

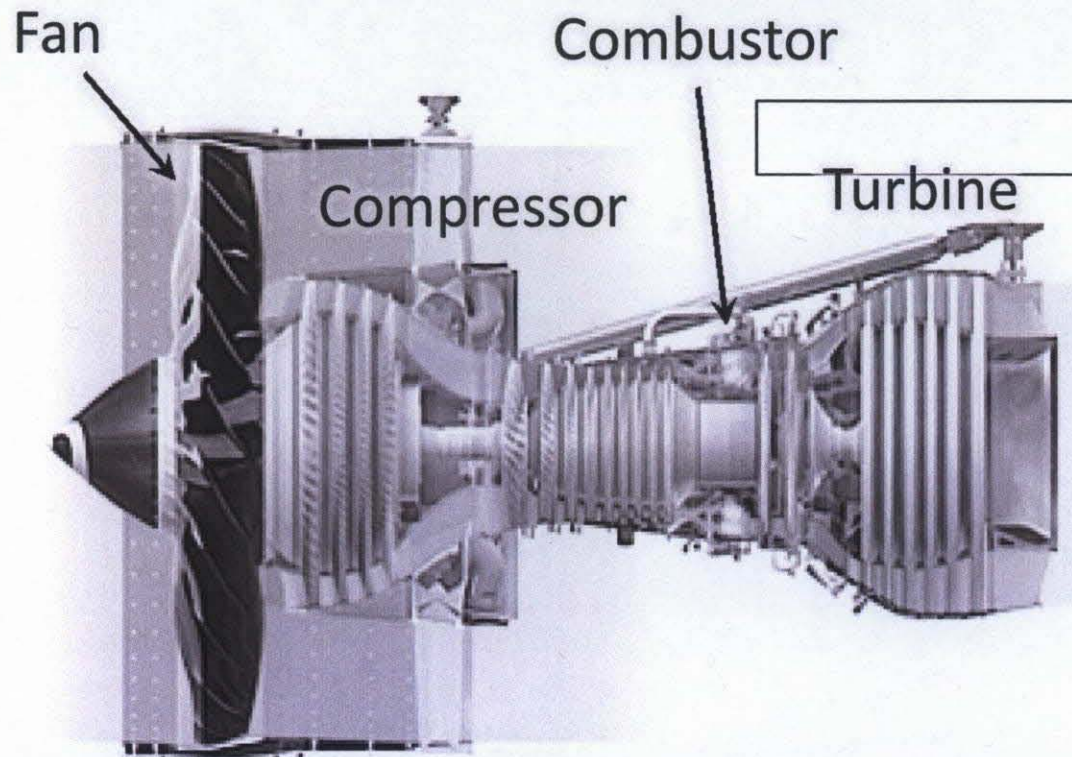


# Overview of NASA GRC Research on Damping of Jet Engine Blades

*Kirsten P. Duffy*  
*Senior Research Associate*  
*University of Toledo*  
*NASA Glenn Research Center*



# Aircraft Engine



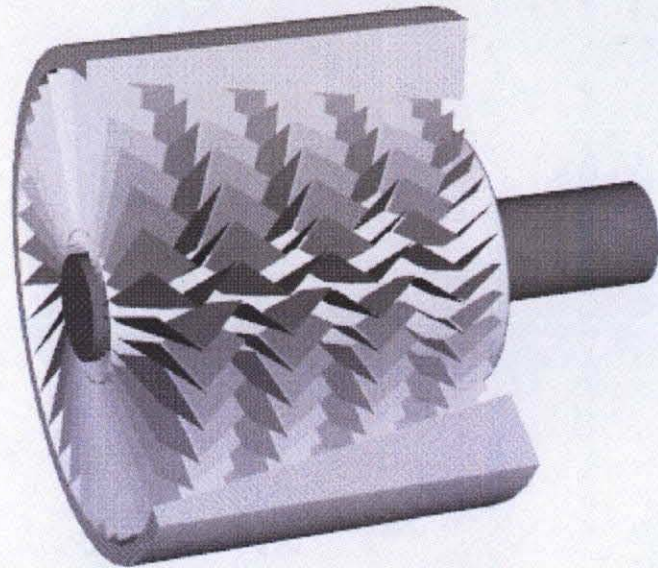
## GE90 Turbofan Engine

<http://www.geaviation.com/education/theatre/ge90/>

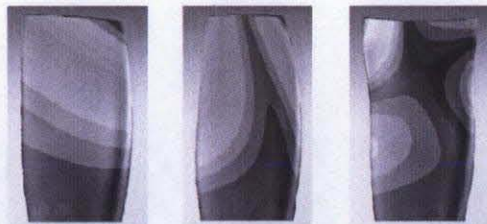




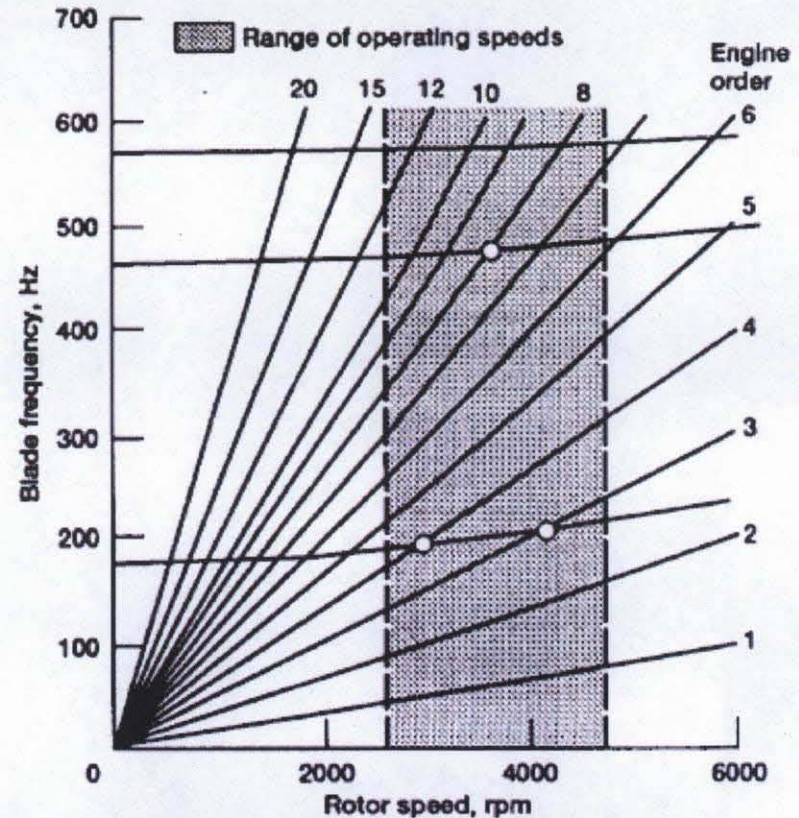
# Engine Blade Forced Vibration



[www.grc.nasa.gov/WWW/K-12/airplane/caxial.html](http://www.grc.nasa.gov/WWW/K-12/airplane/caxial.html)



Blade Vibration Modes



(b) Campbell diagram for rotor blade showing possible forced-response condition from resonance (denoted by circles).

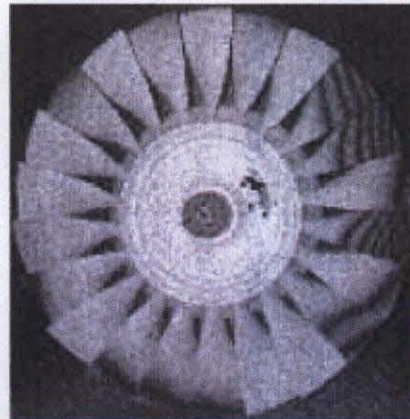
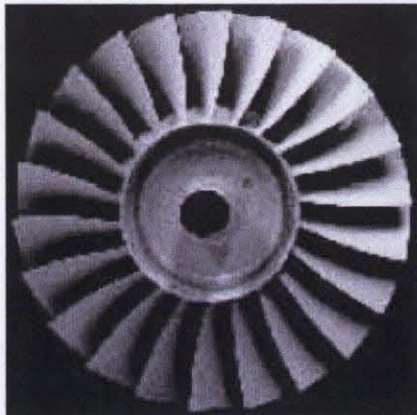
Reddy et. al. 1993 NASA TP-3406  
 "A review of recent aeroelastic analysis methods for propulsion at NASA Lewis Research Center"





# Mistuning

- Blades are manufactured with slight differences
  - Problem → Localized vibration
  - Solutions
    - Increased damping
    - Increased coupling among blades and disk



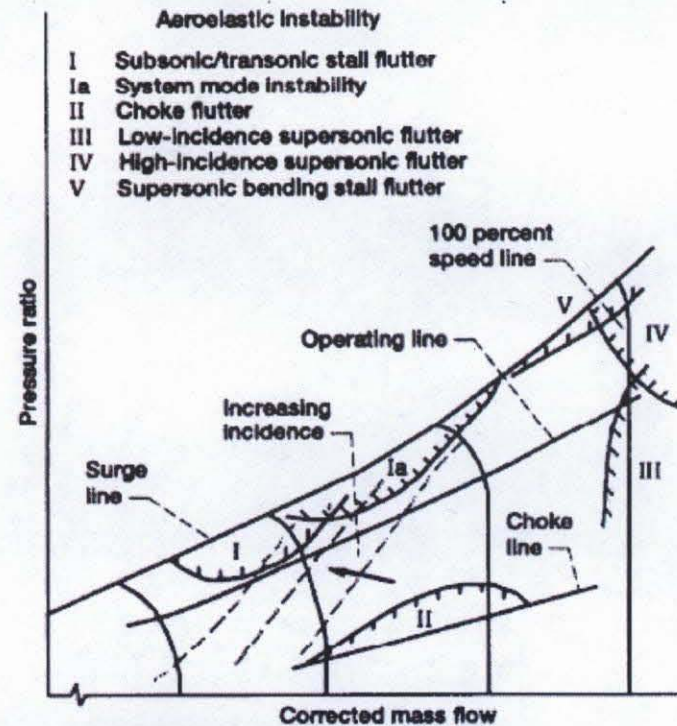
} Response levels  
higher than  
predicted

“Advanced vibration analysis tools and new strategies developed for robust engine rotor development”  
2005 Research and Technology Report – NASA Glenn Research Center  
Castanier & Pierre, U. of Michigan – Min, NASA



# Flutter

- Flutter
  - Self-excited oscillation
  - Airflow/blade interaction  
→ instability
  - Increasing damping can reduce the risk of flutter



(a) Map showing principal types of flutter and regions of occurrence (ref. 4).

Reddy et. al. 1993 NASA TP-3406

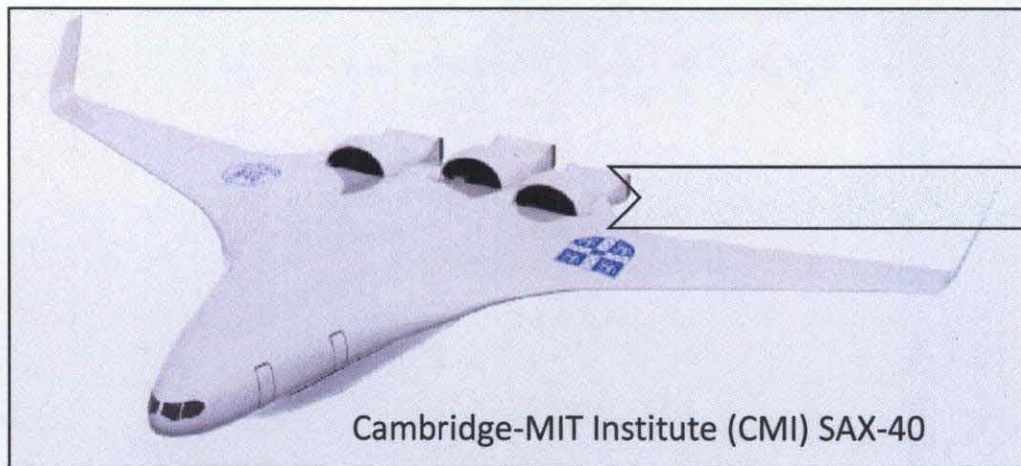
"A review of recent aeroelastic analysis methods for propulsion at NASA Lewis Research Center"





