National Aeronautics and Space Administration



Inflatable Reentry Vehicles and Instrumentation Needs

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Background: Why Inflatables?



- Payload mass to Mars surface is limited by what fits in a rigid capsule that will fit inside the launch vehicle fairing
- Landing altitude at Mars is limited by the ballistic coefficient (mass per area) of the entry vehicle more massive payloads need longer to slow down
- Inflatable technology allows payloads to use the full diameter of the launch fairing, and deploy a large aeroshell before atmospheric interface, landing more payload mass at higher altitude
- Also enable return of large payloads from Low Earth Orbit (LEO)



Mars Surface Access



Inflatables allow access to southern highlands



NDLA Topography £92° Lat, 192° to -1927 W Lo



Entry Heating



15m Inflatable

- The inflatable aeroshell's larger area, blunter nose, and lower ballistic coefficient also reduce the peak heating for the same atmospheric entry conditions and payload mass
- Ballistic entry at Mars:
 - Entry speed: 6km/s
 - Entry mass: 2200kg (MSL-rover class)



- 10m inflatable aeroshell would see ~30 W/cm2 peak flux
- Flexible fabric heat shield has passed ground tests to 75 W/cm2





- NASA Langley has been developing Hypersonic Inflatable Aerodynamic Decelerators (HIADs) for over 10 years
- Systematic technology advancement steps
 - Ground Effort: Project to Advance Inflatable Decelerators for Atmospheric Entry (PAI-DAE): Softgoods technology development
 - Flight Test: Inflatable Reentry Vehicle Experiment (IRVE), 2004-7: 3m diam 60° cone; sounding rocket failed to release payload, no experiment
 - Flight Test: IRVE-II (reflight), 2008-9: Fully successful flight to 218km validated design & analysis techniques, demonstrated HIAD inflation, reentry survivability, & hyper/super/trans/subsonic stable flight
 - Ground Effort: HIAD Project designed improved inflatable structure, tested 6m cone, advanced flexible TPS performance (Gen-1 & Gen-2)
 - Flight Test: IRVE-3, 2009-12: 3m diam 60° cone with improved inflatable structure & Gen-1 TPS; 20G launch, 469km apogee, 20G entry, 14.4 W/cm2
 - Ground Effort: HIAD-2 inflatable structure & TPS development continues
- Next: LEO reentry flight test, akin to Mars direct entry flux
 - Proposed twice (HEART, THOR) but not yet funded













Pending Commercial Use



- United Launch Alliance, maker of Atlas and Delta rockets, announced in April 2015 their plans to use a HIAD on their next generation launch vehicle to recover the 1st stage engines for re-use
 - First flight planned for 2019; first engine recovery for 2024



- Proposing 2019 flight test of 6m HIAD reentry from LEO
- Estimating 10-12m HIAD for ULA engine recovery, same size as potential 2024 Mars demo flight



IRVE-3 Reentry Vehicle



3m diam, 60° , 7-toroid inflatable aeroshell with flexible TPS on forward face

Stowed (18.5")



- Centerbody houses the electronics, inflation system, CG offset mechanism, telemetry module, power system (batteries), attitude control system, & cameras
- Inflatable aeroshell packs to 18.5" diam inside nose cone for launch
- Restraint cover holds aeroshell packed for launch; pyrotechnic release
- Inflation system fills aeroshell to 20psi from 3000psi Nitrogen tank
- Attitude control system uses cold Argon thrusters to reorient for entry
- CG Offset mechanism shifts aft half of centerbody laterally for evaluation of inflatable aeroshell L/D Deployed (3m [118"] diam)
- 20G launch, 20G entry
- 281kg entry mass





IRVE-3 Mission Sequence



Apogee 364s, 469km Coast...

Eject Nose Cone 102s, 176km

ACS damps rates 91s (10s duration)

Separate RV & Nose Cone From 3rd Stage Transition 90s, 148km



Yo-Yo De-Spin, 80s 3rd Stage Burnout, 56.9s 3rd Stage Ignition, 23.0s 2nd Stage Burnout, 18.5s 2nd Stage Ignition, 15.0s 1st Stage Burnout, 6.4s 1st Stage Ignition, 0s

Launch on Black Brant-XI from WFF 940lb payload, El 84deg, Az 155deg

Start Aeroshell Inflation 436s, 448km (0 to 20psi in 186s)



Reorient for Entry 587s, 260km (40s duration)

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Lateral CG Shift 628s, 127km (1s duration)

Atmospheric Interface, 25Pa (664s, 85km)



Peak Heating 14.4W/cm2 678s, 50km, Mach 7 (peak Mach 9.8)

Peak Dynamic Pressure 6.0KPa 683s, 40km, 20.2g's

Reentry Experiment Complete at Mach < 0.7



Bonus: CG Maneuvers

LOS by land radar & TM 910s, 10.5km

Vent NIACS and Inflation System Gas

RV splashdown at 30m/s 1194s (447km downrange)

Recovery Attempt - Unsuccessful

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IRVE-3 Trajectory at Scale









IRVE-3 Instrumentation



- 5 heat flux gauges on nose
- 64 thermocouples
 - Type K, 30 AWG leads, glass braid
 - Electronics mostly set for 0-1000°C
- 19 pressure gauges
- 4 video cameras
- Inflation gas flow meter
- IMU & GPS in attitude control system
- Accelerometers & attitude sensors
- 8 thermistors (electronics temps)
- Current & voltage monitors (power system)
- 6 string potentiometers (CG offset system)
- Ground radar tracking / on-board transponder







