



# Additional Results of Glaze Icing Scaling in SLD Conditions

**Jen-Ching Tsao**  
**Ohio Aerospace Institute**

Supported by  
NASA Advanced Air Transport Technology Project

8<sup>th</sup> AIAA Atmospheric and Space Environments Conference  
13-17 June 2016, Washington, D.C.



# Outline

- Background
  - Progress on scaling method development
- Test Objective
- Test Description
- Ice Shape Comparisons
- Conclusion



# Modified Ruff Method

- Current recommended method for size scaling
  - In App-C & SLD



# Modified Ruff Method

- Current recommended method for size scaling
  - In App-C & SLD
  - Match modified inertia parameter  $K_0$  for scale  $MVD_S$

$$K_0 = \frac{1}{8} + \frac{\lambda}{\lambda_{Stokes}} \left( K - \frac{1}{8} \right)$$



# Modified Ruff Method

- Current recommended method for size scaling
  - In App-C & SLD
  - Match modified inertia parameter  $K_0$  for scale  $MVD_S$
  - Match stagnation-point freezing fraction  $n_0$ , with a scale  $LWC_S$  at user's choice, to find scale  $t_{tot,S}$

$$n_0 = \frac{c_{p,ws}}{\Lambda_f} \left( \varphi + \frac{\theta_0}{b_0} \right)$$



# Modified Ruff Method

- Current recommended method for size scaling
  - In App-C & SLD
  - Match modified inertia parameter for scale  $MVD_S$
  - Match stagnation-point freezing fraction  $n_0$ , with a scale  $LWC_S$  at user's choice, to find scale  $t_{tot,S}$
  - Match accumulation parameter  $A_c$  for scale  $\tau_S$

$$A_c = \frac{LWC V \tau}{d \rho_i}$$



# Modified Ruff Method

- Current recommended method for size scaling
  - In App-C & SLD
  - Match modified inertia parameter for scale  $MVD_S$
  - Match stagnation-point freezing fraction, with a scale  $LWC_S$  at user's choice, to find scale  $t_{tot,S}$
  - Match accumulation parameter for  $A_c$  for scale  $\tau_S$
  - Match Weber Number  $We_L (= \rho_w V^2 d / \sigma_{w/a})$  for scale  $V_S$

$$We_L = c, \Rightarrow V_S = V_R \left( \frac{d_R}{d_S} \right)^{1/2}$$



# Potential Method for SLD Glaze Icing

- Feo (2007) proposed a slightly different approach
  - Match film Weber Number for scale  $V_S$

$$We_f = \rho_w V_f^2 h_f / \sigma_{w/a}$$

$$We_f = c, \Rightarrow V_S = V_R \left( \frac{d_R}{d_S} \right)^{2/3}$$

- Match SLD film thickness correlation for scale  $LWC_S$

$$\frac{h_f}{d} = c, \Rightarrow LWC_S = LWC_R \left( \frac{d_R}{d_S} \right)^{-0.7}$$

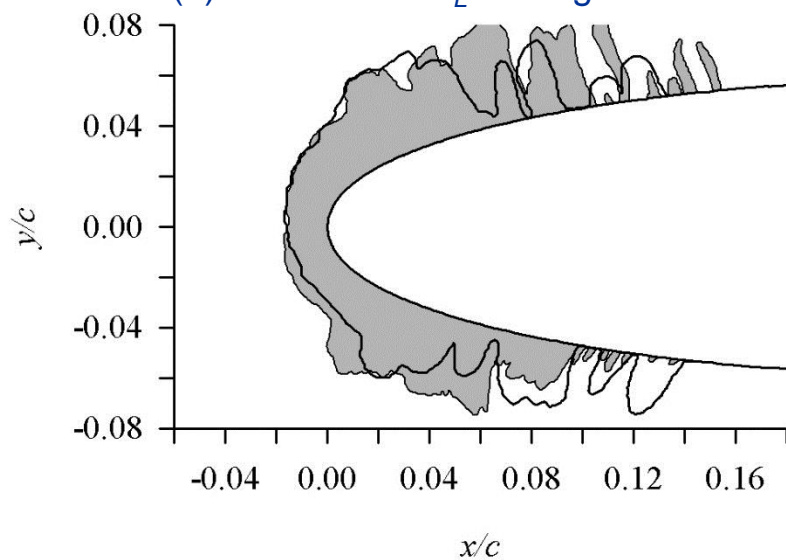




# Typical Scaling Results

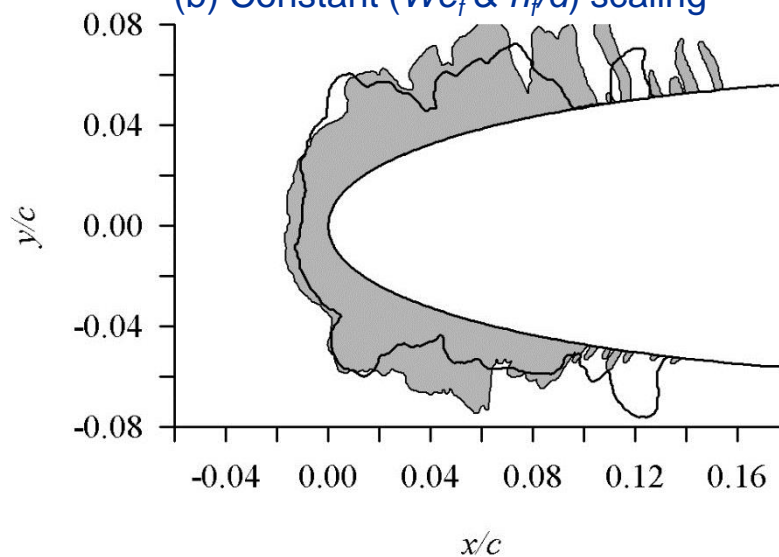
$$V_R = 100 \text{ kt}, MVD_R = 195 \mu\text{m}, n_0 = 0.3$$

(a) Constant  $We_L$  scaling.