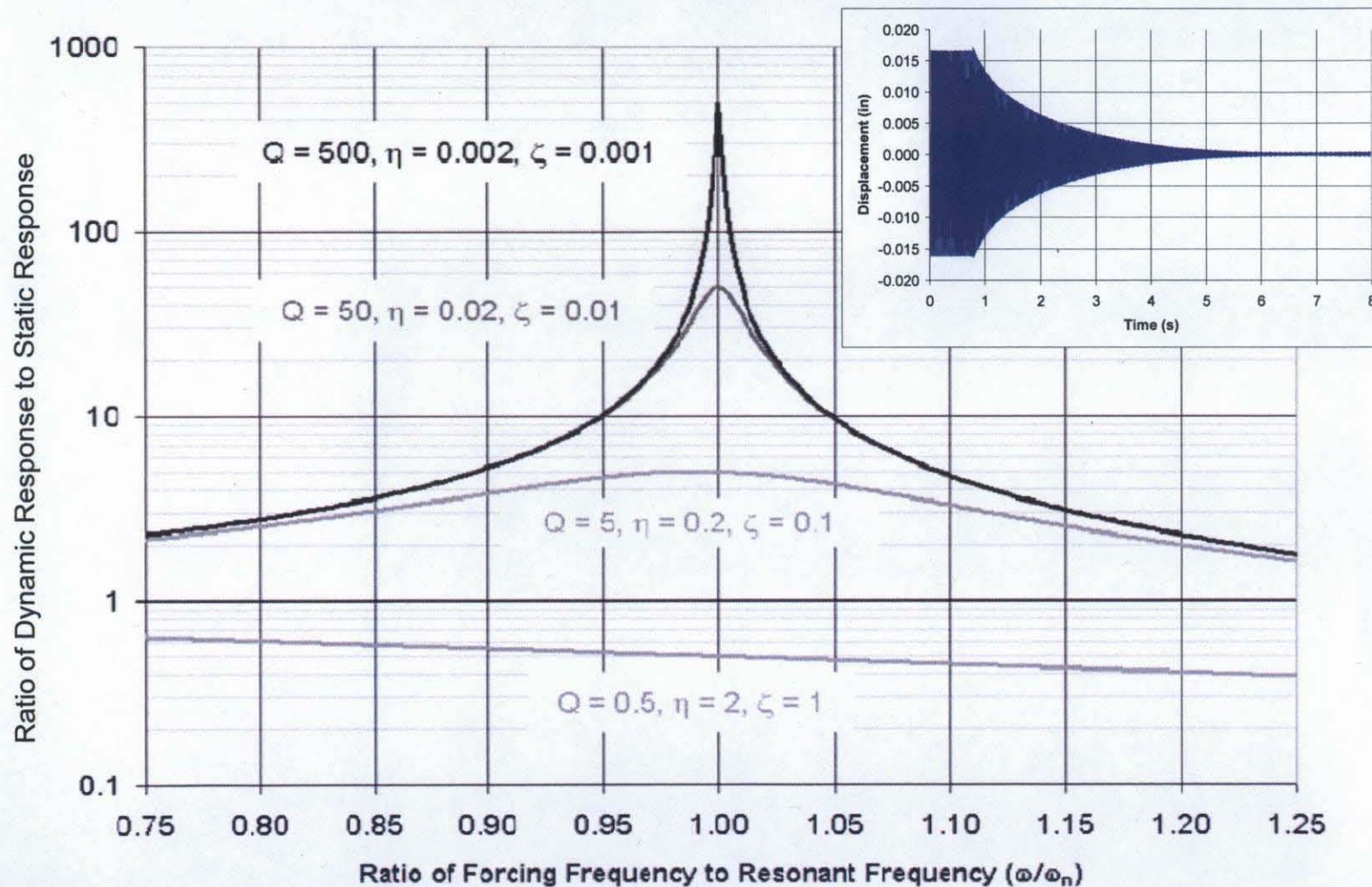
# Future Aircraft

- Embedded engines
  - Benefits:
    - Decreased noise
    - Improved efficiency
    - Possibility of short takeoff and landing
  - Problem: Non-uniform flow into engine – blade excitation





# Solution – Damping

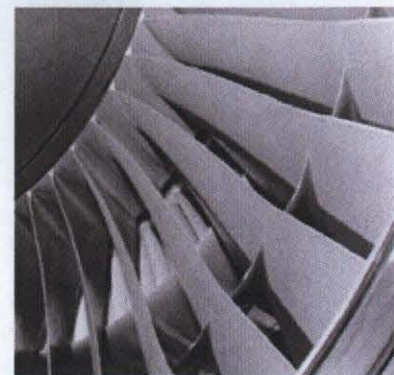




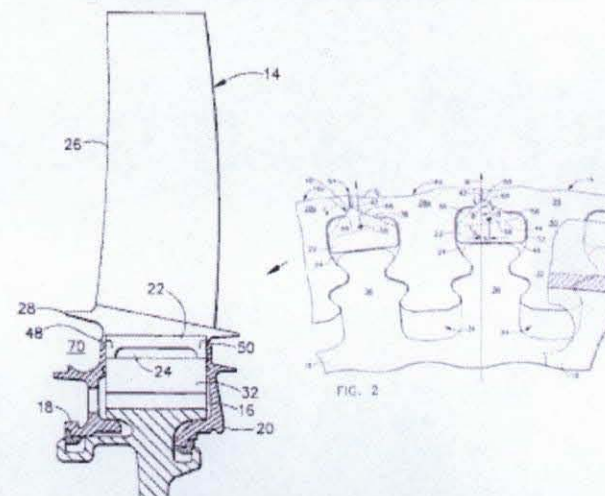


# Engine Blade Damping

- Sources of damping\*
  - Material damping
    - ~0.02%
    - Very low for metals, higher for composites
  - Aerodynamic damping
    - 0.1% - 1%
  - Structural/mechanical damping
    - Friction at the blade root
    - Friction at shrouds
    - Platform damping
    - Added damping treatments
    - 0.5% - 3%
- Newer blade designs
  - Integrally bladed disks (blisks) – no friction at blade/hub attachment
  - Highly-loaded blades – higher efficiency



Pratt & Whitney  
Shrouded Fan Blade



GE Platform Damper  
Patent 5,478,207

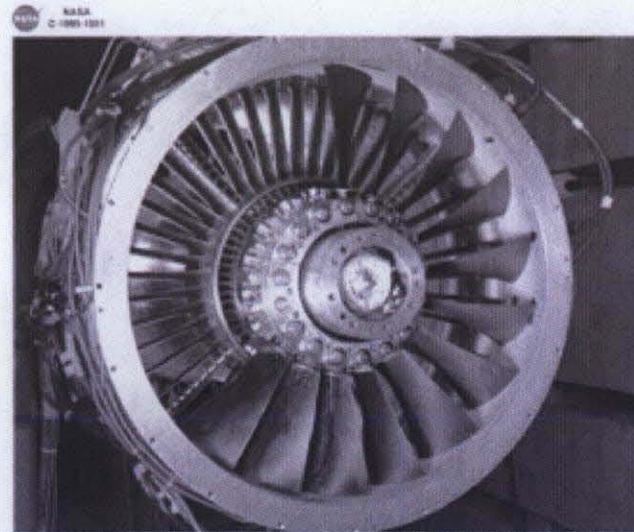
\* Y. El-Aini, R. deLaneuville, A. Stoner, V. Capece, "High Cycle Fatigue of Turbomachinery Components – an Industry Perspective," AIAA-1997-3365.





# NASA Damping Research

- **Turbomachinery blade damping research at NASA Glenn**
  - *Impact damping*
  - *Viscoelastic damping of composite blades (with UC San Diego)*
  - *Plasma-sprayed damping coatings*
  - *High-temperature shape memory alloys*
  - *Piezoelectric materials – passive damping and active control*



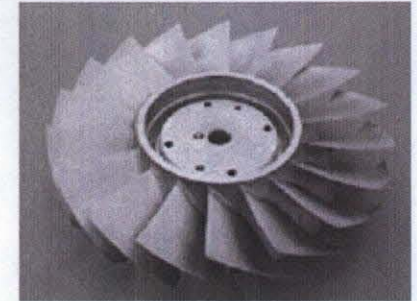
Composite Fan Blades – Tested with Viscoelastic Damping



# Aircraft Engine Blade Environment

## Typical Target Application – lower-temperature:

- *Titanium alloy fan or cold-side compressor blade*
- *Composite fan blade*



Temperature	<i>-40 to 300°C</i>
Vibratory strain amplitude	<i>up to 10<sup>-3</sup></i>
Mean strain (from centrifugal loading)	<i>zero to 10<sup>-3</sup></i>
Frequency	<i>100 to 10,000 Hz</i>
Typical blade loss factor	<i>10<sup>-3</sup> or lower</i>
Target blade loss factor	<i>10<sup>-2</sup></i>

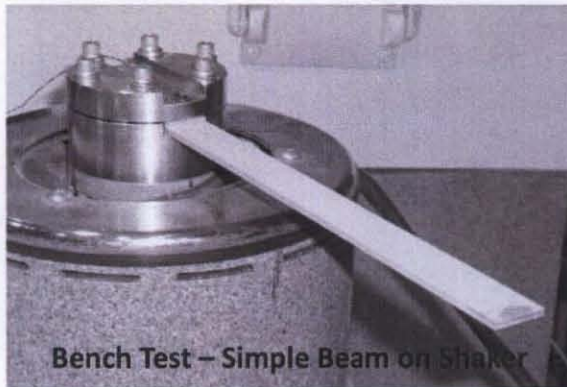
*Note: loss factor  $\eta = Q^{-1} = 2\zeta = \tan \delta$*





# Analysis and Testing Procedure

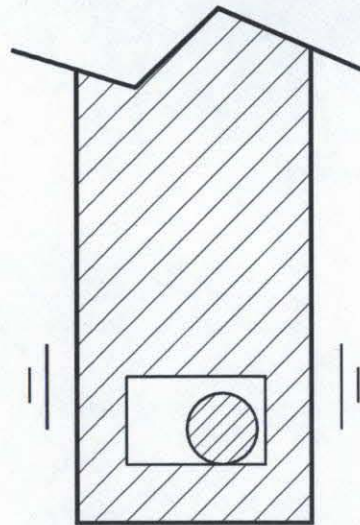
- **Analysis** – Simple reduced order models, structural finite element models, aeroelasticity models (fluid/structure interaction)
- **Testing** – Bench testing, testing in simulated engine environments
- **Test Articles** – simple beam, flat plate, twisted plate, blade





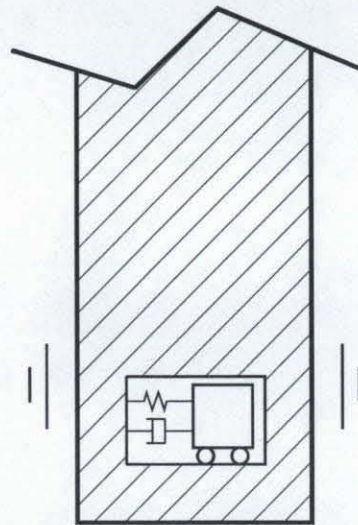


# Self-Tuning Impact Damper



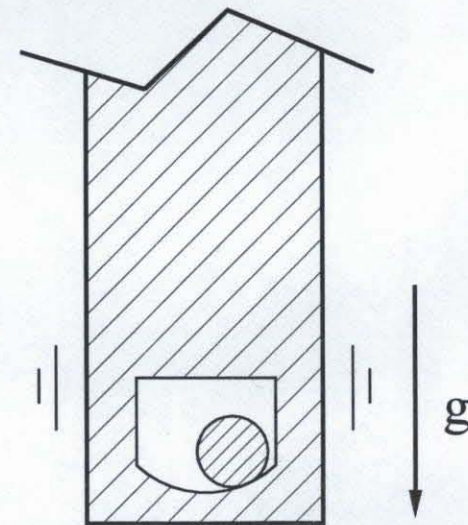
**Impact Damper**

- Displacement-dependent (nonlinear)
- Immobilized at high-g's



**Tuned-Mass Damper**

- Frequency-dependent
- Damping at tuning frequency
- Displacements may be too large for blade cavity



**Tuned Impact Damper**

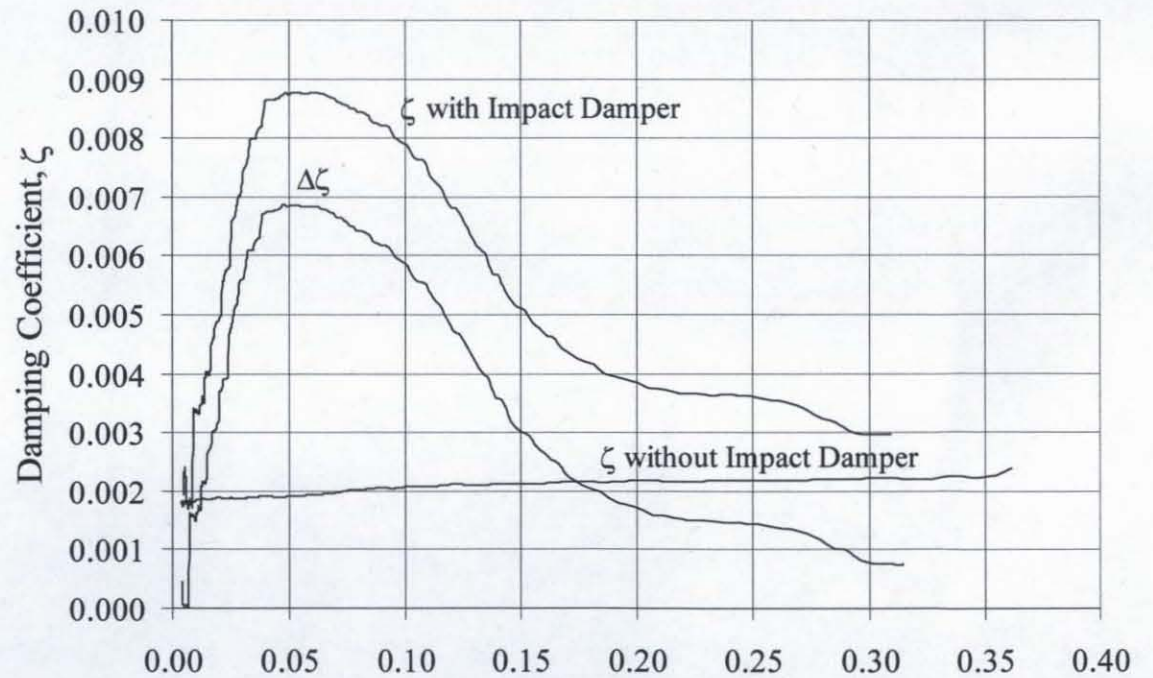
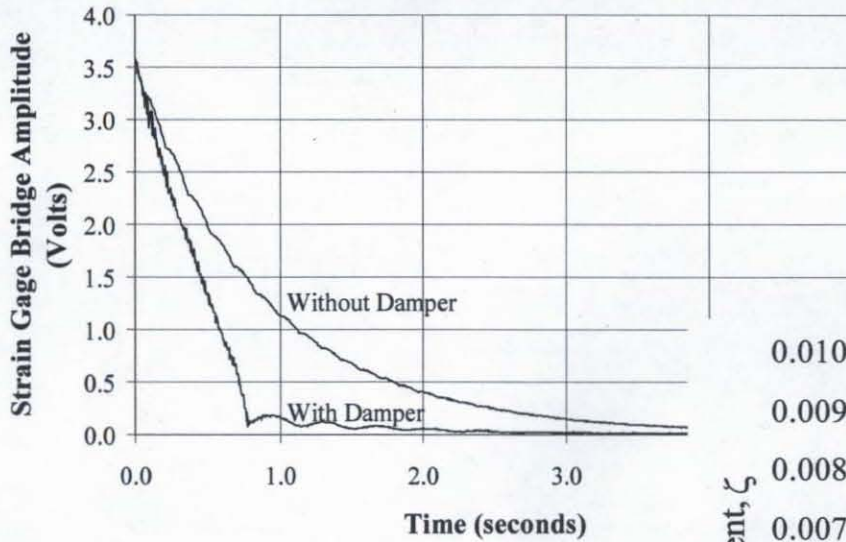
- Frequency- and displacement-dependent (nonlinear)
- Performs better at high-g's





