# On the Development of a New Nonequilibrium Chemistry Model for Mars Entry

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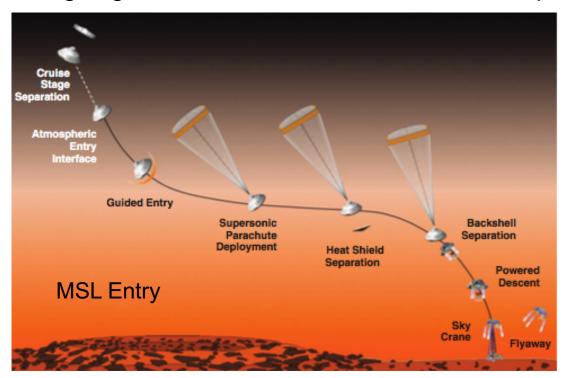
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#### **Motivation**



- NASA has been embarked on a program of scientific exploration of Mars by landing increasingly larger and heavier payloads
  - Prediction of thermal load used to determine TPS requirements
  - Testing in ground facilities and CFD simulations play critical roles



Nonequilibrium chemistry model currently in use is 20+ years old and based on mostly 35+ year old experiments

We are critically examining this "legacy" model and developing a new model based on computational chemistry and physics

Our objective is to reduce the uncertainty in predictions of thermal loads for Mars entry

#### **Outline**



- Legacy nonequilibrium chemistry model
- Computational approach for developing a new model
- Rate Coefficients
  - Chemical rections for Mars entry
  - Uncertainty Quantification
  - CO dissociation
- Comparison with other models
  - Convective heating
  - Radiative Flux
- Next steps in developing the nonequilibrium chemistry model
- Conclusions

## **Legacy Mars Chemistry Model**



- Nonequilibrium between translational and internal energy modes of the flowfield species in the bow shock layer
  - After shock wave gas is compressed and heated
  - Two temperatures (T =  $T_r$  and  $T_v$  =  $T_{el-st}$ )
  - First order relaxation equation describes evolution of  $T_v$  from the shock to thermal equilibrium ( $T_v = T$ ); governed by relaxation time  $\tau_v$
  - Dissociation reactions modeled by Arrhenius rate expression using an average temperature  $T_{av} = (T \cdot T_v)^{1/2}$
  - Rate coefficient parameters originally taken from 1960's-70's shock tube experiments, but subjected to empirical adjustment
- Developed by Chul Park at NASA Ames 1986-1992 (Park et al, JTHT 8, 9-23 (1994))
- Recent modification of parameters by Johnston and Brandis (JSQRT 149, 303-317 (2014))

## Mars Entry: What Collisional Processes are Important?



- Mars atmosphere is ~96% CO<sub>2</sub>, ~2% N<sub>2</sub> ~2% Ar
- Dissociation
  - CO<sub>2</sub> (5eV) very fast and nearly complete
  - CO (11 eV) slow, rate determining process
- Heterogeneous exchange reactions provide lower energy (i.e. faster) routes for CO<sub>2</sub> and CO dissociation

- 
$$CO_2 + O \rightarrow CO + O_2$$

- CO + O 
$$\rightarrow$$
 C + O<sub>2</sub>

- 
$$CO + N \rightarrow O + CN$$

- CO + C 
$$\rightarrow$$
 O + C<sub>2</sub>

For Mars entry at 6-8 km/s, the rate of CO dissociation is critical because CO 4<sup>th</sup> positive emission is the dominant source of radiative heating

## New Paradigm for a Nonequilibrium Chemistry Model



- Accurate quantum mechanics calculations to quantify interaction energy between atoms and molecules
  - Potential Energy Surface (PES) obtained from solution of Schrödinger equation
  - Repeated for many geometric arrangements of the atoms (for n atoms there are 3n-6 degrees of freedom)
  - Goal is ≤ ± 5 kJ/mol relative accuracy (~0.05 eV, ~400 cm<sup>-1</sup>)
- Classical mechanics simulations of heavy particle collisions to compute collision cross sections and rate coefficients
  - Compute trajectories of many individual collisions (Quasi-Classical Trajectory or QCT calculation)
  - Monte Carlo sampling used reproduce random or thermal collisional distributions

