



Thermodynamics and Kinetics of Silicate Vaporization

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Phase Stability, Diffusion Kinetics, and their Applications

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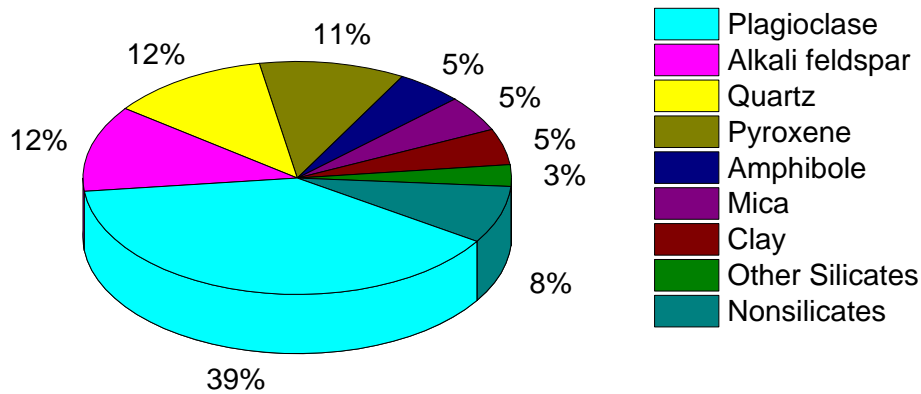


Outline of Presentation

- Silicates are truly the 'ubiquitous material'—found everywhere!
 - Natural systems: found in many minerals and rocks
 - Technology—coatings, structural ceramics
- Apply Knudsen Effusion Mass Spectrometry (KEMS) to study thermochemistry of silicates
 - KEMS allows measurement of equilibrium vapor pressures above condensed phase
 - Unique challenges
 - Complex vaporization behavior
 - Kinetic barriers to vaporization
- Examples
 - Geology: Thermochemistry of Olivine
 - Technology: Thermochemistry Y_2O_3 - SiO_2 and Yb_2O_3 - SiO_2 coating systems
- Vaporization kinetics of silicates

Silicates in Geology, Mineralogy and Planetary Science

- Over 90% of the Earth's crust consists of silicate minerals
 - Olivine ($(\text{Fe}_x\text{Mg}_{1-x})_2\text{SiO}_4$) primary constituent of earth's mantle



D. Perkins, Mineralogy, 3, Prentice Hall, 2011.



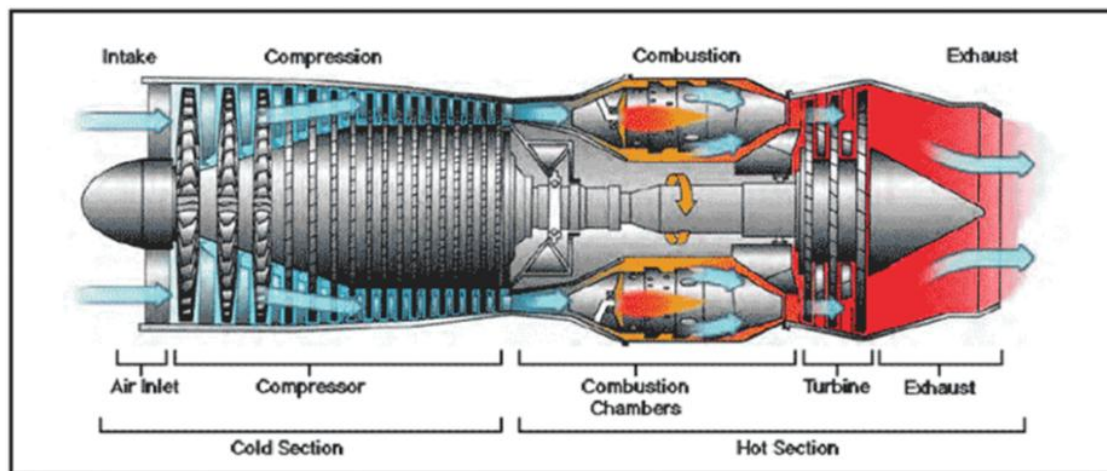
- Moon, Mars, Asteroids, Comets, Interplanetary dust particles and...

..Hot, rocky
exoplanets
(maybe!)



Silicates in Materials Science

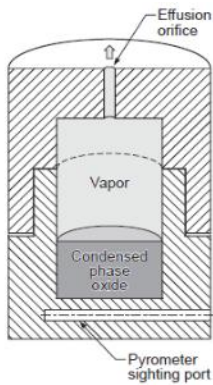
- High-Temperature Materials: Silicate Coatings



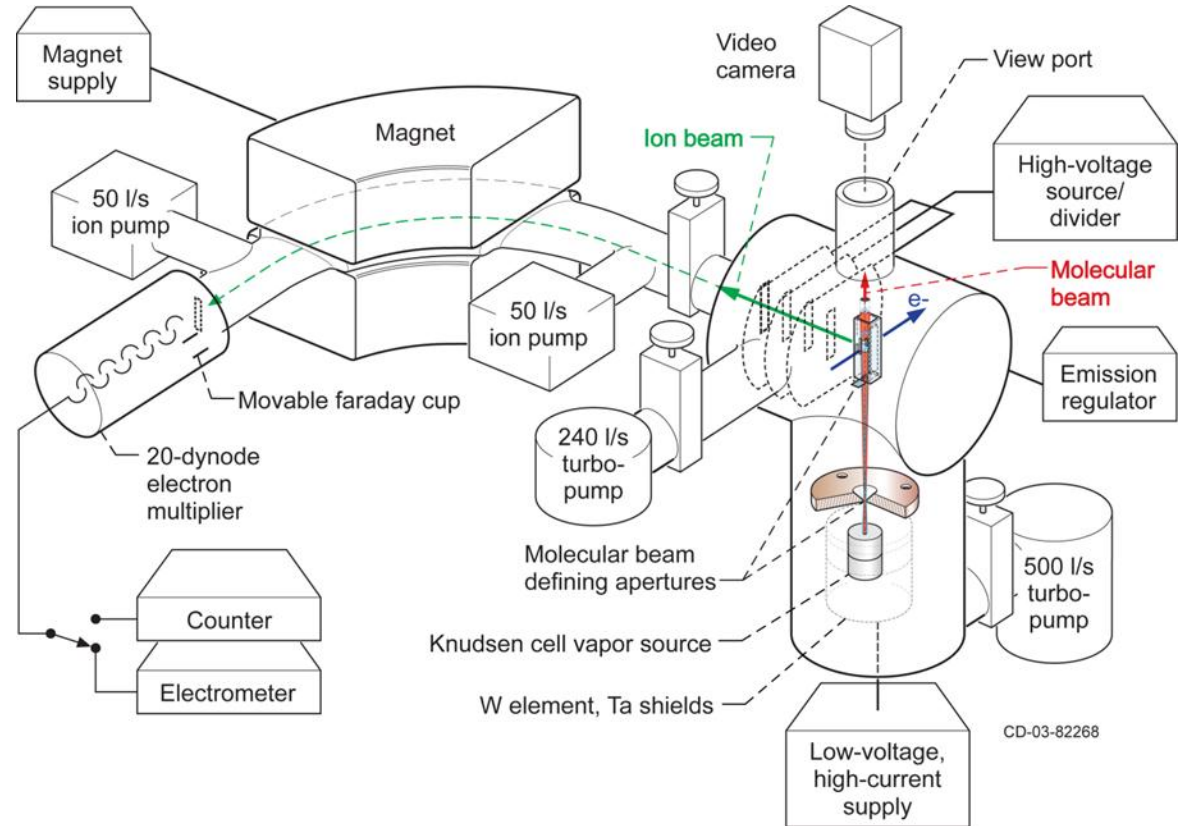
- Silicon-based ceramics: combustion chambers, static parts in hot stage
- Protective coating against water vapor, condensed phase deposits
 - Rare earth (RE) silicates $(RE_2O_3)_n(SiO_2)$

Knudsen Effusion Mass Spectrometry (KEMS)

Knudsen Cell: Condensed Phase/Gas Equilibrium



Direct Molecular Beam from Effusate Into Mass Spectrometer



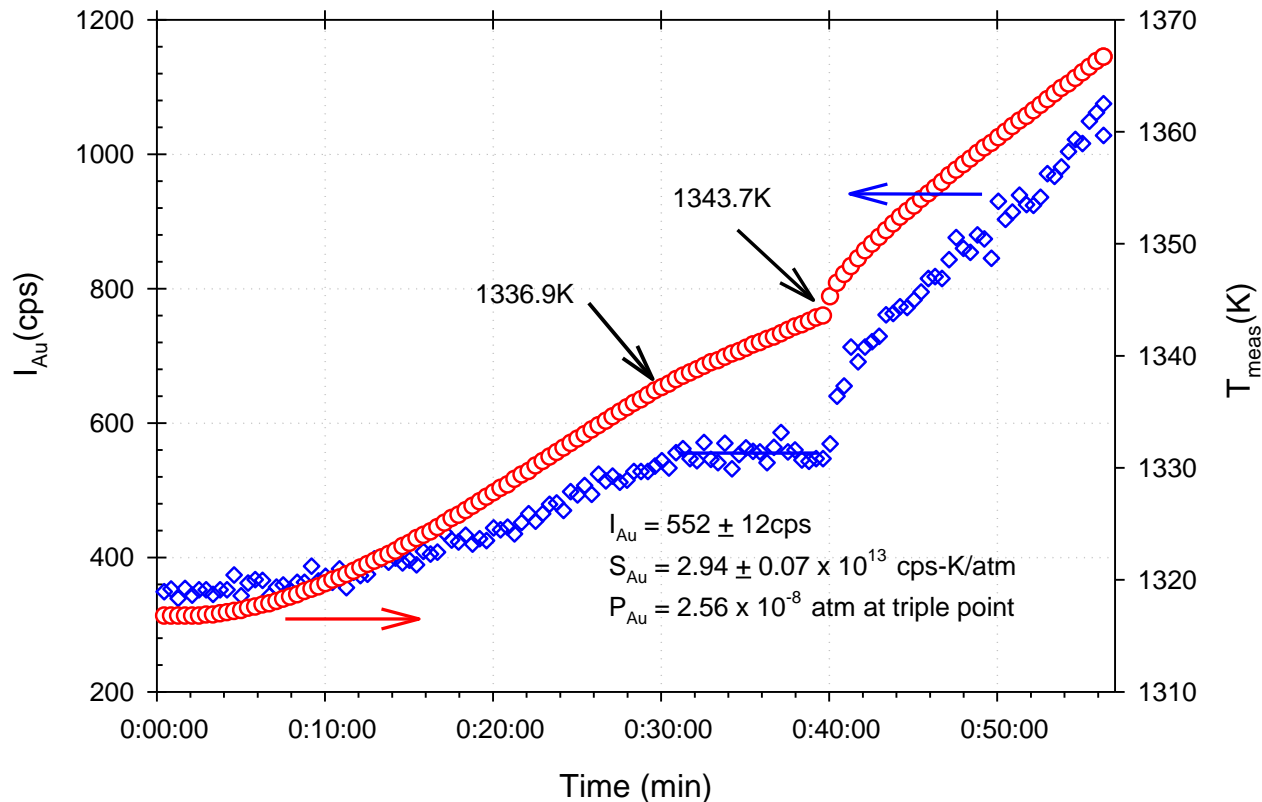
- Knudsen Cell: 1909
- Couple to mass Spectrometer: 1950s (Ingrahm et al.)
- Continuing valuable applications of these methods!



