

Experimental and Theoretical Study of 4H-SiC JFET Threshold Voltage Body Bias Effect from 25 °C to 500 °C

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Abstract. This work reports a theoretical and experimental study of 4H-SiC JFET threshold voltage as a function of substrate body bias, device position on the wafer, and temperature from 25 °C (298K) to 500 °C (773K). Based on these results, an alternative approach to SPICE circuit simulation of body effect for SiC JFETs is proposed.

Introduction

Over the past few years, significant progress has been made in the development of increasingly capable very high-temperature integrated circuits (ICs) that could benefit a variety of aerospace, automotive, and energy production systems. For example, elsewhere at this conference it is reported that a 4H-SiC Junction Field Effect Transistor (JFET) IC with two levels of metal interconnection has demonstrated 500 °C electrical operation in excess of 3000 hours [1]. Increasingly accurate and accessible IC design and simulation tools for such extreme temperatures are clearly relevant to further technology development and application adoption. Towards this end, this work reports a theoretical and experimental comparison study of 4H-SiC JFET threshold voltage (V_T) as a function of substrate body bias (V_S) and temperature (T) from 25 °C (298K) to 500 °C (773K).

Experiment

Fig. 1 schematically depicts the cross-section of the long-channel (gate-length $L_G = 6\mu\text{m}$) 4H-SiC epilayer JFET structure studied. Key structural terms illustrated in Fig. 1 include gate and substrate pn junctions, n-channel epilayer thickness t_c and doping N_{DC} , and sub-channel epilayer doping N_{AS} . Experimental procedures used for device fabrication, pre-dicing wafer probe mapping of JFET V_T , and high temperature packaging and testing are described in [1,2].

Theory. Under one-dimensional depletion approximation [3], the depletion depth x_n on the n-side of a pn step-type junction with built-in voltage V_{bi} under applied pn junction bias V_A is:

$$x_n = \sqrt{\left(\frac{2\epsilon_s}{q}\right) \left(\frac{N_A}{N_D(N_A+N_D)}\right) (V_{bi} - V_A)} = K_n \sqrt{V_{bi} - V_A} \quad (1)$$

N_A and N_D are junction p-type and n-type layer doping densities, ϵ_s is 4H-SiC dielectric constant, q is the electron charge constant, and junction n-side depletion constant K_n defined as:

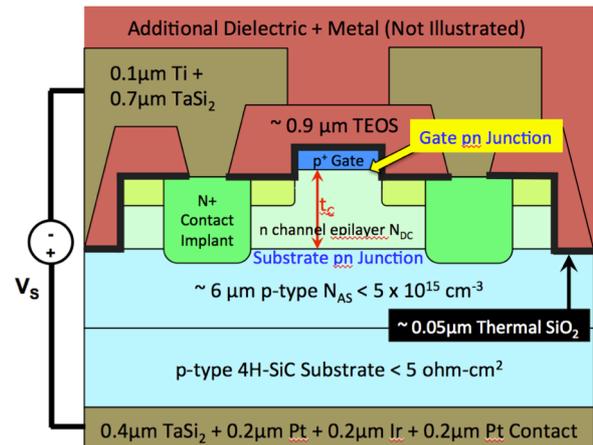


Fig. 1. JFET Cross-sectional diagram.

$$K_n = \sqrt{\left(\frac{2\epsilon_s}{q}\right) \left(\frac{N_A}{N_D(N_A+N_D)}\right)} \quad (2)$$

When the JFET gate bias V_G is at threshold voltage V_T , the gate and substrate pn junction depletion depths extending into the n-channel (x_{nG} and x_{nS}) merge together to effectively remove carriers (electrons) from the entire doped n-channel thickness beneath the p^+ gate. At threshold therefore, the sum of the gate and substrate junction n-side depletions approximates the n-channel thickness t_c :

$$t_c \cong x_{nG} + x_{nS} = K_{nG}\sqrt{(V_{biG} - V_T)} + K_{nS}\sqrt{(V_{biS} - V_S)} \quad (3)$$

where V_S is the applied substrate junction bias. Solving Eq. 3 for V_T :

$$V_T = V_{biG} - \left(\frac{t_c}{K_{nG}}\right)^2 + \left(\frac{2t_c K_{nS}}{K_{nG}^2}\right)\sqrt{V_{biS} - V_S} - \left(\frac{K_{nS}}{K_{nG}}\right)^2 (V_{biS} - V_S) \quad (4)$$

