

Surface Power for Mars

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Overview

This presentation covers two related papers

NETS 5074, Integrated Surface Power Strategy for Mars

- Presented at Nuclear and Emerging Technologies for Space (NETS) 2015 Conference, Albuquerque, New Mexico, February, 2015
- Outlines the advantages of multiple, small fission power systems versus previous schemes that relied on a single, large system

AIAA-2016-5452, Solar vs. Fission Power for Mars

- Presented at AIAA SPACE 2016, Long Beach, September, 2016
- Revisits the solar versus fission surface power trade in light of new Evolvable Mars Campaign (EMC) mission concepts
- Important to note these are very different missions
 - First paper assumed Apollo-style Mars exploration missions
 - \checkmark Each crew explores a different landing site
 - Second paper assumed "pioneering" approach with multiple expeditions to a single landing site (allowing equipment re-use)



Nuclear and Emerging Technologies for Space 2015 Albuquerque, New Mexico



Background: Notional Crewed Mars Mission

Conceptual Mars surface mission assumes two each 40 kWe Fission Surface Power (FSP) Systems

- Primary unit deployed on a Cargo Lander to make return propellant (oxygen)
- Contingency unit arrives later with the crew
- FSP is ~ 7,000 kg and must be operated >1 km from the Habitat



Lands before crew

- Un-crewed Mars Ascent Vehicle (MAV)
- FSP and In Situ Resource Utilization (ISRU)
 - Makes propellant for crew return
- Mobility
 - To relocate the FSP 1 km from Lander

Lands after MAV is fueled

- Surface Habitat and Crew
- Spare FSP
- Mobility
 - To transport Spare FSP and crew

Issues and Study Objectives



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- Validate Mars Surface power needs
- Is 40 kW enough...or is it more than we need?
- Explore ways to reduce contingency mass
 - 7,000 kg is a lot of mass for a contingency item *that is never nominally used*
- Explore ways to accelerate FSP deployment
 - Cargo Lander is self-sufficient for power until FSP is deployed and activated
 - Up to 40 sols: Impacts Cargo Lander Power, Thermal, and Structural mass
- Explore ways to minimize FSP impact on mobility systems
 - FSP may be the largest item that Surface Mobility systems have to move
 - May drive mobility design in a way that is incompatible with other mobility tasks





Notional FSP Concept michelle.a.rucker@nasa.gov



Paper 5074, NETS 2015, Albuquerque

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Objective 1: Validate Surface Power Needs



- Conclusion: < 40 kWe Needed <u>for this particular reference</u> <u>mission and conceptual</u> <u>architecture</u>
 - Includes 30% margin
 - ISRU is the Biggest Power Draw
 Atmospheric ISRU
 - Architecture is notional
 - Forward work to better define elements and power needs



Even if ISRU is eliminated, still need almost as much power to support a Habitat and science operations

Exploring Alternatives



We need at least 33.9 kW (for this particular conceptual mission) ...but it doesn't necessarily have to be in a single package



"Kilopower" design is similar to the FSP, but more compact, and

with fewer moving parts **Dimensions (m)** Power Mass **Radiators** Type (kWe) (kg) Dia Height **KILOPOWER** 1.2 *2.2 /4.9 3 751 $9.6 \, {\rm m}^2$ DESIGN Deployed *2.7/5.9 1,011 1.3 13.5 m² 5 KP *3.0 /6.7 7 1,246 1.4 17.1 m² 10 1,544 1.5 *3.3 /7.3 20 m² -34 m 3,300 1.0 7 m tall 37 m² 10 184 m² **FSP** 40 7,000 2.7 7 m tall 184 m² 7 m DESIGN FSP *Height w/Deployable/Fixed Radiators

Paper 5074, NETS 2015, Albuquerque

Objective 2: Reduce Contingency Power Mass

Baseline assumed a 40 kW contingency FSP on the Crew Lander

-Alternative: With 4 ea. 10 kW units on the Cargo Lander, it's unlikely ALL will fail -Don't necessarily need to bring 4 more on the Crew Lander: 1 or 2 spares will do



