## Modeling the Schott ELZM Thermal Soak Test

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## Opto-thermal test of Zerodur Mirror







stage

## Test Measured Data at 250K

09/16/16 08:10:57





M1- Top Hole	249.9
M2 - North Hole	251.9
M3 - South Hole	250.0
M4 - 12:00	250.0
M5 - 10:00	250.6
M6 - 8:00	250.0
M7 - 6:00	250.5
M8 - 4:00	250.2
M9 - 2:00	250.3
M10- Top Edge	250.2
M11 - 8:00 Edge	249.8
M12 - 4:00 Edge	249.7
M13 - Top Front	250.2
M14 - 4:00 Front	250.0
M33 - 8:00 (w/M6)	250.0
M34 - 8:00 (w/M11)	250.2
M35 - 8:00 (w/M2)	250.2
M36 - 12:00 (w/M4)	249.8
M37 - 4:00 (w/M8)	250.0
M38 - 5:00	250.2
8420 7.00	250.2
W139 - 7:00	250.3
30 - South Pad	250.3
30 - South Pad 31 - Bottom Pad	250.3 250.5 250.6
30 - South Pad 31 - Bottom Pad 32 - North Pad	250.3 250.5 250.6 250.5
30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring	250.3 250.5 250.6 250.5 251.4
30 - South Pad 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3	250.3 250.5 250.6 250.5 251.4 250.5
M39 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2	250.3 250.5 250.6 250.5 251.4 250.5 250.5
M39 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.5 250.6
M39 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.5 250.6 250.8
139 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.8
139 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.8 250.5 250.4
133 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3 22 - Strut L2	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.8 250.8 250.4 250.4
M39 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3 22 - Strut L2 23 - Strut L3	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.8 250.5 250.4 250.4 250.4 250.5
M39 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3 22 - Strut L2 23 - Strut L3 24 - Strut L1	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.8 250.5 250.4 250.4 250.5 250.4 250.5 250.2
30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3 22 - Strut L2 23 - Strut L3 24 - Strut R2	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.4 250.4 250.4 250.5 250.4 250.2 250.2
10139 - 7:00 30 - South Pad 31 - Bottom Pad 32 - North Pad 15 - 12:00 Ring 16 - Delta_3 17 - Delta_2 18 - Top Bracket 19 - South Bracket 20 - North Bracket 21 - Strut R3 22 - Strut L3 24 - Strut L3 24 - Strut L1 25 - Strut R2 26 - Strut R1	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.4 250.4 250.4 250.4 250.4 250.4 250.5 250.2 250.6 250.3
M39 - 7:00        30 - South Pad        31 - Bottom Pad        32 - North Pad        15 - 12:00 Ring        16 - Delta_3        17 - Delta_2        18 - Top Bracket        19 - South Bracket        20 - North Bracket        21 - Strut R3        22 - Strut L2        23 - Strut L3        24 - Strut L1        25 - Strut R2        26 - Strut R1        27 - South Mount	250.3 250.5 250.6 250.5 251.4 250.5 250.5 250.6 250.8 250.4 250.4 250.4 250.4 250.4 250.4 250.5 250.2 250.2 250.6 250.3 250.7
M39 - 7:00        30 - South Pad        31 - Bottom Pad        32 - North Pad        15 - 12:00 Ring        16 - Delta_3        17 - Delta_2        18 - Top Bracket        29 - North Bracket        20 - North Bracket        21 - Strut R3        22 - Strut L2        23 - Strut L3        24 - Strut L1        25 - Strut R1        26 - Strut R1        27 - South Mount        28 - Bottom Mount	250.3 250.5 250.6 250.5 251.4 250.5 250.6 250.8 250.8 250.4 250.4 250.4 250.4 250.4 250.4 250.2 250.2 250.6 250.3 250.7 250.7
M39 - 7:00        30 - South Pad        31 - Bottom Pad        32 - North Pad        15 - 12:00 Ring        16 - Delta_3        17 - Detta_2        18 - Top Bracket        19 - South Bracket        20 - North Bracket        21 - Strut R3        22 - Strut L2        23 - Strut L3        24 - Strut R1        25 - Strut R1        26 - Strut R1        27 - South Mount        28 - Bottom Mount        29 - North Mount	250.3 250.5 250.6 250.5 251.4 250.5 250.6 250.8 250.8 250.4 250.4 250.4 250.4 250.4 250.4 250.2 250.2 250.6 250.3 250.7 250.7 250.7
33 - 7:00        30 - South Pad        31 - Bottom Pad        32 - North Pad        15 - 12:00 Ring        16 - Delta_3        17 - Delta_2        18 - Top Bracket        19 - South Bracket        20 - Horth Bracket        21 - Strut R3        22 - Strut L2        23 - Strut L3        24 - Strut R1        25 - Strut R1        26 - Strut R1        27 - South Mount        28 - Bottom Mount        40 - Delta_1	250.3 250.5 250.6 250.5 250.5 250.5 250.6 250.8 250.8 250.4 250.4 250.4 250.4 250.4 250.4 250.4 250.2 250.6 250.2 250.6 250.3 250.7 250.7 250.7 250.7

