

The development of a deflectometer for accurate surface figure metrology



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Introduction

Marshall Space Flight Center is developing the method of direct fabrication for high resolution full-shell x-ray optics. In this technique the x-ray optics axial profiles are figured and polished using a computer-controlled Zeeko IRP600X polishing machine (shown in figure 1). Based on the Chandra optics fabrication history about one third of the manufacturing time is spent on *moving* a mirror between fabrication and metrology sites, reinstallation and alignment with either the metrology or fabrication instruments. Also, the accuracy of the alignment significantly affects the ultimate accuracy of the resulting mirrors. In order to achieve higher convergence rate it is highly desirable to have a metrology technique capable of in situ surface figure measurements of the optics under fabrication, so the overall fabrication costs would be greatly reduced while removing the surface errors due to the re-alignment necessary after each metrology cycle during the fabrication. The goal of this feasibility study is to demonstrate if the Phase Measuring Deflectometry can be applied for in situ metrology of full shell x-ray optics. Examples of the full-shell mirror substrates suitable for the direct fabrication are shown in figure 2.

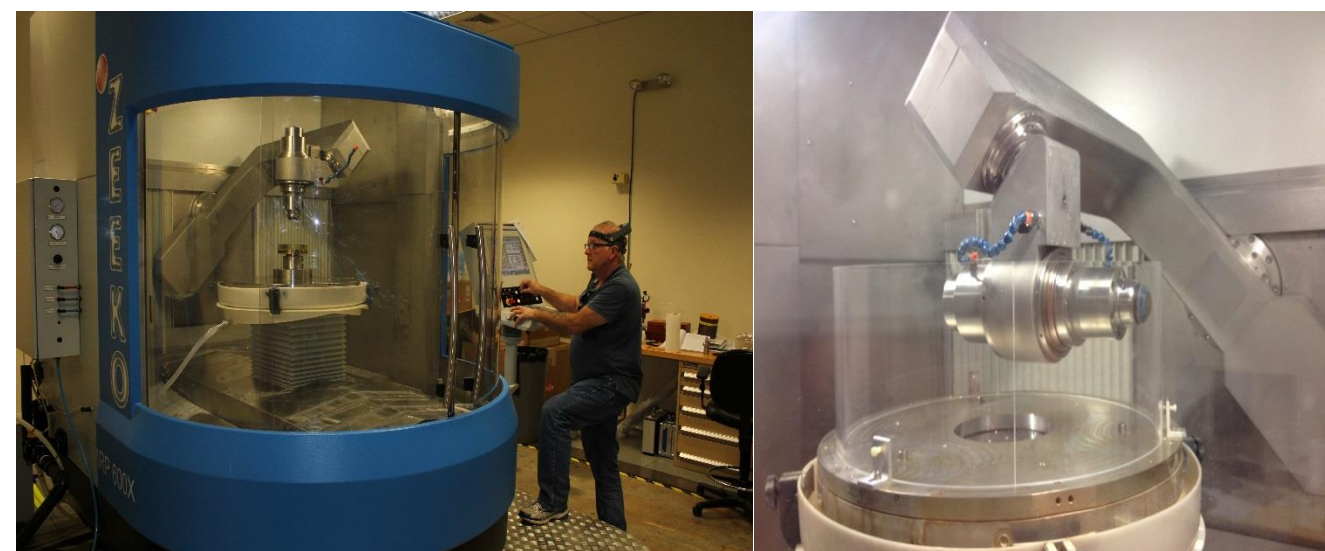


Figure 1. Zeeko IRP600X computer-controlled polishing machine (left). The polishing arm of the machine with the “bonnet” tool installed inside a plastic shell (right).



Figure 2. Aluminum (left) and glass (right) substrates for the direct fabrication of high resolution x-ray optics

Phase Measuring Deflectometry

The concept here is as follows: a perfect fringe pattern displayed by a monitor is observed after refraction from the surface under the test by a camera as shown in figure 1. Deviations from perfect spacing of the observed fringe pattern measured at multiple phases would provide unambiguous measurement of deviations in the slopes of the mirror surface from its ideal shape.

