

*AAS High Energy Astrophysics Division Meeting*

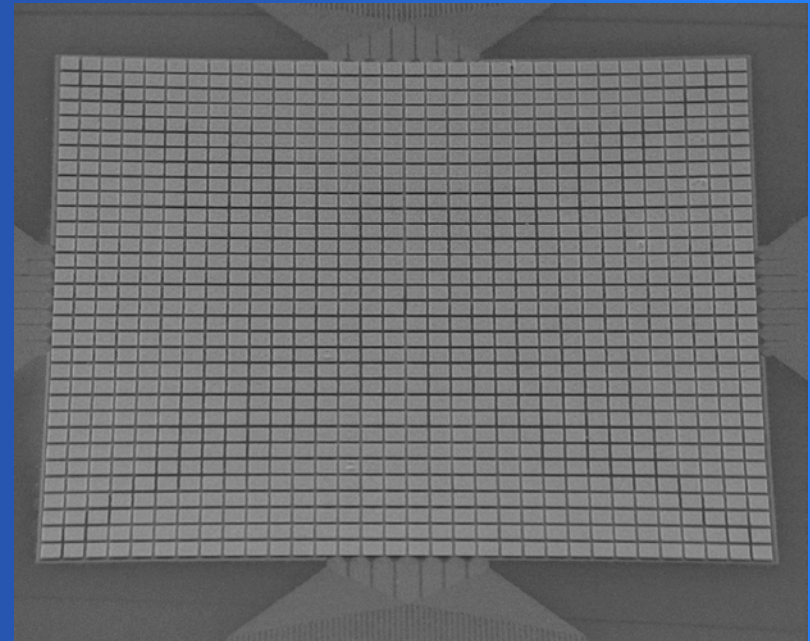
*Monterey, California April 8-11, 2013*

## Future development trajectories for imaging x-ray spectrometers based on microcalorimeters

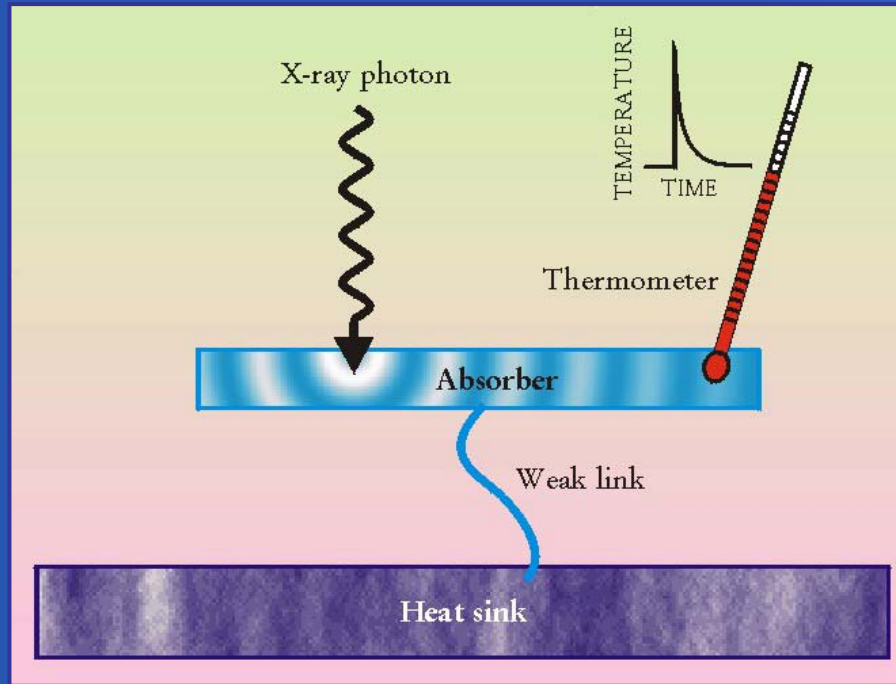
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Caroline Kilbourne and Simon Bandler

NASA Goddard Space Flight Center



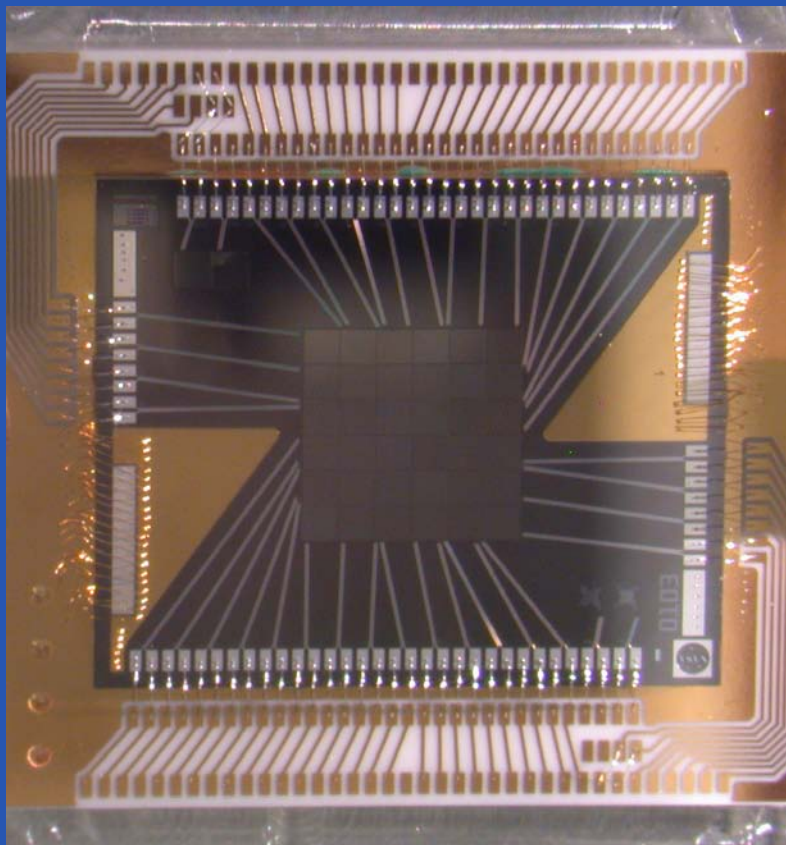
# Looking specifically at microcalorimeters (operated at $T < 0.1$ K)



