



Thermochemistry of Rare Earth Silicates for Environmental Barrier Coatings

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Outline of Presentation

- Advantages of Rare earth silicates as Environmental Barrier Coatings (EBCs)
- Essential parameter – $a(\text{SiO}_2)$
- Methods to measure silica activity
 - **Thermodynamics of rare earth silicates: Knudsen Effusion Mass Spectrometry**
- Results of $\text{Y}_2\text{O}_3\text{-SiO}_2$ and $\text{Yb}_2\text{O}_3\text{-SiO}_2$ systems
- Benefits of coating - example



Rare Earth Silicates as Coatings for Silicon-based Ceramics

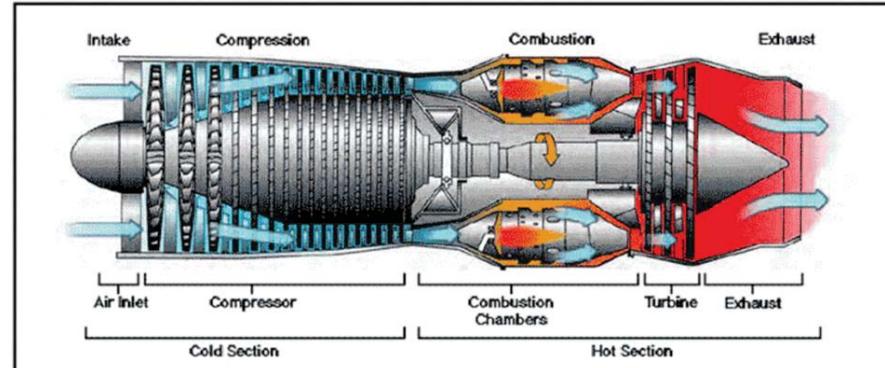
- Stable to high temperatures
- Disilicate: Appropriate thermal expansion match to SiC and SiC composites
- Lower reactivity than pure SiO_2

Applications:

Ceramics in non-moving parts:

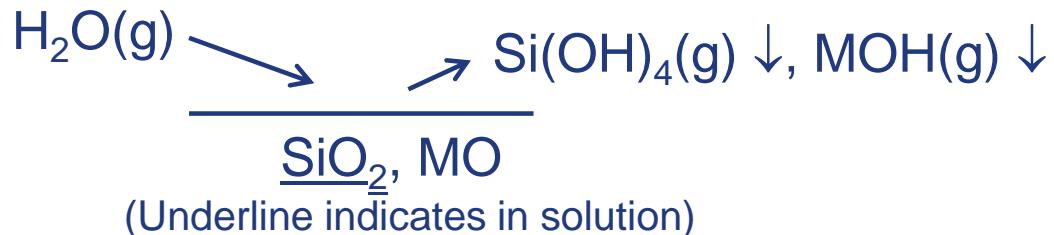
- Combustor liners
- Exhaust nozzles

Eventually moving parts!



Sensors and Electronic Circuits in Extreme Environments: Space and Deep Oil Exploration

Low Reactivity of Rare earth Silicates



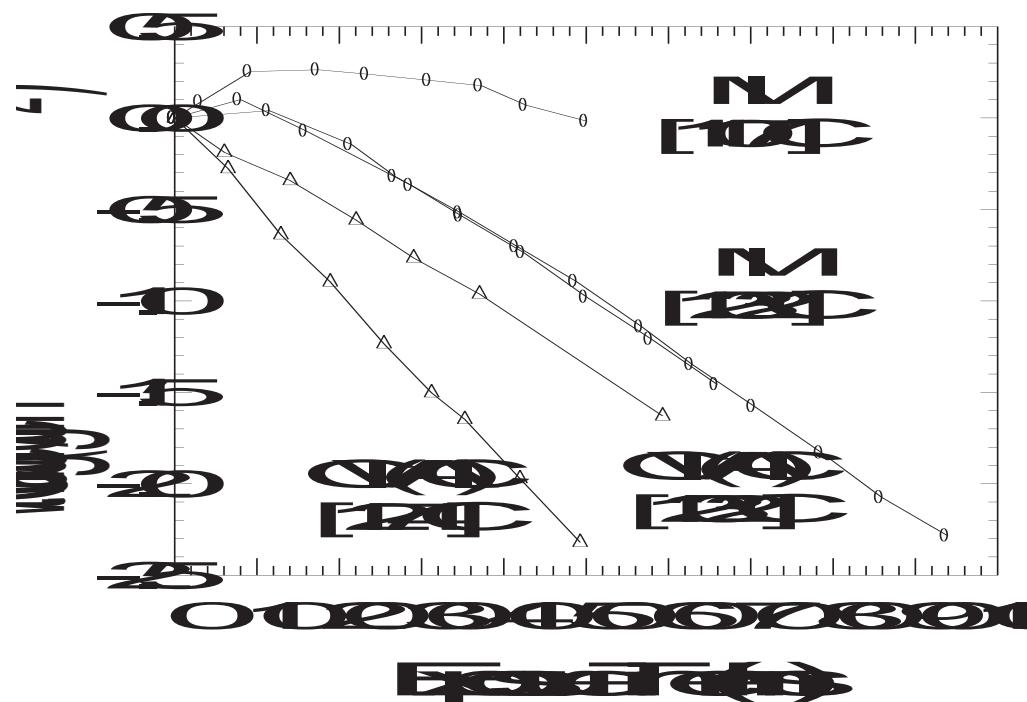
$$P[\text{Si(OH)}_4] = K_a \text{SiO}_2 [P(\text{H}_2\text{O})]^2$$

Y and Yb silicates
Need to be measured!

- Molten Salt Reaction



Lower $a(\text{SiO}_2)$ – less reaction

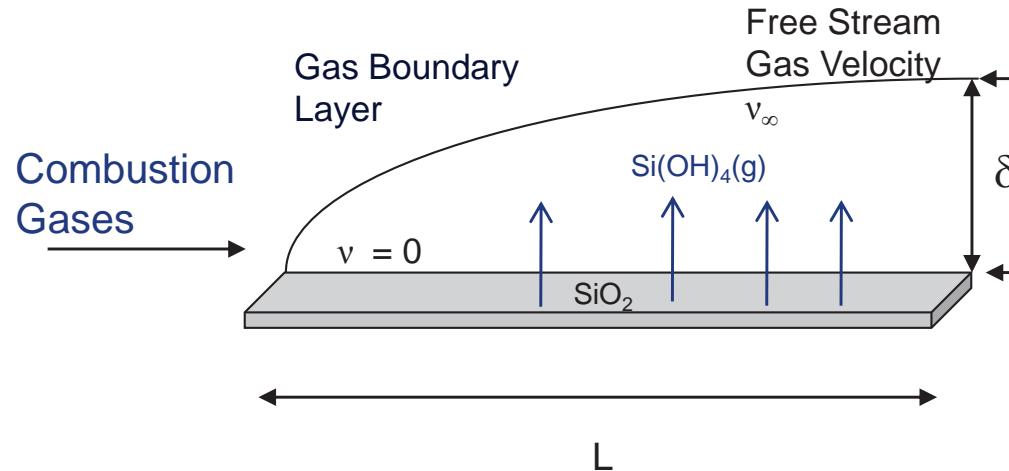


Meschter and Opila., Annu Rev Mater Res 43, 559 (2013)
N. S. Jacobson, J Am Ceram Soc 97, 1959 (2014)



Key Parameters in Boundary Layer Limited Transport Modeling

- $\text{SiO}_2(\text{pure or in silicate soln}) + 2 \text{H}_2\text{O(g)} = \text{Si(OH)}_4(\text{g})$



$$\text{Flux} = 0.664 \left(\frac{\nu_\infty \rho_\infty L}{\eta} \right)^{0.5} \left(\frac{\eta}{D_{\text{Si(OH)}_4} \rho_\infty} \right)^{0.33} \frac{D_{\text{Si(OH)}_4} P_{\text{Si(OH)}_4}}{R T L} =$$

$$0.664 \left(\frac{\nu_\infty \rho_\infty L}{\eta} \right)^{0.5} \left(\frac{\eta}{D_{\text{Si(OH)}_4} \rho_\infty} \right)^{0.33} \frac{D_{\text{Si(OH)}_4}}{R T L} K a_{\text{SiO}_2} (P_{\text{H}_2\text{O}})^2$$

