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Abstract

Phase II data results of the Fundamental Inlet Bleed Experiments study at NASA Glenn Research Center are presented which include flow coefficient behavior for 21 bleed hole configurations. The bleed configurations are all round holes with hole diameters ranging from 0.795 to 6.35 mm, hole inclination angles from 20° to 90°, and thickness-to-diameter ratios from 0.25 to 2.0. All configurations were tested at a unit Reynolds number of $2.46 \times 10^7/\text{m}$ and at discrete local Mach numbers of 1.33, 1.62, 1.98, 2.46, and 2.92. Interactions between the design parameters of hole diameter, hole inclination angle, and thickness-to-diameter as well as the interactions between the flow parameters of pressure ratio and Mach number upon the flow coefficient are examined, and a preliminary statistical model is proposed. An existing correlation is also examined with respect to this data.

Nomenclature

A_b	bleed hole area defined normal to hole axis
A_{\min}	minimum area of bleed orifice
D	bleed hole diameter
g_c	proportionality constant
H_{inc}	incompressible shape factor
L	bleed hole length
M	Mach number
M_{blk}	nominal Mach number of wind tunnel fixed geometry convergent-divergent nozzle
M_{noz}	actual Mach number of wind tunnel fixed geometry convergent-divergent nozzle
N	number of bleed holes in a plate
P	static pressure
P_t	total pressure
\underline{Q}	sonic flow coefficient
R	gas constant
Re	Reynolds number
Re'	scaled Reynolds number ($Re \times 1.0 \times 10^{-7} \text{ m}$)
sccm	standard cubic centimeters per minute
t	bleed plate thickness
T_t	total temperature
w	mass-flow rate

Greek Symbols

α	bleed hole inclination angle
δ	boundary-layer thickness

δ_1	boundary-layer displacement thickness
γ	ratio of specific heats

Subscripts

0	pertaining to the wind tunnel plenum chamber condition
air	pertaining to air gas
<i>e</i>	pertaining to boundary-layer edge condition
<i>i</i>	pertaining to ideal conditions
<i>plen</i>	pertaining to the bleed plenum condition
wall	pertaining to wall condition

Superscripts

*	pertaining to choked conditions
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Introduction

Background

Boundary-layer control is an important topic in the design of supersonic inlets. In such an inlet, it is important to prevent flow separation and to control the effects of Shock-Wave/Boundary-Layer Interactions (SWBLI). The former can radically change the flow structure, while the latter can displace the shock wave pattern into a less efficient configuration. In addition, the terminal normal shock between the supersonic inlet and the subsonic diffuser is neutrally stable, and to ensure its placement, it is necessary to adjust the mass-flow rate reaching the diffuser in response to perturbations in the engine operation or inlet flow. It is possible to address all of these concerns with mass-flow removal via boundary-layer bleed wherein one or more regions of the inlet wall are porous to remove mass from the boundary layer. Thus, boundary-layer bleed decreases the mass-flow to the engine, mitigates the effects of adverse pressure gradients, and reduces the boundary-layer thickness, and thus, the SWBLI. Bleed configurations often are characterized by the sonic flow coefficient (Q), which is defined as:

$$Q = \frac{w}{w_i^*} \quad (1)$$

where the numerator is the measured mass-flow rate and the denominator is the ideal mass-flow rate under choked conditions:

$$w_i^* = \frac{(P_{t,e} \cdot A_b)}{\sqrt{T_{t,e}}} \cdot \sqrt{\frac{\gamma \cdot g_c}{R_{\text{air}}}} \cdot \left(\frac{\gamma + 1}{2} \right)^{\frac{-(\gamma+1)}{2 \cdot (\gamma-1)}} \quad (2)$$

The sonic flow coefficient is typically presented as a function of the ratio of bleed plenum pressure to freestream (boundary-layer edge) total pressure ($P_{plen}/P_{t,e}$). For the present study, the total temperature at the boundary-layer edge ($T_{t,e}$) is assumed to be the same as the total temperature in the wind tunnel plenum chamber ($T_{t,0}$).

A large library of flow coefficient data has been developed, beginning with McLafferty (Ref. 1), which was then expanded by Willis (Ref. 2). These collections are very configuration specific as they are multi-hole or slot configurations that only cover a limited range of hole/slot geometries and bleed-hole orientations. Davis (Ref. 3) showed that with two adjacent 90° holes, the flow coefficient at a choked condition can vary by as much as 6 percent depending on hole orientation. While Slater (Ref. 4) has developed a model for 90° bleed holes based upon the Willis data, that model should be compared with single hole data where there is no interaction between adjacent holes.

Fundamental Inlet Bleed Experiments (FIBE)

The need to develop a more comprehensive experimental database for model development was recognized by NASA Glenn Research Center (GRC) and as a result the Fundamental Inlet Bleed Experiments study (FIBE) was initiated. FIBE aims to create an experimental database to improve modeling of bleed systems through Computational Fluid Dynamics (CFD), as well as to improve supersonic and hypersonic inlets by examining alternate bleed configurations and placement. From 1994 to 1997, GRC conducted bleed research that has been summarized by Davis (Ref. 5). These studies included both single-hole and multi-hole bleed arrays and characterized the flow coefficient behavior as well as the effects of bleed on the boundary layer and on SWBLIs. In 2011 the project was restarted under FIBE with the goal of improving bleed models for CFD codes as well as examining the effects of various configuration parameters.

The FIBE project is being conducted in multiple phases. Phase I testing occurred between April 29, 2011 and September 13, 2011, as reported by Davis (Ref. 6). For Phase I, flow coefficient data were accumulated for a 20° and a 90° bleed hole, both having a hole length-to-diameter ratio of 2.0 (see Figure 1), at various Reynolds numbers and Mach numbers. Detailed approach boundary-layer profiles were also obtained. The primary conclusions of the Phase I testing were that the flow coefficient has little dependence on the Reynolds number, at least over the limited range investigated, and that static pressure scaling works reasonably well for the 90° hole but not for the 20° hole.

Phase II testing, which began on April 24, and ended on December 11, 2012, examines the effects of the following configuration parameters configuration variables:

- Hole inclination angle (α)
- Hole thickness-to-diameter ratio (t/D)
- Hole diameter-to-boundary-layer displacement thickness ratio (D/δ_1)

Reported herein are the results of the Phase II study.

FIBE Phase II Test Program

Test Hardware

Schematics of “thick” and “thin” bleed plates with reference parameters are shown in Figure 1. As noted in Reference 6, when the cosine of the inclination angle (α) is larger than the plate thickness-to-diameter ratio (t/D), the plate is considered “thin” and the minimum flow area exceeds the bleed hole area normal to the hole axis. For Phase II testing, the single-hole bleed problem was investigated with a Design Of Experiments (DOE) approach. With reference to Figure 1, the critical independent dimensions for the single hole were assumed to be the inclination angle (α), bleed hole diameter (D), and thickness-to-diameter ratio (t/D). While it is natural to consider the length-to-diameter ratio (L/D) rather than the thickness-to-diameter ratio, given that the angles and diameters of interest using length-to-diameter would have resulted in configurations with a very large, and impractical, range of thicknesses. Using these as design parameters for the bleed configurations, the ranges of acceptable values were determined based upon ranges likely to be encountered in engineering use. Applying DOE to these limits and their corresponding midpoints formed a face-centered experimental design with a center-point. Upon arriving at this design, however, the intermediate thickness-to-diameter ratios used in combination with the smallest hole diameter of interest were determined to have a thickness less than would be seen in engineering practice, and as such these configurations were neither constructed nor tested. In all, 21 test articles were fabricated with the specific dimensions given in Table 1. The resulting test configurations yielded four that would be considered to be “thin.” Two of these plates (106 and 306) have minimum flow areas approximately 7 percent higher than the bleed hole area and two (109 and 309) had minimum flow areas over twice the bleed hole area. For the smallest hole diameter ($D=0.794$ mm), the resulting plate thickness for the two smallest t/D was too thin to practically fabricate and test so only the thickest

