

Convergence of defect-correction and multigrid iterations for inviscid flows

Boris Diskin*

James L. Thomas†

Convergence of multigrid and defect-correction iterations is comprehensively studied within different incompressible and compressible inviscid regimes on high-density grids. Good smoothing properties of the defect-correction relaxation have been shown using both a modified Fourier analysis and a more general idealized-coarse-grid analysis. Single-grid defect correction alone has some slowly converging iterations on grids of medium density. The convergence is especially slow for near-sonic flows and for very low compressible Mach numbers. Additionally, the fast asymptotic convergence seen on medium density grids deteriorates on high-density grids. Certain downstream-boundary modes are very slowly damped on high-density grids. Multigrid scheme accelerates convergence of the slow defect-correction iterations to the extent determined by the coarse-grid correction. The two-level asymptotic convergence rates are stable and significantly below one in most of the regions but slow convergence is noted for near-sonic and very low-Mach compressible flows. Multigrid solver has been applied to the NACA 0012 airfoil and to different flow regimes, such as near-tangency and stagnation. Certain convergence difficulties have been encountered within stagnation regions. Nonetheless, for the airfoil flow, with a sharp trailing-edge, residuals were fast converging for a subcritical flow on a sequence of grids. For supercritical flow, residuals converged slower on some intermediate grids than on the finest grid or the two coarsest grids.

I. Introduction

Defect correction (DC) is currently a cornerstone approach for solving the Euler and Navier-Stokes equations. Second-order finite-volume discretizations (FVD) require large-stencil linearizations, making direct iterations expensive. Also, linearizations of inviscid discretizations beyond first-order are highly non-positive and difficult to relax. On the other hand, upwind-biased first-order equations are more diagonally dominant and can be relaxed (solved) with conventional approaches. Thus, DC is widely used for second-order solutions,¹ either directly by solving a series of first-order equations with modified residuals or indirectly by using the first-order operator to relax or precondition the second-order equations. The concept is also being applied in p -multigrid methods to solve higher-order discretizations.

Usually, DC is cited as being slow to converge the second-order residuals but fast to converge quantities of engineering interest, such as lift and drag.¹⁻³ On the other hand, DC has been used to solve large-scale turbulent application problems for many years⁴⁻⁶ and relatively fast asymptotic convergence of residuals has been observed in many instances. A hierarchical full-approximation scheme (FAS) multigrid method^{6,7} with a DC-based relaxation scheme, herein referred to as MG-DC, was previously developed and applied in two dimensions, demonstrating fast convergence of residuals for airfoils at compressible and incompressible conditions.

Analysis of DC convergence for two-dimensional (2D) convection has been previously performed in a semi-discrete setting^{6,8} in which boundary conditions in one direction are taken into account. A two-level multigrid analysis⁶ showed that although the number of cycles to attain convergence was dependent on the mesh density, the dependence was reasonably small and fast asymptotic convergence was eventually attained. A more detailed study of DC alone⁸ showed that an asymptotic convergence of about 0.5 per DC iteration is observed in computations. Slow convergent DC iterations may be encountered for nonaligned flows before attaining the asymptotic rate; the number of slow iterations slightly grows on finer grids as $h^{-1/3}$, where h is a characteristic mesh size. This h dependence can be observed for three-dimensional flows as well.

With the current trend of performing complex computations on increasingly larger scales, it is critically important to (re)evaluate performance of traditional algorithms on grids of high density. Analysis of convergence on such grids

*National Institute of Aerospace (NIA), 100 Exploration Way, Hampton, VA 23681, USA, Senior Member AIAA, bdiskin@nianet.org. Also Department of Mechanical and Aerospace Engineering, University of Virginia, Charlottesville, VA 22904, USA. This work is supported by NASA Fundamental Aeronautics Program, Supersonics Project, NRA Contract NNL07AA23C (PI: Prof. N. K. Yamaleev)

†Computational AeroSciences Branch, NASA Langley Research Center, Mail Stop 128, Fellow AIAA, James.L.Thomas@nasa.gov. This work is funded by NASA Fundamental Aeronautics Program, Subsonic Fixed Wing Project

has been conducted in this paper. Some surprising results have been obtained regarding the DC asymptotic rate. Specifically, the asymptotic convergence on typical computational grids is significantly different from the asymptotic convergence on high-density grids. The asymptotic rates are essentially invariant for several refined grids of medium density, but the convergence rates slow significantly with progressive grid refinement. The asymptotic slowdown on high-density grids was found first for the Euler system of equations, but was found to occur even for the convection equation alone. The previous results for asymptotic convergence of DC iterations are revisited in the light of these new findings.

The purpose of this paper is to analyze convergence of iterative solvers for inviscid flows, ranging from incompressible to supersonic Mach numbers, to complement the methodology developed previously for diffusion.^{9,10} The convergence of the MG-DC algorithm is comprehensively studied within different incompressible and compressible regimes on structured grids of progressively high density. The approach is to first assess the convergence away from any boundaries and discontinuities that may exist and this assessment can be performed using the framework of a small-perturbation (SP) flow. With acceptable and quantified performance within this regime, a solid foundation is established for assessing convergence for the general 2D inviscid flow. The entire flow field around an airfoil, for instance, has at least six distinct regions (regimes): (1) flow away from the boundaries and discontinuities; (2) flow near tangency boundaries away from stagnation; (3) flow within the leading-edge (LE) stagnation flow; (4) flow within the trailing-edge (TE) stagnation flow; (5) flow near discontinuities, e.g., shocks; and (6) flow near the far boundary. Each of these flow regimes may introduce difficulties in the multigrid and each should be studied individually, both analytically and computationally.

Several analysis tools are used to characterize performance of the MG-DC scheme. For SP flows, a constant-coefficient approximation is analyzed with the local mode Fourier (LMF) analysis and a semi-discrete (SD) analysis. General quantitative analysis tools^{10,11} idealized coarse-grid (ICG) and idealized relaxation (IR), are applied in actual flow computations for assessing multigrid relaxation and coarse-grid correction. The analytical results, confirmed with actual computations, indicate that asymptotic MG-DC convergence rates are stable and well separated from one and are limited on high-density grids by the quality of the coarse-grid correction. The convergence of MG-DC iterations is significantly better than convergence observed in DC iterations alone because multigrid accelerates convergence of slow DC iterations, especially for near-sonic flows and low-Mach compressible flows.

The material in the paper is presented in the following order. Components of the multigrid and defect correction scheme are presented in Section II. Analysis tools are introduced in Section III. Section IV describes the first-order solver that serves as a driver of the DC iterations. An analysis of DC and MG-DC iterations for SP flows is presented in Section V. Numerical tests and IR/ICG analysis of flows in other regimes are presented in Section VI. The results are discussed in Section VII. Details of the analysis methods used in this paper are provided in Appendices A and B. Asymptotic convergence rates of constant coefficient convection equation on high-density grids are discussed in Appendix C. For reference, Table 1 includes all acronyms used in the paper.

II. Components of MG-DC solver

The conservation form of the 2D steady inviscid flow equations is given as

$$\mathbf{R}(\mathbf{Q}) = 0. \quad (1)$$

Here, the conserved variables for compressible flows are $\mathbf{Q} \equiv (\rho u, \rho v, \rho w, \rho, \rho E)^T$, representing the momentum vector, density, and total energy per unit volume, and $\mathbf{R}(\mathbf{Q})$ is a spatial divergence of convective fluxes

$$\mathbf{R}(\mathbf{Q}) \equiv \partial_x \mathbf{F}(\mathbf{Q}) + \partial_y \mathbf{G}(\mathbf{Q}), \quad (2)$$

$$\mathbf{F}(\mathbf{Q}) = \begin{pmatrix} \rho u^2 + p \\ \rho uv \\ \rho u \\ \rho uE + up \end{pmatrix}, \quad \mathbf{G}(\mathbf{Q}) = \begin{pmatrix} \rho uv \\ \rho v^2 + p \\ \rho v \\ \rho vE + vp \end{pmatrix}.$$

The primitive flow variables are velocity, pressure, and density, $\mathbf{q} = (u, v, p, \rho)^T$. Eq. (1) is discretized with a second-order, cell-centered, upwind-biased FVD scheme that employs an approximate Riemann solver to compute fluxes at the control volume faces. The baseline Riemann solver is the flux-difference-splitting (FDS) scheme¹² but other schemes are also considered, including the low-dissipation flux-splitting (LDFS)^{13,14} and flux-vector-splitting (FVS).¹⁵ Either

