



Reduction of Unsteady Forcing in a Vaned, Contra-Rotating Transonic Turbine Configuration

Minnowbrook VI

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and External Aerodynamics**

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Acknowledgements and Collaborations



AFRL

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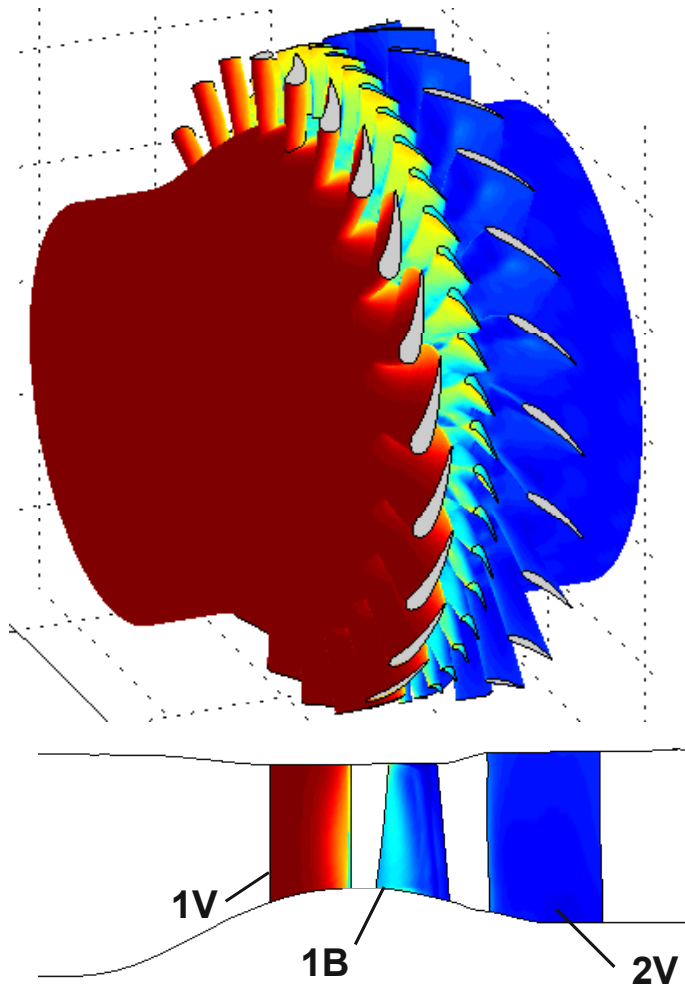
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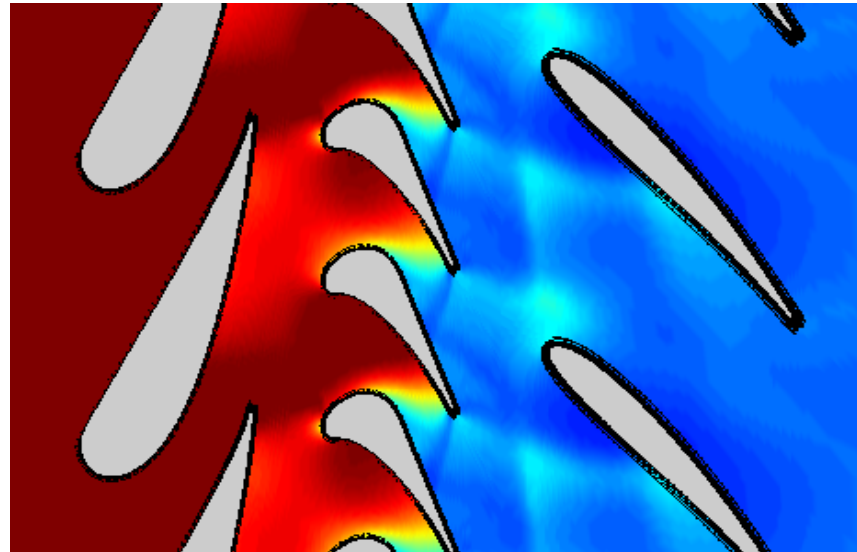


The AFRL High Impact Technologies Research Turbine (HIT RT)



Meanline Design Parameters: HIT RT

PR	3.75 total-total		
Reaction	49.5%		
Flow Coefficient	0.71		
Work Coefficient	2.11		
AN ² (in ² rpm ²)	573 x10 ⁸ (Engine)		
	1V	1B	2V
Turning	77°	116°	11°
M _{exit}	0.88	1.30	0.89
Airfoil Count:	23	46	23

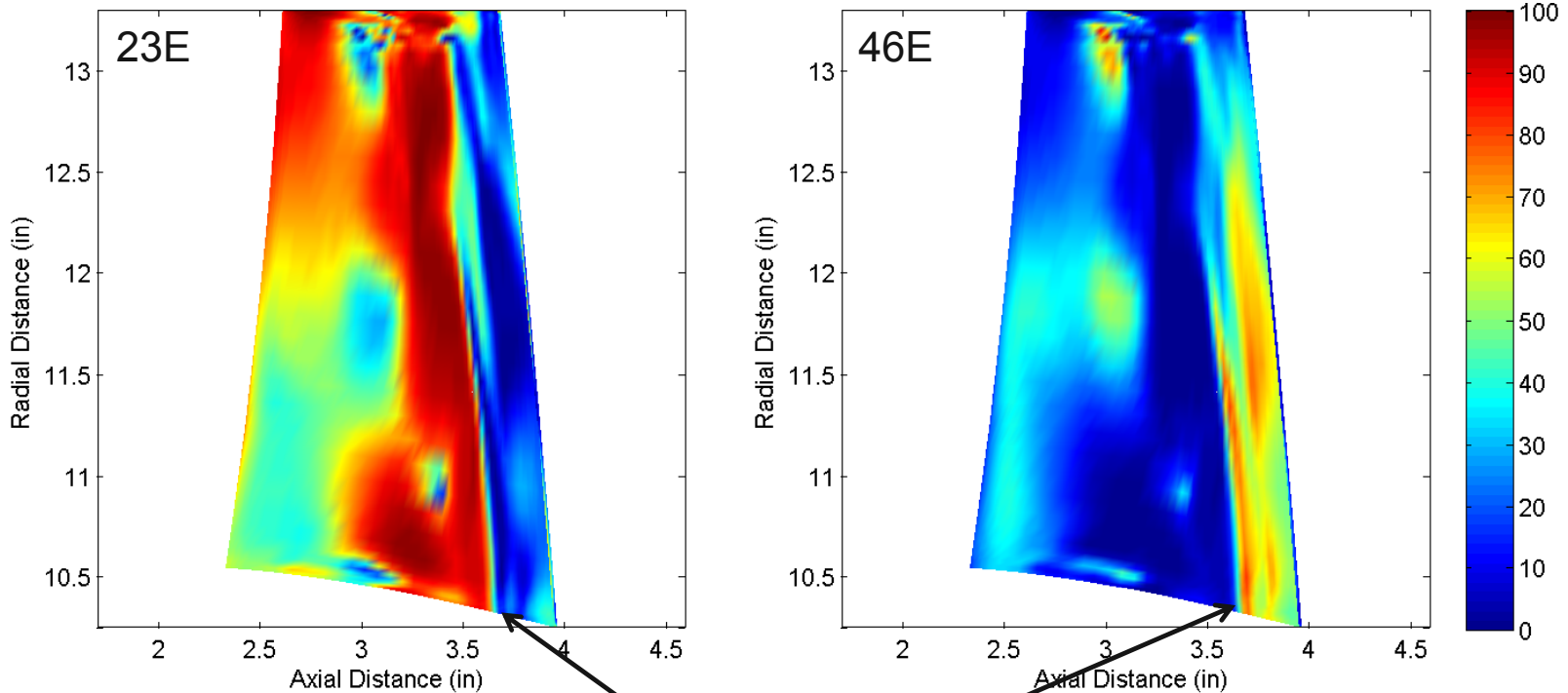




Unsteadiness due to Downstream Interaction is Dominated by First Harmonic of Vane Passing