Mass saved in this example is equivalent to a pressurized rover

Savings are even more significant when cable mass is included

- FSP Concept: Requires more than 1,000 kg of Cable
 - 1 km, 400 VAC transmission cable from FSP to Lander PLUS a 1 km, low voltage DC auxiliary cable from Lander back to FSP
 - FSP Parasitic load: need auxiliary power for FSP fluid pumps, etc.
- Kilopower Concept: Less than 100 kg Cable
 - Fewer moving parts (e.g. heat pipes replace pumps) don't require auxiliary power cable
 - ~60 kg for 1 km of high VAC transmission cable
 - Plus inverter/junction box and jumpers

Objective 2: Reduce Contingency Power Mass

Cumulative Power System Mass (34 kWe Minimum)



- 34 kWe Minimum of Kilopower + 10 kWe Minimum Contingency saves 4 to 8 metric tons compared to baseline 40 kWe FSP
- 4 x 10 kWe Kilopowers + 1 contingency unit is ~200 kg less than an FSP with no contingency unit

Objective 3. Minimize Lander Power Mass

- Lander has to survive up to 40 sols while FSP is being unloaded, relocated 1 km, deployed, and activated
 - —Criticality: Mars Ascent Vehicle (for crew return) needs keepalive power!
 - Lander power mass drives thermal & structural mass, all of which drives descent propellant mass
- With multiple Kilopower units, we have an option to turn one on near the Lander, while remaining units are being deployed
 - Crew hasn't arrived yet, so we can relax separation distance from Lander
 - -Relocate the first unit after the others are on-line

Still may take 40 sols to move all of them, but the Lander doesn't have to be self-sufficient the entire time

4. Minimize Impacts to Surface Mobility

- At 7 m tall and 7 metric tons, FSP is bigger than pressurized rover concepts
- May force rover design or reconfiguration requirements
- Or drive the need for another kind of mobility system
- Current rover concepts with a davit can accommodate smaller Kilopower units



40 kWe FSP

Pressurized Rover Concept

10 kWe Kilopower

Additional Kilopower Concept Advantages

1. Better transportability means Kilopower units can be redeployed

- Use to extend rover range or support remote science operations
- Relocate from one landing site to another
 - After shut-down, safe for crew to approach after ~1 week
 - Safe for robotic approach after ~1 day
- **2.** Deployed Kilopower Units can significantly increase crew exploration radius
 - Solar-only pressurized rover spends 80% of its time charging, 20% roving
 - 2 deployed Kilopower units increase rover driving efficiency from 14 km/day to 46 km/day and adds 37 km to the maximum excursion range from the Habitat
 - 4 units can increase the maximum range to 225 km

3. Kilopower units require less startup power than the FSP

• 2 D-cell batteries vs. 5 kW solar array for FSP



Additional Kilopower Concept Advantages

4. Opens up the *possibility* of reducing the number of landing sites

- Example: 4 areas of interest are within 250 km straight line of each other
- Could potentially land at Jezero Crater and rover to the other 3
- Actual roving range will depend on
 - Terrain factor
 - How many
 Kilopower units are
 available
 - Rover design
 - Risk posture
- But portable power opens up operational concepts not previously considered





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5. Supports small pre-cursor missions without having to develop a sub-scale demo unit

- At 751 kg, the 3 kWe Kilopower unit fits on a Curiosity-class Lander with payload to spare
 - Could be retrieved later and added to a larger Kilopower farm
- At 3,300 kg a small (10 kWe) FSP won't fit on a Curiosity-sized Lander

6. Easier to "evolve" surface capability over time

- 40 kWe FSP requires commitment to 7 ton payload
 - And that's without cables or mobility to relocate it
- With Kilopower units, a program can tailor power for different missions by only flying what's needed
 - One unit for a small precursor or demo mission; multiple units for a crewed mission
- If constrained to a single landing site, can build up capability over time, and expand exploration area with deployable power systems