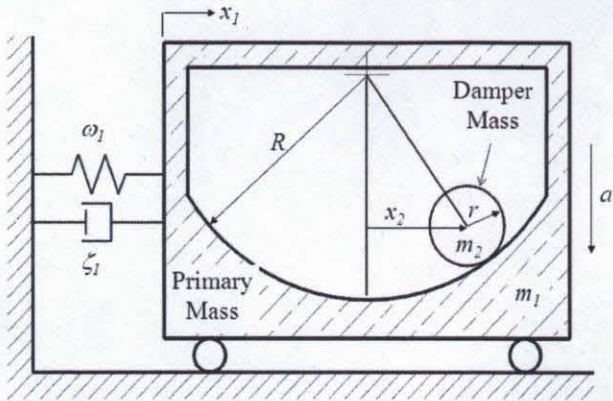
# Self-Tuning Impact Damper

Free Decay Envelope

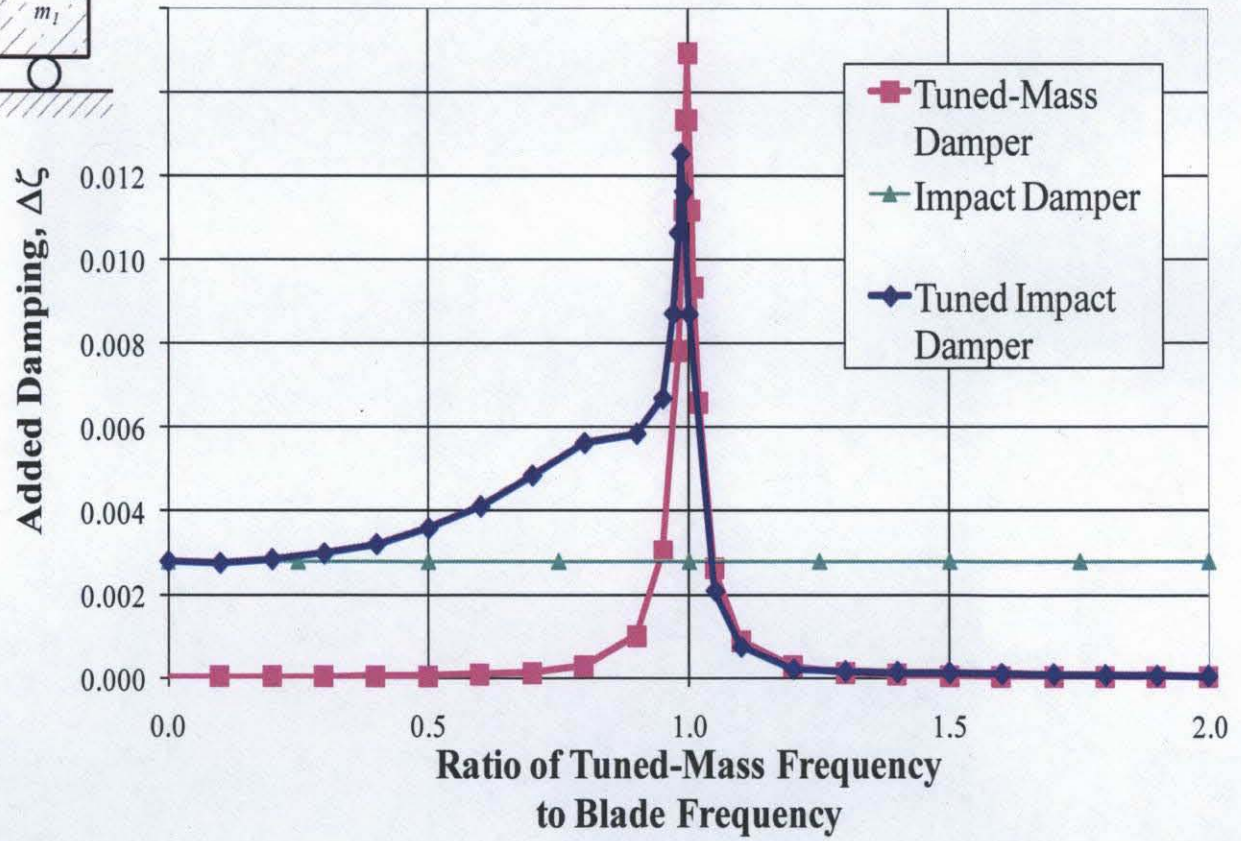




# Self-Tuning Impact Damper



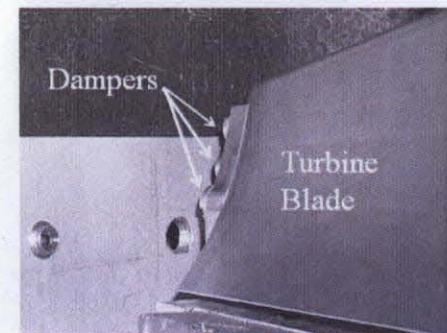
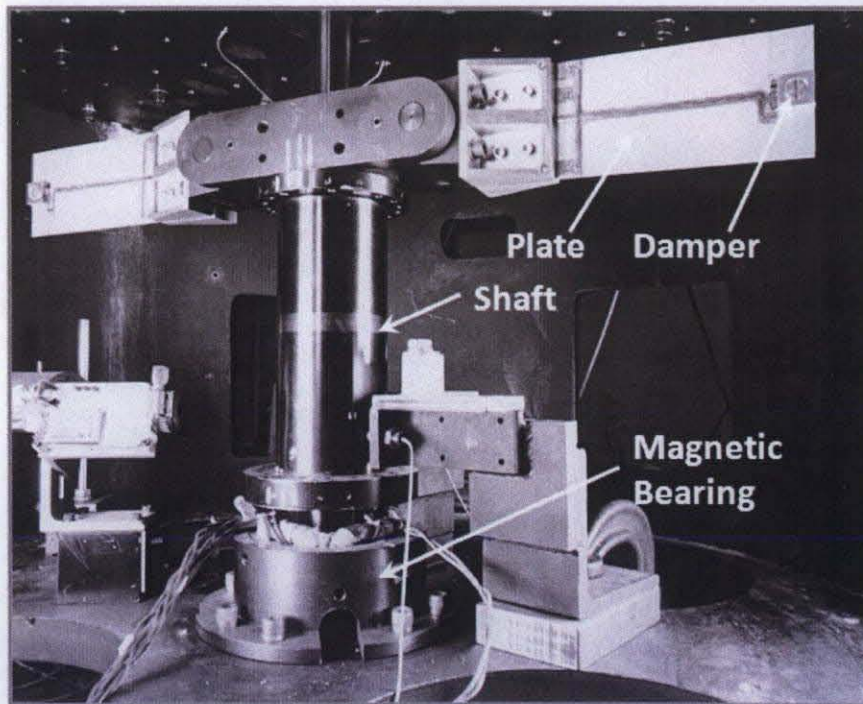
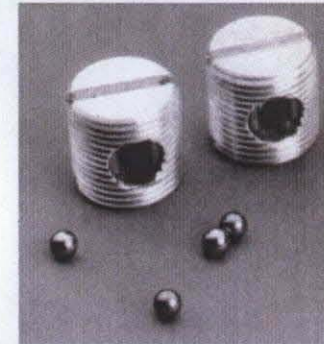
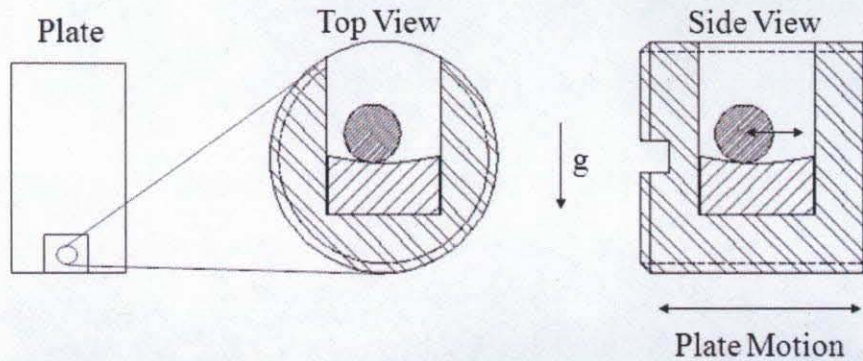
Tuned-Mass Damper vs Tuned Impact Damper