Acronym	Description
Alternating Line-Colored (ALC)	A relaxation method
Courant-Friedrichs-Lewy (CFL) number	An iterative parameter characterizing the ratio of (pseudo) time increment to mesh spacing
Correction Scheme (CS)	A MG scheme that uses linear approximations on coarse grids
damped Alternating Line-Jacobi (dALJ)	A relaxation method
Defect Correction (DC)	Used for single-grid iterations and as relaxation in multigrid
Flux Difference Splitting (FDS)	A less-dissipative approximate Riemann solver
Flux Vector Splitting (FVS)	A more-dissipative approximate Riemann solver
Full-Approximation Scheme (FAS)	A MG scheme that uses non-linear approximations on coarse grids
Full-Multigrid (FMG)	A MG scheme that uses coarser-grid solutions to form finer-grid initial approximations
Finite-Volume Discretization (FVD)	The discretization approach used in this paper
Idealized Coarse Grid (ICG)	General quantitative method for analysis of multigrid relaxation
Idealized Relaxation (IR)	General quantitative method for analysis of coarse-grid correction
Leading Edge (LE)	Designate the leading-edge stagnation area
Low-Dissipation Flux-Splitting (LDFS)	A more-dissipative approximate Riemann solver
Local-Mode Fourier (LMF)	A constant-coefficient analysis for interior of the domain, assumes periodicity in all directions
Multigrid (MG)	A hierarchical computational method
MG-DC	Multigrid method studied in this paper that uses defect-correction based relaxation
Semi-discrete (SD)	A constant-coefficient analysis taking boundary conditions into account, assumes periodicity in the directions tangential to the boundary
Small Perturbation (SP)	Computational model that assumes small deviation from a known (e.g., free-stream) solution
Trailing Edge (TE)	Designate the trailing-edge stagnation area

Table 1. Acronyms used in this paper.

of these latter schemes are generally known to be more dissipative than the FDS scheme. The discrete approximations to derivatives correspond to the Fromm discretization for structured grids used herein.

The same approach is used for incompressible flows with small variations. The variables are $\mathbf{Q} = (u, v, p)^T$ and the fluxes are defined as in Eq. (2), except the density is constant and the fourth (energy) equation is dropped. The incompressible version of the FDS scheme⁴ is used.

In a DC relaxation, a correction, $\delta\mathbf{Q}^h$, to the approximate solution, \mathbf{Q}^h , is computed from the driver equation

$$\mathbf{D}\delta\mathbf{Q}^h = -\mathbf{R}(\mathbf{Q}^h), \quad (3)$$

where \mathbf{D} is the Jacobian of the first-order upwind discretization, and \mathbf{R} is the discretized residual Eq. (1). For DC

relaxation within an outer FAS multigrid cycle, a correction scheme (CS) multigrid is applied to determine $\delta \mathbf{Q}^h$. One CS cycle generally reduces the residual of Eq. (3) by an order of magnitude (see Section IV). For DC iterations, Eq. (3) is solved to high precision. Where practical, e.g., for the SD analysis or a scalar convection equation, Eq. (3) is solved precisely, otherwise multiple multigrid cycles are used.

After DC relaxation, the solution of the target FVD scheme is updated as

$$\mathbf{Q}^h = \mathbf{Q}^h + \delta \mathbf{Q}^h. \quad (4)$$

For the MG-DC solver, FAS multigrid is used to accelerate convergence. An $FAS(\nu_1, \nu_2)$ multigrid cycle starts on the target finest grid, performs ν_1 relaxations on the current grid, restricts solutions and residuals to the coarser grid, solves the coarse-grid problem recursively, prolongs the coarse-grid correction, and completes with additional ν_2 relaxations. Each coarse grid is obtained by full coarsening from the finer grid. The same FVD scheme is used on all grids and W cycles are used. For SD computations, the restriction operator is full weighting, and the prolongation operator is the normalized transposition to the restriction. For fully discrete computations, the restriction operator is the conservative residual restriction and prolongation corresponds to linear interpolation. Full multigrid (FMG) requires a high-order prolongation for full efficiency. In the current FMG solver, the FMG prolongation is the same as within the FAS cycle.

III. Analysis tools

In recent years, a number of powerful methods have been developed to analyze convergence of iterative solvers. For problems well described in terms of small perturbations, e.g., SP flows, analysis of a constant coefficient approximation allows one to estimate various convergence characteristics, such as stability, asymptotic and maximum convergence rate, number of slow iterations, etc. For more general problems, windowing and downscaling techniques¹⁶ can be used to analyze accuracy and grid convergence of discrete solutions. Quantitative analysis methods, IR(ν_1, ν_2) and ICG(ν_1, ν_2),^{10,11} have proved to be invaluable for assessing components of multigrid solvers for general problems. Here, parameters ν_1 and ν_2 denote the respective numbers of fine-grid relaxations performed before and after coarse-grid correction.

III.A. Analysis of constant coefficient equations on regular grids

A constant coefficient linearization to the FVD schemes used here on Cartesian grids is given by

$$\mathbf{A}^+ \partial_x^- w^h + \mathbf{A}^- \partial_x^+ w^h + \mathbf{B}^+ \partial_y^- w^h + \mathbf{B}^- \partial_y^+ w^h = 0, \quad (5)$$

where w^h is a discrete solution vector. For compressible flow, the variables are taken following Mulder¹⁷ as $w^h = (\delta u, \delta v, \delta p/(\rho c), \delta S)^T$, c is the speed of sound, and $S = \log(p/\rho^\gamma)$ is the specific entropy. For incompressible flow, $w^h = (\delta u, \delta v, \delta p)^T$. The operators, ∂_x^- and ∂_y^- are upwind discretizations of derivatives, and ∂_x^+ and ∂_y^+ are downwind discretizations of derivatives.

Different linearizations are associated with each splitting scheme. For the baseline FDS scheme, the linearizations are eigenvalue splittings of the Jacobian matrices associated with non-conservative formulations,

$$\mathbf{A} = \mathbf{A}^+ + \mathbf{A}^-, \quad \mathbf{B} = \mathbf{B}^+ + \mathbf{B}^-,$$

where

$$\mathbf{A} = \begin{pmatrix} u & 0 & c & 0 \\ 0 & u & 0 & 0 \\ c & 0 & u & 0 \\ 0 & 0 & 0 & u \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} v & 0 & 0 & 0 \\ 0 & v & c & 0 \\ 0 & c & v & 0 \\ 0 & 0 & 0 & v \end{pmatrix},$$

The speed of sound is taken as $c = 1$ and the velocities are defined as $u = M \cos(\alpha)$, $v = M \sin(\alpha)$, where M is Mach number and α is the angle of attack.

For subsonic regimes,

$$\mathbf{A}^+ = \begin{pmatrix} (u+c)/2 & 0 & (u+c)/2 & 0 \\ 0 & u & 0 & 0 \\ (u+c)/2 & 0 & (u+c)/2 & 0 \\ 0 & 0 & 0 & u \end{pmatrix}, \quad \mathbf{A}^- = \begin{pmatrix} (u-c)/2 & 0 & -(u-c)/2 & 0 \\ 0 & 0 & 0 & 0 \\ -(u-c)/2 & 0 & (u-c)/2 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix},$$

$$\mathbf{B}^+ = \begin{pmatrix} v & 0 & 0 & 0 \\ 0 & (v+c)/2 & (v+c)/2 & 0 \\ 0 & (v+c)/2 & (v+c)/2 & 0 \\ 0 & 0 & 0 & v \end{pmatrix}, \quad \mathbf{B}^- = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & (v-c)/2 & -(v-c)/2 & 0 \\ 0 & -(v-c)/2 & (v-c)/2 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

For supersonic regimes,

$$\mathbf{A}^+ = \mathbf{A}; \mathbf{A}^- = 0; \mathbf{B}^+ = \mathbf{B}; \mathbf{B}^- = 0.$$

The discretization is defined as

$$\mathbf{A}^+ \partial_x^- w^h + \mathbf{A}^- \partial_x^+ w^h + \mathbf{B}^+ \partial_y^- w^h + \mathbf{B}^- \partial_y^+ w^h = 0.$$

In the LMF analysis, the iterations are considered on a periodic domain for discrete Fourier components $w^h = \exp(i(\theta_x i_x + \theta_y i_y))$, where i_x and i_y are integer grid indexes. The Fourier frequencies are normalized: $|\theta_x| \leq \pi, |\theta_y| \leq \pi$. The outcome of the Fourier analysis is an iteration symbol, which is a 4×4 matrix with complex coefficients parametrized by the Fourier frequencies. The specific grid size is reflected through the range of Fourier frequencies realizable on the given periodic grid. For elliptic equations, the maximum spectral radius of the LMF-symbol matrix, taken over all realizable frequencies, is an accurate indicator of the asymptotic convergence rates. For non-elliptic equations, the spectral radius of the LMF symbol is not a sharp estimate for the asymptotic convergence rate on grids of moderate sizes because the LMF analysis accounts only for local error damping, but does not account for boundary effects and error propagation along the characteristics. Note, however, that LMF analysis provides a useful stability test. A larger-than-one LMF spectral radius is an indication of unstable iterations.

