



# **Background Oriented Schlieren (BOS) and other Flow Visualization Developments & Applications at GRC**

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**21-22 November 2013**



# BOS and Other Flow Vis Developments & Applications

**BOS, shadowgraph, schlieren, focusing schlieren**

## Recent developments, applications & continuations:

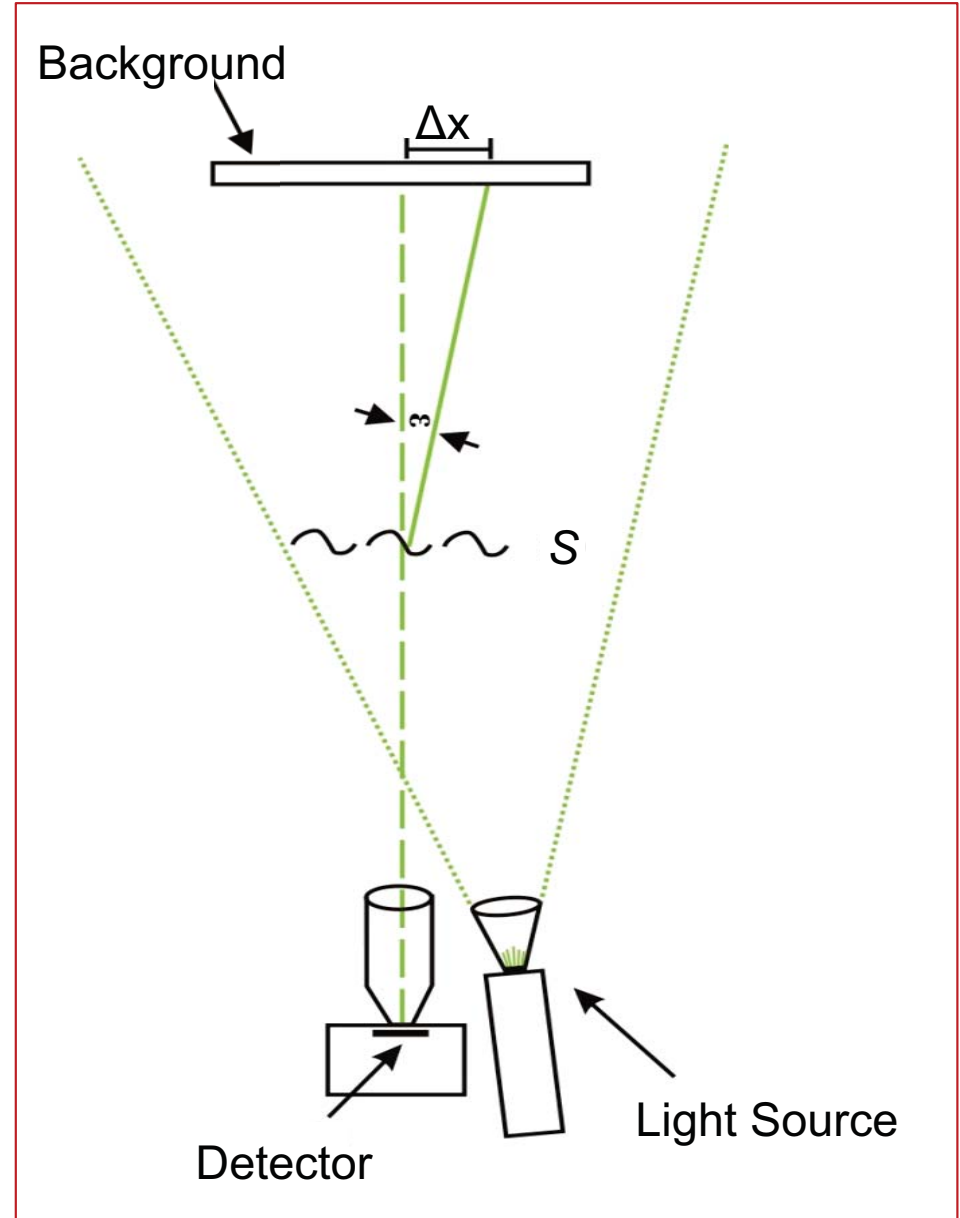
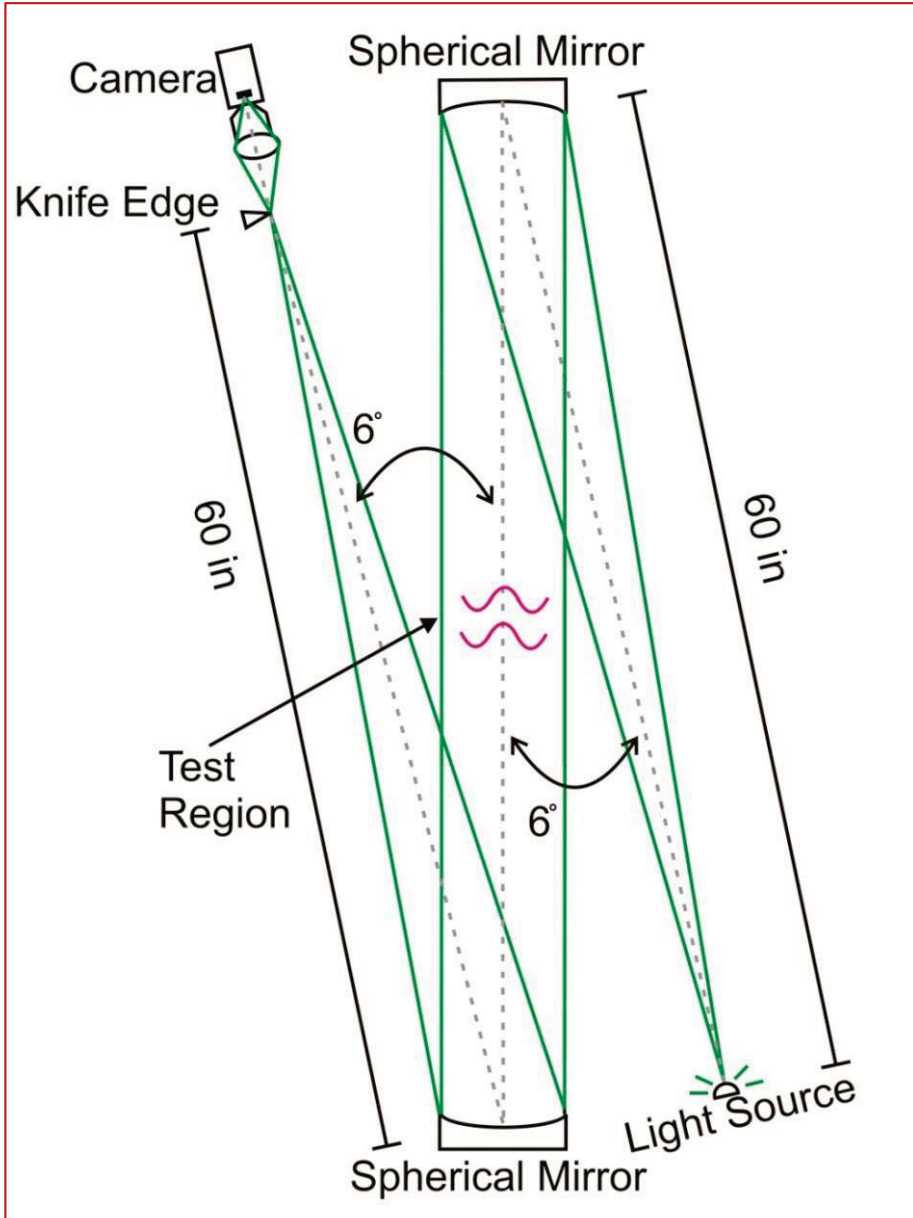
- **Investigate screech in an open jet rig**
  - Initial study performed with BOS
  - Continued on with multiple flow vis techniques / comparative study
- **Investigate BBSN in the Jet Surface Interaction Tests**
  - BOS implemented in the Aero Acoustic Propulsion Lab
  - Parametric study carried out in an open jet rig
  - Comparative study
- **Investigate miscellaneous topics of interest**



# Brief Overview – Background Oriented Schlieren (BOS)

- BOS is a more recent development of the schlieren and shadowgraph techniques used to non-intrusively visualize density gradients.
- Based on an apparent movement of the background when imaged through a density field onto a detector plane.
- Schlieren and shadowgraph techniques can be difficult, time consuming, and costly due to large mirrors/lenses and precise alignment.
- BOS captures the density field but only requires a CCD camera, light source, and a high-contrast background.

# Classical Schlieren vs. BOS

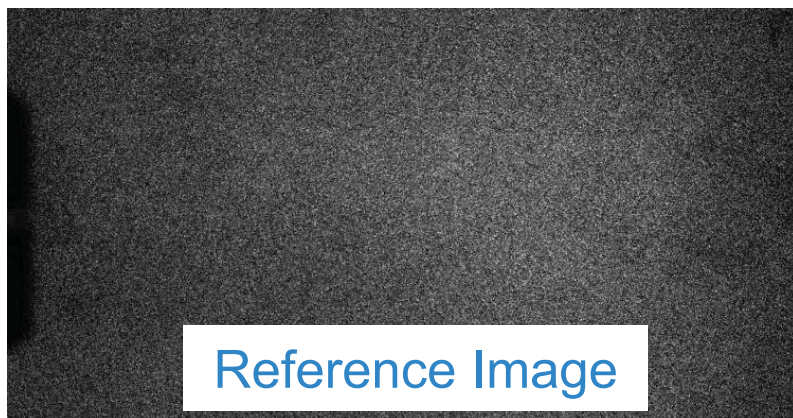


**Classical Z-type Schlieren**

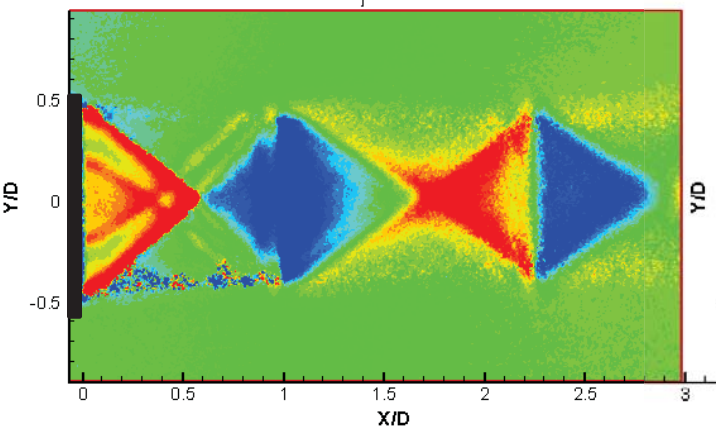
**BOS**

# Sample BOS Data

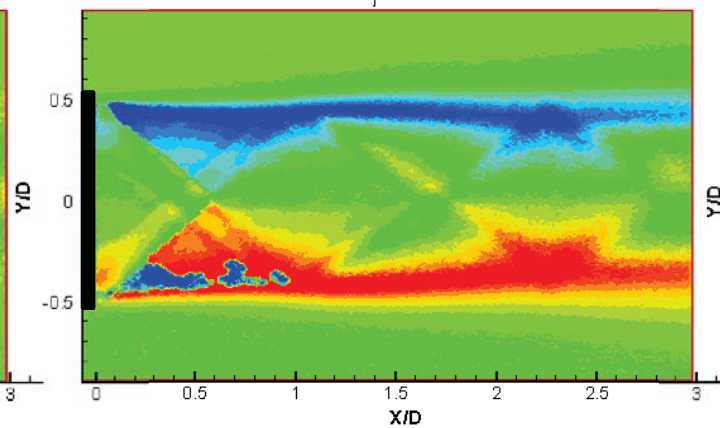
- It is necessary to take **two** images when acquiring BOS data
- Shift between the two images can be calculated by correlation methods (PIV)



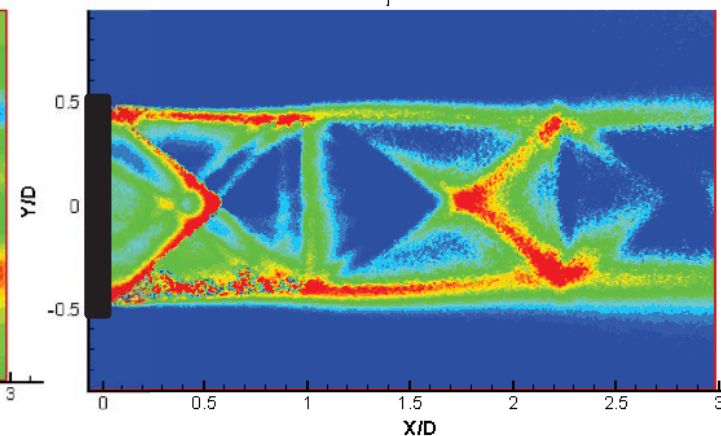
- BOS has the unique ability to distinguish the density gradient as a vector quantity

 $M_j = 1.6$ 

Axial (x) gradient

 $M_j = 1.6$ 

Radial (y) gradient

 $M_j = 1.6$ 

Resultant Magnitude



# Particle Size – PIV Optimization

3 guidelines to follow to optimize correlation peak results:

1. Nominally 10 particles per sub-region
2. Maximum expected displacement  $\Delta x_{max} < 1/4^{\text{th}}$  sub-region size
3. Imaged particle diameter  $d_e$  spans 1-2 pixels

$$d_{diff} = (2.44(1 + M)\lambda f\#)^2 \longrightarrow d_e = \sqrt{(d_p M)^2 + (2.44(1 + M)\lambda f\#)^2}$$

