

Toward a Nonlinear Acoustic Analogy: Turbulence as a Source of Sound and Nonlinear Propagation

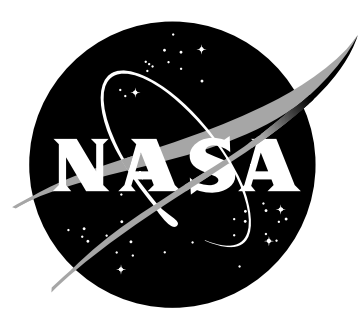
Steven A. E. Miller

The National Aeronautics and Space Administration

NASA Technical Working Group

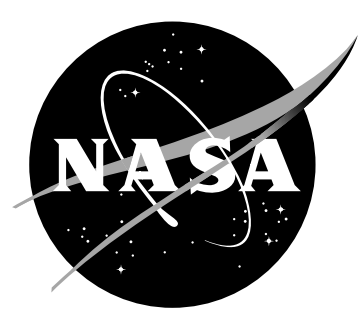
April 21st-22nd 2015

Based on Miller, S. A. E., "Toward a Nonlinear Acoustic Analogy: Turbulence as a Source of Sound and Nonlinear Propagation," NASA TM, 2015.

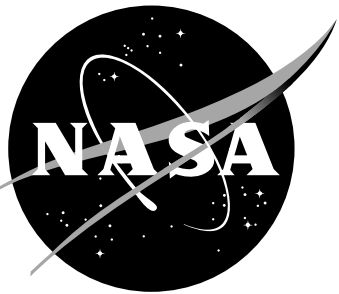


Acknowledgements

- NASA Advanced Air Vehicles Program
Commercial Supersonic Technology Project
- Brian Howerton - NASA Langley - measurements
from NASA Normal Incidence Tube
- Emily Mazur - NASA 2012 Intern - evaluated
Blackstock bridging function
- Many previous curious researchers



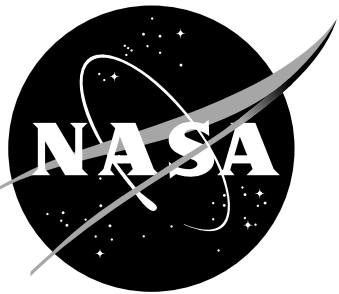
Introduction



Turbulence and Nonlinear Propagation

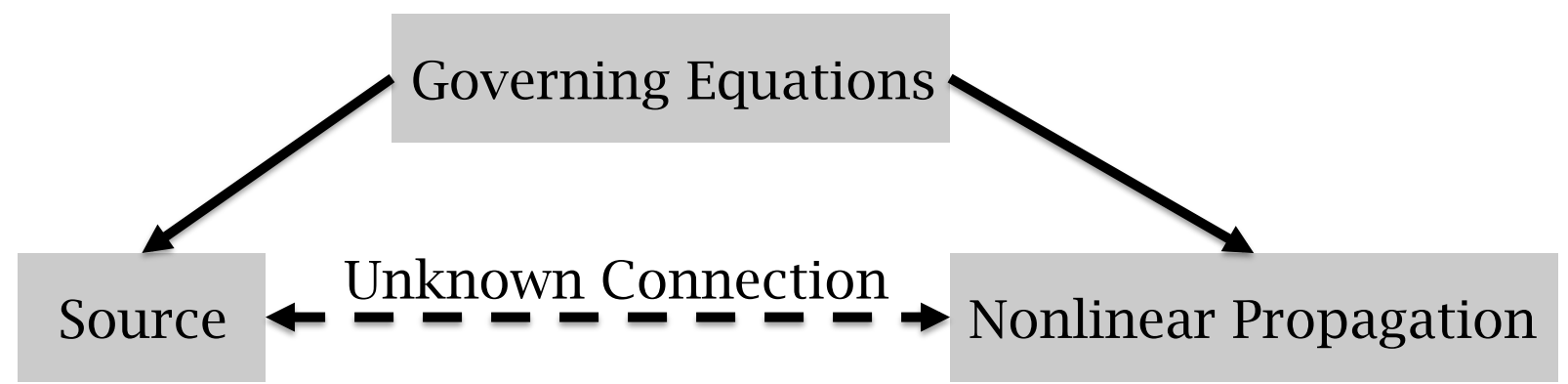
- Aerospace vehicles produce turbulence
- Sound propagates nonlinearly if turbulence is highly intense
- Intense noise is harmful to the vehicle and environment

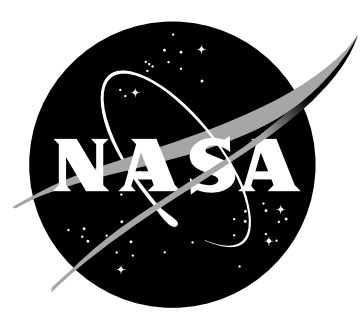




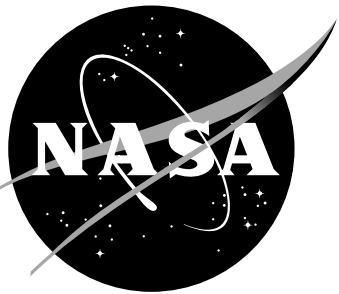
Turbulence and Nonlinear Propagation

- Understand different mathematical models of sound generation and propagation
- Relate the governing equations to sound generation and propagation
- Show a mathematical connection between sound generation (acoustic analogy) and sound propagation (Burgers' equation)





Mathematical Models



Claude-Louis Navier and George Gabriel Stokes

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0 \quad \frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = \frac{\partial \tau_{ij}}{\partial x_j}$$

$$\frac{\partial \rho e_o}{\partial t} + \frac{\partial \rho u_j e_o}{\partial x_j} = - \frac{\partial u_j p}{\partial x_j} - \frac{\partial q_j}{\partial x_j} + \frac{\partial u_i \tau_{ij}}{\partial x_j}$$