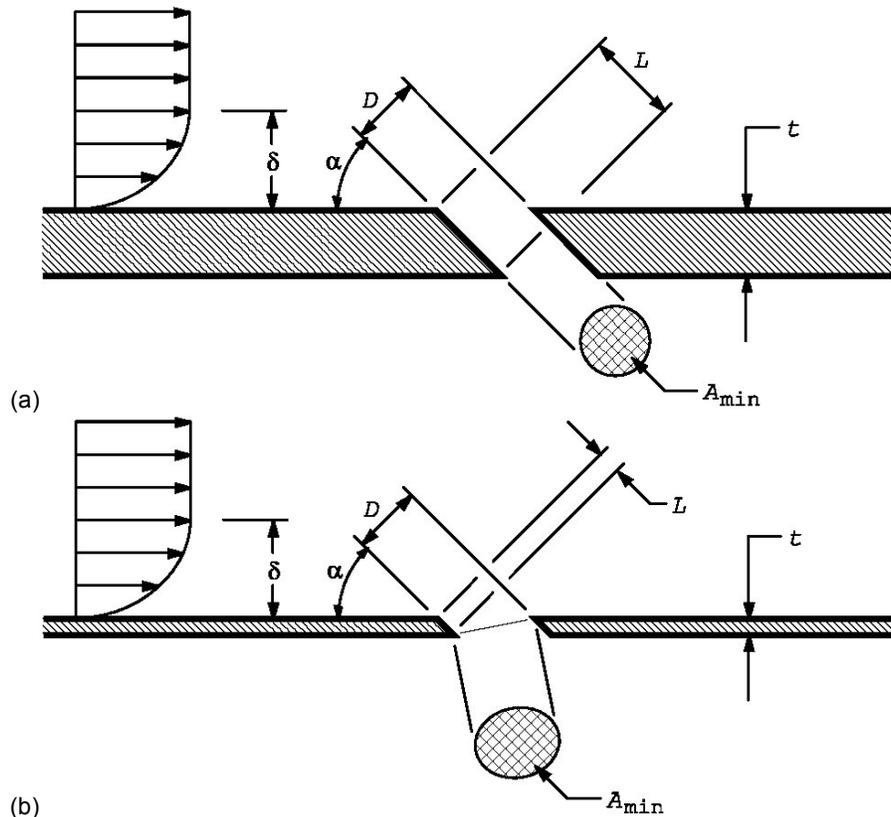


Figure 1.—Schematic of bleed holes. (a) “Thick” bleed plate. (b) “Thin” bleed plate.

TABLE 1.—PHASE II TEST ARTICLE NOMINAL DIMENSIONAL PARAMETERS

Config. No.	α (°)	D (mm)	t (mm)	t/D	L/D	N	A_{min}/A_b
101	90	6.350	12.700	2.000	2.000	1	1.0
102	90	6.350	7.144	1.125	1.125	1	1.0
103	90	6.350	1.588	0.250	0.250	1	1.0
104	55	6.350	12.700	2.000	2.442	1	1.0
105	55	6.350	7.144	1.125	1.373	1	1.0
106	55	6.350	1.588	0.250	0.305	1	1.1
107	20	6.350	12.700	2.000	5.848	1	1.0
108	20	6.350	7.144	1.125	3.289	1	1.0
109	20	6.350	1.588	0.250	0.731	1	2.3
301	90	3.572	7.144	2.000	2.000	3	1.0
302	90	3.572	4.018	1.125	1.125	3	1.0
303	90	3.572	0.893	0.250	0.250	3	1.0
304	55	3.572	7.144	2.000	2.442	3	1.0
305	55	3.572	4.018	1.125	1.373	3	1.0
306	55	3.572	0.893	0.250	0.305	3	1.1
307	20	3.572	7.144	2.000	5.848	3	1.0
308	20	3.572	4.018	1.125	3.289	3	1.0
309	20	3.572	0.893	0.250	0.731	3	2.3
1501	90	0.794	1.588	2.000	2.000	15	1.0
1504	55	0.794	1.588	2.000	2.442	15	1.0
1507	20	0.794	1.588	2.000	5.848	15	1.0

value ($t/D = 2.0$) was considered. Sufficient testing time was available such that all of the geometric configurations had at least one flow coefficient curve collected at each tunnel Mach number.

The test articles (bleed plates) used in Phase II differed in configuration from those used in Phase I. The round inserts used in Phase I created a potential problem with the impingement of the jet exiting the bleed hole on the inner surface of the insert when small inclination angles and thick plates were considered. To mitigate this problem, rectangular bleed inserts with longer axial spans were used. Figure 2 shows a comparison of the 108 configuration (see Table 1) incorporated into the Phase I and Phase II bleed inserts.

Like Phase I, the goal of Phase II is to determine the flow coefficient for various configurations of an isolated bleed hole. The objective here is to first understand the behavior of an isolated bleed hole and then later to look at the same hole configuration as part of an array with various porosities and hole spacings, in order to understand multi-hole interactions. For the present single-hole studies, the hole diameter varies by an order of magnitude which makes flow-rate measurement of a single small hole problematic. CFD performed at GRC, however, suggests that no interaction between holes will occur if the holes are placed in a single row spaced at least four diameters apart. Therefore, multiple holes spaced four diameters apart were used for all but the largest diameter as indicated in Table 1. There is a limit, however, to the number of holes that could be placed spanwise on the insert. Ideally, the total bleed hole area would be similar for each configuration and this is indeed true of the single and three-hole configurations. For the smallest hole diameter, only 15 holes could be placed in the plate resulting in a flow area of about 1/4 that of the other configurations. As described below, modifications to the mass-flow measurement system were made to accurately measure the reduced total flow through the smallest hole configurations. Figure 3 shows representative configurations of the single and multi-hole inserts.

Test Facility

FIBE Phase I and Phase II testing were conducted in the 15- by 15-cm Supersonic Wind Tunnel (SWT), which is a continuous flow facility with Mach number variation set by interchangeable fixed-geometry convergent-divergent (C-D) nozzle blocks. The current Mach number capability is $M=0.3$ to 0.8

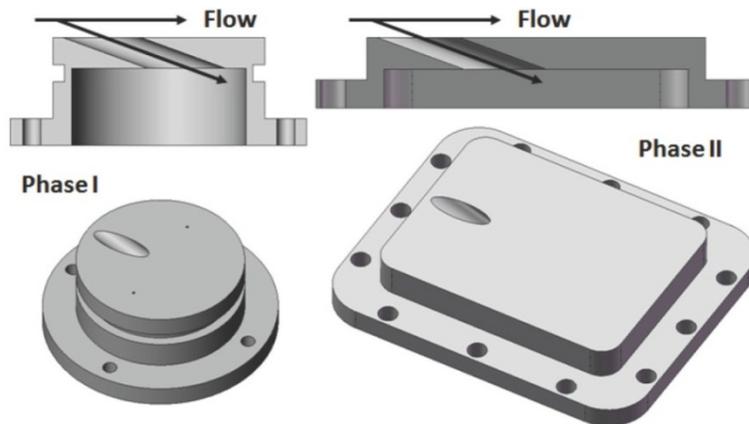


Figure 2.—Comparison of Phase I and Phase II test articles (Configuration 108 shown).



Figure 3.—Phase II single and isolated multi-hole test articles.