Standard Calibration Material: Au

- Temperature Measurement: very critical
- Use pyrometer (non-contact)
- At triple point: determine calibration constant

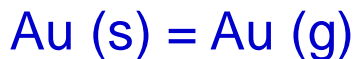
$$P_M = \frac{SIT}{\sigma}$$





Standard Calibration Material: Au

Heat of Vaporization Checks Temperature Calibration and Instrument Response



$$\Delta_v H^0 = -R^*(-41.162) = 342.20 \text{ kJ/mol}$$

Tables = 342 kJ/mol

$$\Delta_v G = \Delta_v H - T\Delta_v S = -RT \ln K_p = -RT \ln(P_M)$$

$$\ln P_M = \frac{-\Delta_v H}{R} \left(\frac{1}{T} \right) + \frac{\Delta_v S}{R}$$

$\ln P_M$ vs $1/T$ is a van't Hoff plot with slope = $\frac{-\Delta_v H}{R}$

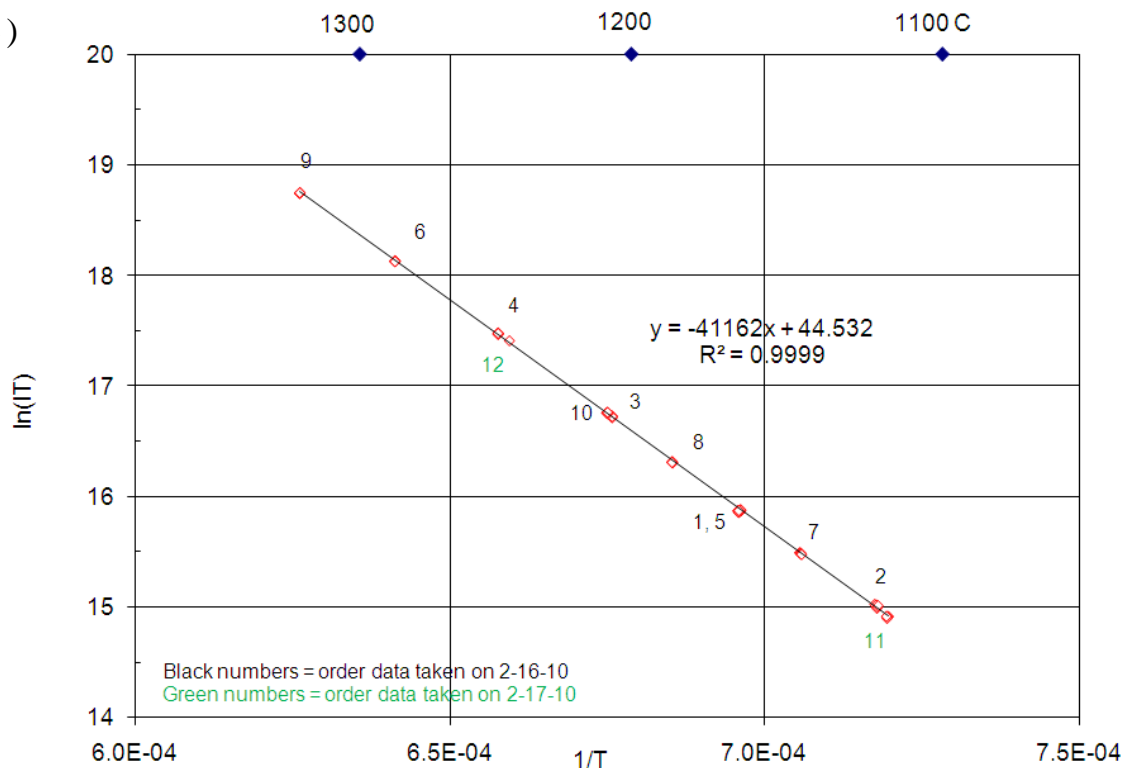
Mass Spectrometer
$$P_M = \frac{kIT}{\sigma}$$

P_M = partial pressure of M;

k = instrument constant; I = ion intensity;

T = Absolute temperature;

σ = ionization cross section





Proceed to Oxide Solutions

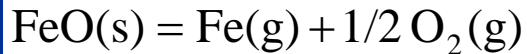
- Partial pressures \leftrightarrow activities
- Complex vaporization and ionization behavior
 - $\text{SiO}_2(\text{s}) = \text{SiO}_2(\text{g})$
 - $\text{SiO}_2(\text{g}) + \text{e}^- \rightarrow \text{SiO}_2^+ + 2\text{e}^-$
 $\rightarrow \text{SiO}^+ + \text{O} + 2\text{e}^-$
 - $\text{SiO}_2(\text{s}) = \text{SiO}(\text{g}) + \frac{1}{2} \text{O}_2(\text{g})$
 - $\text{SiO}(\text{g}) + \text{e}^- \rightarrow \text{SiO}^+ + 2\text{e}^-$
 $\rightarrow \text{Si}^+ + \text{O} + 2\text{e}^-$
- Calculation of cross sections for molecules
- Vaporization may be kinetically limited
- Container Issues
 - Need inert container or container with known interactions: Mo, W, Pt, Ir
 - Silicates are very reactive!



Solutions: Measure Partial Thermodynamic Quantities

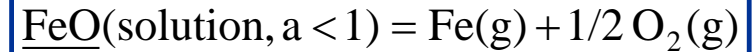
Olivine: $\text{FeO}_{1-\alpha}(\text{MgO})_{1-\beta}(\text{SiO}_2)_{1-\gamma}$
 Same Phase; Variable Stoichiometry

Pure Compound :



$$K_p = \frac{P_{\text{Fe}}^o [P_{\text{O}_2}^o]^{1/2}}{a_{\text{FeO}}} = \frac{P_{\text{Fe}}^o [P_{\text{O}_2}^o]^{1/2}}{1}$$

Solution :



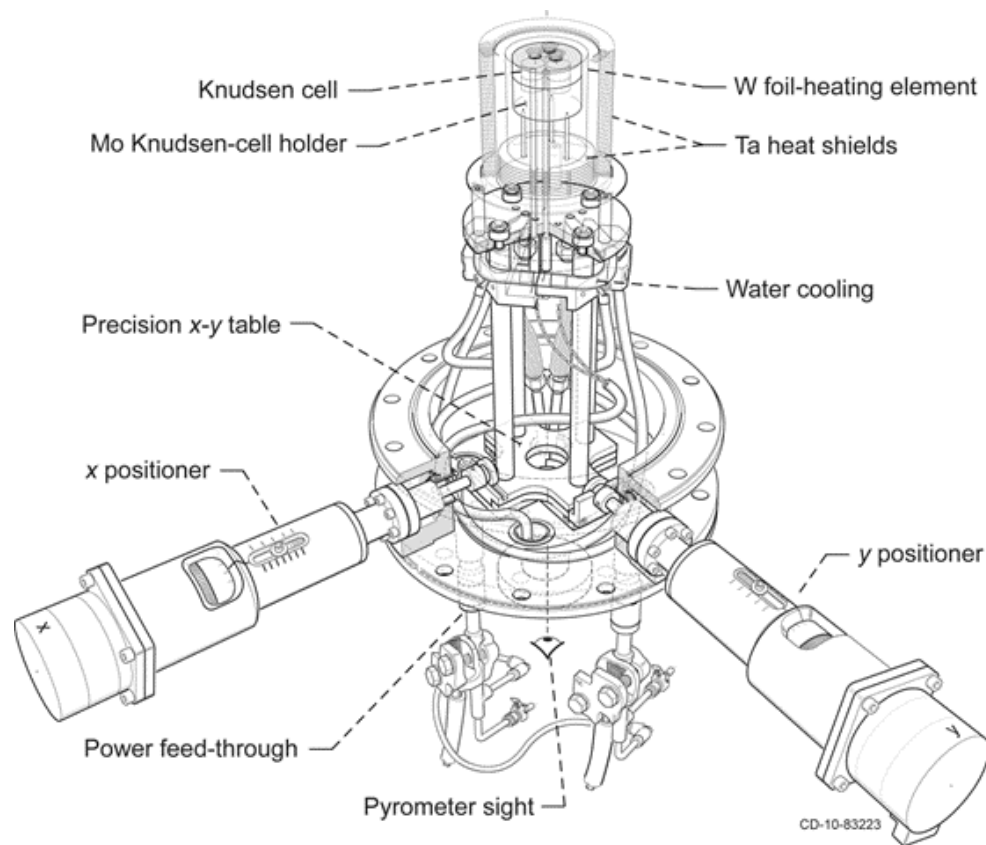
$$K_p = \frac{P_{\text{Fe}} [P_{\text{O}_2}]^{1/2}}{a_{\text{FeO}}}$$

$$a_{\text{FeO}} = \frac{P_{\text{Fe}} [P_{\text{O}_2}]^{1/2}}{P_{\text{Fe}}^o [P_{\text{O}_2}^o]^{1/2}}$$

$\ln(a_{\text{FeO}})$ vs $1/T$ – –partial molar enthalpy

Procedure

- Ion intensity measurements of relevant species for:
 1. Pure compound
 2. Solution
- Best to have *in-situ* pure compound and solution



- BUT, for the highest temperature ($>2000\text{K}$), need to use one cell and change specimens. Assume constant calibration factor.