(Kelvin)

# **Error Sources**

- Error due to Thermal Gradients
  - Thermal gradients cause mirror to bend
  - Caused by non-zero CTE and gradients
- Error due to Mount Effects
  - Mirror mount not athermalized, but very compliant flexures
  - Hexapod legs grow and bend mirror
- Error due to CTE inhomogeneity
  - CTE gradients + isothermal temperature change have effect similar to thermal gradients
- Instrumentation Error





## Error due to Mount

- RMS SFE=0.81nm
- Likely sources of error:
  - Incorrect material properties



### The test was sub-aperture and only the area enclosed in the circle was measured



SigFit 21.10.2016, 14:40:33, DISLIN 10.6 Mount-Effect

## Error due to Thermal Gradients

- RMS SFE=1.28nm
- Likely sources of error:
  - Different temperature distribution
  - CTE(250K) of this
    Zerodur mirror



## Error due to CTE Inhomogeneity



## Error due to CTE Inhomogeneity

- RMS SFE=8.75nm
- Likely sources of error:
  - Incorrect "randomly generated" CTE inhomogeneity shape
  - Incorrect CTE
    inhomogeneity P-V
    (assumed 10ppb/K)





## Surface Figure Error Budget



### CTE Inhomogeneity + Bulk Temperature Change



### Mirror Temperature Gradient + CTE



### Mount Stiffness and CTE + Bulk Temperature Change

Total SFE	Inhomogeneity SFE	<b>Gradient SFE</b>	<b>Mount SFE</b>
(nm)	(nm)	(nm)	(nm)
21.45	21.4	1.28	0.81

Disclaimer: some material properties were unknown and assumed; large uncertainty in epoxy properties.



## 294 to 250



#### A Prior Analysis Results



### Thermal Gradients\* (1.28 nm RMS)



### Mount Effects (0.81 nm RMS)



Inhomogeneity\*\* (21.4 nm RMS)

\*Exact temperature distribution could not be known in advance. CTE(T) was not known in advance (0.02ppm/K assumed at all temperatures)

\*\*CTE Inhomogeneity was not known a priori. A random CTE map was generated that had a 10ppb/K peak to valley.

### Test Results



#### Conclusion

Analysis can match measured SFE by adjusting the assumed CTE inhomogeneity to a new CTE inhomogeneity that is roughly 5ppb/K peak to valley. This is within the range of measured Zerodur CTE inhomogeneity peak to valleys.

### 9.5 nm RMS SFE



### 8.7 nm RMS SFE

### 13.1 nm RMS SFE











# Generated Multiple Homogeneities 🔊

## 294 to 250



### New Homogeneity\* (9.55 nm RMS)

\*CTE Inhomogeneities randomly generated until one matched. P-V homogeneity changed to 5 ppb/K.







#### Measured SFE (9.4 nm RMS)

#### Conclusion

PV: 194.1 nm

RMS: 9.426 nm

Astig: 17.67 nm, -1.308E+06 L

- A 5 ppb/K peak-to-valley inhomogeneity produced 9.55nm RMS of SFE and an root-sum-squared SFE estimate of 9.6nm RMS.
- Zerodur boules have been measured to have a 5 ppb/K peak-to-valley CTE inhomogeneity, therefore, 5ppb/K peak-to-valley inhomogeneity is reasonable.
- Further investigation will match test results to an even greater extend.