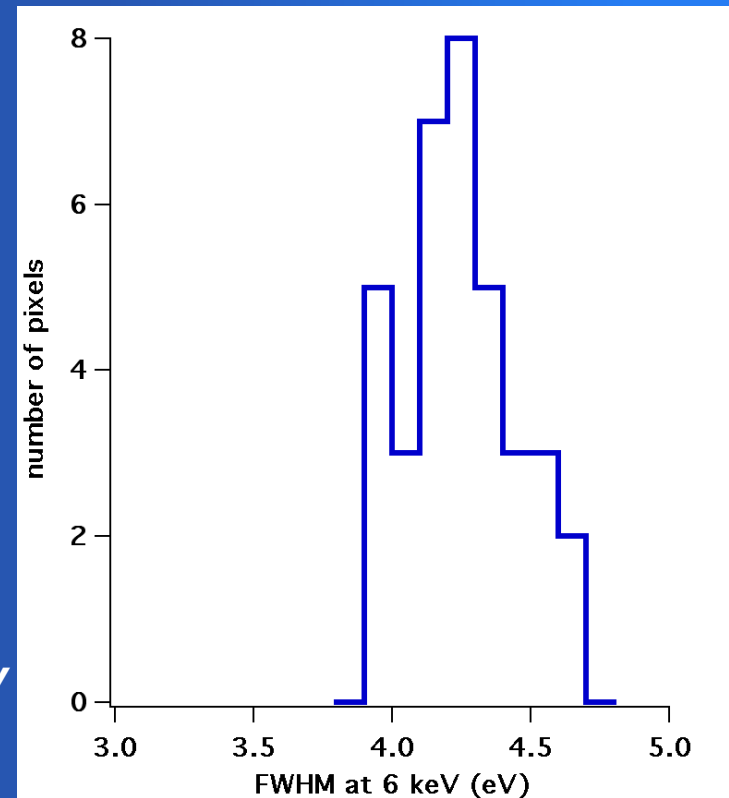
- The leading microcalorimeter thermometer technologies
  - Resistance (semiconductor thermistors and superconductors at their phase transition)
  - Magnetically coupled calorimeters
- What is the state of the art for the leading microcalorimeter sensor and read-out technologies? How far can the limits be pushed?

# Silicon thermistor-based calorimeter array for Astro-H

- Base temperature of 50 mK
- 36 pixels – silicon thermistors on 0.83 mm pitch with HgTe absorbers
- Resolution at 6 keV ranges from 3.6 – 4.6 eV across EM and FM arrays
- Lack of large-scale read-out technology limits arrays to a few hundred pixels
  - Overtaken by TES arrays and SQUID multiplexing
  - Nonetheless, Astro-H is an important pathfinder



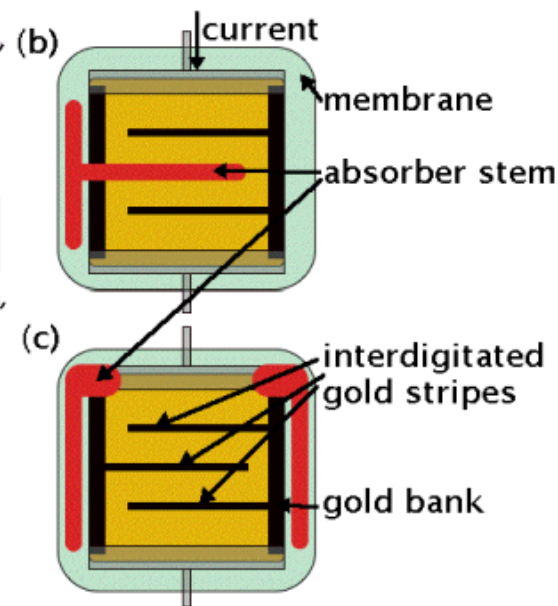
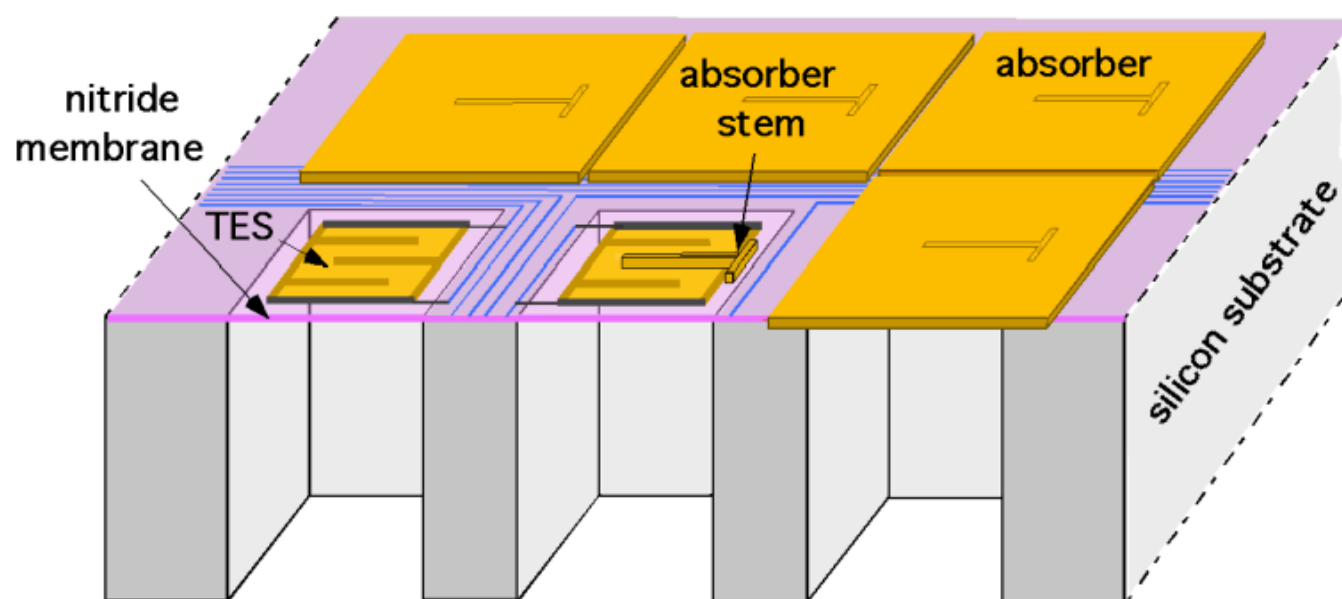
**SXS FM**  
*candidate array*