1B Suction Side, Percent Signal Power



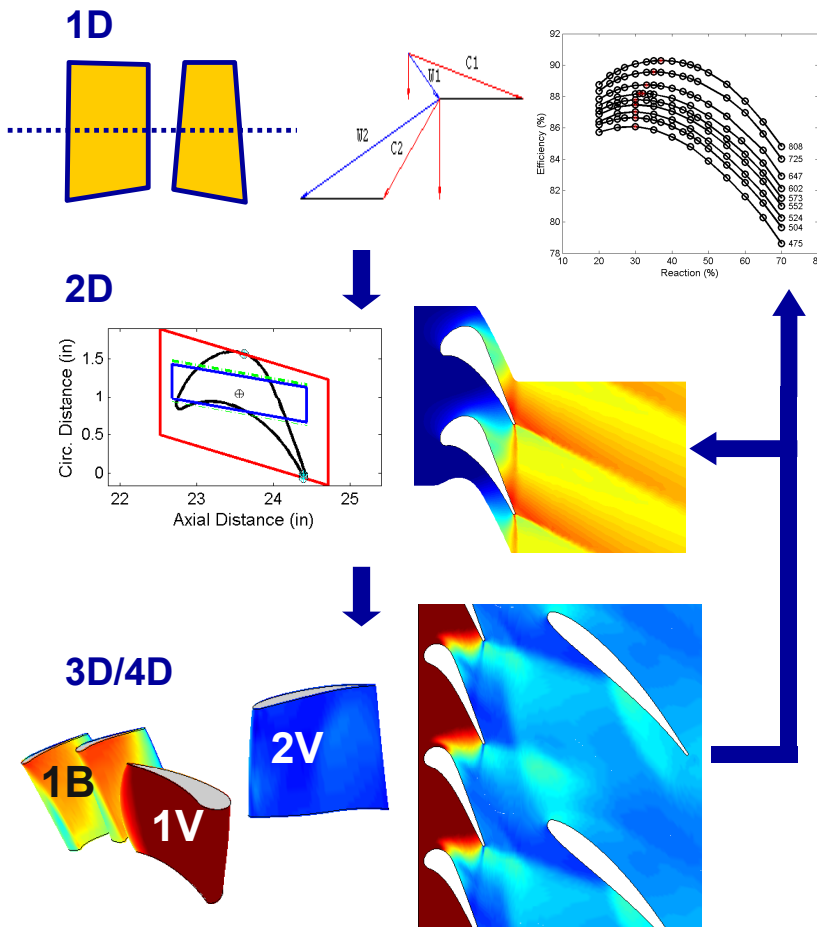
Cross-Passage Shock



Turbine Design And Analysis System : Created to Enable Design of the HIT Research Turbine



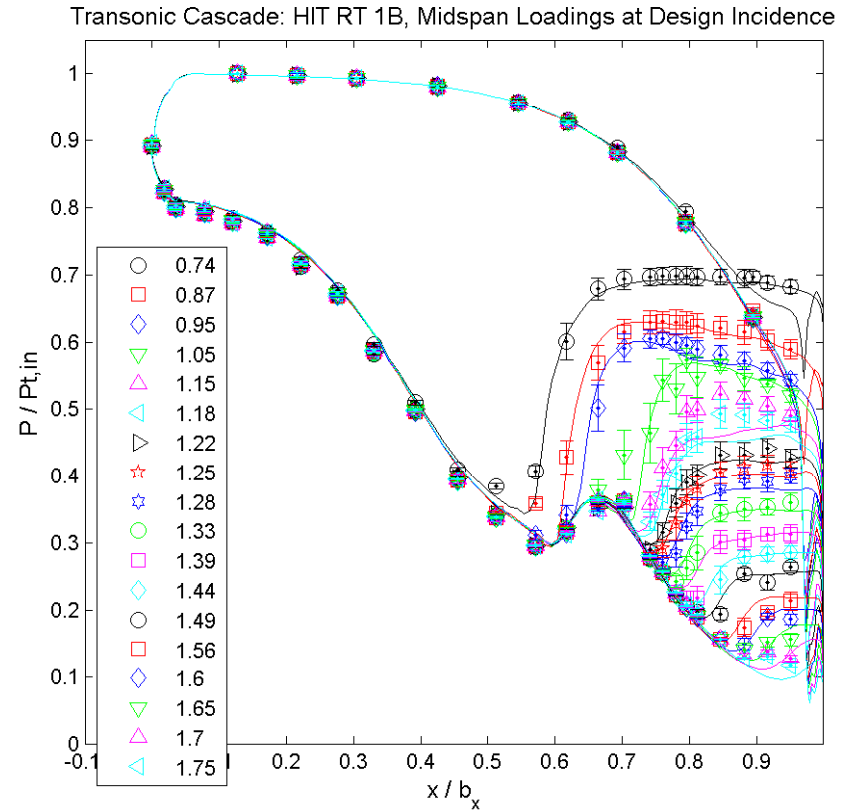
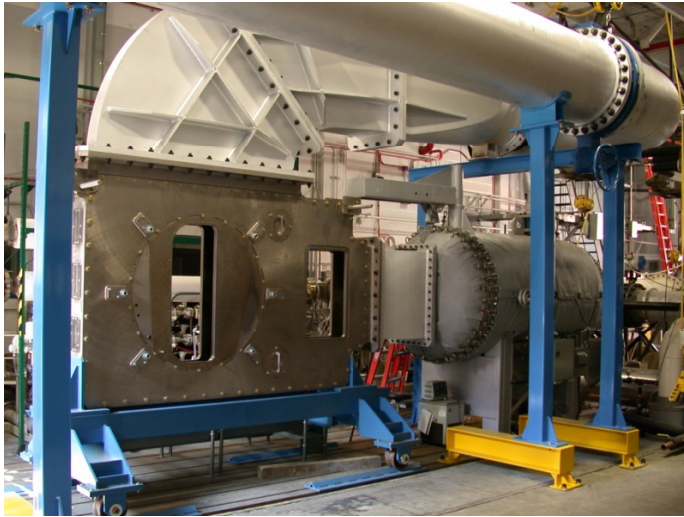
Iterative Turbine-Design Loop



- **1D:** Turbine size and velocity triangles were set with a 1D meanline code (HuberLine, FTT)
- **2D:** Airfoil-section design, analysis, and optimization was conducted in MATLAB
 - HuberFoil (FTT) profile algorithm
 - GUI-based flowfield interrogation
 - Optimization via SQP, genetic algorithms, and DoE
- **4D:** Time-resolved 3D analysis
 - DSP-based convergence-monitoring and unsteady post-processing
 - Enables investigation of unsteady shock interactions and instrumentation design for code validation
- A range of solvers are integrated with the system:
 - Corsair (Dorney, NASA MSFC)
 - LEO (Ni, Aerodynamic Solutions, Inc.)
 - MBFLO (Davis, UC Davis)