#### This strategy should yield rate coefficients accurate to ±20%

(Ref: Jaffe et al. "First principles calculation of heavy particle rate coefficients" in "Hypersonic nonequilibrium Flows: Fundamentals and Recent Advances", E. Josyula, ed, AIAA 2015)

## Important Chemical Reactions for Mars Entry The imag



	Reaction	Experiment	PES	QCT rate coeff.
D1	$CO_2$ + M $\rightarrow$ CO + O + M M = $CO_2$ , $N_2$ , $CO$ , $O$	Shocktube expts 1968-74 & 1984		
D2	$CO + M \rightarrow C + O + M$ M = CO, O	Shocktube expts 1968-74 & 1984	NASA Ames 2016	NASA Ames 2016
<b>*</b> D3	$N_2 + M \rightarrow N + N + M$ $M = N_2, N$	Shocktube expts 1964-74 & 1993	NASA Ames 2010 U. Minnesota 2013	NASA Ames 2010-16 U. Minn. 2013-16
<b></b> ₩ D4	$O_2 + M \rightarrow O + O + M$ M = N <sub>2</sub> , CO, O	Expts 1960s, 84 Hanson 2016	Varandas 1988 Dawes 2011-13	Andrienko 2016
E1	$CO_2 + O \rightarrow CO + O_2$	Ibragimova 1991		
E2	$CO + O \rightarrow C + O_2$	Hanson 1991	NASA Ames 2016	NASA Ames 2016
<b>*</b> E3	$N_2 + O \rightarrow NO + N$	Michael 1992 Roth 1985	Sayos 2003-16	Sayos 2010-12 U. Minn 2016
<b></b> ₩E4	$NO + O \rightarrow O_2 + N$	Fontijn 1998	Sayos 2002	Sayos 2003
E5	$CO + N \rightarrow CN + O$		Nyman 2000-2008	
E6	$CO + N \rightarrow NO + C$		Nyman 2000-2008	
E7	$CN + O \rightarrow NO + C$	Roth 1990	Nyman 2000-2008	
E8	$CO + C \rightarrow C_2 + O$			

## **Uncertainty Quantification (UQ)**



- UQ used to identify critical reactions
  - Monte Carlo sensitivity analysis
    - 96 % CO<sub>2</sub>/4% N<sub>2</sub> (free stream at 0.25 torr and 300 K)
    - 1-d shock at 7.75 km/s
    - Random sampling of rate coefficient and vibrational relaxation parameters
  - Two criteria considered: sensitivity to CO  $4^{th}$  positive radiative intensity and sensitivity to attaining chemical equilibrium (T/T<sub>eq</sub> = 1.05)
- Repeated many times for statistical analysis
- Key reactions:

Reaction	Sensitivity to Radiative Flux	Sensitivity to Equilibration Time
CO + O → C + O + O	55%	48%
CO + CO → C + O + CO	25%	10%
$CN + O \rightarrow C + NO$	9%	24%
$CO + O \rightarrow C + O_2$	4%	8%

### **CO Dissociation**



- The radiative heat flux experienced by spacecraft entering the Martian atmosphere at 5-8 km/s is mostly due to the CO 4<sup>th</sup> positive band system ( $\lambda$  < 200 nm)
  - Radiative heating is therefore proportional to the mole fraction of CO in the bow shock layer
  - CFD-Radiative transport calculations using the T-T<sub>v</sub> model (legacy Mars chemistry model) predict greater radiance than observed in tests run in the Electric Arc Shock Tube (EAST) at Ames
  - Johnston and Brandis (JQSRT, 2014) scaled some of the rate coefficient parameters to force agreement between CFD and EAST for CO 4<sup>th</sup> positive
- Ab initio PESs have been computed for CO + Ar and CO + O and used in QCT calculations of CO dissociation rate coefficients (Schwenke et al., J Chem. Phys. submitted)
  - Experimental data for CO + Ar seem more reliable than for CO + O
  - Efficiency of different collision partners (M) for promoting dissociation has been expressed as ratio k(CO+M)/k(CO+Ar)