—  $c = 91.4 \text{ cm}$ , 09-26-08 Run 1  
—  $c = 35.6 \text{ cm}$ , 09-30-08 Run 2

(b) Constant ( $We_f$  &  $h_f/d$ ) scaling



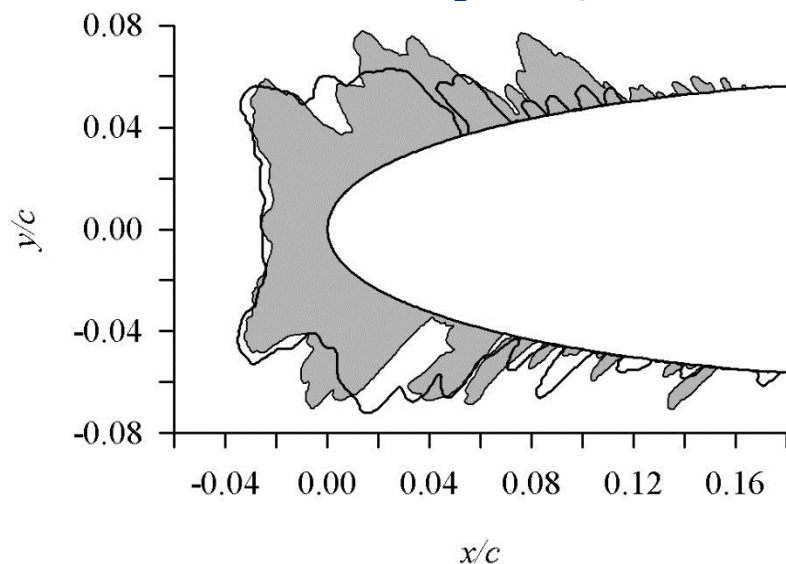
—  $c = 91.4 \text{ cm}$ , 09-26-08 Run 1  
—  $c = 35.6 \text{ cm}$ , 09-30-08 Run 1

		$t_{tot}$	$V$	$MVD$	$LWC$	$\tau$	$\beta_0$	$\beta_0 A_c$	$n_0$	$We_L$	$We_f$	$h_f/d$
		$^{\circ}\text{C}$	$\text{kt}$	$\mu\text{m}$	$\text{g/m}^3$	$\text{min}$	$\%$			$10^6$	$10^{-16}$	$10^{-9}$
—	Ref	-7.8	100	198	1.08	14.0	96.3	1.69	0.31	1.17	0.74	0.82
—	(a)	-2.9	159	87	0.57	6.6	96.2	1.73	0.31	1.16	0.86	1.04
—	(b)	-2.7	185	86	0.54	5.7	96.4	1.63	0.32	1.56	0.72	0.84

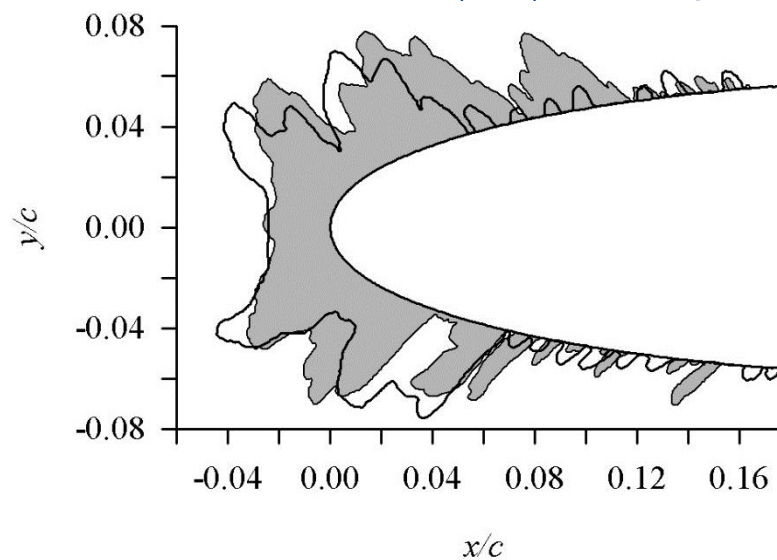
# Typical Scaling Results

$$V_R=100kt, MVD_R=195\mu m, n_0=0.5$$

(a) Constant  $We_L$  scaling.



(b) Constant ( $We_f$  &  $h_f/d$ ) scaling



—  $c = 91.4$  cm, 09-26-08 Run 3

—  $c = 35.6$  cm, 09-30-08 Run 5

—  $c = 91.4$  cm, 09-26-08 Run 3

—  $c = 35.6$  cm, 09-30-08 Run 6

		$t_{tot}$	$V$	$MVD$	$LWC$	$\tau$	$\beta_0$	$\beta_0 A_c$	$n_0$	$We_L$	$We_f$	$h_f/d$
		$^{\circ}C$	$kt$	$\mu m$	$g/m^3$	min	%			$10^6$	$10^{-16}$	$10^{-9}$
—	Ref	-14.1	100	198	1.07	14.0	96.3	1.69	0.52	1.18	0.74	0.81
—	(a)	-5.9	159	87	0.57	6.6	96.2	1.73	0.51	1.16	0.87	1.03
—	(b)	-6.0	186	86	0.54	5.7	96.4	1.64	0.53	1.58	0.72	0.83



# Test Objective

- Data for larger model size and size ratio
- Expanded SLD conditions in IRT
- Strong glaze icing regime



# Test Description

- NASA Glenn Icing Research Tunnel (IRT)
- 72-in and 21-in-Chord NACA 0012 (size ratio 3.4:1)
- $AOA = 0^\circ$
- $n_0 = 0.2, 0.3$
- Reference MVD's –  $85\ \mu\text{m}$  and  $170\ \mu\text{m}$
- Reference Velocities – 100 kt and 130 kt

# NACA 0012 Test Models in IRT



reference model (72")



scale model (21")