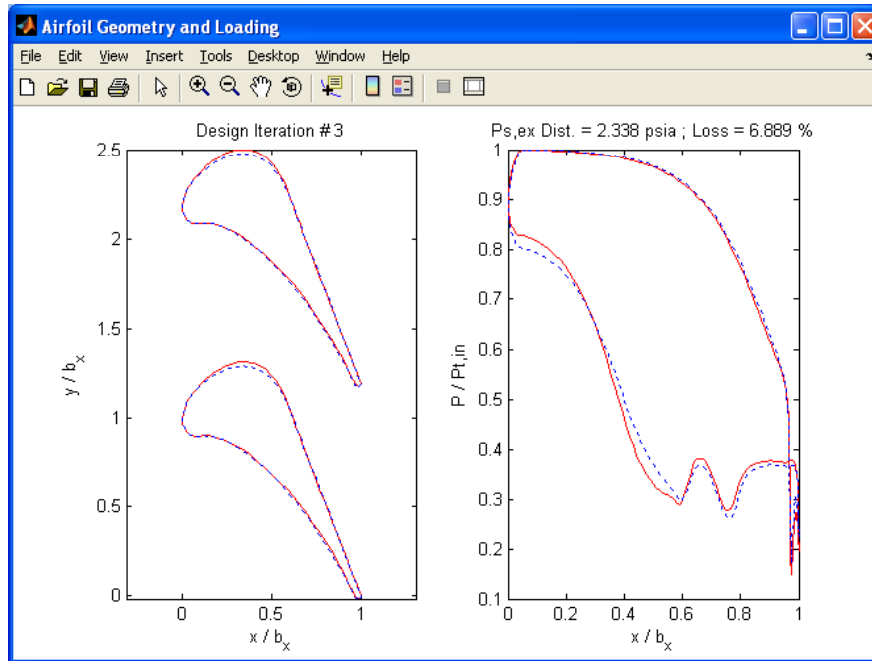
Cascade Experiments are Underway to Validate Design and Analysis Tools



- Match to predictions gives confidence that the source of 1B-2V interaction is controllable via aerodynamic shaping.



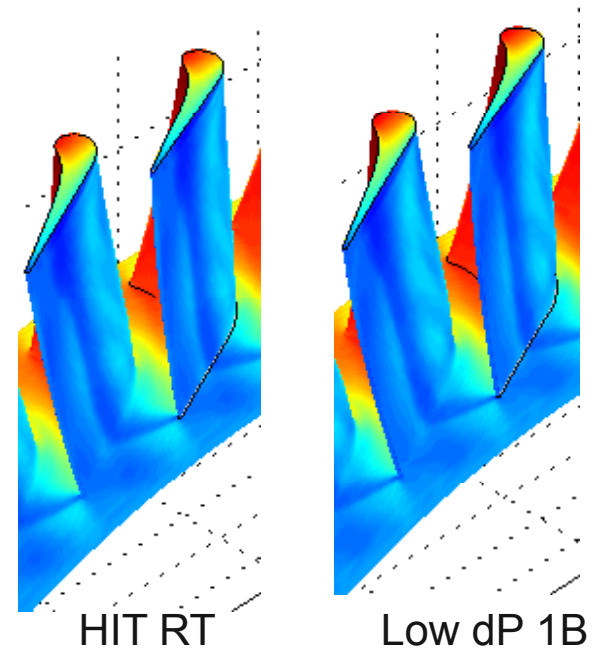
HIT RT Blade was Re-Designed in an Attempt to Reduce Levels of Unsteadiness at 46E



Iteration	1	3
TED	0.0450	0.0431
TEW	5.1562	3.3191
TEWF	0.4516	0.5951
uncvrtrn	0.0440	-2.0191
L3F	0.4706	0.5080
L3R	0.1506	0.2373
L4	0.1000	0.1445

OK

- Design-space exploration was performed to equalize strengths of the double-shock pair.
- Peak-to-peak circumferential distortion in exit static pressure was reduced of order 25%.

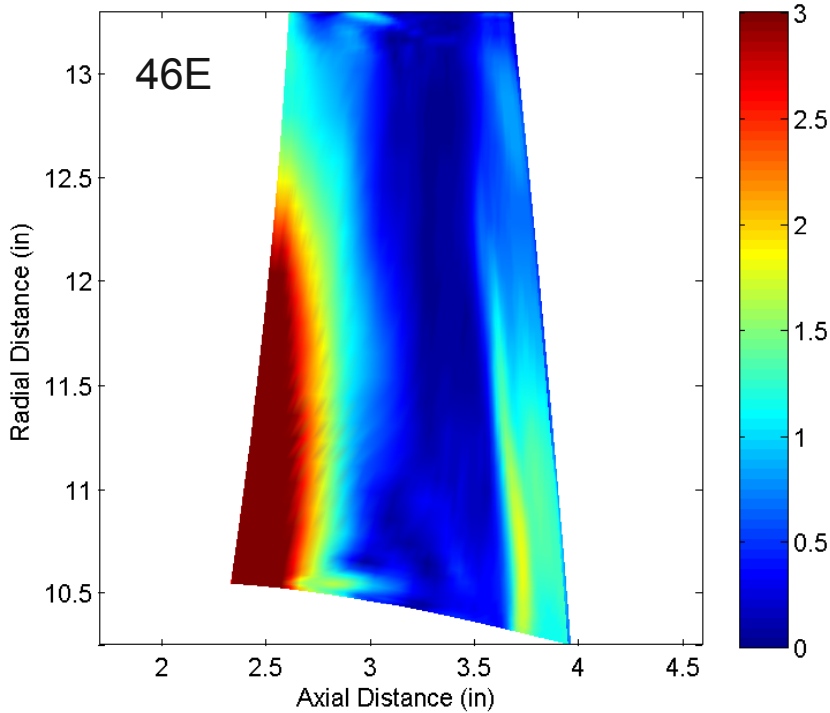




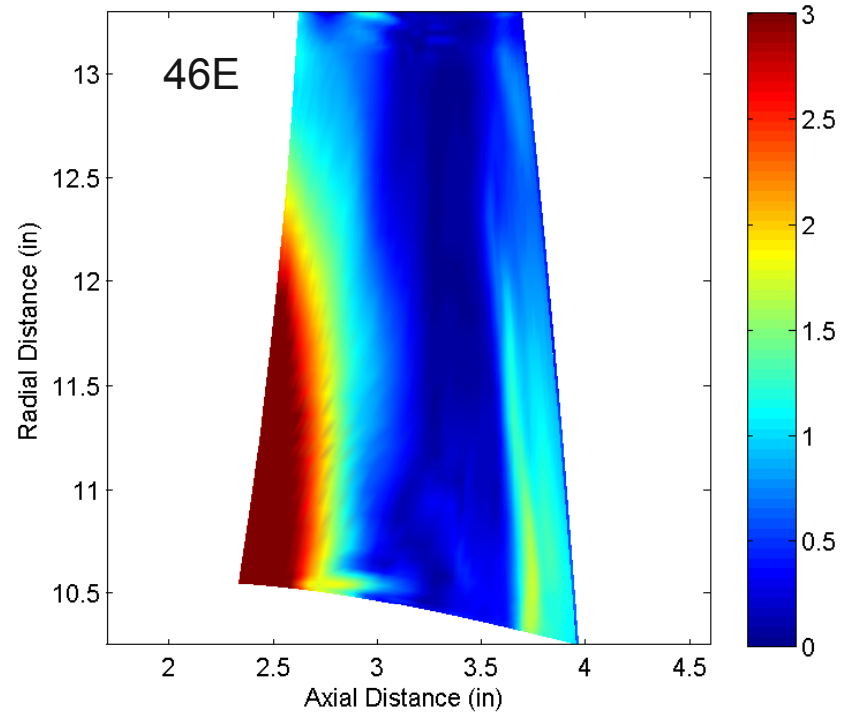
Small Decrease in 46E Unsteadiness Despite $\approx 25\%$ Reduction in Peak-to-Peak P_s Variation



