1 The Airborne Cloud-Aerosol Transport System, Part I: Overview and Description

2 of the Instrument and Retrieval Algorithms

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10 Abstract

11 The Airborne Cloud-Aerosol Transport System (ACATS) is a multi-channel Doppler 12 lidar system recently developed at NASA Goddard Space Flight Center (GSFC). A 13 unique aspect of the multi-channel Doppler lidar concept such as ACATS is that it is also, 14 by its very nature, a high spectral resolution lidar (HSRL). Both the particulate and 15 molecular scattered signal can be directly and unambiguously measured, allowing for 16 direct retrievals of particulate extinction. ACATS is therefore capable of simultaneously 17 resolving the backscatter/extinction properties and motion of a particle from a high 18 altitude aircraft. ACATS has flown on the NASA ER-2 during test flights over California 19 in June 2012 and science flights during the Wallops Airborne Vegetation Experiment 20 (WAVE) in September 2012. This paper provides an overview of the ACATS method 21 and instrument design, describes the ACATS retrieval algorithms for cloud and aerosol 22 properties, and demonstrates the data products that will be derived from the ACATS data 23 using initial results from the WAVE project. The HSRL retrieval algorithms developed 24 for ACATS have direct application to future spaceborne missions such as the Cloud-25 Aerosol Transport System (CATS) to be installed on the International Space Station 26 (ISS). Furthermore, the direct extinction and particle wind velocity retrieved from the ACATS data can be used for science applications such as dust or smoke transport andconvective outflow in anvil cirrus clouds.

29 1.0 Introduction

30 Current uncertainties in the role of aerosols and clouds limit our ability to accurately 31 model the Earth's climate system and to predict climate change. There are several 32 different types of lidar systems that can be used to measure cloud and aerosol properties 33 and motion. Cloud-aerosol lidars measure the elastic backscatter from molecules and 34 atmospheric particulates to resolve vertical profiles of spatial and optical properties of 35 clouds and aerosols. The two most common elastic backscatter lidar techniques are 36 standard backscatter lidars and high spectral resolution lidars (HSRL). The data provided 37 by these lidar systems are essential to investigations of cloud and aerosol properties for 38 numerous reasons. The vertical structure of cloud and aerosol layers resolved by lidar 39 systems cannot be accurately obtained from passive satellite or passive airborne sensors. 40 Furthermore, thin cloud optical depths are often below the detection limits of millimeter 41 cloud radar systems (Comstock et al. 2002). In situ instruments can provide critical 42 measurements of cloud and aerosol microphysical properties. However, they do not 43 easily provide vertical profiles of these measurements and can alter the physical 44 properties of the particles (Jensen et al. 2009; Zhao et al. 2011). Information obtained 45 from cloud-aerosol lidar systems can improve knowledge of cloud and aerosol properties, 46 which in turn advance parameterizations and reduce the uncertainties introduced in 47 GCMs.

48 Standard elastic backscatter lidars are the least complex and most common lidar 49 systems used to study vertical profiles of cloud and aerosol properties. Ground-based and

50 airborne systems have been used in numerous field campaigns over the past few decades. 51 In the last decade, as laser transmitters have become more reliable, the first space-based 52 elastic backscatter lidar systems were designed and launched. The Geoscience Laser 53 Altimeter System (GLAS; Spinhirne et al. 2005) was launched in January 2003 and the 54 Cloud-Aerosol Lidar Infrared Pathfinder Satellite Observations project (CALIPSO; 55 Winker et al. 2009) was launched in April 2006. These lidar systems fundamentally 56 measure vertical profiles of attenuated total backscatter, without separation of particulate 57 (Mie) and molecular (Rayleigh) scattering. There have been many methods developed to 58 retrieve the particulate extinction and particulate backscatter coefficients from a cloud-59 aerosol lidar return signal. One technique is an inversion using standard backscatter lidar 60 data developed by Fernald et al. (1972) and Klett (1981; 1985). The Klett or Fernald 61 method makes it possible to solve the standard lidar equation by assuming a ratio of 62 aerosol extinction to aerosol backscatter coefficients, referred to as the lidar ratio, is 63 known and constant throughout a particulate layer. This assumption reduces the number 64 of unknowns in the system to one. This method is commonly used to retrieve particulate extinction and backscatter coefficients from standard backscatter lidars such as CALIPSO 65 66 (Young and Vaughan 2009) and the Cloud Physics Lidar (McGill et al. 2002). The lidar 67 ratio (units of sr) is highly dependent on the optical and microphysical properties of 68 atmospheric layer being measured. The lidar ratio typically varies from about 10 to 50 sr 69 for tropospheric clouds (Del Guasta et al. 2001; Seifert et al. 2007; Yorks et al. 2011a) 70 and from about 20 to 80 sr for aerosol particles (Ackermann 1998). For cloud and 71 aerosol layers with an optical depth greater than 0.30, a 30 percent error in the assumed

lidar ratio can lead to an error in the extinction retrieval from elastic backscatter lidar
systems greater than 50 percent (Young *et al.* 2014).

74 Another method for retrieving the particulate backscatter and extinction coefficients 75 from a lidar signal is a HSRL, which is based on the use of two measured profiles instead of only one. The HSRL technique utilizes the difference in spectral distribution of the 76 77 molecular and particulate backscattered signals (Fiocco et al. 1971; Shipley et al. 1983; 78 Grund et al. 1991). High spectral resolution optical filters are required to separate the 79 particulate contribution from the molecular backscatter and resolve particulate extinction 80 and backscatter coefficients independently with no assumption about the lidar ratio 81 required. Only a few HSRL instruments have been successfully developed and operated 82 to measure cloud and aerosol optical properties from ground or aircraft platforms. The 83 iodine filter method (Piironen and Eloranta 1994) is the preferred method for HSRL 84 systems to date. Recently airborne HSRL systems that employ iodine filters have been 85 implemented and demonstrated on the NASA King Air (B-200) research aircraft (Hair et 86 al. 2008) and the German Aerospace Center (DLR) Falcon research aircraft (Esselborn et 87 al. 2008). However, a caveat of the iodine filter technique is that the actual particulate 88 backscatter spectral broadening is not measured but inferred from the total and molecular 89 backscatter. The backscattered signal also contains additional information that is 90 imparted in the scattering process, such as the Doppler shift caused by the mean velocity 91 of the particulate.