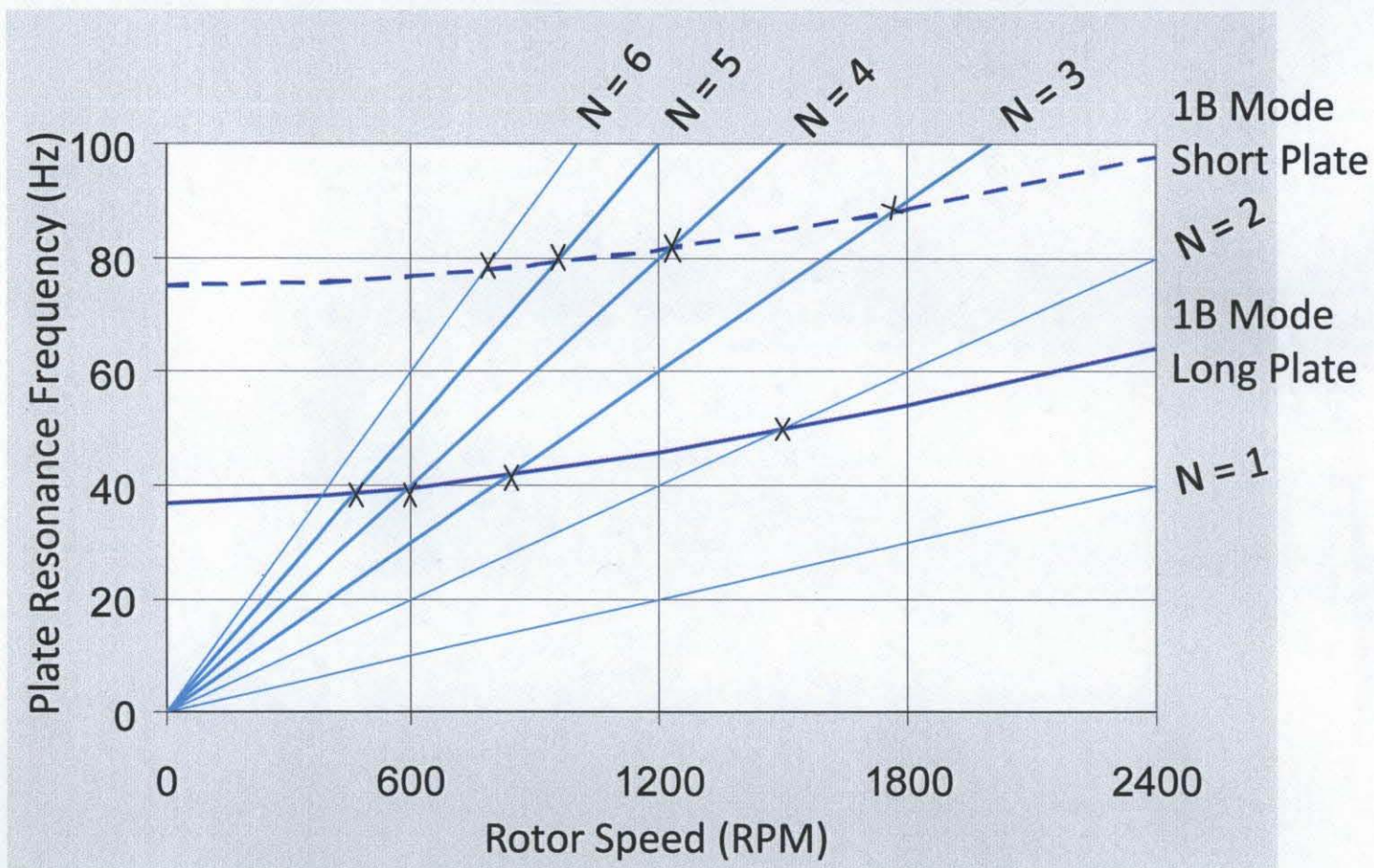
# Self-Tuning Impact Damper







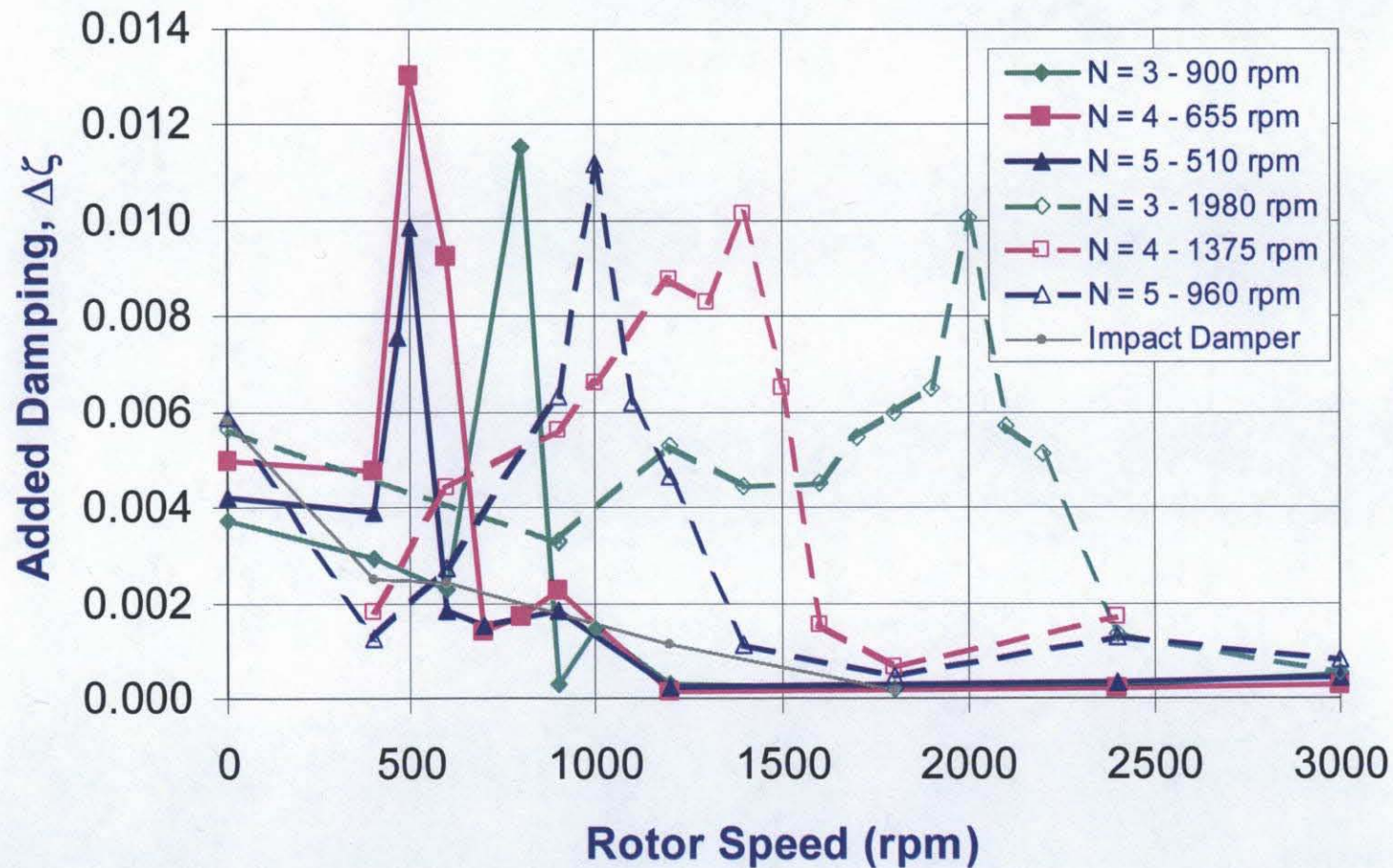
# Self-Tuning Impact Damper







# Self-Tuning Impact Damper





# Viscoelastic Damping

- Complex Modulus

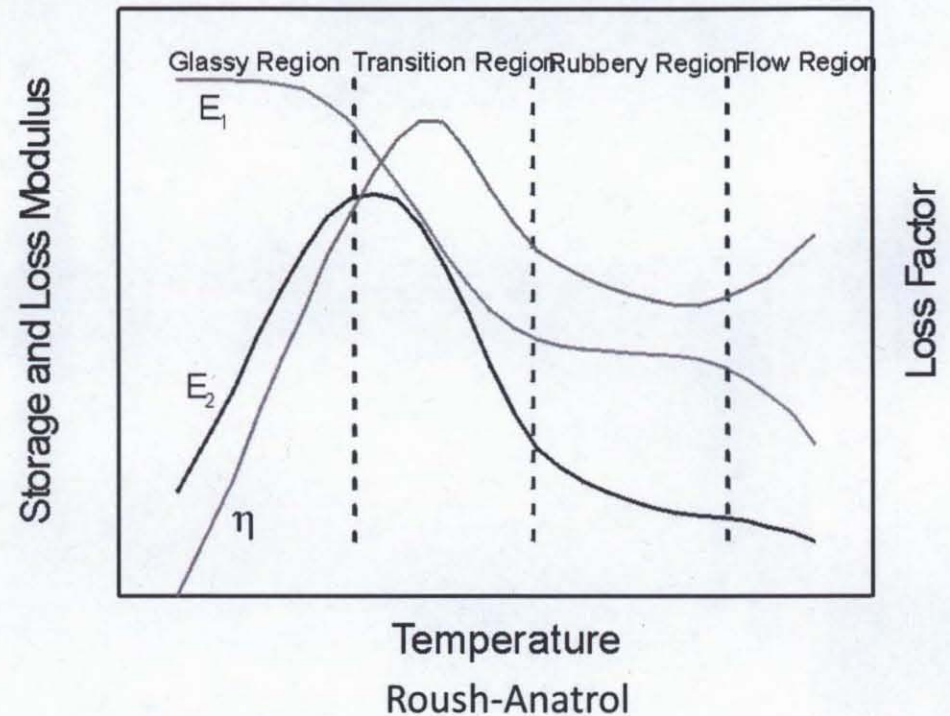
- $E = E_1 + i E_2 = E_1(1 + i \eta)$
- $E_1$  – Storage Modulus
- $E_2$  – Loss Modulus
- $\eta$  – Loss Factor
- **Properties dependent on frequency and temperature**

- Material Behavior

- Glassy region – polymer chains highly ordered – higher stiffness
- Transition region – high damping
- Rubbery region – lower stiffness, lower damping

- Energy Dissipation

- Through **shear stress**
- Constrained layer treatment







# Viscoelastic Damping

## Composite Fan Blade

Kosmatka, Appuhn, Mehmed  
AIAA Paper 2002-1511

“Design and Testing of Integrally Damped First-Stage Composite Fan Blades”

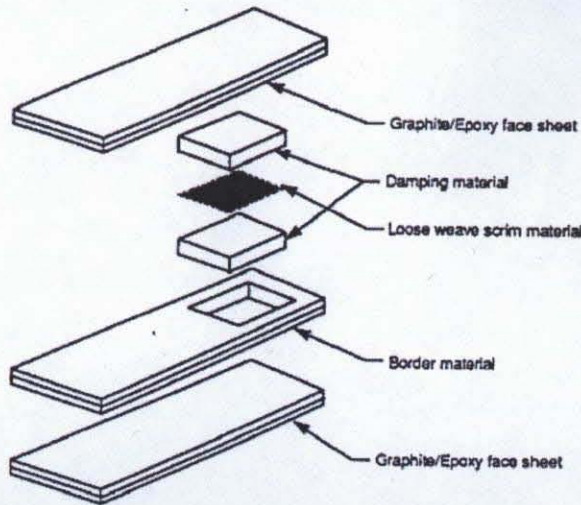
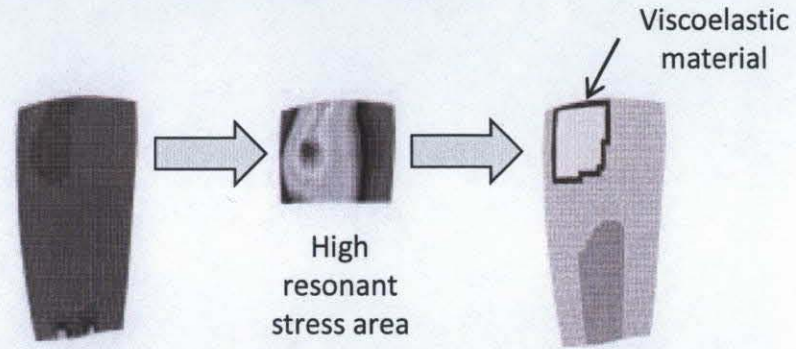
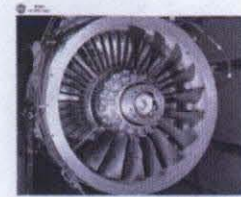


Fig. 3 Blade components

Kosmatka, Lapid, Mehmed – AIAA Paper 96-1598  
“Passive vibration control of advanced composite turbofan blades using integral damping materials”

- Collaboration between NASA GRC and John Kosmatka – UC San Diego
  - Place viscoelastic material within pocket between graphite/epoxy plies
  - Locate visco in area of high modal shear stress
  - Successful demonstration in dynamic spin testing at NASA Glenn





# Viscoelastic Damping

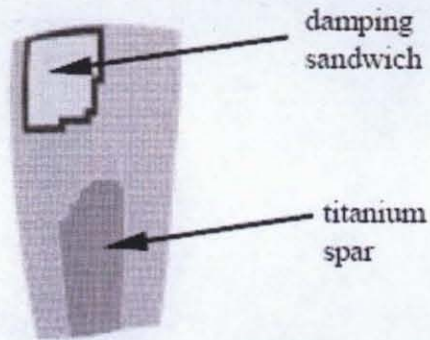


Fig. 6 Patch definition for optimum damping of first chord-wise mode (1581 Hz).

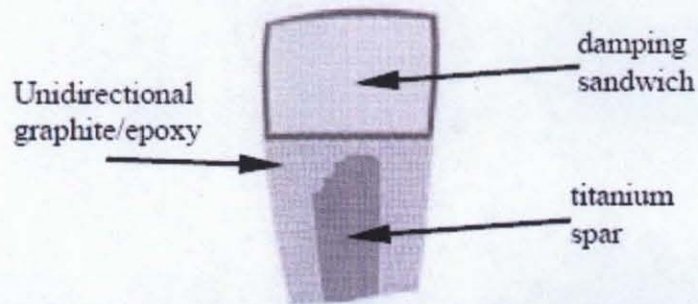


Fig. 5 Patch definition for maximum damping of first chord-wise mode (1581 Hz).

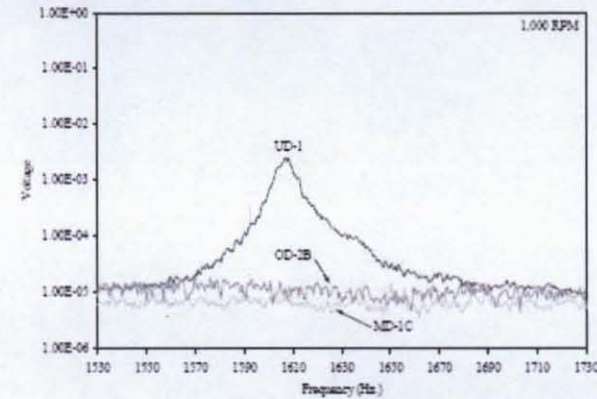


Fig 20 Power Spectrum Comparison for the 1<sup>st</sup> Chordwise Mode at 1,000 RPM

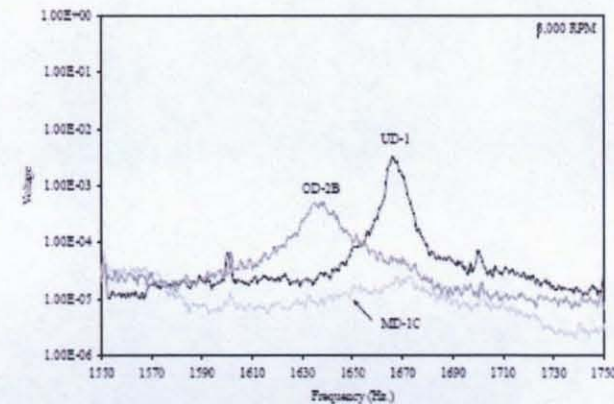


Fig 21 Power Spectrum Comparison for the 1<sup>st</sup> Chordwise Mode at 3,000 RPM

Kosmatka, Appuhn, Mehmed - AIAA Paper 2002-1511  
 "Design and Testing of Integrally Damped First-Stage  
 Composite Fan Blades"

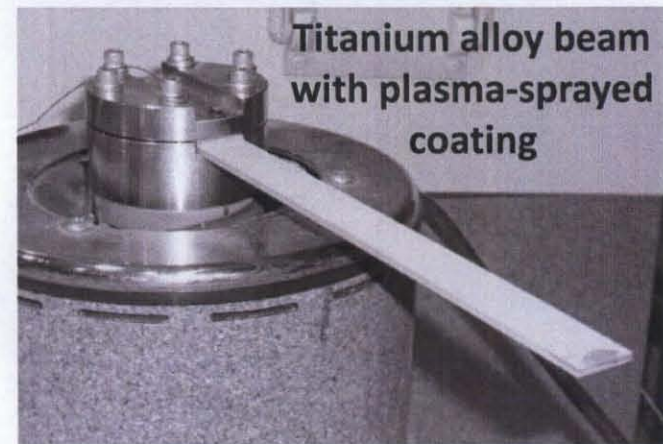




# Damping Surface Treatment

## Examples:

- Viscoelastic surface treatment
- Plasma-sprayed damping coating
- Surface-mounted high-damping shape memory alloy
- Surface-mounted shunted piezoelectric patch