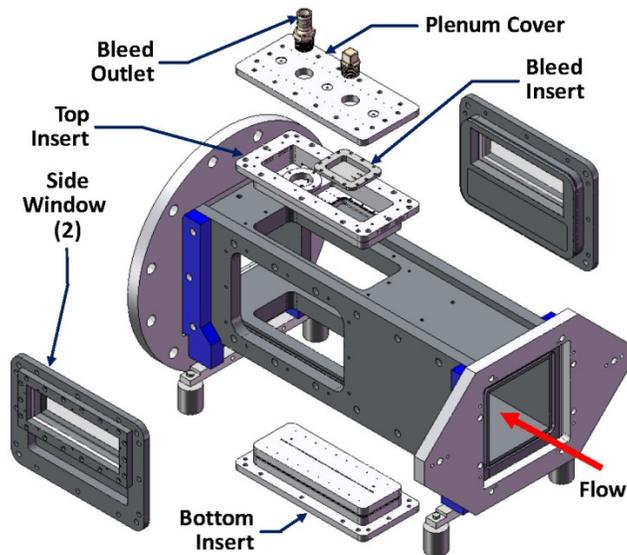


Figure 4.—Bleed setup in 15- by 15-cm SWT test section.

for subsonic operation and $M_{blk}=1.4, 1.7, 2.0, 2.5,$ and 3.0 for supersonic operation. The total temperature is nominally ambient. The wind tunnel is supplied with lab-wide 40 psig combustion air and exhausts to lab-wide Altitude Exhaust which is maintained below 13.8 kPa (2.0 psia). For Phase II, the wind tunnel was configured the same as Phase I except for the aforementioned change to the bleed plate insert.

The 15- by 15-cm SWT test section is configured to accept the test articles as shown in Figure 4. The top window insert of the test section is machined to accept the test articles shown in Figure 3. A cover plate is attached on the top of the window insert to form the bleed plenum. The bleed flow exhausts from the bleed plenum through a male barb fitting outlet that screws into the plenum cover plate. The side window inserts have schlieren glass installed for flow visualization and the bottom window insert has three rows of axial pressure taps. The location of the Phase II bleed plates relative to the reference boundary-layer profiles is the same as Phase I.

Instrumentation

The instrumentation used for Phase II is essentially the same as used in Phase I (see Ref. 6). For the present study, the primary measurement of interest is the bleed mass-flow rate. The bleed mass-flow rate is measured by the method of mixtures (Ref. 7), where the mixer gas is methane and its concentration is measured with a Flame Ionization Detector (FID). Details of the bleed mass-flow measurement system and flow equations are given in Reference 6, but the basic operation is to seed the bleed-flow with a trace amount of a hydrocarbon gas, in this case methane, allow the bleed air and methane to thoroughly mix, and then measure the concentration of methane in the mixed bleed-flow. Knowing the methane flow-rate and the mixed-flow methane concentration allows one to calculate the bleed air flow rate. This mass-flow measurement technique is particularly suited to bleed studies since it is scalable to any flow rate simply by changing the range of the hydrocarbon gas flow controller and doesn't rely on a clean uniform flow at the measurement station. Between Phase I and Phase II testing, several improvements to the system were incorporated including:

1. Addition of a second sample pump in series to allow data accumulation at lower bleed plenum pressures.
2. Tweaks to the sample flow-rate regulation system to ensure a more consistent sample flow-rate to FID.
3. Addition of 10 and 1000 sccm methane flow controllers to the existing 100 sccm unit to allow for more accurate measurement over a wider range of bleed flows.

Operating Conditions

Data were accumulated at nominal Mach numbers of 1.4, 1.7, 2.0, 2.5, and 3.0. The results of Phase I testing indicated only a weak Reynolds number dependence so the Phase II data were accumulated at only the highest Reynolds number, namely, $2.46 \times 10^7 / \text{m}$ ($7.50 \times 10^6 / \text{ft}$). Thus, there were a total of five different conditions tested. The five operating conditions are summarized in Table 2. For consistency, the operating condition number assigned is the same as designated in Phase I. Also in Table 2 is the actual Mach number calculated at the nozzle exit plane as well as the local boundary-layer edge Mach number measured at the boundary-layer measurement plane. The distance from the nozzle exit to the boundary-layer measurement plane is 36.36 cm (14.32 in) so that the edge Mach number is slightly below the nozzle exit Mach number.

TABLE 2.—TEST OPERATING CONDITIONS ($Re' = Re \times 1.0 \times 10^{-7} \text{ m}$)

Cond. No.	M_{blk}	Re'	M_{noz}	M_e	δ (mm)	δ_1 (mm)	H_{inc}
003	1.4	2.46	1.389	1.333	13.2	2.37	1.323
006	1.7	2.46	1.679	1.618	12.3	2.41	1.320
009	2.0	2.46	1.993	1.971	12.1	2.66	1.320
012	2.5	2.46	2.506	2.463	13.1	3.44	1.311
015	3.0	2.46	3.035	2.960	12.2	3.78	1.306

Results and Data Analysis

Overview

Sonic flow coefficient curves were collected for each plate at the five operating conditions and over the complete range of the mass-flow measurement apparatus. As such, each data point represents a unique combination of several unique parameters; the sonic flow coefficient (Q), the plenum pressure ratio ($P_{plen}/P_{t,e}$), the Mach number (M), the bleed hole diameter-to-boundary-layer displacement thickness ratio (D/δ_1), the thickness-to-diameter ratio (t/D), and the hole inclination angle (α). Given that it is likely that Q is dependent on the other five parameters, the multiple interactions create significant difficulties in data presentation. The thickness-to-diameter ratio, and the hole inclination angle are constant for a given plate, but the plenum pressure ratio and diameter-to-boundary-layer displacement thickness ratio are both dependent on Mach number. In previous work, such as Davis (Ref. 6) and Willis (Ref. 2), it has been shown that flow coefficient curves are largely self-similar for a bleed plate configuration and as such multiple Mach numbers are easily plotted on the same graph.

The most noticeable characteristic as a result of changing a single parameter is that of varying the hole inclination angle. Figure 5 presents the changes observed by maintaining a constant nominal diameter and therefore nominally constant diameter-to-boundary-layer displacement thicknesses for each Mach number. As shown in previous work (Refs. 2 and 6), the change in hole angle (moving down the columns of plots) results in a vastly different apparent shape between a 90° and a 20° hole. Interestingly, an examination of the 55° hole yields a shape similar to that of a 90° hole while showing a moderate increase in the maximum sonic flow coefficient. Further, the plenum pressure ratio where the flow unchokes is very near that of the 90° hole. For all bleed configurations, an increase in Mach number resulted in a curve that was scaled down from the previous ones, however for the 20° holes there is some impact on the rate of change near the point at which the flow becomes unchoked. Figure 5(g) shows that as Mach number increases, the curvature in unchoking the hole transitions from a smooth change in slope to a sharp cusp. Further, like some previous data (Ref. 2), the 20° case shows a decreasing pressure ratio as the sonic flow coefficient drops. This region of the flow curve beneath the choked value for the 20° plates exhibited large fluctuations in the plenum pressure ratio; the value shown being a numerical average over a 30 sec time period.