Example I—Natural Systems: Olivine

- Mg_2SiO_4 (Forsterite)- Fe_2SiO_4 (Fayalite)
- Primary Constituent of Earth's Mantle
- Sources:
 - Pure form found on Hawaii Green Sand Beaches: Volcanic pipeline to Mantle
 - Mining debris



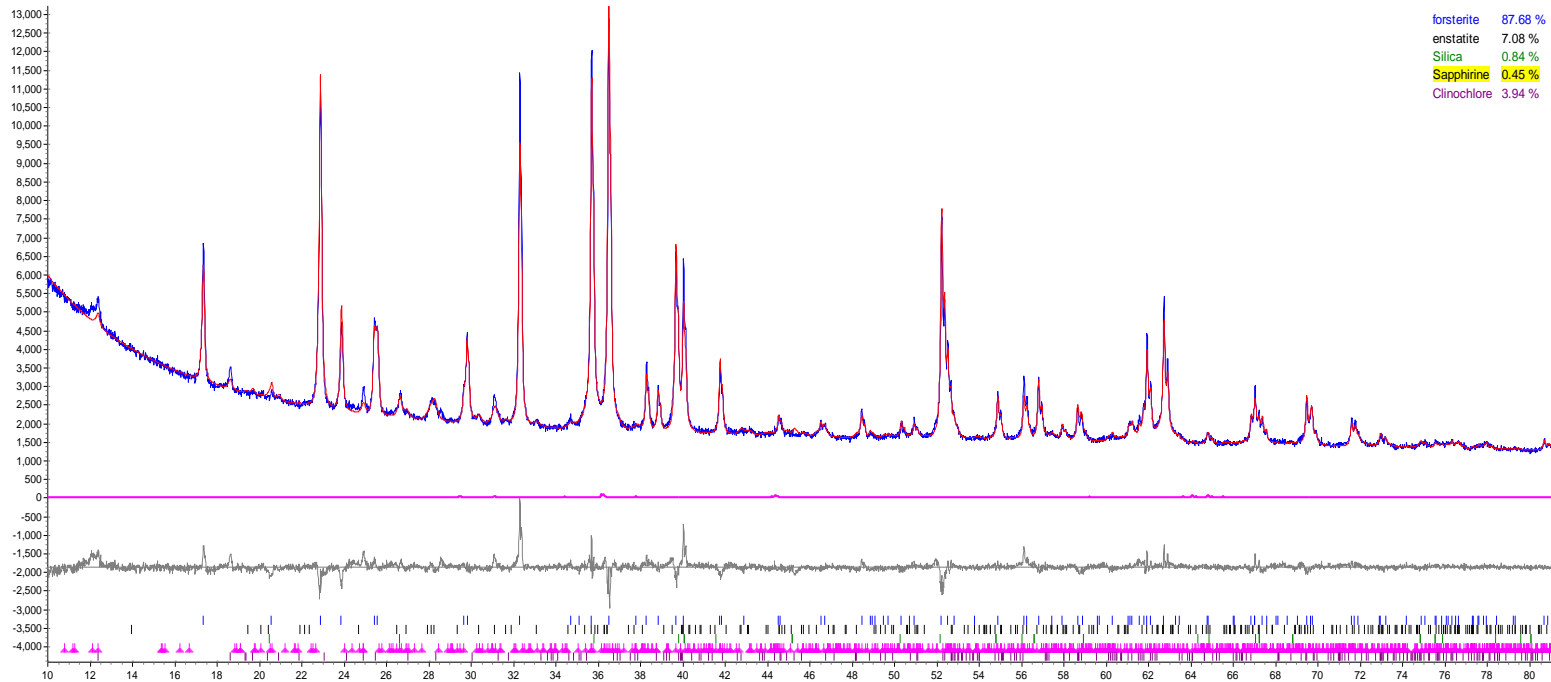
- Important in volcanism, meteorites, likely constituent of other planetary bodies
- Very reactive, particularly above melting. Use Ir cell.



Olivine – Starting Material and Characterization

93% forsterite and 7% fayalite, $\text{Fo}_{93}\text{Fa}_7 - (\text{Fe}_{0.07}\text{Mg}_{0.93})_2\text{SiO}_4$

ICP-OES analysis of the as received olivine samples.



Element	*Wt (%)
Al	0.0120(6)
Ca	0.035(2)
Co	0.0120(6)
Cr	0.052(3)
Fe	5.01(3)
Mg	30(2)
Mn	0.075(4)
Na	0.0080(4)
Ni	0.27(1)
Sc	0.0040(2)
Si	20(1)

*Uncertainties of the analyses are given in parentheses.

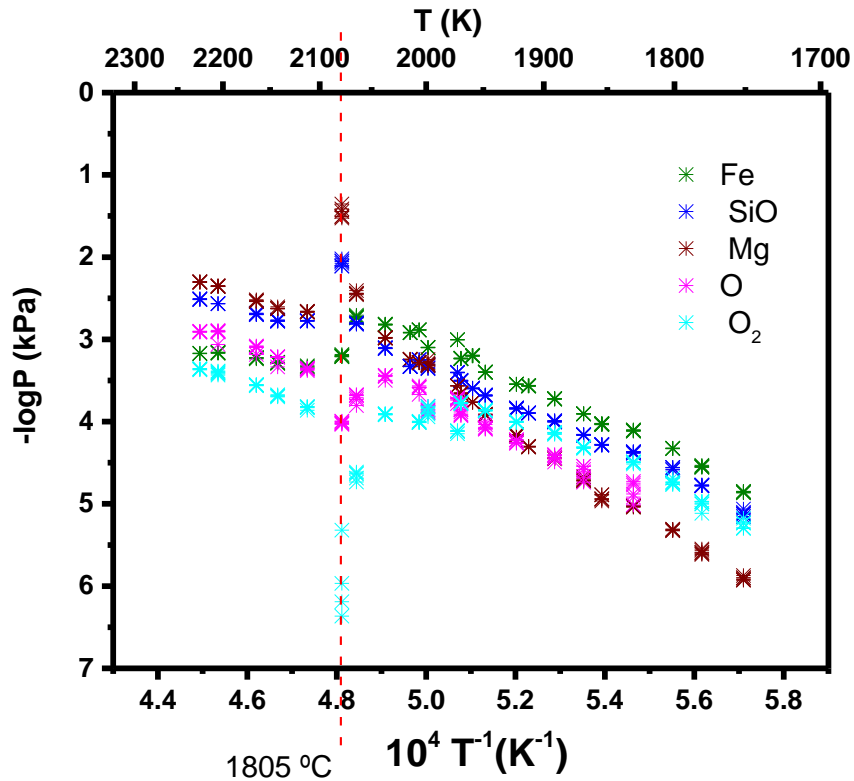
XRD pattern and Rietveld refinement of the as received olivine samples.

Phase content

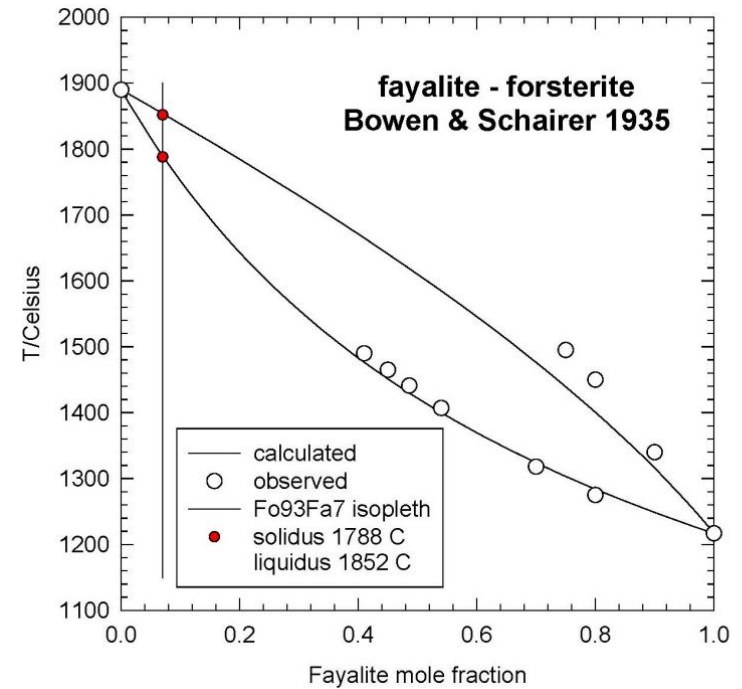
- Forsterite – $87.7 \pm 0.3\%$
- Enstatite – $7.1 \pm 0.2\%$
- Silica – $0.84 \pm 0.6\%$
- Sapphirine – $0.5 \pm 0.1\%$
- Clinocllore – $3.9 \pm 0.2\%$

Heating to $> 1060^\circ\text{C}$
removes impurities

Complete van't Hoff Plot



Temperature dependence of ion intensity ratios of Mg^+ , Fe^+ , SiO^+ , O^+ and O_2^+ in the olivine sample.



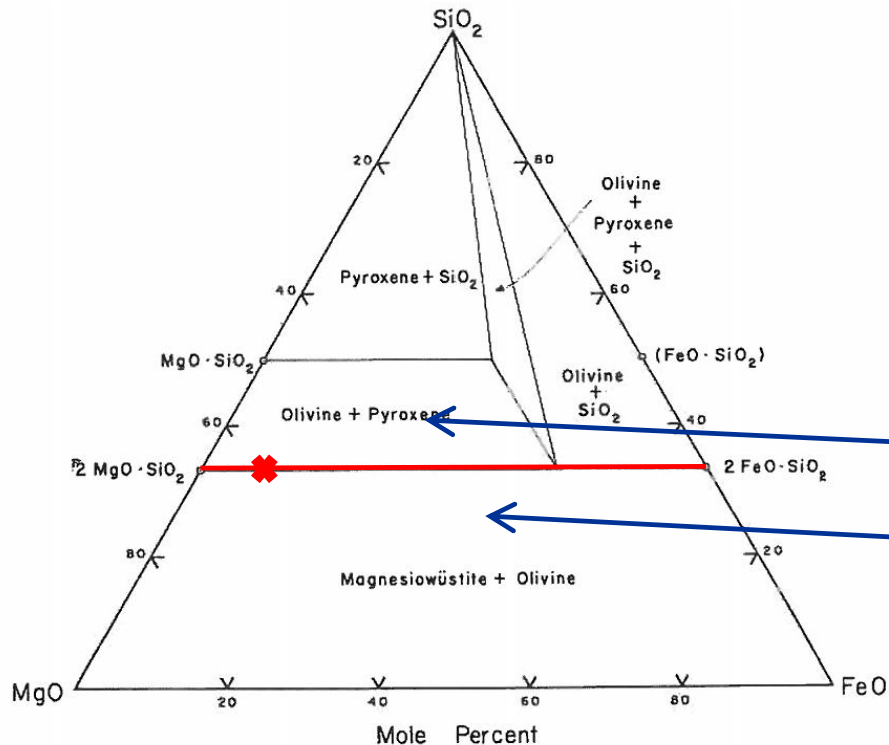
Fegley and Osborne, [Practical Chemical Thermodynamics For Geoscientists](#), Elsevier 2013, Fig. 12-11.

Measurements show good agreement with the phase diagram calculated by Bowen and Schairer.

Bowen and Schairer, *Am. J. Sci.* 29, 151-171 (1935).