For multigrid computations, the relaxation smoothing rate is an important characteristic. The smoothing rate is estimated as the maximum spectral radius of the LMF relaxation symbol, where the maximum is taken over high frequency modes. Typically, high-frequency modes are defined as the modes with $\max(|\theta_x|, |\theta_y|) \geq \frac{\pi}{2}$; all other modes are considered smooth. A more general approach is to define the high-frequency modes as the modes that have relatively large contributions to the residual.¹⁹ An implication of this definition for non-elliptic problems is that the typical set of high-frequencies is reduced: the modes that are smooth in the characteristic directions are excluded, even if their Cartesian frequencies are high. For illustration, for the convection flow at 45° discretized on a uniform Cartesian grid, the mode $\exp(i(\theta_x i_x + \theta_y i_y))$ with $\theta_x \approx \pi$ and $\theta_y \approx -\pi$ is not a high-frequency mode because $\theta_x + \theta_y \approx 0$, and the mode is constant along the characteristic direction. With this modification for non-elliptic problems, the LMF analysis predictions of the smoothing rate are reasonably accurate. A more detailed description of the modified LMF smoothing analysis is provided in Appendix A.

The SD analysis is a good predictor of the asymptotic convergence for non-elliptic problems. The SD analysis assumes solutions in the form $w^h = \exp(i\theta_y i_y) W^h(i_x)$, i.e., the solution is a product of a Fourier component in the y -direction and a discrete function, $W^h(i_x)$, representing solution variations in the x -direction. The SD analysis is accounting for boundary effects and error propagation along the characteristics. For each y -directional Fourier frequency, the asymptotic rate is estimated as the spectral radius of the SD iteration matrix, which has a size proportional to the number of degrees of freedom in the x -direction. Another useful feature of the SD analysis is the capability to identify slow convergent iterations, characterize the error components causing the slow convergence, and explain the mechanism of transition from the slow intermediate convergence to good asymptotic convergence. A detailed description of the SD analysis is provided in Appendix B.

III.B. General quantitative analysis

More general, quantitative analysis methods for multigrid solutions are IR and ICG iterations. The iterations are designed to identify slow relaxation or inefficient coarse-grid correction of a multigrid solver. In these iterations, one part of the cycle (coarse-grid correction for IR iterations and relaxation for ICG iterations) is actual and its complementary part is replaced with an ideal imitation. The IR and ICG methods can be applied to any formulation with a manufactured solution; typically zero solution is used. The initial solution is chosen randomly. In IR iterations, the relaxation in the cycle is replaced with an explicit error averaging procedure. In the IR methods used for this paper, the error at a node is averaged from all the edge-connected neighbors. ICG cycles use actual relaxation scheme and emulate the coarse-grid correction by, first, averaging algebraic errors to the coarse grid and, then, interpolating the averaged error back to the fine grid as a correction. The results of this analysis are not single-number estimates; they are rather convergence patterns of the iterations that may either confirm or refute expectations indicating what part of the actual solver should be improved.

The IR and ICG iterations can be directly applied in the most complicated situations including highly variable (or nonlinear) coefficients, complex geometries, and unstructured grids. The generality of the analysis makes it a very valuable tool for analyzing complicated large-scale computational problems, where no other analysis methods are currently available. Properties and specific implementations of IR and ICG methods can be found elsewhere.^{10,11}

IV. First-order Euler solver

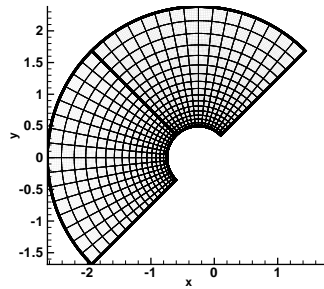


Figure 1. Combined stagnation and tangency grids.

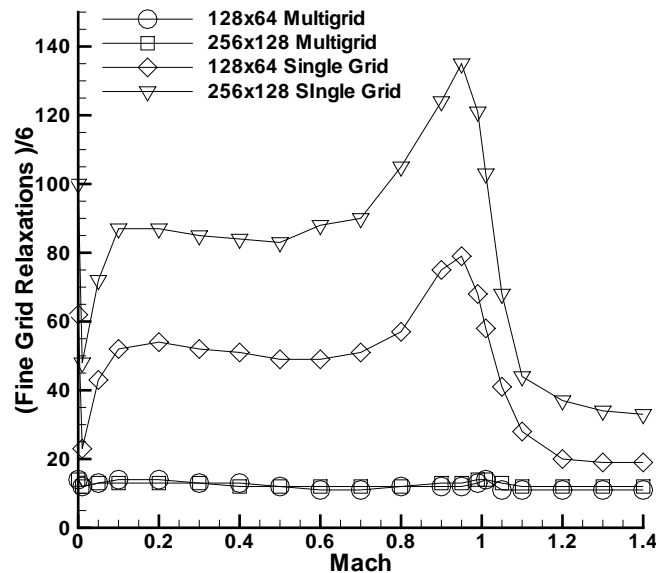


Figure 2. Number of iteration required to reach machine-zero residuals for the first-order solver.

Mulder^{2,17} developed efficient 2D multigrid solvers for the first-order upwind discretizations of the inviscid flow equations using both full-coarsening and semi-coarsening approaches. He analyzed many relaxation schemes using a 2-level LMF analysis and showed that the problem of alignment could be addressed uniformly with damped alternating-line-Jacobi (dALJ) relaxation within a full-coarsening framework or with point-implicit relaxation within a semi-coarsening framework. In this paper, full-coarsening is used with an alternating-line colored (ALC) relaxation. An under-relaxation factor, $\omega = 0.8$, is needed to effectively smooth high-frequency error.^{1,11} The performance of a two-color ALC relaxation is similar to performance of dALJ relaxation.

To illustrate the performance of iterative solvers, computations are performed on a domain around a cylinder. A typical grid is the union of the two cylindrical grids shown in Fig. 1, has local near-unity aspect ratios, and spans 180° of arc sector. Inflow/outflow boundary conditions are applied at all boundaries. The initial solution is a random

perturbation of the uniform free stream conditions.

Fig. 2 compares the number of fine-grid relaxations required to reach the machine-zero residual for single-grid ALC relaxations ($\omega = 1.0$) and $FAS(2, 1)$ multigrid W-cycles.¹ One ALC relaxation is counted as two relaxations and one W-cycle is counted as six relaxations. Results are shown for the FDS scheme on two grids for a range of Mach numbers and for incompressible flow ($M = 0$). The number of single-grid relaxations approximately doubles as the grid is refined by a factor of two in each direction, as expected. The required number of relaxations is highest at $M \approx 1$. The number of relaxations is lowest for the higher Mach numbers and, somewhat unexpectedly, for the least compressible Mach number of $M = 0.01$. The number of fine-grid relaxations observed within MG-DC solver to reach the same residual tolerance is relatively insensitive to variations of Mach number or grid size. Although not shown, the asymptotic convergence per cycle is between 0.2 and 0.4 for all Mach numbers on both grids.

V. Multigrid for small-perturbation flows

A previous study showed that, even when the asymptotic convergence rates of DC iterations are fast, a number of slow iterations precedes the asymptotic regime. The slow convergence occurs for smooth characteristic error components^{18,19} that are very smooth along the characteristic directions. Such components are removed mainly by accuracy propagation from boundaries along the characteristics. Such removal may take many iterations because a less-accurate driver propagates cross-characteristic oscillations for only short distances. Eventually, however, the smooth characteristic errors are removed and asymptotic convergence is attained.

In practical computations, the slow DC iterations may be overlooked on relatively coarse grids because the iterations may arrive to the required solution tolerance before the characteristic components begin to dominate the solution error. In order to observe this slowdown, one should carefully choose the initial solution approximation. On finer grids, this slowdown is a major factor limiting the solution efficiency.

