

# Development of a Pulsed 2-micron Integrated Path Differential Absorption Lidar for CO<sub>2</sub> Measurement

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## ABSTRACT

Atmospheric carbon dioxide (CO<sub>2</sub>) is an important greenhouse gas that significantly contributes to the carbon cycle and global radiation budget on Earth. Active remote sensing of CO<sub>2</sub> is important to address several limitations that contend with passive sensors. A 2-micron double-pulsed, Integrated Path Differential Absorption (IPDA) lidar instrument for ground and airborne atmospheric CO<sub>2</sub> concentration measurements via direct detection method is being developed at NASA Langley Research Center. This active remote sensing instrument will provide an alternate approach of measuring atmospheric CO<sub>2</sub> concentrations with significant advantages. A high energy pulsed approach provides high-precision measurement capability by having high signal-to-noise ratio level and unambiguously eliminates the contamination from aerosols and clouds that can bias the IPDA measurement. Commercial, on the shelf, components are implemented for the detection system. Instrument integration will be presented in this paper as well as a background for CO<sub>2</sub> measurement at NASA Langley research Center.

**Keywords:** Carbon dioxide, active remote sensing, integrated path differential absorption lidar

## 1. INTRODUCTION

Carbon dioxide (CO<sub>2</sub>) is an important greenhouse gas that significantly contributes to the carbon cycle and global radiation budget on Earth. Generally, the CO<sub>2</sub> role on Earth's climate is rather complicated due to different interactions with various climate components that include the atmosphere, the biosphere and the hydrosphere [1-3]. These interactions define CO<sub>2</sub> sources and sinks that influence the gas transport fluxes worldwide. High uncertainties exist in quantifying CO<sub>2</sub> sources and sinks mainly due to insufficient spacial and temporal monitoring of the gas. Understanding the interactions and transport of atmospheric CO<sub>2</sub> around the Earth is critical for carbon cycle studies and climate predictions through environment models [1-12].

Historical CO<sub>2</sub> concentration has been predicted through analyzing trapped gas released from ice cores obtained from Antarctic glaciers samples. Results indicated relatively stable atmospheric CO<sub>2</sub> concentration that fluctuates between 180 and 290 ppm over the past 650,000 years [4]. However, since the industrial revolution the gas concentration is increasing rapidly to a current level of 390 ppm [5]. The recent CO<sub>2</sub> high increase rate is attributed to human activities for different reasons. One reason is the temporal isotopic signature of fossil fuel burning that exists in current atmospheric CO<sub>2</sub> [6]. Another reason is the spatially higher CO<sub>2</sub> concentration in the Northern Hemisphere, where most of the land mass and human activities occur, than the Southern Hemisphere with higher ocean coverage [11]. Atmospheric CO<sub>2</sub> observations made over the past four decades shows similar trends between the gas concentration in the atmosphere CO<sub>2</sub> and industrial emission [3]. These evidences led to extensive efforts worldwide for monitoring atmospheric CO<sub>2</sub> through various techniques including *in-situ* and passive sensors.

CO<sub>2</sub> *in-situ* sensors have been used continuously on towers, aircraft and balloons for several decades for monitoring the gas concentration. Results from tower sensors indicated the existence of seasonal and diurnal cycles of the CO<sub>2</sub> concentration, both related to biosphere activities. Seasonal cycles alternate the biosphere from source to sink between winter and summer respectively. Diurnal cycles respond to the respiration and photosynthesis activities [7]. For example, in a forested area study, tower *in-situ* sensors indicated a variation in the CO<sub>2</sub> diurnal cycle of 5 to 40 ppm between winter and summer seasons, respectively [8, 9]. On the other hand, aircraft *in-situ* sensors identified that the CO<sub>2</sub> con-

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centration and its seasonal cycle depends on latitude [10, 11]. Results confirmed higher CO<sub>2</sub> concentration in the northern Hemisphere compared to the Southern, with higher seasonal cycle amplitude [11]. Balloons and aircraft sensors also were used to sample CO<sub>2</sub> concentrations versus altitude [11, 12]. Results indicated constant CO<sub>2</sub> concentration with respect to altitude up to a level where global air transport patterns take place [11]. Generally, CO<sub>2</sub> *in-situ* sensors coverage is limited due to inadequate sampling sites and time. Thus, it is required to have more rapid and accurate CO<sub>2</sub> monitoring with higher uniform coverage and high resolution. This was addressed by many international satellite missions.