### Rate Coefficient Ratios for CO Dissociation



- Early experimental values (Baulch, based on pre-1972 shock tube experiments)
  - $k_{CO+CO}/k_{CO+Ar} = 1-2$   $k_{CO+O}/k_{CO+Ar} = 15$
- Park (1994) T-T<sub>v</sub> model
  - $k_{CO+CO}/k_{CO+Ar} = 10 k_{CO+O}/k_{CO+Ar} = 15$
- Johnston and Brandis (2014)
  - $k_{CO+CO}/k_{CO+Ar} = 10$   $k_{CO+O}/k_{CO+Ar} = 15$
  - $k_{CO+Ar(JB)}/k_{CO+Ar(Park)} = 5$
- Objectives of our QCT rate coefficient calculations:
  - Evaluate the accuracy of the experimental data used in the legacy model
  - Determine these rate coefficient ratios as a function of temperature
  - Study the importance of the exchange reactions in the shock layer

#### CO + Ar



# After nearly all of the CO<sub>2</sub> is dissociated, CO and O are the major species (with equal mole fraction)

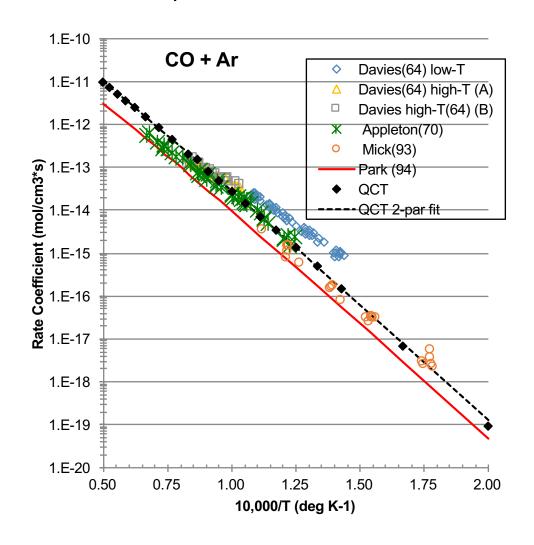
#### Experimental data

Davies (1964) CO + Ar, CO,O Appleton (1970) CO + Ar, CO, O Hanson (1974) CO + CO, O Mick & Roth (1993) CO + Ar, CO

Park (1994) T-T<sub>v</sub> model

NASA Ames (2014-2015) QCT

- Scatter in experimental data is small
- Very good agreement between QCT and Appleton and Mick and Roth expt.
- Fair to good agreement between QCT and Davies and Park (94)



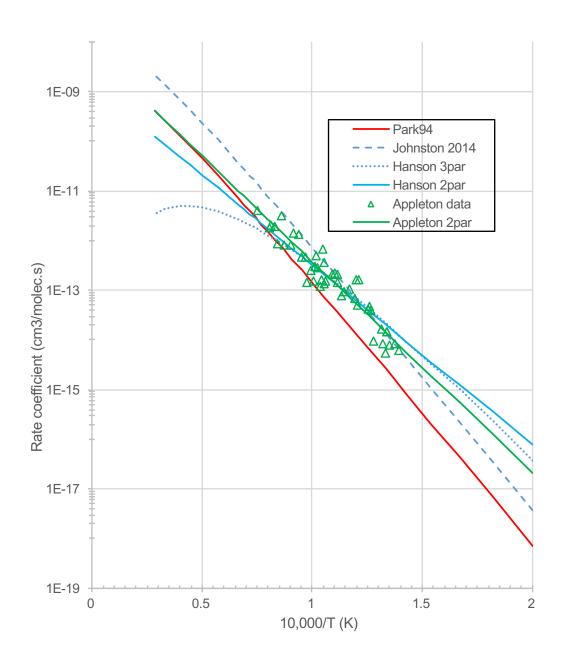
## $CO + O(^3P)$



- Three triplet PESs with equal statistical weight govern CO + O (<sup>3</sup>P) collisions
  - Lead to different non-linear CO<sub>2</sub> triplet electronic states (1 <sup>3</sup>A', 1 <sup>3</sup>A" and 2 <sup>3</sup>A") with O-C-O angle ~120°
  - 1 <sup>3</sup>A' has well depth ~75 kJ/mol (~0.8 eV); other states are more weakly bound
- Heterogeneous exchange reaction forming O<sub>2</sub> + C also possible on these PESs
  - Reaction is endothermic by 6.1 eV (low in comparison to the 11.2 eV dissociation energy of CO)
- All three PESs used for QCT calculations of CO dissociation and exchange reactions