Multigrid is expected to accelerate convergence of slow DC iterations. Note that full-coarsening multigrid has its own problems with characteristic components. The asymptotic convergence of the characteristic errors in a two level cycle can be as slow as 0.75 per cycle¹⁹ because cross-characteristic variations propagate shorter distances on coarser grids than on finer grids. The multigrid effects on asymptotic convergence rates are significant only in those flow regimes in which the asymptotic convergence of DC iterations is slower than the coarse-grid correction for characteristic error components. Such situations occur on fine grids.

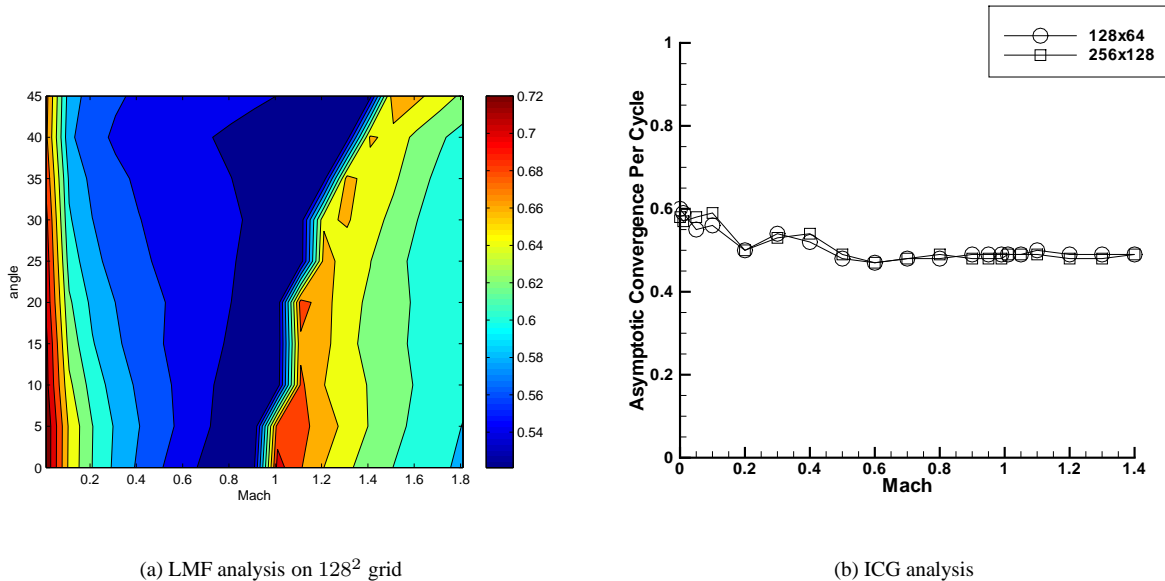


Figure 3. Smoothing rate of DC iterations.

For a subsequent use in MG-DC cycle, the smoothing rate of DC iterations is estimated with the LMF and ICG analysis. Fig. 3 shows the predicted smoothing rates. For all flow conditions (Mach numbers and angles of attack), the predicted smoothing rates are excellent and grid independent. The LMF predicts the smoothing rate of between 0.5 and 0.7, and the ICG predicts the rate between 0.5 and 0.6. The smoothing rates predicted by ICG are slightly

better than the rates predicted by the LMF analysis because ICG predicts the reduction of high-frequency errors in a multigrid cycle, while the LMF analysis predicts the reduction of high-frequency errors in a relaxation. In general, the LMF analysis can be modified to account for the coarse-grid effects on high frequencies.

The need and benefits of multigrid are illustrated in Fig. 4 by the SD analysis for SP flows. The flow conditions are $M = 0.3$, $\alpha = 45^\circ$, the y -directional frequency is smooth $\theta_y = \frac{5\pi}{64}$, and the initial distribution along the x -direction is random. While the asymptotic convergence for both DC and MG-DC iterations is about the same, around 0.6, the slowest convergence rate is significantly slower for DC than for MG-DC iterations.

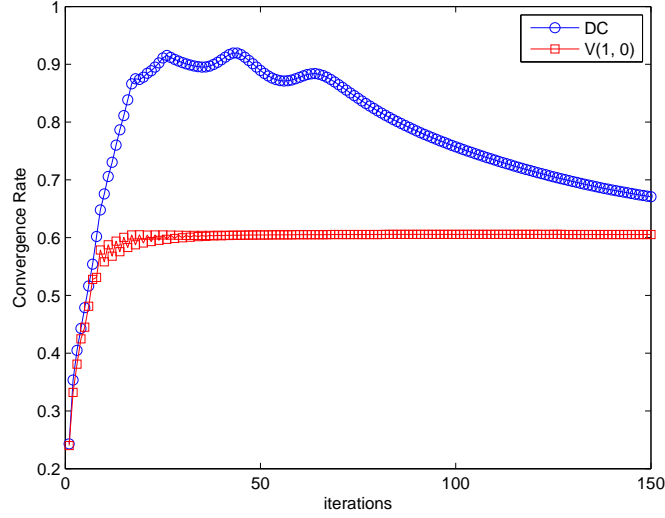


Figure 4. SD analysis: convergence of DC and MG-DC iterations on 256^2 grid, $M = 0.3$, $\alpha = 45^\circ$, and $\theta_y = \frac{5\pi}{64}$.

Fig. 5 shows the asymptotic rates of a two-grid $V(1,0)$ with DC relaxation. The rates are computed with the SD analysis on two coarse grids. The asymptotic rates of MG-DC iterations are stable and well below unity over most of the $M - \alpha$ range. The convergence is slow for near-sonic flows ($M \approx 1$) at intermediate angles of attack and for very low compressible Mach numbers.

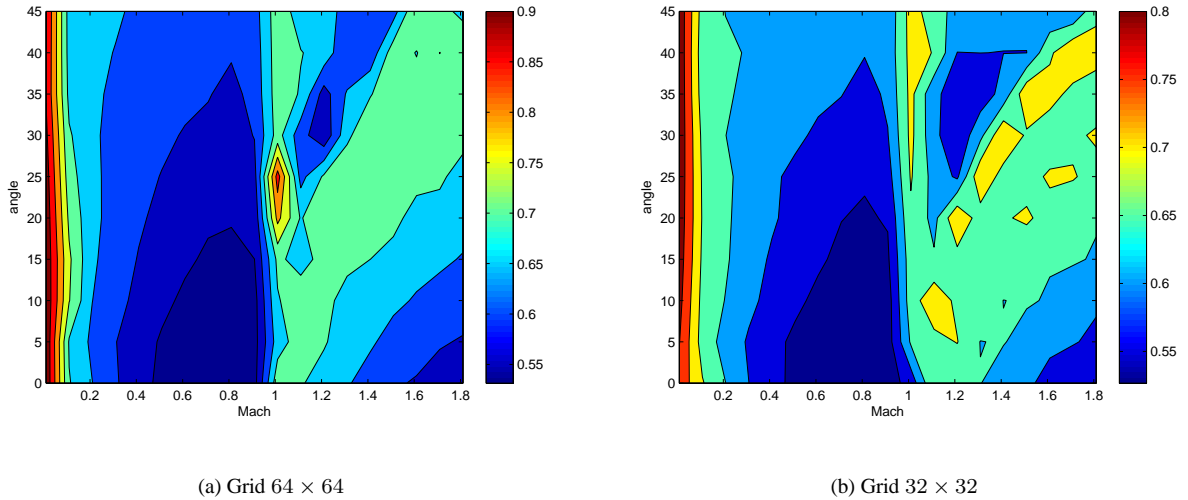


Figure 5. Asymptotic convergence of two-level $V(1,0)$ cycle computed with the SD analysis. The color bars are scaled by the slowest asymptotic convergence observed on the grid.

VI. Flows at other regimes

VI.A. Boundary-tangency and stagnation flows

A typical grid for computations of flows characterized by boundary-tangency and LE stagnation are shown in Fig. 1. Stagnation is computed on the most-forward part of the grid and boundary-tangency is computed on the upper-most part of the grid; each domain spans 90 deg of arc sector. A compressible-flow manufactured solution is composed of the velocities from the exact incompressible cylinder flow along with constant enthalpy and entropy. Medium-size grids are considered. The finest grid has 128 cells in both the circumferential and radial directions. Computations are shown for FAS(2,1) W-cycles using a maximum of six levels. Inflow/outflow conditions are applied at all boundaries away from the cylinder surface.