Additional Kilopower Concept Advantages



Kilopower Concept Disadvantages



1. Requires more HEU

As much as 532 kg HEU for 40 kWe equivalent (+ spares) of 3 kWe units vs. only 220 kg HEU for a baseline FSP (+1 spare)

System Size	HEU Per Unit	Total HEU Needed	Assumptions
40 kWe	110 kg	220 kg	1 primary and 1 contingency unit
10 kWe	50 kg	250 kg	4 primary and 1 contingency units
5 kWe	44 kg	396 kg	7 primary and 2 contingency units
3 kWe	38 kg	532 kg	12 primary and 2 contingency units

2. More HEU may mean more ground handling security overhead

- Especially if multiple units are in various stages of assembly, test, and transport
- Could mitigate by keeping all units together (no partial shipments)

3. More individual reactors means more launch safety overhead

- Each unit has to be located and retrieved in the event of a launch failure
- Could mitigate with a containment shroud
 - Kilopower units will be packaged on a Mars Lander, which will be inside a launch shroud
 - Mars Entry/Descent/Landing (EDL) design could also include an aeroshell

Kilopower Concept Disadvantages



4. More surface delivery (rover) trips to deploy

- FSP only needs 1 trip from Lander to installation site for deployment
- Number of trips to deploy Kilopower will depend on which size is chosen and how many a rover can carry in one trip
 - Current rover concept can likely carry one 10 kWe unit, two 5 kWe units, and at least two 3 kWe units
- Deployment is autonomous/robotic, and once the 1km route has been mapped, subsequent trips aren't especially risky
 - Just wear/tear on the rover

5. Increased operational complexity

- Single FSP can land with cables already connected
- Multiple units may require robotic field connections

6. Potentially lower overall system reliability

- Kilopower unit is internally redundant, so individual units are highly reliable, but more units means more connectors that can fail
 - Can mitigate by making as many connections as possible pre-launch (one end of every cable), add redundant connection ports to each unit, and carry extra cables

Kilopower Concept Disadvantages



7. 10 kWe scaling limit

- Kilopower expected to scale readily up to 10 kWe, but not beyond
- Applications requiring higher power require FSP type design, or would have to accommodate multiple Kilopower systems ganged together
- Not an issue for surface application, but may not be practical for highpower, in-space applications

8. Large deployed system footprint

- Study assumed Kilopower units must be at least 1 body length apart
 - Prevents domino effect if one is knocked over
- In the worst case of 3 kWe units, the overall system footprint is large
 - Though still not as large as the FSP's deployed radiators that would require ~34 m linear area free of obstacles



Mars Surface Power System Unique Needs

1. System Connectivity

- Surface power systems should be designed to operate alone, or in combination with like systems
- Rationale: Need to gang together multiple small systems to meet mission needs

2. Dust Tolerant Mechanisms

- Surface power system mechanisms should be tolerant to surface dust contamination
- Rationale: will be exposed to dust storms, some lasting months. Mechanisms such as deployable radiators and connector covers will be actuated if the systems are redeployed to different areas or to support different activities.

3. Robotic Handling

- Surface power system design should be robust to robotic handling
- Rationale: Power system must be robotically unloaded from the cargo lander, deployed and activated before crew arrives.

4. Surface Transport

- Surface power system design should be robust to Mars surface transportation loads
- Rationale: Power system will be transported a safe distance from the eventual crew habitation area, and may be re-deployed to remote areas to support exploration activities. There are currently no plans to groom roadways on Mars.

5. Compact

- In stowed configuration, surface power systems should be compact
- Rationale: Mars landers will be as much volume-limited as they are mass-limited.

Mars Surface Power System Unique Needs

6. Restart Ability

- Surface power systems should be capable of being started, stopped, and restarted.
- Rationale: Restart ability allows power systems to be moved around the surface to support special activities (such as drilling), and also allows the crew to safely approach for inspections or repairs

7. Surface Environment Compatibility

- Surface power system design should be tolerant to Mars surface environmental conditions.
- Rationale: Unique design features must function in partial gravity, atmospheric pressure, etc.