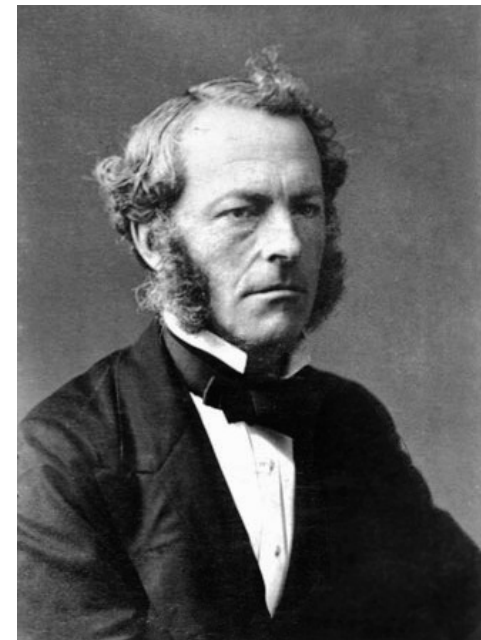
Navier

Claude-Louis Marie
Henri Navier

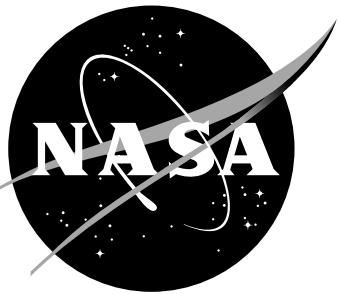
- 1735-1836
- French
- Professor at
École Nationale
des Ponts et
Chaussées
- Known for
elasticity and
structural
engineering

Sir George Stokes

- 1819-1903
- Irish
- Lucasian
Professor
- Fluids, Optics,
Chemistry
- Politics and
Theology



Stokes



Richard D. Fay

Governing Equation (Conjecture)

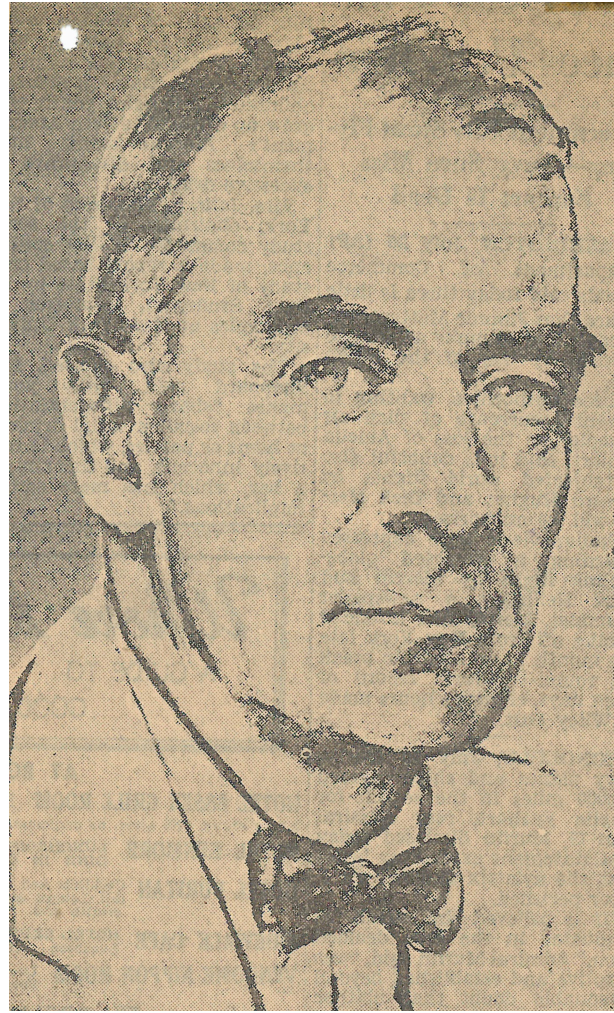
$$c_\infty^2 \frac{\partial^2 y}{\partial x^2} = \frac{\partial y}{\partial x}^{\gamma+1} \left[\frac{\partial^2 y}{\partial t^2} - \frac{4\mu}{3\rho_\infty} \frac{\partial}{\partial t} \left(\frac{\partial^2 y}{\partial x^2} \right) \right]$$

- Governs shocked one-dimensional finite amplitude waves
- y is particle displacement
- Solution via assumptions
 - Periodic
 - dy / dx is Fourier series
 - Substitute and solve Fourier series

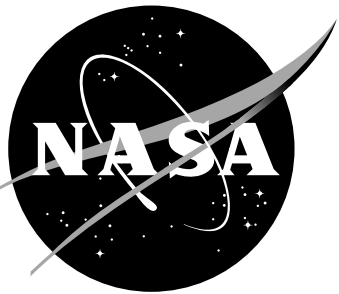
Fay, R. D., "Plane Sound Waves of Finite Amplitude,"
 Journal of the Acoustical Society of America, Vol. 3, No.
 9, 1931, pp. 222-241. doi:10.1121/1.1901928.

Solution

$$\frac{p}{p_\infty} = \frac{32}{3} \frac{\mu\omega}{c_\infty^2 \rho_\infty} \left(\frac{\gamma}{\gamma+1} \right)^{n=\infty} \sum_{n=1}^{\infty} \frac{\sin n (\omega t - \omega x / c_\infty)}{\sinh n \left[\log \left[\frac{16\mu\omega}{3\rho_\infty (\gamma+1) c_\infty^2 K_{1,1}} \right] + \frac{2x\mu\omega^2}{3c_\infty^3 \rho_\infty} \right]}$$



Courtesy of the MIT Electrical Engineering and
Computer Science Department



Guido Fubini-Ghiron

Governing Equation (Conjecture)

$$\frac{\partial^2 \xi}{\partial t^2} + \frac{\partial \xi}{\partial t} \frac{\partial^2 \xi}{\partial x \partial t} = - \frac{1}{\rho} \frac{\partial p}{\partial x}$$

- Continuous non-conservative one-dimensional finite amplitude waves
- ξ is particle displacement
- Solution via Earnshaw approach
 - Write as binomial series and truncate
 - Convert to Eulerian framework and rewrite as Fourier series

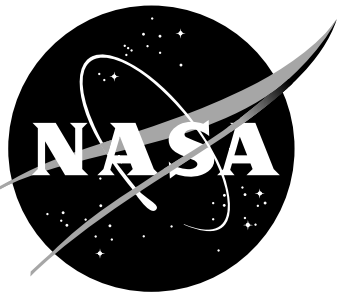
Solution

$$\frac{p}{p_\infty} = \sum_{n=1}^{\infty} \frac{2}{n\sigma} J_n[n\sigma] \sin n(\omega t - kx)$$

Fubini-Ghiron, G., “Anomalie nella Propagazione di onde Acustiche di Grande Ampiezza,” *Alta Frequenza*, Vol. 4, 1935, pp. 530-581.