**Oberst beam** – thin layer of damping material on beam surface

- Very thin layer:

$$\eta_{beam+damping} \approx 3\eta_{damping} \left( \frac{E_{damping}}{E_{beam}} \right) \left( \frac{t_{damping}}{t_{beam}} \right)$$

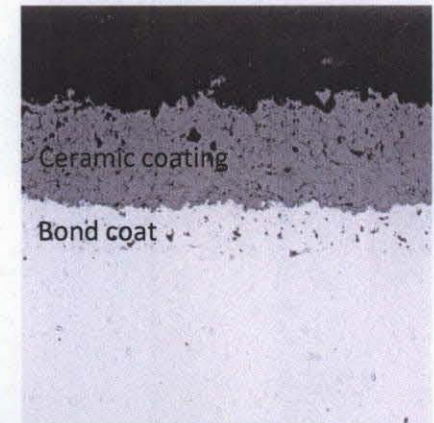


# Plasma-Sprayed Damping Coatings

- Typical coatings currently in use
  - Thermal-barrier coating
    - Allow higher-temperature airflow while insulating metallic blades
  - Environmental-barrier coating
    - Erosion-resistance, durability
  - Added benefit → damping
- Damping mechanism
  - Low temperature (compressor application) – friction between “splats” of coating material – strain level dependent
  - High temperature (turbine application) – elevated damping corresponds with decrease in Young’s modulus of the coating – temperature-dependent



Plasma Spray Torch



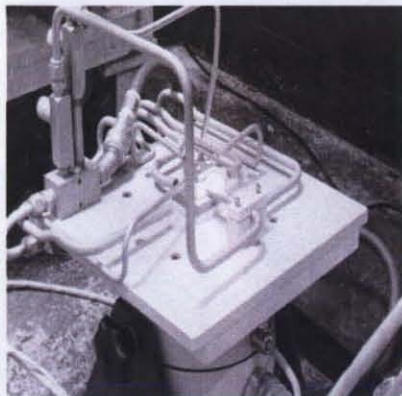
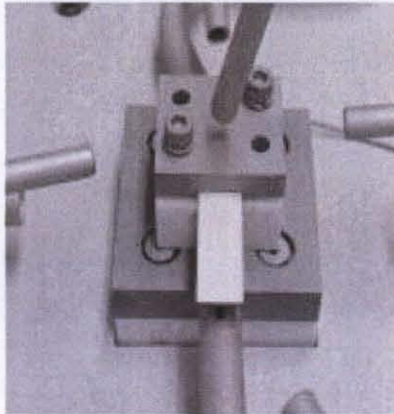
Plasma-Sprayed Coating used for Damping Test





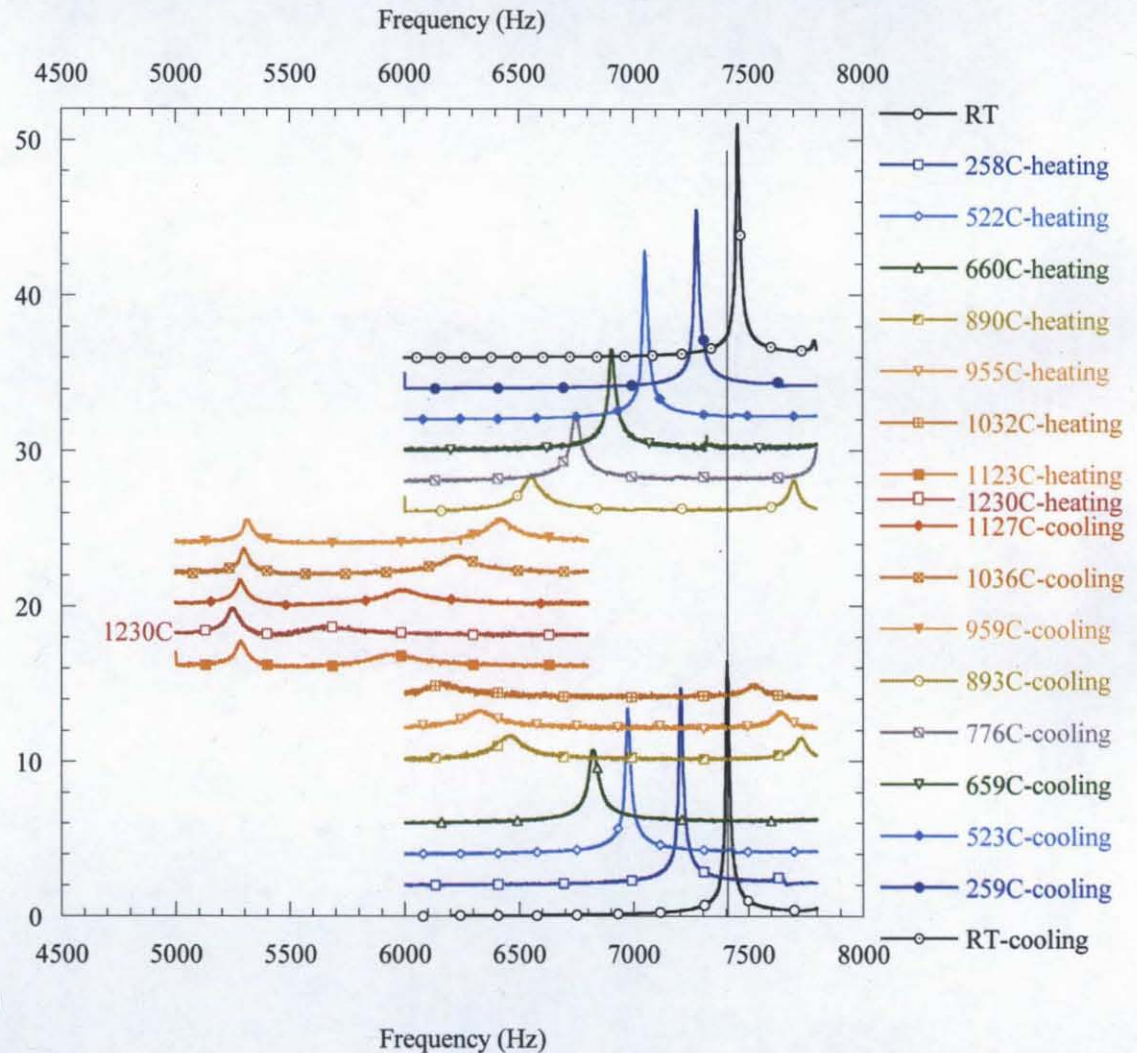
# Plasma-Sprayed Damping Coatings

High-temp application



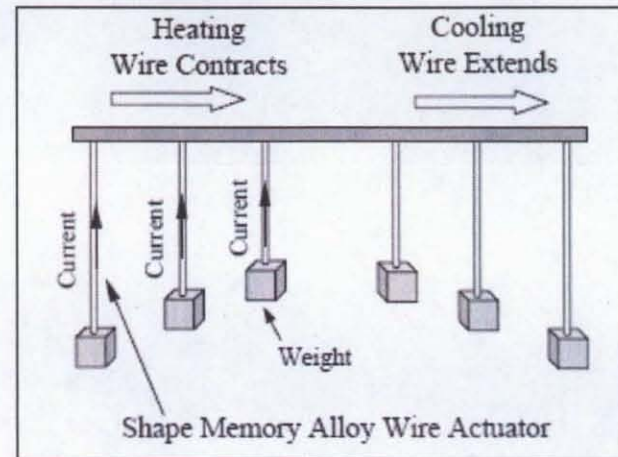
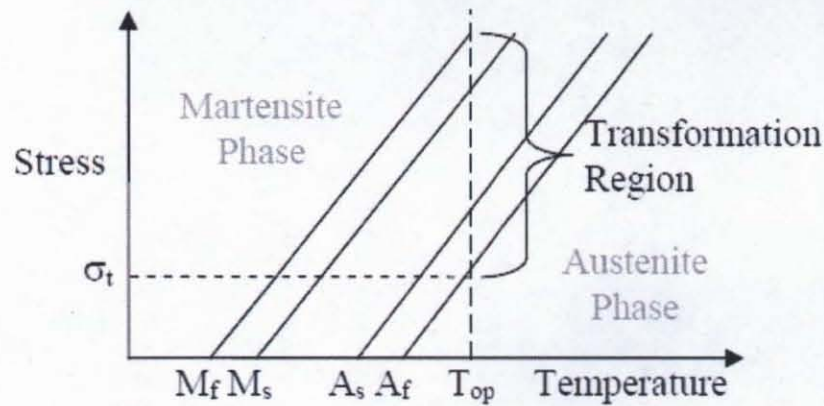
Zhu, Miller, Duffy, Ghosn – 2009

“High Temperature Damping Behavior of Plasma-Sprayed Thermal Barrier and Protective Coatings”  
 The 33rd International Conference on Advanced Ceramics & Composites





# Shape Memory Alloys



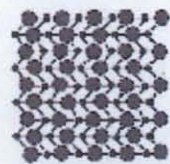
**Austenite**

- High temperature phase
- Cubic Crystal Structure

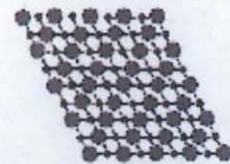


**Martensite**

- Low temperature phase
- Monoclinic Crystal Structure



Twinned Martensite



Detwinned Martensite

smart.tamu.edu  
Lagoudas

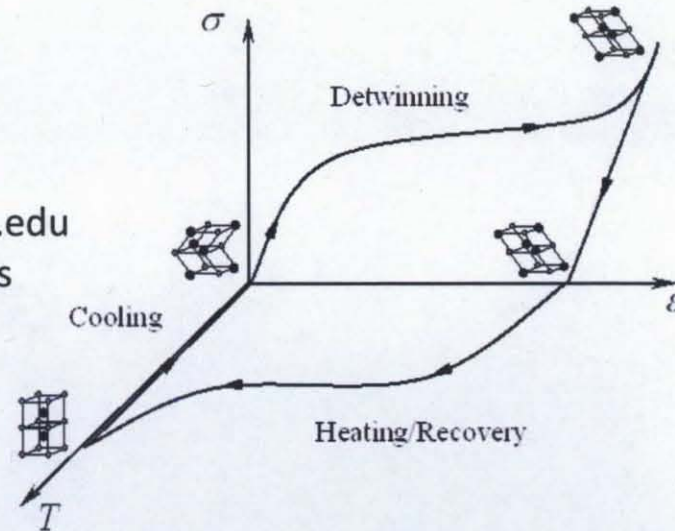


Figure 3. Schematic of a stress-strain-temperature curve showing the shape memory effect.

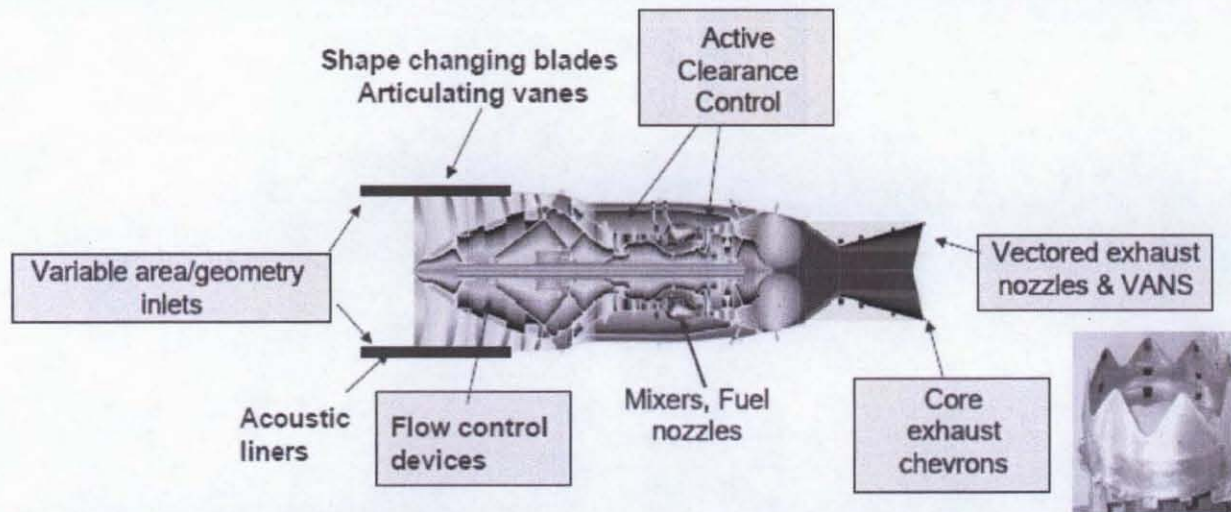
Figure 1. Different phases of an SMA.