Algorithm steps:

- Generation of “perfect sinusoidal fringe pattern
- Phase recovery using phase shifting
- Generating the reference phase map
- Unwrapping the phase difference
- Slope profile recovery by slope profile integration

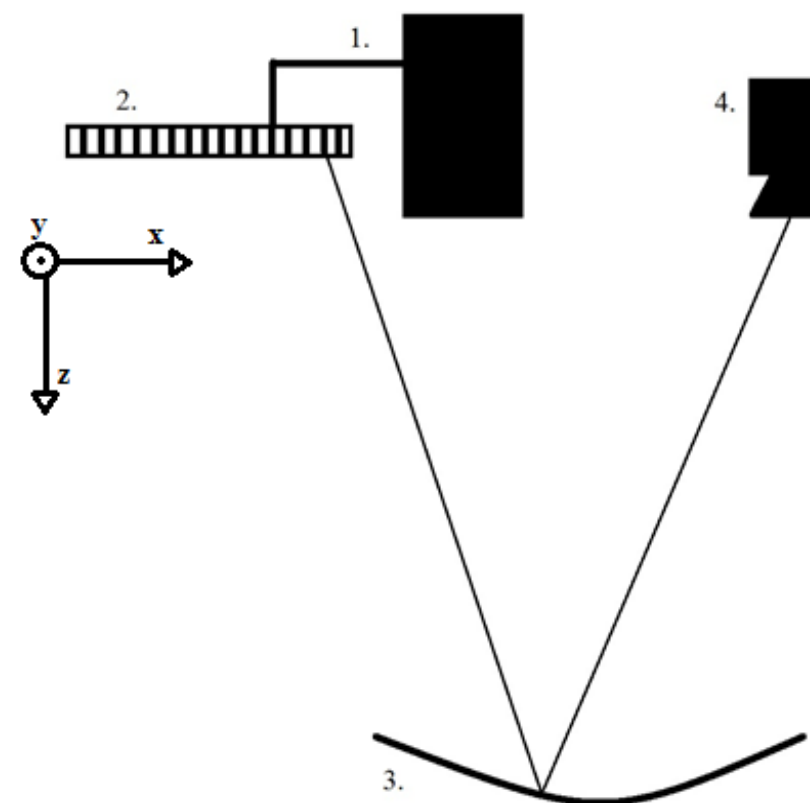


Figure 1. The schematic of the phase measuring deflectometry (PMD) method. A camera (4) observes the fringe pattern generated by computer (1) on a monitor (2) and reflected from the specular surface under the test (3). The observed fringe pattern is distorted. The figure of the surface can be derived from the distorted pattern. As it can be seen the observation angle does not have to be normal to the surface under the test.

Advantages of the PMD:

- It measures the surface slope directly
- It is relatively insensitive to vibrations,
- No trace errors (does not need a compensator)
- immune to coherent noise.
- It is fast, so many data sets can be averaged to reduce any random noise.
- It has been demonstrated that the PMD method is capable of nanometer resolution ^{3, 4} (on small, 100 mm, flat samples and almost at normal incidence with low resolution monitor-camera set)
- it does not require the incidence (observation) angle to be normal for the measurements
- does not require perfect positioning of the surface under test in the measuring system, so it can be adapted for in situ measurements in a manufacturing environment.