Satellites passive remote sensing of CO<sub>2</sub> concentrations provide improved spatial and temporal coverage compared to the surface *in-situ* networks. Satellites offered many advantages including the ability of continuously measuring CO<sub>2</sub> in tropical regions and over southern oceans [1-3]. Present satellite instruments monitoring CO<sub>2</sub> from space include SCIAMACHY, TES, AIRS, IASI and GOSAT [13-17]. To focus only on CO<sub>2</sub> and address the issue of the gas sources and sinks, OCO-2 is fully dedicated for CO<sub>2</sub> monitoring [18]. Generally, satellite passive remote sensing relies on either solar radiation (shortwave infrared) or thermal radiation from Earth. Some of these systems have shown the potential to meet the spatial coverage to improve CO<sub>2</sub> flux estimates on continental scales. However, they are unable to meet the accuracy required to aid in better quantifying the terrestrial sources and sinks. Generally satellite passive systems have limitations. For example shortwave infrared instruments are limited by their reliance on solar illumination which restricts their orbits and latitudinal coverage. On the other hand, thermal infrared systems are not sensitive to the lower atmosphere where the largest CO<sub>2</sub> interactions occur. Furthermore, passive remote sensing systems involve retrieval complexities which suffer from aerosol and cloud contamination and radiation path length uncertainties [2-3, 19]. Active remote sensing of CO<sub>2</sub> is an alternative technique that has the potential to overcome the limitation of the passive sensors.

Active remote sensing of CO<sub>2</sub> has been demonstrated using the differential absorption lidar (DIAL) technique [20-30]. Both 1.6 and 2.0  $\mu\text{m}$  are considered suitable for atmospheric CO<sub>2</sub> measurements due to the existence of distinct absorption features for the gas at these particular wavelengths. Although CO<sub>2</sub> DIAL systems demonstrations were provided for systems validity from ground or airborne, a complete CO<sub>2</sub> DIAL mission that contributes to the science community has not been established [3]. A number of worldwide teams have been engaged in developing CO<sub>2</sub> DIAL instrument using different laser transmitters and detection methods. In France, a CO<sub>2</sub> DIAL was developed based on 2.0- $\mu\text{m}$  pulsed crystal-open path cavity transmitter and heterodyne detection [20]. In Germany a 1.6- $\mu\text{m}$  pulsed optical parametric oscillator transmitter with direct detection has been developed [21]. In Japan similar systems were developed for ground based-measurement [27, 28]. In the USA, the National Research Council (NRC) Decadal Survey recommended an active laser-based CO<sub>2</sub> mission, "Active Sensing of CO<sub>2</sub> Emissions over Night, Days, and Seasons (ASCENDS)", to dramatically increase our understanding of CO<sub>2</sub> sources, sinks, and fluxes worldwide [1]. Research groups at NASA are currently involved in developing different CO<sub>2</sub> DIAL instruments. Two of these instruments operate at 1.6  $\mu\text{m}$  have been developed and deployed as airborne systems for atmospheric CO<sub>2</sub> column measurements [22, 25-26]. One instrument is based on an intensity modulated continue wave (CW) approach [25-26], the other on a high pulse repetition frequency (PRF), low pulse-energy approach [22]. These airborne CO<sub>2</sub> DIAL systems operating at 1.57- $\mu\text{m}$  utilize mature laser and detector technologies by taking advantage of the technology development outcomes in the telecom industry. CO<sub>2</sub> DIAL operating in the 2- $\mu\text{m}$  band offer better near-surface CO<sub>2</sub> measurement sensitivity due to the intrinsically stronger absorption lines. Using a 2.05- $\mu\text{m}$  CW laser absorption spectrometer employing coherent detection method, airborne measurements of CO<sub>2</sub> column abundance has been demonstrated [24]. This paper focuses on the current role played by NASA Langley Research Center (LaRC) in developing a 2- $\mu\text{m}$  pulsed DIAL systems for monitoring atmospheric CO<sub>2</sub> [23, 29-30]. For more than 15 years, NASA LaRC has been involved in maturing the transmitter technology and system capabilities that are focused onto meeting the science objective of the CO<sub>2</sub> measurement described by the decadal survey and A-Scope [1, 2]. Furthermore, the requirement and the potential of scaling such technology to a space mission will be addressed.