8. Shelf Life

- Surface power system should be certified for at least 2.5 year [TBR, To Be Resolved] shelf life
- Rationale: Given payload processing time at the launch facility plus Mars transit time, there
 is likely to be a 2+ year lag between power system final check-out and surface activation

9. Operational Life Limit

- Surface power system components should be rated for a minimum of 10 years [TBR] operation. Operational life may be continuous, or intermittent over a 12 year [TBR] period
- Rationale: The surface power system will arrive on the first cargo lander, but must support subsequent missions. With launch intervals of ~26 months, the power system may have to operate for many years.

10.Planetary Protection

- Surface power system design should be sensitive to planetary protection constraints.
- Rationale: if the system generates enough heat to melt surrounding ice it potentially creates a localized "special region" that would have implications for how close crew, crew rovers, or habitats may be located.

Key Take-Aways

- Conceptual crewed Mars surface mission requires <40 kWe Power
 For this particular reference mission and architecture
- Power needed to make return propellant—and keep it cold—is a driver for surface power
 - Eliminating ISRU saves power (but not much), and it won't save landed mass
- There are better ways to reduce power mass
 - Breaking the stationary power source up into multiple, smaller packages not only saves mass, it improves operational flexibility, increases exploration range, and supports staged build-up and relocation of surface assets
 - There are also disadvantages that would have to be mitigated
- This type of application requires unique power system features that may not be necessary for other applications of this technology
- Choice between a single large reactor vs. several smaller reactors is an Agency-level decision based on factors beyond the scope of this study

This exercise was not intended to recommend a particular concept. Final decisions must weigh programmatic considerations. Mars human system architectures may deviate from current concepts and significantly alter power system needs.





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Questions About the Kilopower Concept?

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Solar vs. Fission Surface Power for Mars

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- 2009: NASA's Design Reference Architecture 5.0 baselined fission surface power for a crewed Mars mission
 - Two landers to one site, then two more landers to a different site
 - Solar power did not trade as well as fission power for mass
 - Fission development costs would be shared with the Constellation Program's lunar surface mission, making fission more attractive
- 2016: NASA revisited the solar vs. fission trade based on new information
 - Paradigm shift to Evolvable Mars Campaign
 - ✓ Multiple landers to the same site, allowing infrastructure build-up
 - Technology advances since the original studies were performed
 - Kilopower fission system, higher density batteries, more efficient solar arrays



COMPASS Team

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The new study was performed by the NASA Glenn Research Center's Collaborative Modelling for Parametric Assessment of Space Systems (COMPASS) Team

NASA Glenn Research Center

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COMPASS COMPASS



Making Mars More Affordable Utilize Martian Resources

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- Mars Ascent Vehicle arrives on Mars with empty Liquid Oxygen propellant tanks
- Fission- or solar-powered In Situ Resource Utilization extracts carbon dioxide from the Martian atmosphere
 - ISRU processes the CO₂ into LOX propellant
 - Paired with Methane brought from Earth
- Once LOX tanks are confirmed full, the crew lands on Mars
 - ISRU production is suspended, and the power system is switched over to crew life support functions
 - Some power needed for cryogenic propellant conditioning
- For solar-power system, dust storm disruption up to 120 sols is assumed

Mars Ascent Vehicle LOX Liquid Oxygen ISRU In Situ Resource Utilization

Acronyms

MAV





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Study Approach

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kWe

kilowatt

(electric)

Pre-cursor demonstration mission

- Primarily an Entry-Descent-Landing demonstrator near the equator
- ISRU payload to demonstrate LOX production from atmosphere, at 1/5 scale of crewed mission
- Compare 10 kilowatt electric (kWe) Kilopower fission system to 3 solar options:
 - A. Daylight-only ISRU operation
 - B. Around-the-clock ISRU production (battery reserves for night)
 - C. Daylight-only, but 2x production rate to make up for night period