Disadvantages

- It is slope measuring method – calibration errors in the case when the height profile needs to be resolved
- Quality of fringe pattern defines the method resolution.
- The reference phase map needs to be calculated for given surface under the test.
- The highest resolution would be achieved at normal observation angle. The method resolution is lower for smaller observation angles

Experimental breadboard

A PMD breadboard have been developed. Photo of the breadboard is shown in Figure 4. In order to investigate the sensitivity of the method to low and mid-spatial-frequency surface errors three 4k cameras (Panasonic DMC-GH4-YAGH Lumix DMC-GH4 4K Micro Four Thirds Digital Camera with DMW-YAGH 4K Video Interface) are mounted on stages. The positions of the cameras regarding the surface under the test can be varied. The cameras can be connected to the Blackmagic Design HyperDeck Studio Pro 2 recorder with solid state hard drives to speed up the image collection and file transfer. Depending on the surface spatial frequency under test three different lenses (Panasonic LUMIX G Leica DG Summilux 15mm f/1.7 ASPH. Lens, Panasonic Leica DG Summilux 25mm f/1.4 ASPH Micro 4/3 Lens, Olympus M.Zuiko Digital ED 75mm f/1.8 Lens) can be installed on the cameras. The sinusoidal fringe pattern is generated on the 4k monitor (Dell UltraSharp UP3214Q 31.5-Inch Screen LED-Lit Monitor).

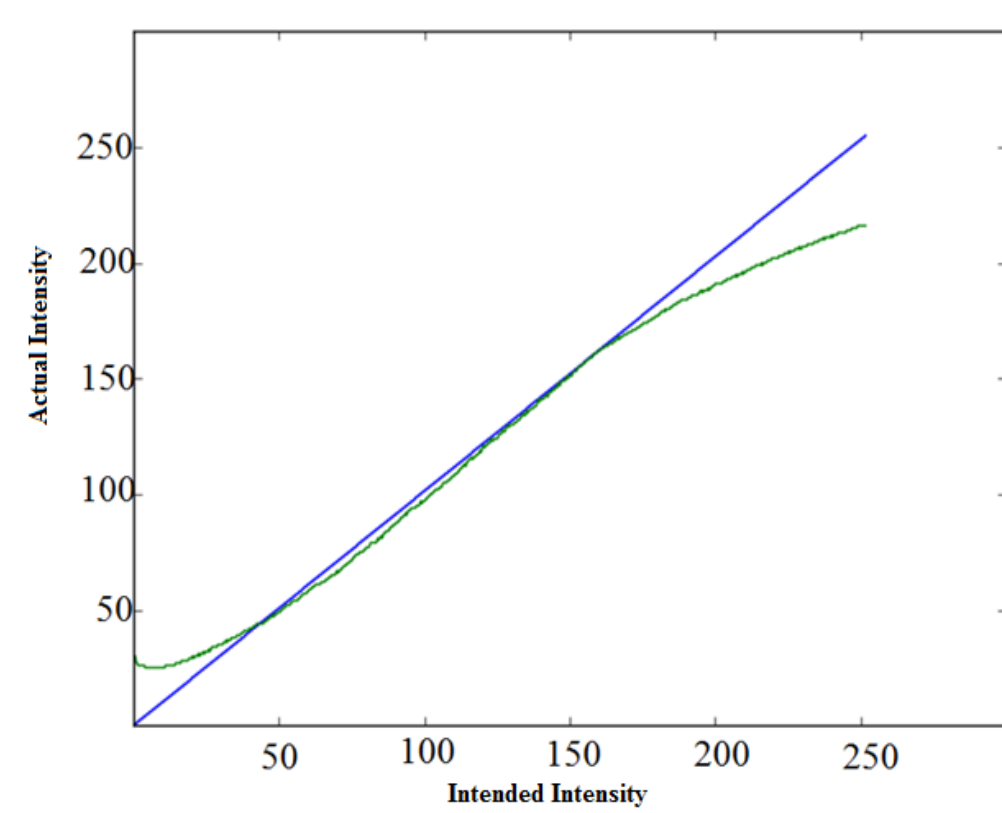


Figure 5. Actual monitor gray scale intensity (green) as captured by the camera. Blue line represents the intended intensity as generated by computer