Doppler wind lidars use the frequency shift imparted on atmospheric aerosols and molecules to determine vertical profiles of the horizontal wind speed and direction. Providing these measurements on a global scale can progress understanding of

95 atmospheric dynamics and improve numerical weather predictions (Baker et al. 1995). 96 The two most common types of pulsed Doppler wind lidar systems are coherent 97 (heteodyne) detection and direct (incoherent) detection. Coherent Doppler lidars use a 98 heterodyning technique that mixes a pulsed lidar signal with a second laser signal to 99 produce a beat frequency that is related to the Doppler shift. The second continuous laser 100 beam is usually a local oscillator offset in frequency (Hall et al. 1984; Huffaker et al. 101 1984). Direct-detection lidars directly measure the frequency shift of the return signal 102 using a high spectral resolution filter, such as a Fabry-Perot interferometer or etalon, and 103 operate at shorter wavelengths than coherent systems (Benedetti-Michelangeli et al. 104 1972; Chanin et al. 1989; Garnier and Chanin 1992; Gentry and Korb 1994). One direct-105 detection method, termed multichannel (MC) by McGill and Spinhirne (1998), measures 106 the Doppler shift by imaging the etalon fringe pattern onto a multiple element detector 107 (Abreu et al. 1992; Fischer et al. 1995) The MC direct-detection concept requires the 108 etalon transmission function to be aligned with the laser wavelength. This method was 109 demonstrated by McGill et al. 1997a for a ground-based lidar developed at the University 110 of Michigan.

A MC direct-detection Doppler lidar system capable of resolving the Doppler shifts inherent to atmospheric motions can simultaneously provide information about both the scattering intensity and the motion of the particle. Such an instrument was recently developed at NASA Goddard Space Flight Center (GSFC) called the Airborne Cloud-Aerosol Transport System (ACATS). ACATS is the first lidar system to simultaneously measure cloud/aerosol properties and wind from an airborne platform. The instrument has flown on the NASA ER-2 during test flights over California in June 2012 and as part

118 of the Wallops Airborne Vegetation Experiment (WAVE) in September 2012. A 119 description of the ACATS instrument design is provided, which includes details of the 120 optical and mechanical components of the subsystems as well as the software that 121 autonomously controls the instrument operation. This work advances the effort of McGill 122 et al. 1997a and McGill et al. 1997b by demonstrating the retrieval algorithms for HSRL 123 direct measurements of cloud and aerosol optical properties (i.e. extinction) that can be 124 applied to future space-based HSRL missions. This study also presents initial ACATS 125 HSRL results and data products from the WAVE campaign.

126 2.0 ACATS Method and Instrument Description

127 2.1 ACATS Methodology

128 The ACATS instrument is a multi-channel (MC) Doppler lidar system built for use on 129 the NASA ER-2 high altitude aircraft. The MC technique passes the returned 130 atmospheric backscatter through a single etalon and divides the transmitted signal into 131 several channels (wavelength intervals), which are measured simultaneously and 132 independently (Figure 1). The resulting aerosol spectral distribution is then compared to 133 the outgoing laser distribution to infer the Doppler shift, as demonstrated in Figure 2a. 134 Subsequent measurements of the atmospheric scattered light will reveal a wavelength 135 offset that is proportional to the Doppler shift and directly related to the velocity of the 136 scattering particles (Figure 2b). The basic concept is summarized in Figures 1 and 2. 137 The MC method was demonstrated using the ground-based University of Michigan 138 Doppler lidar (McGill et al. 1997a; McGill et al. 1997b).

A unique aspect of the MC Doppler lidar concept such as ACATS is that it is also aHSRL. Both the particulate and molecular scattered signal can be directly and

141 unambiguously measured since the broad Rayleigh-scattered spectrum is imaged as a 142 nearly flat background, illustrated in Figure 2c. The integral of the aerosol-scattered 143 spectrum is analogous to the aerosol measurement from the typical absorption filter 144 HSRL technique, providing exactly the same pieces of information as a standard HSRL 145 (Figure 2d). While previous ground-based MC systems have been built and operated 146 (Benedetti-Michelangeli et al. 1972; Abreau et al. 1992; McGill et al. 1997a), there has 147 been no airborne demonstration of the technique and the method has not been used to 148 derive HSRL cloud and aerosol properties.

149 **2.2 ACATS Instrument Description**

The ACATS instrument is composed of three main subsystems; laser transmitter, telescope, and receiver optics. A picture of the ACATS instrument fully assembled, with the receiver and telescope subsystems, is shown in Figure 3. A list of the ACATS instrument parameters is provided in Table 1. The instrument also includes a heating/cooling loop to provide stable thermal operation of the laser.

155 The frequency characteristics of pulsed lasers have recently been advanced due to the 156 development of direct detection Doppler lidars and HSRLs. These techniques impose 157 further requirements compared to standard backscatter lidars, such as lasers that are 158 single frequency on a single pulse basis and more stable in time (central frequency drift 159 of less than 1 MHz per minute). An injection-seeded, pulsed Nd:YAG laser was 160 developed for the TWiLiTE instrument (Hovis et al. 2004) that achieves these frequency 161 characteristics. This laser was later replicated for the ACATS instrument and provides a 162 narrow wavelength distribution suitable for resolving the small frequency shifts due to 163 the Doppler effect. The laser operates at an output power of about 10 mJ per pulse and repetition rate of 250 Hz at 532 nm and is designed for use in the low-pressureenvironment of high-altitude aircraft.

166 The ACATS telescope employs a rotating holographic optic element (HOE) to fit the 167 small volume envelope of the ER-2 superpod and to enable vector wind measurements, 168 which requires more than one viewing direction (Figure 3c). The telescope system is set 169 for 45 degree off-nadir viewing and rotates on a bearing to permit step-stare operation. 170 The number of scan angles (up to 8) and dwell time at each scan angle is controlled by 171 software and can be modified before flight. A schematic of the optical design is presented 172 in Figure 4. As the telescope rotates, the optical alignment changes and may lead to a 173 loss in return signal if not corrected. A procedure that steps the telescope position using 174 piezoelectric actuators and scans for the largest return signal is run during flight to 175 determine the optical alignment at each scan position. The 8-inch diameter telescope is 176 also fiber-coupled to the receiver subsystem to provide greatest flexibility.