By defining $V_{T0} = V_T$ at $V_S = 0$, Eq. 4 can be re-expressed as:

$$V_T = V_{T0} + \left(\frac{2t_c K_{nS}}{K_{nG}^2}\right)(\sqrt{V_{biS} - V_S} - \sqrt{V_{biS}}) + \left(\frac{K_{nS}}{K_{nG}}\right)^2 V_S \quad (5)$$

Measured Results. Consistent with results from our previous study of a different 4H-SiC JFET IC wafer [2], the magnitude of V_T on this wafer increased proportional to the square of radial distance (r) from the wafer center (Fig. 2, blue). Secondary Ion Mass Spectroscopy (SIMS) analysis was performed (by Evans Analytical Group, www.eag.com) on two diced 3mm x 3mm die taken from differing radial wafer locations with significantly different measured JFET V_T . The Fig. 3 SIMS results indicate that n-epilayer thickness variation is primarily responsible for the wafer position variation of V_T . Given position-invariant $1.0 \times 10^{17} \text{ cm}^{-3}$ n-channel epilayer doping N_{DC} evidenced by Fig. 3 SIMS data, Eq. 3 can extract n-epilayer thickness t_c as a function of r (Fig. 2, red), which like V_T exhibits $y = a*r^2 + b$ general behavior. However, it should be noted that variation in p-type sub-channel doping N_{AS} at/below SIMS aluminum detection floor ($\sim 3 \times 10^{15} \text{ cm}^{-3}$) could slightly affect V_T ($\sim 2 \text{ V}$, as seen in Fig. 4). A JFET diced from a different wafer location was custom-packaged for high temperature oven electrical testing [2].

Comparison with Theory. Fig. 4 plots theoretical V_T vs. V_S curves (lines) calculated via Eq. 4 using both Fig. 3 SIMS profiles assuming three different sub-channel doping densities ($N_{AS} = 1, 2,$ and $3 \times 10^{15} \text{ cm}^{-3}$). Good agreement with V_T experimentally measured on corresponding JFETs (plotted as symbols) is obtained. Fig. 5 compares measured (symbols) and theoretical (lines) V_T at $V_S = 0\text{V}, -15\text{V},$ and -25V from 25°C to 500°C from the high-temperature packaged JFET. The V_T temperature dependence arises from junction built-in voltage V_{biG} and V_{biS} temperature dependence. Fig. 5 theoretical V_T approximations fall within 15% of measured V_T , which is reasonable agreement considering uncertainty in N_{AS} and t_c for this device that was not SIMS profiled.

SPICE Model. As SPICE [4,5] is the most broadly available electrical circuit simulation/design program, it is important to implement reasonably accurate and accessible SPICE models for 4H-SiC JFET electrical behavior. To ensure that such models can run on all variants of SPICE software,

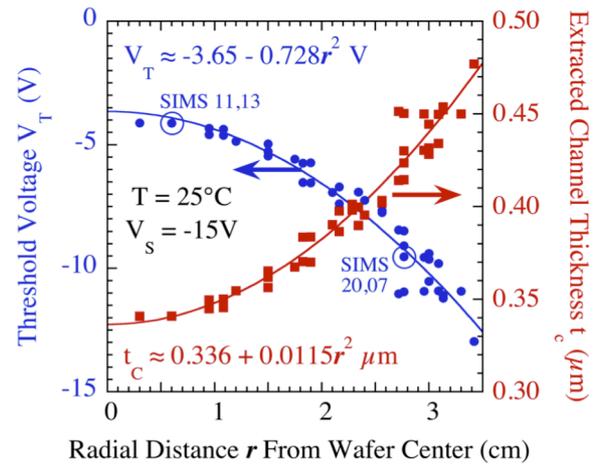


Fig. 2. Measured V_T (blue) and extracted t_c (red) vs. r from 25°C wafer probe map data. The wafer center is Die 13,13.