# Ice Shape Photographs

(a) reference



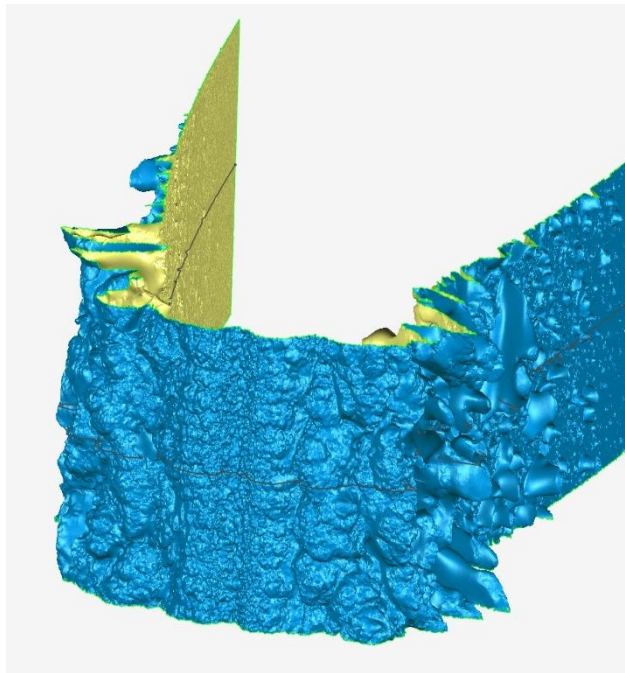
(b) scale



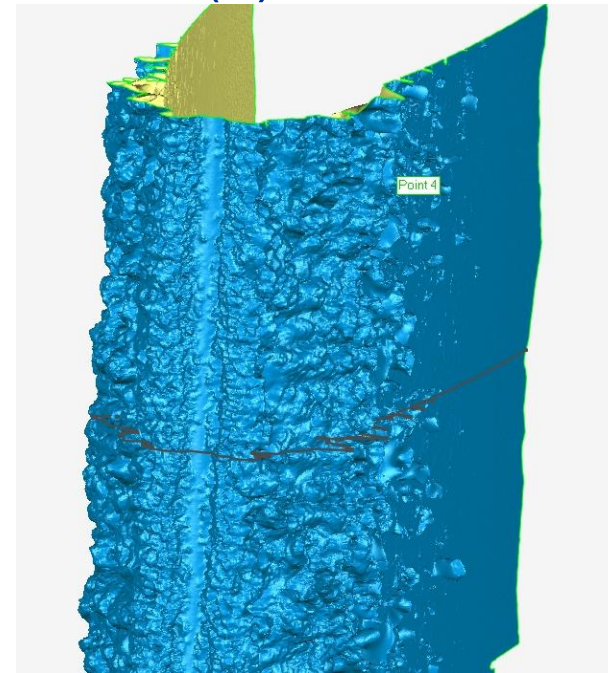
Date/Run	$c$ in	$t_{tot}$ $^{\circ}C$	$V$ kt	$MVD$ $\mu m$	$LWC$ $g/m^3$	$t$ min	$b_o$ %	$A_c$	$b_o A_c$	$n_o$	$We_L$ $10^6$
(a) 12-1-14/3	72	-6.0	99	84	1.2	23.2	82.9	1.61	1.33	0.20	2.30
(b) 1-19-16/6	21	-2.7	184	31	1.0	4.4	83.2	1.62	1.35	0.21	2.33