177 The primary difference between a lidar system capable of only measuring total 178 backscatter intensity (e.g., CALIOP or CPL) and an instrument that directly measures the 179 particulate extinction and Doppler shift, such as ACATS, lies in the receiver subsystem 180 (Figures 3b; 4). The heart of the ACATS receiver system is an etalon that provides the 181 spectral resolution needed for the HSRL measurement and also to resolve the Doppler 182 shift inherent in the backscattered signal. Backscattered light collected by the telescope 183 is passed through the etalon and an image of the etalon fringe pattern is created. A 184 bandpass filter is used in tandem with the etalon to reject background sunlight, permitting 185 daytime operation. The optical gap of the etalon is 10 cm with an operational diameter of 186 35 mm and plate reflectivity of 85%. As with any MC system, it is critical to maintain

the symmetry and shape of the etalon fringe pattern to avoid uncertainty in the measurement. A digital etalon controller was developed by Michigan Aerospace Corporation in which piezoelectric actuators control the etalon electronics to position and maintain the plate parallelism. Considerable work was performed to create autonomous flight software that maintains the etalon alignment over the entirety of an ER-2 flight. The signal transmitted by the etalon is then passed to the detector subsystem.

193 A holographic circle-to-point converter optic (McGill et al. 1997c; McGill and 194 Rallison 2001) is placed in the focal plane to provide the spectral detection. The circle-195 to-point converter simplifies hardware requirements, improves efficiency of measuring 196 the spectral content in the fringe pattern, and allows ACATS to utilize photon-counting 197 detection. The holographic optic is coupled to a Hamamatsu H7260 linear array detector, 198 which utilizes back-end electronics developed by Sigma Space Corporation to permit 199 photon-counting detection at count rates in excess of 50 MHz. The ACATS receiver 200 images ~1.2 orders over 24 detector channels. The ACATS etalon parameters result in a 201 measurement dynamic range of ~400 m/s, more than sufficient for typical atmospheric 202 motions.

An autonomous multi-channel data system is the final component of the instrument and was based entirely on work completed by Sigma Space Corporation in support of the CPL, UAV-CPL, and TWiLiTE lidars. The basis for the data system, the Advanced MultiChannel Scaler (AMCS) card, was first applied in the ER-2 CPL instrument. The data acquisition software is included in the data system and has its heritage in the CPL and UAV-CPL instruments. An important aspect of the ACATS data system, as developed for CPL and UAV-CPL, is the ability to downlink data in real-time from the

210 aircraft using the onboard air and navigation payload server. The data system also

211 incorporates a Novatel model OEMV-3RT2i GPS receiver and OEM-IMU-H58 inertial

212 unit to enable accurate correction for platform motion. The Novatel system provides

213 greater than 20 Hz update rates with 2 cm/s velocity accuracy. The raw ACATS data file

214 consists of photon counts at each horizontal record (1 sec), range bin (30 m) and detector

215 channel, which is then converted to atmospheric parameters such as backscatter and

216 extinction coefficients.

217 2.3 ACATS Calibration Procedures

218 Several calibration parameters are required to accurately retrieve the wind velocity, 219 aerosol and molecular backscatter from the ACATS data. These include normalization 220 constants, instrument defect function parameter, and detector nonlinearity. The 221 illumination and sensitivity of each detector channel are not the same, necessitating 222 normalization constants to compensate. The detector normalization coefficients are 223 determined using a white-light source to illuminate the telescope while the receiving 224 optics remains unchanged. These normalization constants describe the relative response 225 of the detector to broad bandwidth illumination.

The alignment of the circle-to-point converter (HOE) and Fabry-Perot fringe pattern also must be characterized. Each ring in the circle-to-point converter represents a detector channel. Since the circle-to-point converter and etalon are manufactured separately, a ring can have a dissimilar centricity and diameter compared to the fringe pattern projected onto it, resulting in signal loss to the corresponding detector channel. To complicate matters, this loss of signal can vary in each channel. In the case of ACATS the outer rings (higher detector channels) of the circle-to-point converter are not 233 perfectly concentric with the fringe pattern, requiring normalization constants to 234 compensate. The normalization coefficients are determined using the peak transmission 235 of the etalon calibration data in each channel. Assuming perfect alignment in all 236 channels, the peak transmission will remain constant as the signal is stepped through all 237 detector channels. Thus, the ACATS channel with the highest transmission represents 238 the best alignment, allowing all other channels to be normalized to the "best aligned" 239 channel. These normalization constants describe the relative signal loss of the detector 240 channel due to alignment imperfections.

To characterize the instrument defect parameter, an etalon calibration procedure has been developed for ACATS similar to the one outlined in McGill *et al.* (1997a). The etalon transmission equation as a function of detector channel (j) is expressed as (McGill 1996):

245
$$T(\Delta\lambda, j) = \sum_{n=0}^{\infty} A_n \cos\left[2\pi n \left(\frac{\Delta\lambda}{\Delta\lambda_{FSR}} + \frac{j}{N_{FSR}}\right)\right] \sin c \left(\frac{n}{N_{FSR}}\right)$$
(2.3.1)

where $\Delta\lambda_{FSR}$ is the free spectral range and is defined as the change in wavelength necessary to change the order of interference by one. The free spectral range can also be represented by the number of channels necessary to change the order of interference by one, N_{FSR}. The function A_n is defined as:

250
$$A_n = 2\left(1 - \frac{\ell}{1 - R}\right)^2 \left(\frac{1 - R}{1 + R}\right) R^n e^{-4\pi^2 n^2 \Delta d_D^2 \lambda_0^2}$$
(2.3.2)

where ℓ is the loss of light due to absorption or scattering by the etalon plates and R is the plate reflectivity. The etalon transmission equation (2.3.1) is for an idealized etalon. A real etalon function will be broadened by several effects, such as plate bowing,
microscopic plate defects, detector broadening, and off-axis aberrations.