1B Suction Side, DFT Magnitude, Percent $P_{t \text{ inlet}}$



HIT RT



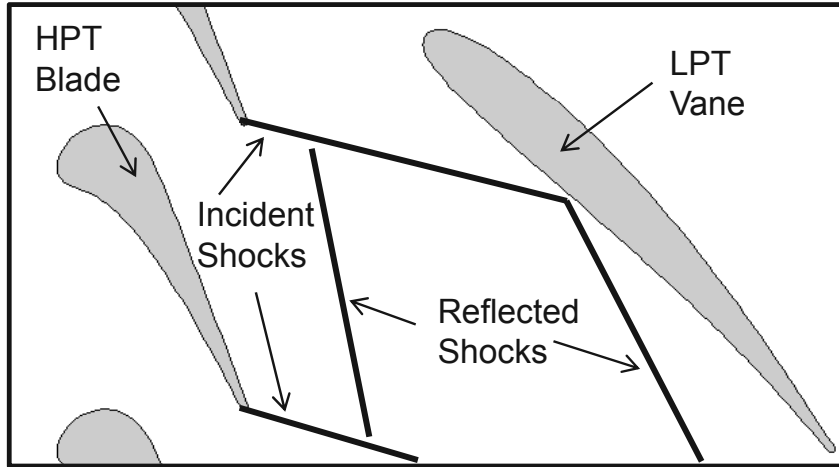
With Low dP 1B



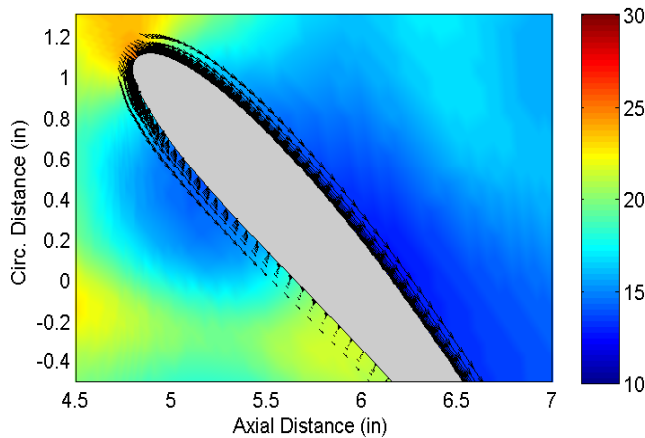
Additional Means to Reduce 1B-2V Interaction: Steady 2V Blowing and 3D Vane Shaping



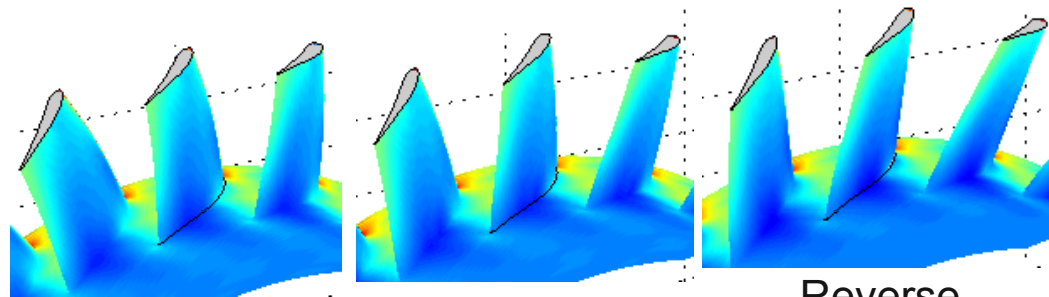
Present Situation



- 2V geometry leads to shock reflections for vaned contra-rotating turbines.
- These arise because induced-flow components due to moving shocks must be cancelled at no-slip surfaces.
- Injection of a small amount of flow equal and opposite the induced velocity should reduce the strength of reflected shocks.
- Bowing of the 2V should affect unsteadiness levels on the 1B surface.



2V With Blowing



Bowed 2V

HIT RT 2V

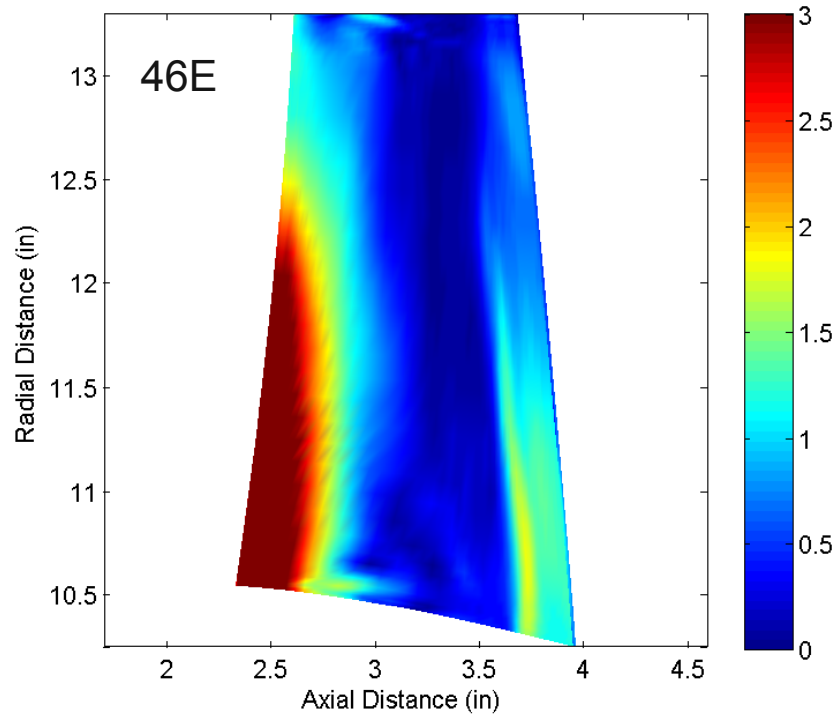
Reverse-Bowed 2V



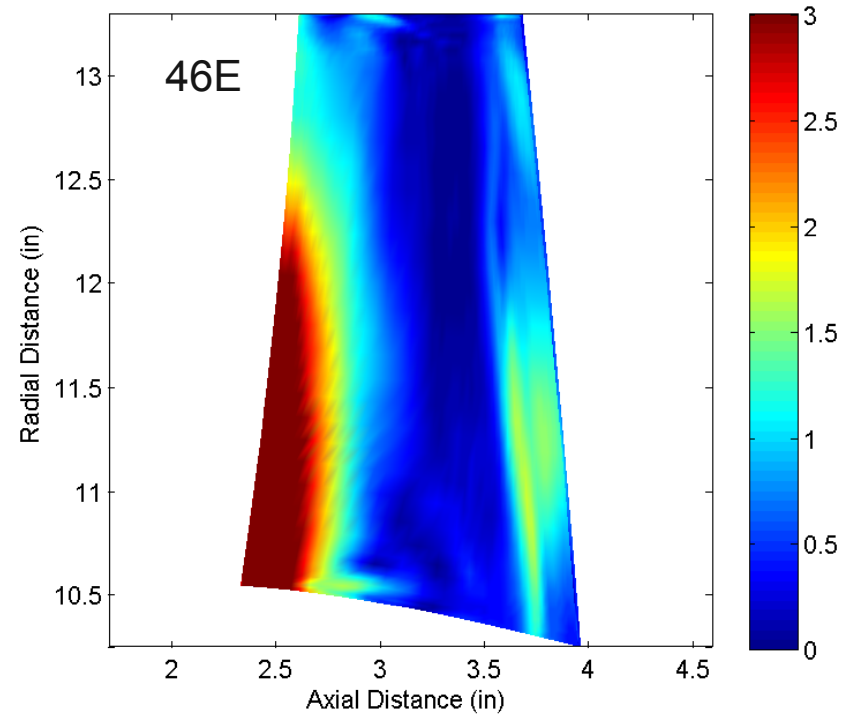
Reverse-Bowed 2V Leads to a Significant Change in Distribution of 46E Unsteadiness