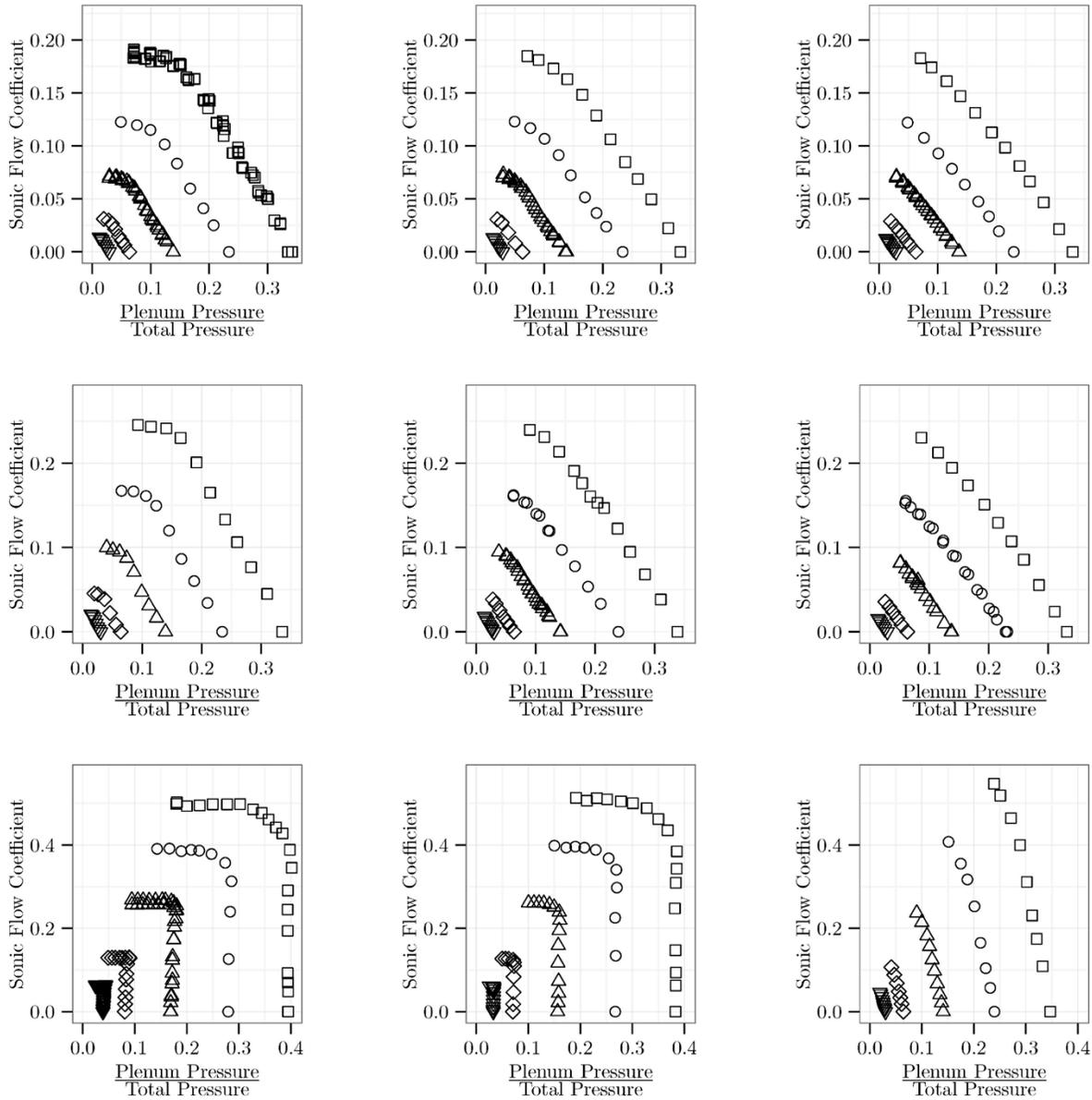


Figure 5.—Flow coefficient curves of selected plates at a constant nominal diameter of $D=6.35$ mm. Nominal Mach numbers: \square - 1.4, \circ - 1.7, \triangle - 2.0, \diamond - 2.5, ∇ - 3.0.

The effect of variance in thickness-to-diameter ratio, and thus the length-to-diameter ratio, is also illustrated in Figure 5. Reducing the thickness (moving right across the plot rows) changes the character of the curves. In particular, the critical point where the curve begins to plateau to a choked condition occurs at a lower pressure ratio. For the 20° hole, the entire curve shifts to a lower pressure ratio. Although the effect of the marginally larger minimum area of plate 106 (Figure 5(f)) cannot be readily discerned, the effect of the significantly larger minimum area of plate 109 is easily discerned whereby the peak value exceeds the thicker plates choked value and shows only a small degree of turning towards a plateau. Unfortunately, the current vacuum pump is not capable of choking all the bleed plate configurations.

Figure 6 examines the effect of changes in hole diameter at the largest thickness-to-diameter ratio. Although the primary interaction variable of interest here is the diameter-to-boundary-layer displacement

thickness ratio, it should also be noted that the length-to-diameter ratio varies (increases) as the inclination angle is reduced. Starting with the 90° hole (moving down the left column of plots), there is little change in the flow coefficient between the two larger holes. For the smallest hole, however, there is a significant increase in the flow coefficient which becomes more pronounced as the Mach number is reduced. It is speculated that the reason for this is the smallest hole size draws off flow at a much lower Mach number and thus does not have the shock losses inside the hole that are associated with larger holes. The trend of increasing flow coefficient with decreasing Mach number is consistent with the increasing thickness of the sonic layer as the Mach number is reduced. For the 55° hole (middle column of plots), the shock losses would be somewhat reduced compared to the 90° hole and there is observed a consistent trend of slightly increasing flow coefficient with decreasing hole size. For the 20° hole (right column of plots), the shock losses are minimized and the trend is reversed with the larger holes capturing higher momentum flow that does not experience the shock turning losses of the holes with higher inclination angles.

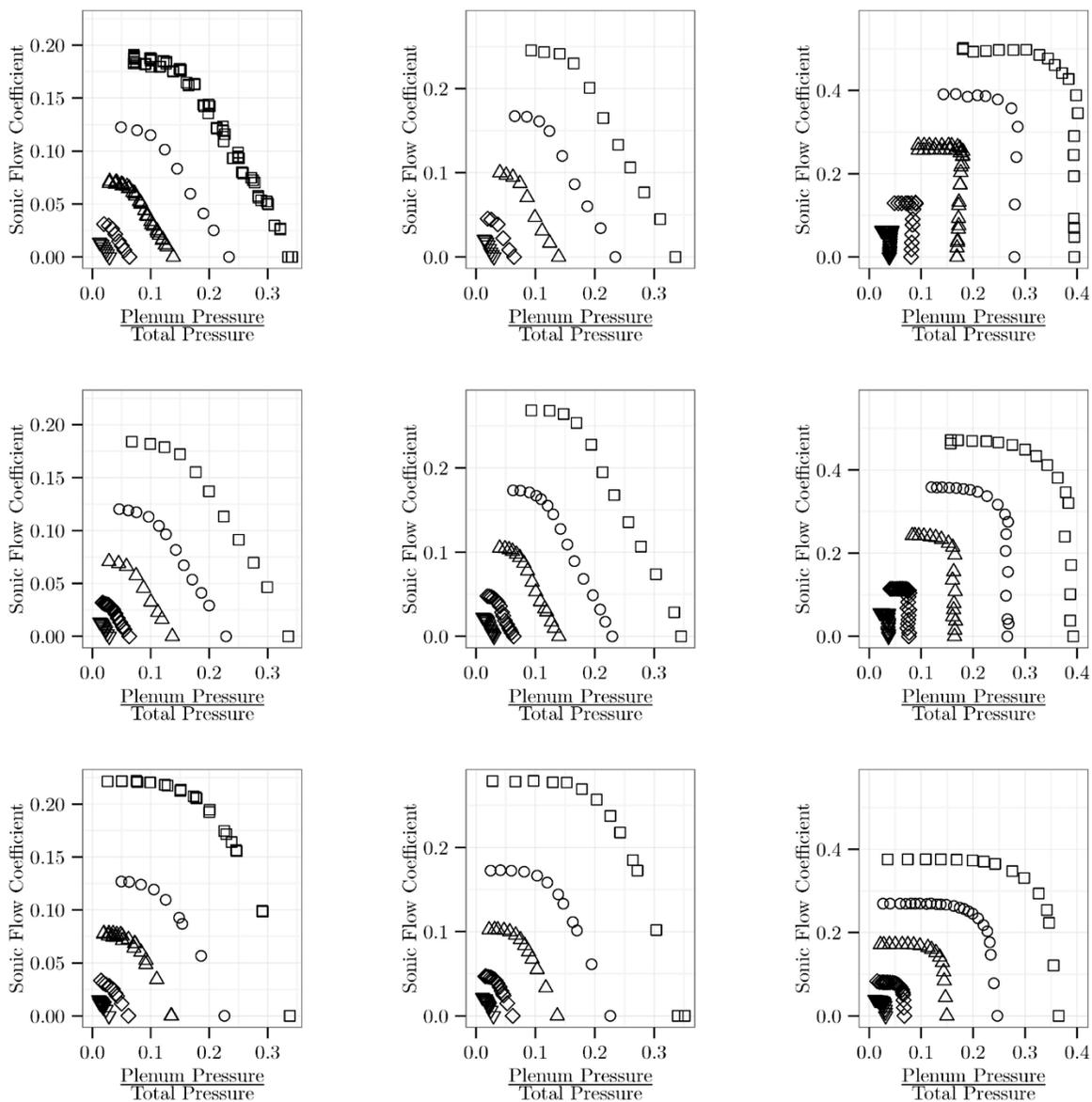


Figure 6.—Flow coefficient curves of selected plates at a constant thickness-to-diameter ratio of 2.0. Nominal Mach numbers: \square - 1.4, \circ - 1.7, \triangle - 2.0, \diamond - 2.5, ∇ - 3.0.