## 2. SINGLE-PULSED 2-MICRON CO<sub>2</sub> DIAL SYSTEMS DEMONSTRATION

Atmospheric CO<sub>2</sub> DIAL measurement using single-pulse 2- $\mu\text{m}$  laser have been demonstrated by NASA LaRC [23, 29-30]. The wavelength of the output laser pulses alternate between on-line and off-line positions at a relatively slow rate (5-10 Hz). Using heterodyne detection, CO<sub>2</sub> DIAL measurements were attempted based on a 90 mJ, 140 ns, 5 Hz pulsed Ho:Tm:LuLiF laser transmitter. The laser transmitter adopted a wavelength control to precisely tune and lock the operating wavelength at any desired offset up to 2.9 GHz from the center of a CO<sub>2</sub> absorption line. Once detuned from

the line center the laser wavelength is actively locked to keep the wavelength within 1.9 MHz standard deviation about the set point. The wavelength controlled allows optimization of the CO<sub>2</sub> optical depth for the DIAL measuring. The laser transmitter has been coupled with a coherent heterodyne receiver for measurements of CO<sub>2</sub> concentration using aerosol backscatter. A byproduct of this system is the wind and aerosols measurements with the same lidar. This provides useful additional information on atmospheric structure. Range-resolved CO<sub>2</sub> measurements were made with < 2.4% standard deviation using 500 m range bins and 6.7 min (1000 pulse pairs) integration time. Measurement of a horizontal column showed a precision of the CO<sub>2</sub> concentration to < 0.7% standard deviation using a 30 min (4500 pulse pairs) integration time. Comparison with a collocated *in situ* sensor, as shown in figure 1, indicated the DIAL capability to measure the same trend of a diurnal variation and to detect shorter time scale CO<sub>2</sub> perturbations. For vertical column measurements the lidar was setup at the WLEF tall tower site in Wisconsin to provide meteorological profiles and to compare the DIAL measurements with the *in situ* sensors distributed on the tower up to 396m height. Assuming the DIAL column measurement extending from 153m altitude to 1353m altitude should agree with the tower *in situ* sensor at 396m altitude, there was a 7.9 ppm rms difference between the DIAL and the *in situ* sensor using a 30 min rolling average on the DIAL measurement as indicated in the same figure [23].

Detection technology usually limits the CO<sub>2</sub> DIAL profiling capability at the 2- $\mu$ m wavelength. Therefore, 2- $\mu$ m phototransistors have been developed and integrated for the first time in lidar applications. This direct detection 2- $\mu$ m CO<sub>2</sub> DIAL system was developed at NASA LaRC [29-30]. Initially, a backscatter lidar system has been demonstrated by utilizing the same 2- $\mu$ m single-pulsed tunable pulsed laser and the infrared phototransistor for the transmitter and the receiver, respectively. To validate the profiling capability of the system, the 2- $\mu$ m atmospheric backscatter profiles were compared to profiles obtained at 1 and 0.5  $\mu$ m using avalanche photodiode and photomultiplier tube, respectively. The 2- $\mu$ m system capability for atmospheric CO<sub>2</sub> temporal profiling using DIAL was demonstrated. This was achieved by tuning the laser at slightly different wavelengths around the CO<sub>2</sub> R22 absorption line in the 2.05- $\mu$ m band as shown in figure 2 [30]. CO<sub>2</sub> temporal profiles were also compared to *in situ* measurements. Preliminary results indicated average mixing ratios close to 390 ppm in the atmospheric boundary layer with 3.0% precision. Field experiments were conducted at West Branch, Iowa, for evaluating the system for CO<sub>2</sub> measurement by comparison with *in-situ* sensors. The NOAA's CO<sub>2</sub> *in-situ* sensors were located on the WBI tower at 31, 99 and 379 m altitudes, besides the NOAA's aircraft was sampling at higher altitudes. Preliminary results, shown in figure 3, demonstrated the capabilities of the DIAL system in profiling atmospheric CO<sub>2</sub> using the 2- $\mu$ m wavelength. One advantage of the DIAL system is the ability to perform integrated CO<sub>2</sub> column measurements. This is demonstrated using data collected on June 26, 2008. On that day, weather conditions included continuous, variable altitude cirrus clouds, as indicated in the false color diagrams of figure 3. Vertical column integration was performed between the near-field high scattering from the