Italian, 1879-1943, Professor of Mathematics at Princeton



David T. Blackstock

Governing Equations (Conjecture)

$$u = g(\phi) \quad \tau = \phi - (\beta c_\infty^{-2})g(\phi)$$

$$\frac{dt'_s}{dx} = -\frac{1}{2}\beta c_\infty^{-2}(u_a + u_b)$$

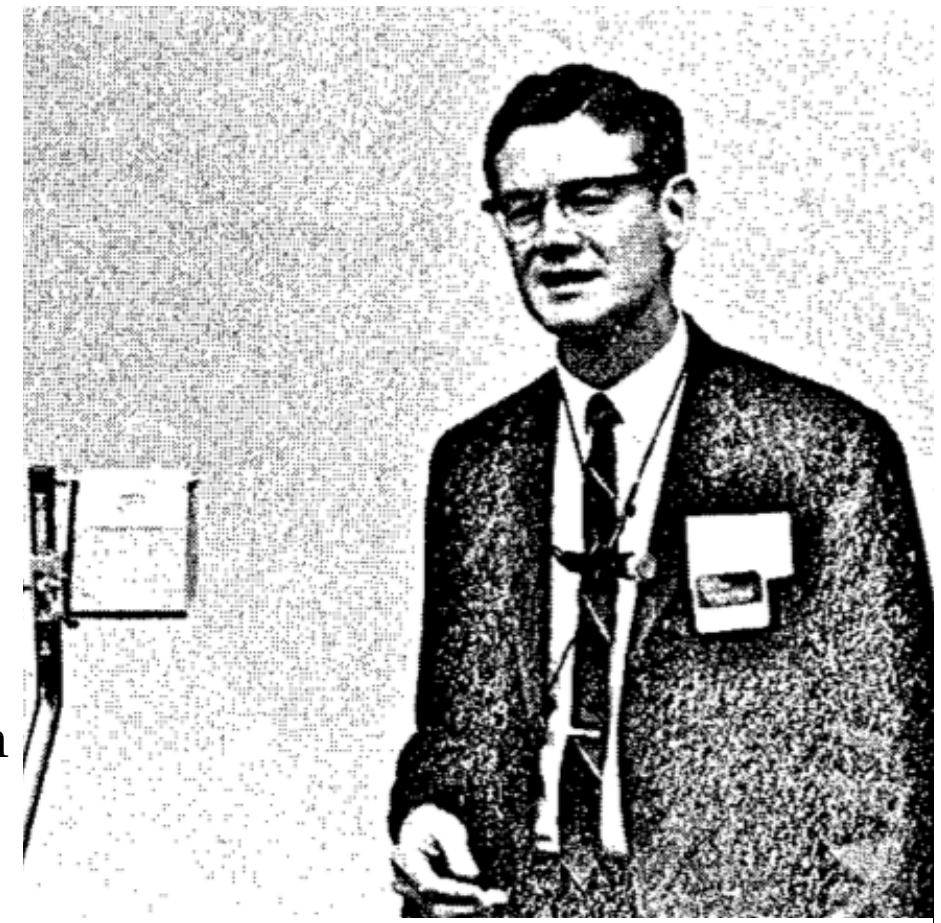
- Weak shock theory
- g is a function and ϕ is emission time
- Direct solution approach by substitution after eliminating ϕ
 - Assume boundary value problem
 - Resultant transcendental equation solved with Fourier series assumption

Solution

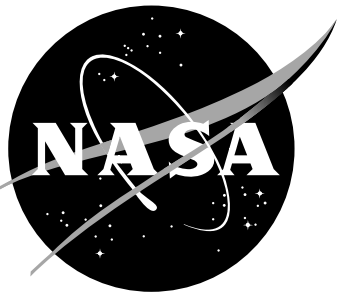
$$p(x, t) = p_o \sum_{n=1}^{\infty} B_n \sin [n\omega\tau]$$

$$B_n = \frac{2}{n(1 + \sigma)} + \frac{2}{n\pi\sigma} \int_{\Phi_{sh}}^{\pi} \cos [n(\Phi - \sigma \sin \Phi)] d\Phi$$

Blackstock, D. T., "Connection Between the Fay and Fubini Solutions for Plane Sound Waves of Finite Amplitude," *Journal of the Acoustical Society of America*, Vol. 39, No. 6, 1965, pp. 1019-1026. doi:10.1121/1.1909986.



Blackstock, D. T., 'History of Nonlinear Acoustics and a Survey of Burgers' and Related Equations,' 1969.



M. J. Lighthill

Governing equations are Navier-Stokes

- Exactly rearrange to form a governing equation, the acoustic analogy

$$\frac{\partial^2 \rho}{\partial t^2} - c_\infty^2 \frac{\partial^2 \rho}{\partial x_i \partial x_i} = \frac{\partial^2 T_{ij}}{\partial x_i \partial x_j}$$

- Right hand side is equivalent source
- Left hand side is linear wave operator

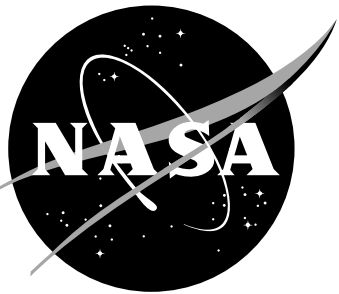
Lighthill, M. J., "On Sound Generated Aerodynamically. I. General Theory," Proc. R. Soc. Lond. A., Vol. 211, No. 1107, 1952, pp. 564–587. doi:10.1098/rspa.1952.0060.

One solution loosely based on Ffowcs Williams

$$S(\mathbf{x}, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{r_i r_j r'_l r'_m}{c_\infty^4 r^2 r'^2} g(\mathbf{x}, \mathbf{y}, \omega) g^*(\mathbf{x}, \mathbf{y}', \omega) \frac{\partial^4}{\partial \tau^4} R_{ijlm}(\mathbf{y}, \boldsymbol{\eta}, \tau) \times \exp \left[-i\omega \left(\tau + \frac{r}{c_\infty} - \frac{r'}{c_\infty} \right) \right] d\tau d\boldsymbol{\eta} d\mathbf{y}$$



English (born Paris), 1924-1998, Lucasian Professor at Cambridge



David G. Crighton

Governing equations is Navier-Stokes

- Assume
 - u is summation of a gradient and cross-product, eliminate high order terms, flow is irrotational
 - Solutions are set of symmetry
 - $Kr \gg 1$, 'linear wavenumber'

Governing Equation (non-gen. Burgers')