Correlation peak estimation error

$$\sigma_{\Delta x} = \frac{d}{N} = \frac{\sqrt{2}d_e}{N}$$

Nominally  $\sigma_{\Delta x} = 0.1$  pixel

Full scale error

$$\sigma_u = \frac{\sigma_{\Delta x}}{\frac{1}{4}N}$$

Nominally  $\sigma_u = 1\%$



# **BOS used in an initial study to investigate screech in an open jet rig**

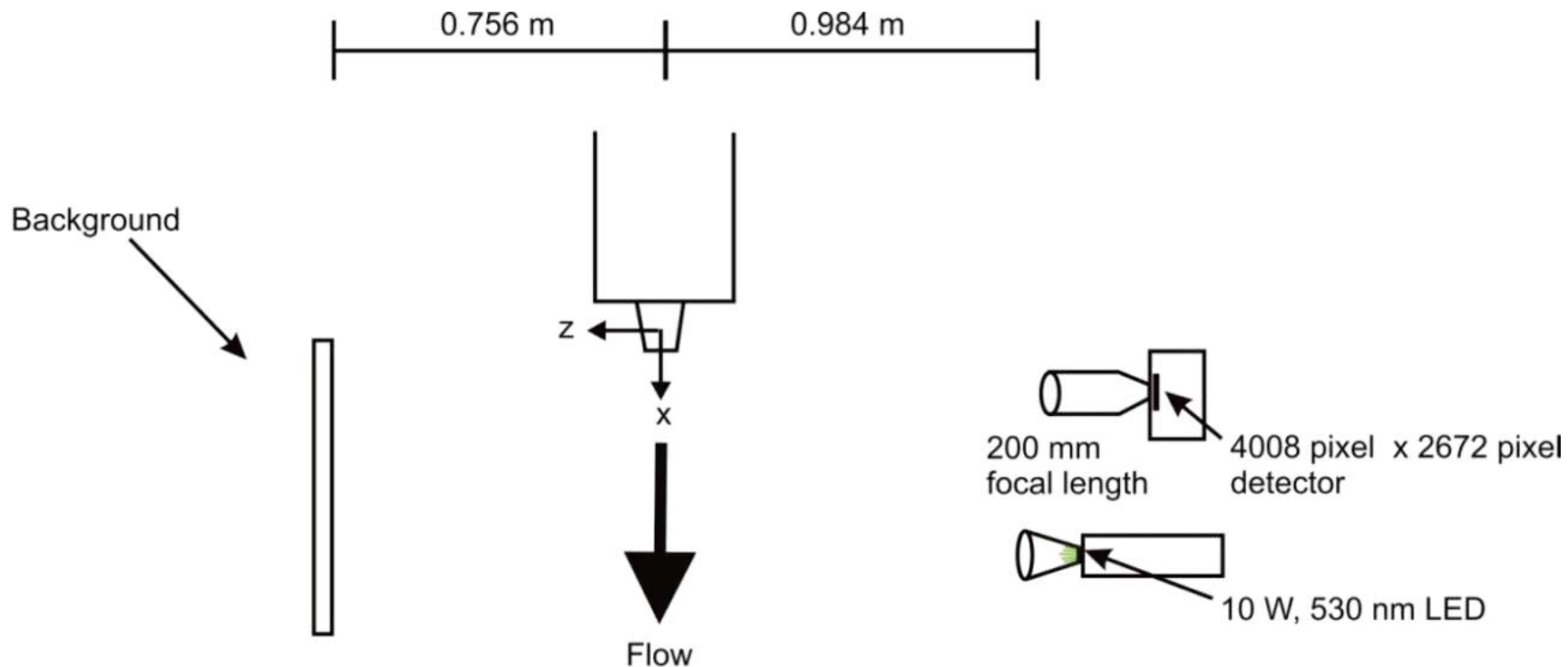


# BOS and Screech

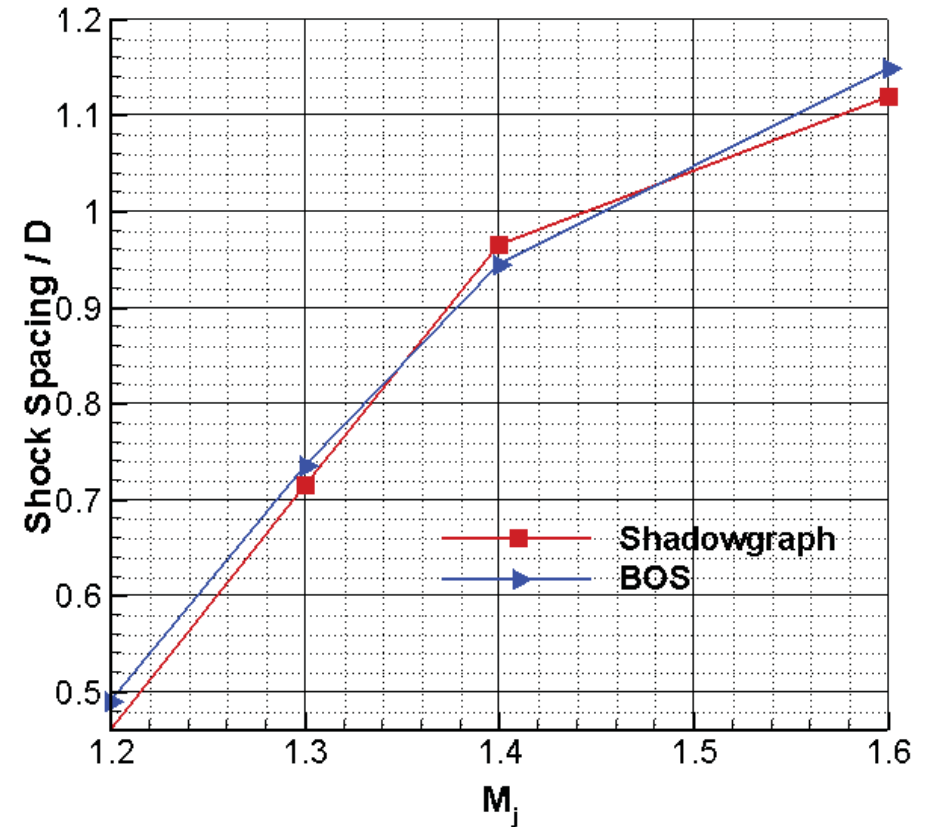
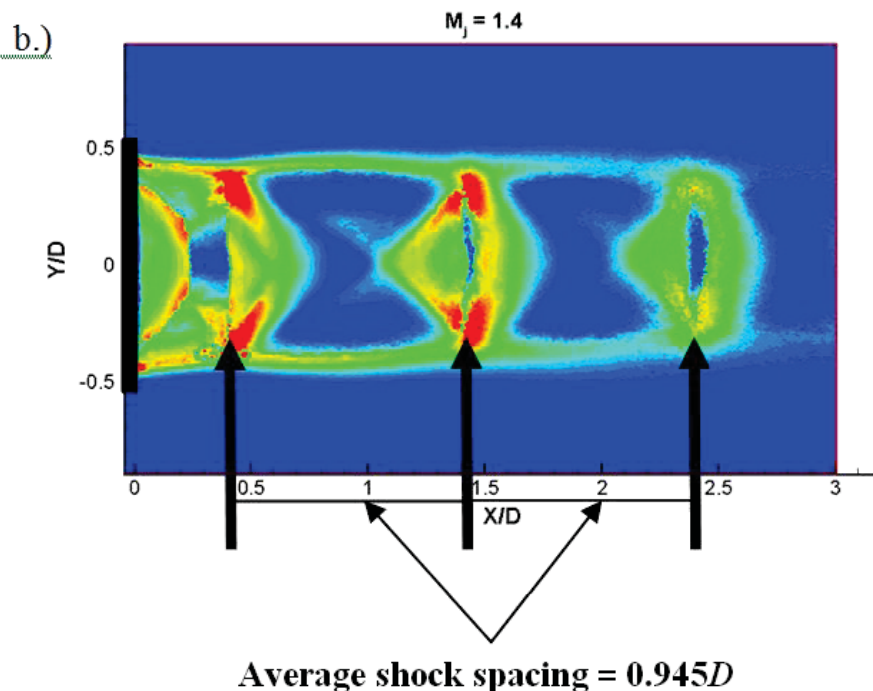
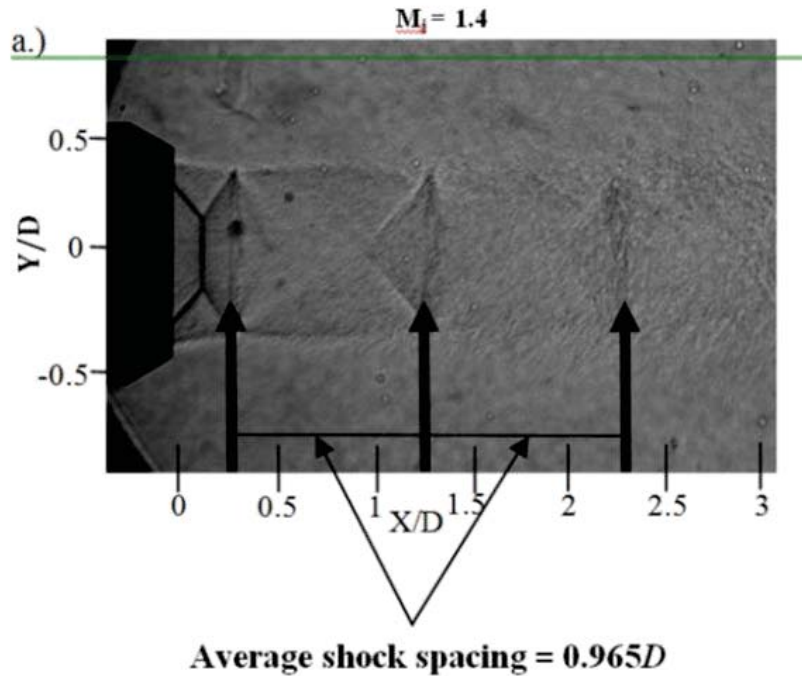
- Screech tones are a component of noise generated by supersonic jets operating at imperfectly expanded conditions
  - Dominant screech tone goes through mode-switching or stage-jumps as the Jet Mach number ( $M_j$ ) is increased
- Screech is not completely understood
  - Does the shock spacing adjust to accommodate a new wavelength during the stage jump?
  - If so, we theorized the shock spacing would display an abrupt change during the stage jump
- Goal to measure the shock spacing across various screech stage jumps to determine its behavior using a flow visualization technique
  - BOS is good choice
  - In order to validate the shock spacing measurement using BOS it is compared to previously acquired shadowgraph data



# Experimental Setup and Procedure



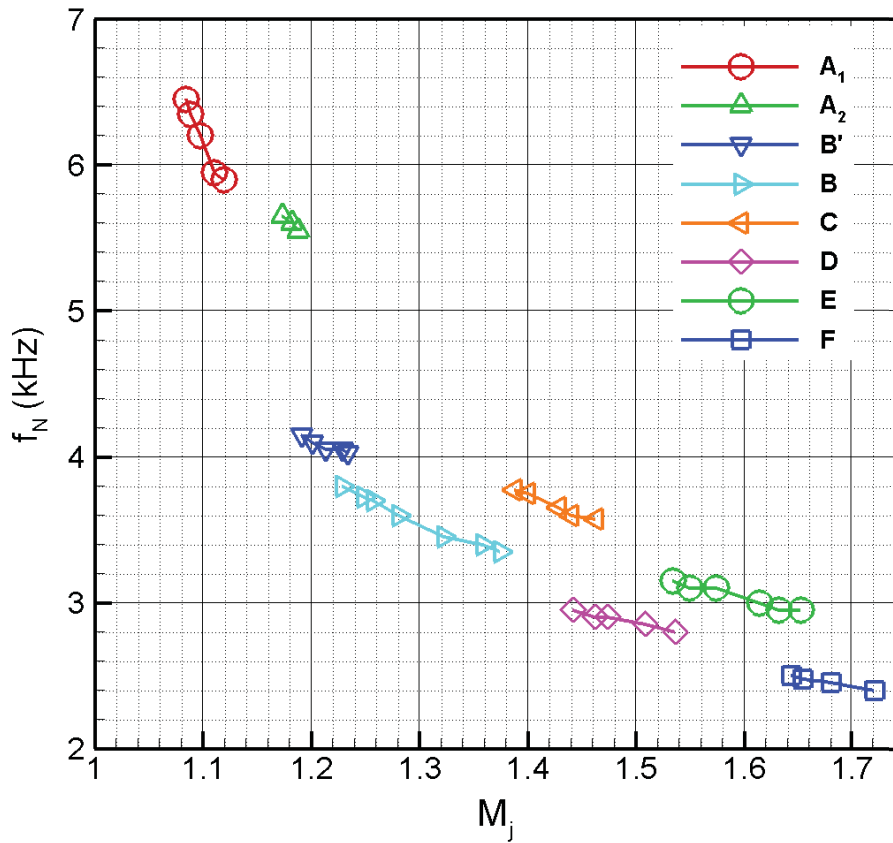
# Results: Shock Spacing Measurement Using BOS



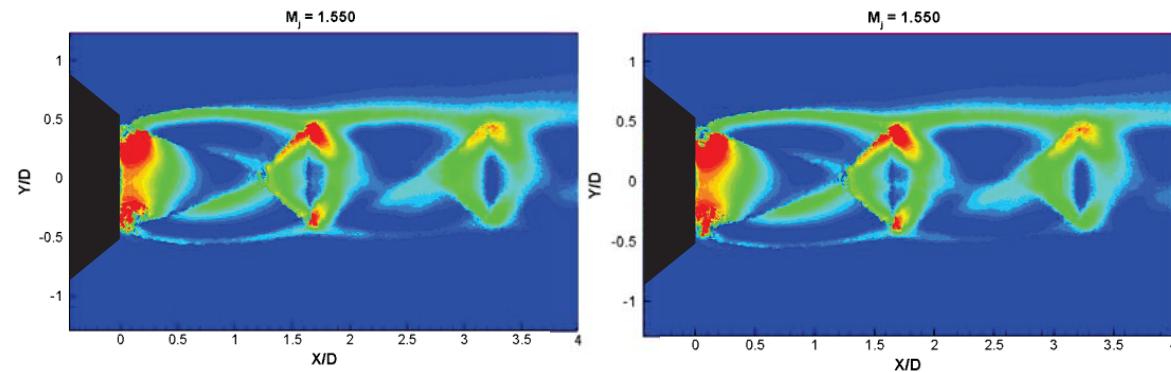
- 50.8 mm nozzle,  $M_D=1.8$
- Flow and shock boundaries are sharper in the shadowgraph
- The overall agreement is good, particularly the inferred shock spacing

# Results: Screech Frequency versus $M_j$

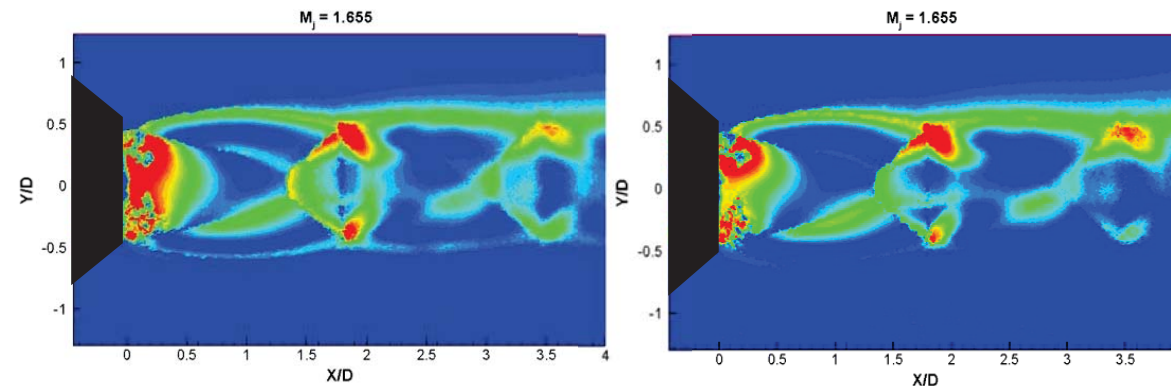
## 37.6 mm Circular Convergent Nozzle



**Hysteresis:** stage jump occurs at a different location depending on whether  $M_j$  is increased or decreased



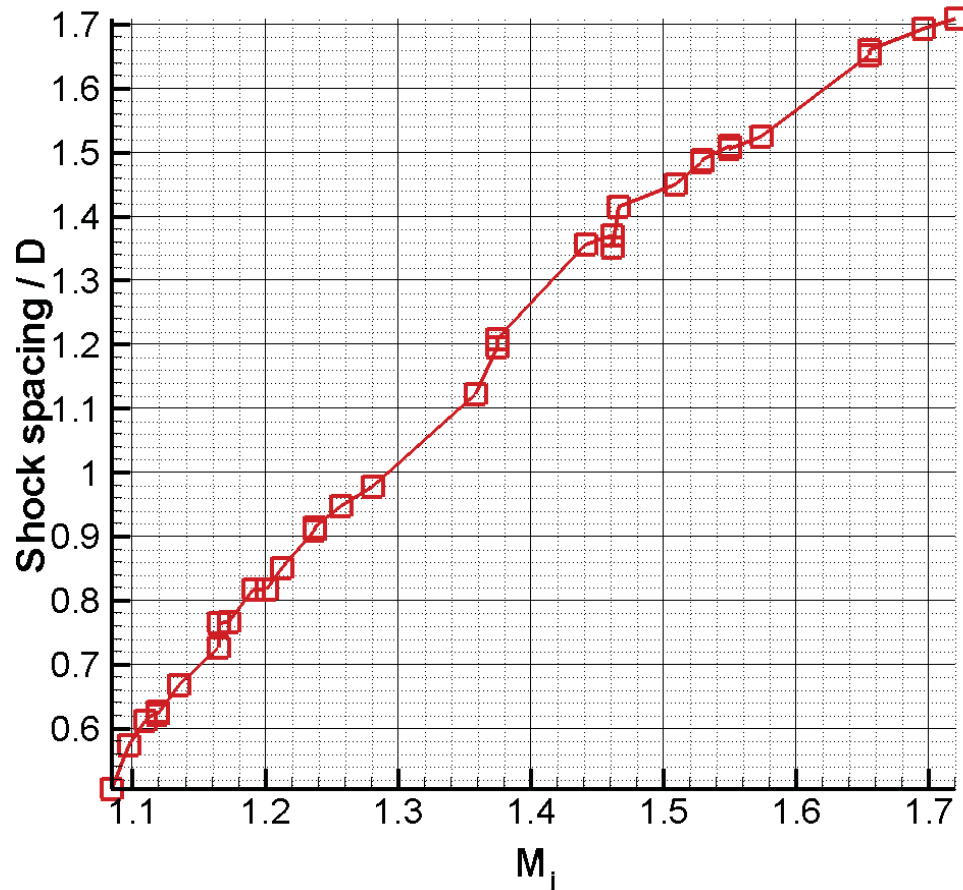
$M_j = 1.550$  - overlapping stage jump region D and E