Flows characterized by boundary-tangency do not represent difficulties for the MG-DC solver. A typical convergence history for a series of grids is shown in Fig. 6 for $M = 0.3$, starting from a random perturbation to the exact solution on the left and from FMG interpolations on the right. Starting from random perturbations, the residuals converge rapidly in the first cycles, converge more slowly in intermediate cycles, and then asymptotically converge faster. Starting from FMG interpolations, the number of cycles needed are considerably smaller and machine-level zero residuals are encountered before the faster asymptotic rates are encountered. Although not shown, similar residual convergence per cycle is attained with ICG(1,0) and IR(2,1) multigrid cycles.

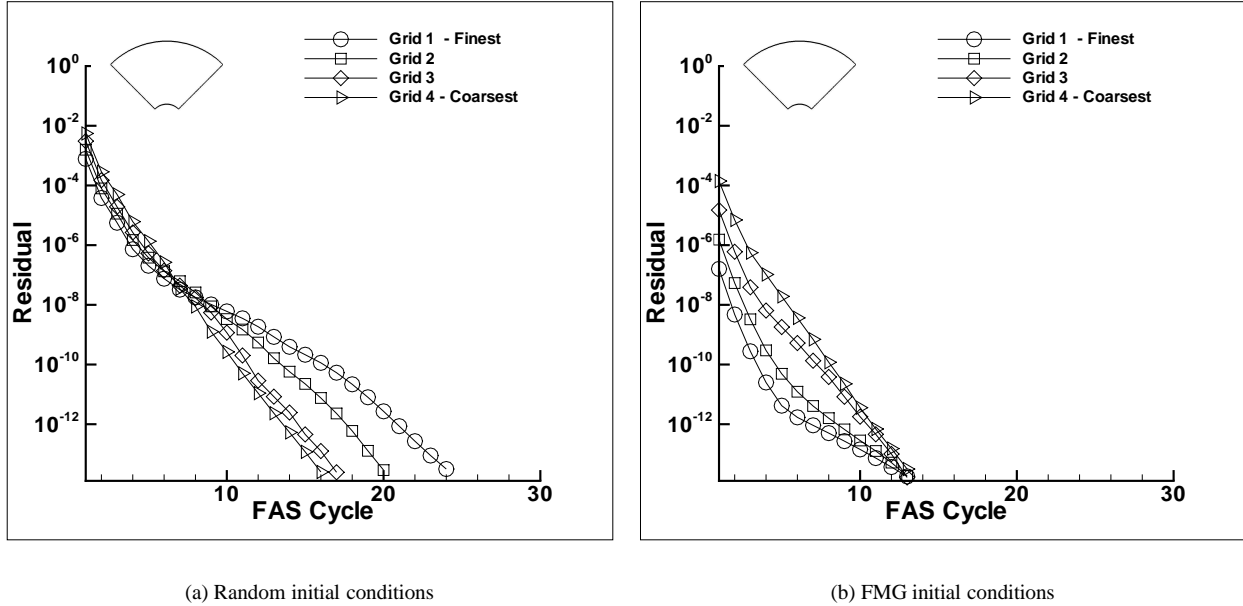


Figure 6. Residual convergence for boundary-tangency computations with the MG-DC solver; $M = 0.3$; FDS scheme.

Within stagnation flows, the Jacobian can differ appreciably from the small perturbation linearization Eq. (5) because the contribution for the velocity gradient (e.g., $O(u_x)$) to the linearization can be comparable with or even greater than the contributions from differences in velocity (e.g., $O(u/h)$). These terms can subtract from the diagonal contributions associated with the momentum equations. For incompressible discretization schemes in which the momentum equations can be marched before solving an elliptic equation for the pressure, these velocity-gradient terms can cause an error amplification when marching into/from stagnation.¹¹ Here, we find that similar difficulties arise for the MG-DC solver because DC can be unstable. The DC convergence is sensitive to the particular discretization schemes used for LE stagnation. For instance, DC does not converge for the FDS scheme but does for the LDFS and FVS schemes. Fig. 7 shows convergence of the MG-DC solver for stagnation flow using the FDS scheme (left) and the LDFS (right) scheme. An infinite CFL number is used for the LDFS scheme but a CFL of 400 is used for the FDS scheme. On the two coarser grids, the MG-DC scheme does not converge for the FDS scheme — a smaller CFL is necessary for the scheme to remain stable. On the finer grids, the overall residual convergence of either scheme within stagnation is similar to that observed for boundary-tangency computations.

Although not shown, for TE stagnation, both schemes are unstable without addition of a pseudo time step. Analysis of convergence within stagnation leads to a variable-coefficient problem that is difficult to analyze using LMF analysis. One can devise neighborhoods which provide relevant constant-coefficient approximations to the full

linearization, but certain parts of stagnation, such as the stagnation streamline, are inaccessible to a constant-coefficient analysis.¹¹ The stagnation flow analysis was actually a motivating factor for the development of more general quantitative analysis methods. For the airfoil computations in the next section, we simply use the LDFS scheme. The airfoil has a sharp trailing edge which does not seem to cause a problem with this scheme.

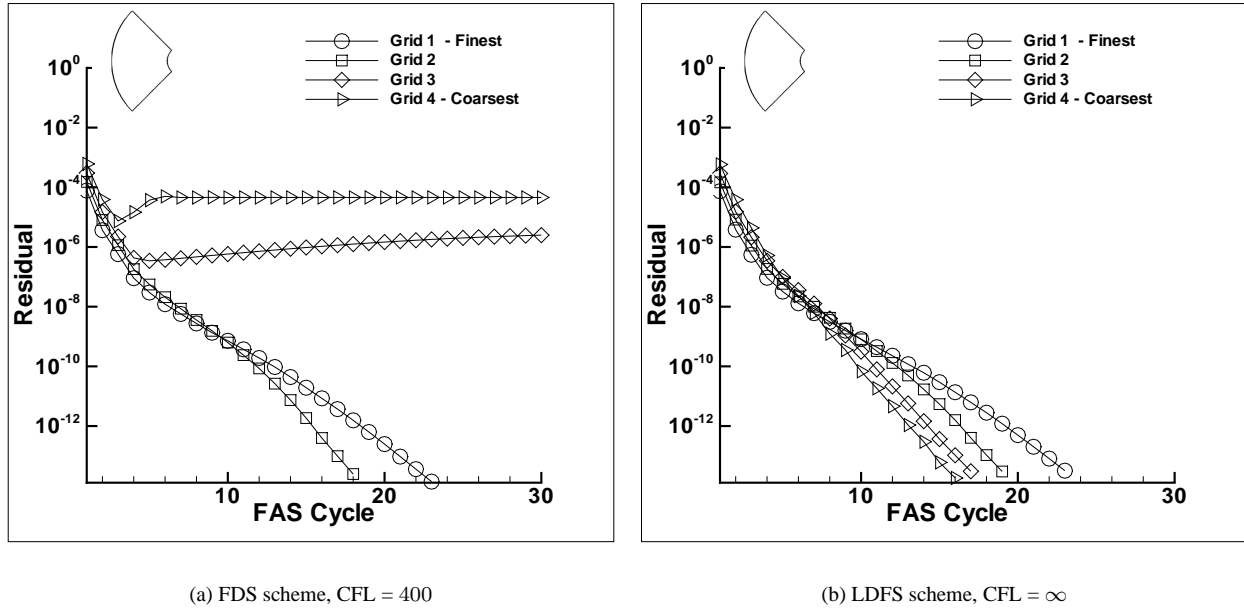


Figure 7. Stagnation computations: residual convergence for the MG-DC solver; finest grid is 128^2 cells, the coarsest grid is 16^2 cells.

VI.B. Multigrid for airfoil

Computations for the NACA 0012 airfoil following the Vassberg and Jameson benchmark study²⁰ are shown here. The grid, similar to that used for the study, is generated through a sheared adaptation of a conformal grid around a Karman-Trefftz airfoil matching the leading-edge radius and trailing-edge angle of the NACA 0012 airfoil. The grid extends 150 chords outwards from the airfoil, and has nearly unity-aspect-ratio cells. The second-order accuracy was verified in computations with lifting and non-lifting manufactured solutions for the Karman-Trefftz airfoil in incompressible flow and in compressible flow at moderate Mach numbers. A compressible-flow manufactured solution was defined with the velocities from the exact incompressible Karman-Trefftz solution along with constant enthalpy and entropy.