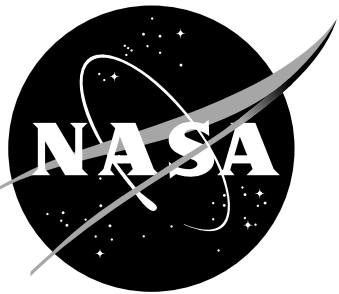
$$\frac{\partial u}{\partial t} + c_\infty \frac{\partial u}{\partial r} + \frac{\gamma + 1}{2} u \frac{\partial u}{\partial r} + \frac{j c_\infty u}{2r} = \frac{\delta}{2} \frac{\partial^2 u}{\partial r^2}$$

- Spherical, cylindrical, and planar nonlinear wave propagation

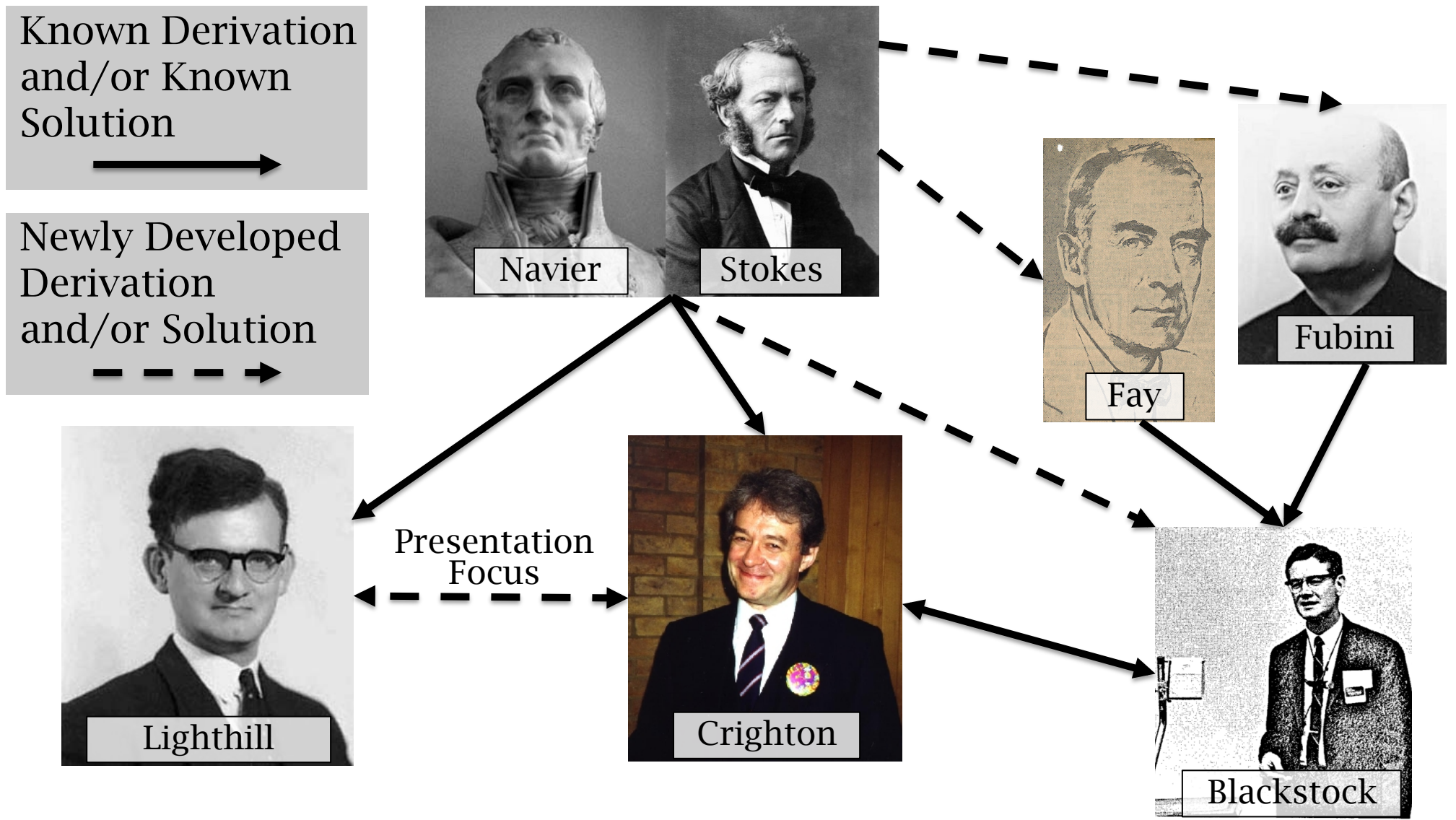
Crighton, D. G., "Model Equations of Nonlinear Acoustics,"
 Annual Review of Fluid Mechanics, Vol. 11, 1979, pp. 11-33.
 doi:10.1146/annurev.fl.11.010179.000303.



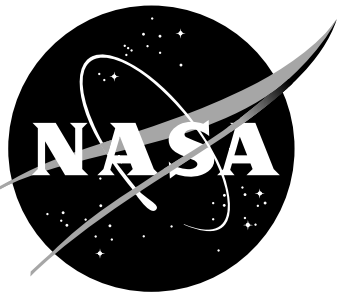
English, 1942-2000, Professor
 of Applied Mathematics
 Cambridge
Also Opera lover - so am I! :)



Mathematical Relationships



Miller NASA TM shows the mathematical connections and solutions of ALL relations!



The Navier-Stokes Equations and the Acoustic Analogy

Governing equations are Navier-Stokes.

We now think of the Green's function as satisfying

$$\rho(\mathbf{x}, t) = \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} g \frac{\partial^2 T_{ij}}{\partial x_i \partial x_j} d\tau d\mathbf{y}$$

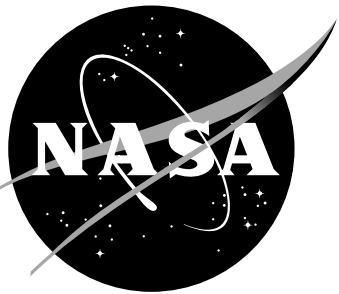
We can show using the cross-spectral acoustic analogy

$$S(\mathbf{x}, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{r_i r_j r'_l r'_m}{c_\infty^4 r^2 r'^2} g(\mathbf{x}, \mathbf{y}, \omega) g^*(\mathbf{x}, \mathbf{y}', \omega) \frac{\partial^4}{\partial \tau^4} R_{ijklm}(\mathbf{y}, \boldsymbol{\eta}, \tau) \times \exp \left[-i\omega \left(\tau + \frac{r}{c_\infty} - \frac{r'}{c_\infty} \right) \right] d\tau d\boldsymbol{\eta} d\mathbf{y}$$