ν_∞ = free stream velocity ρ_∞ = free stream gas density L = characteristic dimension

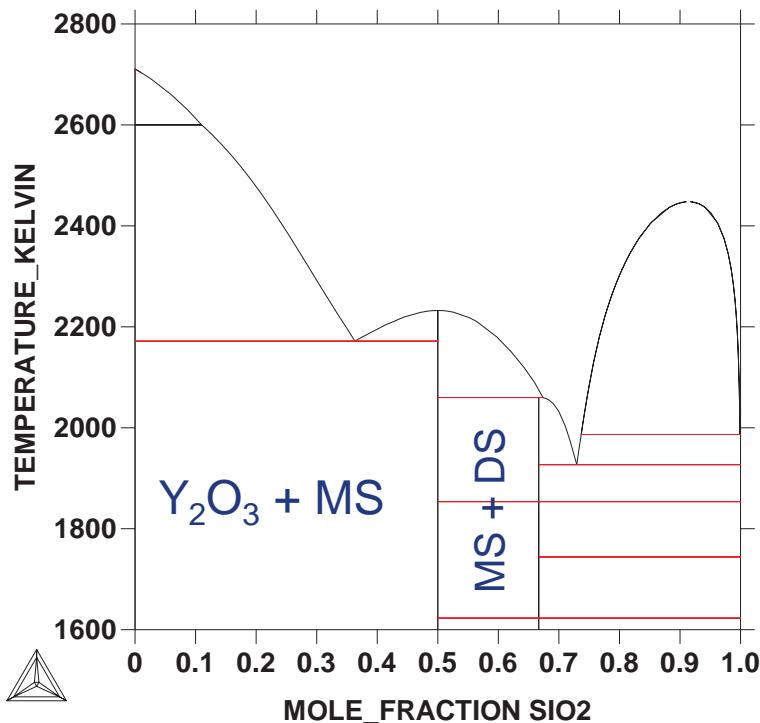
η = viscosity $D_{\text{Si(OH)}_4}$ = gas phase diffusivity of Si(OH)_4

- Reduce $a(\text{SiO}_2)$ \Rightarrow reduce recession. Recession drives need for coatings

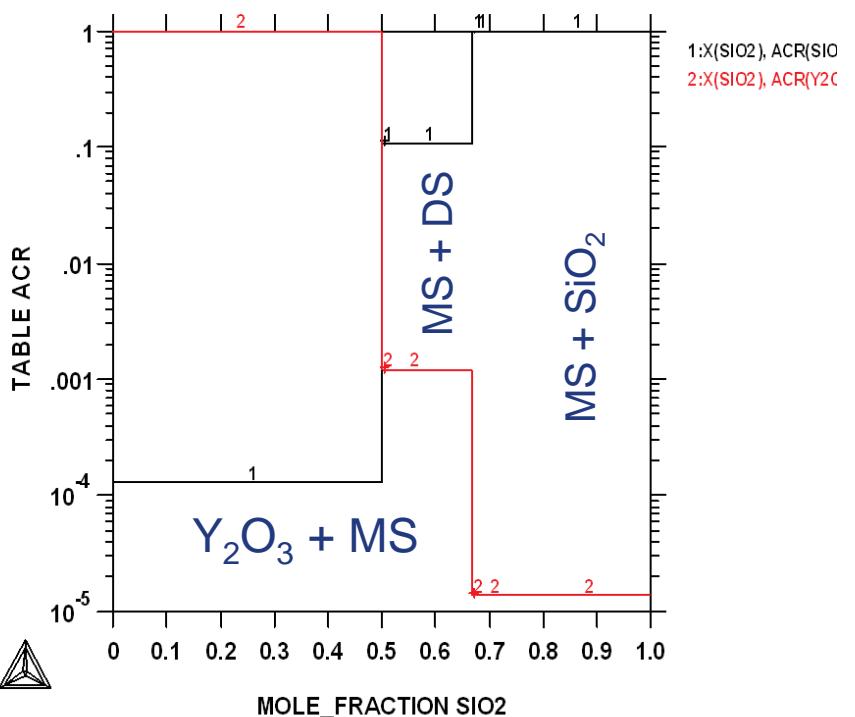


Calculated $\text{Y}_2\text{O}_3\text{-SiO}_2$ Phase Diagram: Fabrichnaya-Seifert Database

THERMO-CALC (2010.08.10:09.24) :
DATABASE:USER
 $\text{AC(O)}=1, \text{N}=1, \text{P}=1.01325\text{E}5;$



THERMO-CALC (2010.08.10:11.43) :
DATABASE:USER
 $\text{AC(O)}=1, \text{T}=1600, \text{P}=1.01325\text{E}5, \text{N}=1;$



Indirect evidence suggests that the SiO_2 thermodynamic activity is lower in the $\text{Y}_2\text{O}_3\text{-Y}_2\text{SiO}_5$ and $\text{Y}_2\text{SiO}_5\text{-Y}_2\text{Si}_2\text{O}_7$ regions
But there are no direct measurements!

Methods to measure silica activity

- Oxidation-reduction equilibrium using gas mixtures or electrochemical cells
- High temperature reaction calorimetry
- **Knudsen Effusion Mass Spectrometry**

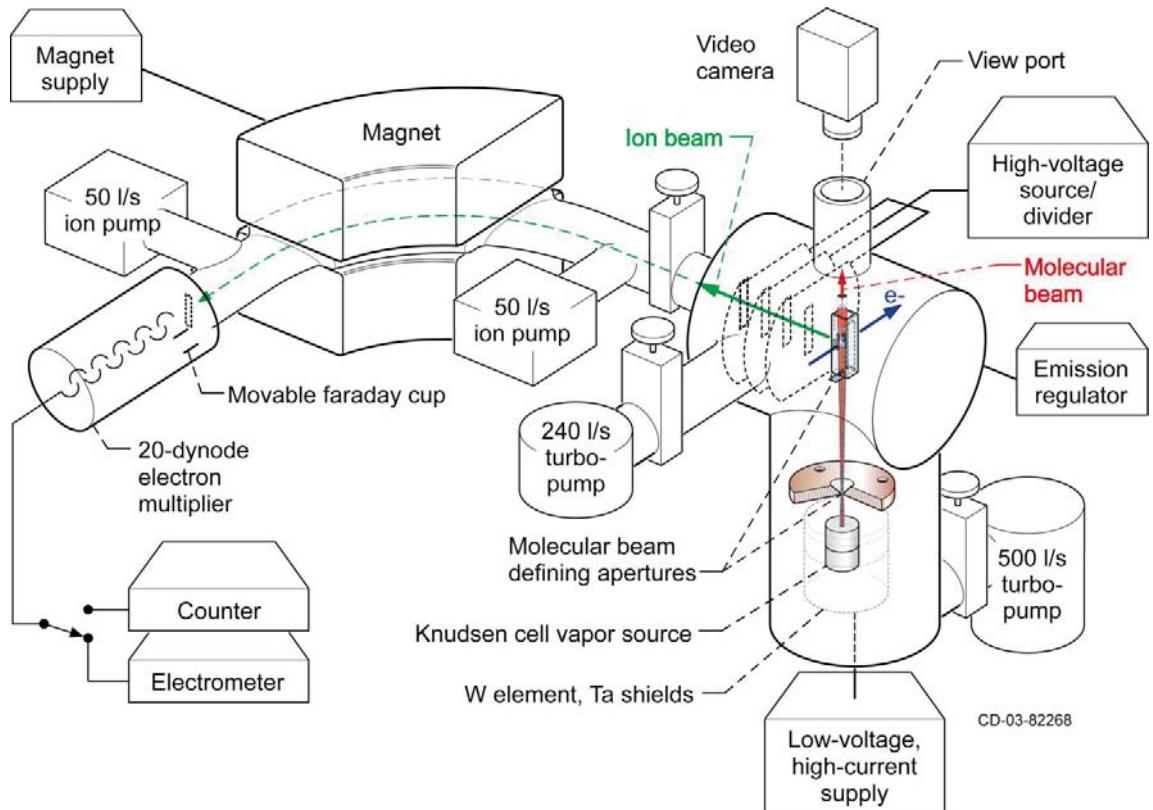
Mass spectrometer: $I(\text{SiO}) \rightarrow P(\text{SiO}) \rightarrow a(\text{SiO}_2)$