# High-Temperature Shape Memory Alloys

High-Temperature Shape Memory Alloys are an enabling technology to a host of “smart” structures in jet engines



## Advantages of HTSMA

- High force per volume/weight - compact, lightweight
- Solid State - eliminates hydraulics, pneumatics, mechanical systems  
simple, frictionless, quiet, maintenance free
- Passive control - eliminates sensors, electronics
- Can be actively controlled for high-force, precision movements

“Characterization of a New Phase and its Effect on the Work Characteristics of a Near-Stoichiometric Ni<sub>30</sub> Pt<sub>20</sub> Ti<sub>50</sub> (at.%) High-Temperature Shape Memory Alloy (HTSMA)”, Garg et. al., Presentation at The International Conference on Shape Memory and Superelastic Technologies (SMST) 2008, 21-25 Sep. 2008; Stresa; Italy



# High-Temperature Shape Memory Alloys

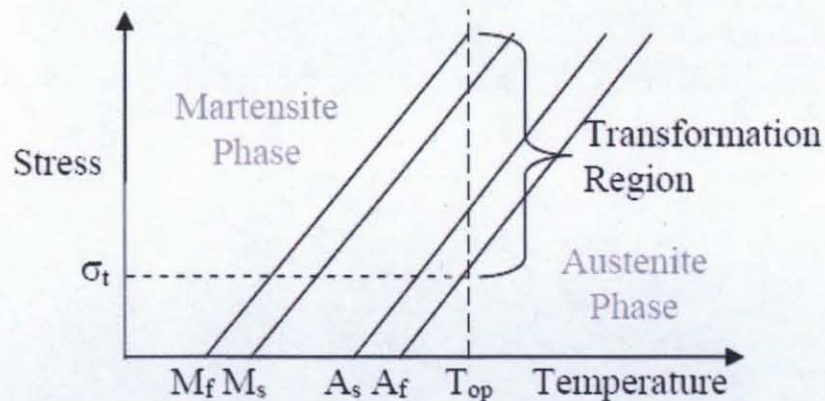
- HTSMAs
  - High temperature and force capability
  - Low frequency applications
- Potential engine applications
  - **Surge control rod for a centrifugal compressor – avoid instability**
    - “Development of a HTSMA-Actuated Surge Control Rod for High-Temperature Turbomachinery Applications” Padula et. al., 15th AIAA/ASME/AHS Adaptive Structures Conference; 23-26 Apr. 2007
  - **Supersonic inlet compression ramp – improve engine efficiency**
    - “Development and Test of an HTSMA Supersonic Inlet Ramp Actuator (Future of SMA)” Quackenbush et. al., Proceedings of the 15th SPIE Smart Structures/NDE Annual International Symposium, vol. 6930, 2008, paper 6930–25.
  - **Active blade tip clearance control – improve engine efficiency**
    - “Progress on Shape Memory Alloy Actuator Development for Active Clearance Control” DeCastro, Melcher, and Noebe, NASA-CP-2006-214383
  - **Adaptive exhaust chevrons – noise reduction**
    - “Benchtop Demonstration of an Adaptive Chevron Completed Using a New High-Temperature Shape-Memory Alloy” Noebe and Padula, NASA GRC 2005 Research and Technology Report





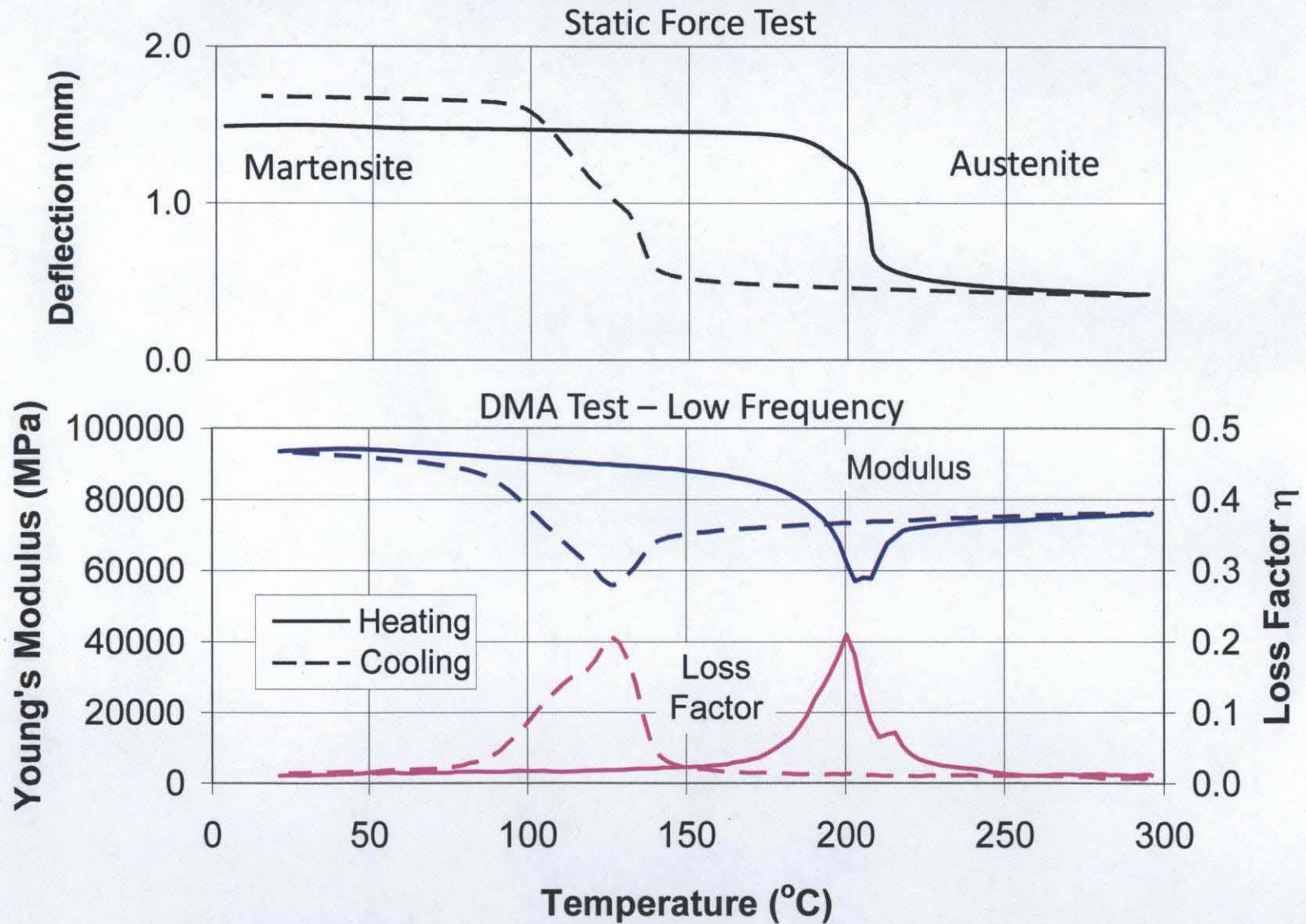
# Shape Memory Alloy Damping

- **NiTiHf samples tested for modulus and damping properties**
  - Looking for damping in phase-transition region
  - Purely passive damping properties
  - Damping is temperature-dependent
  - Tested using Dynamic Mechanical Analysis (DMA) at 0-300°C and at 0.1-200 Hz





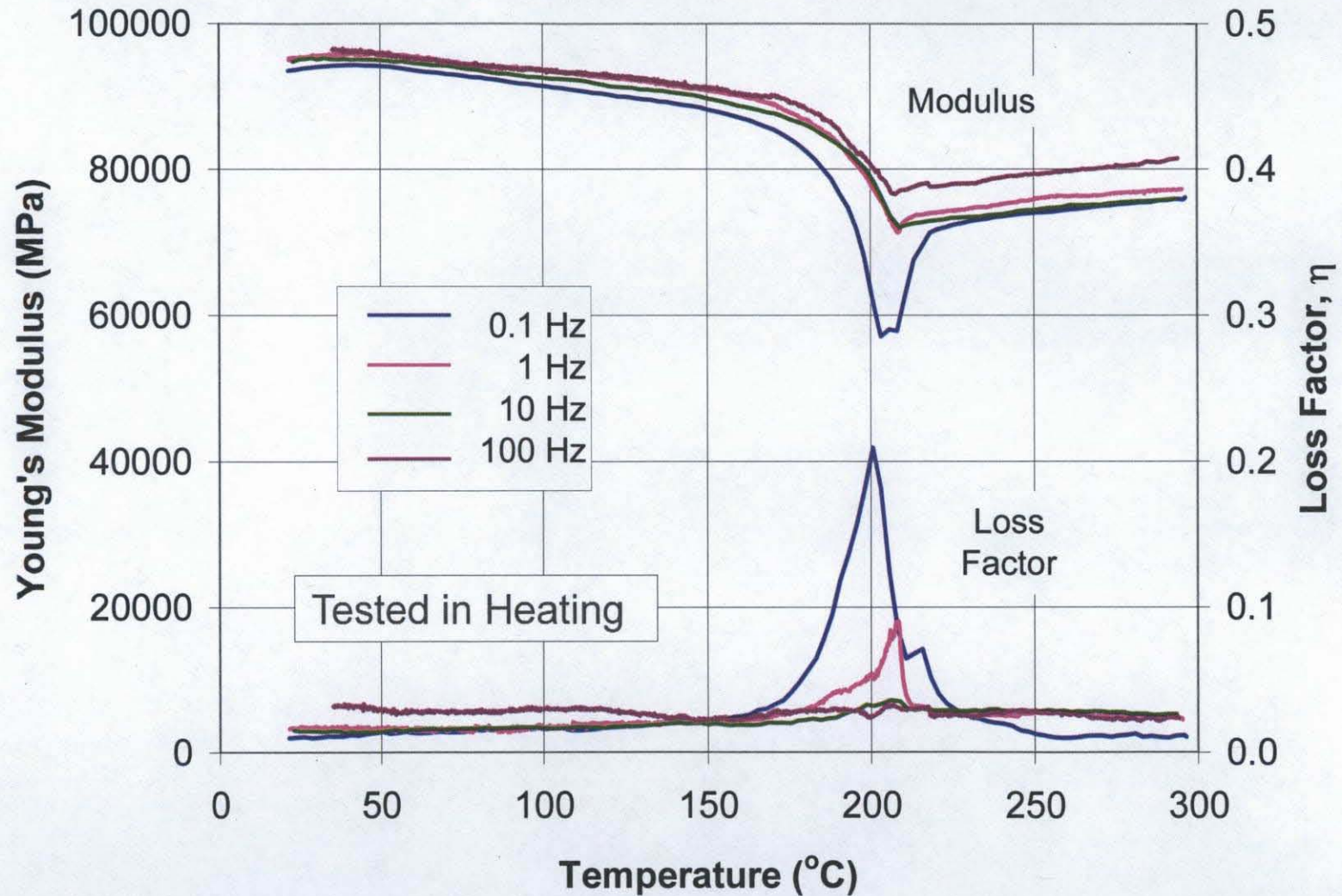
# Shape Memory Alloy Damping







# Shape Memory Alloy Damping





# Piezoelectric Materials

- High-temperature piezoelectric materials
  - Off-the-shelf high-temperature material – Type-II PZT –  $T_c = 350^\circ\text{C}$
  - NASA GRC-developed materials –  $T_c = 430^\circ\text{C}$
- Potential engine applications
  - **Active combustion control**
    - Mitigate thermo-acoustic instabilities and/or gas flow control to improve efficiency
  - **Synthetic jets for active flow control**
  - **Energy harvesting**
  
  - “High-Temperature Piezoelectric Material Developed” Sayir and Sehirlioglu, NASA GRC 2007 Research and Technology Report
  - “Doping of BiScO<sub>3</sub> -PbTiO<sub>3</sub> Ceramics for Enhanced Properties” Sehirlioglu, Sayir, and Dynys, Materials Science and Technology Meeting ASM/ACERS; 5-9 Oct. 2008; Pittsburgh, PA

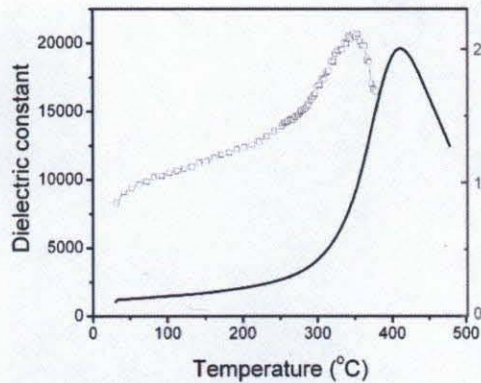




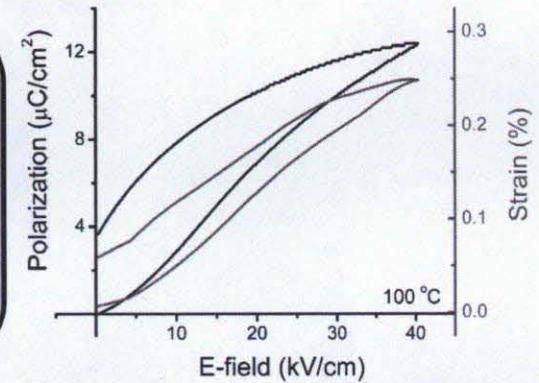
# High-Temperature Piezoelectric Material

• **Objective:** Piezoelectric material development for damping system for high temperature turbomachinery blade applications.