Olivine—Solution of Mg₂SiO₄ (Fosterite)-Fe₂SiO₄ (Fayalite)



- Composition of Interest: $\text{Fo}_{0.93}\text{Fa}_{0.07}$
- Activity gradient across olivine
- Work in two phase regions
- Excess SiO₂: Olivine + Pyroxene
- Excess MgO: Olivine + Magnesiowüstite

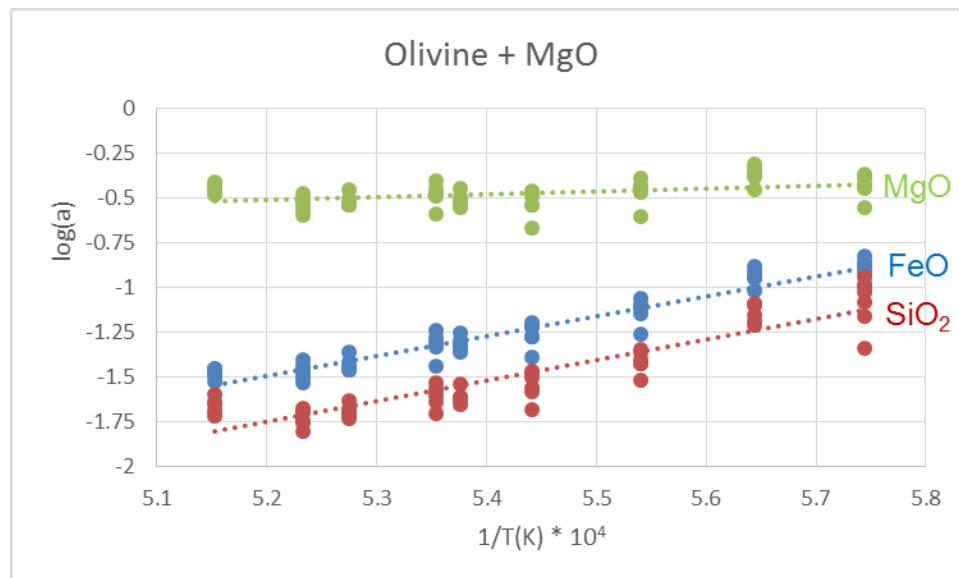


Previous Data and Models of Olivine

- Thermodynamic measurements
 - Nafziger & Muan (1967); Kitayama & Katsura (1968)—from $P(\text{O}_2)$ and stable phases
 - Sakawa et al. (1976): Equilibration method for $a(\text{FeO})$
 - Plante et al. (1992): KEMS measurements of $a(\text{FeO})$
 - Wood & Kleppa, Kojitani & Akaogi: Calorimetry
 - General agreement: $a(\text{FeO})$: Positive deviation from ideality
- Saxena et al. (1993): $(\text{Mg,Fe})_2\text{SiO}_4$ Regular Solution $L_0 = 9000$
- Decker et al.: Sublattice
- Fabrichnaya (1998): $(\text{Mg,Fe})_2\text{SiO}_4$ β and γ spinel; subregular solution with temperature dependent mixing parameters



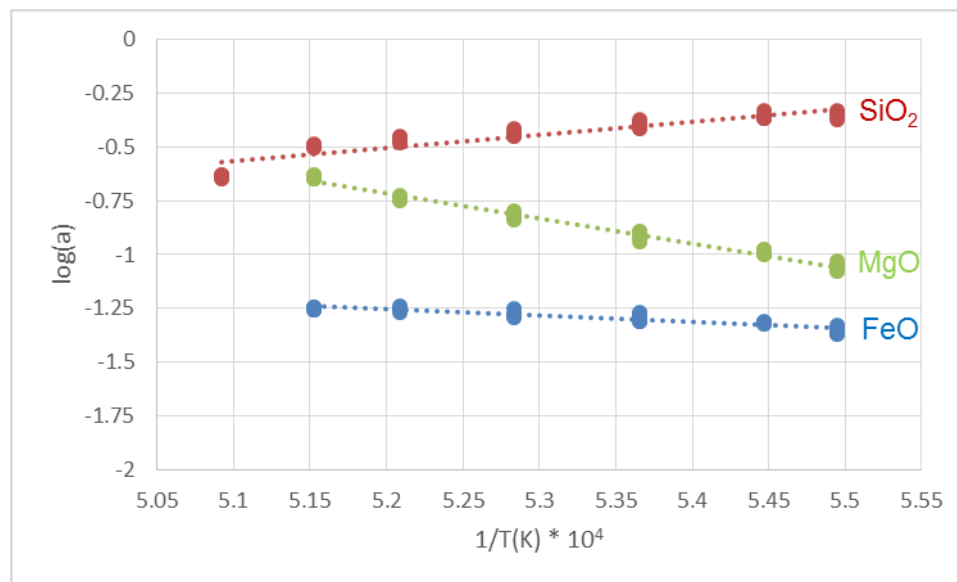
Thermodynamic Activities in Olivine – $(\text{Fe}_2\text{SiO}_4)_{0.07}(\text{Mg}_2\text{SiO}_4)_{0.93} + \text{MgO}$



Component	x	a (1800K)	Compare to Ideality	$\overline{\Delta H}_i(1700-1950)$	
MgO	0.62	0.353	(-)ve deviations	30.2 kJ/mol	
“FeO”	0.047	0.081	(+)ve deviations	212.5 kJ/mol	Consistent with literature
SiO ₂	0.33	0.046	(-)ve deviations	220.2 kJ/mol	



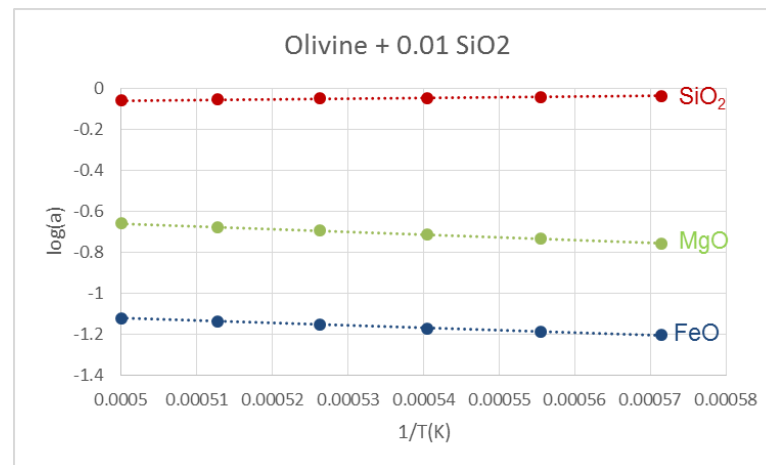
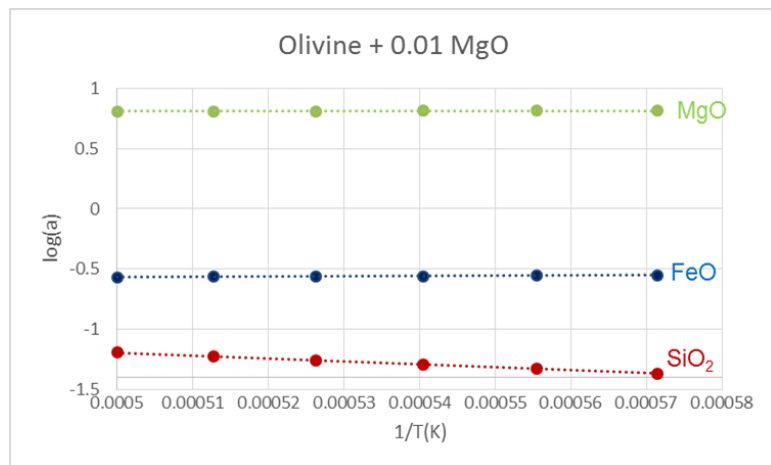
Thermodynamic Activities in Olivine – $(\text{Fe}_2\text{SiO}_4)_{0.07}(\text{Mg}_2\text{SiO}_4)_{0.93}$



Component	x	a (1900K)	Compare to ideality	$\overline{\Delta H}_i(1700-1950)$	
MgO	0.62	0.165	(-)ve deviation	-222.0 kJ/mol	
“FeO”	0.047	0.053	(+)ve deviation	-55.2 kJ/mol	Consistent with literature
SiO ₂	0.333	0.341	(+)ve deviation	116.2 kJ/mol	



Comparison to Models (FactSage)





Thermodynamics of Olivine: Lots to Do!

- Understand changes in activities on melting
- Compare partial molar enthalpies to total excess free energy
- Refine current models: our data suggests some components far from ideality

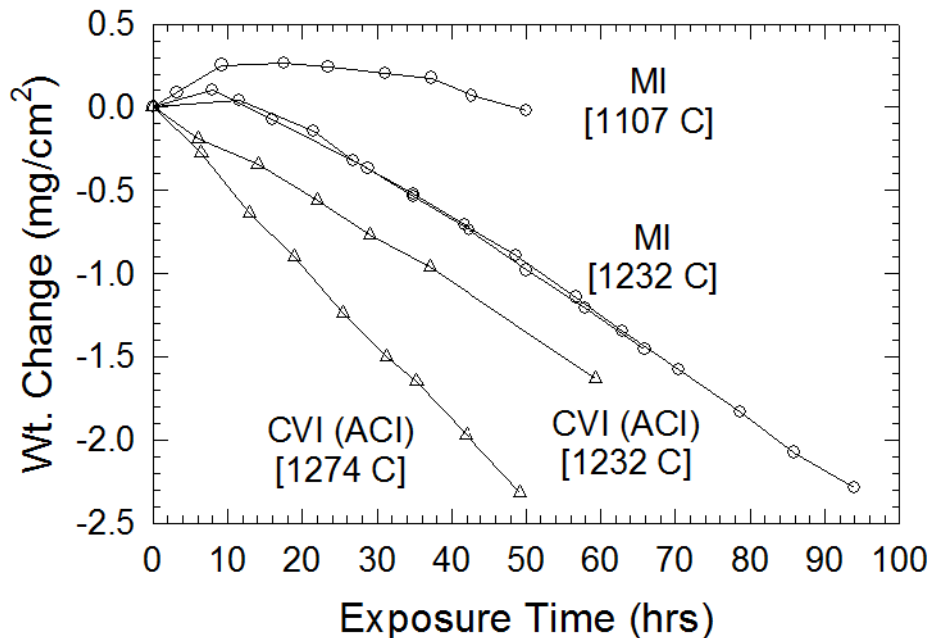
Example 2: Rare Earth Silicates





SiC and SiC based Composites for Heat Engines

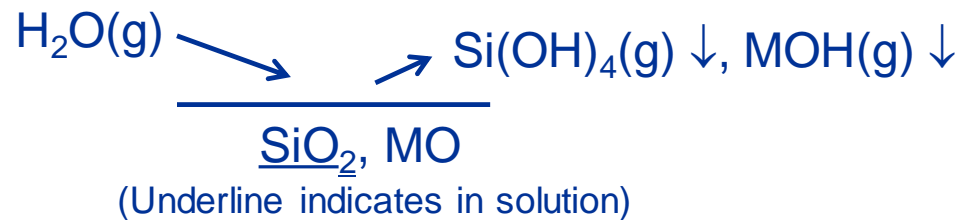
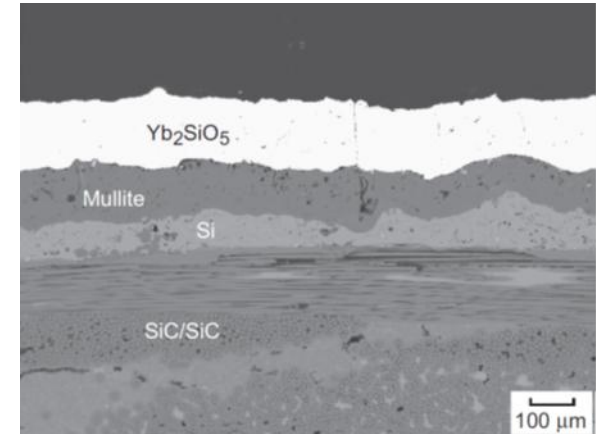
- Strength retained to higher temperatures than metals
- Lighter weight
- Fiber Reinforced composites give some fracture toughness
- Protected by SiO₂ scale
 - Slow growing, good in pure oxygen
 - BUT...Attacked by basic molten salts; volatilized by water