# Transition-edge sensors (TES) – basic pixels

- The temperature and current dependence of the transition from the zero-resistance to normal-resistance state is used for thermometry
- Consist of thermometer (with superconducting leads and normal-metal features), x-ray absorber, and controlled link to heat sink

(a)



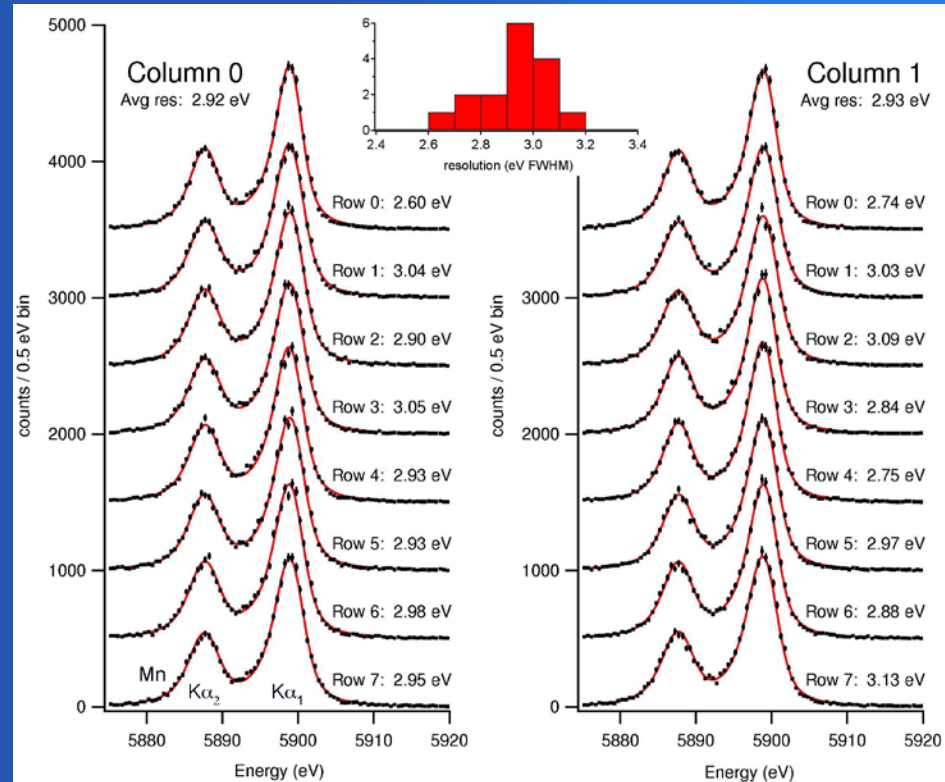
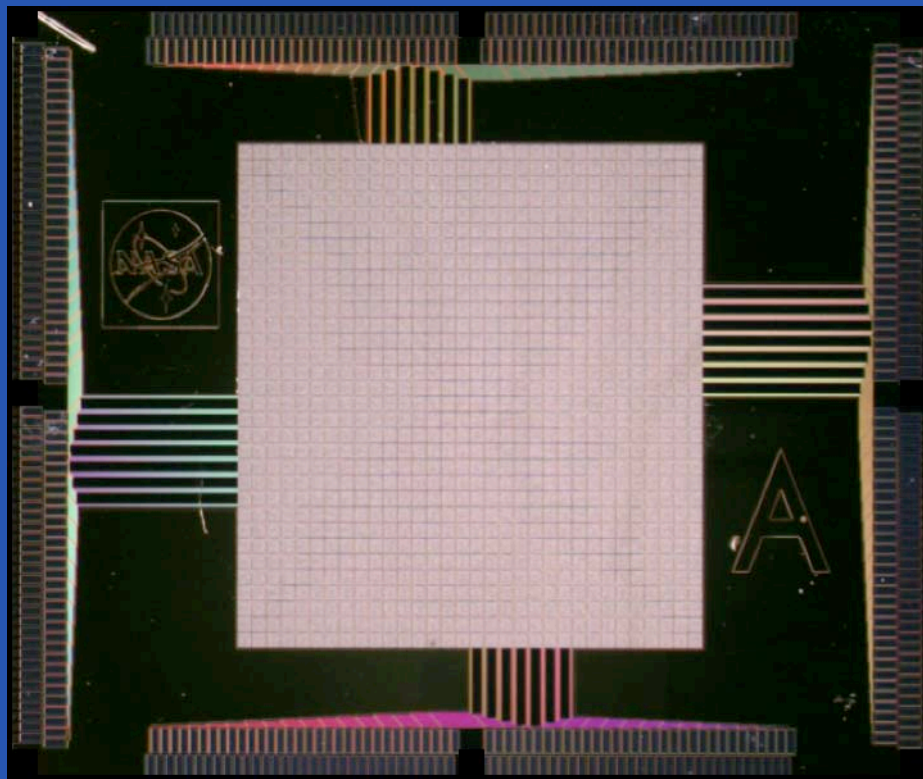
- Pixel pitch → thermometer size → transition properties and whether membrane needed for thermal link
  - “small” TES thermometers  $< 0.05$  mm; “standard”  $\sim 0.14$  mm