255 For the purpose of this study, it is sufficient to use an instrument defect parameter 256 $(\Delta d_{\rm D})$ to represent the etalon broadening effects and tune the etalon model so that it 257 matches the measured ACATS spectral response. There are two important assumptions in 258 determining the ACATS defect parameter. First, the defect parameter varies with detector 259 channel to account for the variability of the etalon finesse with channel. It is also assumed 260 that any broadening effects, and thus the etalon defect parameter, will follow a Gaussian 261 distribution. The ACATS defect parameter is then determined by a calibration procedure 262 similar to the one demonstrated in McGill et al. (1997a). Software runs a calibration 263 procedure at least once per flight that varies the etalon gap using piezoelectric actuators. 264 Varying the etalon gap moves the interference fringe pattern across the detector in 128 265 small steps, sampling nearly 3 orders (42 points per order). One can then determine the 266 defect parameter for each channel by performing a least-squares fit to match the modeled 267 etalon transmission function to the ACATS measured etalon response function using a 268 similar technique to McGill et al. 1997a. The light source used to measure the ACATS 269 etalon response is the same laser that is used for atmospheric measurements. 270 Additionally, the calibration technique automatically compensates for any uncertainty in 271 computing the laser bandwidth, since the laser width follows a Gaussian distribution 272 similar to the etalon broadening term.

The measured ACATS spectrum can become distorted due to detector dead time and must be compensated for. All lidar systems that employ photon-counting detection experience this effect, which is a limitation on the number of photons that can be counted

276 in a given time interval. For ACATS, the large near-field return pushes the detector into 277 a nonlinear counting region. The nonlinear effects for this type of detector can be 278 quantified by a detector dead time coefficient. This coefficient represents the fact that 279 only one photon event can be counted at once, and the detector system has a certain time 280 delta, or dead time, before it can count another. A typical Hamamatsu linear array 281 detector, such as the one employed in ACATS, has a discriminator dead time of 65 to 75 282 ns for a discriminator maximum count rate on the order of 15 MHz. To improve this 283 performance, the ACATS Hamamatsu linear array detector is customized with a 284 discriminator built by Sigma Space Corporation under Small Business Innovative 285 Research (SBIR) funding that has a shorter discriminator dead time. This permits 286 photon-counting detection at count rates in excess of 40 MHz before there is a 10% 287 reduction in observed count rate. The ACATS detector rarely experiences count rates 288 higher than 10 MHz in atmospheric bins below 17 km (assuming an ER-2 altitude greater 289 than 19 km). Therefore, the detector dead time coefficient is less than 1.05 for 99.5% of 290 atmospheric bins with the exception of the near-field return.

291 **3.0** Development of ACATS Retrieval Algorithms

ACATS provides data products similar to other cloud-aerosol lidars, HSRL systems, and Doppler wind lidars. The system is currently set for 45 degree off-nadir viewing and the telescope rotates to allow for two orthogonal line-of-sight (LOS) wind measurements, which are then used to compute vertical profiles of horizontal wind velocity and direction within particulate layers. The ACATS retrieval algorithms and data products for the horizontal wind velocity will be presented at a later date. This paper focuses on two types of aerosol/cloud products available from ACATS data that are directly applicable to the ISS CATS instrument. Standard backscatter products are computed similar to CPL and CALIPSO (McGill *et al.* 2007). HSRL products are produced at courser resolutions (450 m vertical and 5 km horizontal), but include direct retrievals of attenuated particulate backscatter, optical depth, as well as particulate extinction and backscatter coefficients. These products are similar to those produced by other HSRL systems.

304 3.1 Development of Standard Backscatter Algorithms

305 If the measured ACATS photon counts are summed over all channels as to neglect the 306 spectral information provided by the etalon, vertical profiles of total backscatter can be 307 retrieved from ACATS data. Similar to a standard backscatter lidar system (i.e. 308 CALIOP), this total signal is composed of both the particulate scattering and molecular 309 scattering. The standard lidar equation can be regrouped and solved for the attenuated 310 total backscatter (ATB or γ), which has units of km⁻¹ sr⁻¹ and is defined as:

311
$$\gamma(\pi, r) = \left[\beta_M(\pi, r) + \beta_P(\pi, r)\right]^* e^{-2\int_0^{\sigma(r')dr}}$$
(3.1.1)

312 The molecular backscatter coefficient (β_{M}) is determined from Rayleigh scattering theory 313 (Tenti et al. 1974; Young 1981) and is proportional to atmospheric density. Furthermore, 314 the molecular extinction coefficient ($\sigma_{\rm M}$) is resolved from the molecular backscatter coefficient though the relationship $\sigma_{\rm M}(r) = \beta_{\rm M}(\pi, r) * (8/3)\pi$. The ACATS standard 315 316 ATB is computed using the standard lidar equation and calibrated by normalizing the 317 signal to the molecular backscatter profile at high altitudes where aerosol loading is 318 weakest (Russell et al. 1979; Del Guasta 1998). This calibration technique is the well-319 accepted method of calibrating backscatter lidar signals and is used in CALIPSO and 320 CPL retrievals (McGill et al. 2007). ACATS cloud and aerosol layer boundaries are

determined using a similar method to CPL (Yorks *et al.* 2011b). The advantage of using
this retrieval scheme is that the particulate layer properties can be obtained at higher
resolutions, both vertically and horizontally, than using the HSRL retrieval algorithms.
Therefore, this "standard" lidar method is used to compute ACATS attenuated total
backscatter, as well as cloud and aerosol layer boundaries at a vertical resolution of 40 m
and horizontal resolution of 400 m (2 sec).