Crewed Surface Mission

- Cargo Phase: Around-the-clock production 23 t of LOX in 420 Earth days
- Crew Phase: Crew support functions + MAV keep alive and propellant conditioning (no ISRU)
- Evaluated the same crewed mission to two different landing sites
 - ✓ Jezero Crater, located 18.9° North
 - ✓ Columbus Crater, located 29.5° South
- Kilopower fission vs. [solar + batteries] vs. [solar + fuel cell]





ISRU Demonstrator

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Assumptions Demonstrator Mission

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- Land at Opportunity rover site at Meridiani (~2° south)
 - Benefit of Opportunity's 12 years of actual solar array performance data, favorable night durations, and minimal seasonal variations
- Mars environment based on Opportunity data
 - Assumed one dust storm, 120 days in duration, maximum wind 20 m/s
 - Optical depth varies from 1.0 (clear skies) to 5.0 (dust storm)
 - Opportunity data: dust scatters light, so diffuse light during a storm is ~30-40% of direct light on a clear day
- Average of 12 hours sunlight per sol
 - But assume 10 hours/sol ISRU operation to allow for system warm-up



Dust storm time lapse as viewed by Opportunity



Fission Power Concept Demonstrator Mission

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- ISRU system sized for 0.45 kg/hr LOX production with a goal of 4,500 kg
 - LOX tank only sized for 1,500 kg, with the balance vented overboard
- 10 kWe Kilopower unit providing 6.45 kWe (6.52 kWe at night)
 - Fixed, conical upper radiator requiring no deployment
 - 1,754 kg including 15% mass growth allowance and radiation shield sized to reduce crew exposure to <3 mR/hr within 500 m
- 6 m diameter landed footprint x 5.14 m dia. height
 - 2.61 m center of gravity height
 - 106 W keep-live power after landing
- 2,751 kg total payload mass
 - Including growth allowance

Kilopower is oversized for this application But it's an opportunity to demo crew mission technology



Solar Power Concepts **Demonstrator Mission**

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4 x 7.5 m

+ 2x ISRU

- Same ISRU assumptions as for fission power case
- 120V Orbital ATK UltraFlex[™] arrays or equivalent
 - Inverted Metamorphic Multi-junction solar cells of 33% conversion efficiency
 - Measured at Earth distance solar flux, 28°C, beginning of life
 - 45° Gimbal for sun tracking and dust removal
- Panasonic cell type Lithium-ion batteries
 - 60% depth of discharge, 165 Watt-hours per kilogram





Solar vs. Fission Comparison Demonstrator Mission

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Closest "apples to apples" comparison				
Option	Solar 1A: 1/5 rate Daytime Only	Solar 1B: 1/5 rate Around the Clock	Solar 1C: 2/5 Rate Daytime Only	Fission: 1/5 Rate Around the Clock Fission Power
Total Payload Mass (including growth)	1,128 kg	2,425 kg	1,531 kg	2,751 kg
Electrical System Mass	455 kg	1,733 kg	639 kg	1,804 kg
ISRU Subsystem Mass	192 kg	192 kg	335 kg	192 kg
Power	~8 kW Daylight	~8 kW Continuous (with 16 kW of arrays)	~16 kW Daylight	~7 kW Continuous
Solar Arrays	4 each x 5.6 m diameter	4 each x 7.5 m dia.	4 each x 7.5 m diameter	None
Night Production?	No	Yes	No	Yes
LOX Production	4.5 kg/sol	10.8 kg/sol	9.0 kg/sol	10.8 kg/sol
Time to Produce 4,400 kg LOX, including 120- Day Dust Storm Outage	1,098 sols	527 sols	609 sols	407 sols
ISRU On/Off Cycles	1,098	<5	609	<5

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Observations *Demonstrator Mission*