# “Standard” TES pixels –XMS baseline of IXO, Athena, etc.

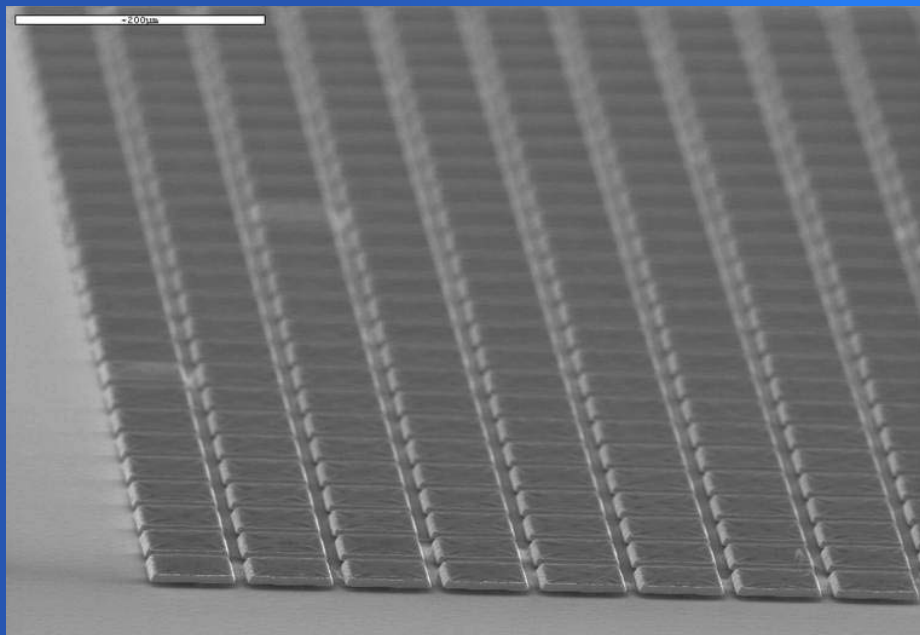
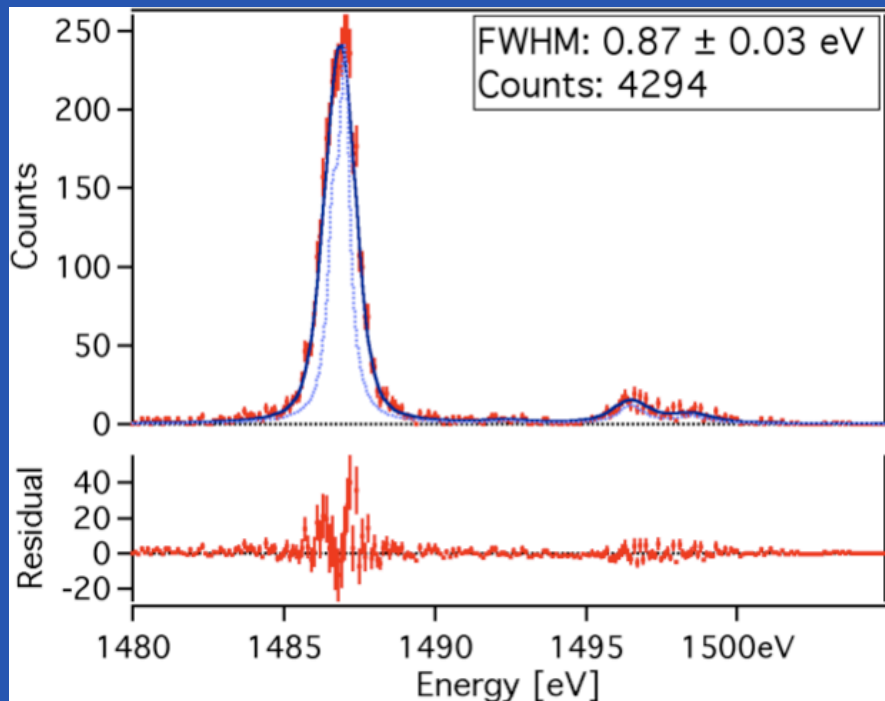
## ■ XMS reference design based on GSFC TES design

- Membrane-isolated Mo/Au TES with  $T_c \sim 90$  mK, (base temperature at 50 mK)
- Electroplated Bi/Au absorbers, 0.25 – 0.30 mm pitch
- 1.8 eV resolution demonstrated, 2 – 3 eV routine in this design
- Multiplexed SQUID read-out close to requirements for few-thousand pixel array
- 32x32 arrays with microstrip leads successfully fabricated

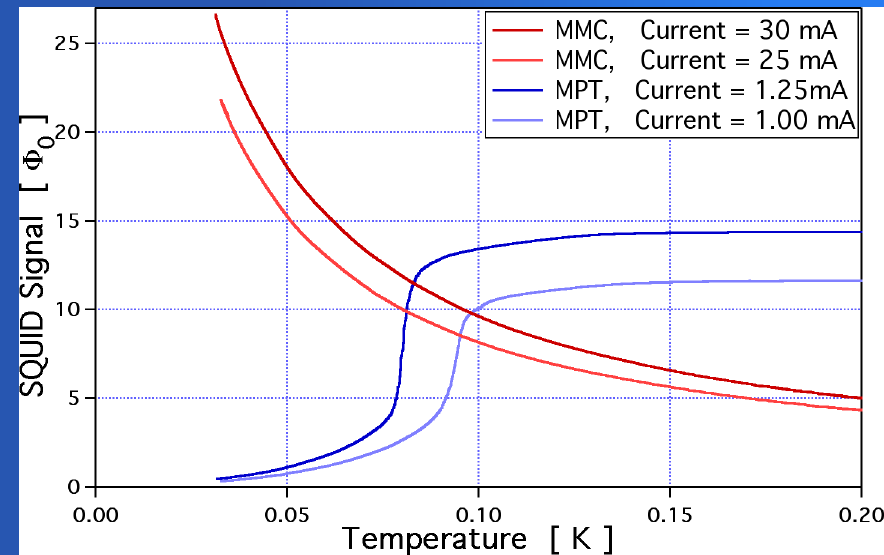
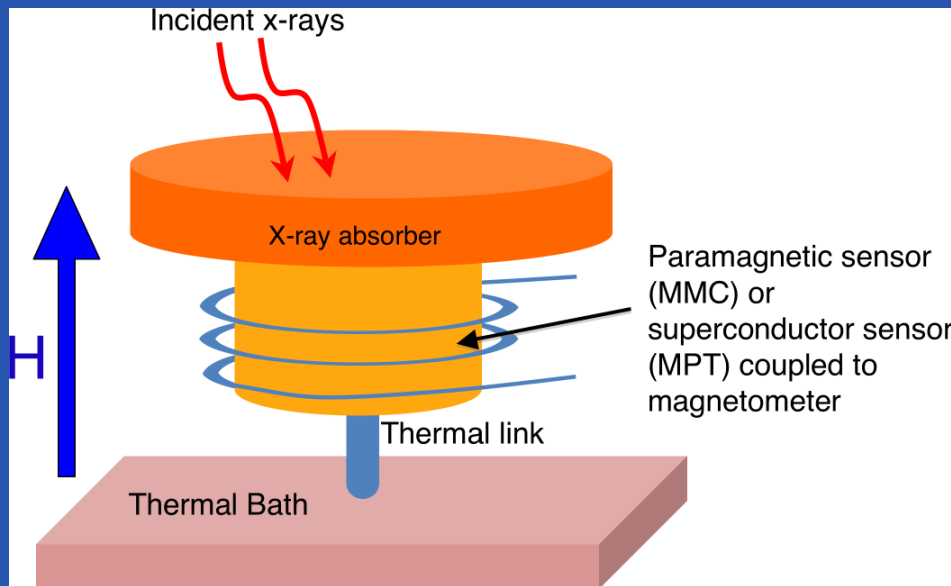