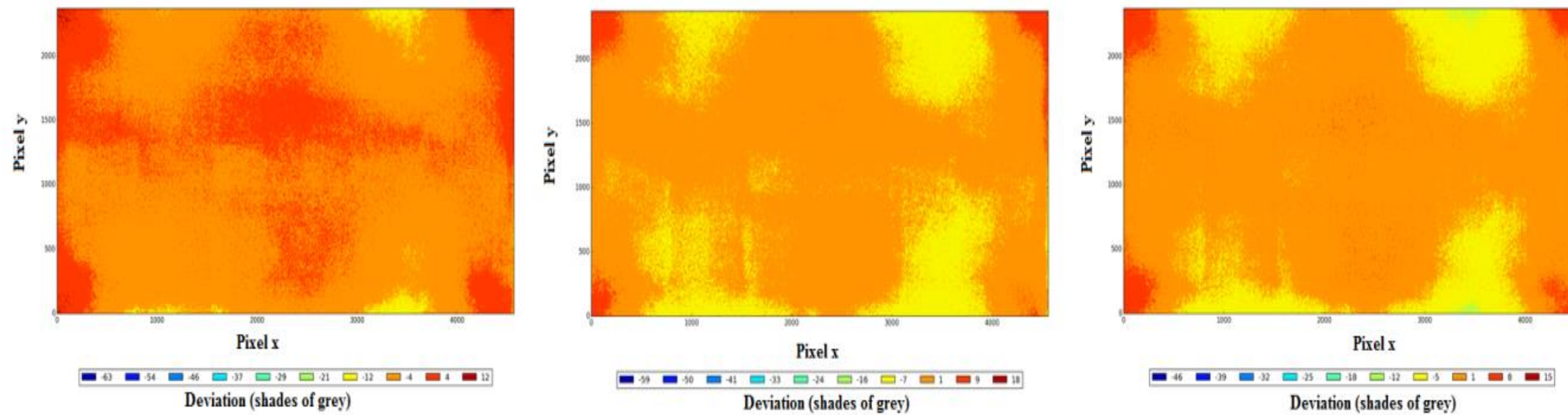


Figure 6. Examples of the monitor intensity distributions captured by camera for three different levels of gray scale generated by computer

PMD Breadboard calibration

To ensure high accuracy surface error measurements the monitor response and the camera lens distortions needs to be measured and calibrated out. Initial calibration was done using the ColorMunki calibrator at the center of the monitor. Then, the linear gray scale was generated at the center of computer monitor and one of the cameras was used to capture the gray scale image. The captured gray scale intensities are plotted on the Figure 5. This calibration curve was used to produce linear gray scale for each monitor pixel. The scale was also limited to the range from 60 to 220 to minimize the fringe distortions.

In order to define the global gray scale offset for the monitor the images of 160 uniform gray scale intensities were collected. Samples of the captured intensity maps are shown in figure 6. The gray scale distortion pattern was calculated for each monitor pixel using these data. The average gray scale offset was calculated, the offset map is shown in figure 7. This map was used to correct global distortion of the gray scale on the monitor.