SiC/SiC CMC HPBR Paralinear
 (1100 °-1300°C, 6 atm; Robinson/Smialek 1998)
 Si(OH)₄ volatility (Opila et al., 1998-2006)

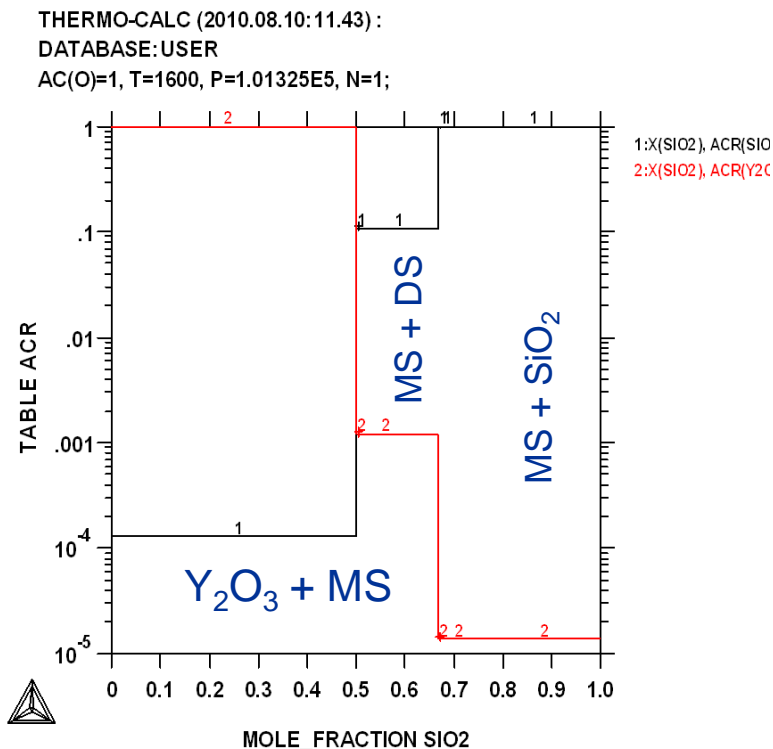
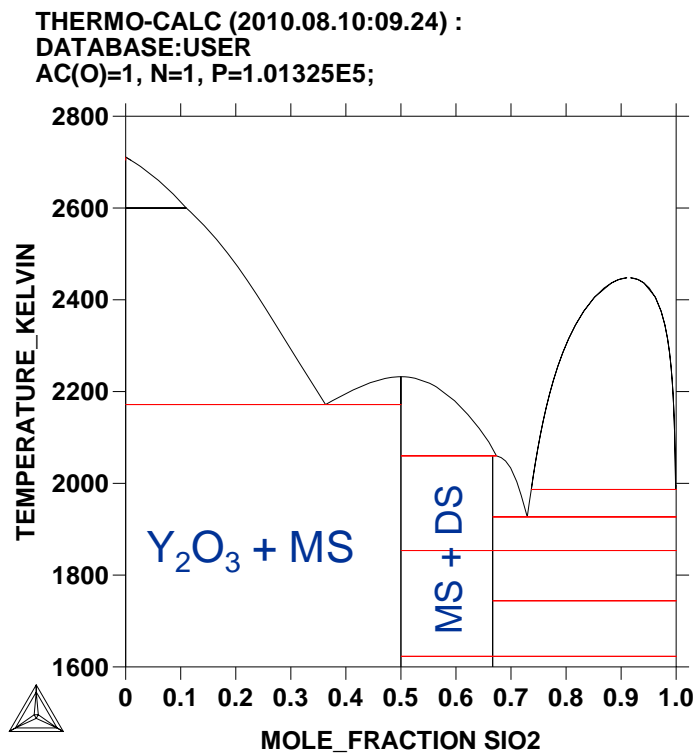
Combine *Desirable Mechanical Properties of SiC* with *Chemical Inertness of Refractory Oxide*

- Lower activity of silica \Rightarrow less reaction
- Molten salt reaction
 - $\text{Na}_2\text{O}(\text{s}) + \text{SiO}_2(\text{s}) = \text{Na}_2\text{O} \cdot x\text{SiO}_2$
- Water vapor enhanced volatilization
 - $\text{SiC} + 3/2 \text{O}_2(\text{g}) = \text{SiO}_2 + \text{CO}(\text{g})$
 - $\underline{\text{SiO}_2} + 2 \text{H}_2\text{O}(\text{g}) = \text{Si}(\text{OH})_4(\text{g})$
 - $P[\text{Si}(\text{OH})_4] = K a(\text{SiO}_2) [P(\text{H}_2\text{O})]^2$



Rare Earth Silicates: Good CTE Match to SiC

Calculated Y_2O_3 - SiO_2 Phase Diagram



Indirect evidence suggests that the SiO_2 thermodynamic activity is lower in the Y_2O_3 - Y_2SiO_5 and Y_2SiO_5 - $Y_2Si_2O_7$ regions
But there are no direct measurements!



Issues with Measuring $a(\text{SiO}_2)$ in RE Silicates

- Vapor pressure of SiO_2 too low to measure in temperature range of interest
- Need measurable signal for SiO_2 —use reducing agent to make excess $\text{SiO}(\text{g})$. Tried several, selected Mo or Ta
 - For $a(\text{SiO}_2) > \sim 0.02$
 - $\text{Mo}(\text{s}) + 3\underline{\text{SiO}_2}(\text{soln}) = 3\text{SiO}(\text{g}) + \text{MoO}_3(\text{g})$
 - For $a(\text{SiO}_2) < \sim 0.02$
 - $2\text{Ta}(\text{s}) + 2\underline{\text{SiO}_2}(\text{soln}) = 2\text{SiO}(\text{g}) + \text{TaO}(\text{g}) + \text{TaO}_2(\text{g})$
 - Note reducing agent must not change solid phase composition
 - Monosilicates + disilicates + Ta – leads to tantalates
- Need to account for non-equilibrium vaporization
- SiO overlaps with CO_2 ($m/e = 44$)
 - Use LN_2 cold finger for improved pumping
 - Shutter to distinguish vapor from cell and background
 - High resolution instrument (in our dreams...)
 - Gettering pump for CO_2

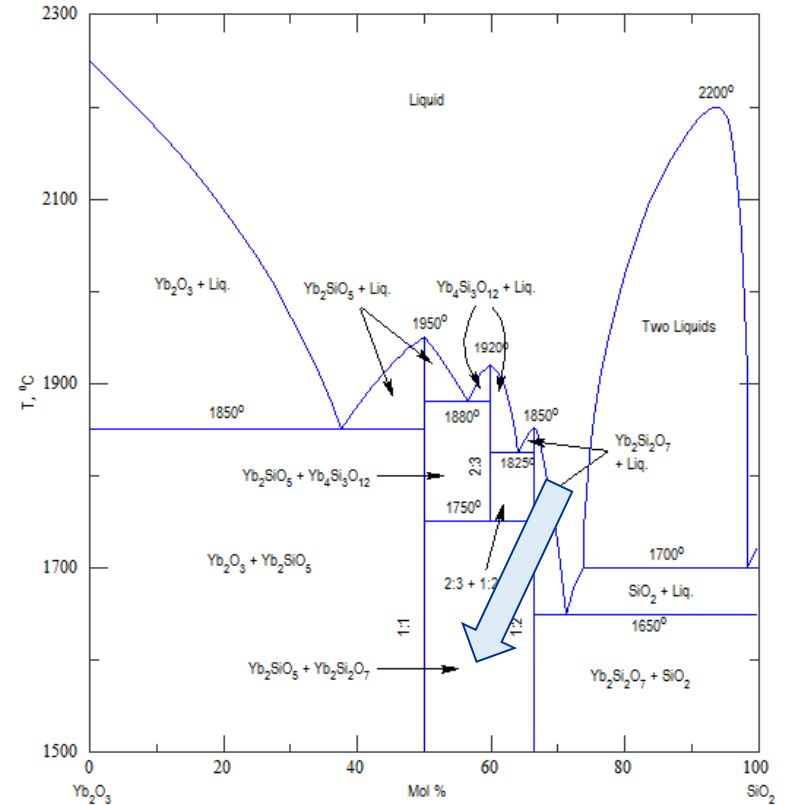
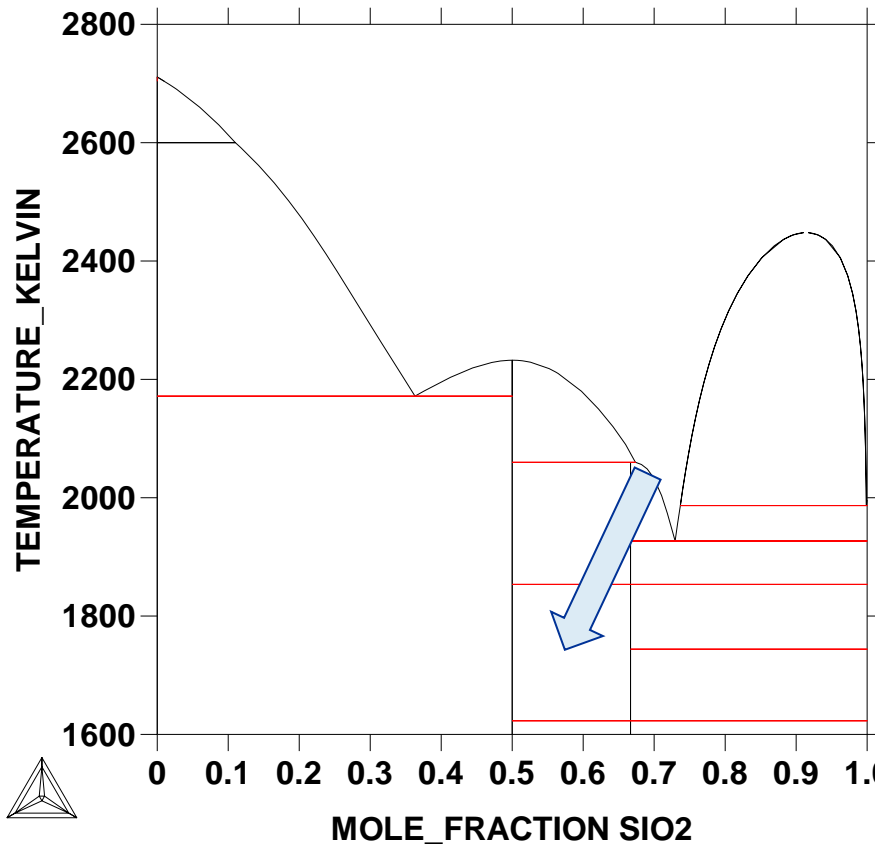
Monosilicate + Disilicate