Heat Flux Gauges on IRVE-3 Nose



- 5 MedTherm Schmidt-Boelter gauges
- Copper, 1" diameter x 1" long
- Mounted through rigid Al nose
- End is flush with surface of TPS
- Lip of 1.9" diameter copper mounting bracket holds edge of TPS
- Step from edge of bracket to TPS filled with RTV 159
- Assembled, 0.5lb each, plus cabling
- Are too large & heavy for convenient installation on inflatable structure





18 Thermocouples on IRVE-3 Nose



- S = Surface (between or below Nextel)
- M = Middle (between insulation layers)
- D = Deep (under insulation)
- Some locations have stack of 3 TC's, other locations have solo TC's
- TC's sewn to surrounding material
- To avoid puncturing TPS gas barrier, TC leads run between layers to outer edge of nose, then into centerbody









Thermocouples on IRVE-3 Aeroshell



- Most are Surface / Mid / Deep in TPS, as on the nose
- A few on centerbody, & on aft side of the structural straps that connect the inflatable toroids
- To avoid puncturing TPS gas barrier, TC leads run between layers to max diameter, to aft edge of TPS, then (between TPS & inflatable) back to centerbody
 - Long leads affect readings, & can pick up EMI
- Aeroshell must be hard packed for launch:
 - Tight folds, vacuum bagging, & hand-working to smooth out fabric bumps, etc
 - Zig-zag extra lead length to accommodate folds-
 - IRVE-3 hard-packed to 39 lb/ft3
- 4 TC leads broke during packing
 - 1st pack for deployment test, 2nd for flight
- 2" diam bundle of TC wires heavy, difficult to pack
- Want more TC's on 6m flight test article
- What wireless capabilities exist?









IRVE-3 Pressure Gauges



- Taber pressure gauges, ~1" diam x 3" long
- 5 on ports built into nose heat flux gauges; pressure gauges inside nose
- 1 on inflation tank
- 1 downstream of pressure regulator
- 2 in inflation manifolds
- 7 to monitor toroid pressures
- 3 in centerbody measure ambient pressure



• Like our heat flux gauges, the pressure gauges are too large for convenient installation out on the inflatable structure



IRVE-3 Video Cameras



- Flew 4 VGA video cameras
- Positioned atop centerbody, to monitor inflated aeroshell geometry
- Used most of the available 10Mbps downlink
- Extremely useful for diagnostics, outreach, and conveying flight events
- Planning for HD cameras on future flights, with solid state recorder
- May fly infrared cameras as well (room temp to 200-300C)





IRVE-3 Flight Video (2 minutes)





Several related videos are on YouTube: Search for IRVE-3.

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- Not all TC's survive integration & test installed symmetric ones
- Saw some unexpected events in flight, where multiple sensors helped
- Free fall hindered the inflation tank heater more than expected
 - No convection in free fall, then impressive amount at 20G's
 - Electrical current sensor confirmed flight heat generation matched ground test, not a glitch in TC reading
- Post-flight reconstruction showed 1.5G deceleration dip for 100msec
 - Seen by IMU, accelerometers, & pressure gauges; not just a glitch
 - Video showed no aeroshell change
 - Required an 11% density drop for ~100m ("hole in the sky")
 - Similar pockets were seen during Shuttle reentries







- Future flights won't duplicate 2012 IRVE-3 test conditions
- IRVE-3 TPS (Nextel/Pyrogel) saw peak heat flux of 14.4W/cm2
- Gen-2 TPS (SiC/Carbon Felt) has survived ground testing to levels analogous to 75W/cm2 flight
 - Ground test facility used 220sec square pulse (no ramp up/down)
 - Peak TPS capability vs flight-like heating profile (ramp up to peak flux, ramp down) is unclear
- Research underway on potential Gen-3 TPS materials
- TPS insulator thickness sized so back surface of TPS peaks at 300-400°C
- Working toward 400°C-capable inflatable structure, though structure will only reach that where in contact with TPS
- Lower launch acceleration; large rockets to orbit accelerate more slowly than small solid rockets
- Lower reentry deceleration; IRVE-3 reentered almost straight down to maximize heating on the TPS, but LEO reentry will be at a shallow angle
- Note: Gen-2 HIAD TPS is conductive & RF opaque





- Want everything smaller & lighter
 - Data system electronics
 - Heat flux gauges, pressure sensors, gas flow meter, etc
- Interested in wireless measurement of temperature in/behind the TPS
 - How small could the sensor package be?
 - Need a small sensor to accurately measure rapid thermal changes; perhaps use a TC a short distance from the associated electronics?
 - How to power it?
- Interested in additional measurement capabilities
 - For ground tests, used a laser scanner to measure displacement
 - During flight, use embedded fiber optics?
- Sensors for the aeroshell would need to tolerate packing & folding, with no sharp edges to damage fabric & films
- Need to be pyro-safe, or at least powered off until pyro events are done
- Need to tolerate flight conditions / ground handling



Many Thanks to the HIAD-2 Team







Questions?





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