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



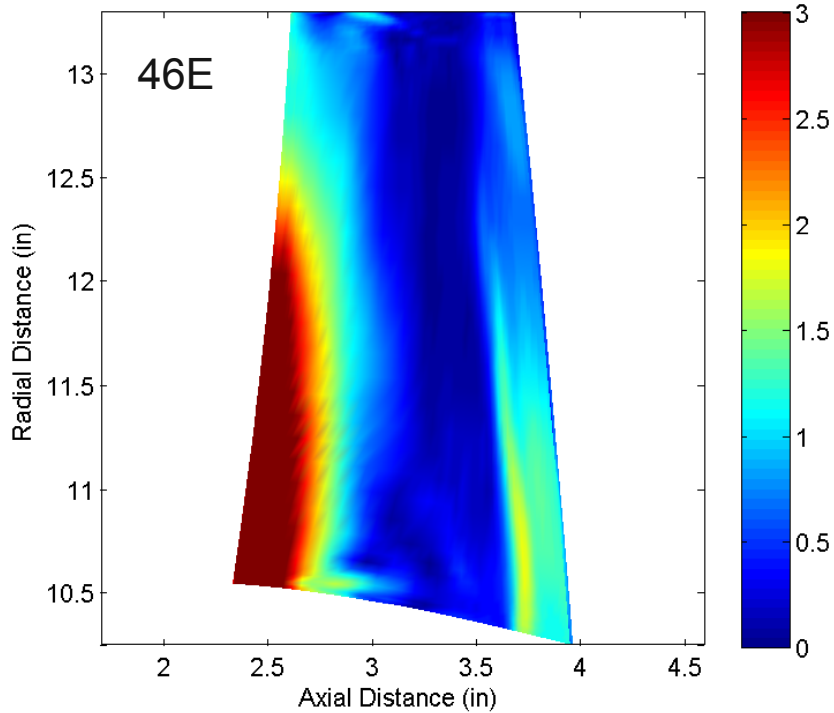
Reverse-Bowed 2V



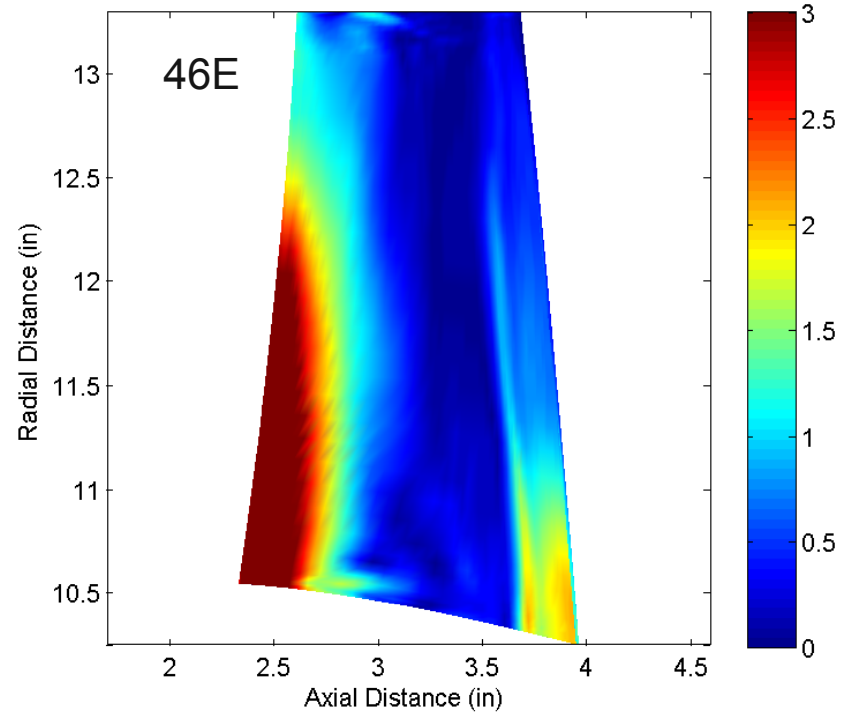
Bowed 2V Also Leads to a Significant Change in Distribution of 46E Unsteadiness