## CO + O Rate Coefficients (experiment)

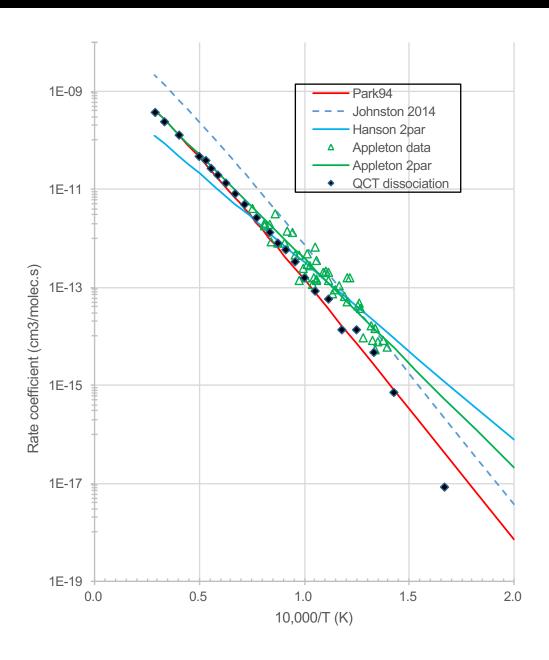




- Considerable scatter in the Appleton data
- Fairly good agreement between Appleton (8,000-15,000 K) and Hanson (5500-9000 K) data
- Hanson 3-parameter fit is not suitable for exptrapolation
- Park and Johnston recommendations bracket the experimental results

## CO + O Rate Coefficients (only dissociation)

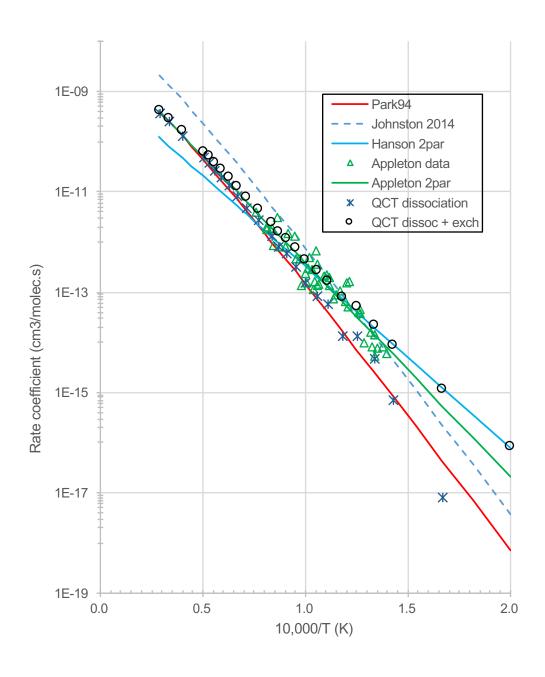




- Good agreement between QCT dissociation rate coefficient and Park model
- Agreement between QCT dissociation rate coefficient and expt is poor
- k<sub>CO+O</sub>/k<sub>CO</sub>+Ar ~3-5 for QCT not 15 as in Park model

## The imag

## CO + O Rate Coefficients (dissoc. + exchange)



- Addition of hetero exchange rate coeff to dissociation greatly improves agreement with expt (especially at lower temperatures
- Good agreement with Johnston scaled value
   ~8,000 K, but temperature dependence is quite different
- Exchange is the dominant CO removal process for T< 8000K