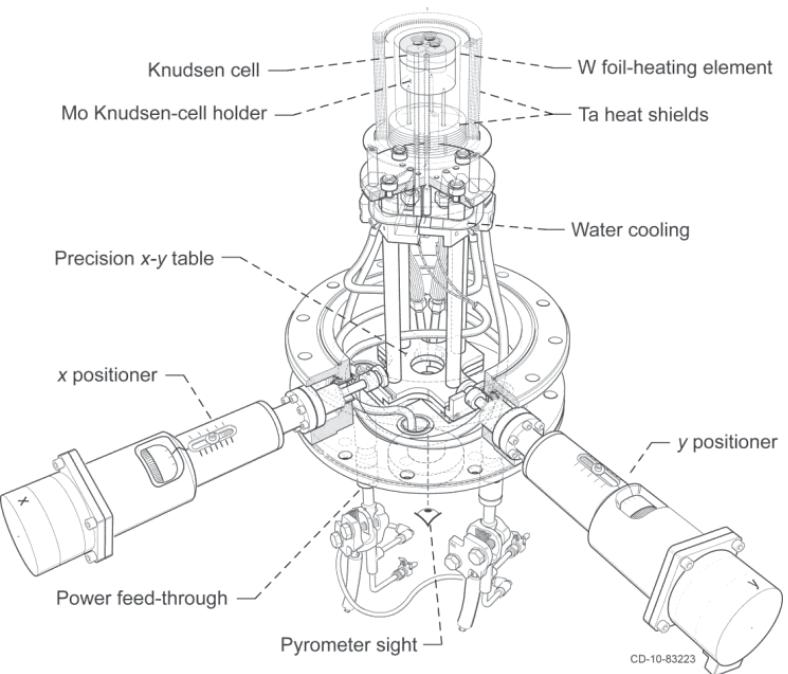
Two approaches

Y and Yb silicates + *reducing agent to boost vaporization of SiO_2 without changing solid composition!

Knudsen Effusion Mass Spectrometry (KEMS)

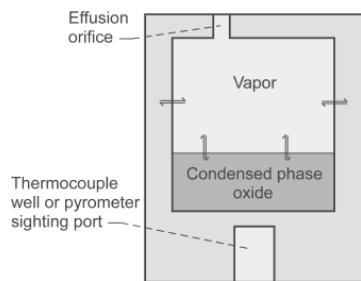


Use Multi-Cell Flange for a(SiO_2)



Design of E. Copland 2002

- 90° magnetic sector; non-magnetic ion source ion counting detector \Rightarrow no mass discrimination
- Cross axis electron impact ionizer
- Resistance heated cell; multiple Knudsen cell system
- Measurements to 2000°C, Pressure to 1×10^{-10} bar



$$p_i = k I_i^+ T / S_i$$

p_i = pressure of component i

k = instrument constant

T = Temperature (K)

S_i = ionization cross section





Issues with Measuring $a(\text{SiO}_2)$ in RE Silicates

- Vapor pressure of SiO_2 too low to measure in temperature range of interest
- Need measurable signal for SiO_2 —use reducing agent to make excess SiO(g) . Tried several, selected Mo or Ta
 - For $a(\text{SiO}_2) < \sim 0.02$
 - $2\text{Ta(s)} + 2\text{SiO}_2(\text{soln}) = 2\text{SiO(g)} + \text{TaO(g)} + \text{TaO}_2(\text{g})$
 - For $a(\text{SiO}_2) > \sim 0.02$
 - $\text{Mo(s)} + 3\text{SiO}_2(\text{soln}) = 3\text{SiO(g)} + \text{MoO}_3(\text{g})$
 - Note reducing agent must not change solid phase composition
 - Monosilicates + disilicates + Ta – leads to tantalates
- Need to account for non-equilibrium vaporization
- SiO overlaps with CO_2 ($m/e = 44$)
 - Use LN_2 cold finger for improved pumping
 - Shutter to distinguish vapor from cell and background
 - Gettering pump for CO_2

Approaches use two phase regions

Cells are part of the system

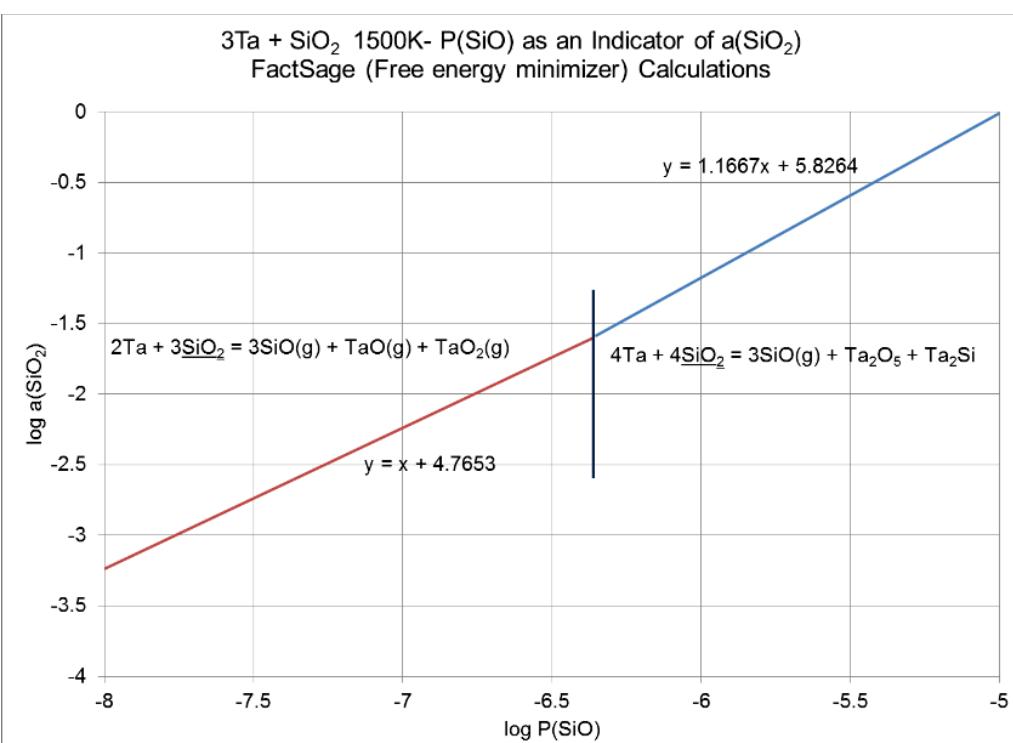
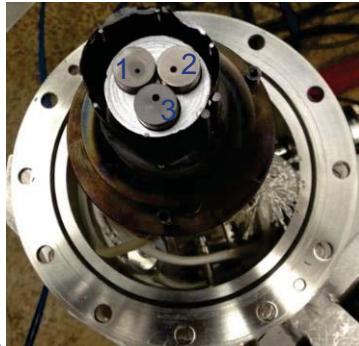
1 – Monosilicate + RE₂O₃

Two cells:

- Au
- 3Ta + Y₂O₃ + Y₂O₃ · SiO₂



- Using P_{eq}(SiO) and FactSage (free energy minimization)
- Correction for non-equilibrium vaporization

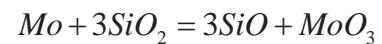


2 – Monosilicate + Disilicate

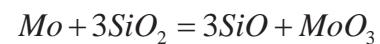
Three cells:

- Au (reference)
 - 3Mo + Y₂O₃ · 2SiO₂ + Y₂O₃ · SiO₂
 - 3Mo + SiO₂
- Mo(s) + 3SiO₂(soln) = 3SiO(g) + MoO₃(g)
- Compare cells 1 and 2
 - Less data processing than with Ta
 - Correction is not needed.