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



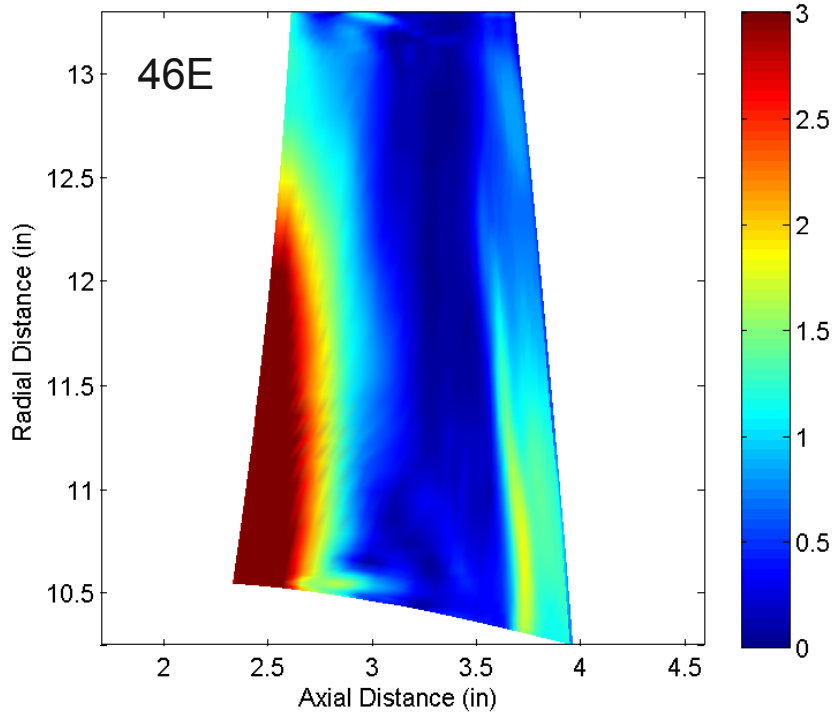
Bowed 2V



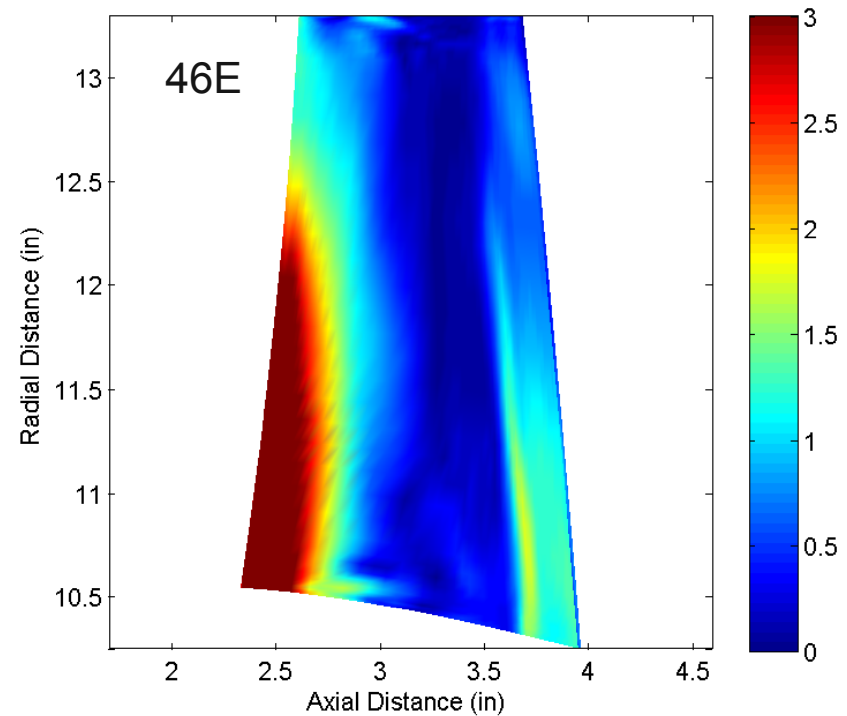
Small Decrease in 46E Unsteadiness Due to Steady Blowing on 2V Pressure Side



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



With Steady 2V Blowing

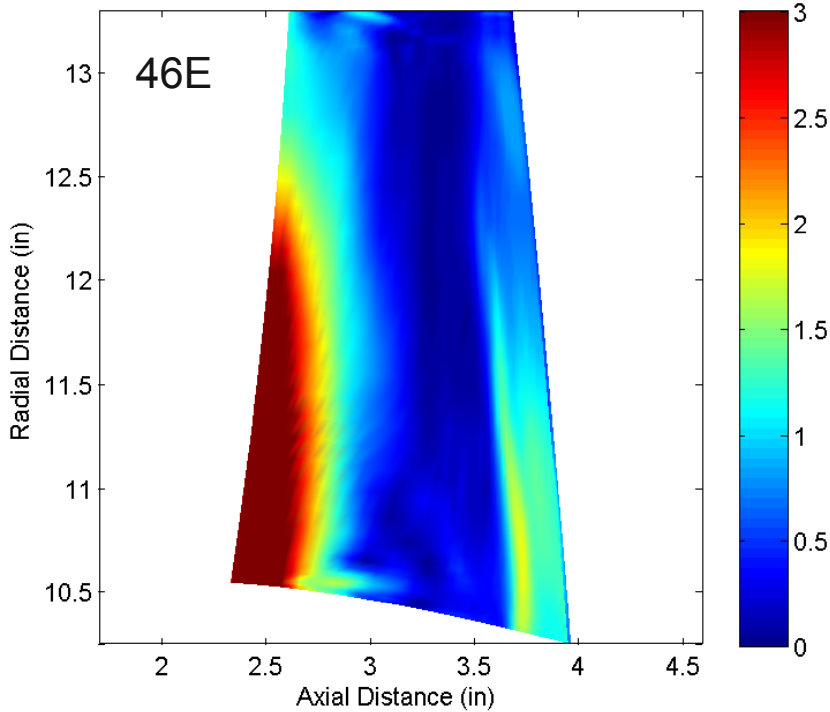
1113 holes, $Pt_{cool} = 28$ psia, 0.8% Flow, $\alpha = 90^\circ$



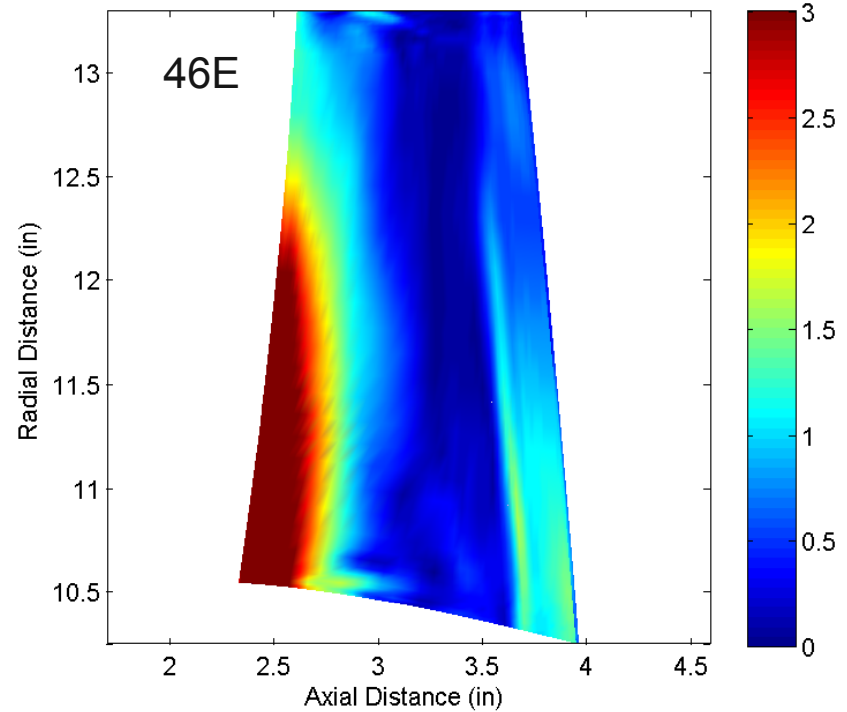
Reduction in 46E Unsteadiness Increases with Increasing Mass Flow



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



With Steady 2V Blowing

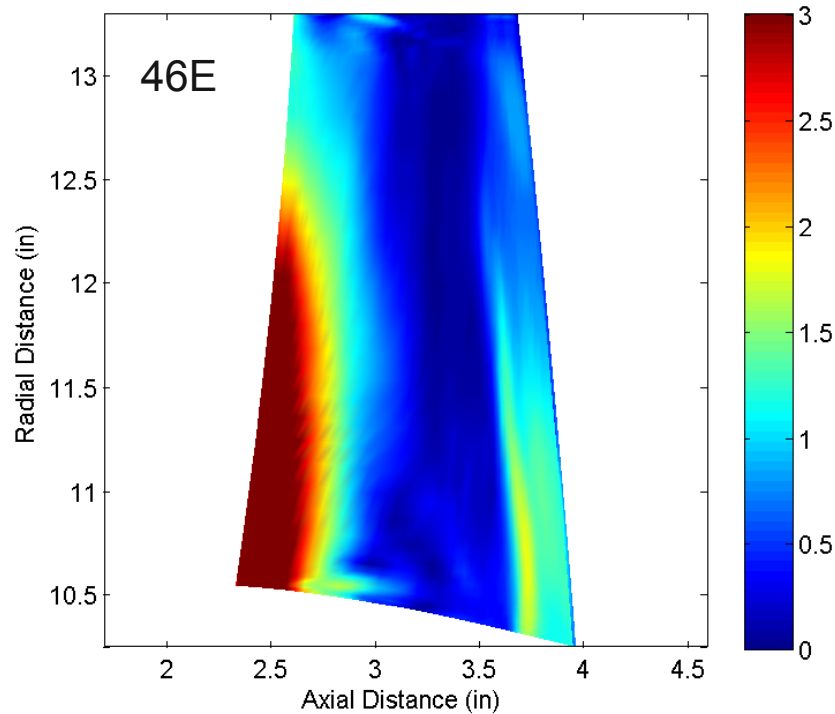
1113 holes, $Pt_{cool} = 28$ psia, 1.7% Flow, $\alpha = 90^\circ$