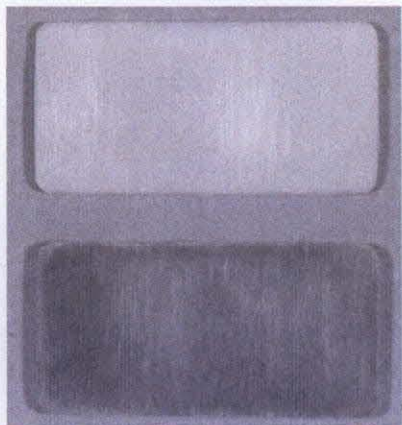
**Slip cast patches of GRC-63L composition developed and processed at NASA Glenn Ceramics Branch**



- ✓ Higher operating temperature
- ✓ Higher piezoelectric coefficient
- ✓ Higher Coercive field
- X Lower energy conversion efficiency



Material



Device



Comparison to the state of the art material						
PZT Type II by Piezo Kinetics, Inc	Temperature (°C)		Ferroelectric and Piezoelectric (100 °C)		Electromechanical coupling coefficients	
	Curie	Depoling	$E_c$ (kV/cm)	$d_{33}$ (pC/N)	$k_p$	$k_{31}$
GRC-63L	430	352	23	625	0.43	0.22
PZT-II	315	280	12	585	0.52	0.28

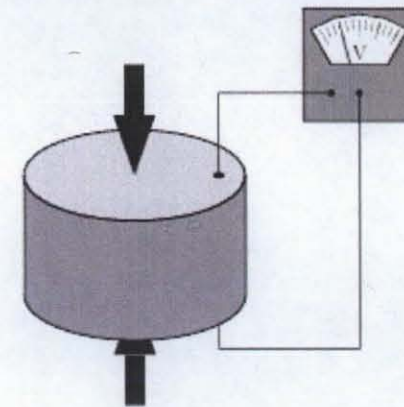




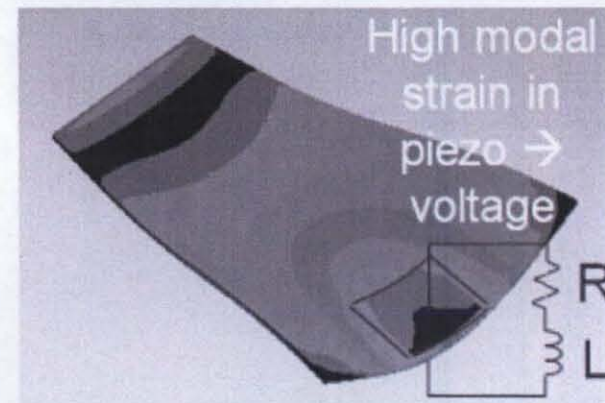
# Piezoelectric Damping

- **Concept:**

- Piezoelectric material under load produces an electric field
- Place piezoelectric material in an area of high modal stress in/on the blade
- **Passive damping technique** – place a shunt circuit across the piezo material to dissipate energy
- **Active vibration control** – use piezo materials as actuators and sensors with a control system to actively reduce vibration level



[www.wikipedia.org](http://www.wikipedia.org)

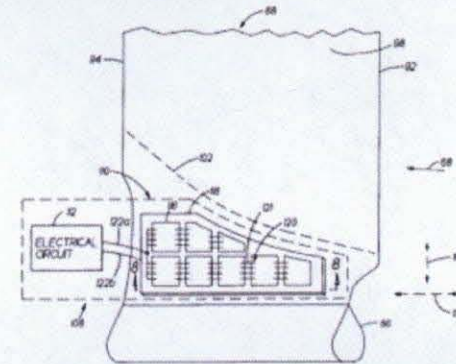






# Piezoelectric Damping

- Metal blades
  - Require machining to place piezoelectric material and circuits
  - Possible placement below blade platform
- Composite blades
  - Embed piezoelectric material between plies
  - Weave piezoelectric fibers into the plies – 15-250 micron diameters



Hilbert et. al. Patent 6,299,410



Fibers – Advanced Cerametrics Inc.



Kosmatka et.al.



# Piezoelectric Damping

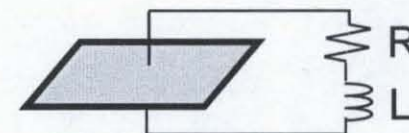
- **Resistive Circuit (R-Circuit)**

- *Energy dissipated through the resistor*
- *Broad frequency range, lower damping*



- **Tuned Resonant Circuit (RL-Circuit)**

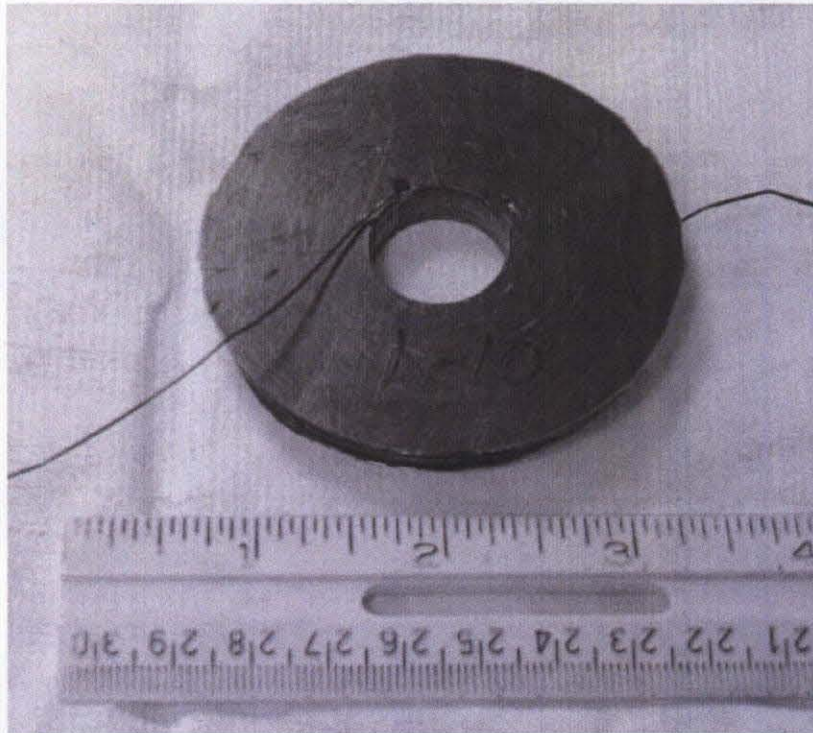
- *Tuned to resonance frequency through the inductor*
- *Higher damping at target frequency*
- *Inductor is a simple coiled wire*
  - ***fully passive***







# Piezoelectric Damping



Air-Core Inductor

**Optimal inductor for 700-800Hz**

**0.69 H wound inductor:**

- *34-gauge wire*
- *0.75-inch inner diameter*
- *2.6-inch outer diameter*
- *0.30-inch length*
- *510 W*
- ***Too large for blade application***

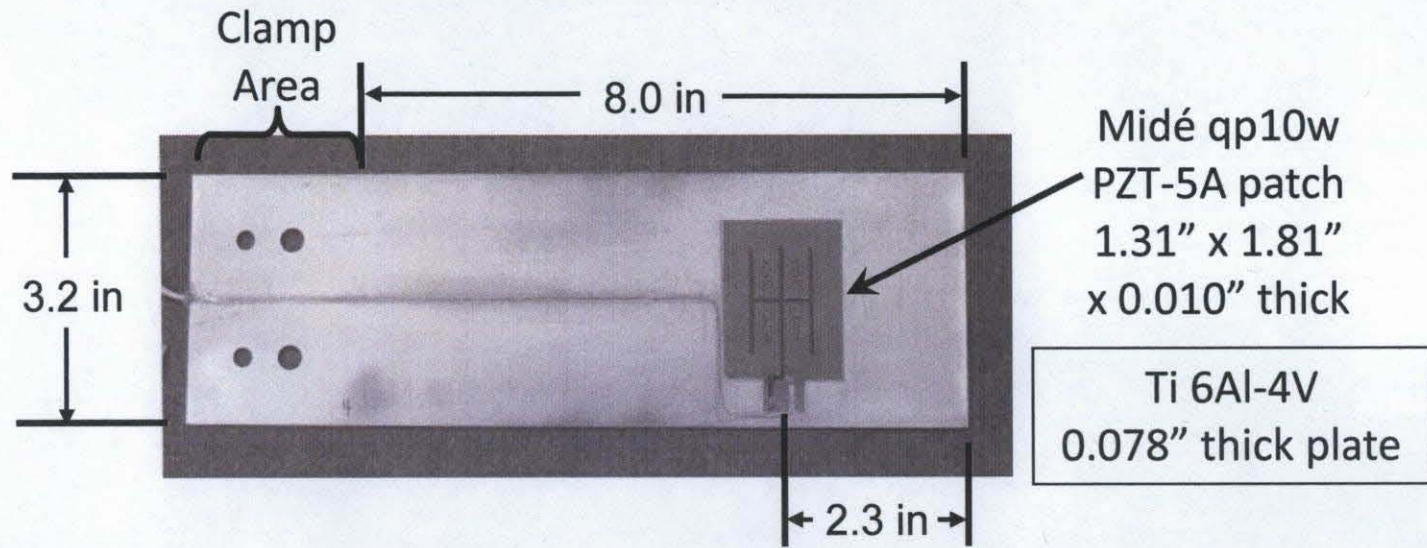
**Inductor size required for higher frequencies:**

- *2000 Hz – 0.1 H*
- *5000 Hz – 0.015 H*

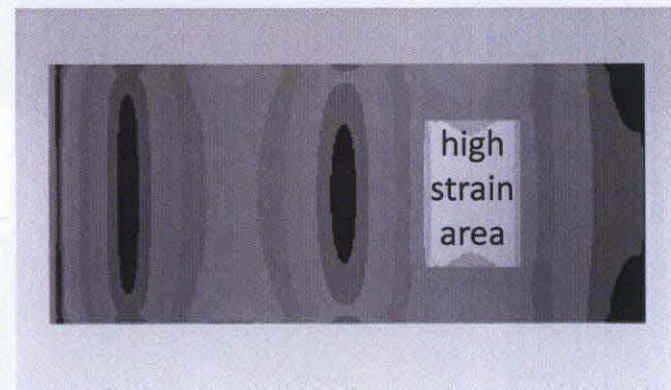




# Piezoelectric Damping



3B Mode – Modal Deformation

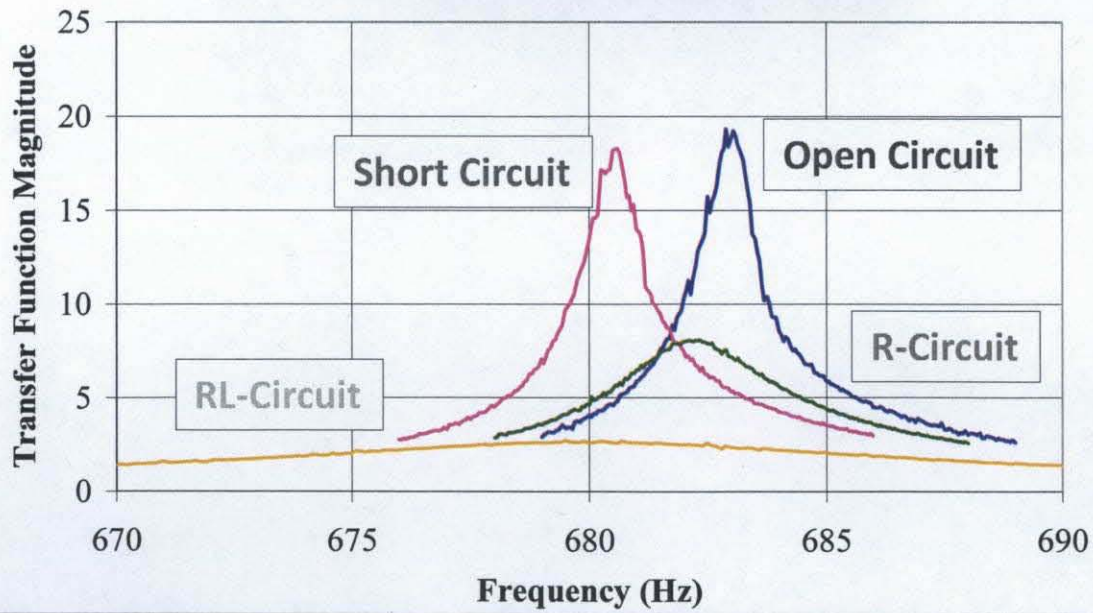
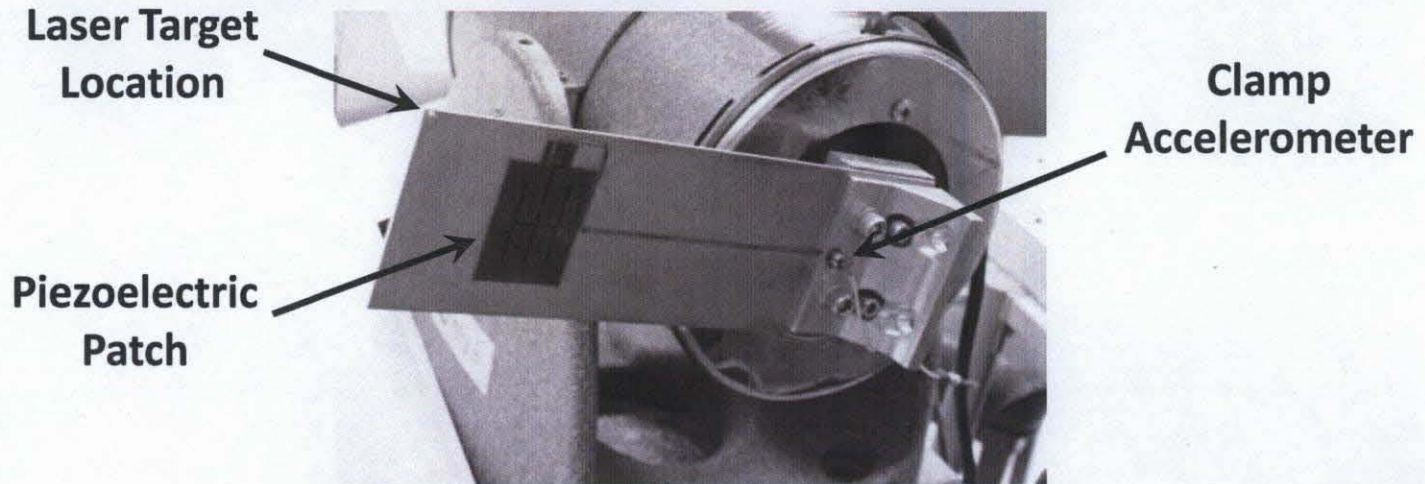