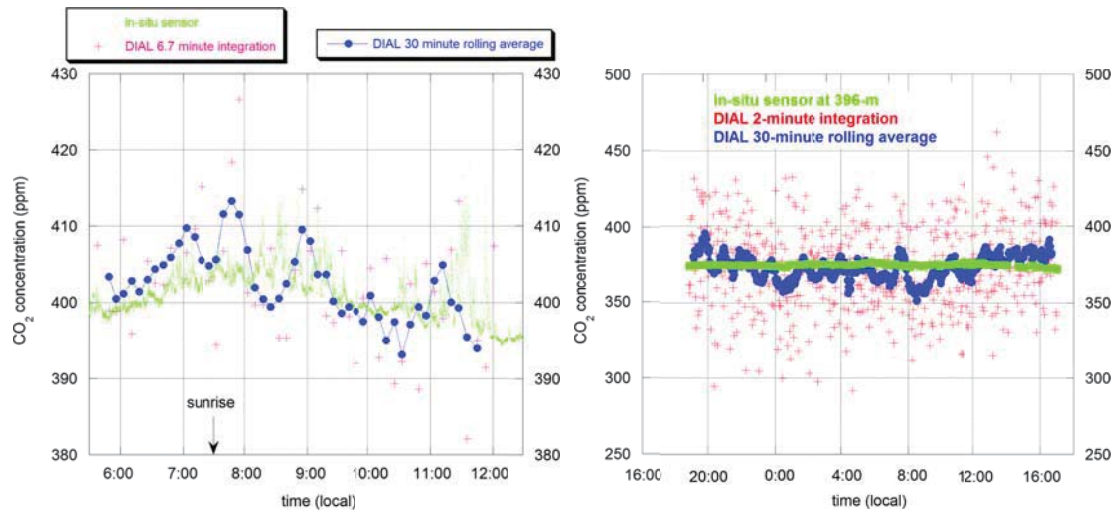


Figure 1. (Left) 2- $\mu$ m heterodyne CO<sub>2</sub> DIAL results compared to *in situ* sensor. Experiment was conducted on March 23, 2007 in Hampton, Virginia. The DIAL beam is pointing horizontally for a column measurement at the same altitude as the *in situ* sensor. (Right) Results from the same DIAL instrument compared to *in situ* measurements conducted on June 13-14, 2007 at the WLEF tower site. The *in situ* sensor is at 396m altitude. DIAL measurements are averaged over a vertical column extending from 153 to 1353m altitude [23].