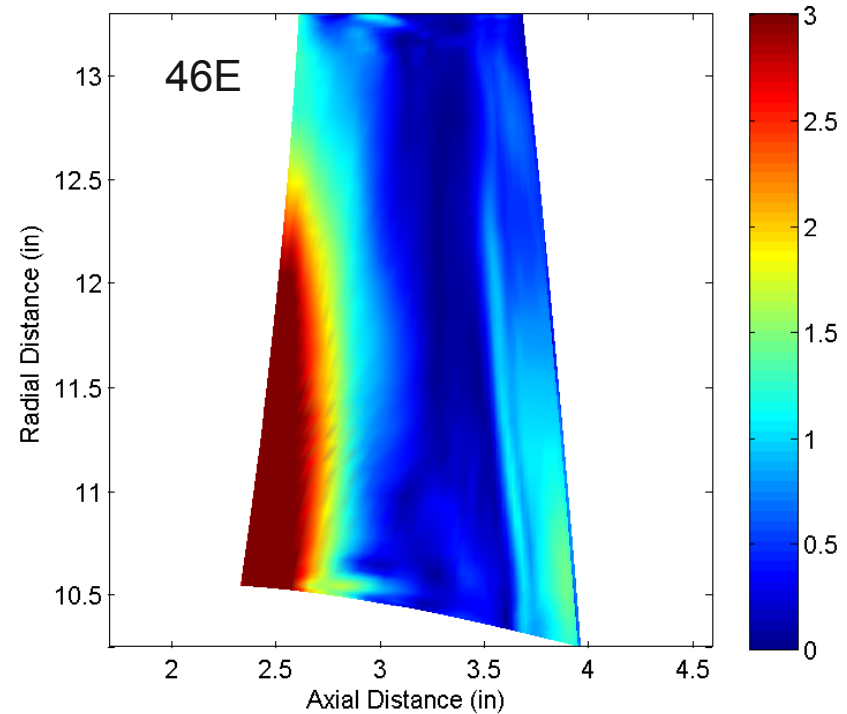
Reduction in 46E Unsteadiness Increases with Increasing Mass Flow



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



With Steady 2V Blowing

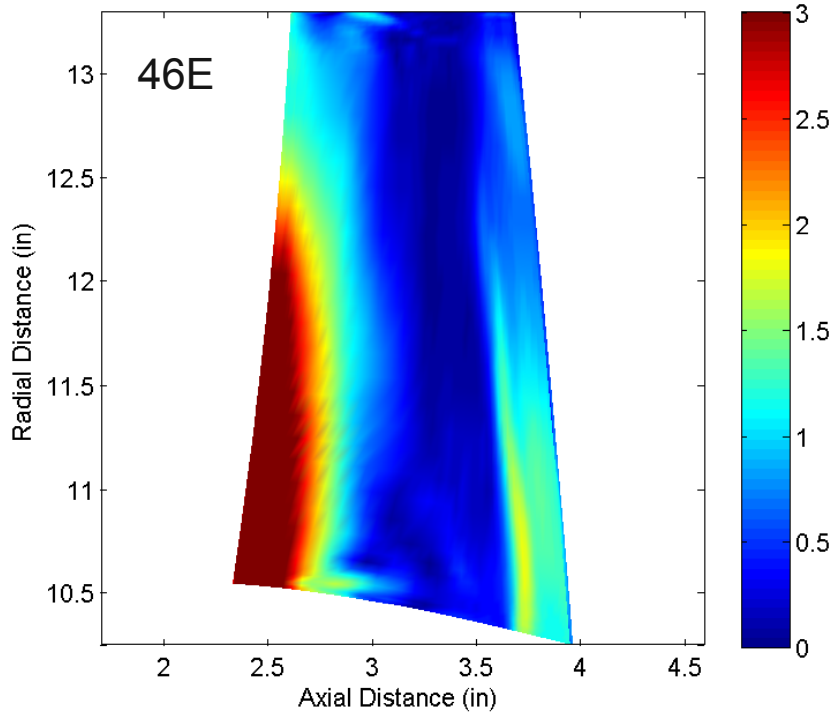
450 holes, $Pt_{cool} = 28$ psia, 2.8% Flow, $\alpha = 90^\circ$



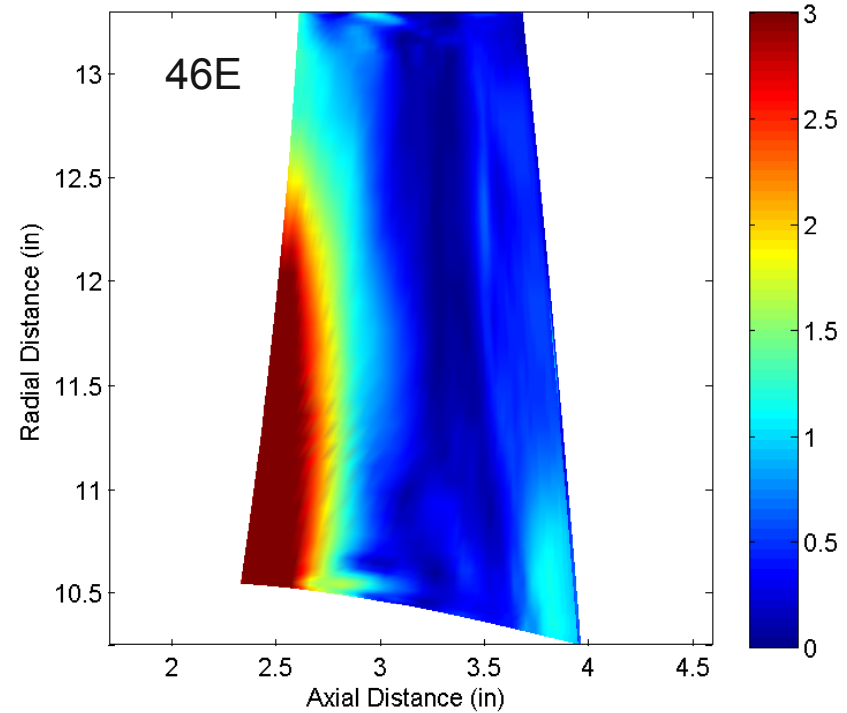
Reduction in 46E Unsteadiness Increases with Increasing Mass Flow



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT



With Steady 2V Blowing

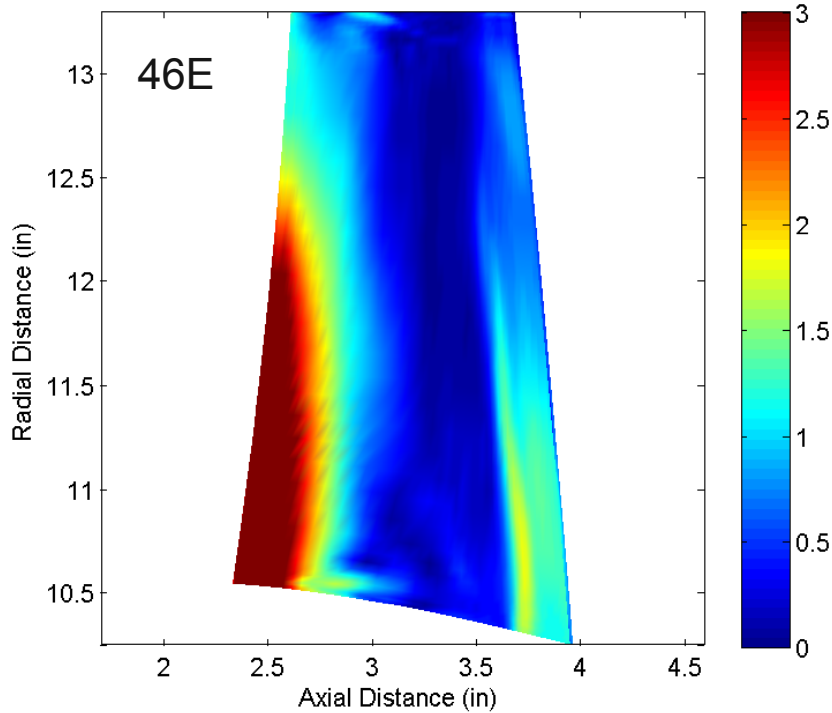
1113 holes, $Pt_{cool} = 28$ psia, 6.8% Flow, $\alpha = 90^\circ$