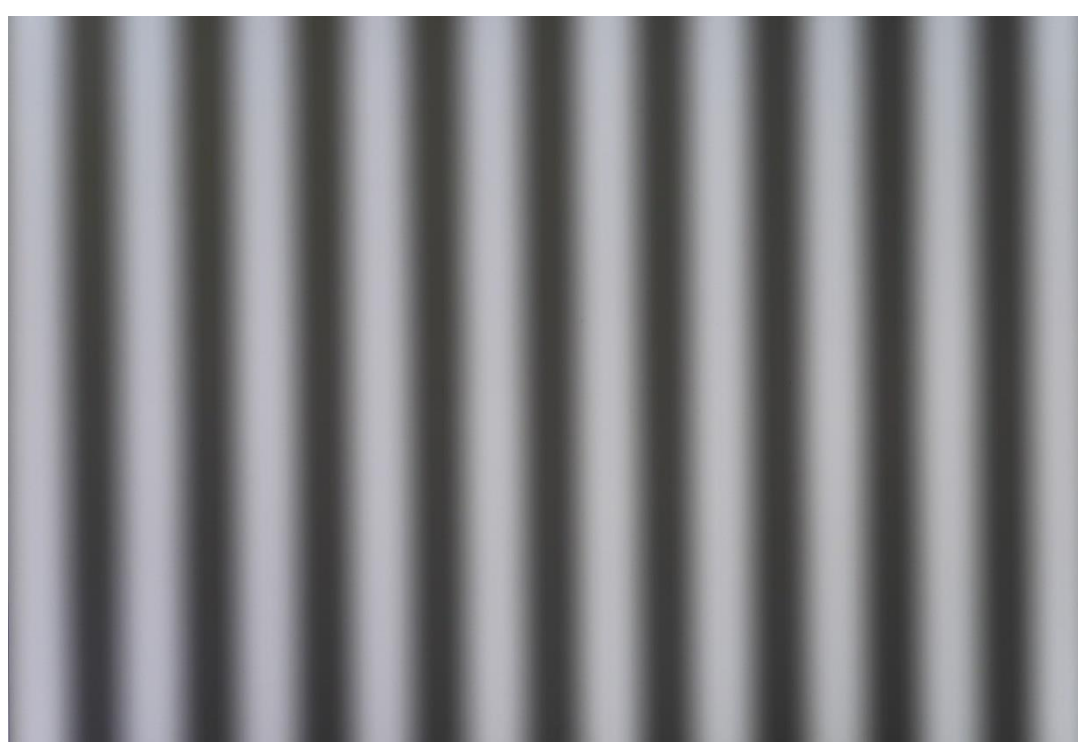


Figure 8. Sinusoidal fringe pattern generated using gray scale and global offset calibration results.

The sinusoidal fringe pattern was generated using the monitor calibration data. The fringe pattern was captured by camera and it is shown in Figure 8. To demonstrate the improvement of the pattern quality the captured and fitted fringe patterns with and without monitor calibration are shown in figure 9.

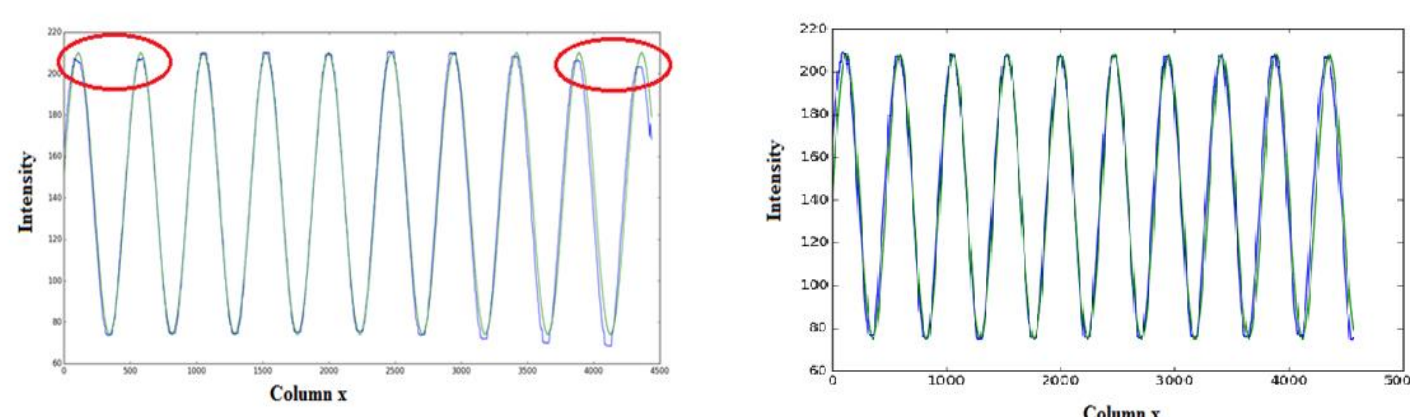


Figure 9. Captured sinusoidal fringe pattern with the fitted fringe pattern before (left) and after (right) gray scale and offset calibration