$M_j = 1.655$  - overlapping stage jump region E and F



# Results: BOS Shock Spacing Measurements

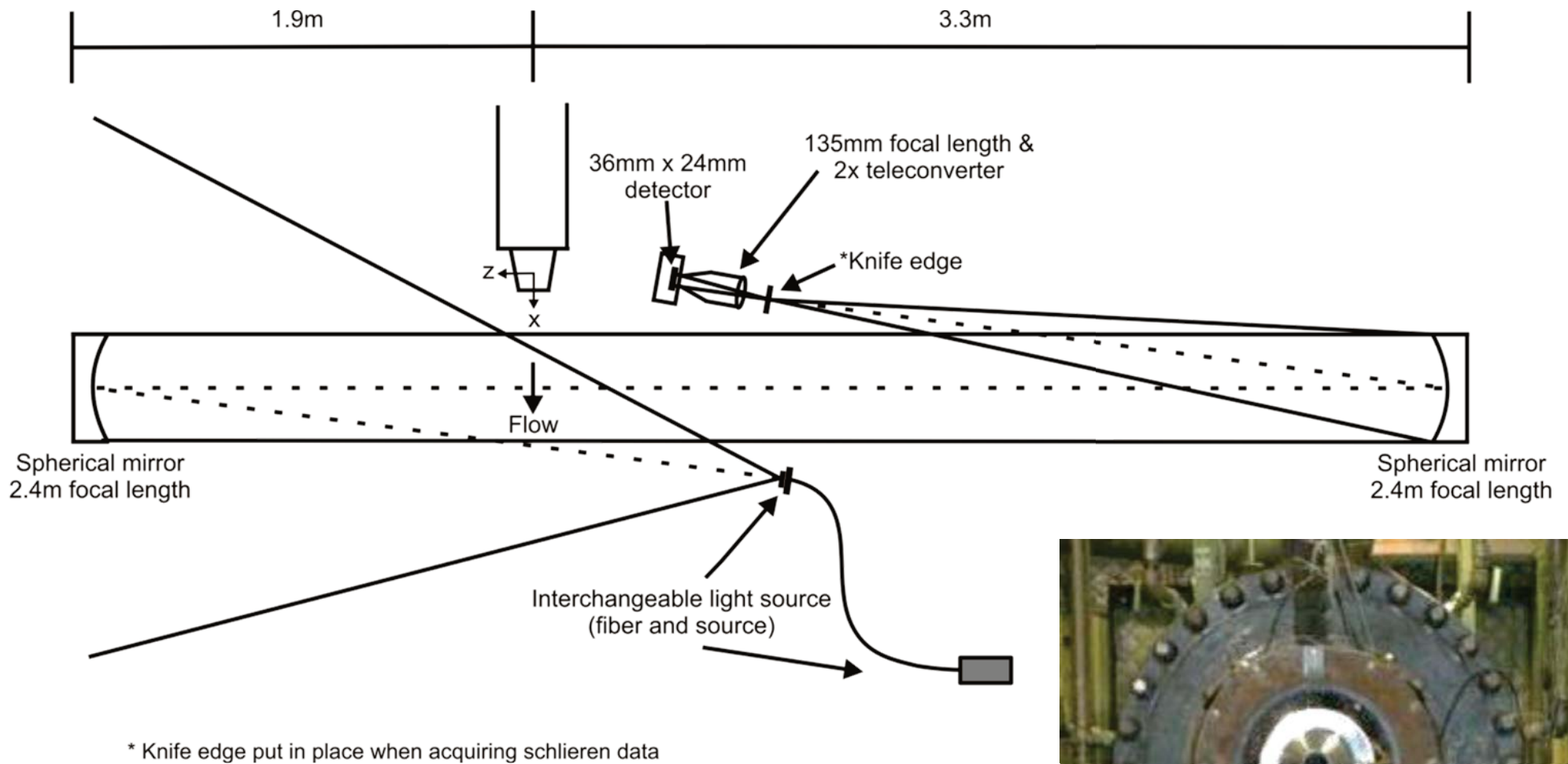


- Shock spacing follows the expected monotonic trend – no large departures
- Does NOT display an abrupt change for overlapping stages at the  $M_j$  where hysteresis occurred
- Therefore inferred shock spacing is NOT the parameter that adjusts to accommodate a new frequency when a stage jump occurs

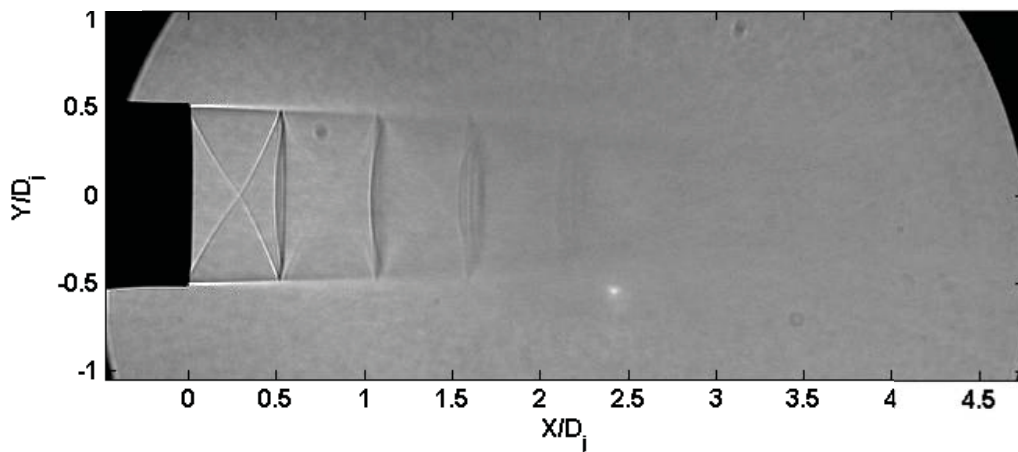
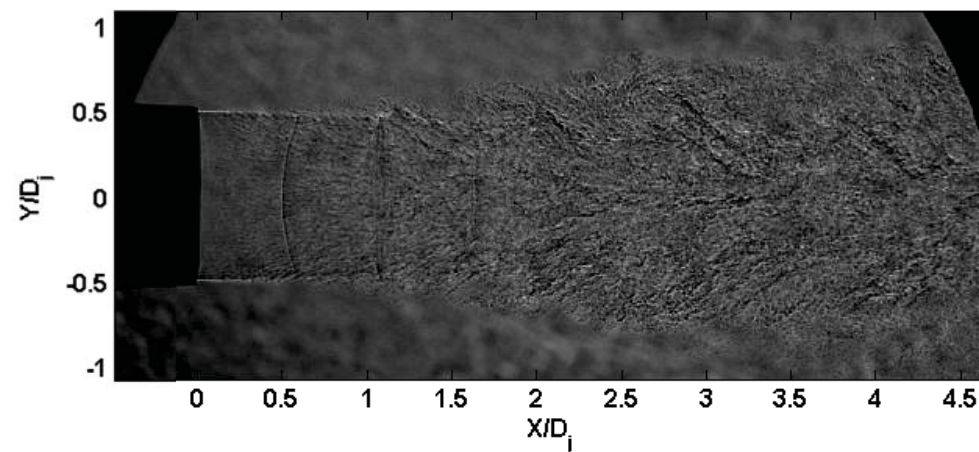
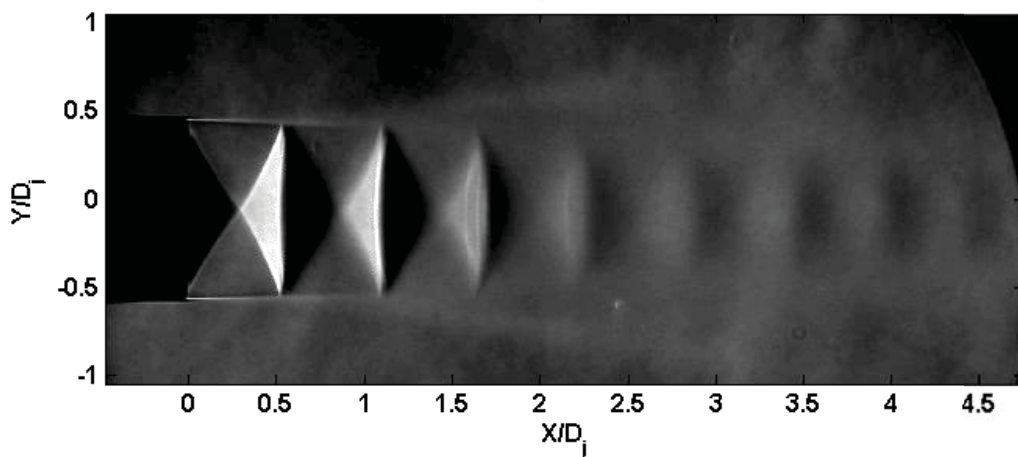
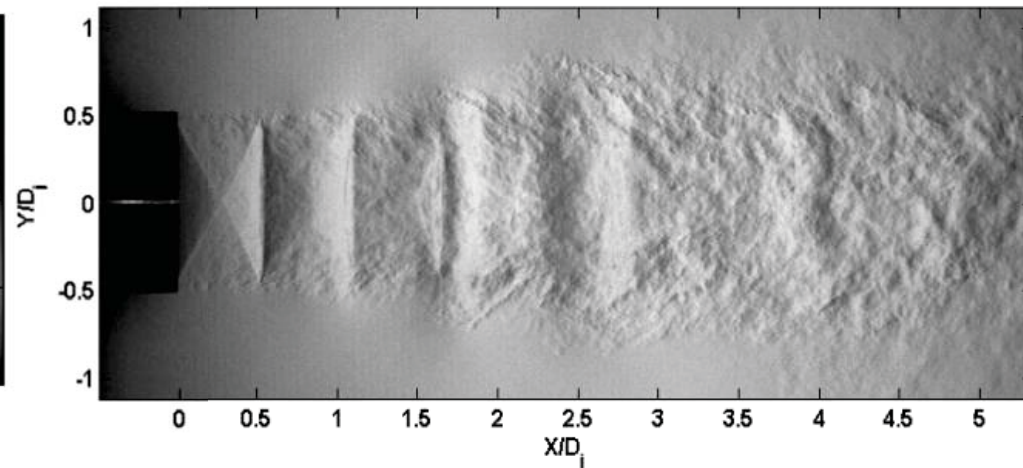


# Continuation of screech study with other flow vis techniques

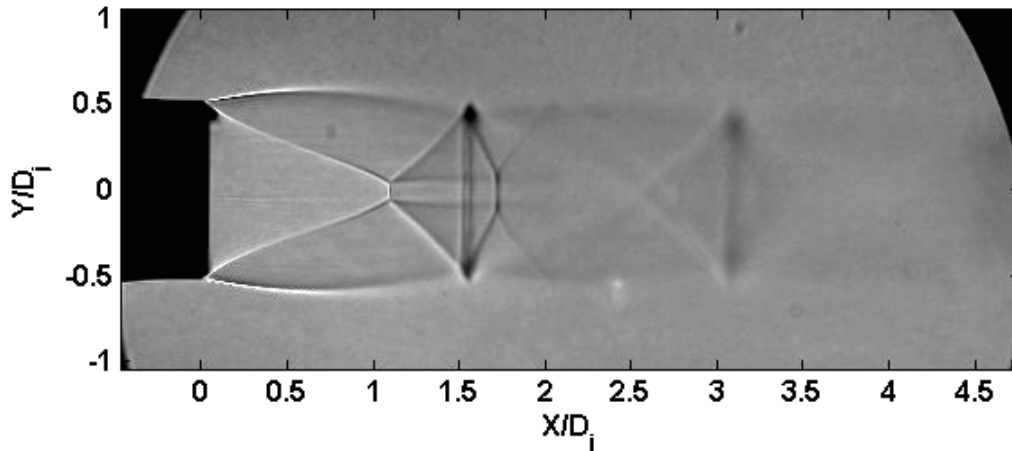
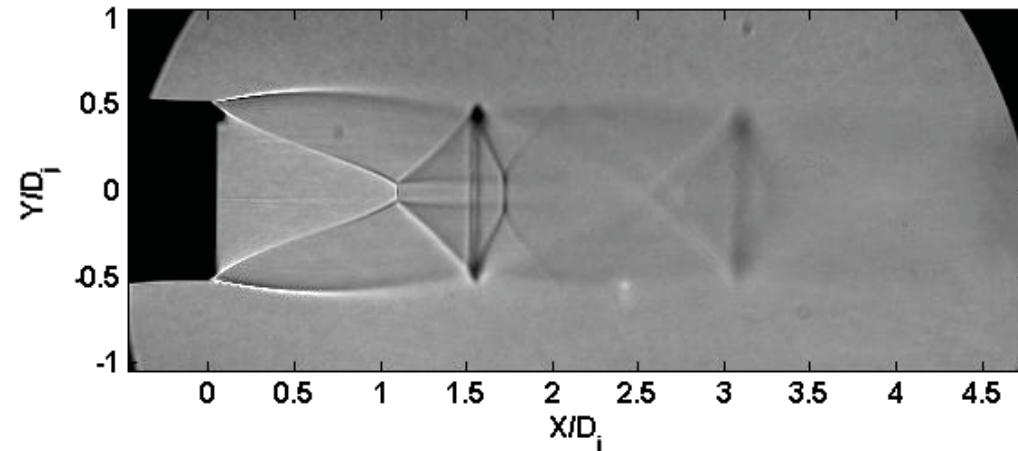
# 2<sup>nd</sup> look: Multiple Flow Vis Techniques