Fig. 8 and Fig. 9 shows residual and drag convergence history of FAS(2,1) cycles for the NACA 0012 airfoil at subcritical lifting conditions ($M = 0.5$ and $\alpha = 1.25$) and supercritical non-lifting conditions ($M = 0.8$ and $\alpha = 0$), respectively. Six grids were used in the computations. FMG cycles were started on the coarsest grid composed of 16^2 cells. The finest grid contained 256 cells in the directions around and outward from the airfoil. For the subcritical computations, convergence rates per cycle are uniformly fast. Residual convergence per cycle is 0.3 on the finest grid. Convergence of drag (and also lift, although not shown) is quite fast, within one FMG cycle. The exact drag is zero, reflected in the benchmark level shown as well as the value on the finest grid. The drag is converging with second order accuracy although finer grids are necessary to confirm this.

For the supercritical computation, convergence rates per cycle are quite disparate between grids. The two grids before the finest grid in the FMG sequence are converging much slower than the finest grid or the two initial coarser grids. No limiter is used in these computations. Drag is again converging within one FMG cycle. The drag is converging with second order accuracy to the benchmark level.

VII. Discussions

The MG-DC solver used here is similar to the multigrid scheme developed previously.^{6,7} The previous scheme used alternating-line Jacobi and/or colored relaxations that do not provide sufficient damping of high-frequency errors in purely inviscid regions of the flow. Analysis methods were not applied to identify this shortcoming and instead other parts of the algorithm were modified to compensate, namely a pseudo-time step limited by a maximum CFL

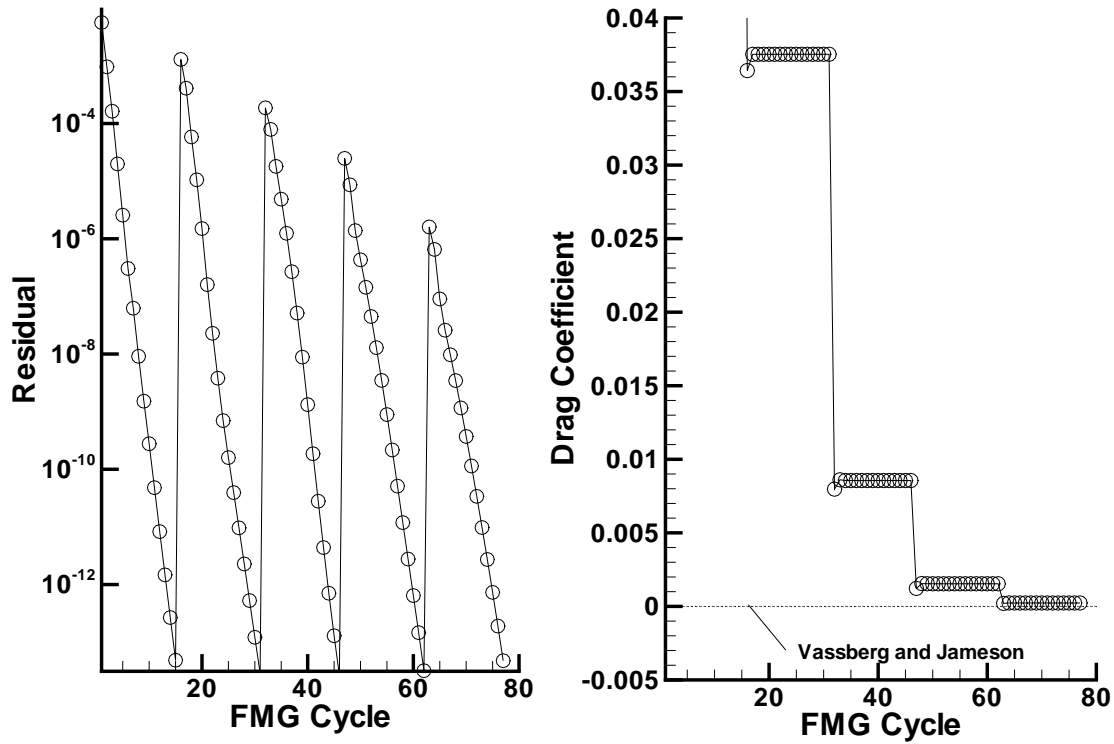


Figure 8. Residual and drag convergence history of FAS(2,1) cycles for NACA 0012 airfoil at subcritical lifting conditions; $M = 0.5$ and $\alpha = 1.25$.

of $O(100)$ was added to the implicit relaxation operator, relaxation subiterations were performed, and dissipation via entropy fixes to all fields was added to the FDS discretization. In the present work, we apply under-relaxation based upon optimization of ICG(1,0) cycles, do not add a pseudo-time step except within stagnation, and do not add any entropy fixes.

The convergence of the MG-DC solver has been comprehensively studied within different incompressible and compressible inviscid regimes. The properties of the solver away from any boundaries and discontinuities are analyzed on high-density grids because this region forms the foundation of the methodology. Within this region, the smoothing properties of the scheme have been shown to be bounded away from one using both a modified LMF analysis and a more general ICG analysis. DC alone has some slowly converging iterations on grids of medium density. This behavior has been shown previously for convection but the convergence for the Euler equations is slower than that for pure convection. The convergence is especially slow for near-sonic flows and for very low compressible Mach numbers. Additionally, the asymptotic convergence seen on medium-density grids is significantly different from the asymptotic convergence on high-density grids. Certain downstream-boundary modes are very slowly damped on high-density grids. The FAS multigrid scheme accelerates convergence of the slow DC iterations to the extent determined by the coarse-grid correction. The 2-level asymptotic convergence rates are well separated from unity over most of the region but slow convergence is noted for near-sonic and very low-Mach compressible flows.

We have applied the MG-DC solver to the NACA 0012 airfoil and to different flow regimes, such as near-tangency and stagnation. The MG-DC solver encounters problems within stagnation regions. The FDS scheme is unstable without a time step addition for leading-edge stagnation and all schemes have a problem for smooth trailing-edge stagnation. Analysis of the linearization within stagnation predicts difficulties associated with the loss of diagonal contributions to the momentum equation linearization within decelerating flow. A pseudo-time step addition can provide convergence, although the amount varies from grid to grid. Nonetheless, for the airfoil flow, with a sharp trailing-edge, residuals were fast converging for a subcritical flow on a sequence of grids. For supercritical flow, residuals converged slower on some intermediate FMG grids than on the finest grid or the two coarsest grids. The

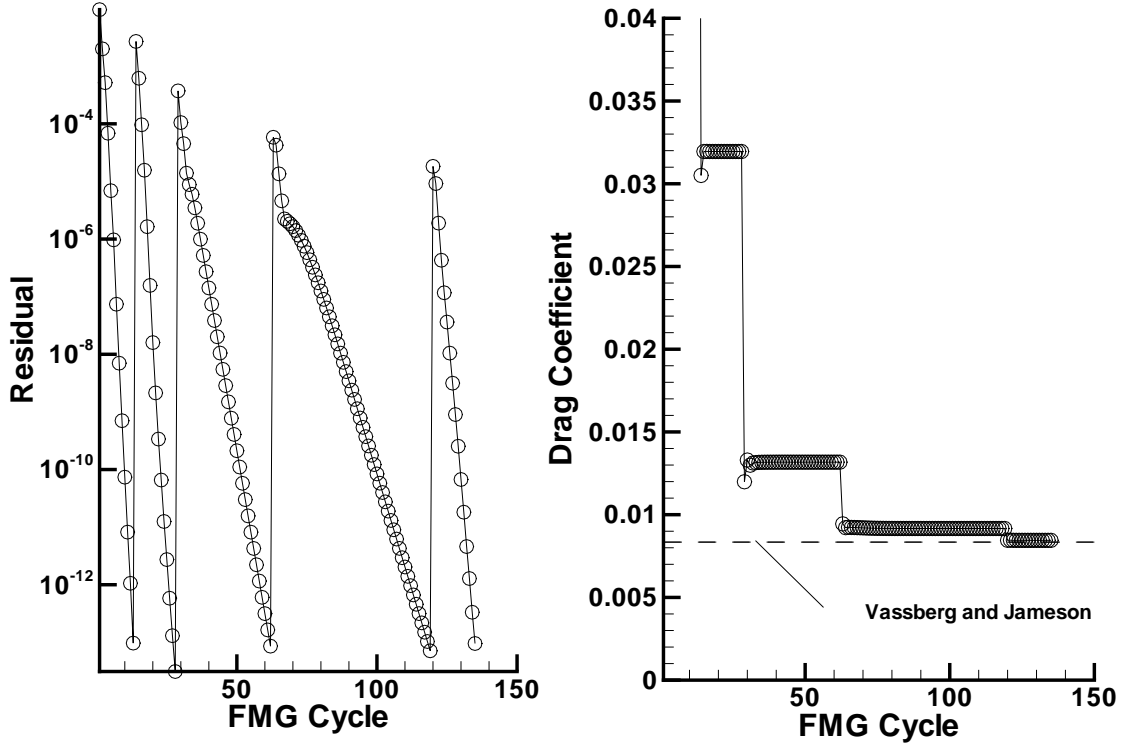


Figure 9. Residual and drag convergence history of FAS(2,1) cycles for NACA 0012 airfoil at supercritical non-lifting conditions; $M = 0.8$ and $\alpha = 0$.

cause of the slowdown may be associated with the coarse-grid correction near Mach unity. Also, the lift and drag both showed second-order accuracy in grid refinement for subcritical and supercritical conditions.