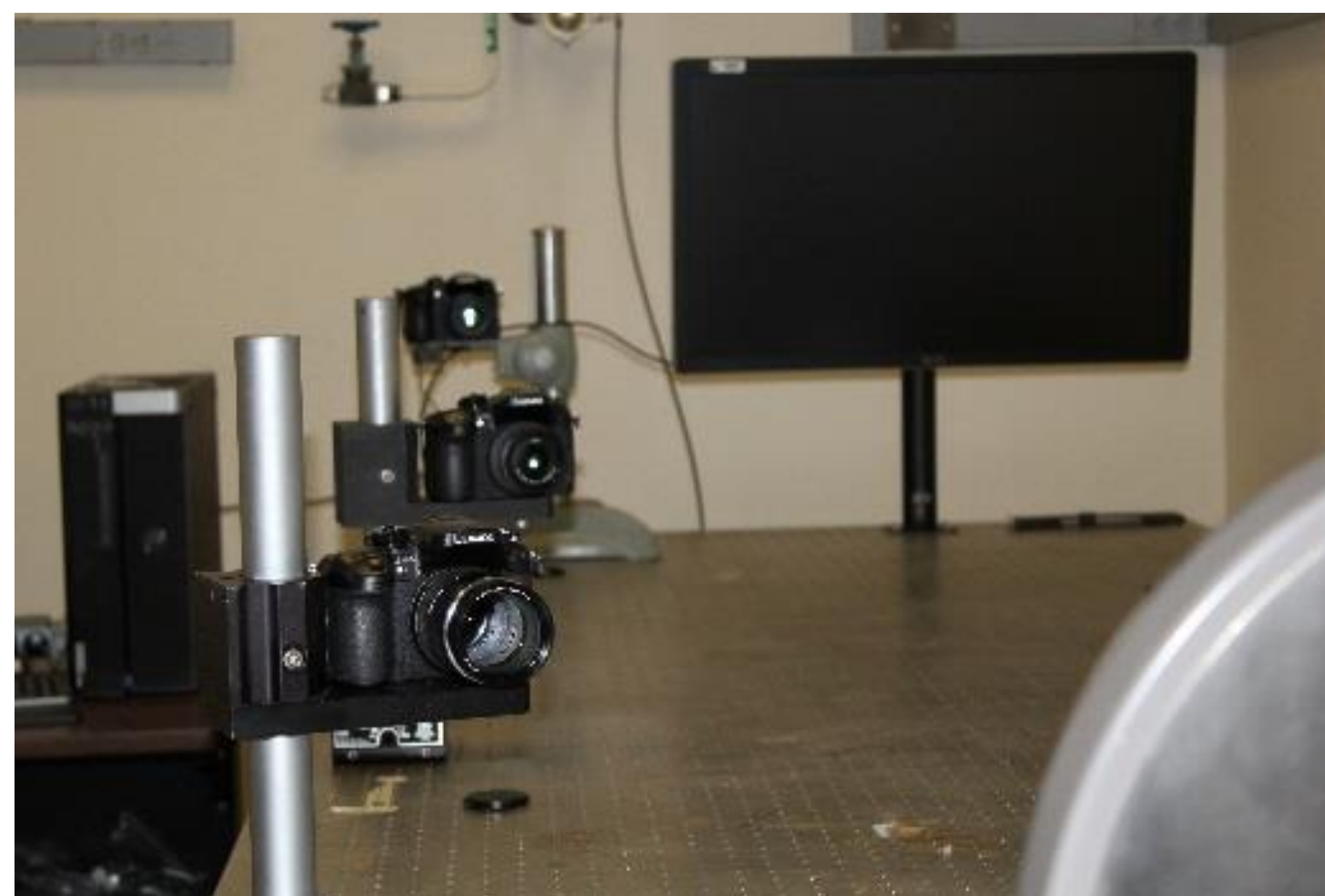


Figure 4. Experimental breadboard developed for the PMD studies. Three cameras positioned on an optical table collect the interference pattern generated by the monitor and reflected from a mirror under the test. Back of the mirror support stage is seen on the right bottom corner of the photo