The similarity of a given configuration across Mach number has led the authors of previous works to consider scaling the sonic flow coefficient and plenum pressure ratio so as to collapse the data to a single distribution. Davis (Ref. 6) concluded that the scaling method presented by Slater (Ref. 4) was a better, but imperfect, fit for single-hole data than the scaling method Davis has previously proposed based upon a semi-empirical correlation of the data collected by Willis. As such, the data can be roughly collapsed by scaling the flow coefficient and plenum pressure ratio to be:

$$P_{plen,scaled} = \frac{(P_{plen}/P_{t,e})}{(P_{wall}/P_{t,e})} = \frac{(P_{plen}/P_{t,e})}{\left(1 + \frac{\gamma-1}{2} M_e^2\right)^{\frac{-\gamma}{\gamma-1}}} \quad (3)$$

$$Q_{scaled} = \frac{Q}{(P_{wall}/P_{t,e})} = \frac{Q}{\left(1 + \frac{\gamma-1}{2} M_e^2\right)^{\frac{-\gamma}{\gamma-1}}} \quad (4)$$

The above wall static pressure scaling assumes that the total pressure in the hole is nearly the same as the surface wall static pressure. This is likely a reasonable assumption for holes with large inclination angles as all the freestream total pressure is lost turning the flow through a large angle. As the inclination angle is reduced, however, some of the freestream total pressure is expected to be recovered in the hole and it is thus expected that the above scaling will not work as well, particularly at high flow rates. This suggests that a physics-based model must account for the total pressure recovery in the hole which may be a function of a number of parameters.

Several examples of collapsed data using the equations above for specific bleed holes are given in Figure 7. Unlike the data collected by Davis (Ref. 6), the data from many of these plates collapse very well when this scaling is applied. Of particular note are plates with the smallest nominal thickness-to-diameter ratio ($t/D=0.25$), Figure 7(a) to (c) (top row of plots), which collapse very well independent of hole angle. That these plates collapse well isn't necessarily surprising inasmuch as very thin plates do not have the same internal shock structure as thicker plates do. Figure 7(d) to (f) (middle row of plots) display the collapse for hole configurations where the nominal thickness-to-diameter ratio is 2.0 and the hole angle is 55° and in this case the collapse appears to have higher degree of scatter, however there is little apparent trend in Mach number. The final selection, Figure 7(g) to (i), present the 20° hole data and as Davis (Ref. 6) concluded, the scaling does not work particularly well for 20° holes. These have a distinct difference in magnitude where the maximum scaled sonic flow coefficient increases with Mach number. Further this tendency is related to the hole diameter as the smaller hole diameters show less separation between the curves.

A comparison of all collapsed data is shown in Figure 8. The values for the 20° holes are noticeably larger than those of the 90° and 55° holes which themselves form two distinct groups. The 90° holes seem to form tight bands for specific thickness-to-diameter ratios, however both the 55° and 90° holes only show a loose grouping where that ratio is small.

Existing Correlation

As the data were collapsed per the method proposed by Slater (Ref. 4), it is worthwhile to consider that the correlation he proposed was for a bleed configuration that was most similar to the current Plate 102. As shown in Figure 9. The correlation is similar but exact neither in maximum scaled sonic flow coefficient nor in predicting the shape of the curve. As the correlation is based upon the data of Willis (Ref. 2), which is for a multi-hole configuration, some variance is expected as a result of hole-to-hole interactions.

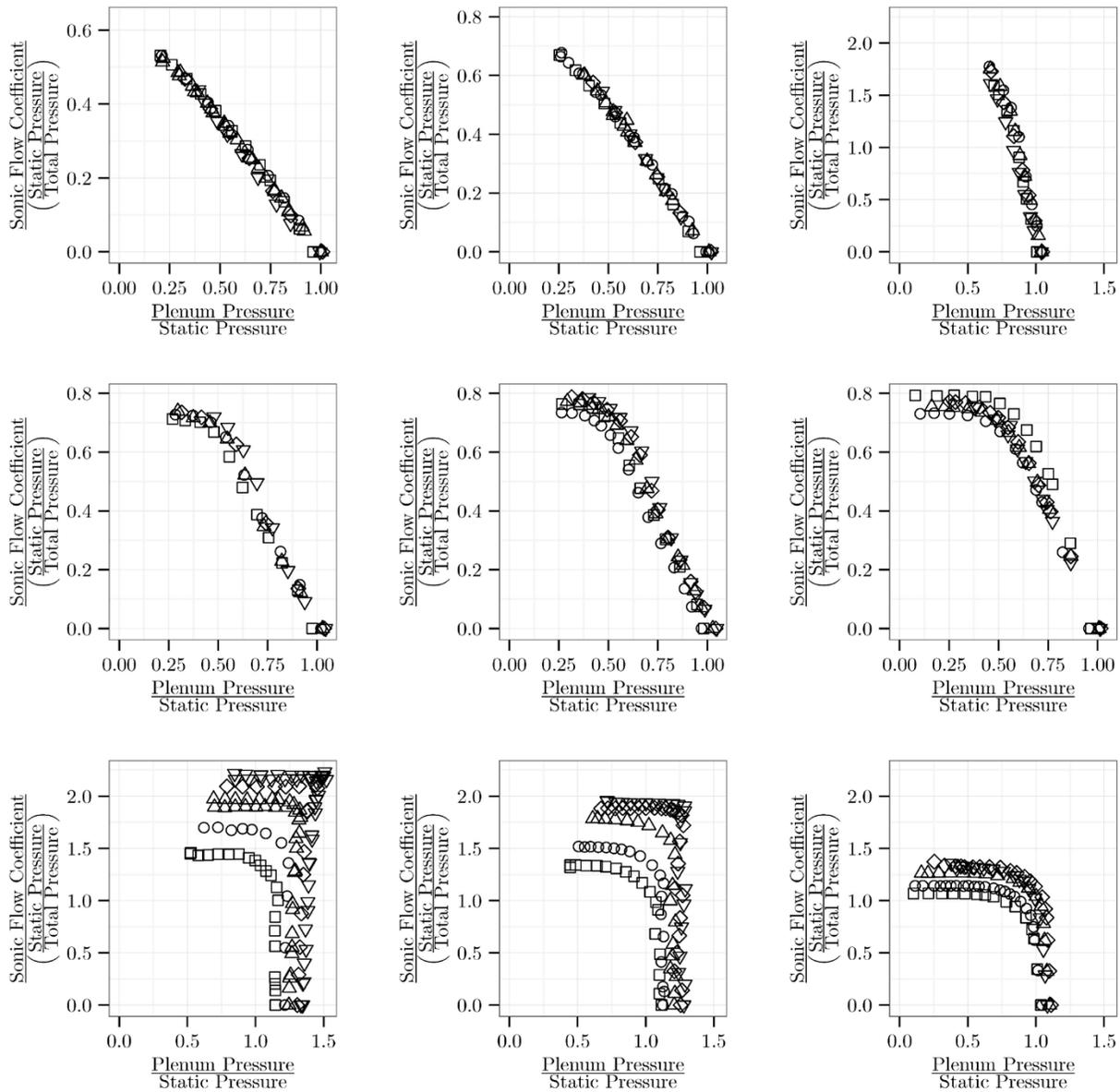


Figure 7.—Flow coefficient curves of selected plates collapsed by pressure ratio. Nominal Mach numbers: \square - 1.4, \circ - 1.7, \triangle - 2.0, \diamond - 2.5, ∇ - 3.0.