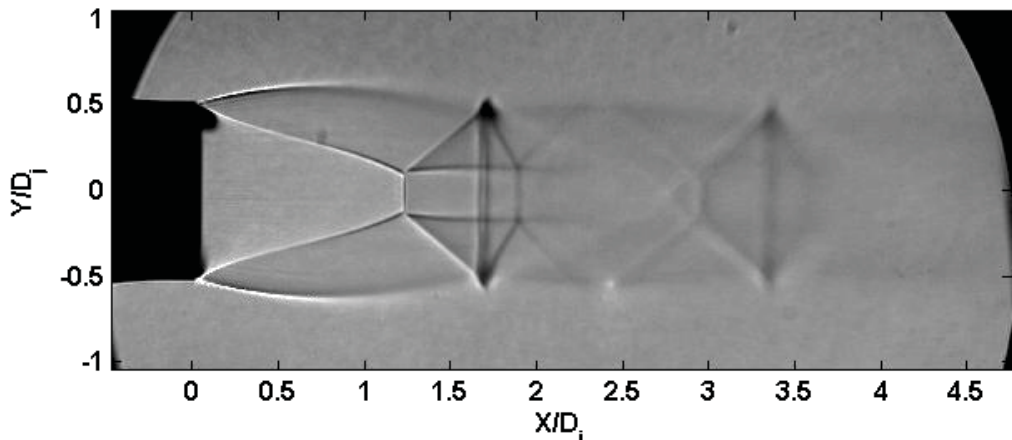
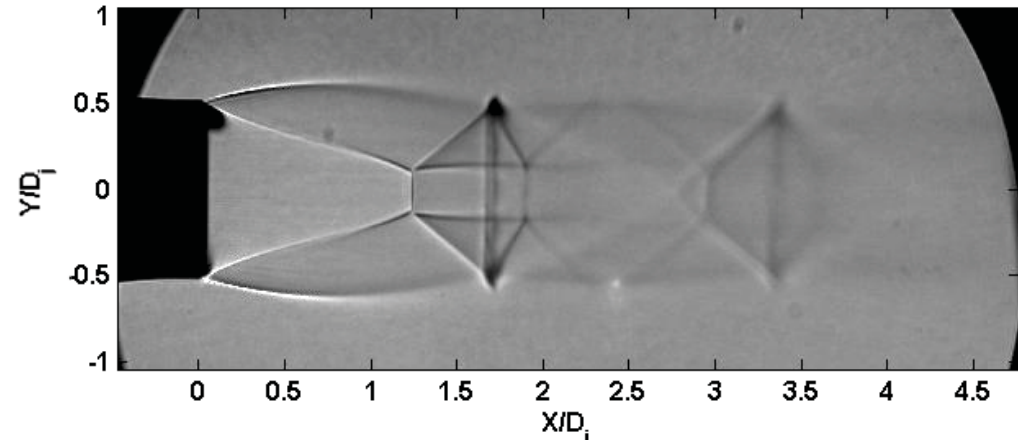
# 2<sup>nd</sup> look: Multiple Flow Vis Techniques

 $M_i = 1.11$  $M_i = 1.1$  $M_i = 1.1$  $M_i = 1.1$ 

# Results: Screech Frequency versus $M_j$

 $M_j = 1.536$ 

 $M_j = 1.536$ 


$M_j = 1.536$  - overlapping stage jump region D and E

 $M_j = 1.640$ 

 $M_j = 1.640$ 


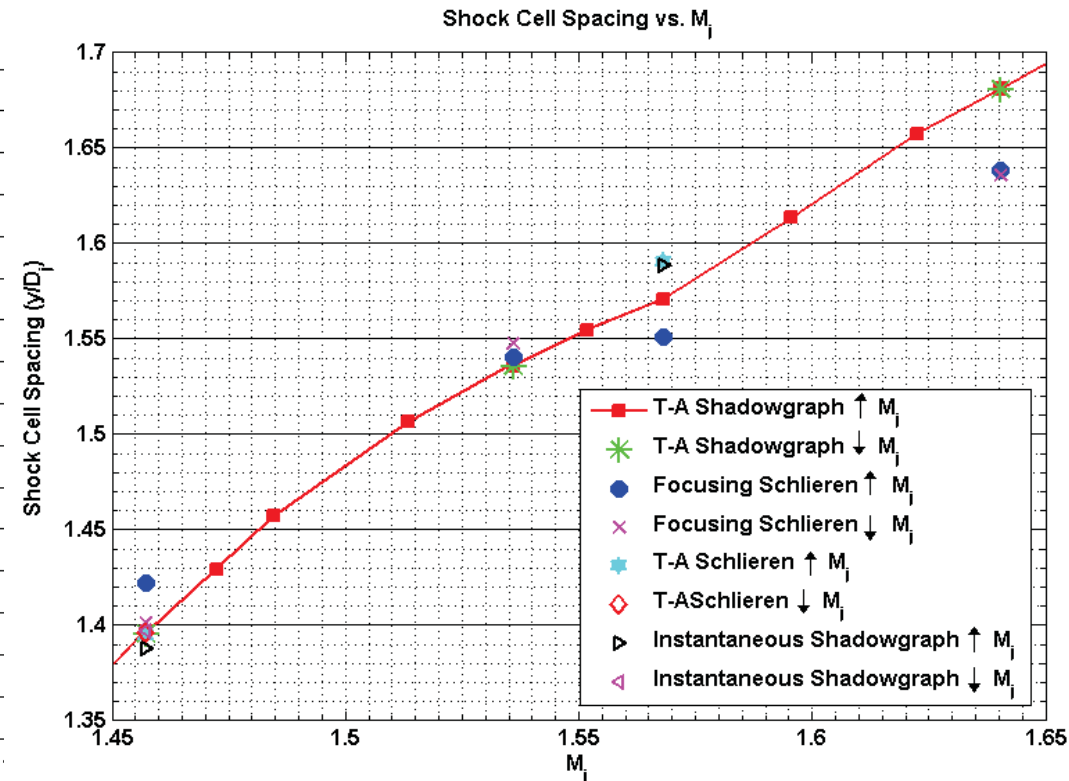
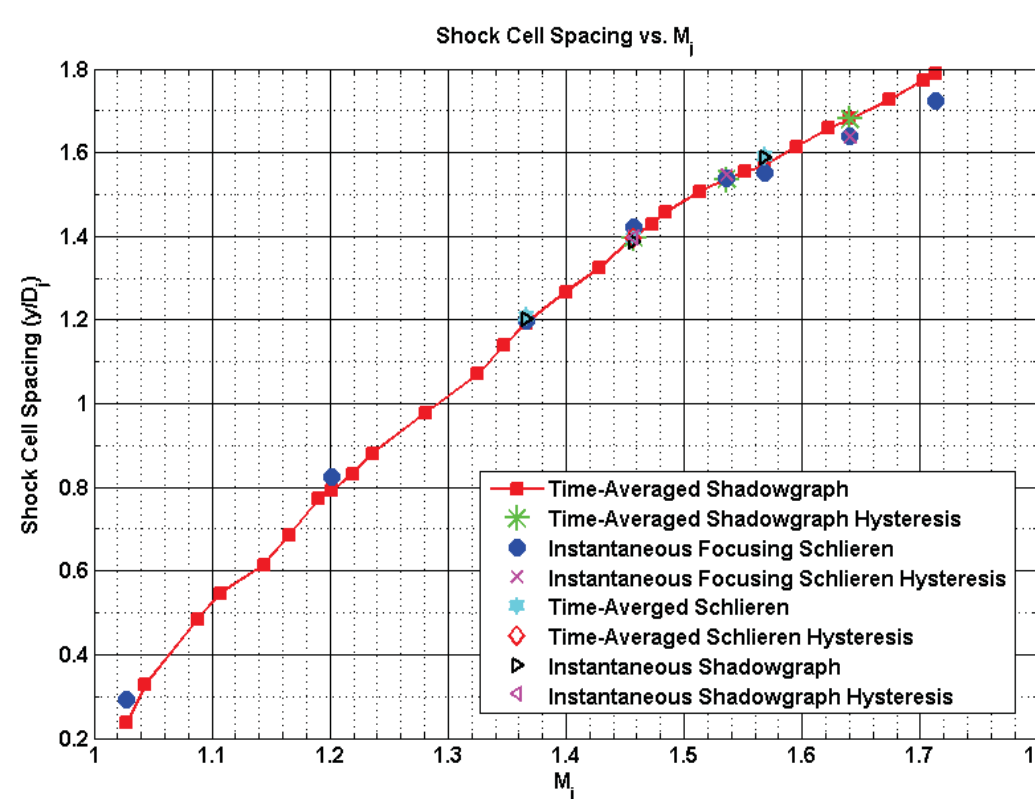
$M_j = 1.640$  - overlapping stage jump region E and F

**Hysteresis:** stage jump occurs at a different location depending on whether  $M_j$  is increased or decreased





# Results: Flow Vis Shock Spacing Measurements



- Repeatable results - Shock spacing follows the monotonic trend
- Reiterates results that inferred shock spacing is NOT the parameter that adjusts to accommodate a new frequency when a stage jump occurs

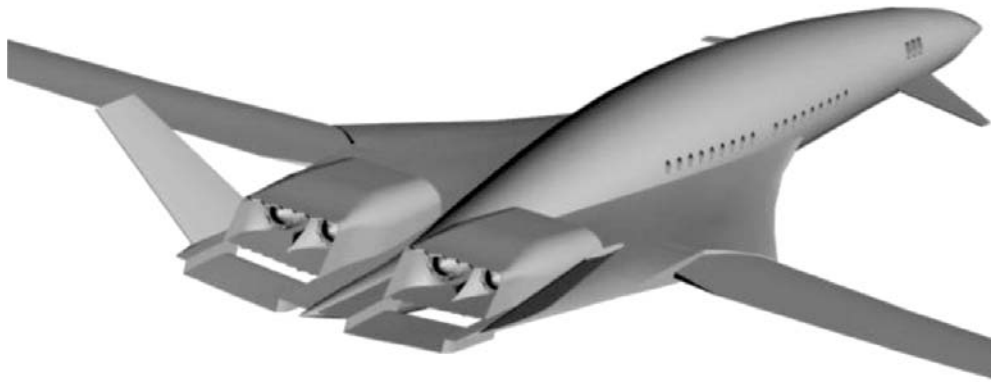


# **BOS used in the Jet-Surface Interaction Tests (JSIT)**

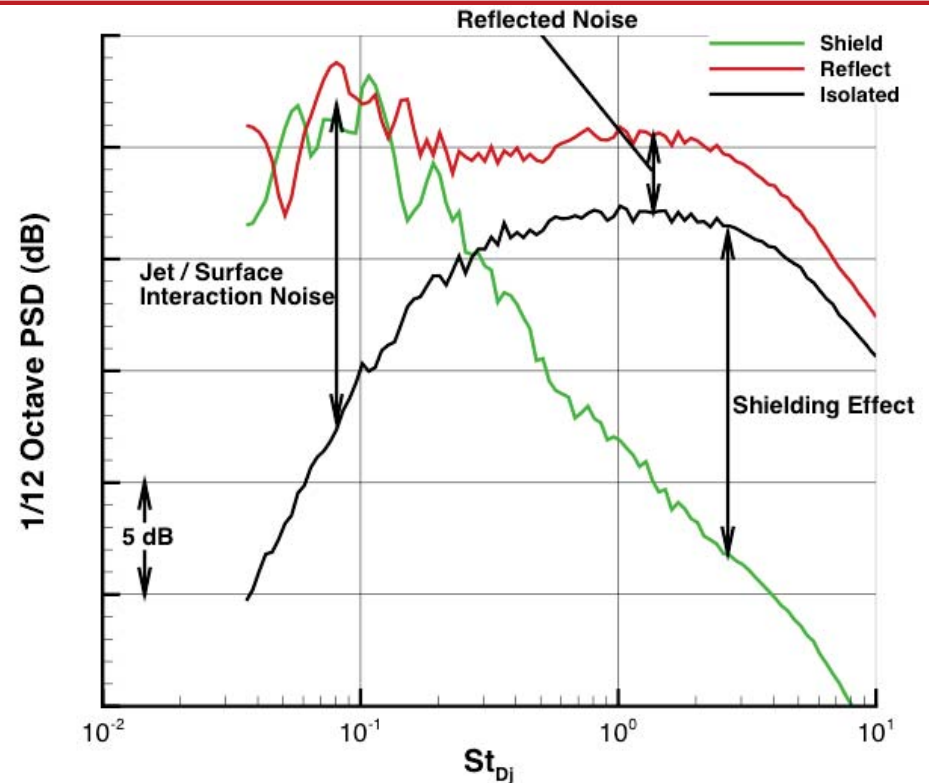
# Jet-Surface Interaction Noise

- Many current and future generation aircraft designs incorporate airframe surfaces near the engine exhaust

**Jet-surface interaction noise** - Noise created by the high-speed engine exhaust striking/passing near a solid surface



**NASA Supersonic Iconic Vehicle**



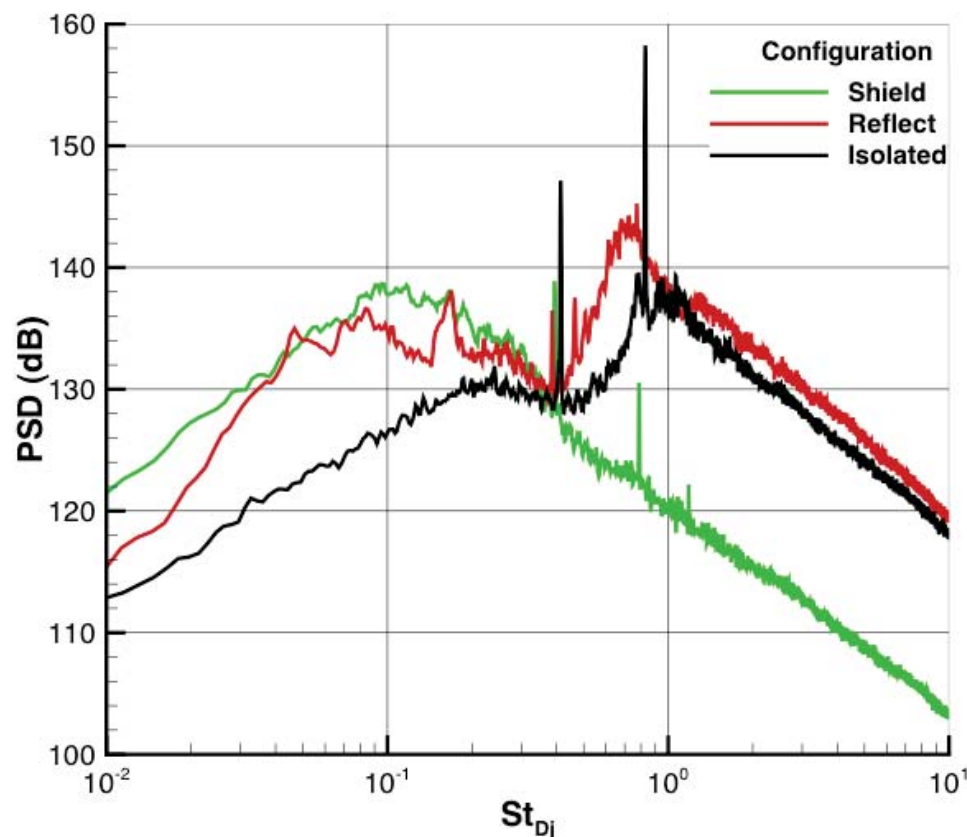
- The current generation of noise prediction tools / methods are not well equipped for the tight engine & airframe designs



# Motivation - BBSN

Jet-Surface Interaction Tests were conducted to supply experimental data to support the development/validation of new noise prediction codes and methods that include the affect of nearby surfaces

Phase 1: Far-field acoustic data showed that the BBSN was greatly reduced by the surface when the jet was over-expanded



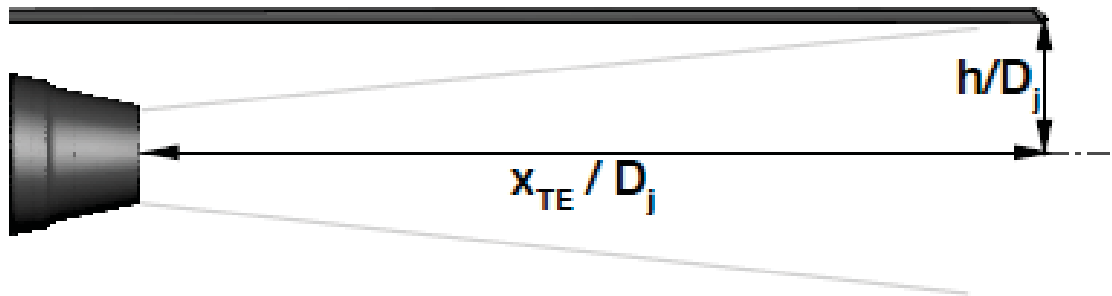
11976  
13689  
12843

- The amplitude and frequency characteristics of BBSN are a function of the strength, number, and location of the shock cells
- It is still unclear how (or if) a surface affects the shock cells, and, thereby, reduces the BBSN
- Is it a surface shielding effect or is the surface interacting with the shock cell structures?