# 3-D Scanned Ice Shapes

(a) reference



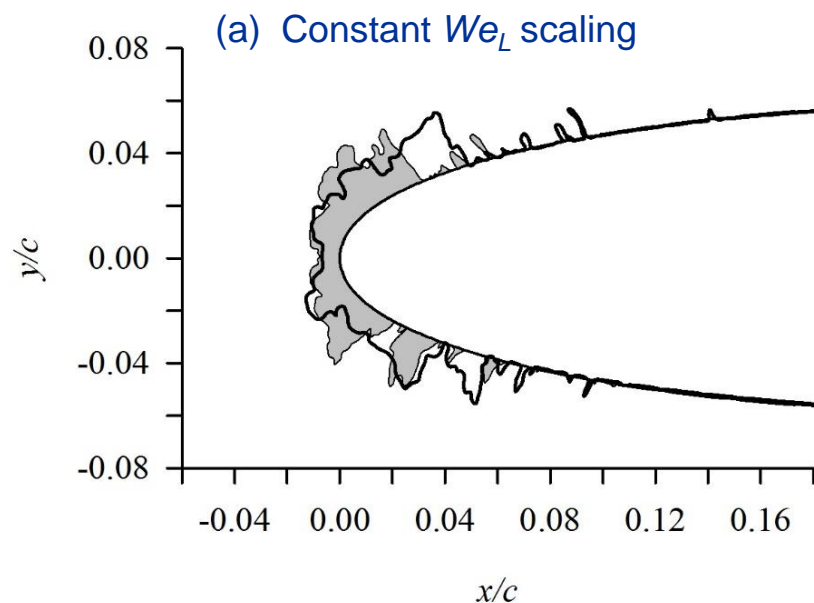
(b) scale



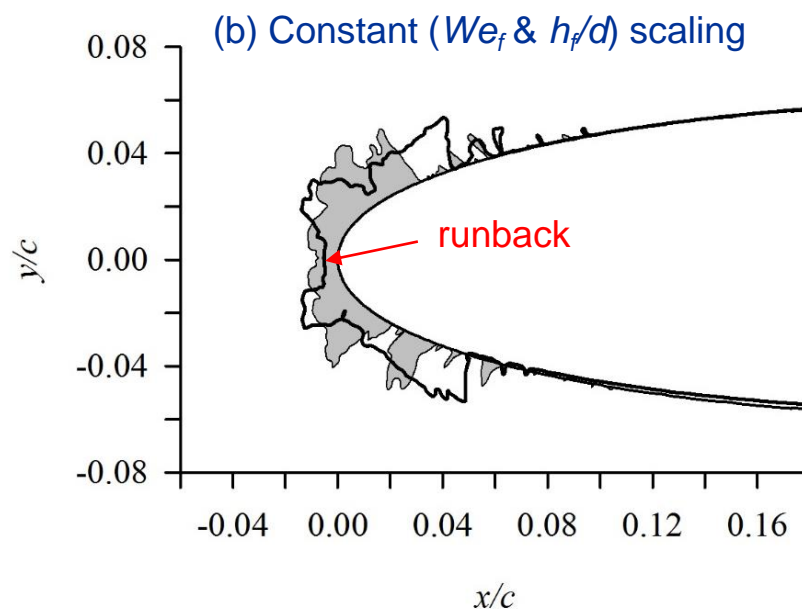
Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g}/\text{m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$
(a) 12-1-14/3	72	-6.0	99	84	1.2	23.2	82.9	1.61	1.33	0.20	2.30
(b) 1-19-16/6	21	-2.7	184	31	1.0	4.4	83.2	1.62	1.35	0.21	2.33

# Ice Shapes Comparison (1)

$$V_R=100\text{kt}, MVD_R=85\mu\text{m}, n_0=0.2$$



—  $c = 72$  in, 12-01-14/03  
—  $c = 21$  in, 01-19-16/06



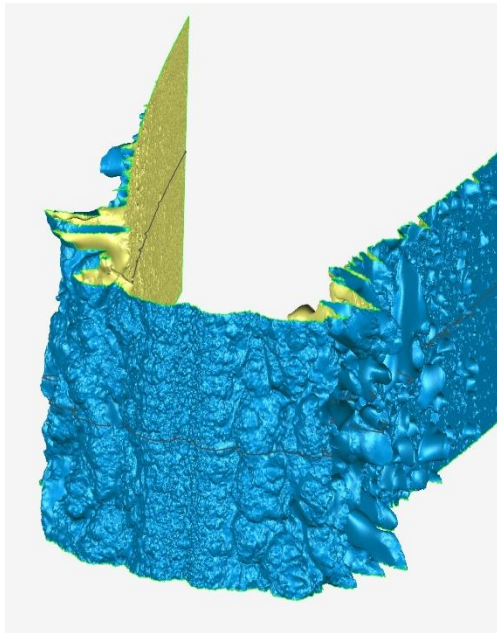
—  $c = 72$  in, 12-01-14/03  
—  $c = 21$  in, 01-19-16/01

Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g/m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-01-14/03	72	-6.0	99	84	1.2	23.2	82.9	1.61	1.33	0.20	2.30	2.68	0.80
01-19-16/06	21	-2.7	184	31	1.0	4.4	83.2	1.62	1.35	0.21	2.33	2.33	1.42
01-19-16/01	21	-0.2	225	28	0.54	6.3	83.2	1.66	1.38	0.20	3.55	2.81	0.83