3B Mode – von Mises Modal Strain



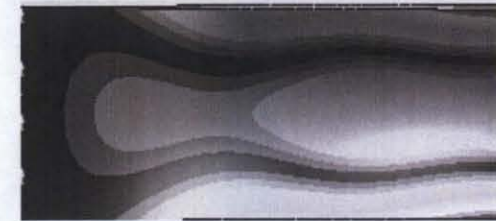
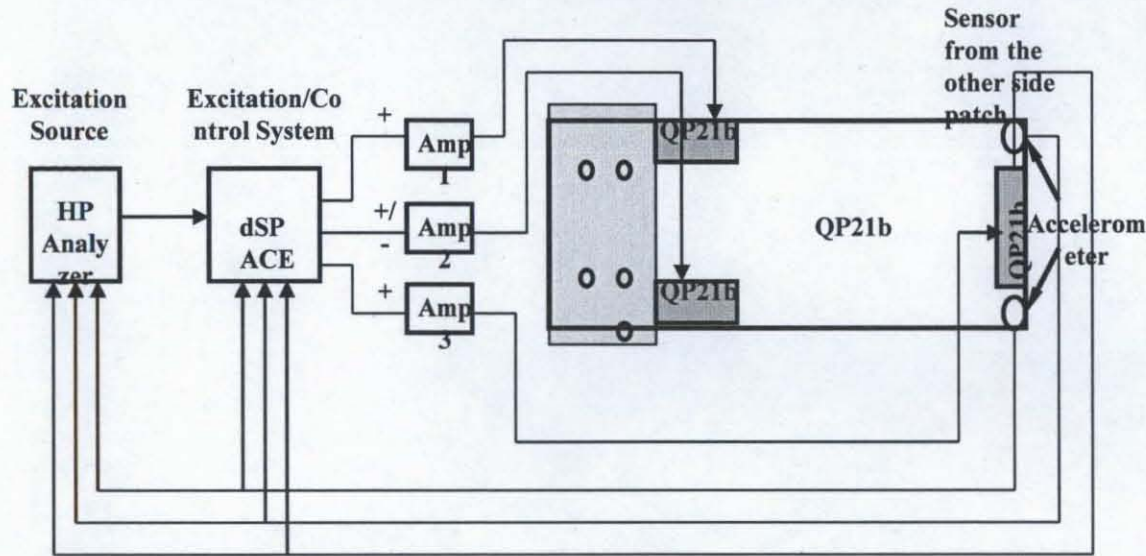


# Piezoelectric Damping



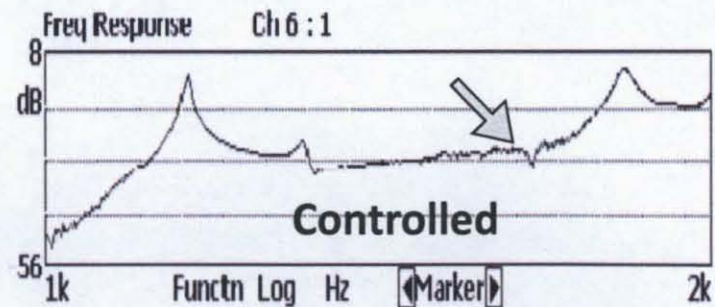
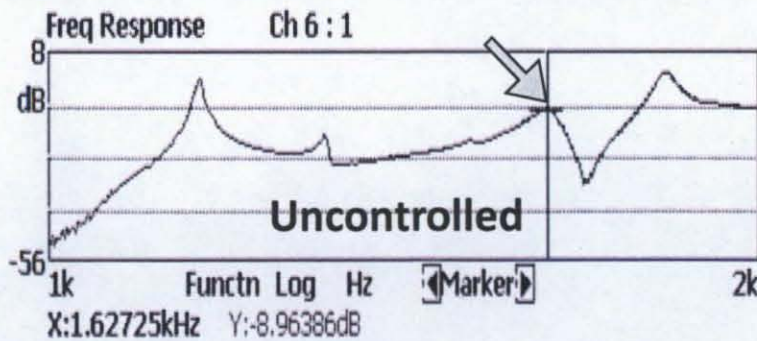


# Active Control with Piezoelectrics



2-Stripe Mode Shape

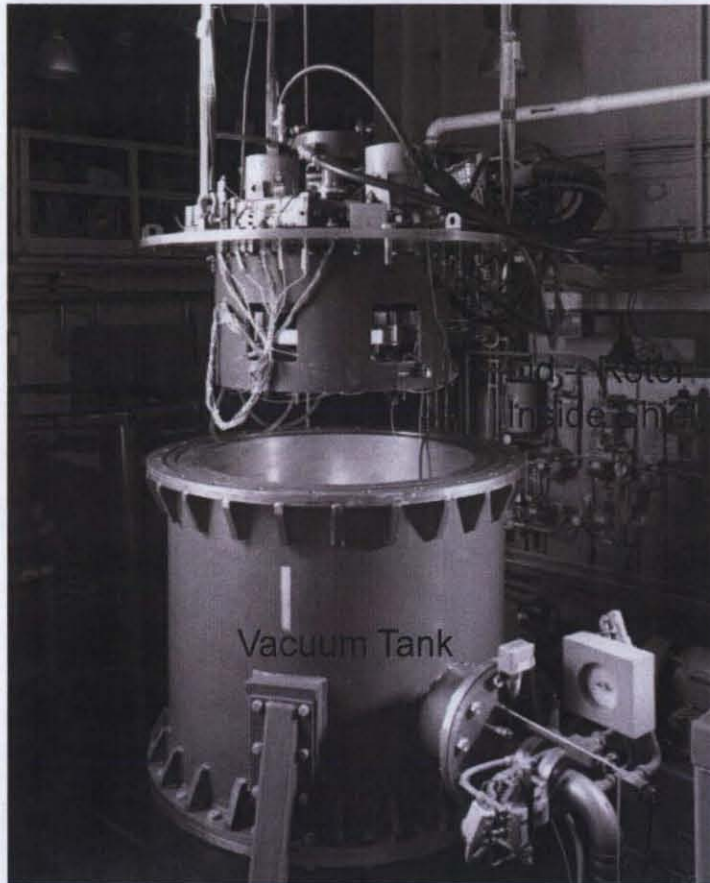
Ben Choi – NASA GRC



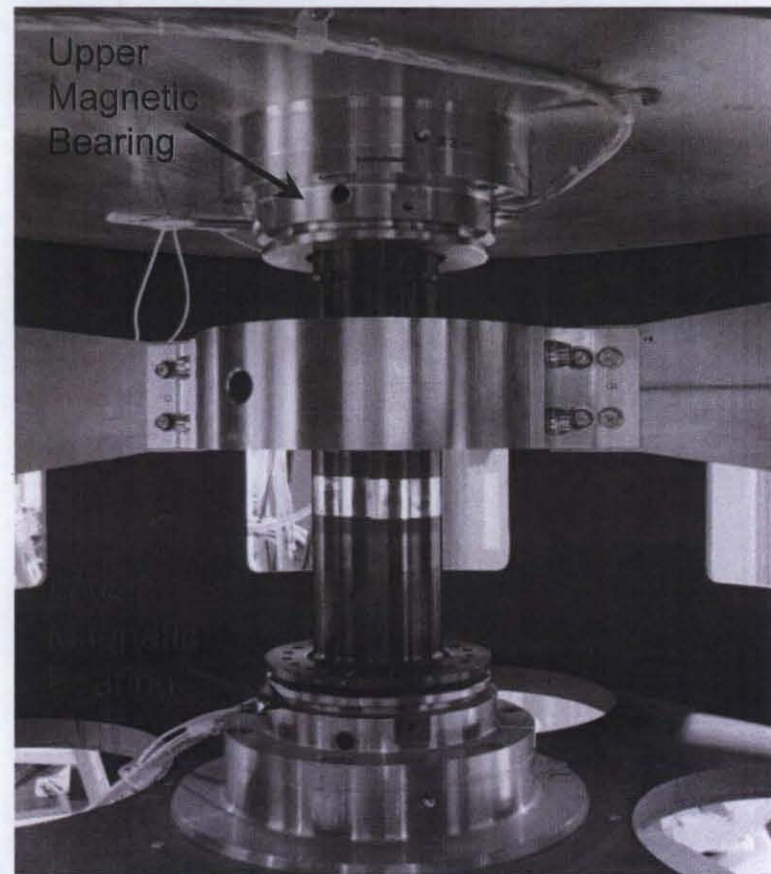




# Piezoelectric Damping



**Dynamic Spin Facility**

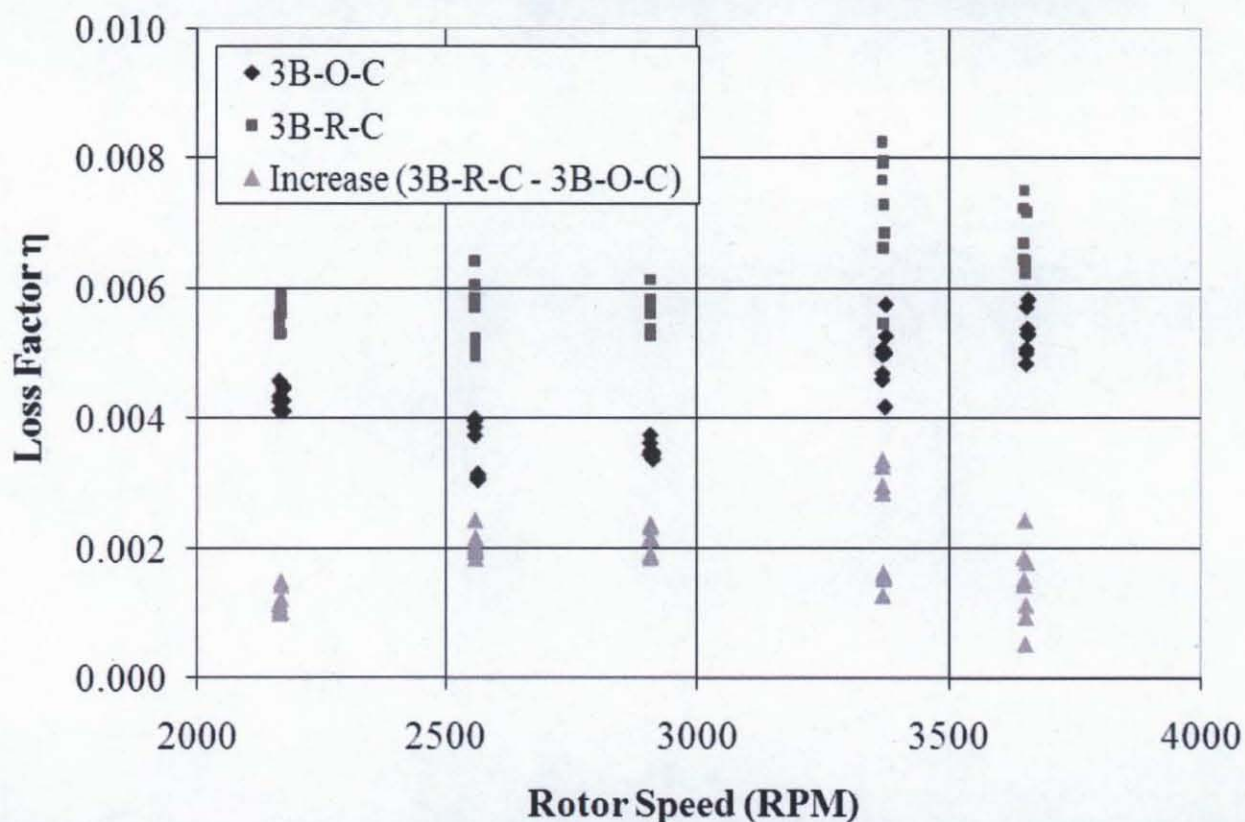


**Rotor with Tapered Test Plates**



# Piezoelectric Damping

## R-Circuit vs. Open Circuit Damping in Spin Rig



*Spin test:  $\Delta\eta = 0.0018$  (average based on tip displacement)*  
*Shaker test:  $\Delta\eta = 0.0025$  (based on tip velocity)*





# Current Research Plans

- Plasma-sprayed damping coatings
  - Measure modulus and damping of individual coatings
- HTSMA damping
  - SMA materials with less temperature hysteresis
  - SMA materials with phase transitions less frequency-dependent
- Piezoelectric damping
  - Application to metal blades
    - Continue spin testing of passive damping with tuned RL-circuit
    - Begin spin testing of actively controlled plates
  - Application to composite fan blades
    - Embedding piezoelectric materials/patches within composite blades
  - Trade studies
    - Determine potential weight savings for entire engine