$$K = \frac{[P(\text{SiO})]^3 P(\text{MoO}_3)}{[a(\text{SiO}_2)]^3}$$



$$a(\text{SiO}_2) = 1 = \left\{ \frac{[P^\circ(\text{SiO})]^3 P^\circ(\text{MoO}_3)}{K} \right\}^{0.33}$$



$$a(\text{SiO}_2) = \left\{ \frac{[P(\text{SiO})]^3 P(\text{MoO}_3)}{K} \right\}^{0.33}$$

Cell 2

$$a(\text{SiO}_2) = \left\{ \frac{[I(\text{SiO})]^3 I(\text{MoO}_3)}{[I^\circ(\text{SiO})]^3 I^\circ(\text{MoO}_3)} \right\}^{0.33}$$

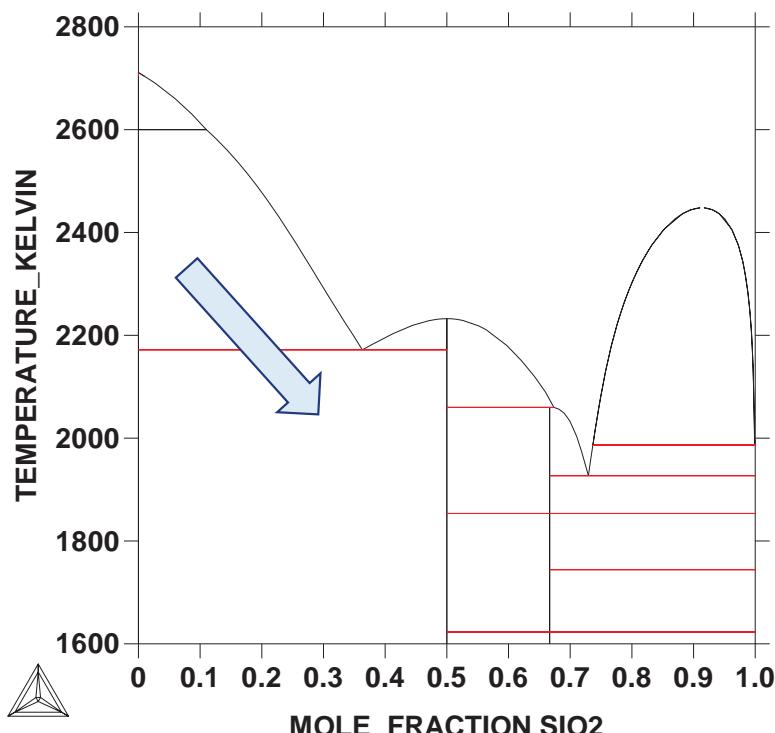
Cell 3



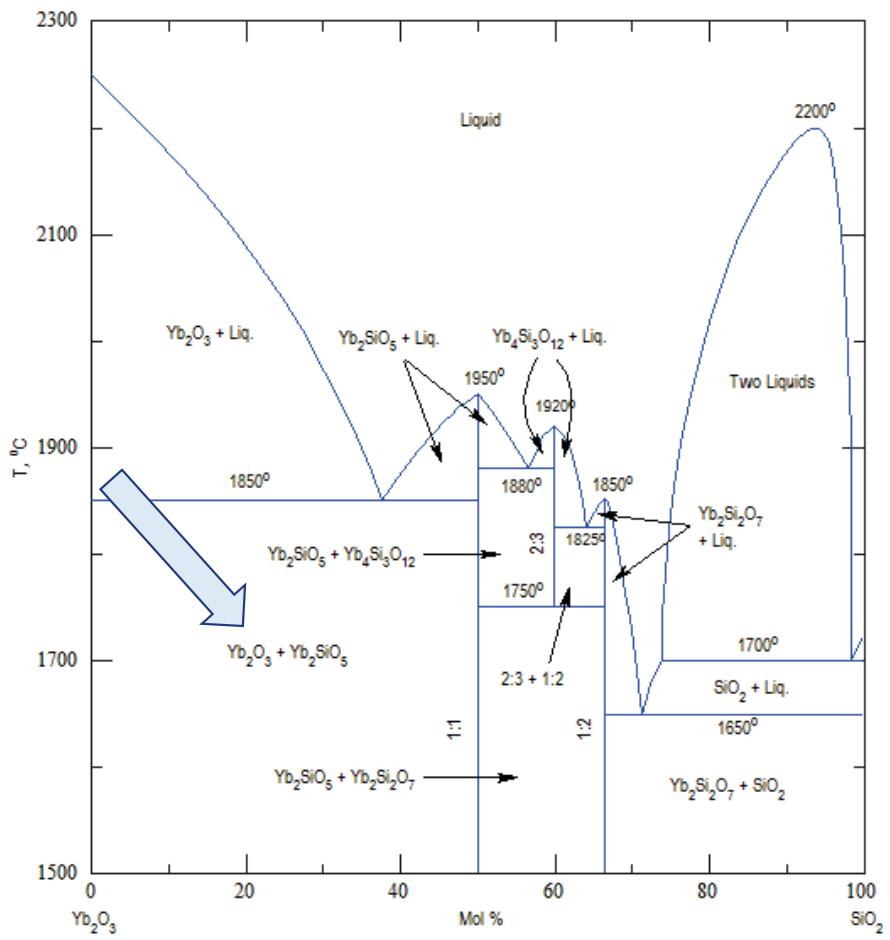
Monosilicate + RE₂O₃

Y₂O₃-SiO₂

THERMO-CALC (2010.08.10:09.24) :
DATABASE:USER
AC(O)=1, N=1, P=1.01325E5;

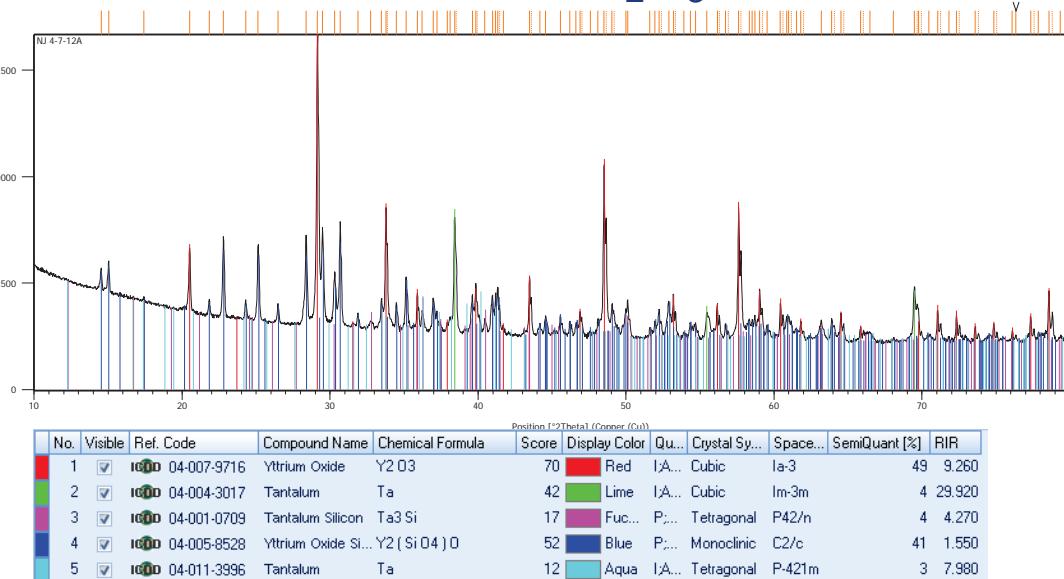


Yb₂O₃-SiO₂

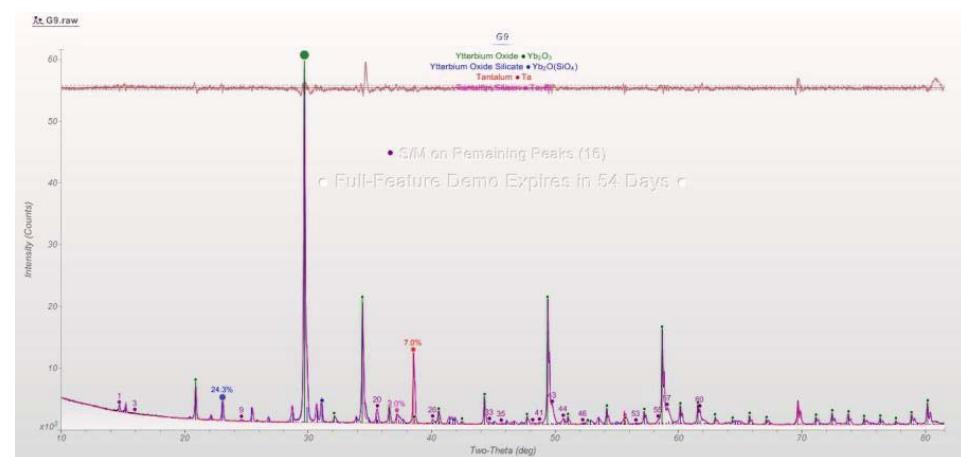


XRD after KEMS Measurements of RE Monosilicates + RE₂O₃ + Ta:

Yttrium monosilicate + Y₂O₃ + Ta



Ytterbium monosilicate + Yb₂O₃ + Ta



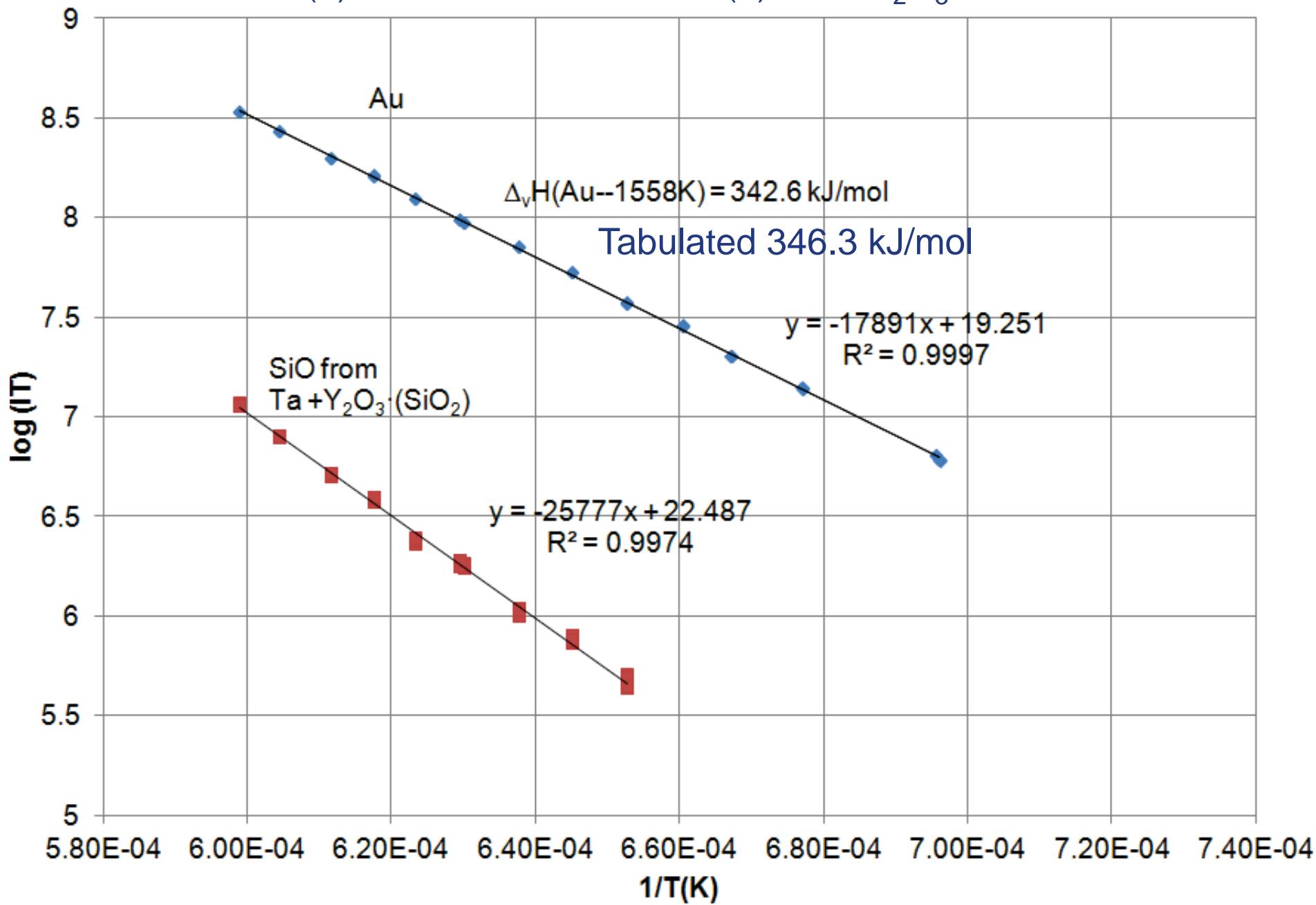
Phase	wt (%)
Y ₂ O ₃ ·(SiO ₂)	41
Y ₂ O ₃	49
Ta	4
Ta ₃ Si	4

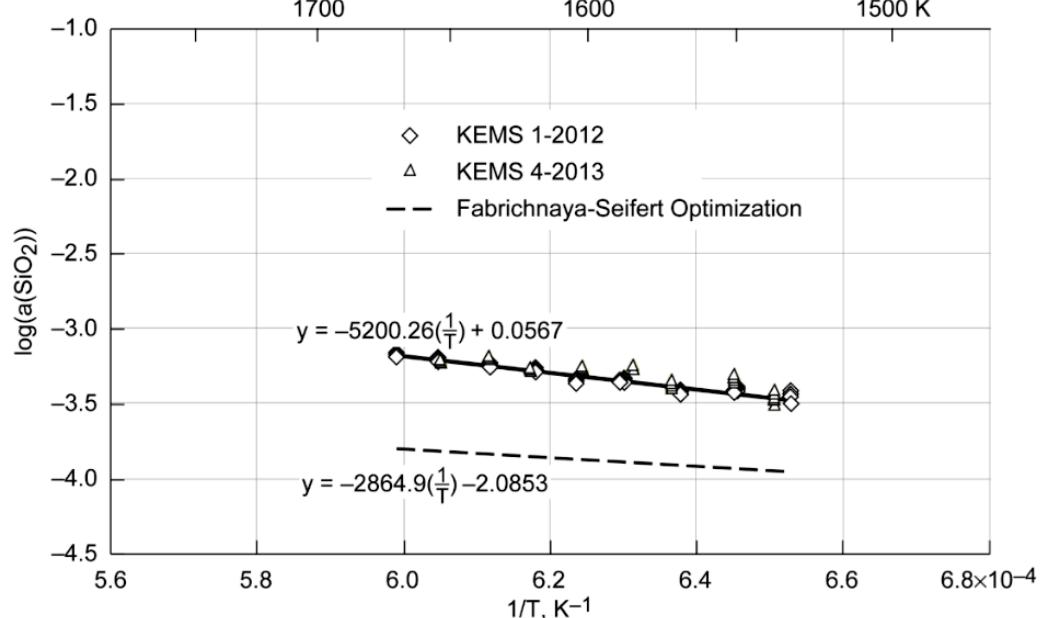
Phase	wt (%)
Yb ₂ O ₃ ·(SiO ₂)	24
Yb ₂ O ₃	66
Ta	2
Ta ₂ Si	2