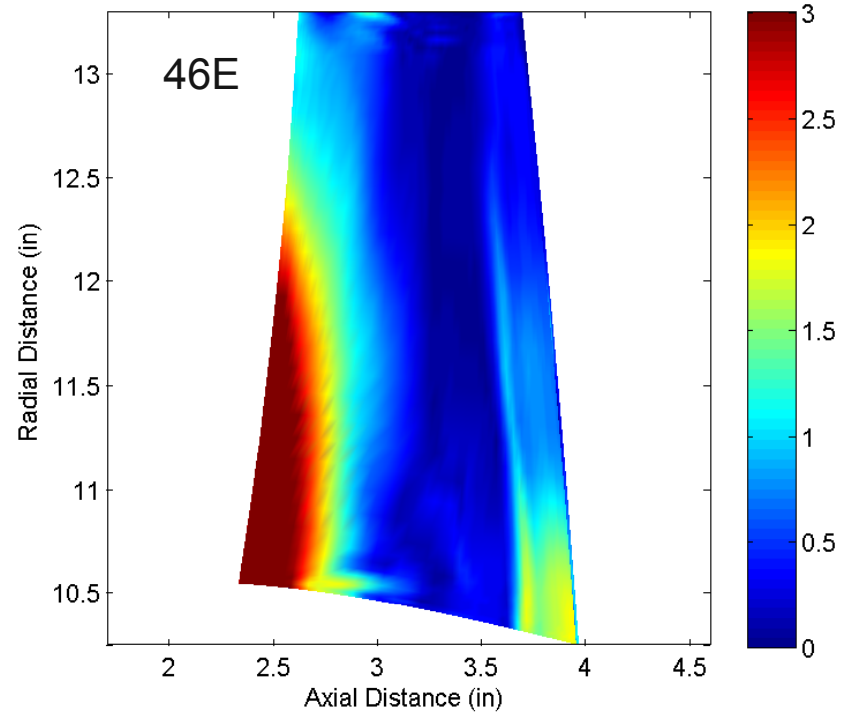
A Combination of 2V Pressure-Side Blowing and 2V Bow Looks Promising



1B Suction Side, DFT Magnitude, Percent Pt_{inlet}



HIT RT

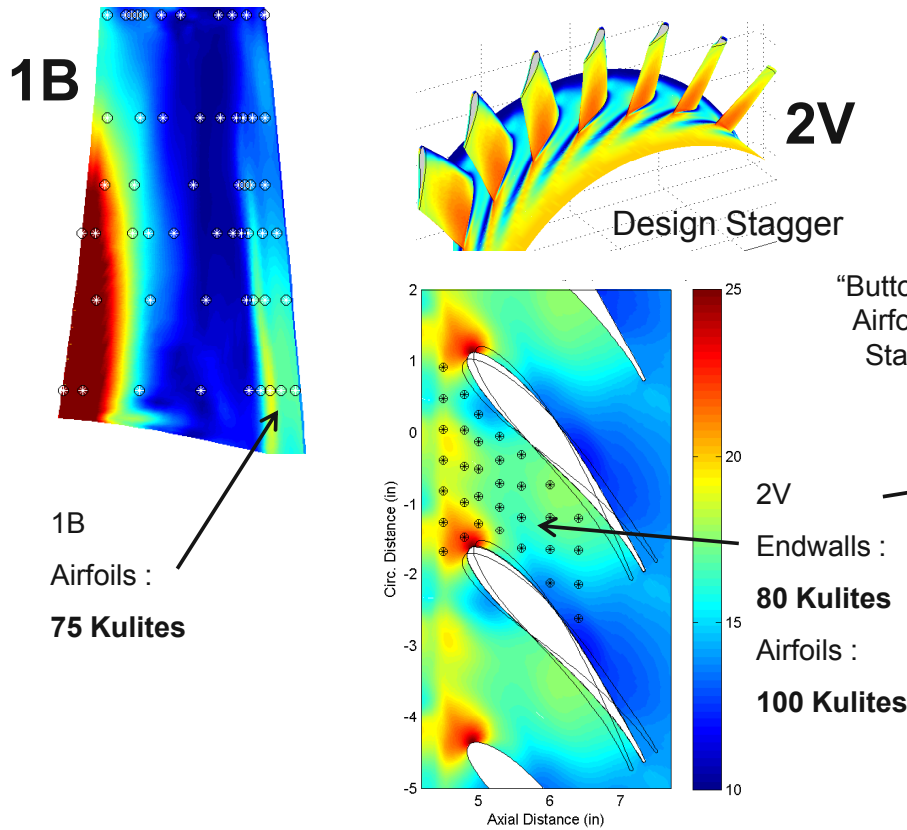


With Steady 2V Blowing and Bowed 2V

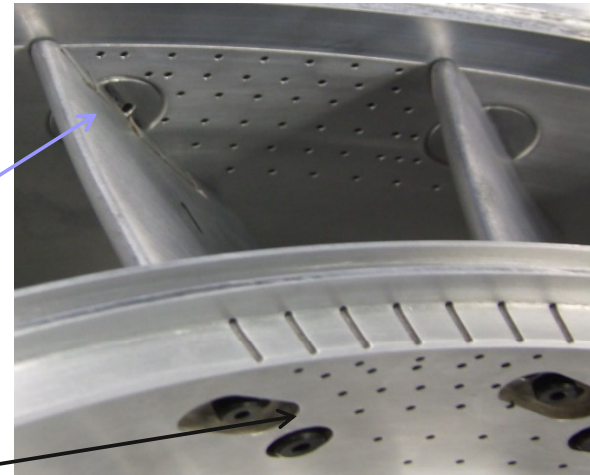
1113 holes, $Pt_{cool} = 28$ psia, 1.7% Flow, $\alpha = 90^\circ$



HIT RT is Intended to Assess 1B-2V Unsteady Interaction in Great Detail



"Buttons" for Airfoil Re-Stagger



Full-Scale Testing in Turbine Research Facility, Spring 2010

- Variable Stagger 2V ($\pm 10\%$ A45 variation)
 - Also enables the investigation of vane asymmetry and re-stagger to reduce unsteady loading
- Vane-row clocking to affect phase of unsteadiness



Summary



- HPT blade unsteadiness in the presence of a downstream vane consistent with contra-rotation is characterized by strong interaction at the first harmonic of downstream vane passing.
- An existing stage-and-one-half transonic turbine rig design was used as a baseline to investigate means of reducing such a blade-vane interaction.
- Methods assessed included:
 - Aerodynamic shaping of HPT blades
 - 3D stacking of the downstream vane
 - Steady pressure-side blowing
- Of the methods assessed, a combination of vane bowing and steady pressure-side blowing produced the most favorable result.
- Transonic turbine experiments are planned to assess predictive accuracy for the baseline turbine and any design improvements.