This exchange reaction was not previously thought to be important

## **Key Points for CO Dissociation**

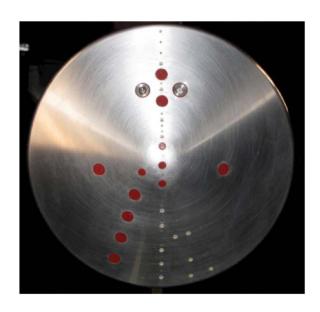


- Experimental data look quite good!
  - However, it is advantageous to use experimental data points (if available), not just Arrhenius expressions
- Heterogeneous exchange reaction provides an important pathway for CO removal, especially for T < 10,000 K</li>
  - Converts CO to O<sub>2</sub>, which is readily dissociated at these temperatures
  - Experimental CO dissociation rate coefficients implicitly include this reaction by having spuriously large dissociation rates and larger temperature exponents
  - When combined with dissociation, agreement betwee QCT and experimental results is excellent
- QCT rate coefficients needed for CO + CO to complete work on this set of reactions

### **Use in CFD Simulations**



- Used new rate coefficient data in simulations of convective heating for LENS XX shock tunnel tests
  - Pure CO<sub>2</sub> flow impinging on 12" diameter model
  - Flow enthalpies up to 43 MJ/kg
  - Compared Park94 model with new CO rate coefficients from present work to the Johnston modification of the original Park model in DPLR simulations



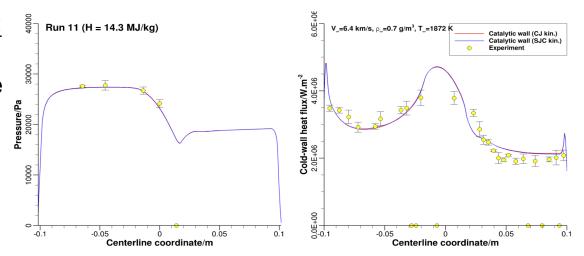


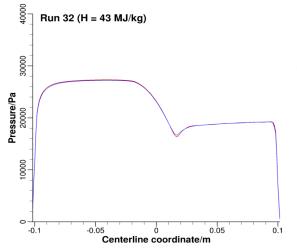
### Simulation vs LENS XX Test Data

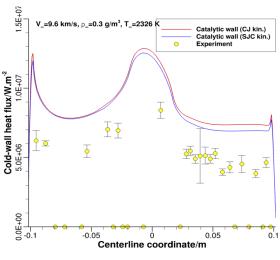


#### Moderate enthalpy (14.3 MJ/kg):

- Convective heat flux predictions for the models are barely distinguishable
- CFD and test data in good agreement
- This condition applicable to Mars entry







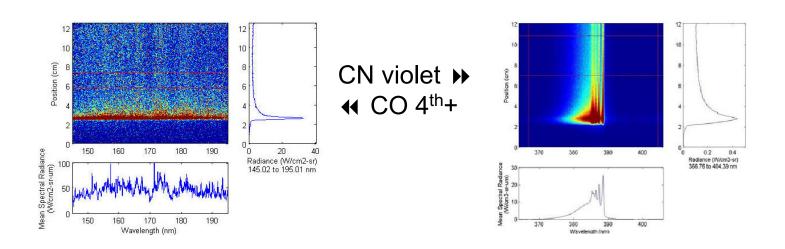
#### High enthalpy (43 MJ/kg):

- Heat flux prediction lower for new rate coefficients
- Agreement between CFD and test data is not good
- This condition is applicable to Venus entry

#### **Use in CFD Simulations**



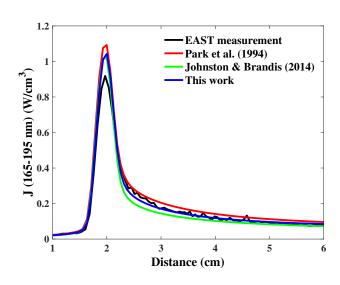
- Used new rate coefficient data in simulations of CO 4<sup>th</sup> positive and CN violet integrated intensities from EAST tests
  - 96% CO<sub>2</sub>/4% N<sub>2</sub> in Electric Arc Shock Tube at NASA Ames
  - Flow enthalpy up to 43 MJ/kg
  - Compared Park94 with new CO rate coefficients from present work with Johnston modification and the original Park model in LAURA-HARA simulations