A statistical source model for sound generation (altered from Miller) is

$$\frac{\partial^4}{\partial \tau^4} R_{ijklm}(\mathbf{y}, \boldsymbol{\eta}, \tau) = \frac{4A_{ijklm} \bar{u}^4}{\pi^{1/2} l_s^8} (3l_s^4 - 12l_s^2(\xi - \bar{u}\tau)^2 + 4(\xi - \bar{u}\tau)^4) \times \exp \left[\frac{-|\xi|}{\bar{u}\tau_s} \right] \exp \left[\frac{-(\xi - \bar{u}\tau)^2}{l_s^2} \right] \exp \left[\frac{-\eta^2}{l_{sy}^2} \right] \exp \left[\frac{-\zeta^2}{l_{sz}^2} \right]$$

Miller, S. A. E., "Prediction of Near-Field Jet Cross Spectra," AIAA Journal, 2015. doi:10.2514/1.J053614.



The Navier-Stokes Equations and the Acoustic Analogy

Using the source model, assuming that the observer is in the far-field, simplifying, and carefully rearranging yields

$$S(\mathbf{x}, \omega) = \frac{\pi\omega^4}{c_\infty^4} g(\mathbf{x}, \omega) g^*(\mathbf{x}, \omega) \int_{-\infty}^{\infty} A_{ijklm} \frac{r_i r_j r_l r_m}{r^4} \frac{l_s l_{sy} l_{sz}}{\bar{u}} \exp\left[\frac{-l_s^2 \omega^2}{4\bar{u}^2}\right] \times \int_{-\infty}^{\infty} \exp\left[\frac{-i\xi\omega}{\bar{u}}\right] \exp\left[\frac{-|\xi|}{\bar{u}\tau_s}\right] d\xi dy_1$$

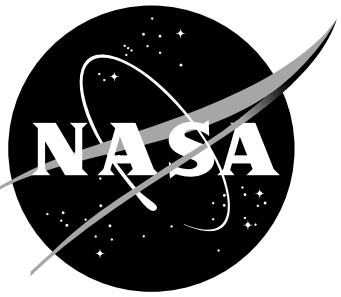
Green's function

Source Spectrum

Selective far-field assumption

- Source remains a volumetric integral
- Propagation approximated from a point within source volume

Need to find what gg^* is to capture nonlinear propagation effects



The Navier-Stokes Equations and a Burgers' Equation

The Navier-Stokes equations

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0 \quad \text{and} \quad \frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = \frac{\partial \tau_{ij}}{\partial x_j}$$

Following Crighton then finding a more compact form governing pressure

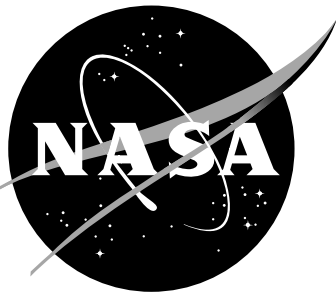
$$\frac{\partial p}{\partial x} + m \frac{p}{r} - \epsilon p \frac{\partial p}{\partial \tau} = \frac{\delta}{2c_\infty^3} \frac{\partial^2 p}{\partial \tau^2}$$

Select analytical solutions exist - eg: Blackstock, Fay, and Fubini

Seek a numerical solution in the frequency domain (as shown by Saxena)

$$\frac{\partial \tilde{p}}{\partial r} + m \frac{\tilde{p}}{r} + (\alpha + i\beta) \tilde{p} = \frac{i\omega\epsilon}{2} \tilde{q}$$

Pseudo-spectral numerical method marches solution in space from prescribed boundary condition (same BC as Blackstock)



The Connection Between the Acoustic Analogy and Generalized Burgers' Equation

Conjecture: Given the solution of

$$\frac{\partial \tilde{p}}{\partial r} + m \frac{\tilde{p}}{r} + (\alpha + i\beta) \tilde{p} = \frac{i\omega\epsilon}{2} \tilde{q}$$

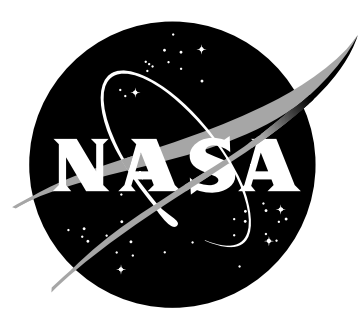
subject to the boundary condition of a source spectrum of the acoustic analogy and $x \gg D$ then

$$g(\mathbf{x}, \omega)g^*(\mathbf{x}, \omega) \approx \tilde{p}(\mathbf{x}, \omega)\tilde{p}^*(\mathbf{x}, \omega)$$

within the acoustic analogy. As $\lim \tilde{p} \rightarrow \epsilon$

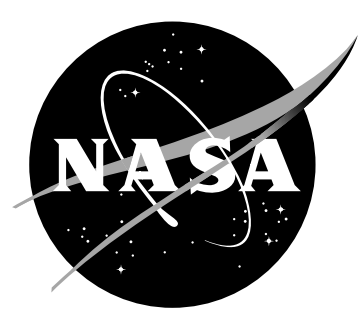
$$g(\mathbf{x}, \omega)g^*(\mathbf{x}, \omega) = \tilde{p}(\mathbf{x}, \omega)\tilde{p}^*(\mathbf{x}, \omega)$$

for the traditional approach only.

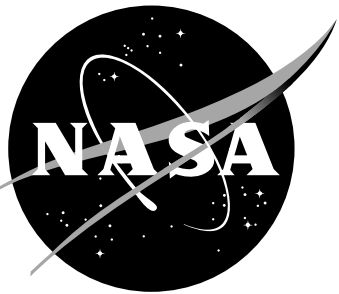


Acoustic Analogy and Burgers' Equation

- Approximation of gg^* is obtained from solution of generalized Burgers' equation
- Boundary condition (at $r = 0$) of generalized Burgers' equation is broadband source spectrum
- Source spectrum at low intensities results in predictions that are equivalent to those produced by traditional acoustic analogies
- Source spectrum at high intensity causes nonlinear terms within generalized Burgers' equation to be dominant
- Characteristics of nonlinear propagation are apparent in predicted jet mixing noise spectrum.