# BOS Experimental Setup

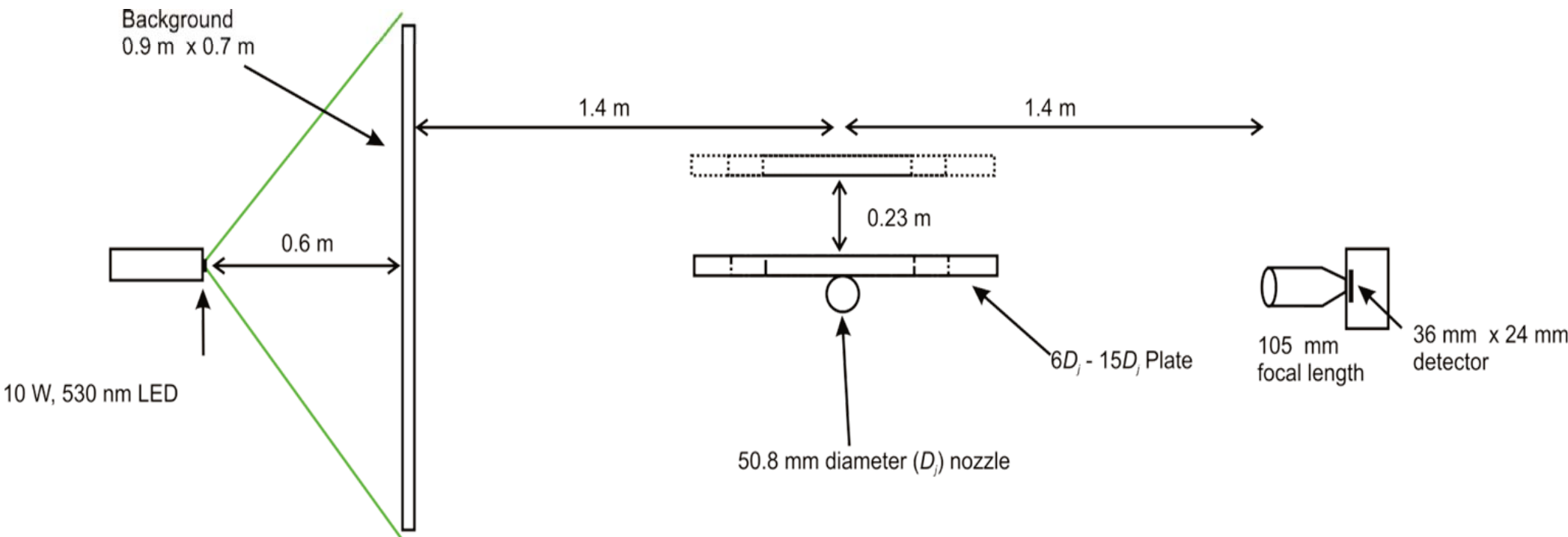
- The jet-surface interaction configuration was formed using a flat planar surface (plate) and a round convergent-divergent nozzle ( $M_d=1.5$ )

"Shielded" Observer



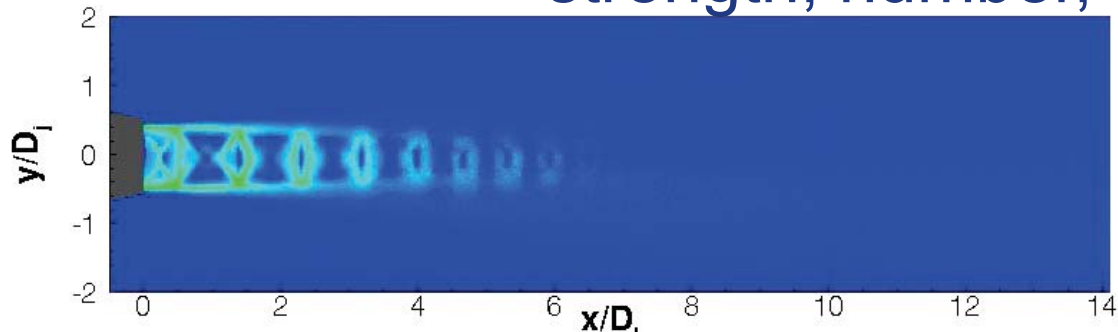
3 plate lengths were tested:  
 $x_{TE} = 6D_j$ ,  $10D_j$ , and  $15D_j$

"Reflected" Observer

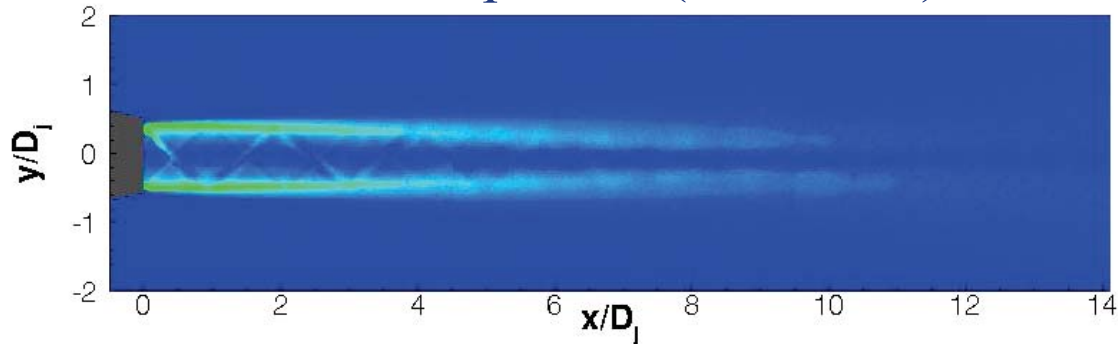


# Isolated Supersonic Jet

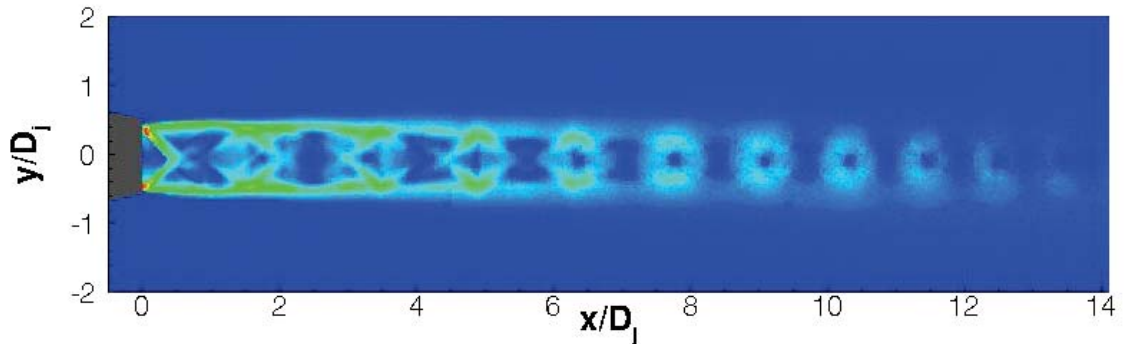
BBSN spectral characteristics are a function of shock cell strength, number, and spacing



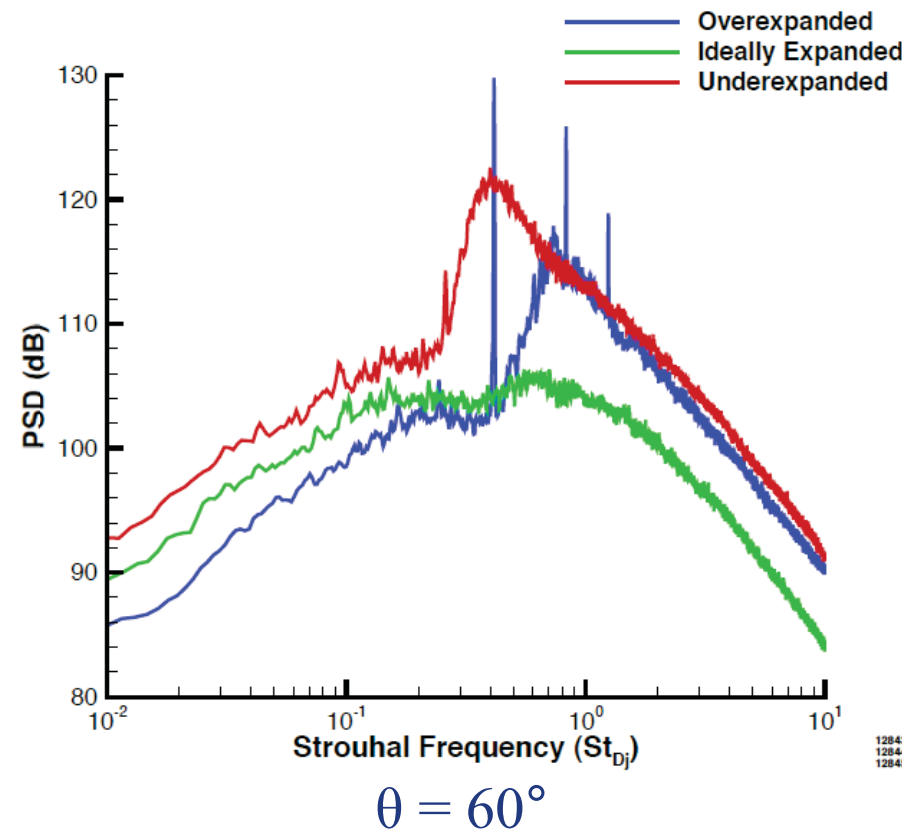
Over – expanded (Mid=1.29)



Ideally expanded (Mid=1.48)

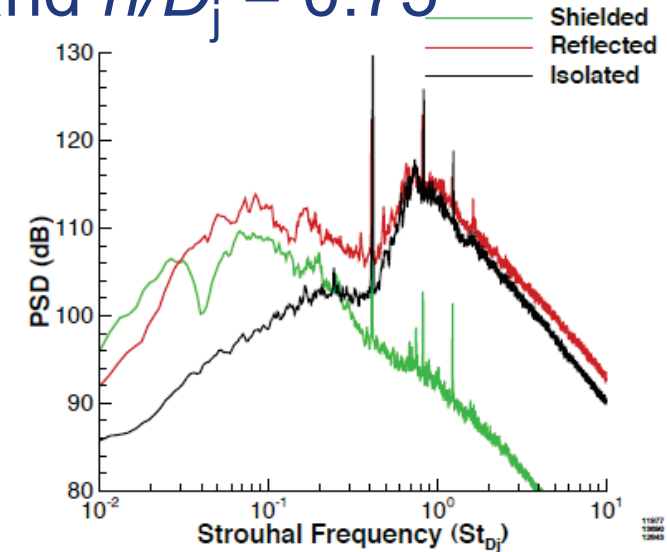
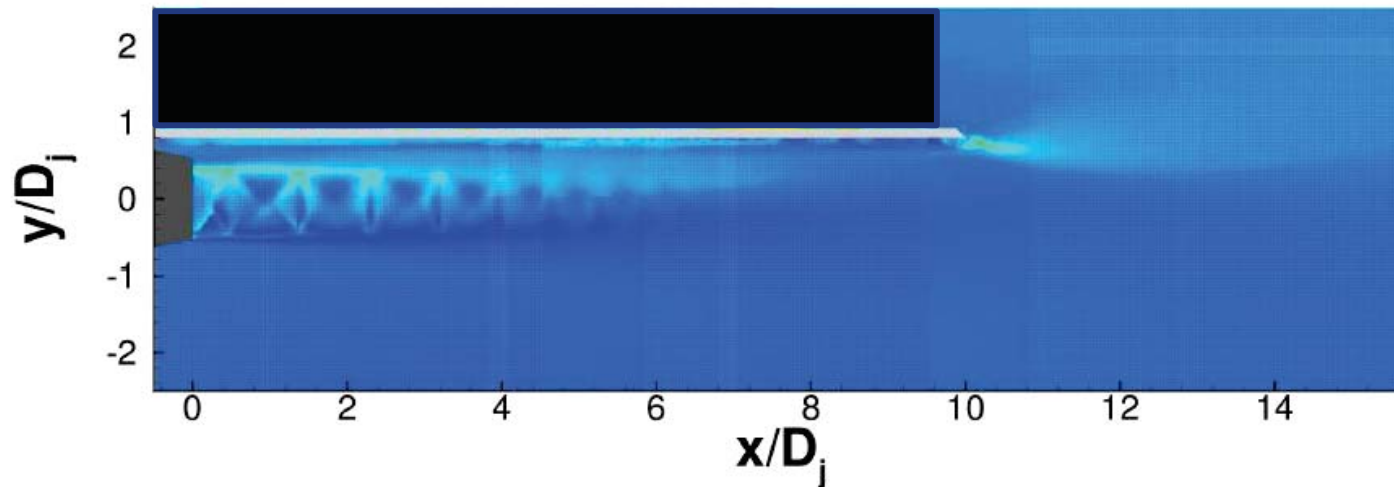


Under – expanded (Mid=1.61)