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- Daytime-only solar power concept offers lowest landed mass
 - High number of ISRU on/off cycles could pose reliability issues
- Fission power was at a mass disadvantage in this trade
 - 10 kW Kilopower was oversized for 7 kW application, plus mass included crew protection shield that wasn't necessary for demo
 - Equatorial site represents minimum solar power mass
 - Expect higher mass at other latitudes
- All options fit comfortably within allowable payload limits
 - So mass alone is unlikely to drive a decision for an equatorial mission
 - Power system selection probably depends on other factors
 - Technology investment strategies, program budgets, and risk mitigation needs for later crewed missions
- Demonstrator mission solar power hardware costs are ~\$100M less than comparable fission power hardware costs
 - Does not include technology development through Technology Readiness Level 6





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Crewed Mission

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Mission Concept of Operations Crewed Mission

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r	Expedition 1 Four Landers	Expedition 2+ Three Landers per Expedition		
	1. Power System + Cargo	1. MAV + ISRU		
Cargo Phase	2. MAV + ISRU	2. Cargo and Consumables		
	3. Mixed Cargo and Consumables			
Crew Phase	4. Habitat Module + Crew	3. Habitat Module + Crew		

- Landers located no more than 1 km from each other
- Fission: Kilopower units remain together on/near the first lander
 - Robotic connections to subsequent landers
 - Power can be disconnected when a lander is no longer in use
- Solar: arrays on every lander, at least through Exp 3
 - All landers connected into a power grid
 - Remain connected even if lander is no longer active



Surface Power Needs Crewed Mission

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ISRU: Produce 22,728 kg of LOX in 420 Earth days

	Peak I Neede	Power ed (W)	Keep-Alive Power Needed (W)		
Element	Cargo Phase	Crew Phase	Cargo Phase	Crew Phase	
ISRU	19,700	0	19,700	0	
MAV	6,655	6,655	6,655	6,655	
Surface Habitat	0	14,900	0	8,000	
*Science Laboratory	0	9,544	0	174	
Total	26,355	31,099	26,355	14,829	

*Optional element shown with all systems running. Assume power can be phased to stay below cargo ops total peak



Note that eliminating ISRU doesn't reduce overall surface power need



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Fission-Powered Option Crewed Mission

- Four each 10-kWe Kilopower units would provide up to 35 kWe continuous power for all mission phases at either hypothetical landing site
- Fission power generation mass is 9,154 kg
 - Includes one spare Kilopower and mass growth allowance
 - Not including power farm-to-lander Power Management and Distribution
- Up to 1,038 kg PMAD could be needed on the Lander 1, depending on whether Kilopowers are relocated and whether any other cargo requires 1,000 - 120 VDC conversion
 - Landers 2, 3 and 4 would each require 1 km spool of high voltage cabling, connectors, and voltage converters

Description	Lander	Lander	
Description	1	2, 3, 4	Expedition
Power Generation			1 Fission
50 kWe Kilopower	8,769	0	Power
Power Management			Generation
Stirling AC Cable	62.4	0	Total
Stirling Controller	322.4	0	
FISSION SYSTEM TOTAL	9,154	0	9,154 kg

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PMAD Power Management and Distribution

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Solar-Powered Option Jezero Crater Crewed Mission

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- Study team estimated that all four Expedition 1 landers would require four each 12 m diameter UltraFlex[™] arrays or equivalent
 - Deployed on a 9.1 m diameter lander would extend the overall footprint to ~33 m
 - With arrays in neutral position on a 2.66 high lander deck, overall height was ~9.69
 - Deploying arrays high minimizes interactions with surface or payloads
 - Gimbals help shed dust
 - Lander deck provides stable operating platform
 - ✓ Allows arrays to be brought on-line quickly
- Under nominal Jezero Crater conditions, around-theclock propellant production with the first two landers requires 34.2 kW during the day and 35 kW at night
 - During dust storm, power would be reduced to 10,985 W during the day and 11,728 W at night.
 - Once crew arrived, combined loads of the first four Expedition 1 landers were 31,915 W during nominal daytime operation and 26,790 W at night
 - Loads drop to 22,945 W during the day, and 24,060 W at night during a dust storm