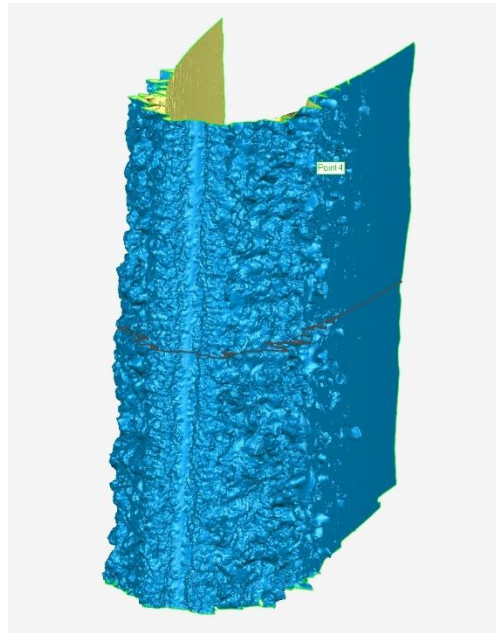


# 3-D Scanned Ice Shapes

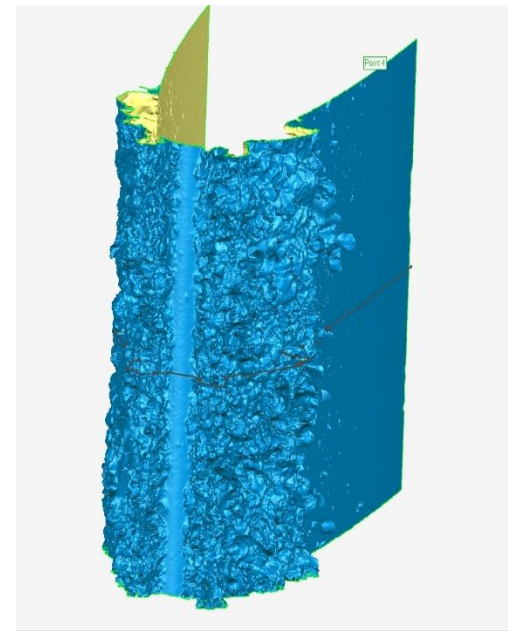
12-01-14/03



01-19-16/06



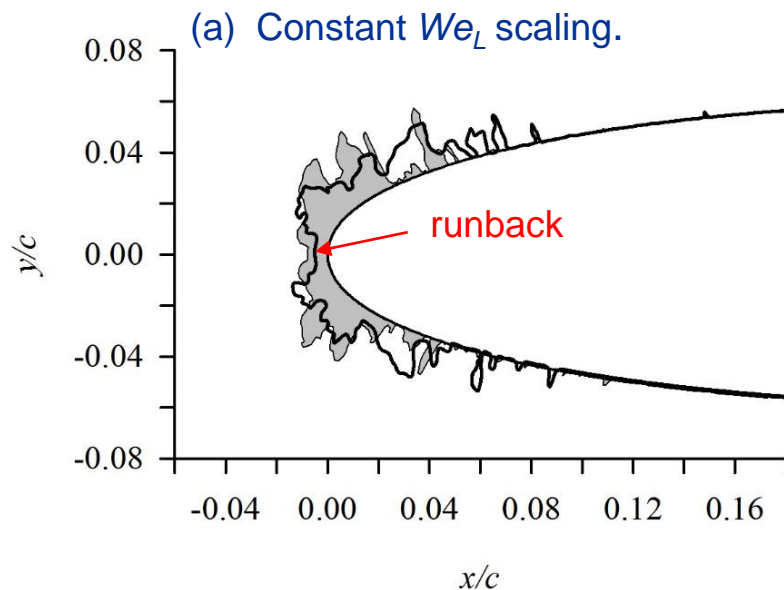
01-19-16/01



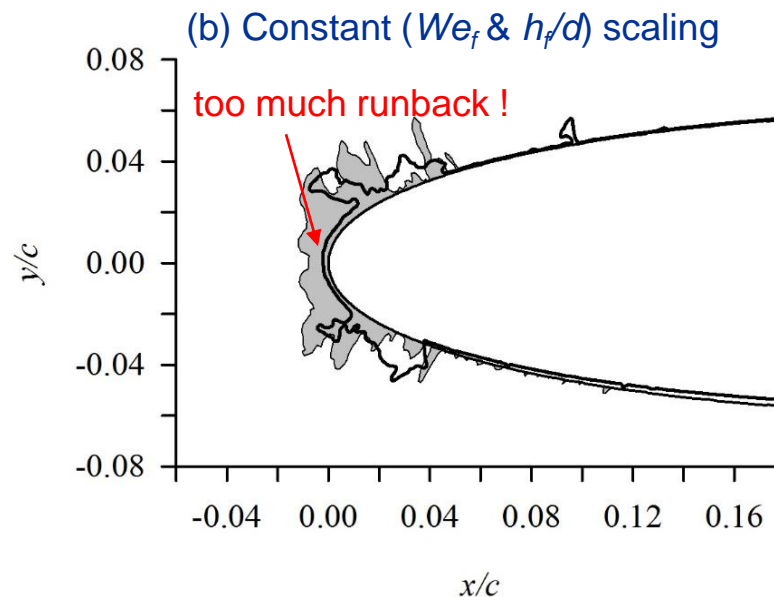
Date/Run	$c$ in	$t_{tot}$ °C	$V$ kt	$MVD$ $\mu m$	$LWC$ $g/m^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-01-14/03	72	-6.0	99	84	1.2	23.2	82.9	1.61	1.33	0.20	2.30	2.68	0.80
01-19-16/06	21	-2.7	184	31	1.0	4.4	83.2	1.62	1.35	0.21	2.33	2.33	1.42
01-19-16/01	21	-0.2	225	28	0.54	6.3	83.2	1.66	1.38	0.20	3.55	2.81	0.83

# Ice Shapes Comparison (2)

$$V_R=130\text{kt}, MVD_R=85\mu\text{m}, n_0=0.2$$



— c = 72 in, 12-01-14/02  
— c = 21 in, 01-20-16/01

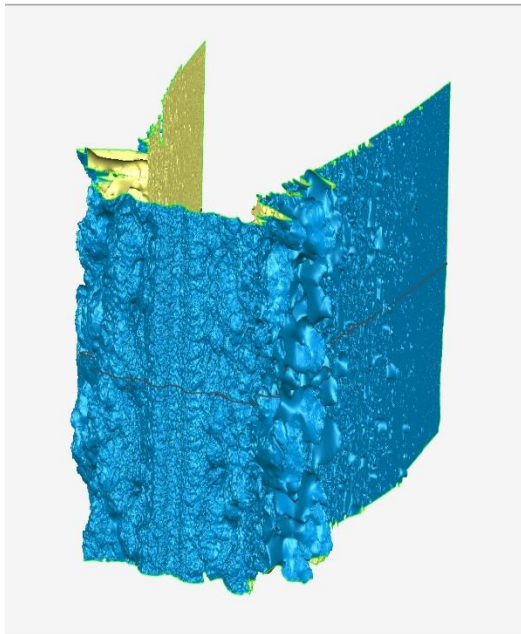


— c = 72 in, 12-01-14/02  
— c = 21 in, 01-26-16/01

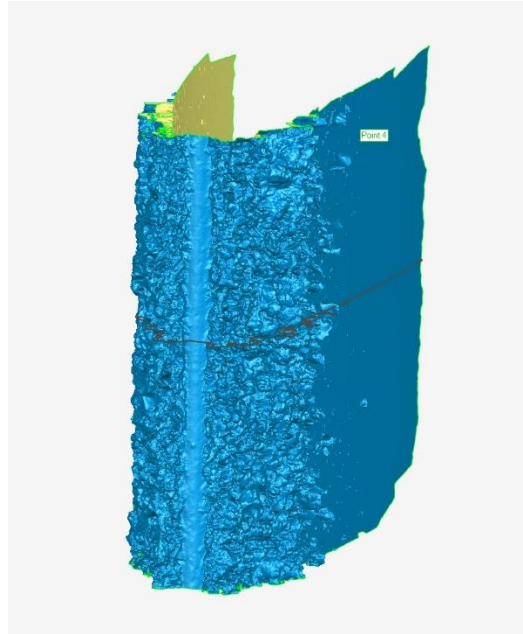
Date/Run	c in	$t_{tot}$ °C	V kt	MVD $\mu\text{m}$	LWC $\text{g/m}^3$	t min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-01-14/02	72	-5.3	129	85	0.95	22.1	84.7	1.57	1.33	0.21	3.91	1.52	0.51
01-20-16/01	21	-0.4	239	30	0.60	5.5	84.8	1.59	1.34	0.20	3.93	3.06	0.81
01-26-16/01	21	1.7	296	28	0.42	6.7	84.9	1.67	1.41	0.20	6.00	1.71	0.55