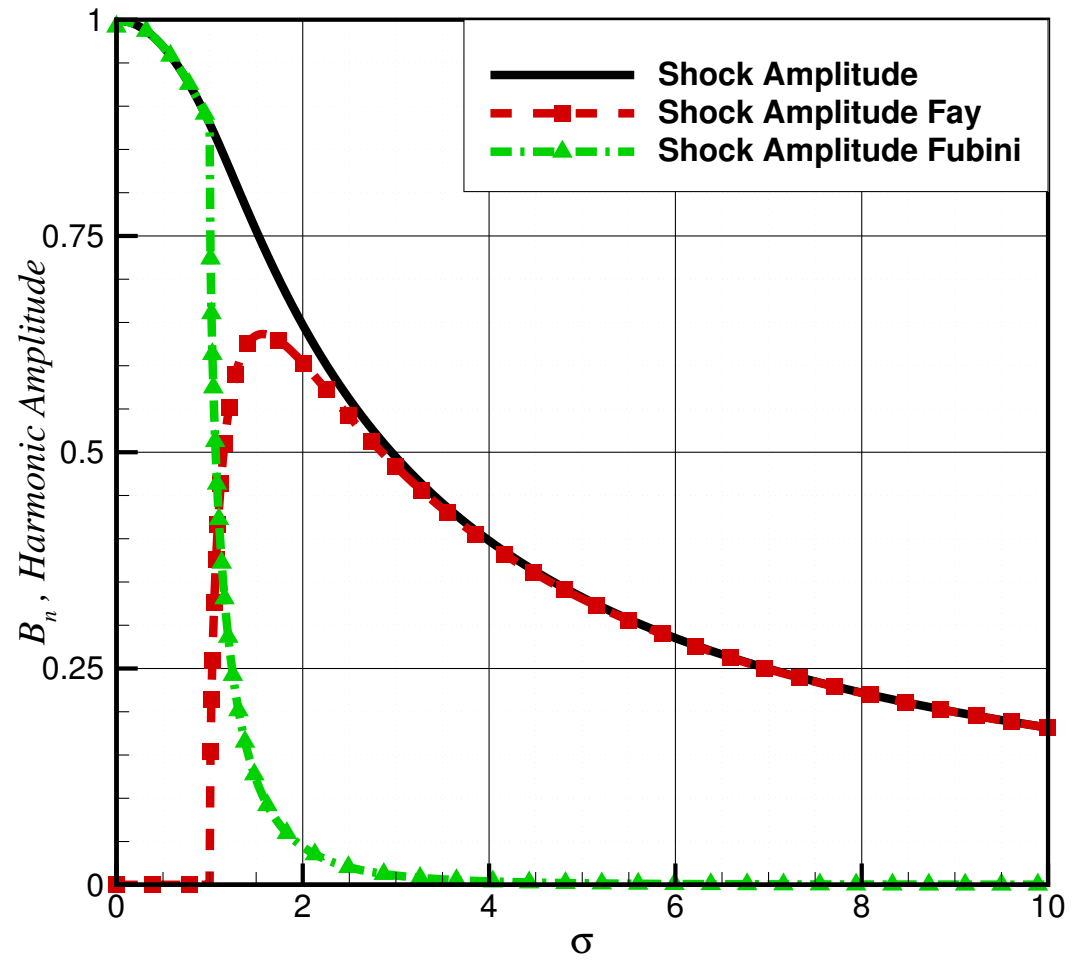


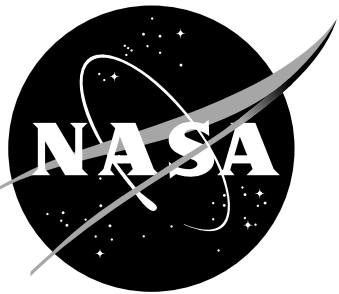
Results



Examination of Blackstock, Fay, and Fubini

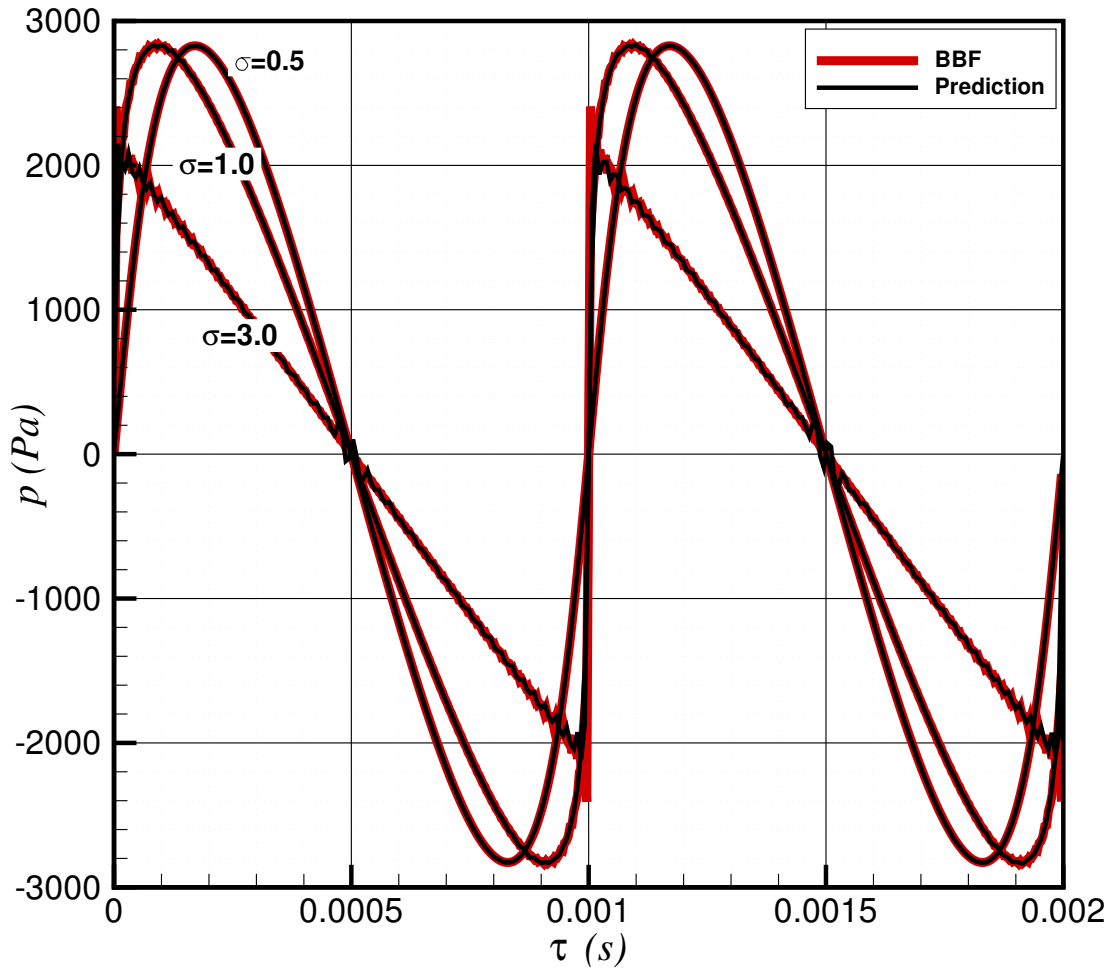
- Almost exact solutions of generalized Burgers' equation
- Source planar sin wave at 160dB and 1000Hz
- Regions of validity