THERMO-CALC (2010.08.10:09.24) :

DATABASE:USER

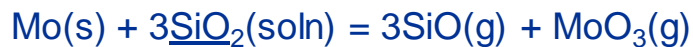
AC(O)=1, N=1, P=1.01325E5;



Work in Two Phase Region: Monosilicate + Disilicate

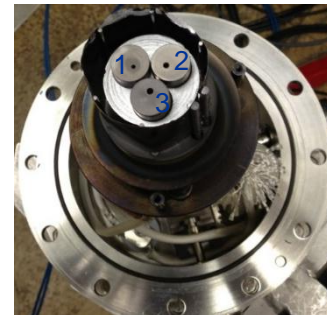
Three cells:

- Au (reference)
- $3\text{Mo} + \text{Y}_2\text{O}_3 \cdot 2\text{SiO}_2 + \text{Y}_2\text{O}_3 \cdot \text{SiO}_2$
- $3\text{Mo} + \text{SiO}_2$
- Mo as powder and cell material

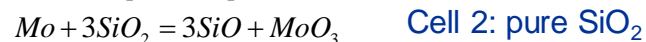


- Compare cells 1 and 2

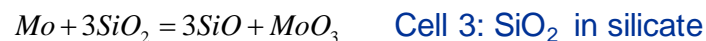
Note that cell is part of the thermodynamic system: Best way to overcome container issue!



$$K = \frac{[P(\text{SiO})]^3 P(\text{MoO}_3)}{[a(\text{SiO}_2)]^3}$$

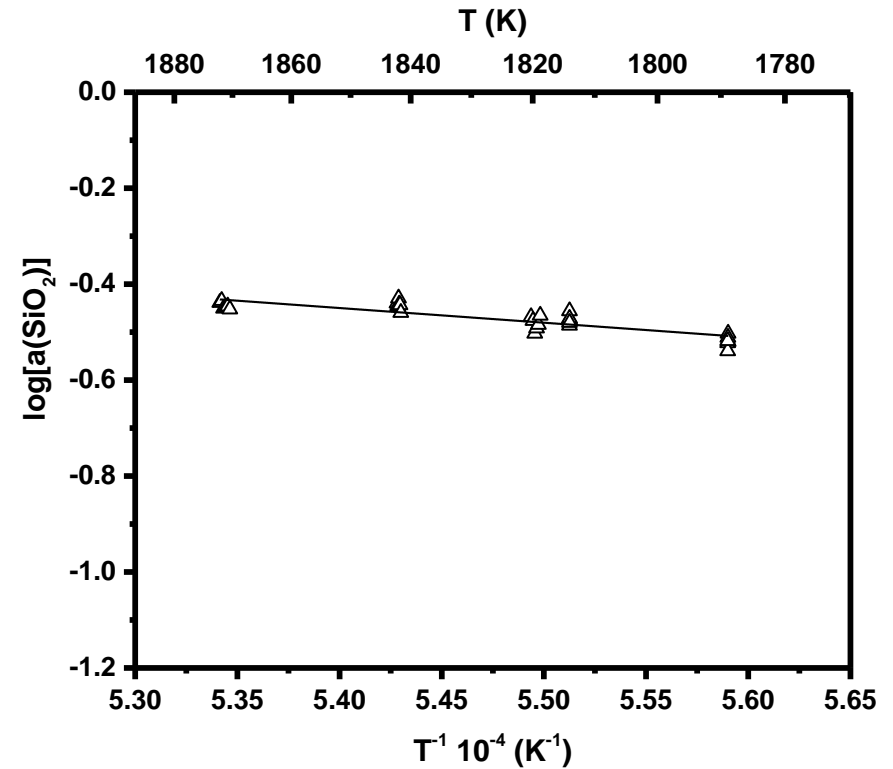
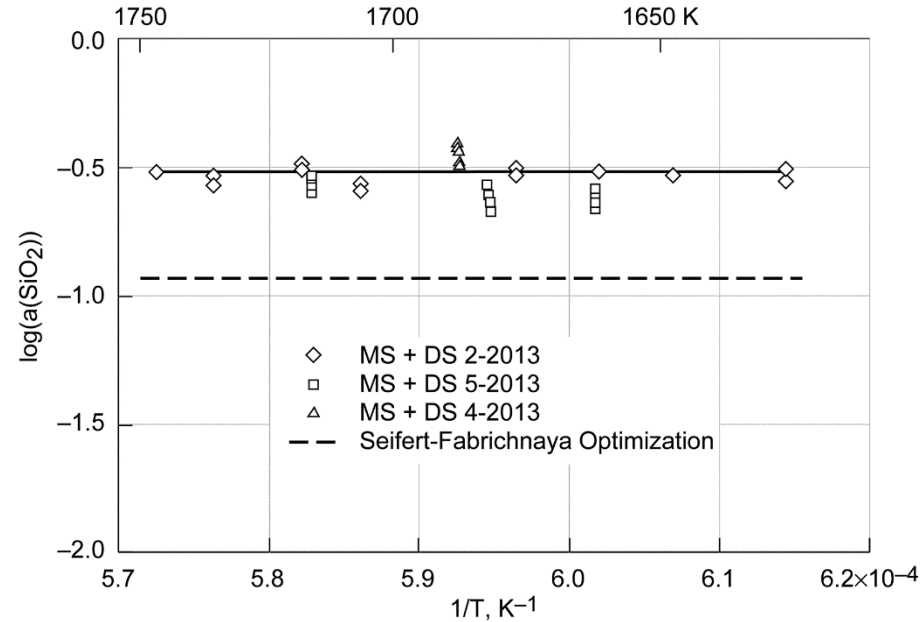


$$a(\text{SiO}_2) = 1 = \left\{ \frac{[P^\circ(\text{SiO})]^3 P^\circ(\text{MoO}_3)}{K} \right\}^{0.33}$$



$$a(\text{SiO}_2) = \left\{ \frac{[P(\text{SiO})]^3 P(\text{MoO}_3)}{K} \right\}^{0.33}$$

$$a(\text{SiO}_2) = \left\{ \frac{[I(\text{SiO})]^3 I(\text{MoO}_3)}{[I^\circ(\text{SiO})]^3 I^\circ(\text{MoO}_3)} \right\}^{0.33}$$

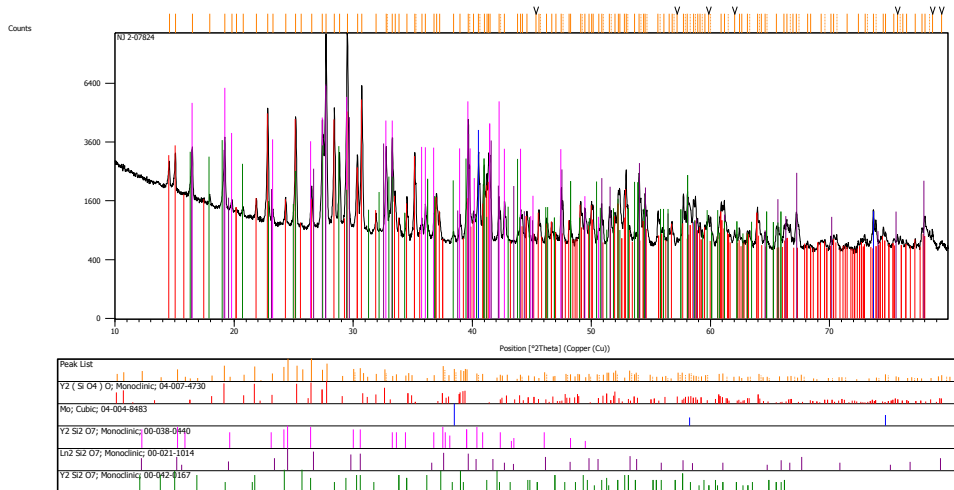


Two Phase Mixture	$a(SiO_2)$, 1650K
$Y_2O_3 \cdot (SiO_2) + Y_2O_3 \cdot 2(SiO_2)$	0.281
$Y_2O_3 \cdot (SiO_2) + Y_2O_3 \cdot 2(SiO_2)$	0.194

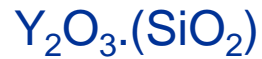


XRD after KEMS Measurements of RE Monosilicates + Disilicates + Mo:

Yttrium monosilicate + disilicate + Mo

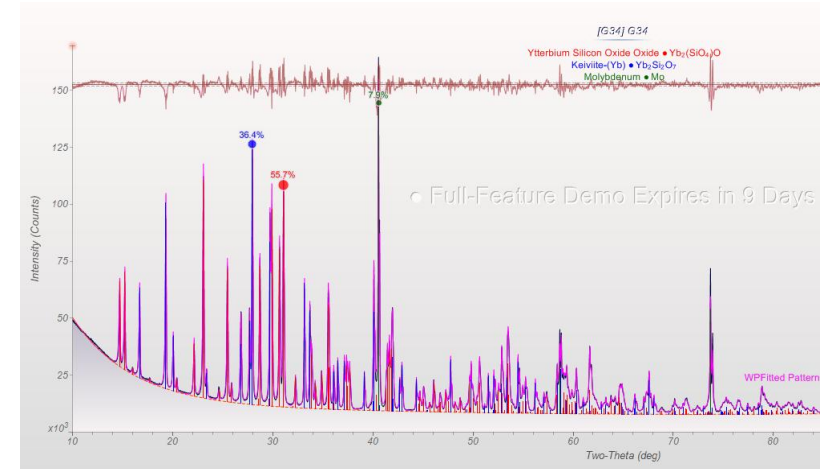


Phase

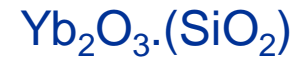


Mo

Ytterbium monosilicate + disilicate + Mo



Phase



Mo

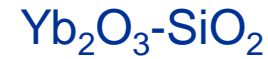
wt (%)