Statistical Fit

As the previous correlation is insufficient to describe the breadth of the data collected, a preliminary statistical fit of the data was determined. As the 20° data included a region of large flow instability and lacks a functional form in pressure ratio at high Mach numbers, the 20° data was excluded from the model. A theoretical model may be needed to include the 20° data. The remaining data was considered with the dependent variable as the scaled sonic flow coefficient and the independent variables of scaled plenum pressure ratio, Mach number, hole inclination angle, diameter-to-boundary-layer displacement thickness ratio, and thickness-to-diameter ratio.

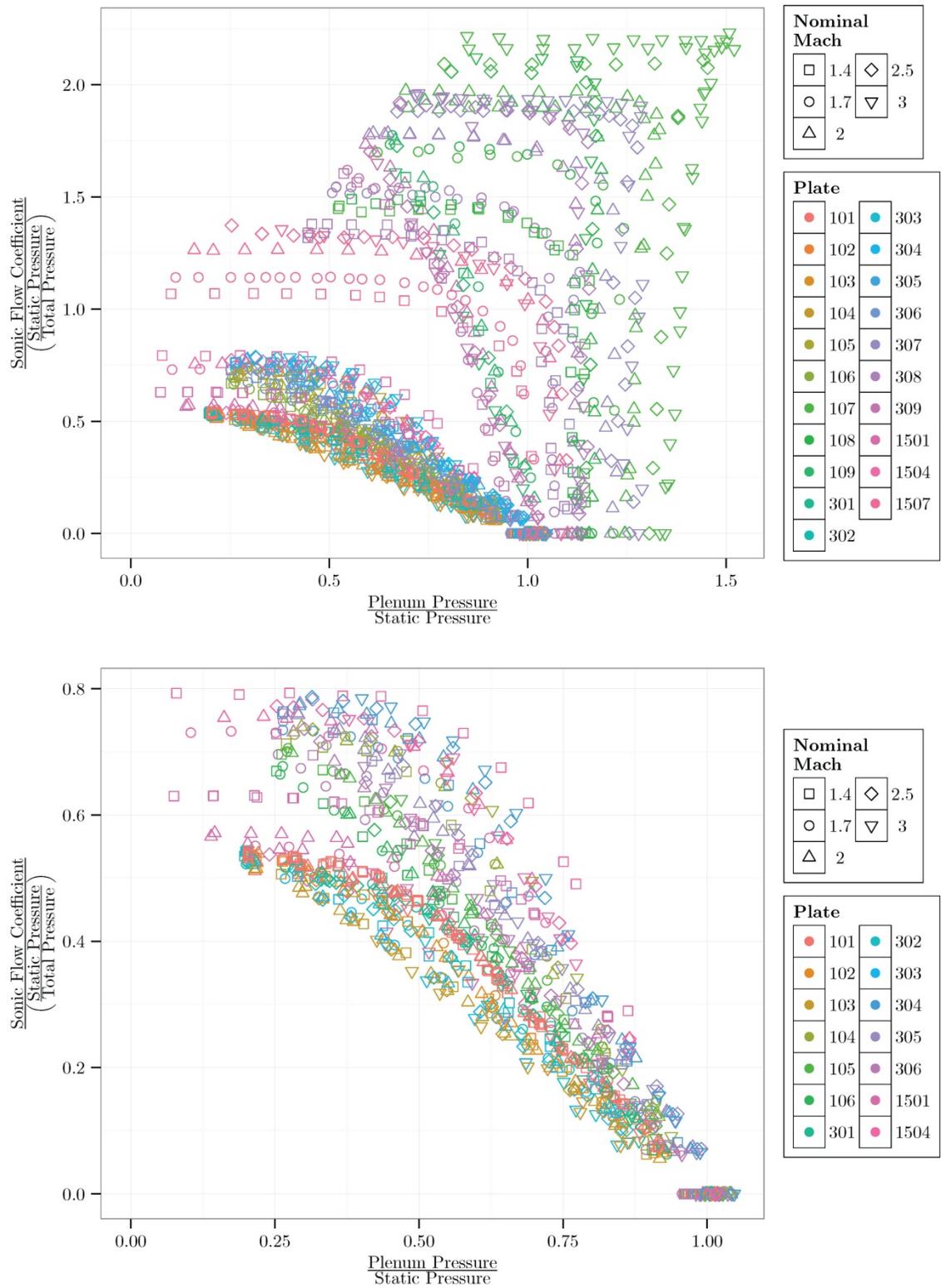


Figure 8.—Collapsed flow coefficient curves for all flow conditions.

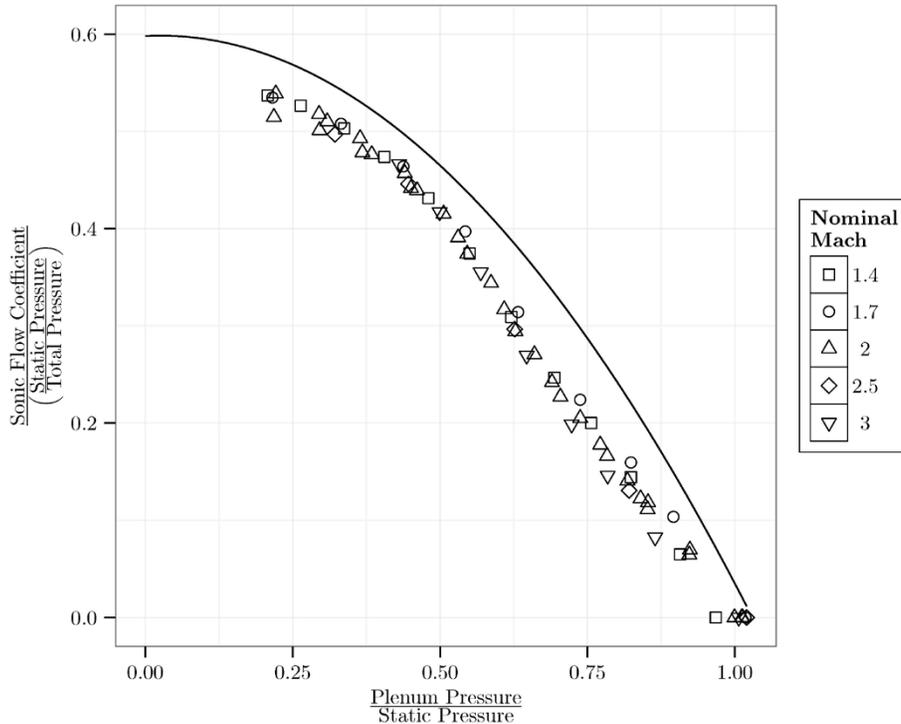


Figure 9.—Comparison of the Slater correlation to bleed configuration 102.