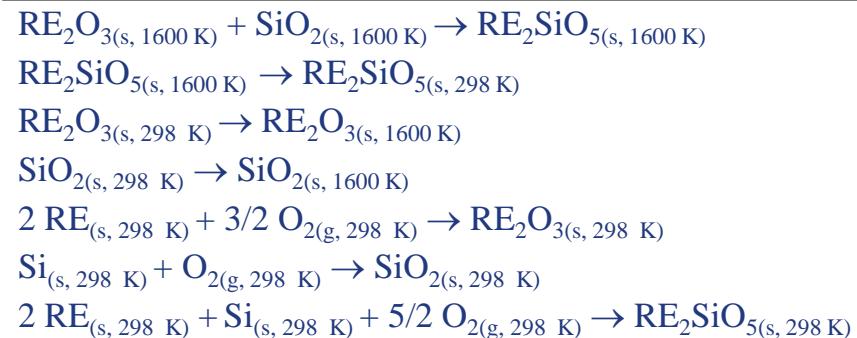
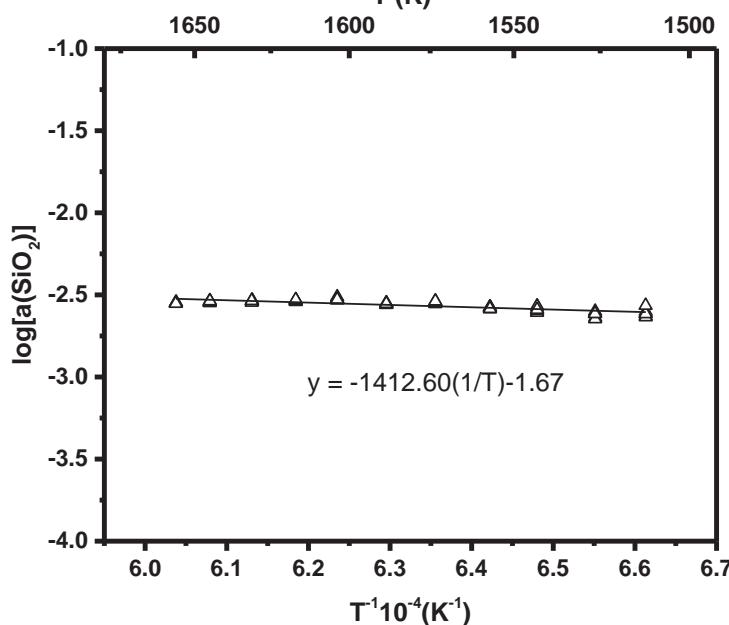
Raw Data—log (IT) vs 1/T

Cell (1): Au Reference

Cell (2): Ta + Y₂O₃ + MS

 $\text{Y}_2\text{O}_3 + \text{Y}_2\text{O}_3 \cdot (\text{SiO}_2)$ 

$$\Delta H_{(\text{SiO}_2, 1600 \text{ K})} = (5200.26) \cdot R \cdot 2.303 = 99.57 \text{ kJ/mol}$$

 $\text{Yb}_2\text{O}_3 + \text{Yb}_2\text{O}_3 \cdot (\text{SiO}_2)$ 

$$\Delta H_{(\text{SiO}_2, 1600 \text{ K})} = (1412.60) \cdot R \cdot 2.303 = 27.05 \text{ kJ/mol}$$

ΔH_1 = measured in this work

$\Delta H_2 = H_{1600 \text{ K}} - H_{298 \text{ K}}$

ΔH_3

ΔH_4

ΔH_5

ΔH_6

$\Delta H_7 = \Delta H_{f, \text{RE}_2\text{SiO}_5, 298 \text{ K}}$

$\Delta H_f, \text{RE silicate, 298 K (kJ/mol)}$

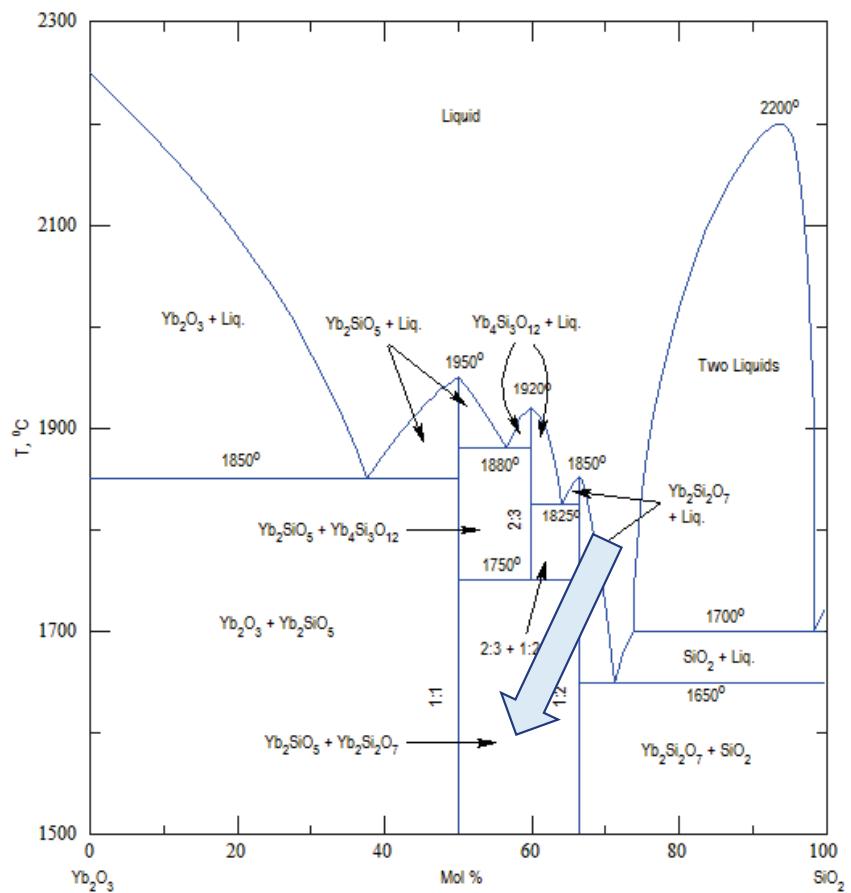
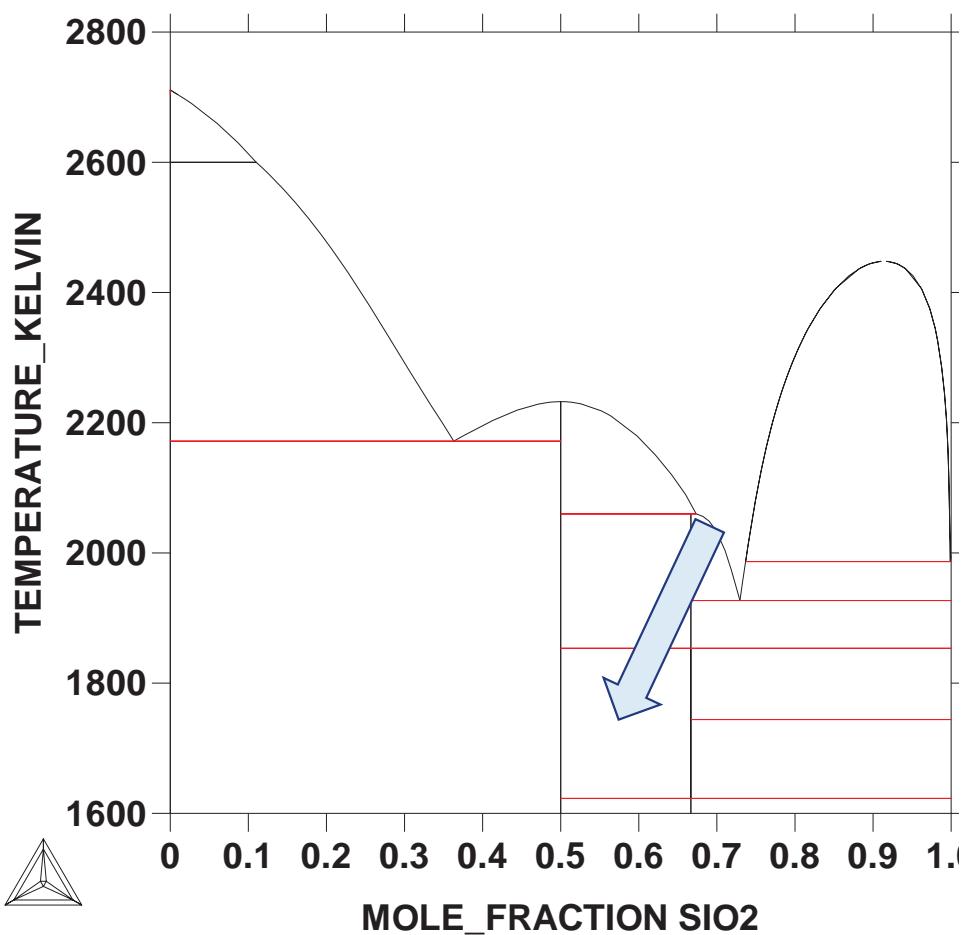
	KEMS	Calorimetry*	Optical basicity**	$a(\text{SiO}_2), 1650 \text{ K}$
$\text{Y}_2\text{O}_3 \cdot (\text{SiO}_2)$	-2907 ± 16	-2868.54 ± 5.34	0.786	0.000804
$\text{Yb}_2\text{O}_3 \cdot (\text{SiO}_2)$	-2744 ± 11	-2774.75 ± 16.48	0.729	0.00298