327

3.2 Development of HSRL Algorithms

The ACATS HSRL retrieval algorithms are unique and different compared to the algorithms of current iodine filter HSRL systems (Hair *et al.* 2008). The inclusion of an etalon in the ACATS instrument design results in a more complicated ACATS lidar equation compared to the standard lidar equation and iodine filter HSRL equations. The etalon transmission function (Equation 2.3.1) is convolved with the standard backscatter lidar equation to yield the expression for the number of photon counts detected per channel (j), as derived in McGill 1996:

$$N(r,j) = \frac{E_T \lambda}{hc} O_A(r) \frac{A_T}{4\pi r^2} \Delta r Q_E T_O T_F(\lambda) \frac{\eta(j)}{n_C}$$

$$\times \sum_{n=0}^{\infty} A_{n,j} \operatorname{sinc}(\frac{n}{N_{FSR}}) \exp(\frac{-\pi^2 n^2 \Delta \lambda_L^2}{\Delta \lambda_{FSR}^2}) [\alpha(r) + \omega(r) \exp(\frac{-\pi^2 n^2 \Delta \lambda_M^2}{\Delta \lambda_{FSR}^2})]$$

$$\times \cos[2\pi n (\frac{\lambda_0 - \lambda_C}{\Delta \lambda_{FSR}} - \frac{2U_{LOS}(r) \lambda_0 \sin \varphi}{c \Delta \lambda_{FSR}} - \frac{j}{N_{FSR}})] \qquad (3.2.1)$$

335

336 The first term represents the instrument parameters and the definitions of individual 337 parameters are shown in Table 2. The second term contains the laser broadening ($\Delta\lambda_L$), 338 molecular broadening ($\Delta\lambda_M$), and the atmospheric physics. The attenuated particulate 339 backscatter (α) and attenuated molecular backscatter (ω) are expressed as:

340
$$\omega(\pi, r) = \beta_M(\pi, r) * e^{-2\int_0^r \sigma(r')dr}$$
(3.2.2)

341
$$\alpha(\pi, r) = \beta_P(\pi, r) * e^{-2\int_0^r \sigma(r')dr}$$
(3.2.3)

The Doppler shift is characterized by the second part of the third term, where U_{LOS} is the LOS wind velocity in ms⁻¹. The attenuated particulate backscatter, attenuated molecular backscatter, and LOS wind velocity are the three unknown variables in Equation 3.2.1. Since there are 24 detector channels, the ACATS system is an over-determined set of equations. These three unknowns are determined using a method developed by McGill *et al.* (1997b). First, the ACATS lidar equation (Equation 3.2.1) is linearized by expanding the relevant variables in a Taylor series. The equation is then written in matrix form:

$$\begin{bmatrix} N_{1} - N_{0,1} \\ \vdots \\ N_{24} - N_{0,24} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_{1}}{\partial U_{LOS}} \middle|_{U_{LOS,0}} & \frac{\partial N_{1}}{\partial \alpha} \middle|_{\alpha_{0}} & \frac{\partial N_{1}}{\partial \omega} \middle|_{\omega_{0}} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial N_{24}}{\partial U_{LOS}} \middle|_{U_{LOS,0}} & \frac{\partial N_{24}}{\partial \alpha} \middle|_{\alpha_{0}} & \frac{\partial N_{24}}{\partial \omega} \middle|_{\omega_{0}} \end{bmatrix} \begin{bmatrix} U_{LOS} - U_{LOS,0} \\ \alpha - \alpha_{0} \\ \omega - \omega_{0} \end{bmatrix}$$
(3.2.4)

350 This equation can also be written as:

349

$$\Delta N = G\Delta x \tag{3.2.5}$$

352 An iterative weighted least-squares fitting technique is employed to resolve these three 353 parameters and their corresponding uncertainty, in which the solution is:

$$\Delta x^{est} = \left(G^T W G\right)^{-1} G^T W \Delta N \tag{3.2.6}$$

355 where W is the weighting matrix and G is the generalized matrix to be inverted. The 356 solution for the molecular and particulate signals are linear, but non-linear for the 357 Doppler shift. This least-squares fit method was tested and proven by McGill et al. 358 (1997b) to retrieve the horizontal wind velocity. This work advances the effort of McGill 359 et al. (1997a) and McGill et al. (1997b) by developing HSRL retrievals of cloud and 360 aerosol properties. The first step is to compute the molecular backscatter coefficient ($\beta_{\rm M}$) and two-way transmission (T_M^2) from Rayleigh scattering theory and meteorological data 361 362 from a nearby radiosonde. The definition for the attenuated molecular backscatter (Eq. 363 3.2.2) can be rewritten in terms of the two-way transmission, corrected for the slant path, and solved for the two-way particulate transmission (T_p^2) : 364

365
$$T_P^2(r) = \left[\frac{\omega(\pi, r)}{\beta_M(\pi, r)T_M^2(r)}\right]^{\cos\theta}$$
(3.2.7)

Therefore, the two-way particulate transmission can be determined without making unnecessary assumptions about the lidar ratio, as in the Klett or Fernald method (Fernald *et al.* 1972; Klett 1981, 1985). Once T_p^2 is known, the definition of the attenuated particulate backscatter (Eq. 3.2.3) can be rewritten and used to directly retrieve the particulate backscatter coefficient (β_P):

371
$$\beta_P(\pi, r) = \frac{\alpha(\pi, r)}{T_M^2(r)T_P^2(r)}$$
(3.2.8)

372 The particulate optical depth is then:

373
$$\tau_P(r) = -\frac{1}{2} \ln \left[T_P^2(r) \right]$$
(3.2.9)

374 The particulate extinction coefficient (σ_P) is directly retrieved using the equation:

$$\sigma_{P}(r) = \frac{\partial \tau_{P}(r)}{\partial r}$$
(3.2.10)

and the particulate lidar ratio is:

$$S_P(r) = \frac{\sigma_P(r)}{\beta_P(r)}$$
(3.2.11)

This method is used to compute profiles and layer-integrated values of the aforementioned variables at a vertical resolution of 450 m and horizontal resolution of 5 km (25 sec). Their corresponding uncertainties are computed using propagation of errors. If high-resolution optical properties are desired, the directly retrieved lidar ratio can be utilized as a parameterization to compute high-resolution optical properties using the Klett or Fernald method.