Three different statistical models were calculated, all were based upon a cubic in scaled plenum pressure and linear interactions in the other independent variables. The first model was a full interaction with 64 coefficients. This model was cumbersome, but has a multiple r-squared error of 99.11 percent. A reduced term model considering only first order interactions had 26 coefficients and a multiple r-squared error of 98.80 percent. Graphically, it was observed that this model deviated somewhat from the data and the full interaction model. An intermediate model was then considered using selected interactions where it was possible to develop a model with 43 coefficients that has a multiple r-squared error of 99.05 percent and that exhibited a negligible difference graphically from the full interaction model. The residual standard error for this model is 0.02185 on 972 degrees of freedom. The equation for the model is given as:

$$Q_{\text{scaled}} = \sum_{i=1}^{43} c_i \cdot I_i \quad (5)$$

where c_i are the interaction coefficients and I_i are the interaction terms which are both summarized in Table 3. The resulting statistical fit is compared to selected data in Figure 10. Both the 26 term fit and the 43 term fit are compared illustrating a reasonable fit for the 43 term model of Table 3. This fit is considered preliminary only as refinements will be made as further data is collected and analyzed.

Computational Fluid Dynamics

CFD was run using the method described by Slater (Ref. 4). The simulations were run at Mach 1.58 with a hole diameter of 6.35 mm. The center cross-section Mach number plots are shown in Figure 11. In the results, it is readily seen that there are two distinct flow regimes with a change over between 60° and 45°. As the 55° holes showed a response similar to the 90° holes we can conclude that the flow transition of the hole and a bow shock from the downstream edge of the hole whereas the 20° hole experiences neither of these. The increase in scaled sonic flow coefficient between the 55° and the 90° holes is apparent in that the 55° hole exhibits less separation and has a smaller wedge angle at the downstream

edge of the hole. Both of these properties cause the intersection of the shear-layer and the bow shock to occur deeper in the hole such that the effective minimum flow area is increased.

TABLE 3.—BLEED MODEL COEFFICIENTS AND INTERACTIONS

Constant	Interaction	Estimate	Standard error
c_1	intercept	5.923×10^{-1}	3.312×10^{-2}
c_2	$P_{plen_{scaled}}$	-9.614×10	6.346×10^{-1}
c_3	$P_{plen_{scaled}}^2$	-7.564×10^{-2}	6.700×10^{-1}
c_4	$P_{plen_{scaled}}^3$	3.200×10^{-1}	6.772×10^{-1}
c_5	M	8.268×10^{-2}	1.287×10^{-2}
c_6	$\frac{D}{\delta_1}$	-3.081×10^{-2}	1.689×10^{-2}
c_7	α	-4.236×10^{-3}	5.582×10^{-4}
c_8	$\frac{t}{D}$	1.450×10^{-2}	8.864×10^{-3}
c_9	$P_{plen_{scaled}} M$	-7.148×10^{-1}	2.842×10^{-1}
c_{10}	$P_{plen_{scaled}}^2 M$	-1.247×10^{-1}	2.943×10^{-1}
c_{11}	$P_{plen_{scaled}}^3 M$	1.287×10^{-1}	2.614×10^{-1}
c_{12}	$P_{plen_{scaled}} \frac{D}{\delta_1}$	3.844×10^{-1}	1.661×10^{-1}
c_{13}	$P_{plen_{scaled}}^2 \frac{D}{\delta_1}$	5.820×10^{-1}	1.734×10^{-1}
c_{14}	$P_{plen_{scaled}}^3 \frac{D}{\delta_1}$	-1.547×10^{-1}	1.810×10^{-1}
c_{15}	$P_{plen_{scaled}} \alpha$	4.210×10^{-2}	6.636×10^{-3}
c_{16}	$P_{plen_{scaled}}^2 \alpha$	-2.749×10^{-2}	6.911×10^{-3}
c_{17}	$P_{plen_{scaled}}^3 \alpha$	-1.597×10^{-4}	6.691×10^{-3}
c_{18}	$P_{plen_{scaled}} \frac{t}{D}$	-7.733×10^{-1}	2.644×10^{-1}
c_{19}	$P_{plen_{scaled}}^2 \frac{t}{D}$	-1.297×10^1	2.780×10^{-1}
c_{20}	$P_{plen_{scaled}}^3 \frac{t}{D}$	-4.820×10	2.871×10^{-1}
c_{21}	$M \frac{D}{\delta_1}$	-4.318×10^{-2}	9.045×10^{-3}
c_{22}	$M \alpha$	-6.910×10^{-4}	2.049×10^{-4}
c_{23}	$\frac{D}{\delta_1} \alpha$	7.601×10^{-4}	2.575×10^{-4}
c_{24}	$\alpha \frac{t}{D}$	1.414×10^{-3}	2.141×10^{-4}
c_{25}	$P_{plen_{scaled}} M \frac{D}{\delta_1}$	-6.286×10^{-3}	7.408×10^{-2}
c_{26}	$P_{plen_{scaled}}^2 M \frac{D}{\delta_1}$	-2.389×10^{-1}	7.604×10^{-2}
c_{27}	$P_{plen_{scaled}}^3 M \frac{D}{\delta_1}$	3.678×10^{-2}	7.274×10^{-2}
c_{28}	$P_{plen_{scaled}} M \alpha$	7.051×10^{-3}	3.218×10^{-3}
c_{29}	$P_{plen_{scaled}}^2 M \alpha$	1.375×10^{-2}	3.290×10^{-3}
c_{30}	$P_{plen_{scaled}}^3 M \alpha$	-1.788×10^{-3}	2.814×10^{-3}
c_{31}	$M \frac{D}{\delta_1} \alpha$	2.916×10^{-4}	1.125×10^{-4}
c_{32}	$P_{plen_{scaled}} M \frac{t}{D}$	3.903×10^{-1}	8.763×10^{-2}
c_{33}	$P_{plen_{scaled}}^2 M \frac{t}{D}$	-3.032×10^{-1}	9.226×10^{-2}
c_{34}	$P_{plen_{scaled}}^3 M \frac{t}{D}$	3.082×10^{-1}	8.363×10^{-2}
c_{35}	$P_{plen_{scaled}} \frac{D}{\delta_1}$	-8.032×10^{-2}	5.161×10^{-2}
c_{36}	$P_{plen_{scaled}}^2 \frac{D}{\delta_1}$	9.751×10^{-2}	5.400×10^{-2}
c_{37}	$P_{plen_{scaled}}^3 \frac{D}{\delta_1}$	2.486×10^{-1}	5.755×10^{-2}

TABLE 3.—BLEED MODEL COEFFICIENTS AND INTERACTIONS

Constant	Interaction	Estimate	Standard error
c_{38}	$M \frac{D}{\delta_1} \frac{t}{D}$	1.966×10^{-2}	2.419×10^{-3}
c_{39}	$P_{plen_{scaled}} \alpha \frac{t}{D}$	9.928×10^{-4}	1.930×10^{-3}
c_{40}	$P_{plen_{scaled}}^2 \alpha \frac{t}{D}$	1.164×10^{-2}	2.004×10^{-3}
c_{41}	$P_{plen_{scaled}}^3 \alpha \frac{t}{D}$	-3.836×10^{-3}	2.053×10^{-3}
c_{42}	$M \alpha \frac{t}{D}$	-4.764×10^{-4}	5.406×10^{-5}
c_{43}	$\frac{D}{\delta_1} \alpha \frac{t}{D}$	-5.602×10^{-4}	6.232×10^{-5}