A key measure of efficiency for a multigrid method is the number of FMG cycles required to converge algebraic errors below the level of discretization errors. Ideally only a single cycle is needed. For both airfoil solutions, algebraic errors in lift and drag were well below discretization errors after a single FMG cycle. Another key property for an iterative solver is to ensure that the residual can be driven (fast) to the zero level if needed. The MG-DC solver provides fast residual convergence. The efficiency of the scheme is limited by the coarse-grid correction. Previous work has shown that a modified coarse-grid discretization can substantially improve the correction. The effectiveness of the scheme needs to be explored on high-density grids and in the regimes with slower convergence. Local relaxations in slow-convergence regions may accelerate convergence even further.

A. Modified Local Mode Fourier Analysis

For given Mach number and angle of attack, the respective symbols of the target, \mathbf{T} , and driver, \mathbf{D} , operators on a uniform Cartesian grid with mesh spacing h are defined as

$$\begin{aligned} \mathbf{T}(\theta_x, \theta_y) \equiv & \mathbf{A}^+ \frac{1}{4h} (e^{i\theta_x i_x} + 3 - 5e^{-i\theta_x i_x} + e^{-2i\theta_x i_x}) \\ & - \mathbf{A}^- \frac{1}{4h} (e^{-i\theta_x i_x} + 3 - 5e^{i\theta_x i_x} + e^{2i\theta_x i_x}) \\ & + \mathbf{B}^+ \frac{1}{4h} (e^{i\theta_y i_y} + 3 - 5e^{-i\theta_y i_y} + e^{-2i\theta_y i_y}) \\ & - \mathbf{B}^- \frac{1}{4h} (e^{-i\theta_y i_y} + 3 - 5e^{i\theta_y i_y} + e^{2i\theta_y i_y}). \end{aligned} \quad (6)$$

$$\begin{aligned} \mathbf{D}(\theta_x, \theta_y) \equiv & \mathbf{A}^+ \frac{1}{h} (1 - e^{-i\theta_x i_x}) - \mathbf{A}^- \frac{1}{h} (1 - e^{i\theta_x i_x}) \\ & + \mathbf{B}^+ \frac{1}{h} (1 - e^{-i\theta_y i_y}) - \mathbf{B}^- \frac{1}{h} (1 - e^{i\theta_y i_y}). \end{aligned} \quad (7)$$

The symbol of the DC iteration is a 4×4 matrix

$$\mathbf{DC}(\theta_x, \theta_y) \equiv \mathbf{I} - \mathbf{D}^{-1}\mathbf{T}, \quad (8)$$

where \mathbf{I} is the identity matrix.

The smoothing rate, μ , is estimated as the maximum spectral radius

$$\mu = \max \rho(\mathbf{DC}d), \quad (9)$$

where d is a high-frequency indicator. For a flow with $\alpha \leq 45^\circ$,

$$d = \begin{cases} 1, & \text{if } \max(|\theta_x|, |\theta_y|) \geq \frac{\pi}{2} \text{ \& } |\text{mod}(\theta_x + \frac{v}{u}\theta_y, 2\pi) - \pi| \leq \frac{\pi}{2}; \\ 0, & \text{otherwise.} \end{cases} \quad (10)$$

B. Semi-Discrete Analysis

The SD analysis considers the solutions in the form of $e^{i\theta_y}W_{i_x}$, $i_x = 0, \dots, N_x$, where N_x is the number of nodes in the x -direction. The original multidimensional discrete problem is, thus, translated into a one-dimensional problem parametrized by the normalized Fourier frequency, $|\theta_y| \leq \pi$. The discrete function W_{i_x} is either a scalar solution for the convection equation, or a vector solution for the system of flow equations (5). The analysis takes into account specific implementations of boundary conditions and is capable to predict details of solution evolution in individual iterations. When zero manufactured solution is used, the round-off error does not affect computations, which is critical for the ability to observe asymptotic convergence in computations. SD tests routinely encounter and treat residuals as small as 10^{-150} . The asymptotic convergence rate can be directly evaluated as the spectral radius of the iteration matrix. The analysis is precise for a constant-coefficient formulation with y-periodic boundary conditions. A description of the analysis in application to constant-coefficient convection equation is provided in a previous paper.⁸

The DC iteration matrix has the form:

$$\mathbf{DC} = \mathbf{I} - \mathbf{D}^{-1}\mathbf{T}. \quad (11)$$

Here \mathbf{I} , \mathbf{T} , and \mathbf{D} are the identity, target, and driver matrices, respectively. For the convection equation, $aw_x + bw_y = f$, the matrix \mathbf{T} corresponds to the Fromm discretization, with a row composed of the following coefficients:

$$\mathbf{T} = \begin{bmatrix} \cdots & 0 & \frac{a}{4h_x} & \frac{-5a}{4h_x} & \underline{\frac{3a}{4h_x} + B_2} & \frac{a}{4h_x} & 0 & \cdots \end{bmatrix}, \quad (12)$$

$$B_2 = \frac{b}{4h_y} (e^{i\theta_y} + 3 - 5e^{-i\theta_y} + e^{-2i\theta_y}), \quad (13)$$

and the main diagonal coefficient is underlined. \mathbf{D} is a driver two-diagonal matrix:

$$\mathbf{D} = \begin{bmatrix} \cdots & 0 & \frac{a}{h_x} & \underline{\frac{a}{h_x} + B_1} & 0 & \cdots \end{bmatrix}, \quad (14)$$

$$B_1 = \frac{b}{h_y} (1 - e^{-i\theta_y}). \quad (15)$$

For the system of equations the corresponding matrices are block diagonal.

The iteration matrix of a two-level MG-DC $V(\nu_1, \nu_2)$ cycle is

$$\mathbf{MG} = (\mathbf{DC})^{\nu_2} \mathbf{CGC} (\mathbf{DC})^{\nu_1}, \quad (16)$$

$$\mathbf{CGC} = \mathbf{I} - \mathbf{P} \mathbf{T}_c^{-1} \mathbf{R} \mathbf{T}. \quad (17)$$

Here \mathbf{CGC} is the coarse-grid-correction matrix, \mathbf{R} and \mathbf{P} are restriction and prolongation matrices, respectively, and \mathbf{T}_c is the coarse-grid-operator matrix. The size of the multigrid matrices is twice as large as the size of corresponding single-grid matrices because multigrid couples two components corresponding to Fourier frequencies θ_y and $\theta_y + \pi$.

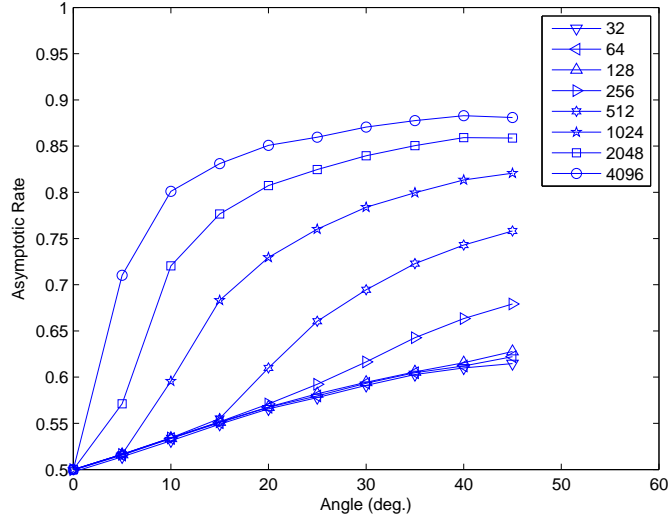


Figure 10. Asymptotic convergence rate of DC iterations for constant-coefficient convection equation computed with the SD analysis.