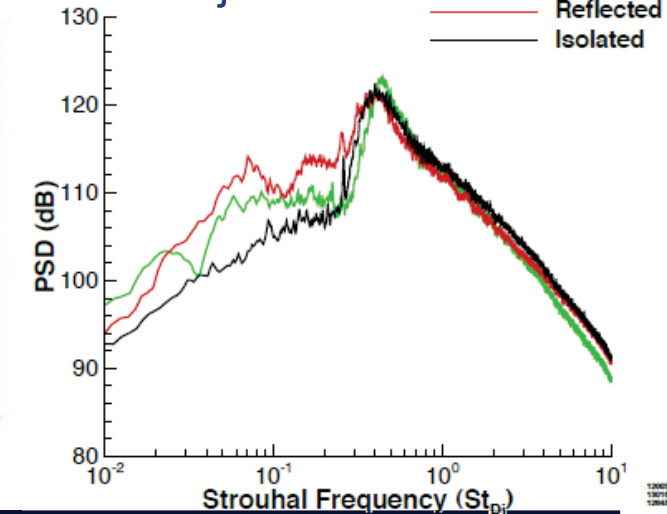
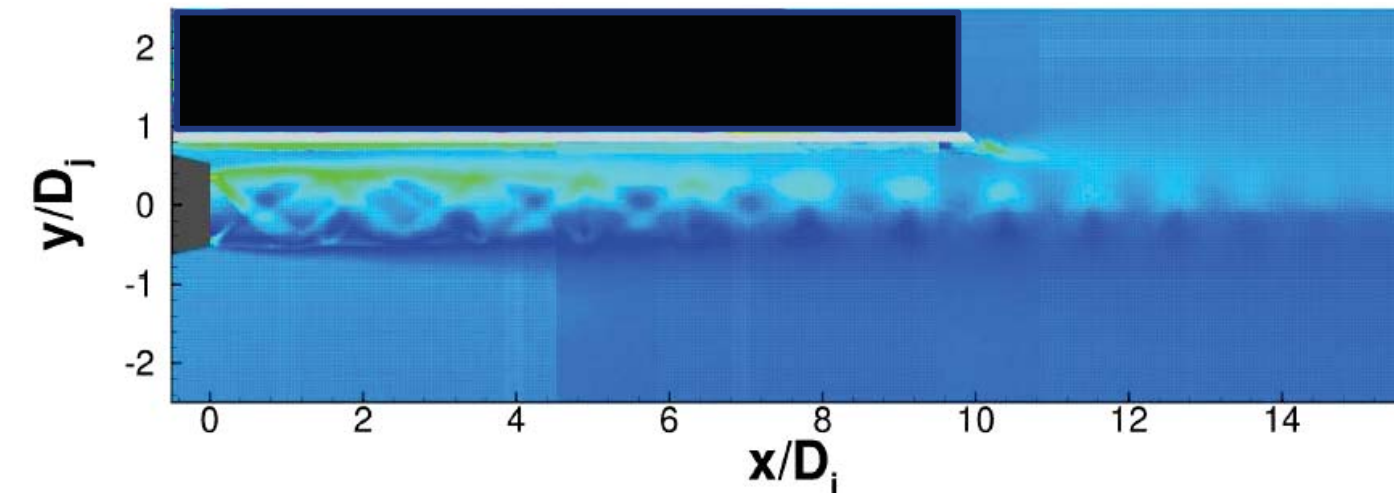


# Results: Jet Near a Surface

Over-expanded Jet Surface at  $x_{TE}/D_j = 10$  and  $h/D_j = 0.75$

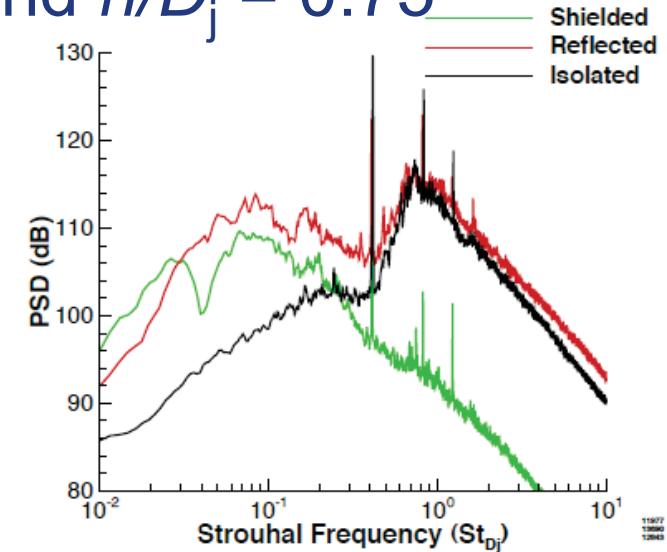
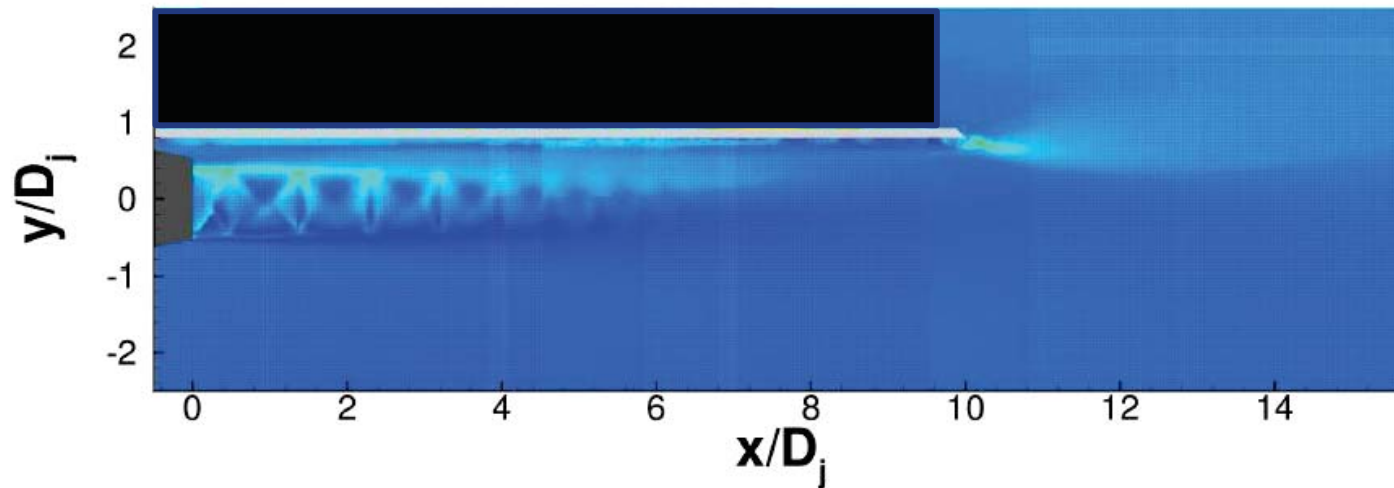


Under-expanded Jet Surface at  $x_{TE}/D_j = 10$  and  $h/D_j = 0.75$

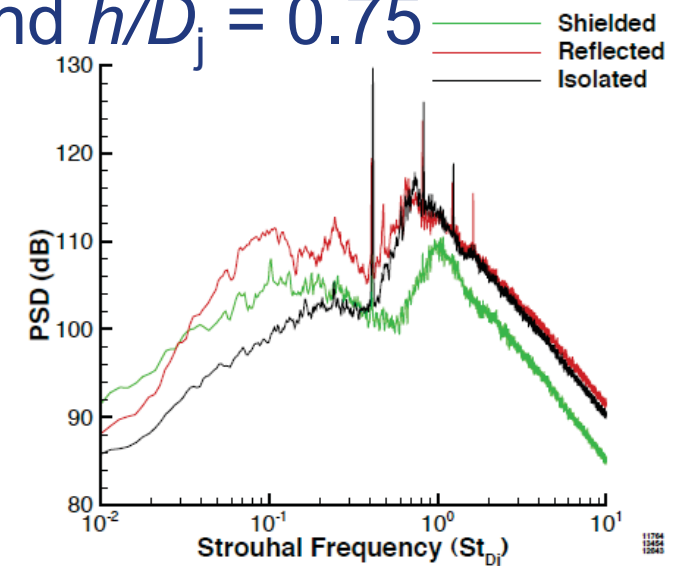
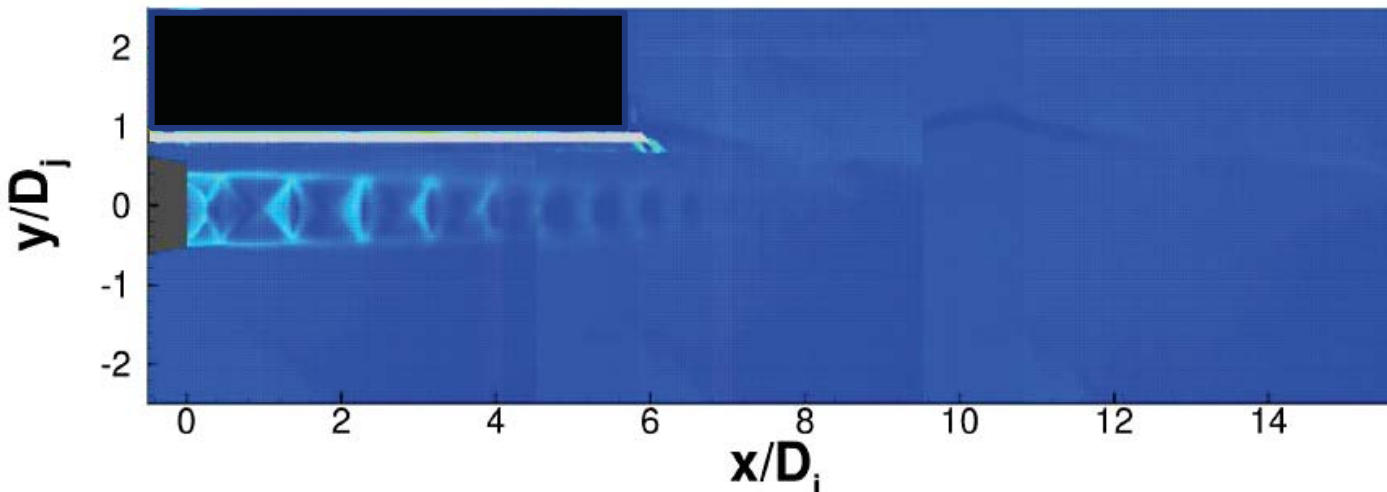


# Results: Effect of Surface Length

Over-expanded Jet Surface at  $x_{TE}/D_j = 10$  and  $h/D_j = 0.75$



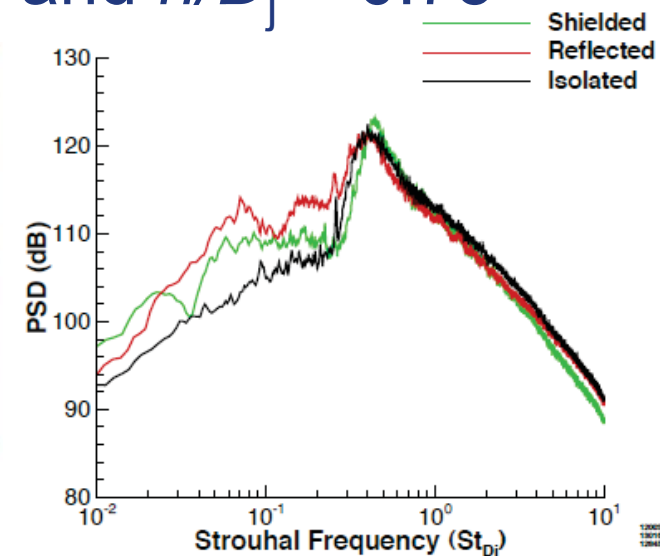
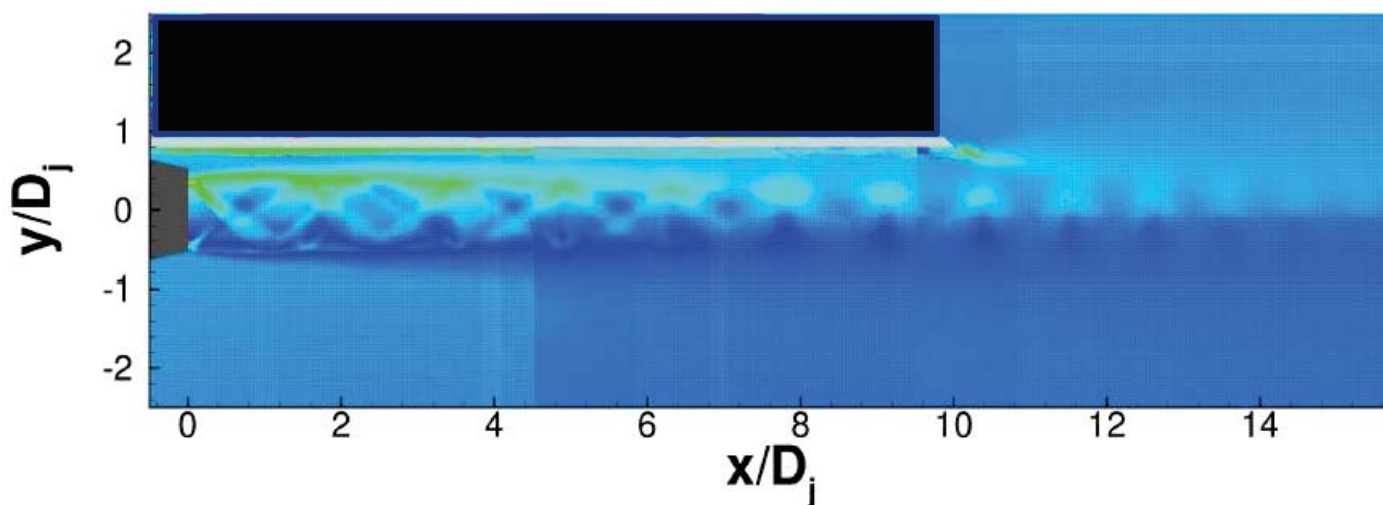
Over-expanded Jet Surface at  $x_{TE}/D_j = 6$  and  $h/D_j = 0.75$



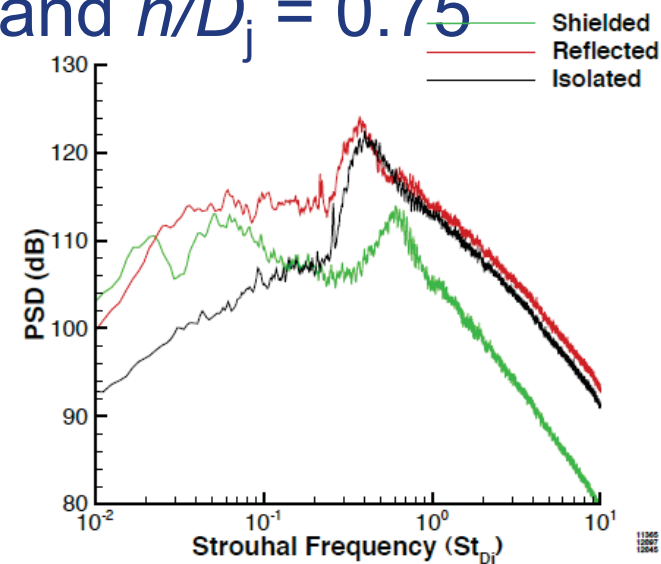
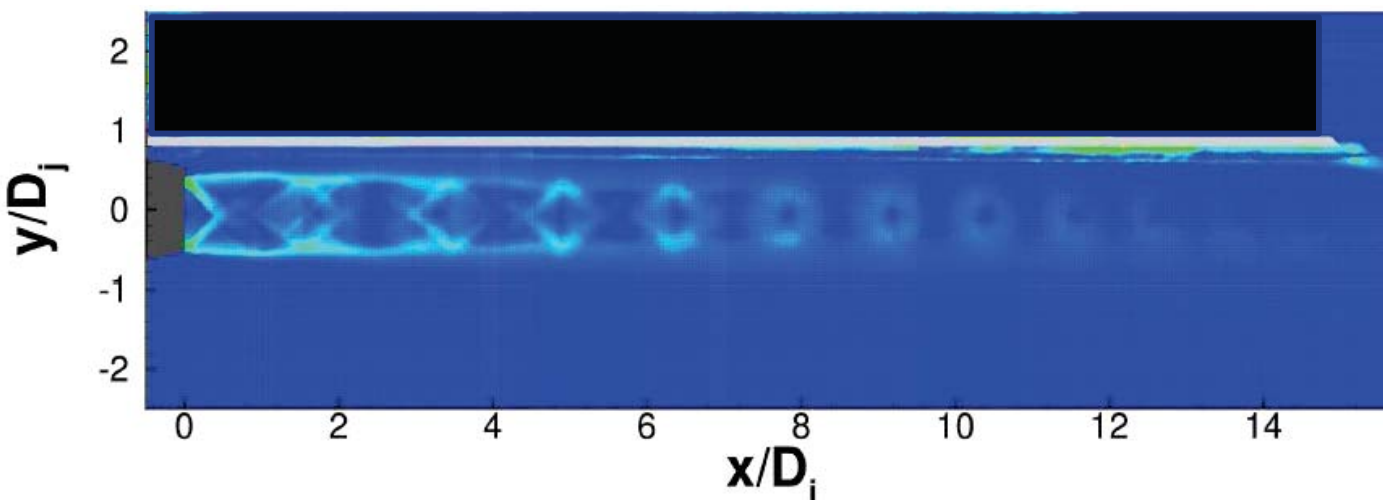