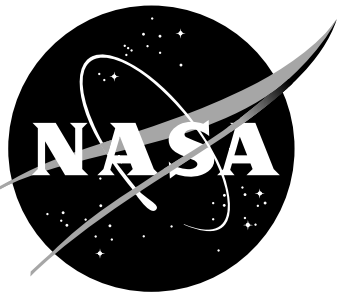




Numerical Solver of Generalized Burgers' Equation and Blackstock Bridging Function

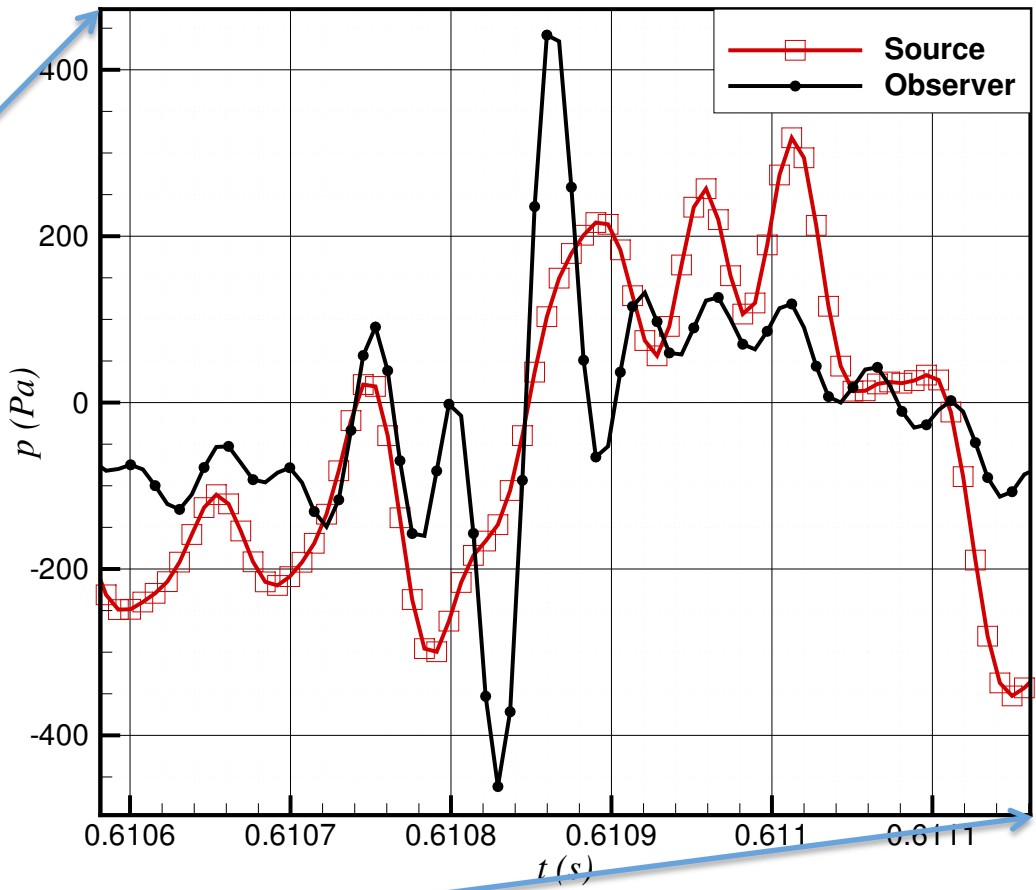
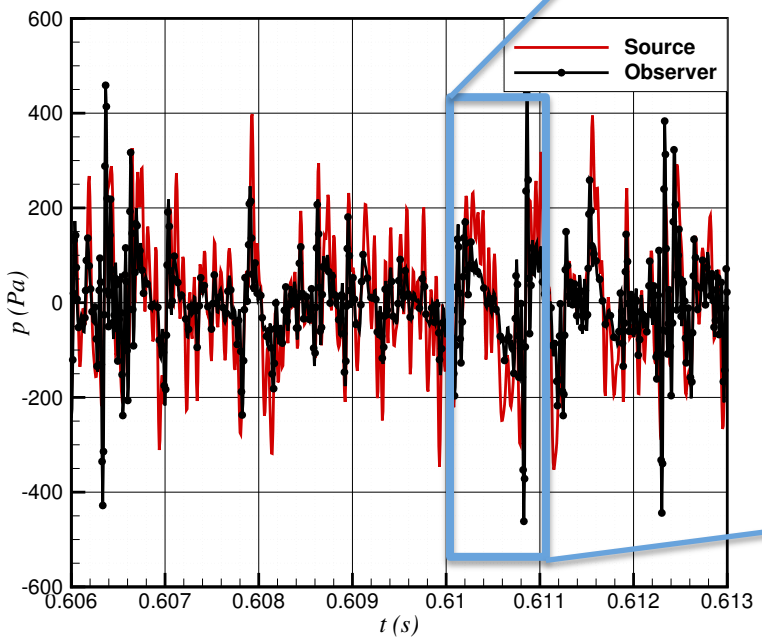
- Comparison at three observer positions
- Numerical solver agrees with analytic result
- Source planar sin wave at 160dB and 1000Hz
- Gibb's phenomenon present