## “Small” TES pixels

- Small pixels suited to shorter focal lengths and/or higher spatial resolution
- In small TES devices,  $T_c$  depends sensitively on current – extends linear operating range of pixels
- Don't need membrane isolation; small size limits coupling to solid substrate
  - Heat sinking of solid substrate minimizes thermal crosstalk
- Through choice of  $T_c$ , can be optimized for speed (0.03 ms fall time) or resolution (0.9 eV FWHM) (GSFC devices).



# Inductive thermometers – using temperature dependence of paramagnetism or magnetic penetration of a superconductor



- Arrays of Nb meanders with layer of magnetic material (Au:Er) or a low- $T_c$  superconductor (Mo/Au), with high-fill-factor absorbers as with TES.
  - change of magnetization measured as change of inductance
- The Heidelberg group has achieved just better than 2.0 eV resolution at 6 keV with a Au:Er metallic magnetic calorimeter (MMC).
- GSFC group has obtained 2.3 eV resolution with Mo/Au magnetic penetration thermometer (MPT).

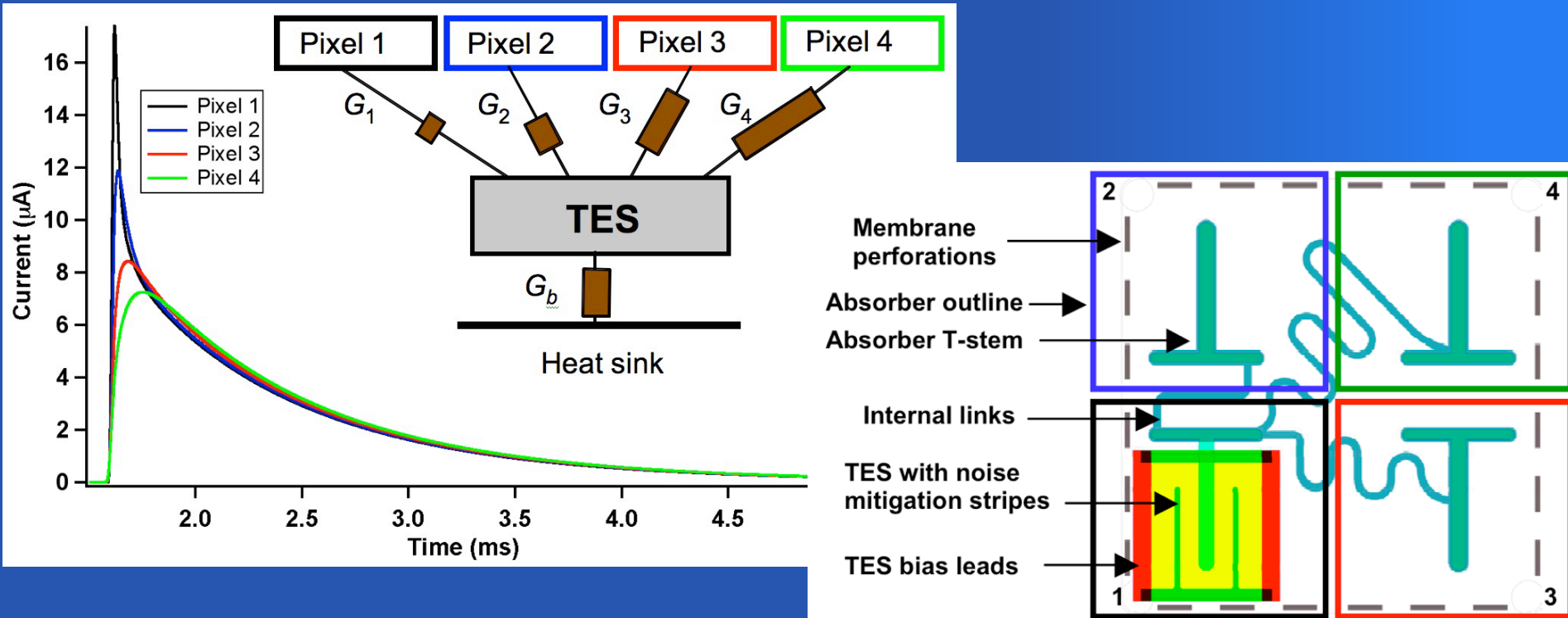
# Magnetically coupled calorimeters (MCC) compared with TES

- MCCs are intrinsically dissipationless
  - very large-format focal-plane arrays
- MCC sensor material is electrically isolated
  - can be directly connected to metallic heat sink – simplifying reduction of thermal crosstalk
- Dissipation in TES calorimeters allows electrothermal feedback
  - stabilizes operating temperature, relaxing temperature stability required at heat sink
- TES read-out allows easy signal filtering, greatly simplifying multiplexing.

Each has advantages and disadvantages – continued parallel investment in both TES and MCCs is needed.