# Results: Effect of Surface Length

Under-expanded Jet Surface at  $x_{TE}/D_j = 10$  and  $h/D_j = 0.75$



Under-expanded Jet Surface at  $x_{TE}/D_j = 15$  and  $h/D_j = 0.75$

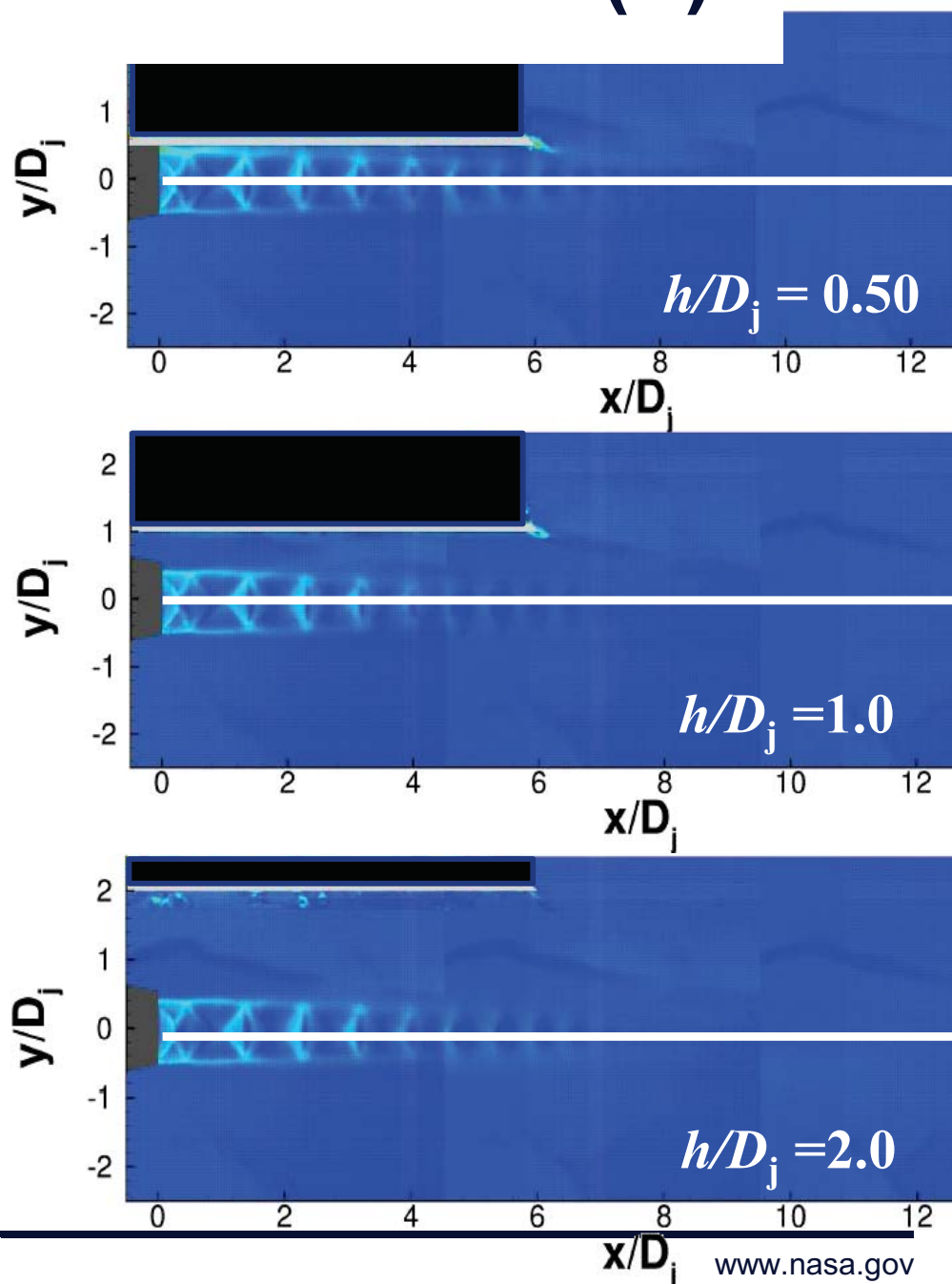




# Results: Effect of Surface Distance (h)

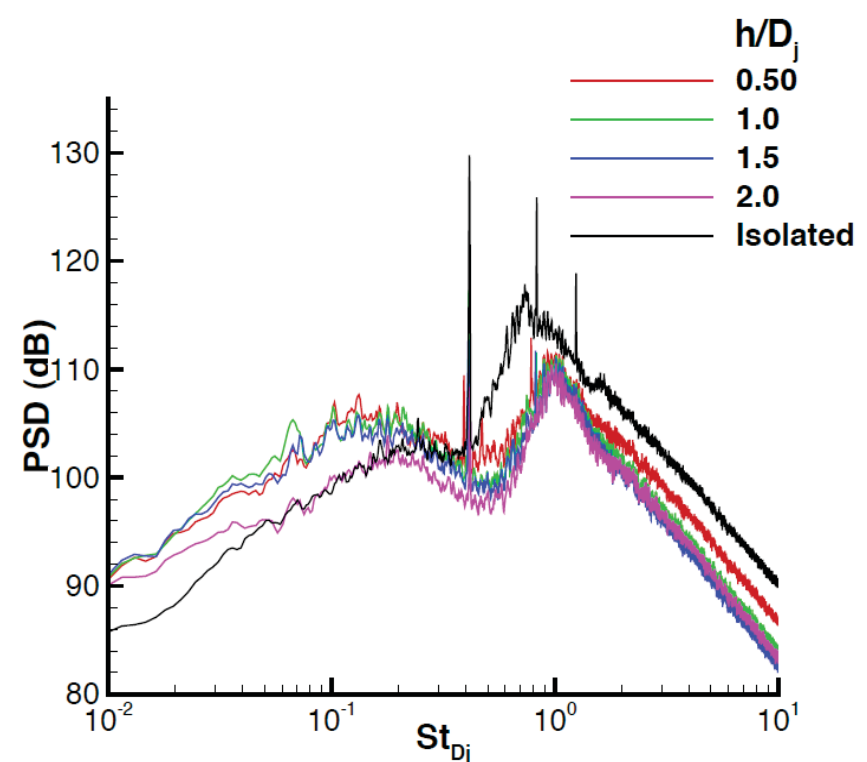
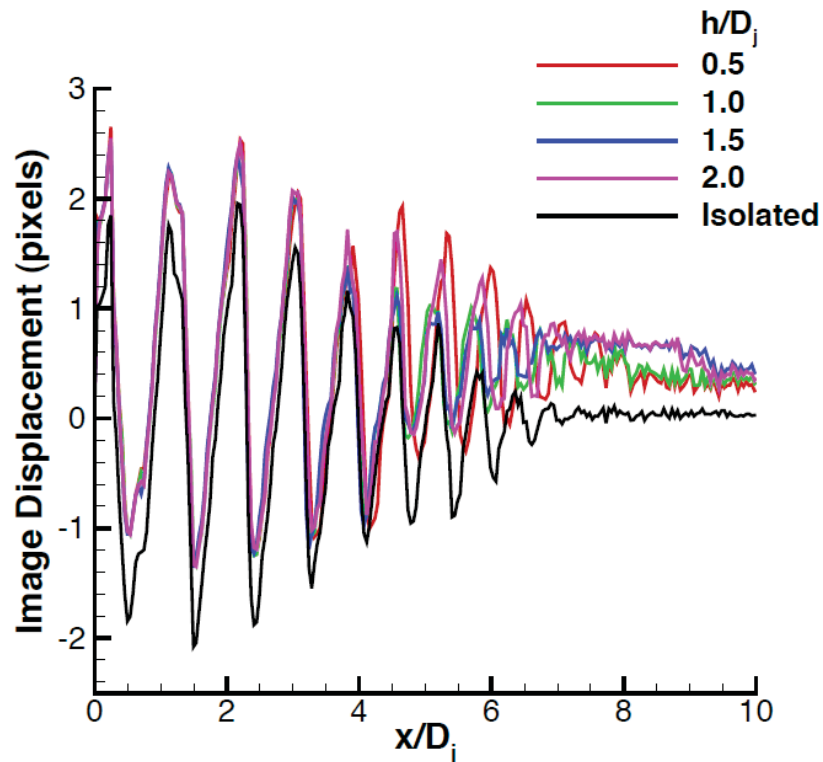
- Over-expanded jet with surface at  $x_{TE}/D_j=6$ ,  $h/D_j=0.5, 1.0, 2.0$
- Shock cells appear to behave independent of surface distance
- Shock cells near trailing edge are sufficiently weak and hard to detect amongst the background
- It is difficult to make firm conclusions based on inspection

Extract axial image displacements along the nozzle centerline to display shock cell spacing and amplitude information



# Results: Effect of Surface Distance

Over-expanded jet for surface at  $x_{TE}/D_j = 6$  and  $h/D_j = 0.5, 1.0, 1.5,$  and  $2.0$



- Surface has minimal impact upstream of the trailing edge distance  $x/D_j \leq 4$
- Around trailing edge shock cells appear to change amplitude and spacing but have small effect on the BBSN
- **BBSN reduction is due to noise shielding rather than changes in shock cells**



# Conclusions: - JSIT

- BOS data were analyzed and compared to corresponding far-field acoustic data to study how the shock cell structure and BBSN are affected by a nearby surface.
- The following observations were made:
  1. Changes to the shock cell structure have a smaller impact on the BBSN compared to the surface shielding effect
  2. BBSN may be shielded by surfaces close to the jet if those surfaces are sufficiently longer than the shock cell train
- Data will aid in the design of future aircraft and the development of supersonic engine exhaust noise prediction tools

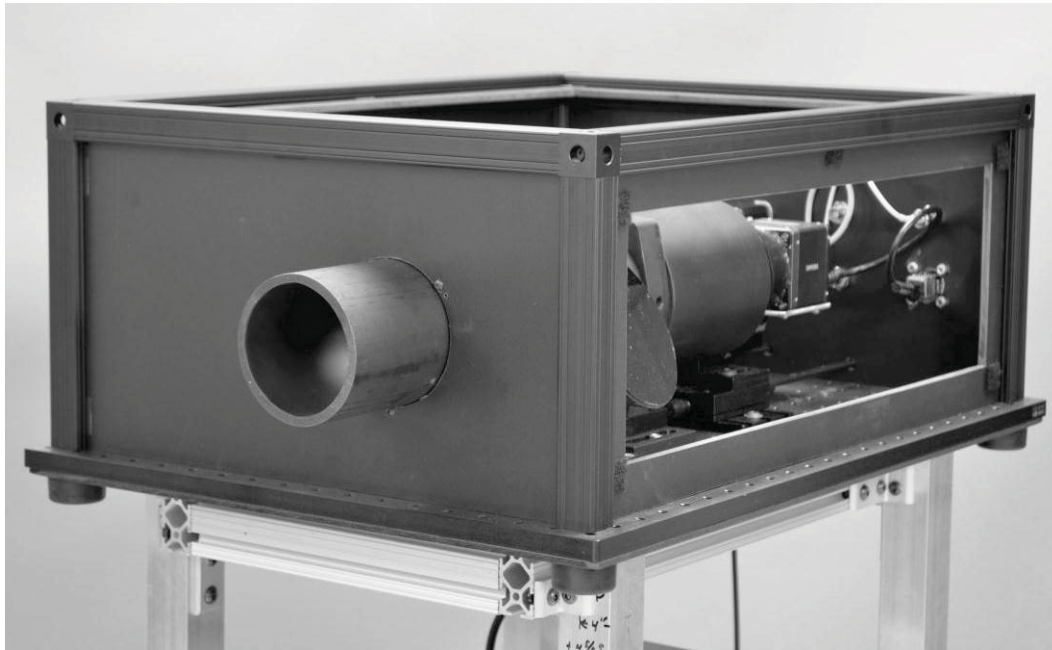


# Miscellaneous topics of interest

- **Focusing Schlieren**
- **JSIT Parametric Study**
- **Phase Knife**
- **Comparative study**