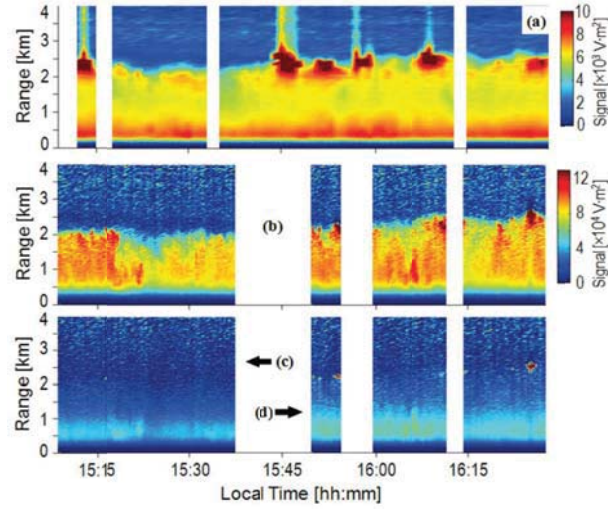


Figure 2. False color diagrams for the near-field boundary layer profiles measured on May 19, 2008 using lidar instruments operating at (a) 1064 nm and the 2- $\mu$ m lidar operating in DIAL mode at (b) off-line 2053.449 nm and (c) 2.15 GHz sideline and (d) 2.80 GHz side-line. Time discontinuity in the data is attributed to system adjustments [30].

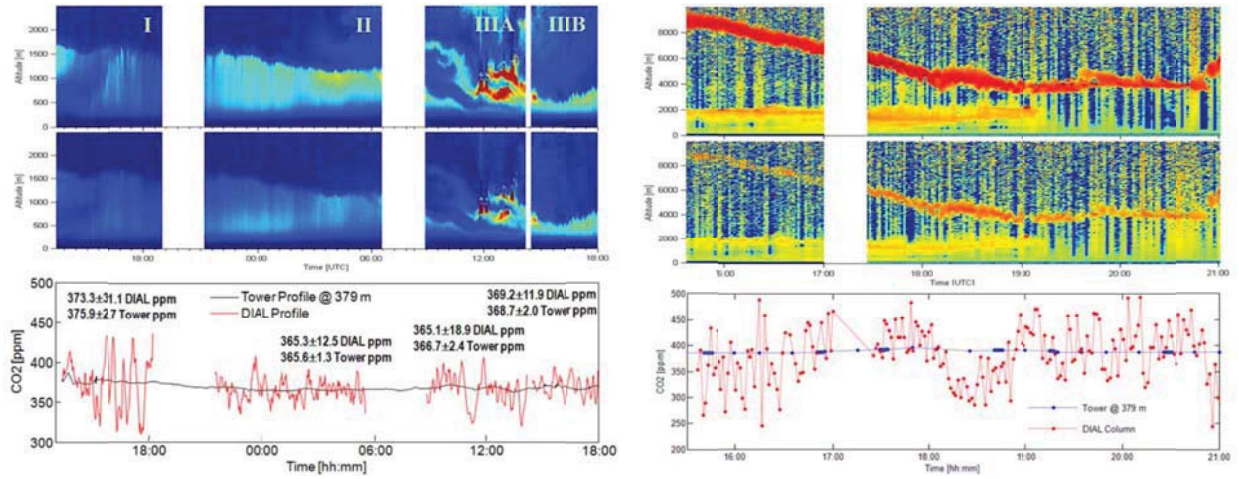


Figure 3. (Left) False color diagrams for the off-line (top) and side-line (middle) of the range corrected signal profiles. The data was collecting from the morning of July 5th till the afternoon of July 6th, 2008 with 2.80 GHz (sections I and IIIB) and 2.15 (sections II and IIIA) tuning. The calculated  $\text{CO}_2$  mixing ratio of the DIAL and 379 m tower sensor are compared in the bottom. (Right) False color diagrams for the log of the range corrected off-line and side-line profiles (top and middle) from measurements on June 26, 2008. The calculated effective average  $\text{CO}_2$  mixing ratio of the DIAL and tower sensor are compared in the bottom [29].

boundary layer and the far-field scattering from the cloud. The measurement results are shown in the same figure [29].

The conducted single-pulse 2- $\mu$ m  $\text{CO}_2$  DIAL experiments point out several system improvements that would enhance the measurement capability. First, the selected target  $\text{CO}_2$  R22 line includes high water vapor interference that coexists at the same operating wavelength. Operating on the  $\text{CO}_2$  R30 line potentially increases the system sensitivity while reducing the water vapor interference close to zero. Besides, locking the off-line position, as well as the on-line, increases the accuracy of the measurement by reducing laser jitter errors. These improvements required upgrading the 2- $\mu$ m laser transmitter technology. Another upgrade that is necessary for airborne DIAL systems is the pulse repetition rate. With single-pulse, 5 Hz transmitter, the on-line and off-line pulses are separated by a long period resulting in inconsistent volume sampling between the two wavelengths. This led to the adoption of the high repetition rate double-pulsed 2- $\mu$ m laser transmitter.