Solar-Powered Option Jezero Crater- Expedition 1

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Description	Lander 1	Lander 2	Lander 3	Lander 4	
Electrical Power Subsystem	4,890	1,512	1,512	1,512	
Power Generation	1,321	1,321	1,321	1,321	Jezero
Lander Internal Power Management and Distribution	401	192	192	192	Crater Expedition
Energy Storage	3,168	0	0	0	1
Structures and Mechanisms	660	476	476	476	Solar
Secondary Structure	416	418	418	418	Generation
Mechanisms	244	59	59	59	and
Thermal Control (Non-Propellant)	61	45	45	45	Storage
Active Thermal Control	2.4	3.4	3.4	3.4	Total
Passive Thermal Control	41.8	42	42	42	
Semi-Passive Thermal Control	16.8	0	0	0	
SOLAR POWER SYSTEM	5,611	2,034	2,034	2,034	11,713 kg

Does *not* include lander-to-lander PMAD Mass grows to 12,679 kg at Columbus Crater

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Solar vs. Fission Comparison Crewed Mission

- <u>Mass</u>: Expedition 1 comparison doesn't tell the whole story
 - All fission power arrives with Expedition 1, but solar power performance doesn't catch up until Expedition 3
 - Extrapolate through 3 expeditions for apples-to-apples comparison
- Performance: comparable by Exp 3



Cumulative power generation/storage mass (kg)

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- <u>Robustness</u>: fission power is more tolerant of dust, but the distributed solar power network is more tolerant to cable damage
 - Allows quick post-landing power, but arrays on MAV lander will have to be removed before MAV departs
 - ✓ Additional risk for crew/robotics to handle large arrays close to the MAV
- <u>Service Life</u>: 12-year Kilopower service life is probably about the same as solar power's rechargeable battery life



Observations *Crewed Surface Mission*



- 50 kWe of fission power is ~20% less landed mass than 35 kW of solar power generation and storage for the 1st Expedition to Jezero Crater
 - Not including lander-to-lander PMAD for either option, which could add a metric ton per lander
 - All solar powered landers become part of an integrated network, so they have to remain cabled together, even after cargo has been unloaded
 - Fission system only needs to be cabled to landers with active surface payloads
 - Assumptions will alter the analysis: landing site, propellant production rate, time available to make propellant, dust storm duration, transmission voltage
- By the 3rd Crew Expedition, cumulative solar array mass is more than 2x fission power mass
 - But enough solar array area will have been accumulated to accommodate a 120-sol dust storm with little disruption
- Mass differential is greater at Columbus Crater landing site



Conclusions Solar vs. Fission Mars Surface Power

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- Solar-powered crew surface mission is more feasible under EMC than previous mission concepts
- Solar-powered crew surface mission is certainly possible, at least for some latitudes
 - Forward work to evaluate all landing sites of interest
- Advantages and Disadvantages



Colar: High technology readiness, lower cost, and quick to switch from on-board stored energy to surface power; but high mass penalty may limit landing site options, and higher risk during a storm



Fission: Reliable, lower mass for most landing sites, same mass regardless of site, season, day/night, or weather; but lower technology readiness and higher development cost

Either power system will require substantial technology development and flight hardware investment



Key Take Aways From the two combined papers



- No Mars surface power decisions have been made
- Estimated power needs fluctuate, depending on assumed mission concept and operations
 - Need better definition on surface elements, transmission losses, etc.
 - 40 kW is probably the right ball-park for a long-duration, 4-crew Mars outpost with science activity
- Surface power generation and storage is an important decision that warrants careful consideration
 - If we select a particular surface power technology first, it could limit landing site options or operations
 - Conversely, if we select a landing site first, it could drive us to a specific surface power solution

NASA'S JOURNEY TO

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Questions?



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