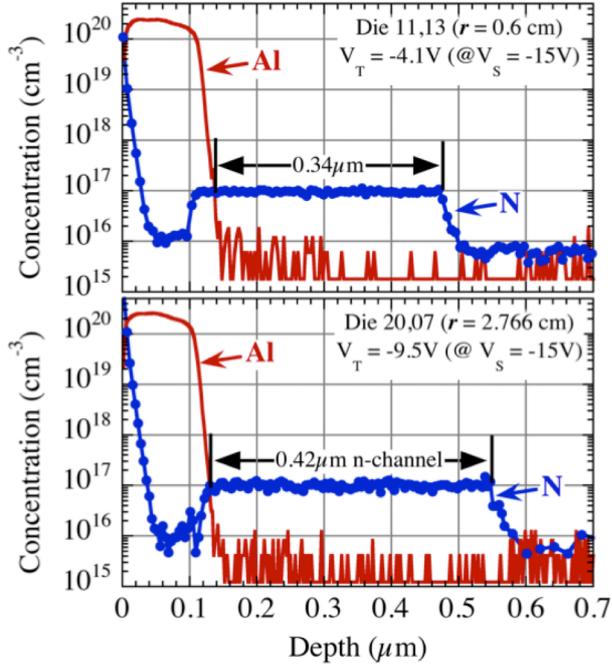


Fig. 3. SIMS of JFET epilayers at two locations on the wafer.

this modeling should be implemented using baseline-version SPICE device models. However, the baseline SPICE JFET model makes no provision whatsoever for body bias effect. Therefore, the baseline SPICE NMOS model, which importantly includes body bias effect, is instead chosen for first-order SPICE modeling of 4H-SiC JFET electrical behavior. *It is important to note that this NMOS modeling approach is only valid so long as gate and substrate junctions do not become forward biased* (which would draw substantial gate/substrate junction current in a physical JFET not accounted for in the NMOS SPICE model). While this general approach was previously used for 6H-SiC JFET SPICE modeling [6], this previous work did not study body bias effect. Eq. 6 shows the baseline SPICE NMOS body effect model formula for V_T as a function of V_S in terms of baseline SPICE NMOS model parameters PHIB, VTO, and GAMMA [4,5].

$$V_T = VTO + GAMMA(\sqrt{2 \cdot PHIB - V_S} - \sqrt{2 \cdot PHIB}) \quad (6)$$

Comparison of Eq. 5 to Eq. 6 readily reveals that they have the same mathematical form except for the linear V_S term residing at the end of Eq. 5. For SiC epitaxial JFET IC designs of interest (i.e., those that approximate Fig. 1 with $|V_S| < 50V$), the linear V_S term is numerically the smallest term of Eq. 5.

Table I shows two proposed mappings for substituting 4H-SiC JFET physical parameters directly into the Eq. 6 SPICE NMOS body effect model. Parameter Map #1 is obtained by directly mapping Eq. 5 terms into obviously corresponding Eq. 6 terms while completely neglecting the linear V_S term at the end of Eq. 5. Map #2 features a mathematically adjusted GAMMA that approximates the impact of the linear V_S term at the end of Eq. 5 within the form of Eq. 6. The V_T vs. V_S plots of Fig. 6 compare

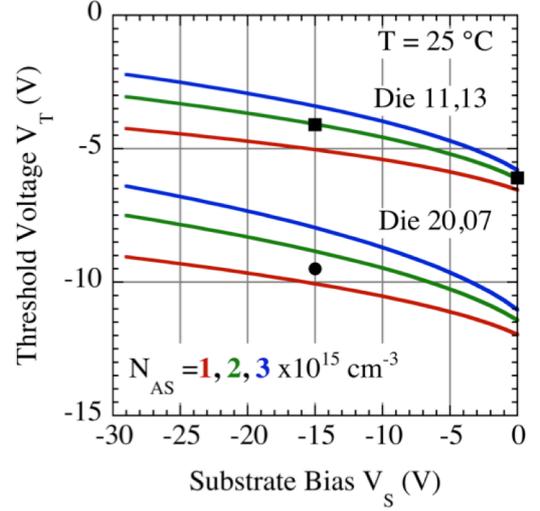


Fig. 4. Theoretical (lines, calculated via Eq. 4) and measured (symbols) JFET V_T vs. V_S for die characterized by SIMS.