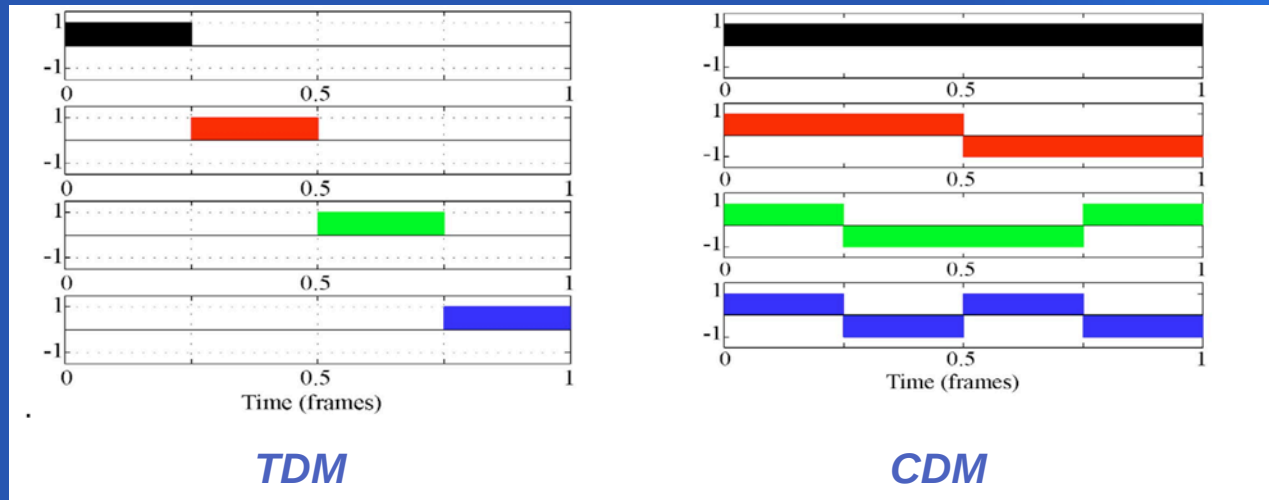


# Using the non-equilibrium signal in equilibrium devices for position discrimination



- Multiple absorbers connected thermally to the same thermometer via different thermal links
- Demonstrated for TESs and MMCs
  - 2.4 eV resolution obtained in 9-pixel TES device with 0.065 mm pixels
- Ideal “hydra” obtains somewhat worse resolution than for one big pixel of the same area due to thermal fluctuations between the absorbers.

# Multiplexed TES read out: switched SQUID multiplexing



- XMS reference design included time-division multiplexing (TDM)
  - Individual TES pixels are coupled (via each pixel's SQUID) to a single amplifier
  - Multiplexed by sequential switching between SQUIDs
  - Used in TRL-4 TES read-out demo in 2008 (2.6 – 3.1 eV across 16 mux'd TESs)
- Code Division Multiplexing (CDM) will soon reach TDM TRL level
  - All pixels ON all the time, polarity of coupling is switched
  - CDM has a  $\sqrt{N}$  noise advantage over TDM, where N is the multiplexing scale
    - IXO/XMS noise budget was extremely tight – CDM could provide important margin
    - Facilitates faster pixels with larger slew rates by providing the noise margin to allow the coupling of the TES to the input SQUID to be reduced
- CDM demonstrated: < 3 eV on 16 switched pixels using flux-matrixed CDM

# Frequency domain multiplexing (FDM)

## ■ TES bias modulation

- Different TES pixels AC-biased at different frequencies read out by single SQUID
- X-ray pulses seen in amplitude modulation
- Like CDM, pixels on all the time, imparting a  $\sqrt{N}$  advantage over TDM
- However, in identical pixels tested with AC and DC bias, significantly better resolution was obtained in the DC bias case, which may be fundamental

## ■ Microwave multiplexing

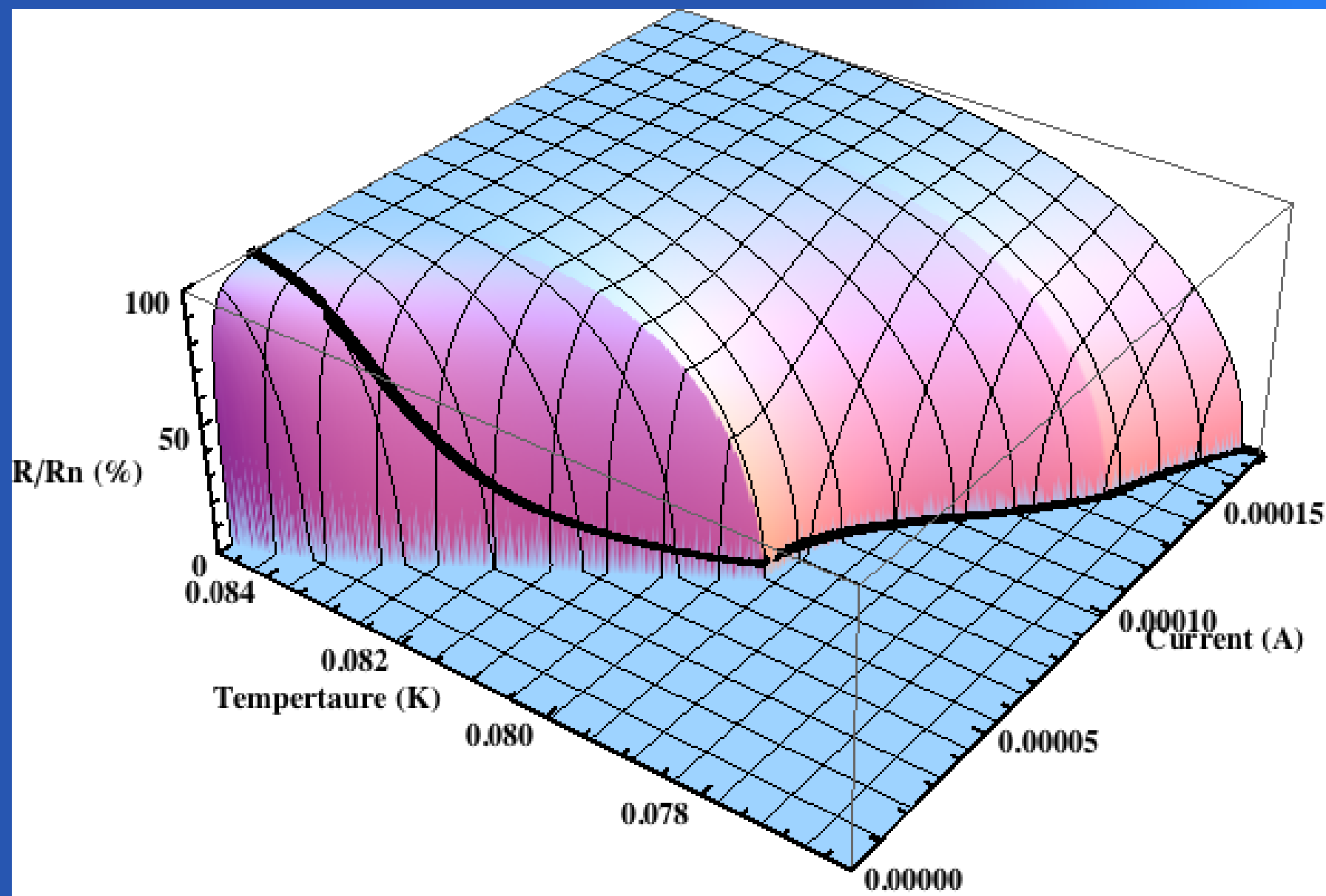
- Pixel electronics form high-Q microwave resonant circuits (GHz scale), hundreds of which can be combined on a single coax
- For TESs, MMCs, and MPTs, an unshunted rf SQUID is incorporated into the read out of each pixel, which is in turn coupled to a resonant circuit
- A successful microwave multiplexing demonstration has recently been completed at NIST on two gamma-ray TES pixels.