### 3. DOUBLE-PULSED CO<sub>2</sub> IPDA AIRCRAFT DEVELOPMENT

Double-pulse 2- $\mu\text{m}$  lasers have been demonstrated with energy as high as 600 mJ and up to 10 Hz repetition rate [31]. The two laser pulses are separated by 150  $\mu\text{s}$  and can be tuned and locked separately. Applying double-pulse laser in DIAL system enhances the CO<sub>2</sub> measurement capability by increasing the overlap of the sampled volume between the on-line and off-line [32]. To avoid detection complicity, integrated path differential absorption (IPDA) lidar provides higher signal-to-noise ratio measurement compared to conventional range-resolved DIAL. Rather than weak atmospheric scattering returns, IPDA rely on the much stronger hard target returns that is best suited for airborne platforms. In addition, the IPDA technique measures the total integrated column content from the instrument to the hard target but with weighting that can be tuned by the transmitter. Therefore, the transmitter could be tuned to weight the column measurement to the surface for optimum CO<sub>2</sub> interaction studies or up to the free troposphere for optimum transport studies. Currently, NASA LaRC is developing and integrating a double-Pulsed 2- $\mu\text{m}$  direct detection IPDA lidar for CO<sub>2</sub> column measurement from an airborne platform [32].

#### 3.1 Transmitter Development

The compact, rugged, highly reliable CO<sub>2</sub> IPDA laser transmitter is based on the Ho:Tm:YLF high-energy 2- $\mu\text{m}$  pulsed laser technology. This laser transmitter is side pumped by AlGaAs diode arrays at 792 nm. It is capable of generating 100 mJ at 10 Hz. The laser transmitter is designed to be operated in a unique double pulse format to mitigate the effect of the surface reflection difference between the on-and-off line pulses on the precision of the IPDA measurement. When the Ho upper laser level population reaches its maximum value at the end of the pump cycle, a first Q-switched pulse is generated which extracts the energy stored in the Ho <sup>5</sup>I<sub>7</sub> upper laser level, resulting in a sharp decrease in the upper laser level population. Then, a new population equilibrium between the Tm <sup>3</sup>F<sub>4</sub> and Ho <sup>5</sup>I<sub>7</sub> manifolds is established by energy transfer from the excited Tm ions towards Ho ions even though the pump no longer exists. The population at Ho upper laser level <sup>5</sup>I<sub>7</sub> comes to its second maximum about 150 micro after the first pulse. The second Q-switch pulse is triggered at this moment resulting in the desired double pulse operation with energy of up to 40 mJ depending on the time interval from the first pulse. A unique feature of this laser operation is that it provides two Q-switched pulses with a single pump pulse due to the long upper laser lifetime.

The exact wavelengths of the pulsed laser transmitter are controlled by the wavelength control unit output. The first pulse and the second pulse are injection seeded alternately by the on-line frequency and the off-line frequency. All the optical mounts are custom designed with space heritage. They are designed to be adjustable and lockable and hardened to withstand vibrations that can occur in airborne operation. Figure 4 is a picture of the engineering packaged laser transmitter. This laser transmitter is 11.5 x 26.5 x 6.4 inch (29 x 67.3 x 16.5 cm) in size, and weighted less than 70lbs.