56

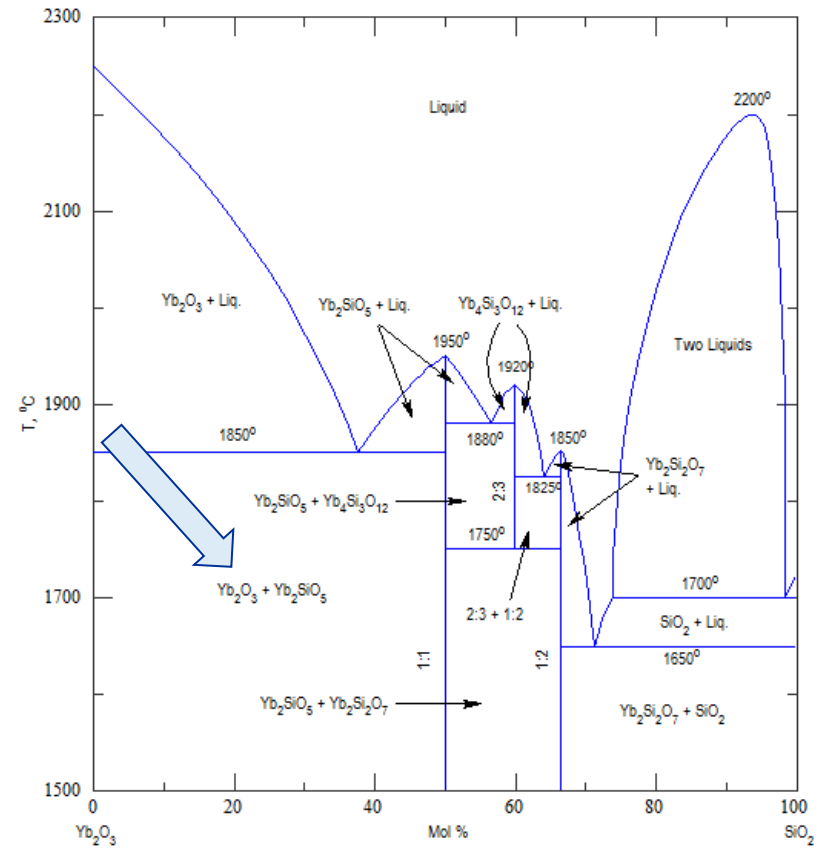
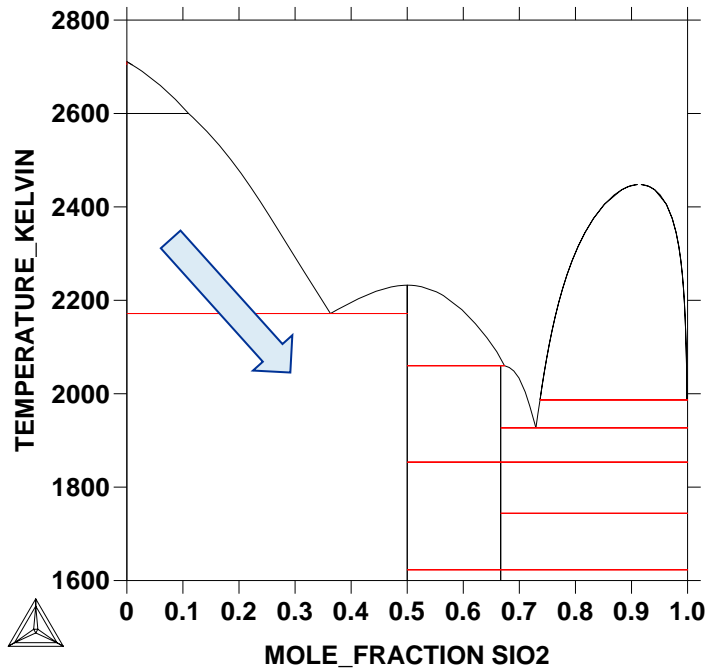
36

8

Monosilicate + RE₂O₃



THERMO-CALC (2010.08.10:09.24) :
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 AC(O)=1, N=1, P=1.01325E5;



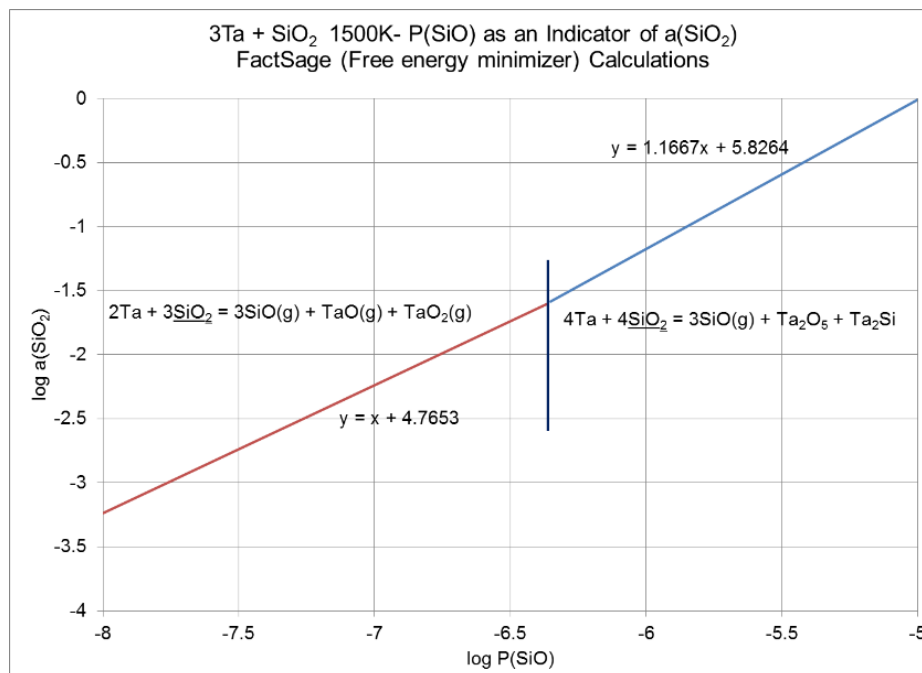
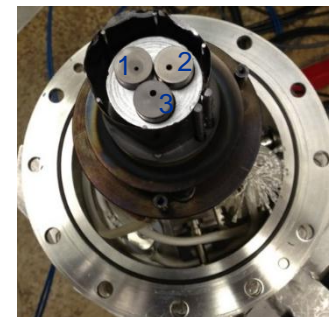
Monosilicate + RE₂O₃

Two cells:

- Au
- $3\text{Ta} + \text{Y}_2\text{O}_3 + \text{Y}_2\text{O}_3 \cdot \text{SiO}_2$
 - Ta as powder and cell material—cell is part of system



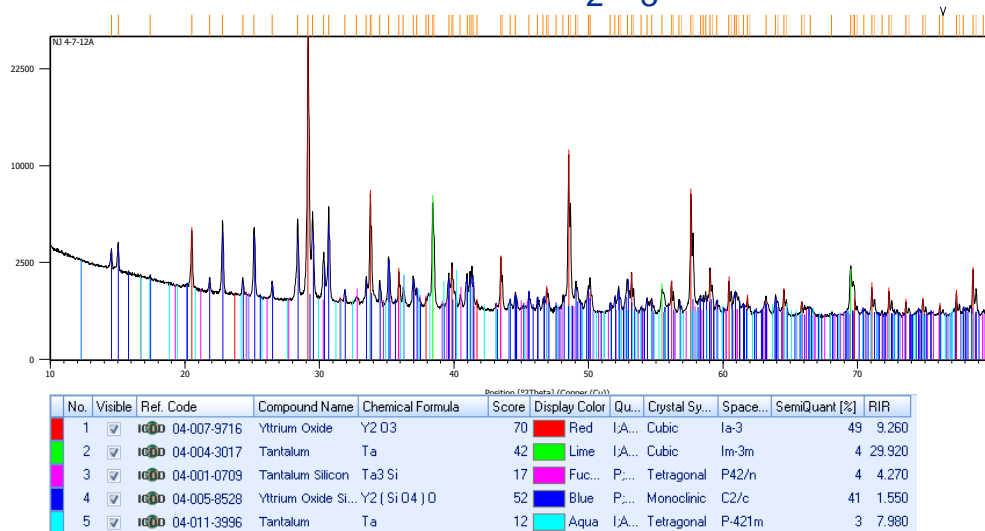
- Using $P_{\text{eq}}(\text{SiO})$ and FactSage (free energy minimization)
- Correction for non-equilibrium vaporization





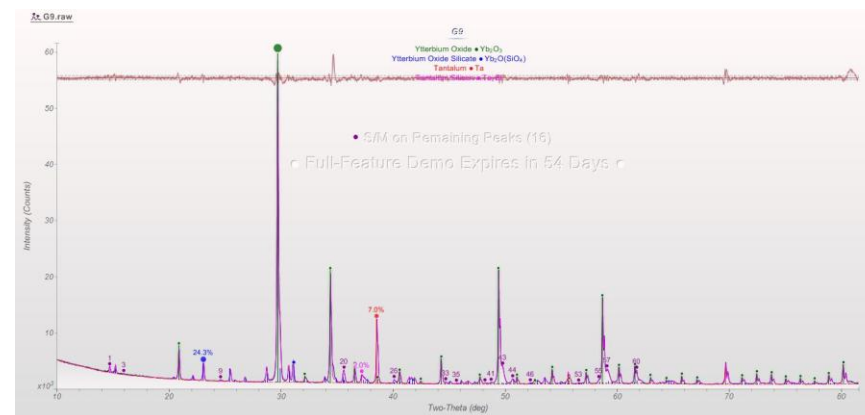
XRD after KEMS Measurements of RE Monosilicates + RE₂O₃ + Ta:

Yttrium monosilicate + Y₂O₃ + Ta

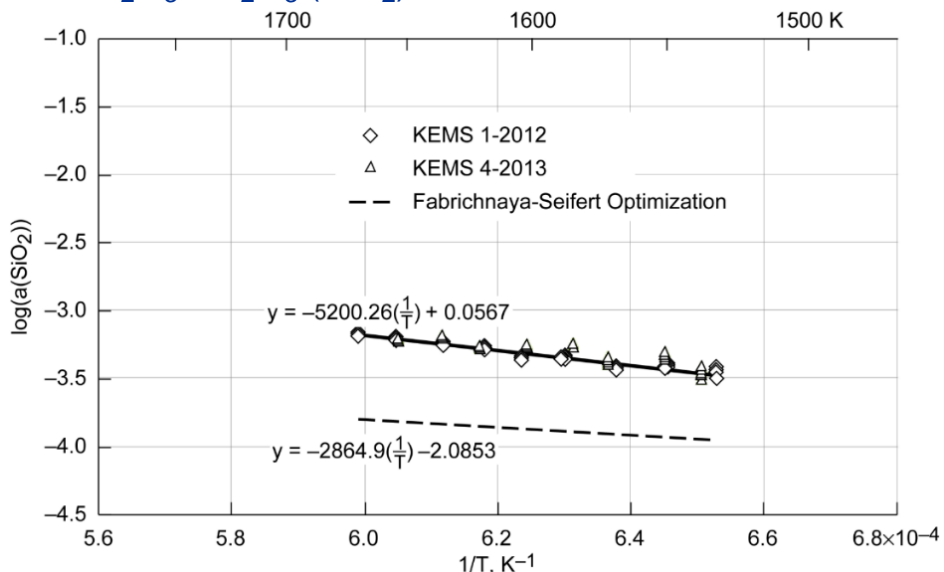


Phase	wt (%)
Y ₂ O ₃ ·(SiO ₂)	41
Y ₂ O ₃	49
Ta	4
Ta ₃ Si	4

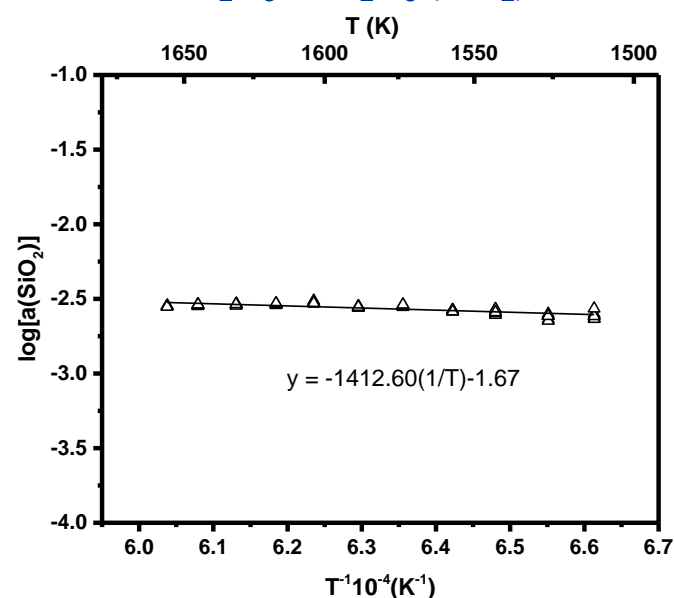
Ytterbium monosilicate + Yb₂O₃ + Ta



Phase	wt (%)
Yb ₂ O ₃ ·(SiO ₂)	24
Yb ₂ O ₃	66
Ta	2
Ta ₂ Si	2



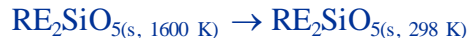
$$\Delta H_{(SiO_2, 1600 K)} = (5200.26) \cdot R \cdot 2.303 = 99.57 \text{ kJ/mol}$$



$$\Delta H_{(SiO_2, 1600 K)} = (1412.60) \cdot R \cdot 2.303 = 27.05 \text{ kJ/mol}$$