# 3-D Scanned Ice Shapes

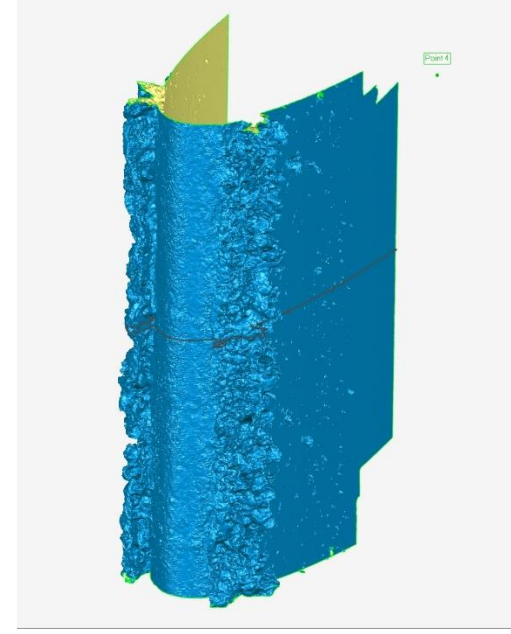
12-01-14/02



01-20-16/01



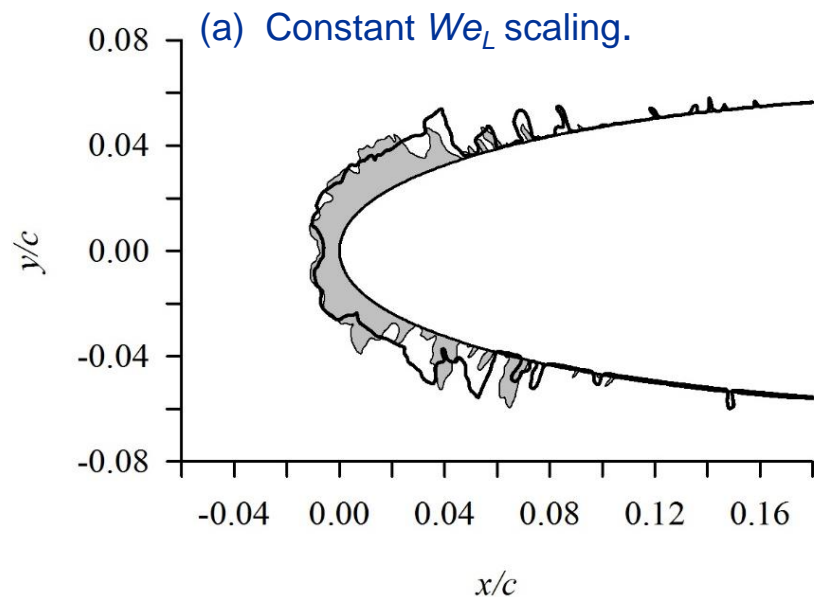
01-26-16/01



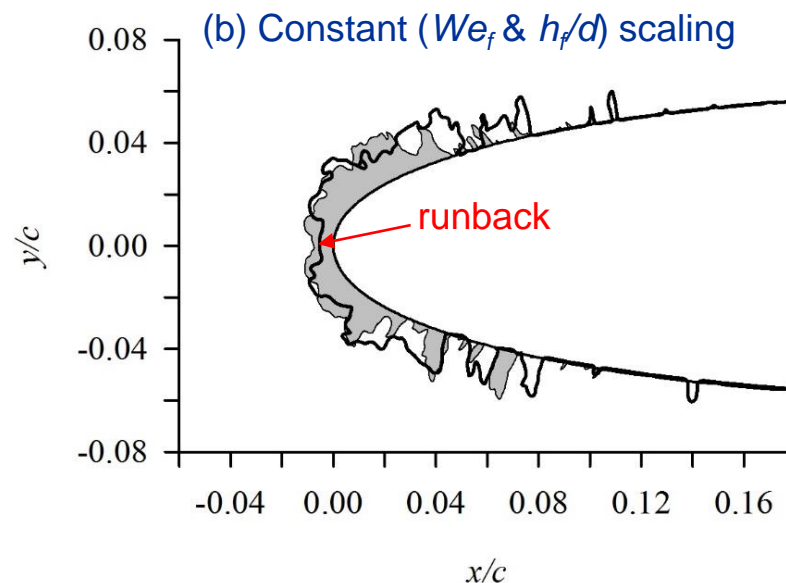
Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g}/\text{m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-01-14/02	72	-5.3	129	85	0.95	22.1	84.7	1.57	1.33	0.21	3.91	1.52	0.51
01-20-16/01	21	-0.4	239	30	0.60	5.5	84.8	1.59	1.34	0.20	3.93	3.06	0.81
01-26-16/01	21	1.7	296	28	0.42	6.7	84.9	1.67	1.41	0.20	6.00	1.71	0.55

# Ice Shapes Comparison (3)

$$V_R=100\text{kt}, MVD_R=170\mu\text{m}, n_0=0.2$$



—  $c = 72$  in, 12-02-14/04  
—  $c = 21$  in, 01-20-16/02



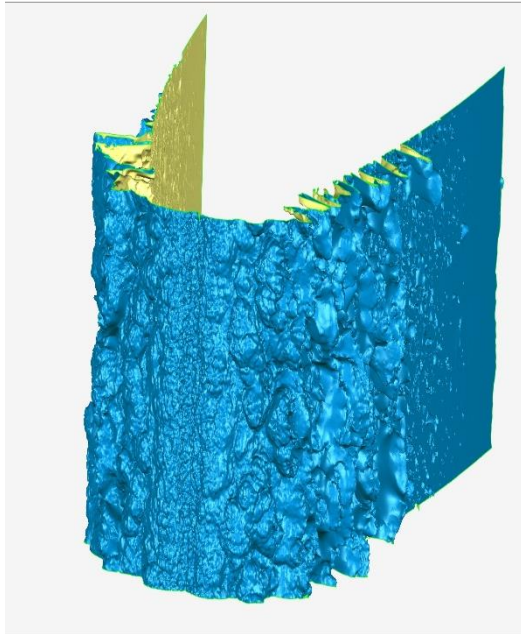
—  $c = 72$  in, 12-02-14/04  
—  $c = 21$  in, 01-19-16/03

Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g/m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-02-14/04	72	-6.9	99	171	1.35	18.6	92.3	1.45	1.34	0.20	2.30	1.10	0.60
01-20-16/02	21	-1.2	185	59	0.50	7.9	92.2	1.46	1.35	0.21	2.34	1.02	0.72
01-19-16/03	21	-0.8	226	58	0.56	5.7	92.6	1.44	1.33	0.20	3.52	1.08	0.60

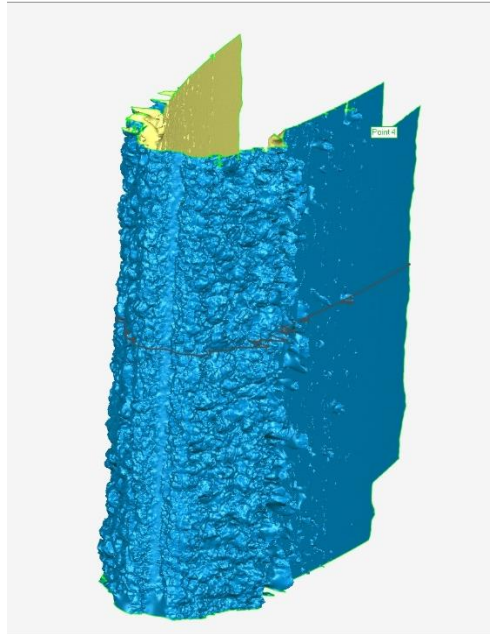


# 3-D Scanned Ice Shapes

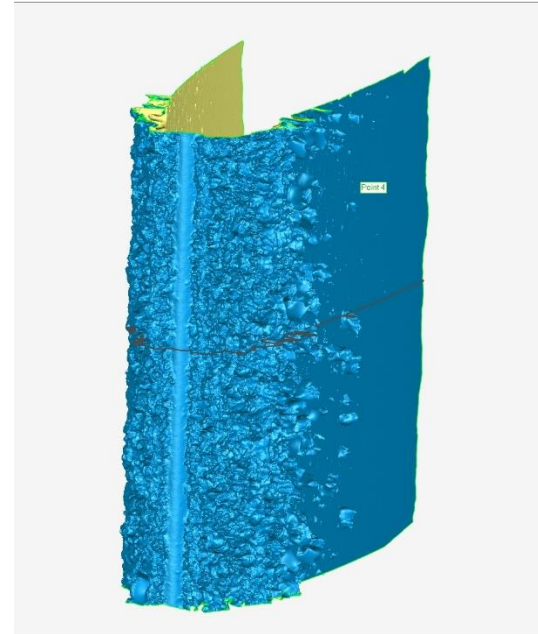
12-02-14/04



01-20-16/02



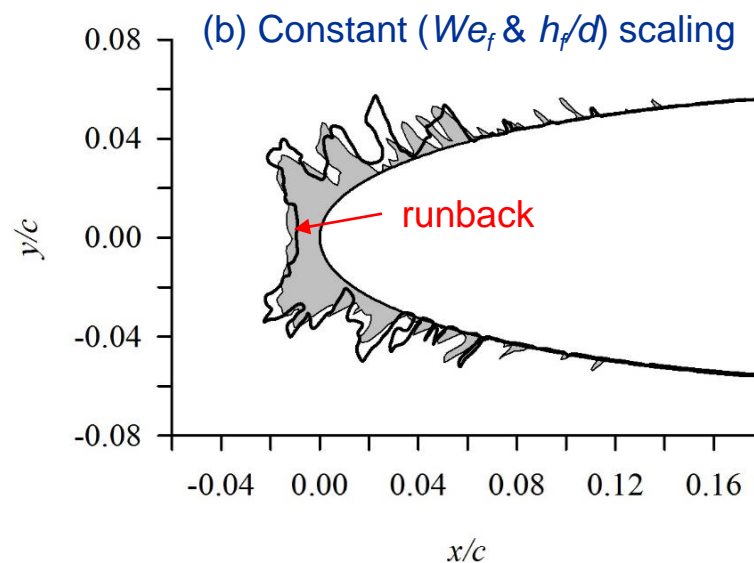
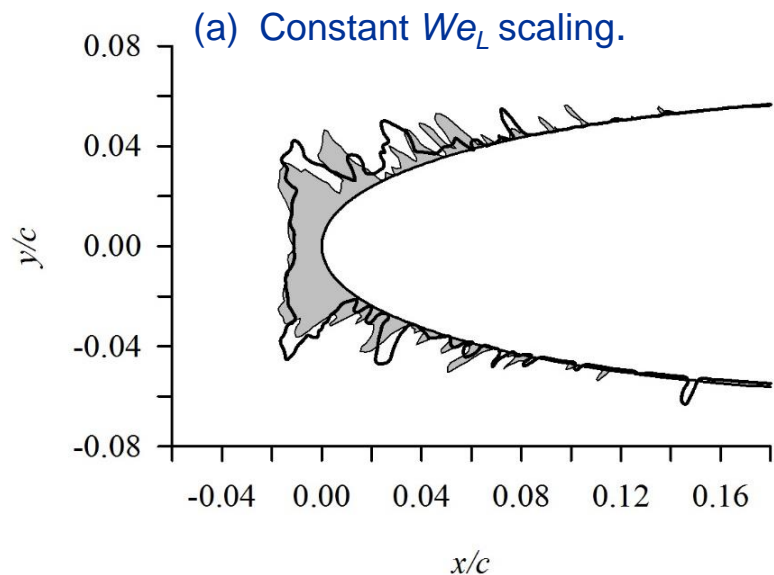
01-19-16/03



Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g}/\text{m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
12-02-14/04	72	-6.9	99	171	1.35	18.6	92.3	1.45	1.34	0.20	2.30	1.10	0.60
01-20-16/02	21	-1.2	185	59	0.50	7.9	92.2	1.46	1.35	0.21	2.34	1.02	0.72
01-19-16/03	21	-0.8	226	58	0.56	5.7	92.6	1.44	1.33	0.20	3.52	1.08	0.60

# Ice Shapes Comparison (4)

$$V_R=100\text{kt}, MVD_R=170\mu\text{m}, n_0=0.3$$



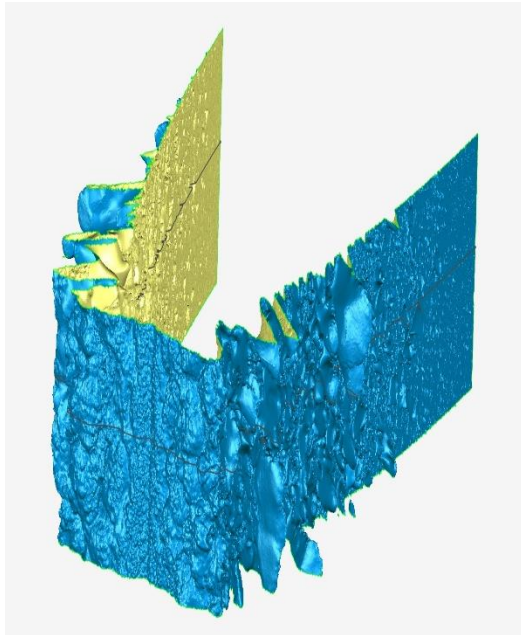
—  $c = 72$  in, 10-20-14/02  
—  $c = 21$  in, 01-16-15/03

—  $c = 72$  in, 10-20-14/02  
—  $c = 21$  in, 01-27-16/01

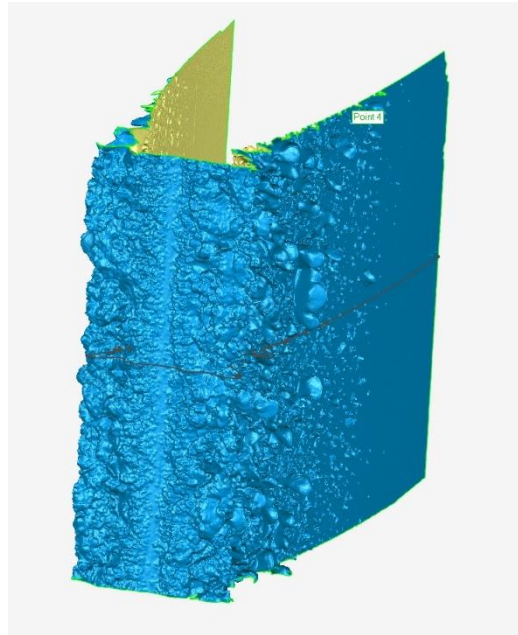
Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g/m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
10-20-14/02	72	-10.8	99	171	1.35	18.6	92.4	1.45	1.34	0.30	2.30	1.10	0.59
01-16-15/03	21	-3.1	185	59	0.50	7.3	92.2	1.35	1.25	0.33	2.35	1.01	0.72
01-27-16/01	21	-2.8	226	58	0.56	5.7	92.6	1.44	1.33	0.30	3.50	1.08	0.60

# 3-D Scanned Ice Shapes

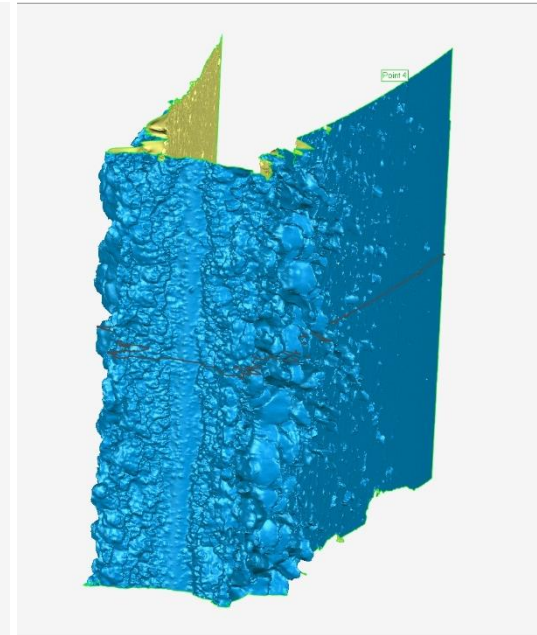
10-20-14/02



01-16-15/03



01-27-16/01



Date/Run	$c$ in	$t_{tot}$ $^{\circ}\text{C}$	$V$ kt	$MVD$ $\mu\text{m}$	$LWC$ $\text{g}/\text{m}^3$	$t$ min	$b_0$ %	$A_c$	$b_0 A_c$	$n_0$	$We_L$ $10^6$	$We_f$ $10^{-16}$	$h_f/d$ $10^{-9}$
10-20-14/02	72	-10.8	99	171	1.35	18.6	92.4	1.45	1.34	0.30	2.30	1.10	0.59
01-16-15/03	21	-3.1	185	59	0.50	7.3	92.2	1.35	1.25	0.33	2.35	1.01	0.72
01-27-16/01	21	-2.8	226	58	0.56	5.7	92.6	1.44	1.33	0.30	3.50	1.08	0.60



# Conclusion

- Modified Ruff method evaluated
- Feo method evaluated
- For limited testing at  $n_0 = 0.2, 0.3$  (strong glaze icing),
  - Better match of reference ice shapes with constant  $We_L$  provided  $t_{tot} < -2$  °C.
  - All still within the ice shape repeatability.
- Size of ice accretion, icing limits well simulated.
- Large feather simulations need improvement





# Acknowledgement

- Personal thanks to
  - Mr. Quentin Schwinn for the imaging & scan data process support.
  - IRT cloud cal team and the crew for their excellent support.