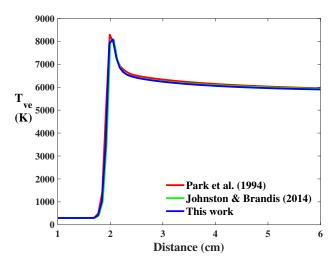


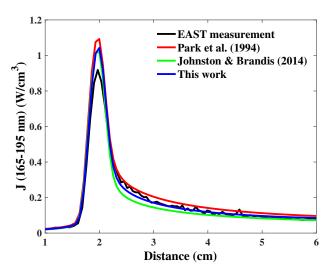
## Simulation vs EAST Test Data

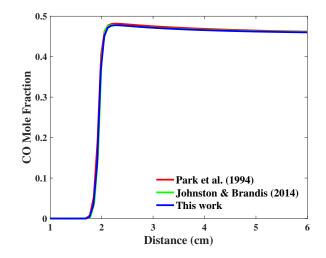


#### $P_0 = 0.25$ torr and shockspeed = 6.43 km/s





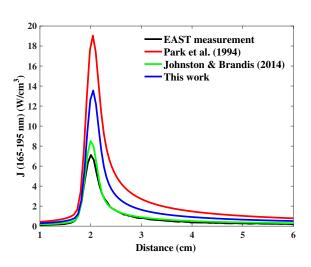


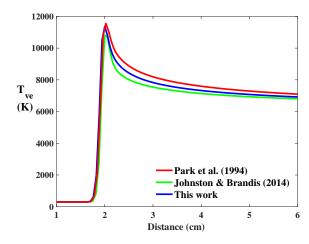


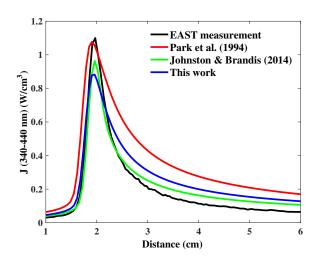
## **Simulation vs EAST Test Data**

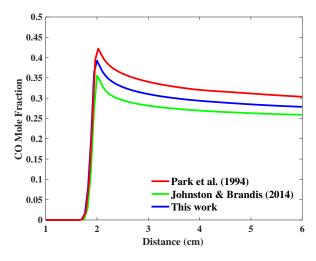


 $P_0 = 0.1$  torr and shockspeed = 7.98 km/s









## **On-going Work**



- Potential energy surfaces:
  - PES for CO + CO collisions to enable determination of rate coefficients for CO dissociation by CO + CO collisions
- Rate coefficients:
  - QCT calculations for CO + N reactions forming CN + O and NO + C
  - QCT calculations for O<sub>2</sub> dissociation and Zel'dovich reactions (N<sub>2</sub> + O and NO + O) using published PESs
- Analysis of quasi-steady state (QSS) models and internal energy relaxation ( $\tau_v$ ,  $\tau_{int}$ ) using coarse-grained QCT methods developed by Prof. Panesi at U. Illinois at Urbana-Champaign
- Examination of alternative multi-temperature models and other approaches to describing nonequilibrium flows

#### Conclusions



- The effort to create a new physics-based model for describing nonequilibrium phenomena in Mars entry flowfields is bearing fruit
- Potential energy surfaces and thermal rate coefficients for dissociation and exchange reactions have been computed for many of the important chemical reactions
  - Independent calculations for N<sub>2</sub> dissociation from two research groups show remarkable agreement
  - Rate coefficients for different dissociation reactions show limitations and successes in the older data from shock tube experiments
- Work is progressing toward creation of a data base of QCT rate coefficients for the complete set of heavy particle reactions for modeling Earth and Mars entry
  - Relaxation parameters  $(\tau_v)$  and thermochemical data (specific heats, enthalpies and entropies) are also being computed
- We are also examining alternatives to the T-T<sub>v</sub> model using coarsegrained QCT calculations

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  - Simone Venturi
  - Robyn Mcdonald

Mars tourism is coming!