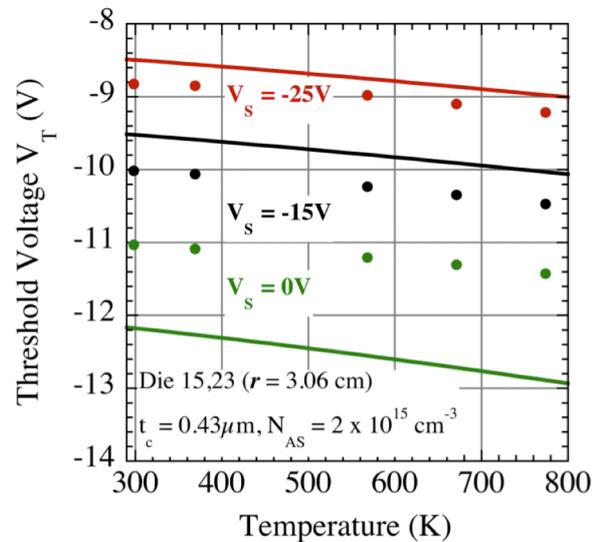


Fig. 5. Theoretical (lines) and measured (symbols) temperature dependence of JFET V_T at $V_S = 0V, -15V, \text{ and } -25V$.

Table I. Parameters for SiC JFET body effect modeling.

| SPICE NMOS Parameter [4] | JFET Parameter Map #1 | JFET Parameter Map #2 |
|--------------------------|--------------------------------|---|
| VT0 | V_{T0} | V_{T0} |
| PHIB | $0.5 V_{bis}$ | $0.5 V_{bis}$ |
| GAMMA | $\frac{2t_c K_{nS}}{K_{nG}^2}$ | $\frac{K_{nS}}{K_{nG}^2} (2t_c - K_{nG})$ |

these two SPICE Eq. 6 approximations against the full Eq. 5 body effect theory for the two Fig. 3 SIMS devices. As seen in Fig. 6, improved agreement with Eq. 5 is obtained for Parameter Map #2.

It is important to note that the NMOS model will crash baseline-version SPICE software when the SPICE TEMP (temperature) parameter exceeds ~ 300 °C. This fact precludes direct use of TEMP=500 input with baseline-version SPICE to simulate 500 °C JFET behavior starting from a 27 °C (SPICE default TEMP) NMOS model [6]. Therefore, a different/unique “500 °C” NMOS model (with parameters adjusted to match 500 °C JFET behavior) must be run with TEMP=27 to carry out baseline-version SPICE simulations of 500 °C circuits. This approach to SPICE modeling the full characteristics of 4H-SiC JFETs and circuits for temperatures up to 500 °C will be presented in more detail in future work.

Summary

This work has derived and experimentally verified equations for modeling the body/substrate bias effect of 4H-SiC n-channel epilayer JFETs over a wide range of temperature and substrate bias. Parameters for using the baseline-version SPICE NMOS transistor model for simulating 4H-SiC JFET body bias behavior have been described. This study has also ascertained that n-channel epilayer *thickness* variation (not doping variation) is responsible for the observed increase in V_T as a function of the radial distance from the center of the experimental 76mm diameter wafer.

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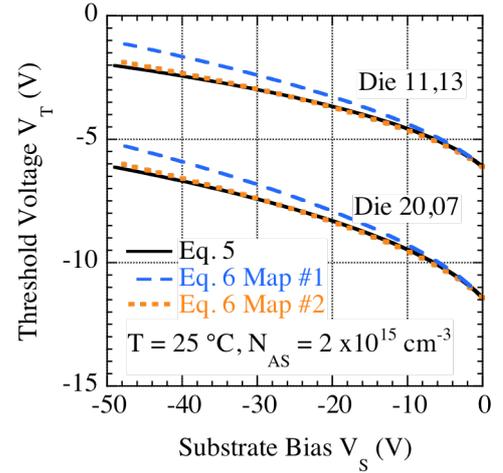


Fig. 6. Comparison of V_T vs. V_S calculated for Fig. 3 SIMS JFETs at $T=25$ °C. Black solid lines are Eq. 5, while colored/dashed use the Eq. 6 with parameter maps listed in Table I.