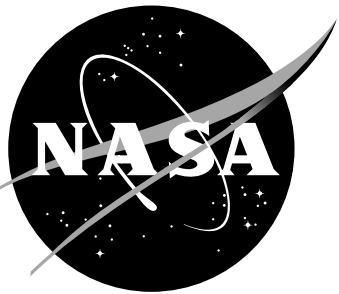




Propagation of a Broadband Signal

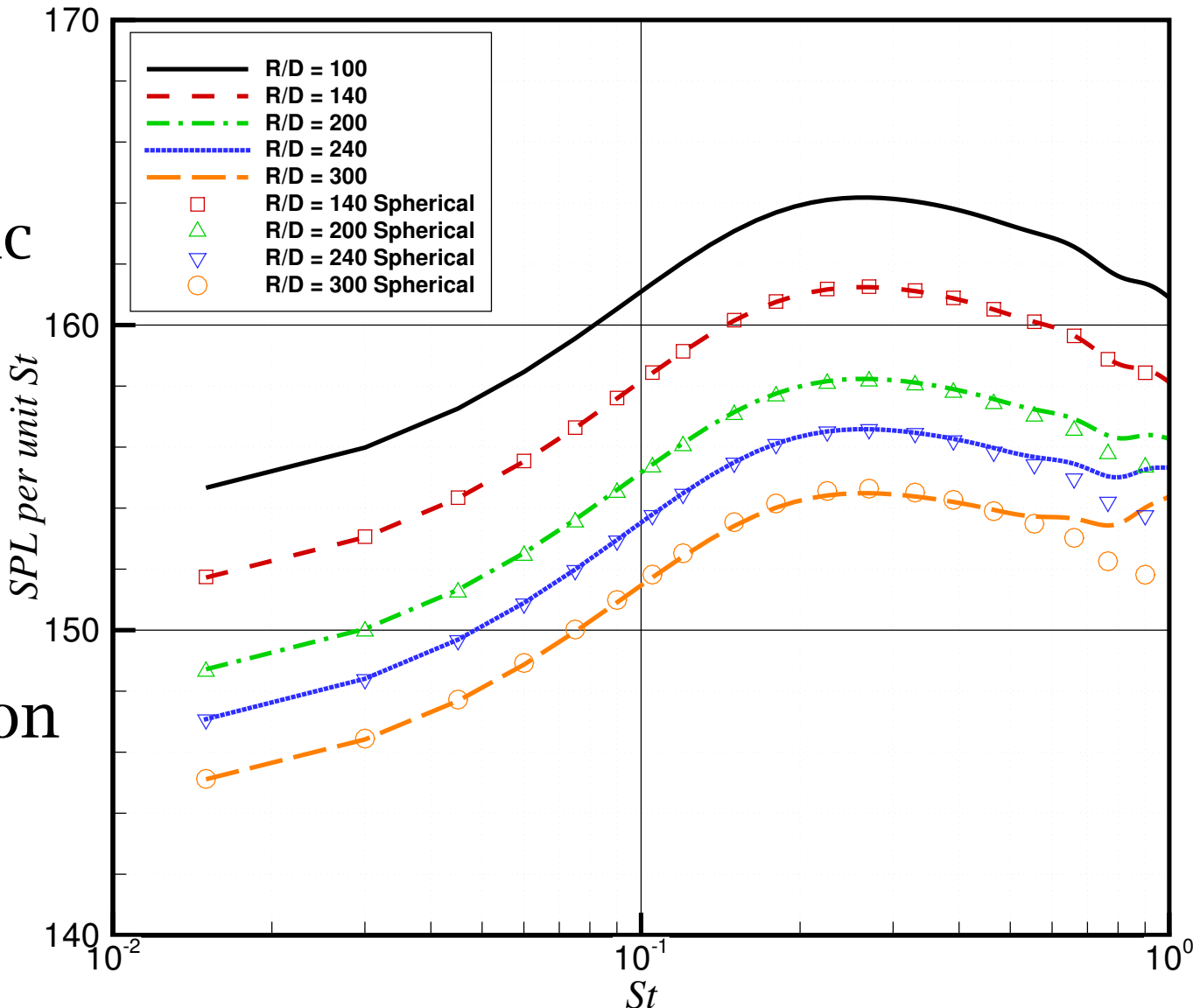
- Shocked observer waveform due to wave coalescence
- Discontinuities not present in source signal
- Not observed in linear acoustics
- Jet $M_j = 1.86$
- Jet TTR = 3.20
- Sideline direction

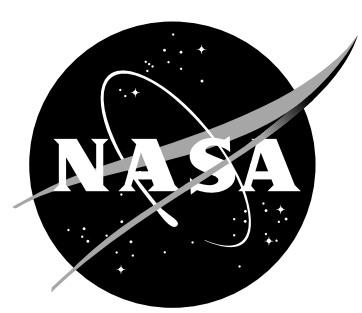




Example Jet Noise Prediction Directly Incorporating Nonlinear Propagation

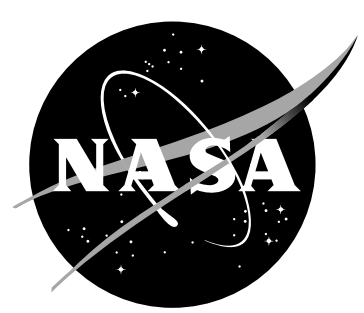
- Unified Acoustic Analogy with Nonlinear Propagation
- Jet $M_j = 1.86$
- Jet TTR = 3.20
- Sideline direction



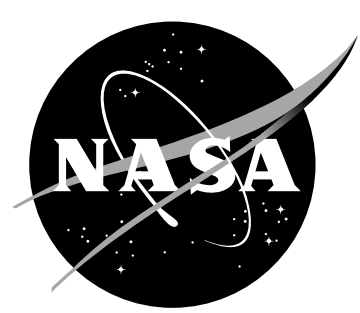


Summary and Conclusion

- Showed connection between Navier-Stokes equations, generalized Burgers' equation (sound propagation), and Acoustic Analogy (sound source)
- Nonlinear propagation taken into account directly from source to observer
- A single equation contains sound source and nonlinear propagation from turbulence
- Evaluated select equations to demonstrate relevant physics

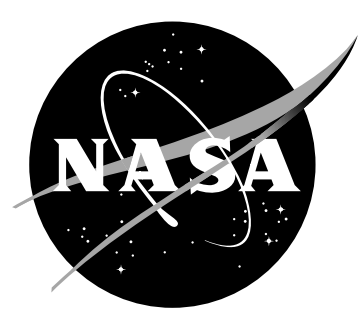


Questions



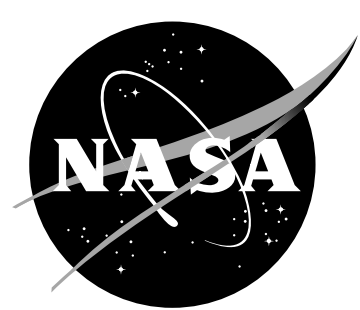
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