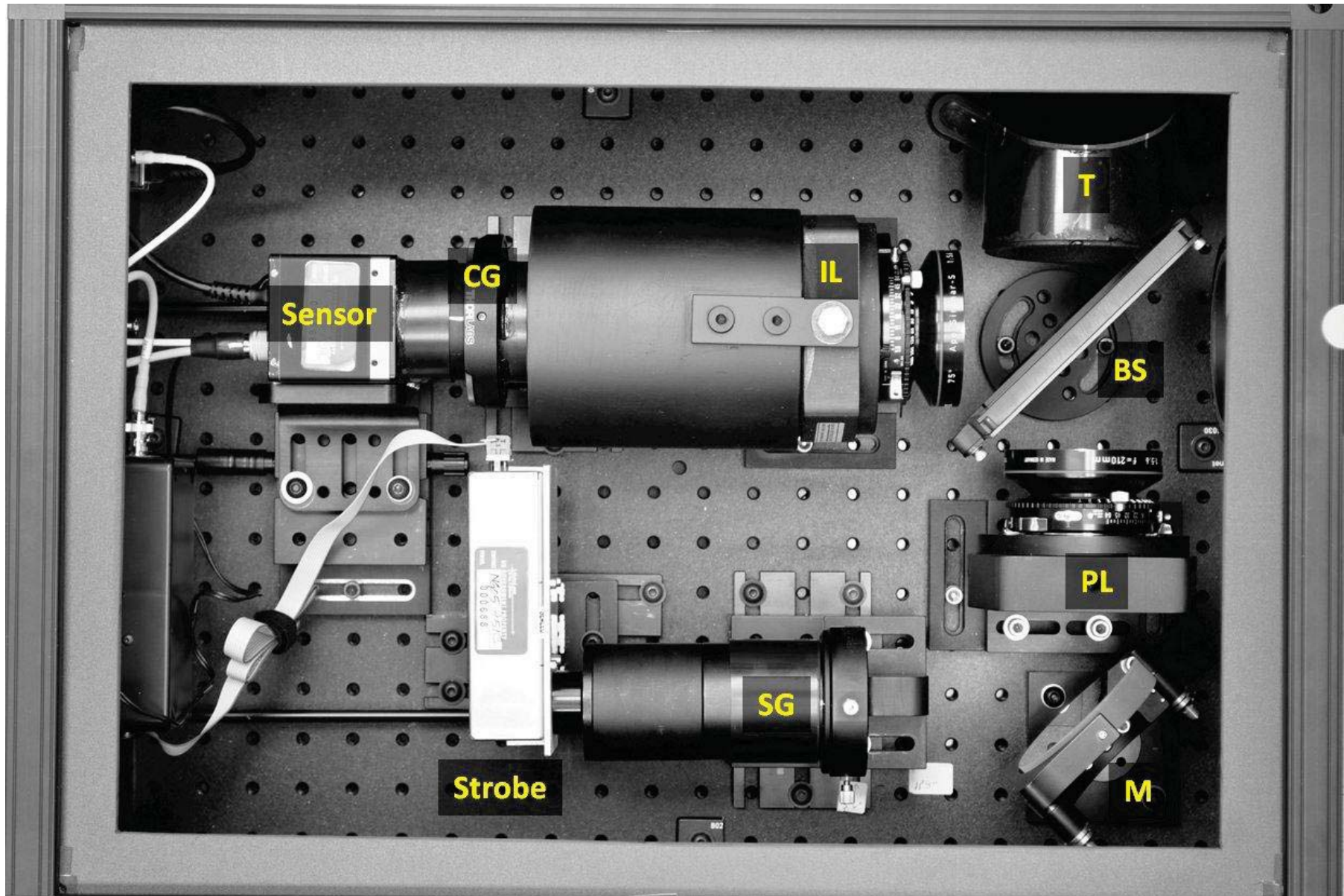
# Brief Overview – Focusing Schlieren



**SBIR – Metrolaser**  
**COTR - Amy Fagan**  
**Goal:** Develop a robust, portable schlieren system, with variable FOV

- Schlierenscope – Focusing schlieren system
  - Dual grid projection system
  - All critical controls are contained within the instrument housing
  - Utilizes a Xenon strobe (1  $\mu$ s) that freezes motion and captures images with a scientific CCD camera
  - Alignment between the screen and the camera is not critical, which simplifies the setup

# Brief Overview – Focusing Schlieren





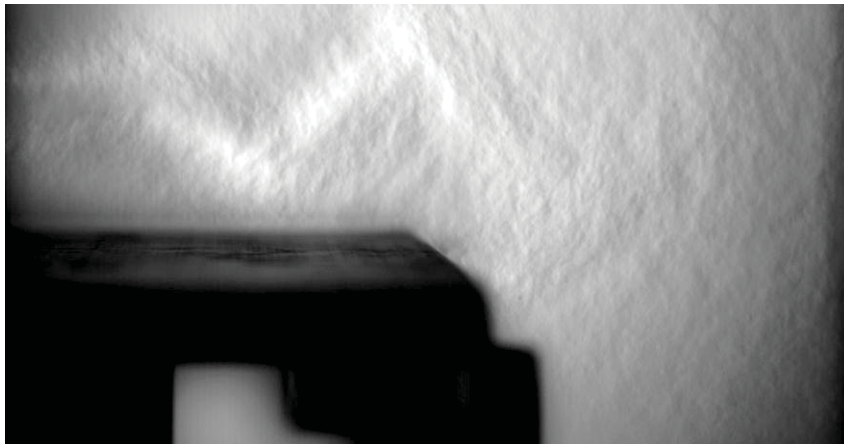
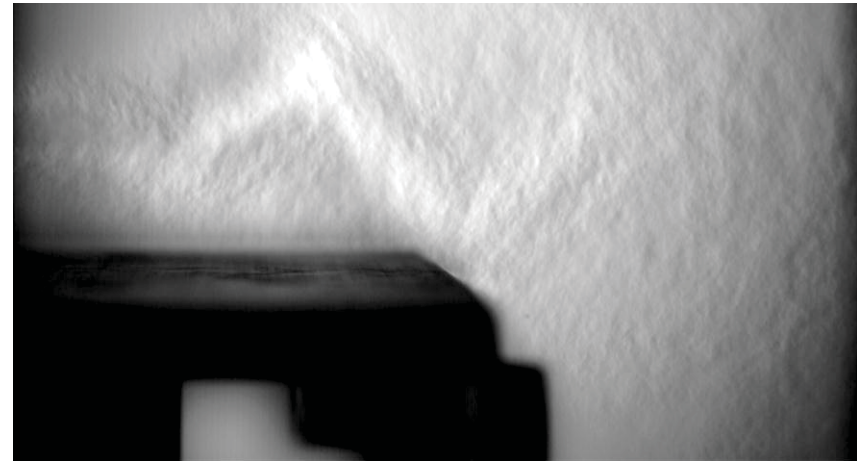
# Continuation – JSIT Parametric Study





# Continuation – JSIT Parametric Study

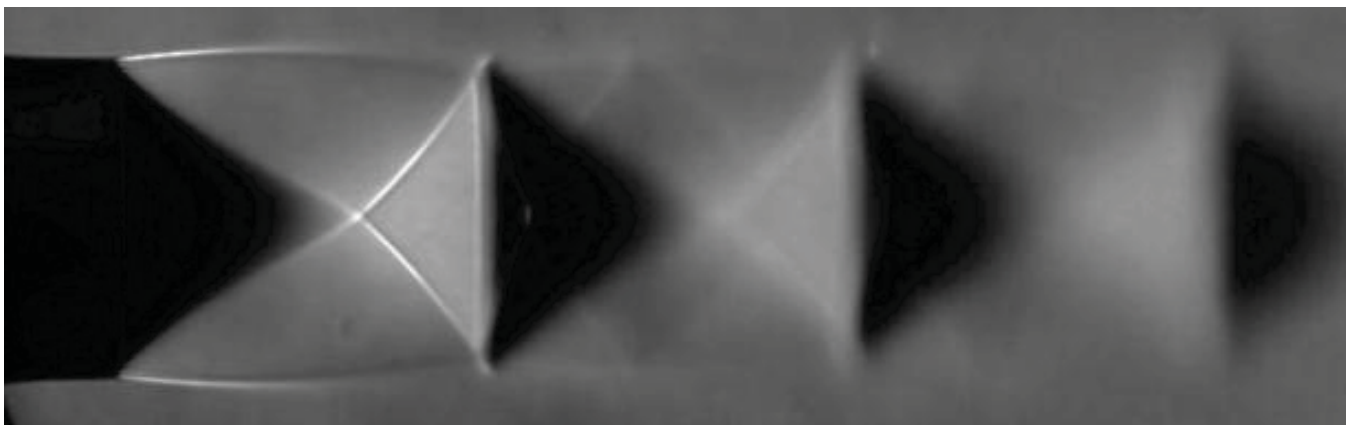
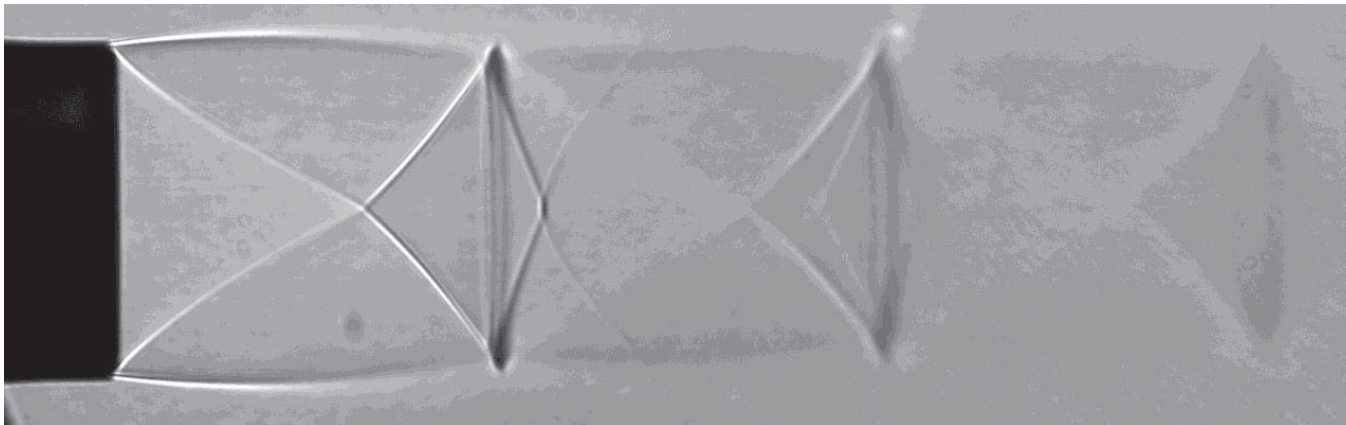
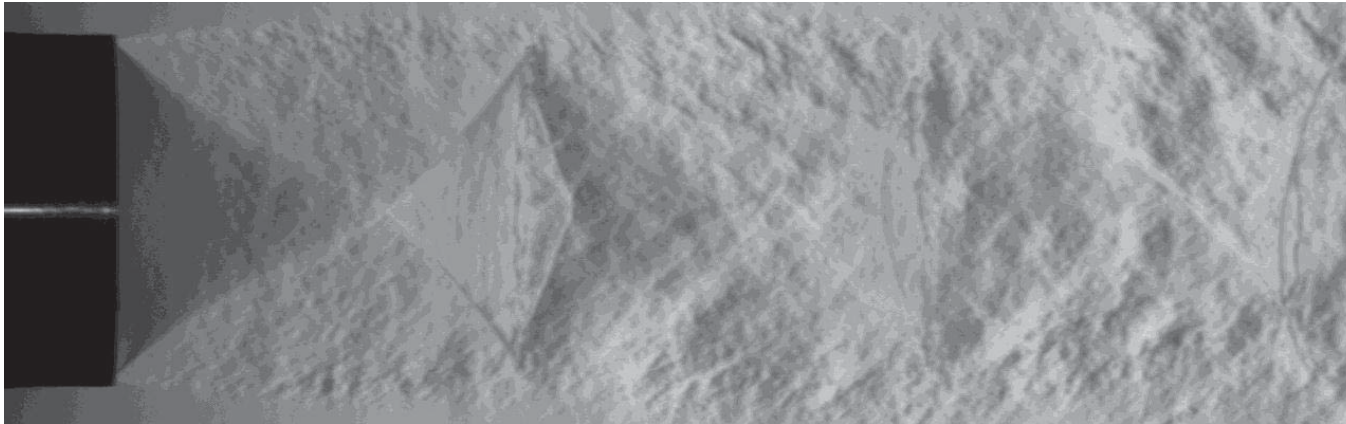
Plate length: 8 in., T.E. distance: 8.5 in., stand off distance: 1.35 in.,  
 $M_j = 0.96$



Use tone frequency to trigger/capture schlieren images in 1 period

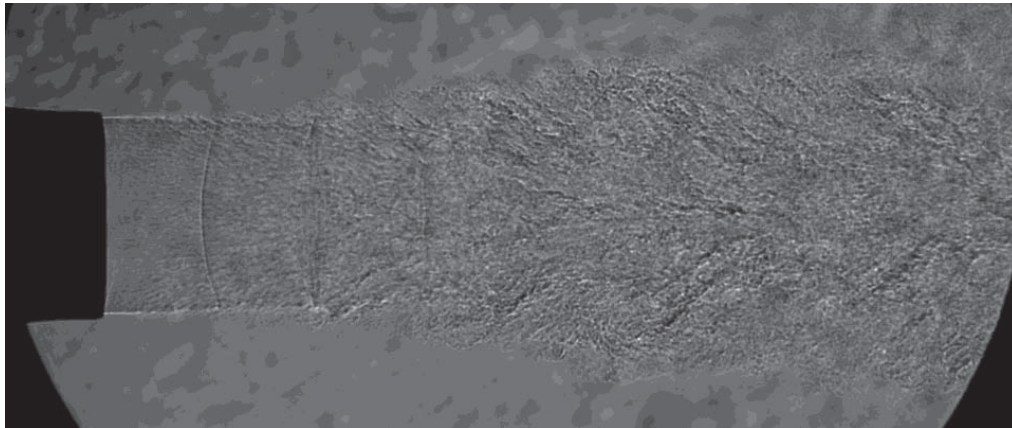
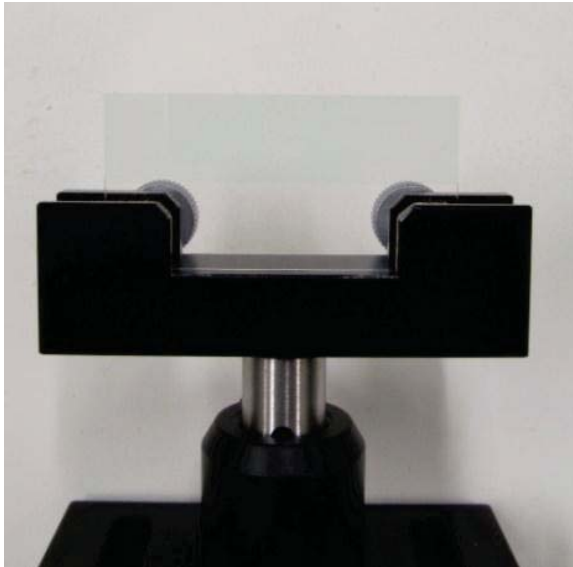


# Continuation: Comprehensive Comparative Study

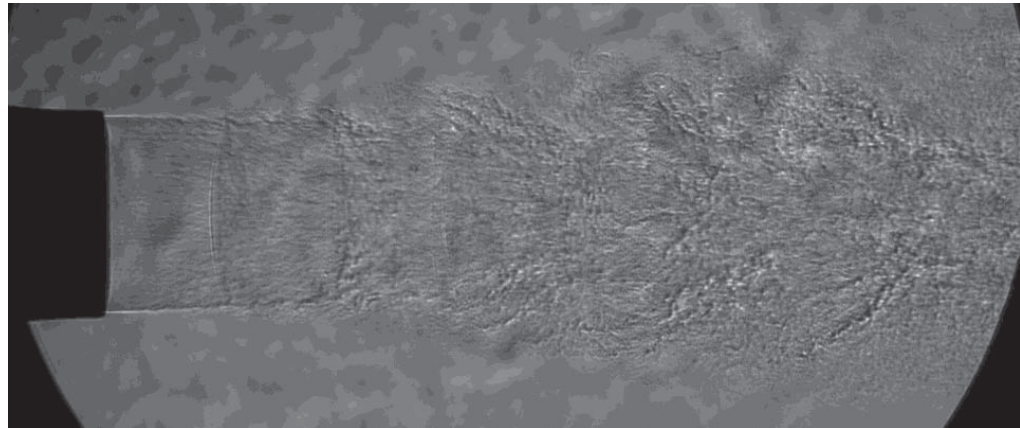


- Better characterize and enhance each technique
- Being used to further investigate the aeroacoustic screech phenomena
- Determine shock spacing

# Further Investigate Phase Knife



Shadowgraph – No phase knife



Schlieren - phase knife in place



# Further Investigate Common Issues





# VIPR 1





Thank you for your time!

Questions?