C. Scalar convection equation

The asymptotic convergence of DC iterations for the scalar convection equation is computed with the SD analysis. The variation of the asymptotic rate with the grid density and the angle of attack is shown in Fig. 10. The convergence plots on grids of moderate size with up to 128^2 degrees of freedom are practically over-plotted. For small angles of attack, grids with 256^2 and 512^2 degrees of freedom also show similar rates. On finer grids, however, the convergence rates are dramatically different. Slow asymptotic rates are observed for solutions that are exponentially decaying from the outflow boundary toward the interior. Fig. 11 shows the real and imaginary components of an eigensolution for DC iterations on a grid with $N_x = 2048$ and $\alpha = 45^\circ$; only variation near the outflow boundary is shown. The eigensolution corresponds to $\theta_y = \frac{\pi}{5}$ and the eigenvalue $\mu = 0.8464 - 0.1382i$.

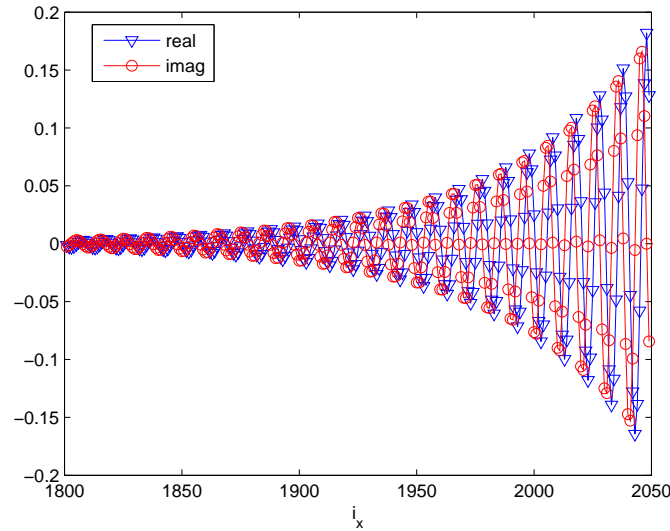


Figure 11. Eigensolution on a grid with $N_x = 2048$; $\alpha = 45^\circ$; $\theta_y = \frac{\pi}{5}$; and the corresponding eigenvalue is $\mu = 0.8464 - 0.1382i$.

Even for combinations of grids and solutions with fast asymptotic convergence, many slow DC iterations may be encountered before the asymptotic regime is attained. Algorithmic enhancements are required to accelerate slow iterations preceding the asymptotic convergence and to improve asymptotic convergence, if necessary. Multigrid

addresses both these issues. Convergence of standard full-coarsening multigrid cycles for second-order convection discretizations on high-density grids is limited by the factor 0.75.¹⁹ For the diagonal flow alignment the scheme becomes third-order accurate and the limiting factor is even more severe, 0.875. However, these rates are significantly better than slow-iteration DC rates.

D. Defect-correction iterations for small-perturbation flows

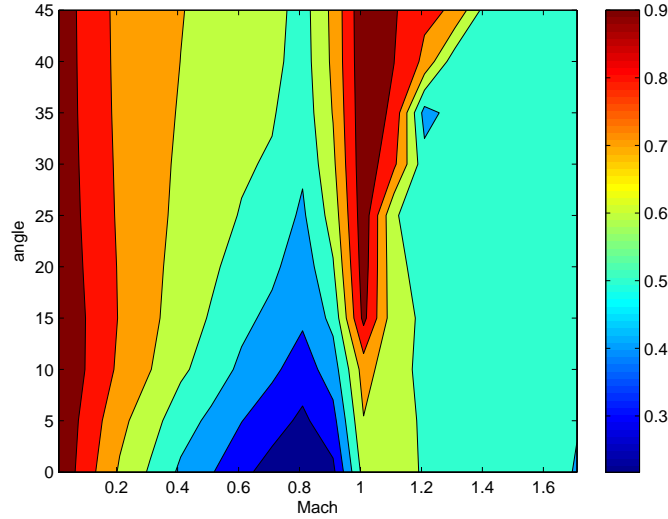


Figure 12. Asymptotic convergence of DC iterations computed with the SD analysis.

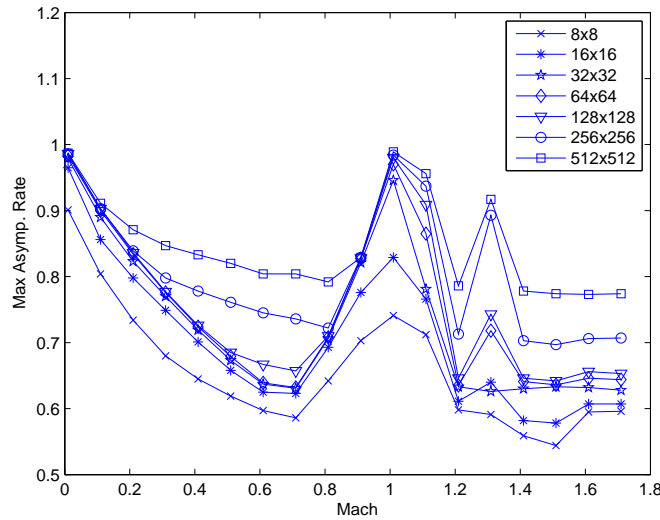


Figure 13. Asymptotic convergence of DC iterations computed with the SD analysis.

In this section, DC iterations are applied for SP flows away from boundaries and singularities. The asymptotic rates of DC iterations are computed with the SD analysis. The angles of attack are varying as $0 \leq \alpha \leq 45^\circ$ and Mach number is varying between (almost) zero and fully supersonic, $0.01 \leq M \leq 1.81$. Fig. 12 shows levels of the asymptotic rate on a 128^2 grid. The grid is not a high-density grid and the rates do not necessarily show the maximum values approached in grid refinement, but the distribution is representative for the medium-density grids. It shows that the slowest convergence is expected at low and near-sonic Mach numbers.

Fig. 13 shows the variation of asymptotic convergence rates versus Mach number on grids of progressively high density. The maximum rate over the range of angles of attack $0 \leq \alpha \leq 45^\circ$ is shown. Slowdown at low and sonic Mach numbers is observed on all grids. Similar to the convection convergence pattern shown in Fig. 10, the rates slow down for all Mach numbers on finer grids.

Actual computations performed on the inflow/outflow domain shown in Fig 1 indicate similar trends. Fig. 14 shows the “asymptotic” rate, namely, the last rate exhibited before achieving the machine-zero error, and the maximum convergence rate observed over the course of iterations. The rates shown in Fig. 14 are somewhat different from the rates predicted by the SD analysis because the error is sometimes reduced to the machine-zero level before the actual asymptotic convergence is achieved. As expected, the maximum rate is closer to one than the asymptotic rate. Both maximum and asymptotic rates peak at $M \approx 0$ and $M \approx 1$.

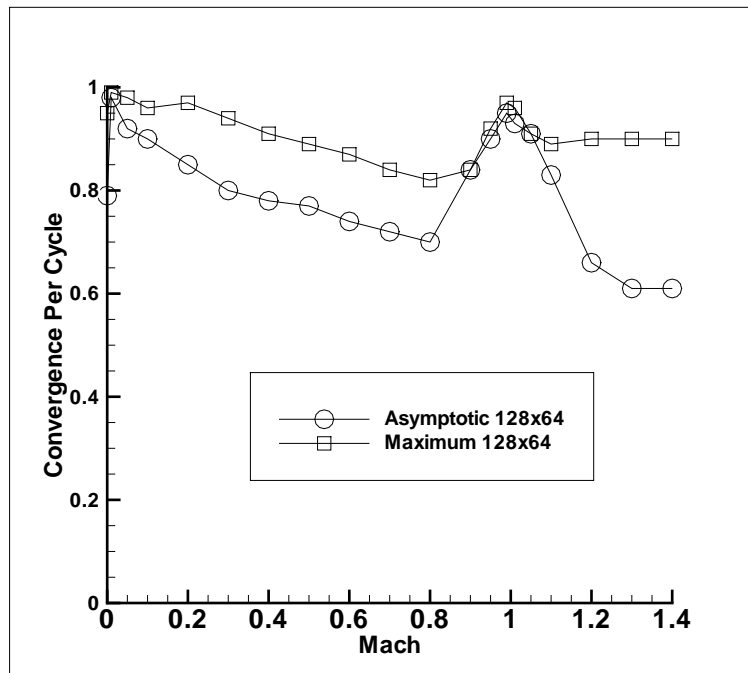


Figure 14. Convergence rates of DC iterations observed in actual SP flow computations.

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