# Pushing the limits on spectral resolution

## ■ Resolving power for soft x-rays

- All microcalorimeters are non-linear. If we set  $dT_{\max}$  as the maximum allowed temperature change, then we need to design the TES so that  $E_{\max}$  produces  $dT_{\max}$ .  $E_{\max}$  scales as  $C/\alpha$ , but resolution  $dE$  scales as  $\sqrt{C/\alpha}$ . Thus designing for 0.5 keV instead of 6 keV will not preserve the resolving power achieved at 6 keV. Getting to 0.2 eV resolution at 0.5 keV will not be possible without signal processing techniques (under development) that enable analysis of highly non-linear signals with high resolution. Reducing  $C$  by more than a factor of  $\sim 10$  will need reductions in the TES size as well as the absorber  $C$ .
- In small TES devices,  $T_c$  depends sensitively on current – extending the linear operating range of pixels for a given  $C/\alpha$ . However, the Johnson noise of a resistor with current dependence fundamentally increases with this current sensitivity,  $\beta$ .
- Paramagnetic calorimeters also have scaling issues. They are more linear, but their sensitivity scales with the heat capacity of the spin system.

➔  $R = 1000$  within reach at 0.5 keV,  $R = 3000$  probable, but much higher than that is unlikely.





# Pushing the limits on counting rate

## ■ Limits at the pixel (trade against resolution and array size)

- Decreasing the thermal time constant of a pixel starts to degrade resolution when it approaches thermalization time scales in the absorber.
- Increased thermal conductance requires higher bias current with ramifications for the operating point in the transition and for heat sinking.
- Faster paramagnetic calorimeters fundamentally have worse resolution than slower ones ( $\tau^{0.25}$  scaling).

## ■ Limits on the readout (trade against multiplexer scale, array size)

- The more bandwidth per pixel, the fewer pixels per multiplexer channel.

## ■ Limits on the signal processing

- Historically, optimal digital filtering used. Long records containing a single pulse are required in order to have sufficient frequency resolution in the optimal filter as well as to avoid pile up; resolution degraded when shorter records used.
- Recently, new optimizations specifically for high count rates are being developed (e.g. by B. Alpert, NIST).

➔ Expect that 1000/s/pixel rates at > 80% live time will be possible in small sub-arrays with new processing techniques.

# Pushing the limits on number of pixels

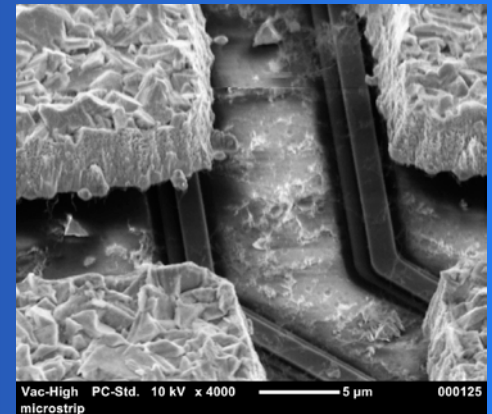
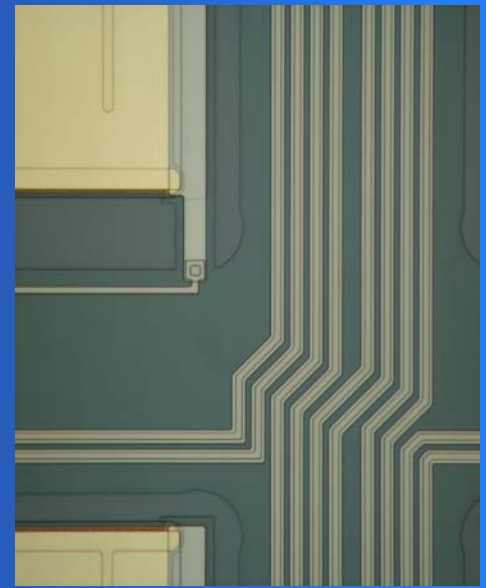
## ■ Array architecture

- Limit on bringing out wires between the pixels will be reached at the  $\sim 10^4$  pixel level (depending on pitch, etc.). Larger arrays will need close integration of the pixels and the multiplexing. NIST is working on integrating CDM with TES arrays.
- Use of Hydras eases demands on heat-sinking, wiring, and electronics, at the expense of resolution and per-pixel count rate.