*Liang et al. "Enthalpy of formation of rare-earth silicates Y_2SiO_5 and Yb_2SiO_5 and N-containing silicate $\text{Y}_{10}(\text{SiO}_4)_6\text{N}_2$ ", J. Mater. Res. 14 [4], 1181-1185. **J. A. Duff, J. Phys. Chem. A 110, 13245 (2006)

Monosilicate + Disilicate

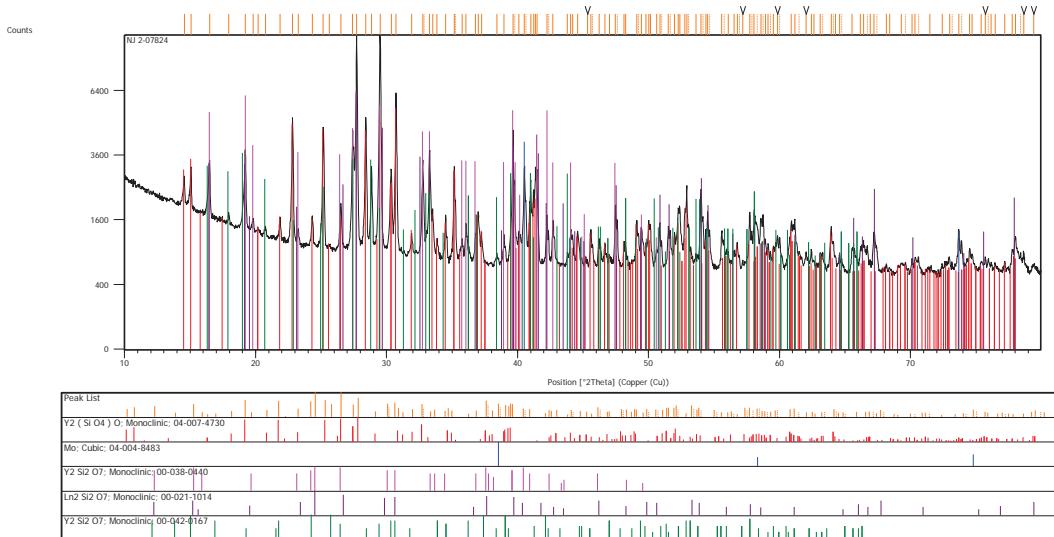


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 AC(O)=1, N=1, P=1.01325E5;



XRD after KEMS Measurements of RE Monosilicates + Disilicates + Mo:

Yttrium monosilicate + disilicate +Mo



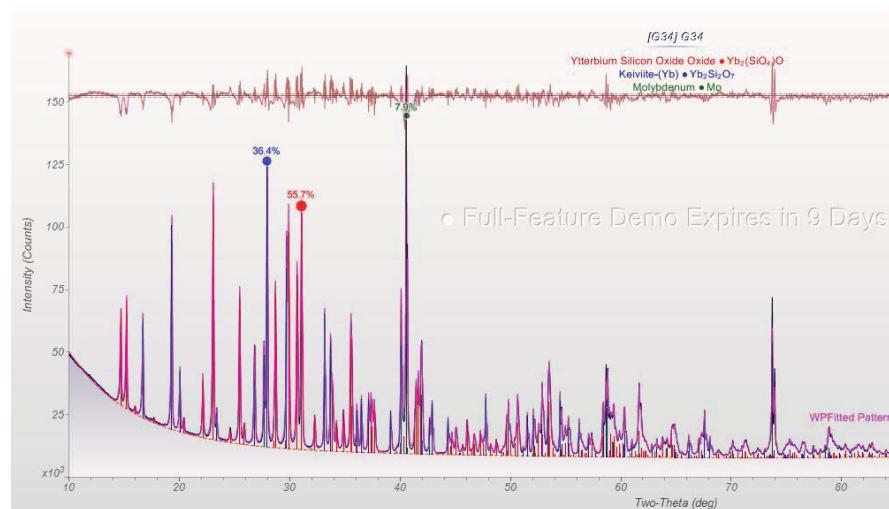
Phase

$\text{Y}_2\text{O}_3\cdot(\text{SiO}_2)$

$\text{Y}_2\text{O}_3\cdot2(\text{SiO}_2)$

Mo

Ytterbium monosilicate + disilicate + Mo

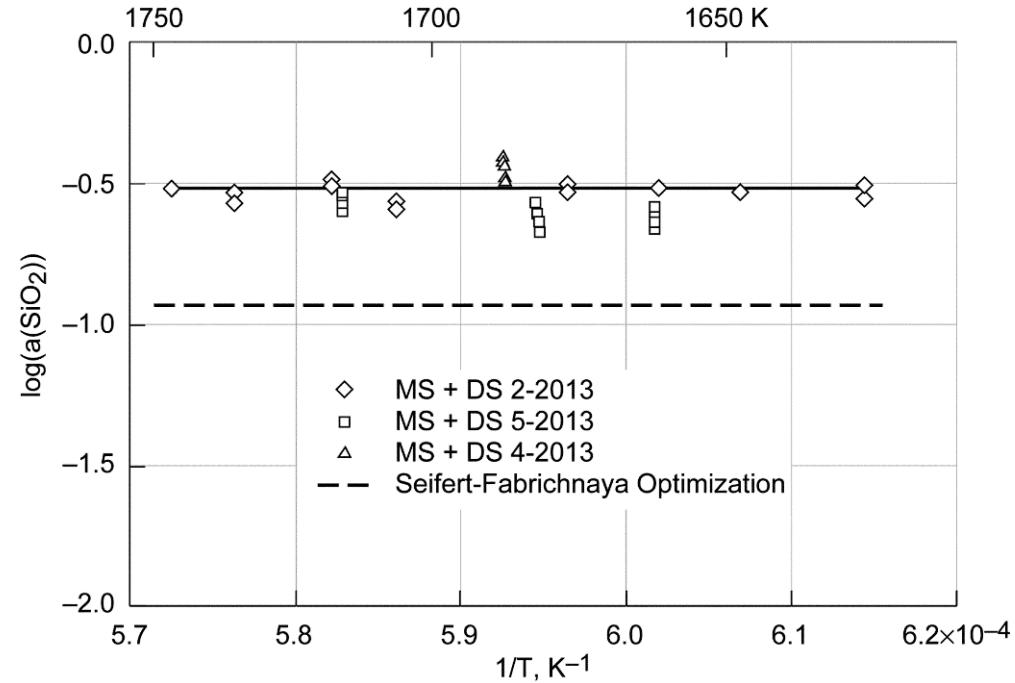
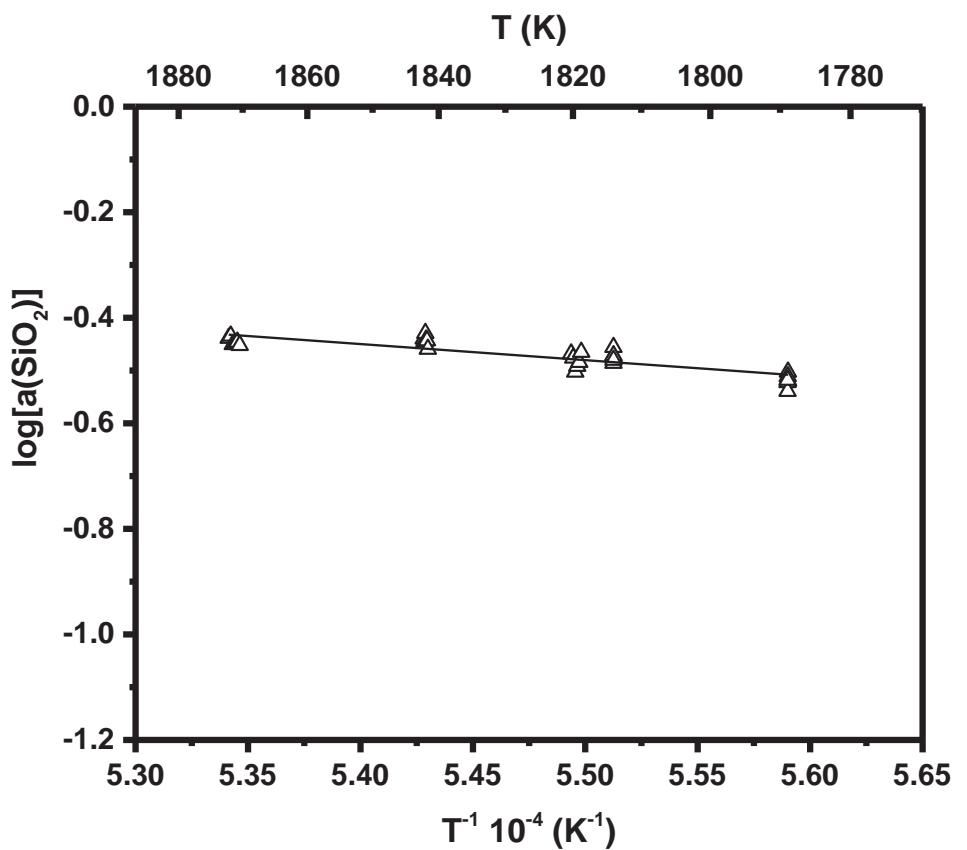