384 4.0 Initial Results from WAVE Campaign

385 During the period of 9 to 27 September 2012, ER-2 aircraft flights were 386 conducted out of Wallops Island, VA as part of the WAVE project. These flights were 387 planned over land, targeting specific land and vegetation surfaces with a scientific 388 objective of simulating Ice, Cloud and land Elevation Satellite 2 (ICESat-2) data using 389 the Multiple Altimeter Beam Experimental Lidar (MABEL; McGill et al. 2013). ACATS 390 was a payload on a total of 13 ER-2 flights, which included observations of thin cirrus 391 clouds, and smoke layers. During these flights, software directed the ACATS telescope to 392 rotate counter-clockwise to four look angle positions denoted by azimuth angle relative to 393 the aircraft nose: 0° (fore), 90° (right), 180° (aft), and 270° (left). At each look angle, the 394 dwell time was set for 60 seconds. The WAVE campaign represents the first science 395 flights for the ACATS instrument in which the telescope rotated and more than one look 396 angle was used. Due to limited time before the project, the telescope alignment was

397 optimized only at the 270-degree look angle. The telescope alignment for the other three 398 look angles was performed in the field using the new and untested in-flight telescope 399 alignment procedure. Portions of flights, and in some cases entire flights, were used to 400 test and refine the etalon calibration procedure and telescope alignment. Furthermore, 401 only two look angles were used for some flights if proper telescope alignment was not 402 achieved at all four look angles. An example of the photon counts summed across all 24 403 detector channels at each of the four look angles from the 26 September 2012 flight is 404 shown in Figure 5 and demonstrates the ability of ACATS to observe cirrus clouds 405 (between 10 and 12 km) at multiple look angles. Overall, ACATS collected science data 406 with high signal-to-noise ratio (SNR) in at least one look angle during 8 of the 13 total 407 flights. The telescope alignment and LOS wind retrievals will be improved before future 408 ACATS flights. This study will focus on ACATS retrievals of cloud and aerosol 409 properties from the WAVE project, particularly those at the 270-degree look angle and 410 high quality data from the other look angles.

411 There were several flights during WAVE in which ACATS collected quality data 412 at multiple look angles. Perhaps the best ACATS performance was on the 26 September 413 ferry flight back to Palmdale, CA when all four look angles were well aligned. Figure 6 shows the 532 nm ATB $(km^{-1} sr^{-1})$ computed using the standard method (a), the 414 Attenuated Particulate Backscatter (km⁻¹ sr⁻¹) using the HSRL method (b), and the 415 directly-retrieved Particulate Extinction Coefficient (km⁻¹) at the 0 degree look angle (c) 416 for the flight on 26 September 2012. Clearly visible in these images are cloud layers 417 418 observed by ACATS as the ER-2 flew over the Ohio River Valley (20:28:05 to 21:30:00 419 UTC) and over North Dakota (about 00:24:10 UTC). ACATS also measured a large smoke plume (00:24:10 to 02:10:00 UTC) that extended as high as 6 km over Montana.
The images in Figure 6 demonstrate the typical ACATS cloud and aerosol data products.
The extinction and backscatter values are typical for cloud and smoke layers and appear
to be similar across retrieval methods.

424 The ACATS telescope alignment on the 14 Sep. flight at the 270 degree look 425 angle was the best for the entire campaign, making it a good case to assess biases in the 426 two retrieval methods. Figure 7 shows the 532 nm ATB computed using the standard 427 method (a) and using the HSRL method (b). The latter is essentially $\alpha + \omega$. Cirrus 428 clouds between 9 and 13 km are observed throughout the flight. Figure 8 shows the 429 mean profiles of 532 nm ATB computed using the standard method (blue) averaged to 430 the resolutions of the HSRL products, as well as the ATB using the HSRL method (red) for the grey shaded box in Figure 7b centered around 22:32:22 UTC. Both ATB profiles 431 432 follow the modeled molecular profile closely above the cirrus layer and show similar 433 structure inside the cirrus layer. The standard ATB retrieval is about 10 percent higher 434 than the ATB computed using the HSRL method within the cirrus layer. This difference 435 is likely due to the errors in the calibration technique used in both retrievals. The error in 436 the CPL calibration constant is estimated to be around 5 percent at 532 nm due to signal 437 noise and the presence of aerosols in the CPL calibration zone (Campbell *et al.*, 2008; 438 Vaughan et al. 2010). Errors in the determination of the etalon defect parameter can lead 439 to errors of as much as 5 percent in the HSRL retrieved attenuated molecular and 440 particulate backscatter. Although this comparison provides confidence in the ACATS 441 HSRL algorithms, it does not resolve any possible instrument biases. To address this 442 issue, the ACATS standard backscatter and HSRL products are compared to coincident

443 CPL cloud and aerosol properties during the WAVE campaign in a companion paper.

444 **5.0 Summary**

445 A new multi-channel direct-detection Doppler wind lidar has been developed at NASA GSFC for use on the NASA ER-2 called the Airborne Cloud-Aerosol Transport 446 447 System (ACATS). ACATS employs a Fabry-Perot interferometer to provide the spectral 448 resolution needed to retrieve the Doppler shift, similar to the ground-based University of 449 Michigan MC direct-detection Doppler wind lidar (McGill et al. 1997a). The ACATS 450 instrument design includes a seeded laser and circle-to-point converter, as well as a 451 heating/cooling loop for stable laser performance during airborne operation. The ACATS 452 telescope rotates to four look angles to permit the retrieval of the horizontal wind velocity 453 within atmospheric layers. ACATS also advances the technology of a MC direct-454 detection Doppler wind lidar by demonstrating the utility of such an instrument for HSRL 455 retrievals of cloud and aerosol properties.

456 The nature of a MC direct-detection Doppler wind lidar such as ACATS permits 457 three types of cloud and aerosol lidar retrievals: standard backscatter lidar products such 458 as ATB and layer boundaries, directly retrieved cloud and aerosol optical properties such 459 as extinction and lidar ratio using the HSRL technique, and horizontal wind velocity of 460 the cloud or aerosol particles within an atmospheric layer. This paper outlines the 461 retrieval algorithms for all two of these types of ACATS data products, focusing on the 462 HSRL derived cloud and aerosol properties. The first ACATS science flights were 463 conducted during the WAVE project in September 2012. Initial results demonstrate the 464 effectiveness of ACATS as an airborne HSRL system. The HSRL ATB retrieval for

465 cirrus observed during the 14 September flight at the 270-degree look angle agrees with 466 the ATB derived using the standard backscatter method to within 10 percent. Since the 467 ISS CATS HSRL receiver is designed similar to ACATS, the algorithms and data 468 products developed for ACATS have direct application to this future spaceborne mission 469 Furthermore, the ACATS HSRL and wind products can be used for science applications 470 such as aerosol transport, smoke plume properties and convective outflow in tropical 471 storms.