## ■ Wiring to room temperature

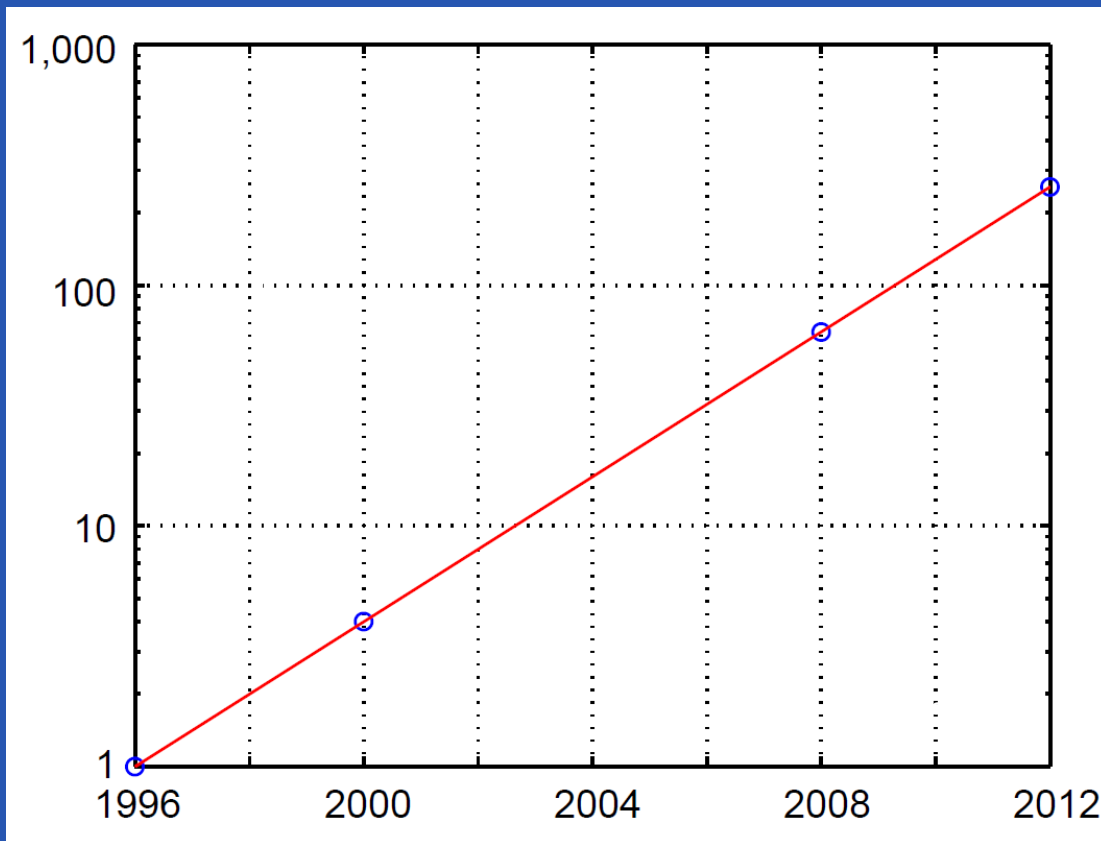
- Combining integrated CDM with microwave multiplexing holds the promise of reading out  $10^5$  sensors (pixel pitch  $> 0.25$  mm) with as few as two coaxes (depending on sensor speed).

➔ Expect to get to  $10^5$  TES in the next 20 years ( $10^6$  with Hydras), though compromises on count rate may be necessary.



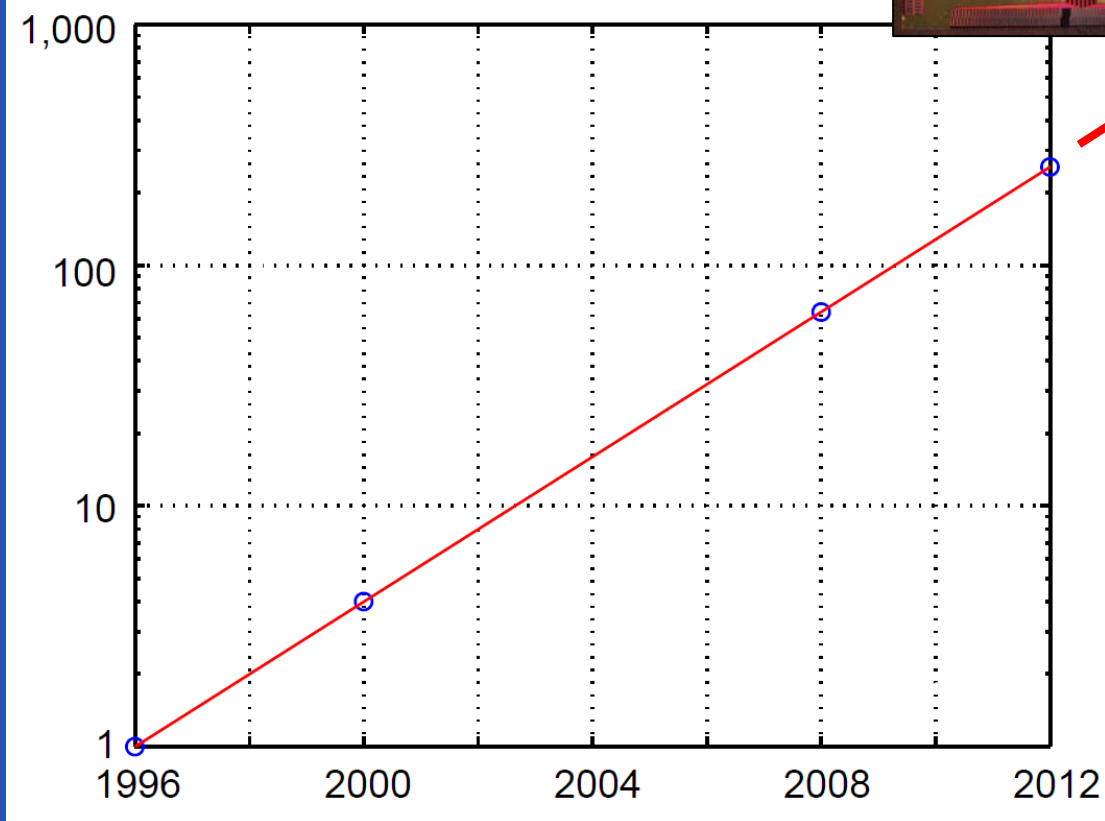
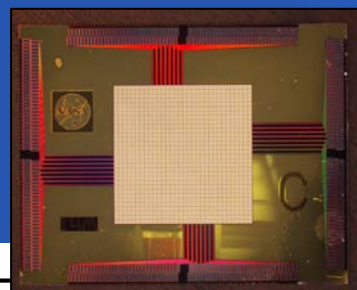
# Moore's Law for instrumented TES microcalorimeter arrays (courtesy of Kent Irwin)

Doubling time: 2 years



# Moore's Law for instrumented microcalorimeter arrays

Doubling time: 2 years



TES with  
TDM

TES with  
CDM

TES or  
MCC with  
microwave  
MUX

