module_text character*(*)    The module name for error msg
*   variable_text character*(*)  The data name for error msg
*
* Notes:
*   The upper bound >= lower_bound
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*****

```

```

subroutine RANGE_CHECK(source, lower_bound, upper_bound,
& module_text, variable_text)

```

```

implicit none

```

```

*** define the subroutine arguments ***

```

```

real*8      source
real*8      lower_bound
real*8      upper_bound
character*(*) module_text
character*(*) variable_text

```

```

*** include a global common store ***

```



```

include 'external.for'

*** format statements ***

***
* v1 Changes for AR#23. Item 29. "x" added before "I4".
***
10 format (x,'%EXCEPTIONAL-CONDITION-GCS-LOWER_LIMIT_EXCEEDED')
20 format (x,'%EXCEPTIONAL-CONDITION-GCS-UPPER_LIMIT_EXCEEDED')
30 format (x, A6, X, A32, x,I4)
40 format (x, A32, E23.14)

***
* v1 Changes for AR#23. End Change.
***
*** execution begins here ***

      if (source .LT. lower_bound) then
        write (6, 10)
        write (6, 30) module_text, module_text, FRAME_COUNTER
        write (6, 40) variable_text, source
      else if (source .GT. upper_bound) then
        write (6, 20)
        write (6, 30) module_text, module_text, FRAME_COUNTER
        write (6, 40) variable_text, source
      end if

      return
end

*** end of RANGE_CHECK ****

*****
* Title: NEG_VALUE_CHECK
* Facility: Pluto
* Abstract:
*   Given a real*8 data element determine if the data element
*   has a value of less than zero. If the value is less than zero,
*   then display an error message.
*
* Arguments:
*   source      real*8           The value to check.
*   module_text character*(*)    The module name for error msg
*
* Revision History:
*   v0 15-sep-1994 Rob Angellatta (RKA) Original.
*   v1 30-Nov-1994 Philip Morris (PEM)
*****

subroutine NEG_VALUE_CHECK(source, module_text)

```

```

    implicit none

*** define the subroutine arguments ***

    real*8          source
    character*(*)   module_text

*** include a global common store ***

    include 'external.for'

*** format statements ***

***
* v1 Changes for AR#23. Item 29. "x" added before "I4".
***
    10  format (' ',%EXCEPTIONAL-CONDITION-GCS-NEGATIVE_SQUARE_ROOT')
    30  format (x, A6, X, A32, x,I4)
    40  format (x, E23.14)

***
* v1 Changes for AR#23. End Change.
***
*** execution begins here ***

    if (source .LT. 0) then
        write (6, 10)
        write (6, 30) module_text, module_text, FRAME_COUNTER
        write (6, 40) source
    end if

    return
end

*** end of NEG_VALUE_CHECK ****

*****
* Title: ZERO_CHECK
* Facility: Pluto
* Abstract:
*     Given a real*8 data element determine if the data element
*     has a value of zero. If the value is zero, then display
*     an error message.
*
* Arguments:
*     source    real*8          The value to check.
*     module_text character*(*) The module name for error msg
*
* Revision History:
*     v0 15-sep-1994 Rob Angellatta (RKA) Original.
*     v1 30-Nov-1994 Philip Morris (PEM)

```

```

*****

      subroutine ZERO_CHECK(source, module_text)

      implicit none

      *** define the subroutine arguments ***

      real*8          source
      character*(*)   module_text

      *** include a global common store ***

      include 'external.for'

      *** format statements ***

      ***
      * v1 Changes for AR#23. Item 29. "x" added before "I4".
      ***
      10  format (x,'%EXCEPTIONAL-CONDITION-GCS-DIVIDE-BY-ZERO')
      30  format (x, A6, X, A32, x,I4)

      ***
      * v1 Changes for AR#23. End Change.
      ***
      *** execution begins here ***

      if (source .EQ. 0) then
         write (6, 10)
         write (6, 30) module_text, module_text, FRAME_COUNTER
      end if

      return
      end

      *** end of ZERO_CHECK *****

      ***** end of module UTILITY.FOR *****

```

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<p>The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.</p> <p><b>PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.</b></p>					
1. REPORT DATE (DD-MM-YYYY) 01-12-2008		2. REPORT TYPE Technical Memorandum		3. DATES COVERED (From - To)	
4. TITLE AND SUBTITLE Guidance and Control Software Project Data - Volume 2: Development Documents			5a. CONTRACT NUMBER		
			5b. GRANT NUMBER		
			5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S) Hayhurst, Kelly J. (Editor)			5d. PROJECT NUMBER		
			5e. TASK NUMBER		
			5f. WORK UNIT NUMBER 457280.02.07.07.06.02		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) NASA Langley Research Center Hampton, VA 23681-2199			8. PERFORMING ORGANIZATION REPORT NUMBER  L-19549		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, DC 20546-0001			10. SPONSOR/MONITOR'S ACRONYM(S)  NASA		
			11. SPONSOR/MONITOR'S REPORT NUMBER(S)  NASA/TM-2008-215551		
12. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 61 Availability: NASA CASI (301) 621-0390					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT The Guidance and Control Software (GCS) project was the last in a series of software reliability studies conducted at Langley Research Center between 1977 and 1994. The technical results of the GCS project were recorded after the experiment was completed. Some of the support documentation produced as part of the experiment, however, is serving an unexpected role far beyond its original project context. Some of the software used as part of the GCS project was developed to conform to the RTCA/DO-178B software standard, "Software Considerations in Airborne Systems and Equipment Certification," used in the civil aviation industry. That standard requires extensive documentation throughout the software development life cycle, including plans, software requirements, design and source code, verification cases and results, and configuration management and quality control data. The project documentation that includes this information is open for public scrutiny without the legal or safety implications associated with comparable data from an avionics manufacturer. This public availability has afforded an opportunity to use the GCS project documents for DO-178B training. This report provides a brief overview of the GCS project, describes the 4-volume set of documents and the role they are playing in training, and includes the development documents from the GCS project.					
15. SUBJECT TERMS Software engineering; Computer programming; Software reliability; DO-178B					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT	b. ABSTRACT	c. THIS PAGE			STI Help Desk (email: help@sti.nasa.gov)
U	U	U	UU	380	19b. TELEPHONE NUMBER (Include area code) (301) 621-0390