$\Delta H_1 =$ measured in this work



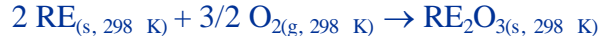
$$\Delta H_2 = H_{1600 K} - H_{298 K}$$



$$\Delta H_3$$



$$\Delta H_4$$



$$\Delta H_5$$



$$\Delta H_6$$



$$\Delta H_7 = \Delta H_{f, RE_2SiO_5, 298 K}$$

$\Delta H_{f, RE \text{ silicate}, 298 K}$ (kJ/mol)

	KEMS	Calorimetry*
$Y_2O_3 \cdot (SiO_2)$	-2907 ± 16	-2868.54 ± 5.34
$Yb_2O_3 \cdot (SiO_2)$	-2744 ± 11	-2774.75 ± 16.48

$a(SiO_2), 1650 K$

0.000804

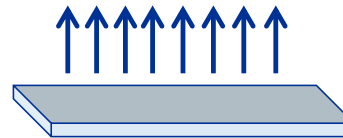
0.00298

*Liang et al. "Enthalpy of formation of rare-earth silicates Y_2SiO_5 and Yb_2SiO_5 and N-containing silicate $Y_{10}(SiO_4)_6N_2$ ", J. Mater. Res. 14 [4], 1181-1185. **J. A. Duff, J. Phys. Chem. A 110, 13245 (2006)

Vaporization Coefficients

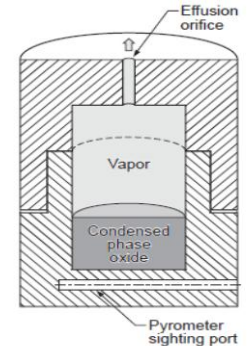
- Vapor Flux (mole/unit area-unit time) leaving a free surface into a vacuum:
Described by Hertz-Knudsen-Langmuir (HKL) equation

$$J(\text{max}) = \frac{P_{eq}}{\sqrt{2\pi MRT}}$$



- Measured flux--Modified by a factor α : Vaporization Coefficient

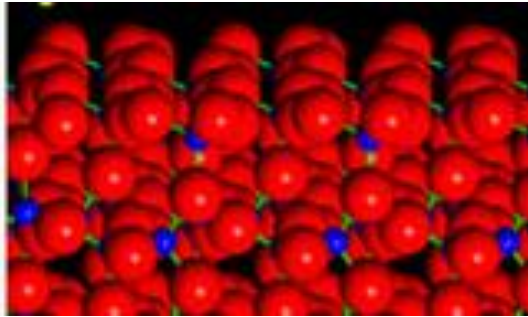
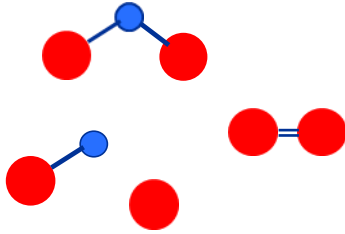
$$J(\text{measured}) = \frac{\alpha P_{eq}}{\sqrt{2\pi MRT}}$$



- Metals: Generally unity; Oxides 10^{-1} to 10^{-5} !
- Free surface vaporization = Langmuir vaporization
- Important parameter—relatively little expt'l or theoretical work since 1970s
 - True vapor flux in a deposition processes
 - High temperature material vaporization limit
 - True vapor flux in a geochemical/cosmochemical processes



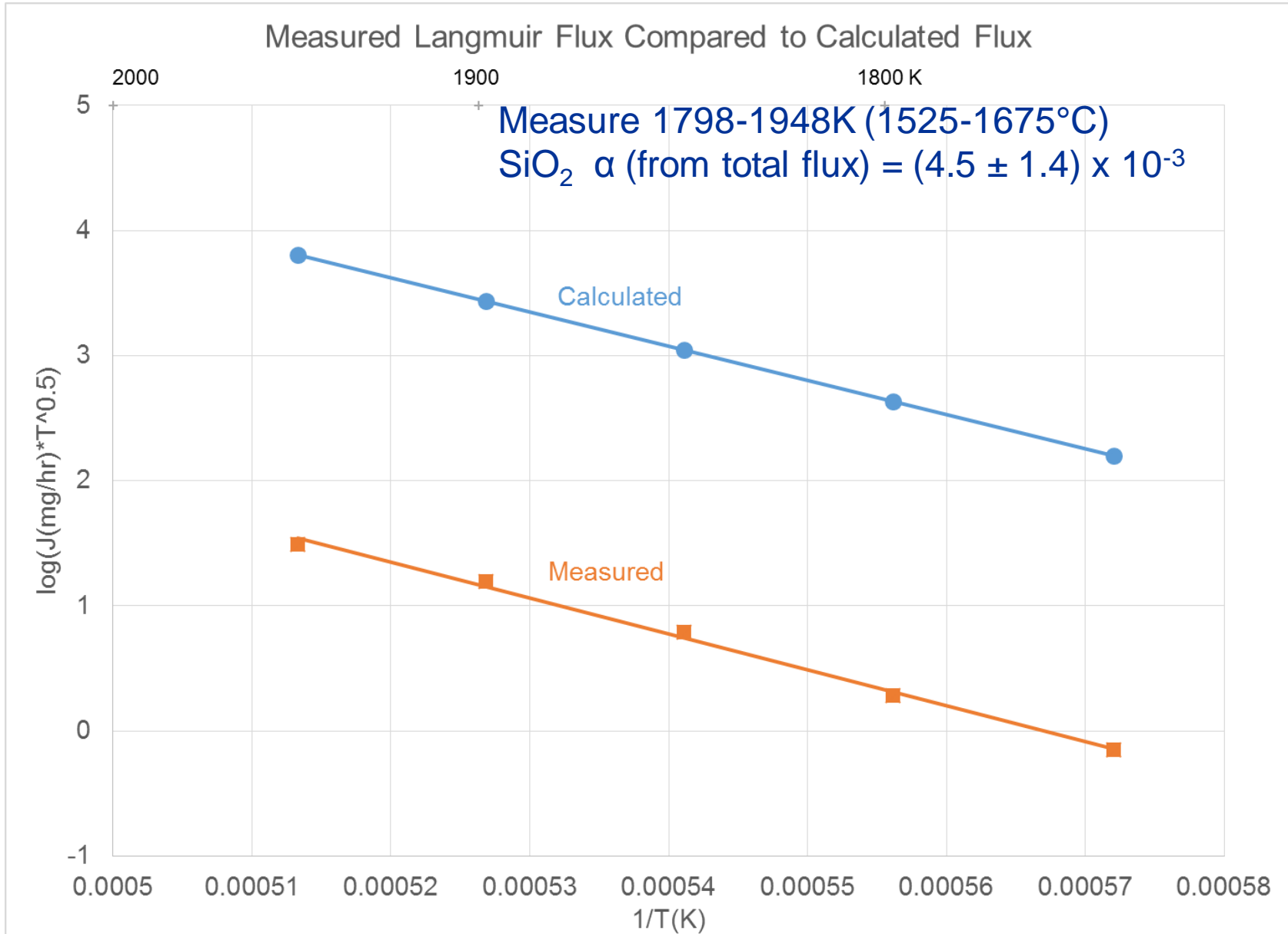
What Leads to non-unity Vaporization Coefficients?



- Vaporization of silica
 - $\text{SiO}_2(\text{s}) = \text{SiO}_2(\text{g})$
 - $\text{SiO}_2(\text{s}) = \text{SiO}(\text{g}) + \frac{1}{2} \text{O}_2(\text{g})$
 - $\text{SiO}_2(\text{s}) = \text{SiO}(\text{g}) + \text{O}(\text{g})$

- Complex process
 - Break apart SiO_4^{-2}
 - Adsorbed $\text{SiO}_2(\text{a})$, $\text{SiO}(\text{a})$, $\text{O}_2(\text{a})$, $\text{O}(\text{a})$
 - Desorption to $\text{SiO}_2(\text{g})$, $\text{SiO}(\text{g})$, $\text{O}_2(\text{g})$, $\text{O}(\text{g})$
 - Break O-O, Si-O bonds; make O=O double bond

- Expect a kinetic barrier \Rightarrow flux reduced from equilibrium





Importance of Vaporization Coefficient

- Calculate vapor pressures above a condensed phase oxide:
 - Modify by vaporization coefficient
- Thermodynamic measurements
 - Implicitly assume that $\alpha(A(g), \text{solution}) = \alpha(A(g), \text{pure component})$
 - A(g)—particular species
- Measurements of these until 1970s, then relatively little work
- Important parameter has major effect on vapor pressures



Summary

- Knudsen Effusion Mass Spectrometry
 - Powerful tool for thermodynamic measurements
 - In use for many years; but still very useful particularly for solutions
 - Procedures are system specific
- Example: Olivine
 - Challenge to find 'inert' cell material. Iridium probably the best
 - Treat as solid solution of 'FeO', MgO, SiO₂
 - The melting point of the olivine sample was determined by the ion intensity discontinuity to be 1805 °C
 - Compare to standards and derive thermodynamic activities in solid phase. Appears to be significant partial molar heats, deviations from ideality
- Example: Rare-earth silicates
 - The reduced SiO₂ activity in Rare-earth silicates should limit their reactivity with water vapor
 - Solid State rare earth oxides—activity of SiO₂
 - Need reducing agent to obtain a measurable signal for SiO(g), which in turn relates to activity of SiO₂. Reducing agent must not change solid phase composition.
 - Method and choice of reducing agent depends on particular silicate
- Vaporization Kinetics: Described by vaporization coefficient



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