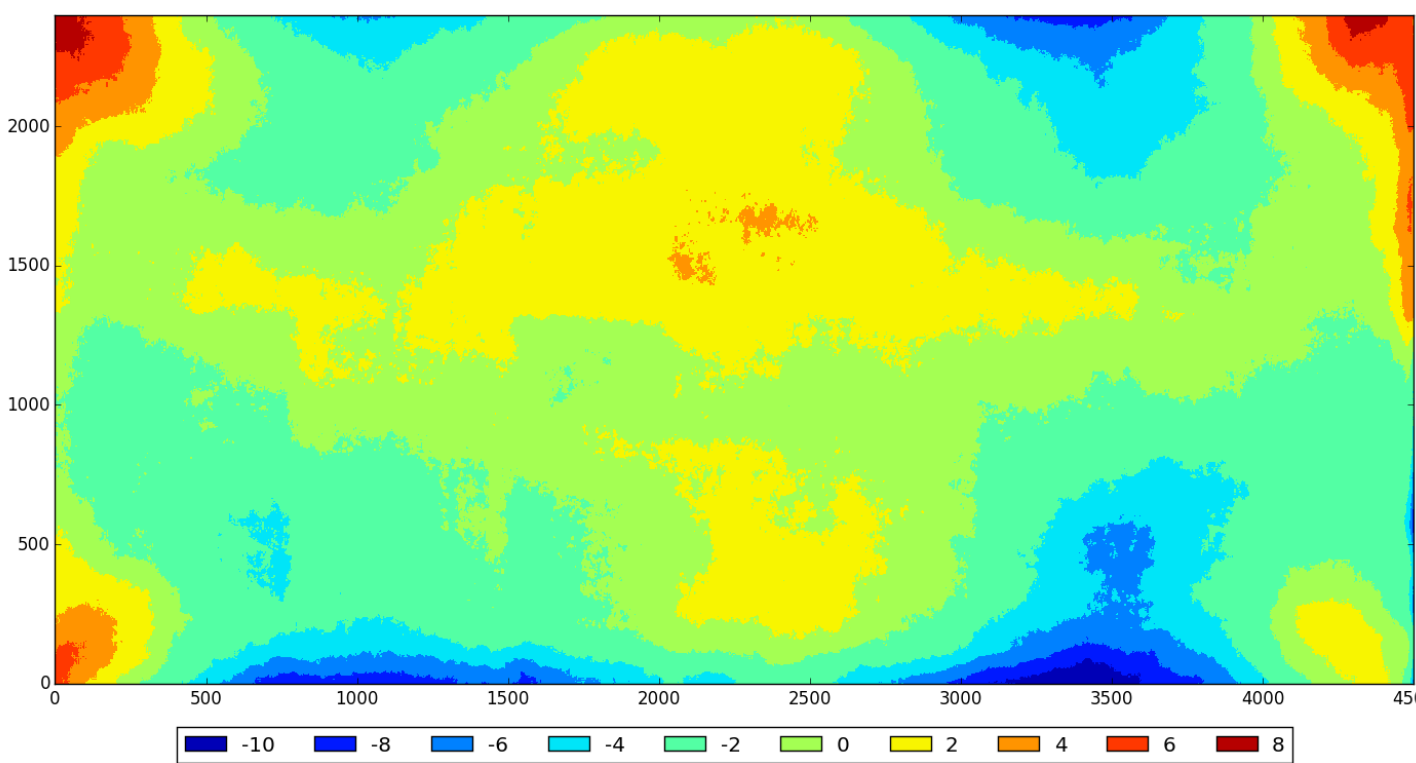


Figure 7. The heat map of the gray scale offset at the monitor

Conclusions and Future Work

- The PMD breadboard is assembled at the MSFC. The breadboard calibrations are currently in progress.
- The PMD measurements of flat and cylindrical samples are planned for September 2015.

Acknowledgements

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