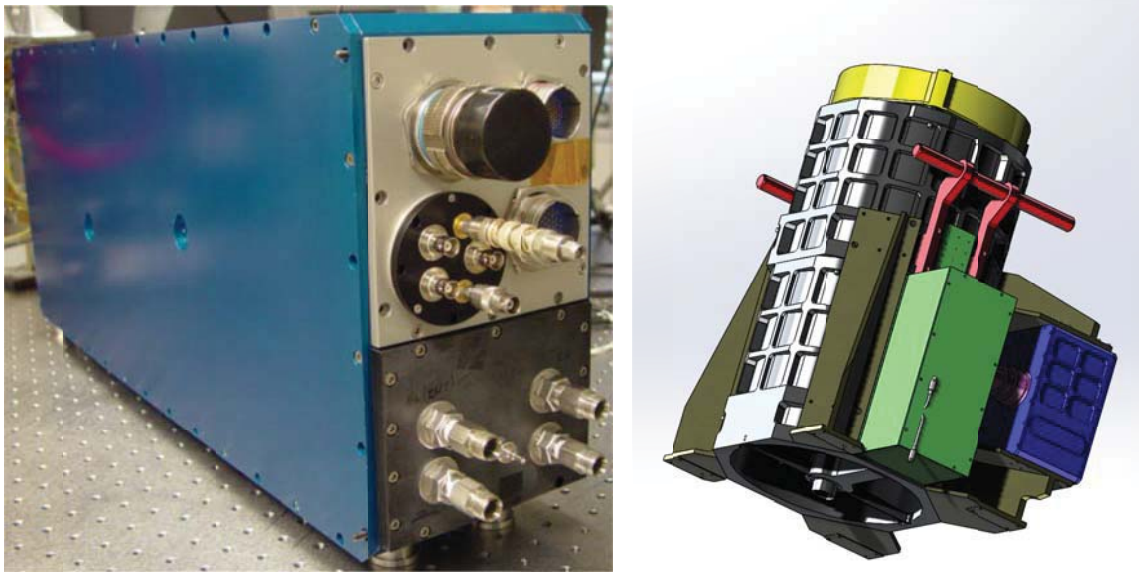


Figure 4. (Left) Packaged 2- $\mu\text{m}$  double-pulsed CO<sub>2</sub> IPDA laser transmitter. (Right) Integrated, 2- $\mu\text{m}$ , double-pulsed IPDA lidar for airborne CO<sub>2</sub> measurement [32].

### 3.2 Receiver Development

The receiver telescope is a custom designed Newtonian type with 40cm diameter aluminum primary mirror. The shape of the primary mirror is hyperbolic to minimize the aberration, so that the returning signal can be focused to less than 300  $\mu\text{m}$  diameter spot size compatible with selected detector. The telescope is designed to maintain the focus point position in the temperature range between 5 and 35  $^{\circ}\text{C}$ . A 300  $\mu\text{m}$  diameter InGaAs pin photodiode (Hamamatsu; G5853) was selected for this mission. Detector characterization resulted in an NEP of  $6.8 \times 10^{-14} \text{ W/Hz}^{0.5}$  at 30 $^{\circ}\text{C}$  that is suited for the IPDA lidar application. After amplification the lidar signals are digitized and stored by a data acquisition unit. The data acquisition unit is based on two 12-bit digitizers (Agilent; DC252). One of which monitors the laser energy and the other for the lidar return. The system runs Microsoft XP with a 64-bit/66 MHz PCI bus, which is capable of transferring data at sustained rates up to 400 MB/sec to a host personal computer. The system is able to digitize a large amount of lidar return signal at a fast trigger rate with the given specifications. Figure 4 shows the mechanical assembly for the airborne integrated 2- $\mu\text{m}$  double pulsed  $\text{CO}_2$  IPDA instrument.