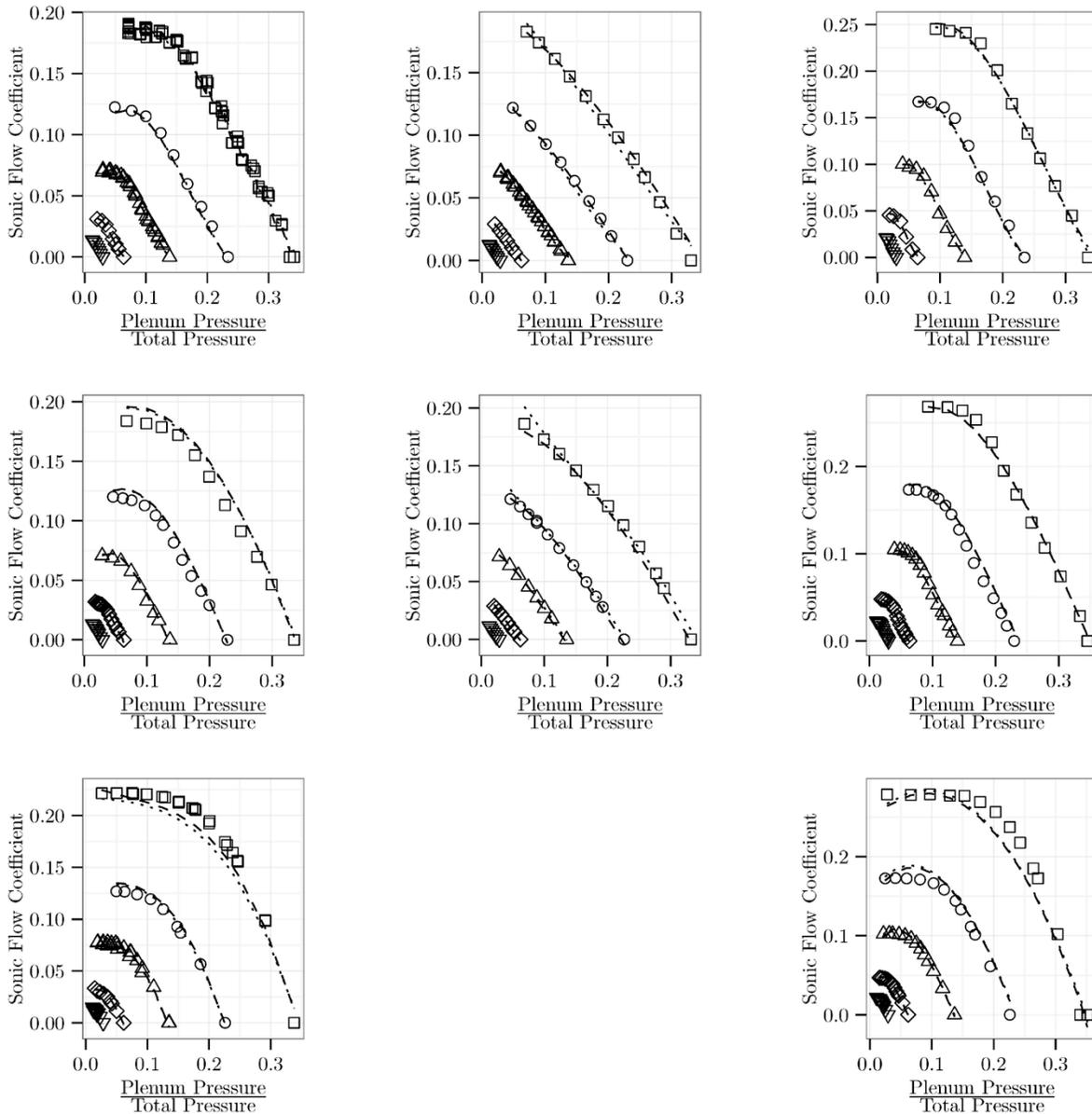


Figure 10.—Flow coefficient curves of selected plates compared to the statistical fit. Nominal Mach numbers: \square - 1.4, \circ - 1.7, \triangle - 2.0, \diamond - 2.5, ∇ - 3.0.

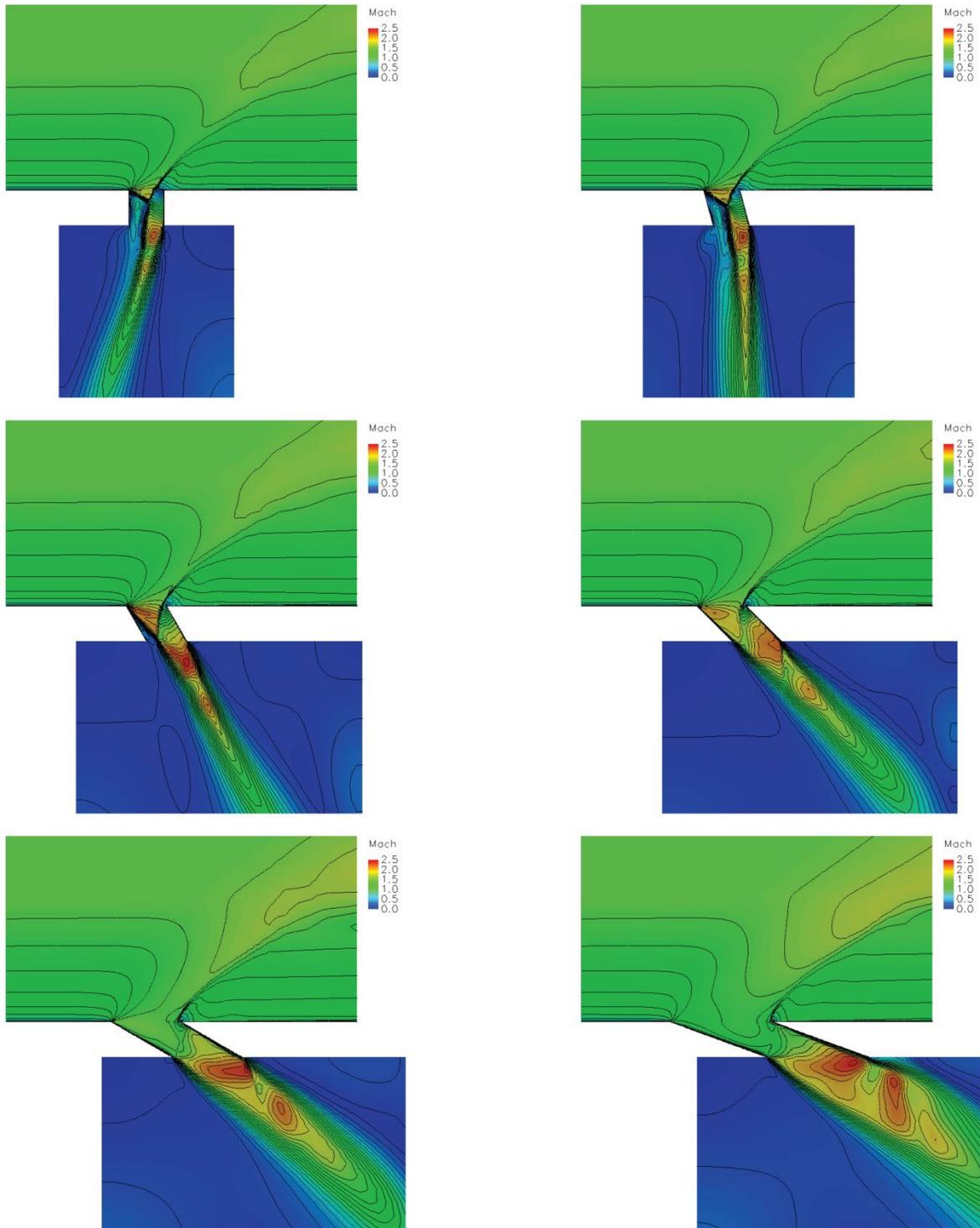


Figure 11.—CFD of a single round-hole at various hole inclination angles ($M=1.58$).

Summary and Conclusions

Flow coefficient data for 21 bleed hole configurations at five Mach number conditions have been presented. This data is intended to be used for the development of flow coefficient models to be used by inlet designers and in CFD computer codes. The results show that for accurate bleed flow modeling of

round holes, in addition to the local flow conditions, the effect of hole inclination angle, hole diameter, and bleed plate thickness must be included. While a physics based model is always desired and indeed have been attempted (Refs. 8, 9, and 10) the large number of parameters suggests that a statistical model, perhaps coupled with a simple flow model might be the best approach for a comprehensive flow coefficient model. And although they are likely secondary effects, a single-hole model might need to be extended to include hole array parameters such as hole-to-hole spacing and porosity.

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