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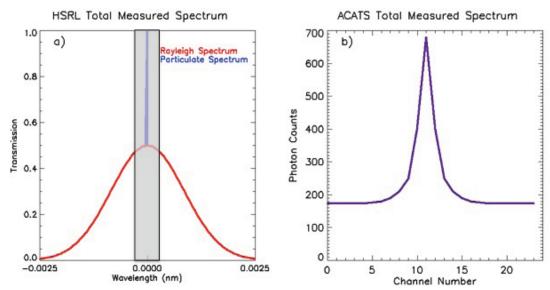
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611 612	
613	Table 1. Primary system parameters for ACATS lidar.
015	Table 1. Trimary system parameters for ACATIS findar.

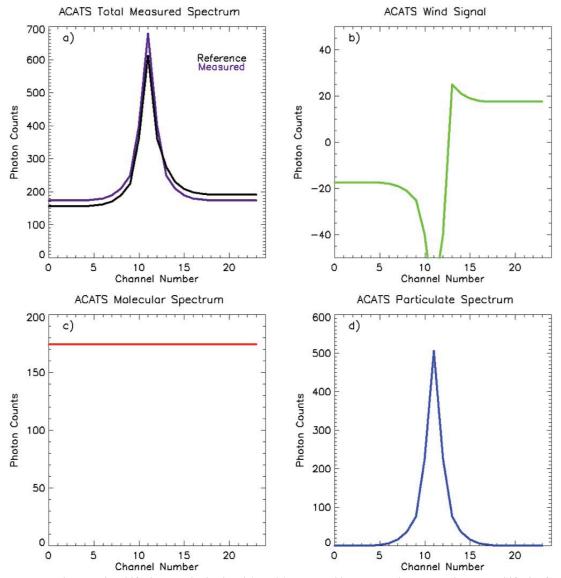
Parameter	Value
Laser Type	Nd: YAG, seeded
Wavelength	532 nm
Laser Repetition Rate	250 Hz
Laser Output Energy	~10 mJ/pulse
Telescope Diameter	8 inches
Viewing Angle	45 degrees
Telescope FOV	350 µradians (full angle)
Bandpass Filter	150 pm FWHH
Etalon Spacing	10 cm
Etalon Reflectivity	85%
Orders Imaged	1.2
Detector Channels	24
Raw Range Resolution	30 m
Horizontal Resolution	1 sec (~200 m)
Platform Speed	~200 m/s
Platform Altitude	~ 20 km (65,000 ft)

Variable	Definition	Units
N(r)	number of photons detected per range bin	-
r	distance to the scattering particle	m
j	detector channel	-
E _T	transmitted laser energy	J
λ	laser wavelength	m
h	Planck's constant	J sec
с	speed of light	$m s^{-1}$
A _T	area of lidar telescope	m^2
Δr	range bin width	m
Q_{E}	detector quantum efficiency	-
To	system optical efficiency	-
T _F	optical filter efficiency	-
$O_A(r)$	overlap function	-
n _c	number of detector channels	-
η _c	detector normalization	-
N _{FSR}	free spectral range (channel number)	-
$\Delta\lambda_{FSR}$	free spectral range (wavelength)	m^{-1}
$\Delta \lambda_{\rm L}$	laser broadening 1/e width (wavelength)	m^{-1}
$\Delta \lambda_{M}$	molecular broadening 1/e width (wavelength)	m^{-1}
$\alpha(\mathbf{r})$	attenuated particulate backscatter coefficient	$m^{-1} sr^{-1}$
$\omega(\mathbf{r})$	attenuated molecular backscatter coefficient	$m^{-1} sr^{-1}$
φ	off-nadir pointing angle	degrees
U _{LOS}	LOS wind velocity	$m s^{-1}$
λ_c	center position of the laser linewidth	m
λ _c	center wavelength of the etalon	m

Figures

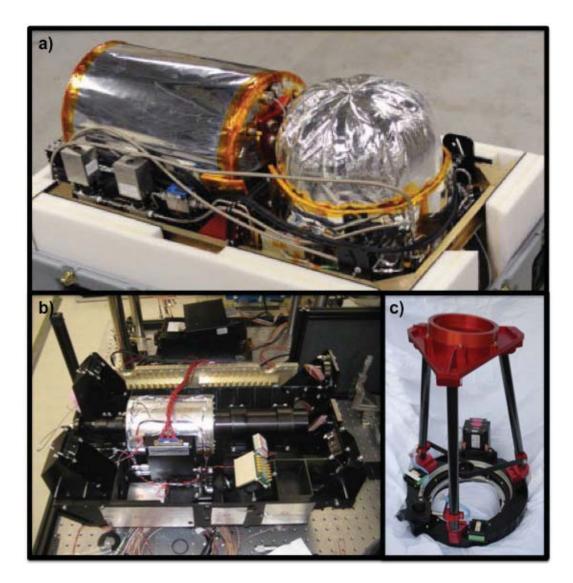


642 643 644 645 Figure 1. The ACATS method images the grey shaded area of the returned atmospheric signal (a) onto a 24 channel array detector, which measures the photon counts at each wavelength interval independently as a total backscattered signal (b).

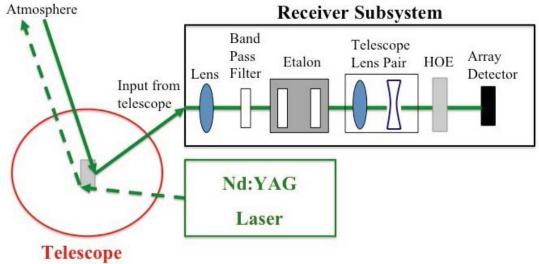


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Figure 2. The Doppler shifted atmospheric signal (purple) measured by ACATS is compared to an unshifted reference spectrum (a), which yields the Doppler wind signal (b) of the ACATS measurement. The broad Rayleigh scattered spectrum (c) is measured by ACATS as a nearly flat background of the total atmospheric return signal, resulting in a 650 sharp particulate spectrum (d) that is directly measured.