### 3.3 Aircraft integration

The compact IPDA lidar system is designed for integration into a small research aircraft such as the NASA B-200 or UC-12. By considering fitting the  $\text{CO}_2$  IPDA instrument into a B-200 aircraft platform, the completed lidar system shall be easily adapted to any other bigger aircraft such as DC-8 aircraft. The mechanical design of the  $\text{CO}_2$  IPDA lidar system is compact and light weighted to meet the payload requirements for the aircraft, simultaneously with any validation instruments. The lidar integration includes mechanical system design, fabrication, integration, testing and verification of system performance with respect to aircraft's flight loading profile. A mechanical supporting structure is being designed to integrate the transmitter, the telescope and receiver into an adjustable, yet rigid platform. The primary objective of this structure is to maintain alignment integrity throughout the operating flight envelope of the aircraft, and at the same time minimize aircraft vibration from adversely affecting the lidar measurements. The mechanical structure is optimized to satisfy the stiffness, mass and volume constraints of the aircraft. Figure 5 shows a preliminary design concept of the Transmitter-Telescope-Receiver Integrating Structure of the  $\text{CO}_2$  IPDA Lidar system as installed in a B-200 aircraft. The optical portal has already been modified and installed to readily accept the lidar system as shown.

### 3.4 Ground Testing

The integrated lidar instrument will be tested in ground with horizontal target before the lidar instrument is integrated into the aircraft. The number density of  $\text{CO}_2$  along with pressure, temperature, and relative humidity information obtained from ancillary measurements from *in situ* sensors are used to retrieve dry  $\text{CO}_2$  mixing ratios. The data obtained during instrument testing will be evaluated, including comparisons to *in situ* instruments and evaluation of the data with respect to the weather and geographical environment. The goal will be evaluation of the performance of the lidar relative to the scientific measurement goals.

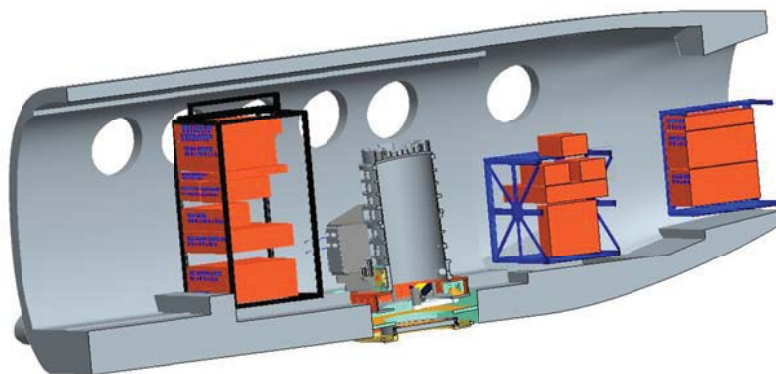


Figure 5. The 2- $\mu\text{m}$   $\text{CO}_2$  double-pulsed IPDA system integration inside an aircraft, such as the NASA B-200 [32]. The IPDA instrument, shown in figure 4, (gray) is mounted on top of the aircraft bottom window. Assisting flight-qualified instrumentations (orange) are integrated on three racks (blue and black).

## 4. CONCLUSION

Understanding atmospheric CO<sub>2</sub> interactions and transport dynamics is important for studying carbon cycle and global radiation budget on Earth. In situ and satellite based passive remote sensors have several limitations that could be recovered with active remote sensors. CO<sub>2</sub> active remote sensing has been demonstrated at NASA LaRC using the DIAL technique. The demonstration was limited to 2- $\mu$ m single-pulsed transmitter based on heterodyne and direct detection. This resulted in limited instrument capabilities in terms of measurement accuracy. Currently, NASA LaRC is developing a pulsed, high energy 2- $\mu$ m IPDA lidar instrument for CO<sub>2</sub> concentration measurement by implementing the integrated path differential absorption lidar technique (IPDA). The IPDA transmitter is a unique double-pulsed Ho laser capable of producing ~100mJ energy per pulse; and it is compactly and ruggedly packaged. High accuracy, stable and repeatable wavelength control and switching unit have been demonstrated. This unit is upgraded and engineering packaged to become a flyable unit. The IPDA also include a high quality 16 inch telescope and a commercial detector that has been purchased and characterized. Data acquisition unit, electrical control unit and thermal control unit are being developed and tested. The integrated IPDA lidar structure is being designed to fit in B-200 research aircraft. It is expected to provide a unique instrument tool for measuring atmospheric CO<sub>2</sub> concentration. Field-testing of the developed instrument will be conducted from ground and aircraft. This unique capability could be scaled for future space missions.

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