Phase wt (%)

$\text{Yb}_2\text{O}_3\cdot(\text{SiO}_2)$ 56

$\text{Yb}_2\text{O}_3\cdot2(\text{SiO}_2)$ 36

Mo 8


 $\text{Y}_2\text{O}_3\cdot(\text{SiO}_2) + \text{Y}_2\text{O}_3\cdot2(\text{SiO}_2)$

 $\text{Yb}_2\text{O}_3\cdot(\text{SiO}_2) + \text{Yb}_2\text{O}_3\cdot2(\text{SiO}_2)$


Optical basicity**

 $\text{Y}_2\text{O}_3\cdot(\text{SiO}_2) \quad \text{Y}_2\text{O}_3\cdot2(\text{SiO}_2)$

0.786 0.699

 $\text{Yb}_2\text{O}_3\cdot(\text{SiO}_2) \quad \text{Yb}_2\text{O}_3\cdot2(\text{SiO}_2)$

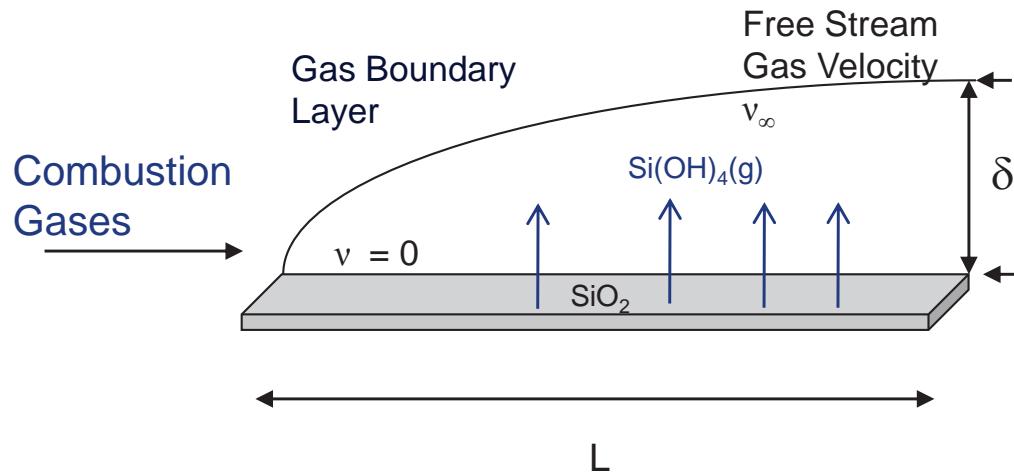
0.729 0.657

 $a(\text{SiO}_2), 1650 \text{ K}$

0.281

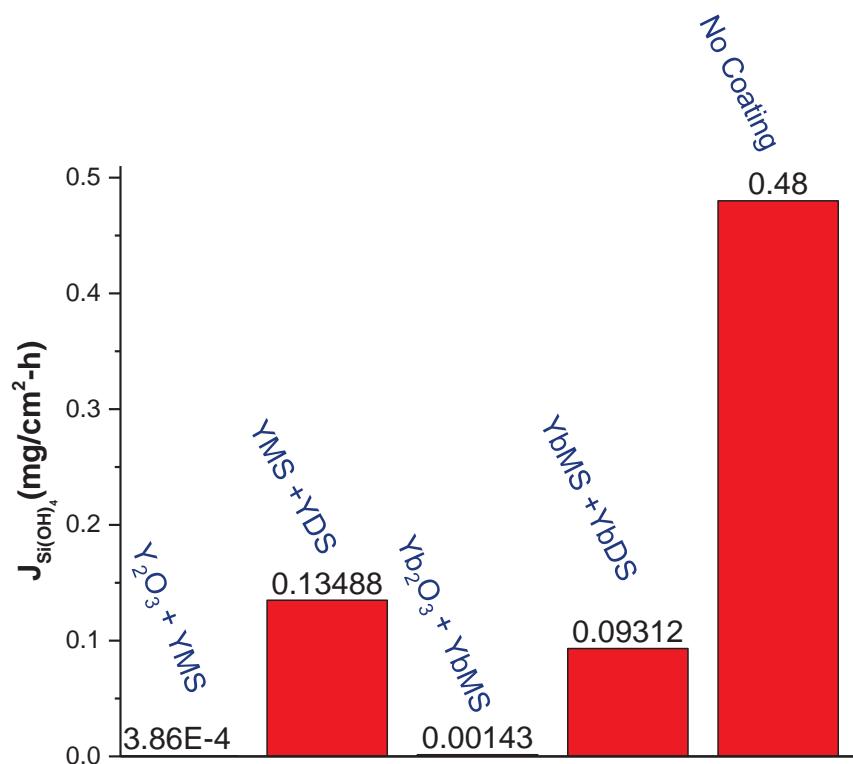
0.194

Now Have the Needed Quantities for Modeling Recession



$$\text{Flux} = 0.664 \left(\frac{v_\infty \rho_\infty L}{\eta} \right)^{0.5} \left(\frac{\eta}{D_{Si(OH)_4} \rho_\infty} \right)^{0.33} \frac{D_{Si(OH)_4}}{R T L} K a_{SiO_2} (P_{H_2O})^2$$

- $T = 1300^\circ\text{C}$; $P = 10 \text{ bar}$; $P(\text{H}_2\text{O}) = 1 \text{ bar}$
- $v_\infty = 20 \text{ m/s}$
- $L = 10 \text{ cm}$
- $\eta = 5 \times 10^{-4} \text{ g/cm-s}$
- $\rho_\infty = 2.2 \times 10^{-3} \text{ g/cc}$
- $D_{Si(OH)_4} = 0.19 \text{ cm}^2/\text{s}$
- $\log K = -2851.2/T - 3.5249$ ($Si(OH)_4(g)$ transpiration measurements)
- $a(SiO_2)$ from activity measurements





Summary: Thermochemistry of EBC materials

- The reduced SiO_2 activity in Rare-earth silicates should limit their reactivity with water vapor
- Solid State rare earth oxides—activity of SiO_2
 - Vapor pressure techniques—Knudsen effusion mass spectrometry
 - Need reducing agent to obtain a measurable signal for SiO(g) , which in turn relates to activity of SiO_2 . Reducing agent must not change solid phase composition.
 - Method and choice of reducing agent depends on particular silicate
- Thermodynamic data for gas phase hydroxides and solid candidate coating \Rightarrow recession modeling input data



Acknowledgements

- Helpful discussions with B. Opila (Formerly NASA Glenn now Univ of Virginia)
- Multiple cell and sampling system improvements to mass spectrometer: E. Copland (formerly NASA Glenn now CSIRO, Sydney, Australia)
- XRD: R. Rogers (NASA Glenn)