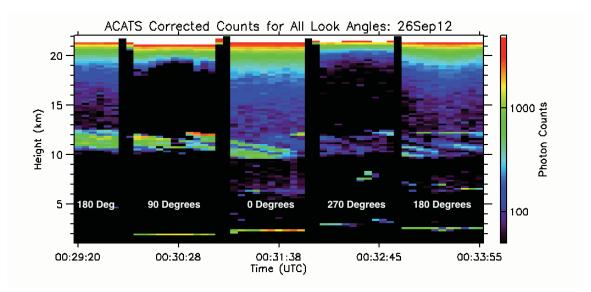


653 654 655 656 657 Figure 3. The fully assembled ACATS instrument (a) includes the receiver tube covered in insulation (left) and a pressurized telescope dome (right). A picture of the inside of the receiver subsystem (b) shows the etalon (silver device in the middle), the 24-channel array detector, and circle-to-point converter. The inside of the telescope subsystem (c) contains a motor to rotate the telescope and a HOE.



ACATS Optical Schematic

658 659 Figure 4. The ACATS optical schematic shows the outgoing 532 nm laser light (dashed green), originating from the 660 Nd:YAG laser, directed out of the telescope by a mirror. The return signal (solid green) is passed through the telescope 661 662 and into the receiver subsystem using an optical fiber, where it is transmitted through optical lenses and filters, including the etalon. 663



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665 Figure 5. ACATS photon counts from an ER-2 flight on 26 September 2012. The high count rates between 10 and 12 666 km show the detection of a cirrus layer at all four look angles at intervals of 60 seconds.

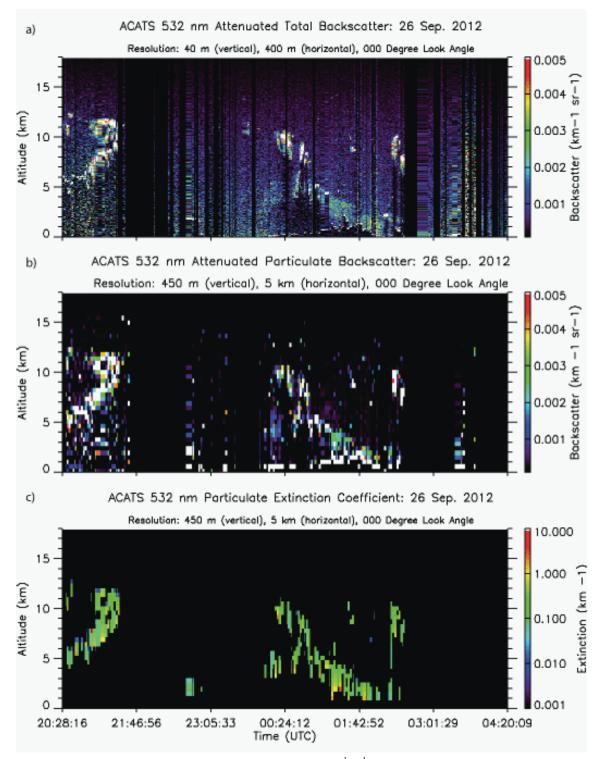


Figure 6. The ACATS 532 nm Attenuated Total Backscatter ($\text{km}^{-1} \text{ sr}^{-1}$) computed using the standard method (a), the Attenuated Particulate Backscatter ($\text{km}^{-1} \text{ sr}^{-1}$) derived using the HSRL method (b), and the directly-retrieved Particulate Extinction Coefficient (km^{-1}) at the 0 degree look angle (c) for the ER-2 flight on 26 September. ACATS observed clouds as the ER-2 flew over the Ohio River Valley (20:28:05 to 21:30:00 UTC) and a large smoke plume (00:24:10 to 02:10:00 UTC) that extended as high as 6 km over Montana.

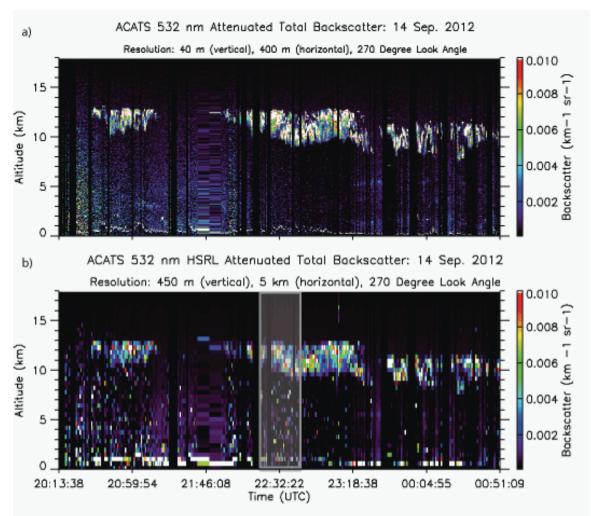
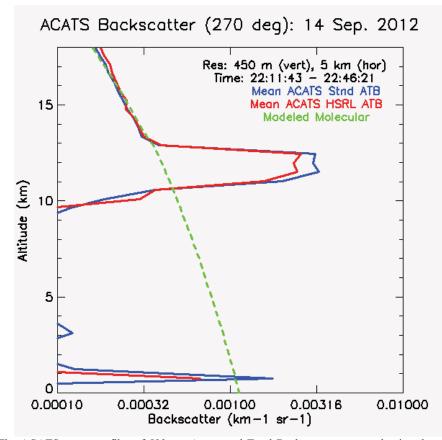




Figure 7. The ACATS 532 nm Attenuated Total Backscatter computed using the standard method (a) and using the HSRL method (b) at the 270 degree look angle for the ER-2 flight on 14 September. The grey box focuses on a 35 minute segment in which the mean profiles are compared in Figure 8 for cirrus clouds.



680 681 682 683 Figure 8. The ACATS mean profiles of 532 nm Attenuated Total Backscatter computed using the standard method (blue) averaged to the resolutions of the HSRL products, as well as the Attenuated Total Backscatter using the HSRL method (red) for the grey shaded box in Figure 7b (22:11:43 - 22:46:21 UTC).