

**The Technology and Future of In-Situ  
Resource Utilization (ISRU)**

**The University of Central Florida**

**Mars Atmospheric Capture  
[and Processing]**

**Presented by Dr. Tony Muscatello**

**NASA Applied Chemistry  
Laboratory**

**Kennedy Space Center**

**February 27, 2017**



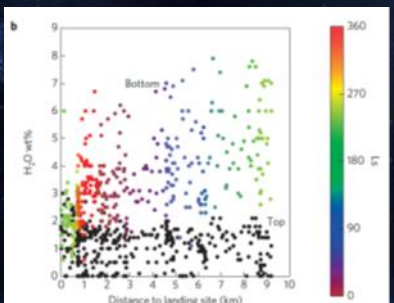
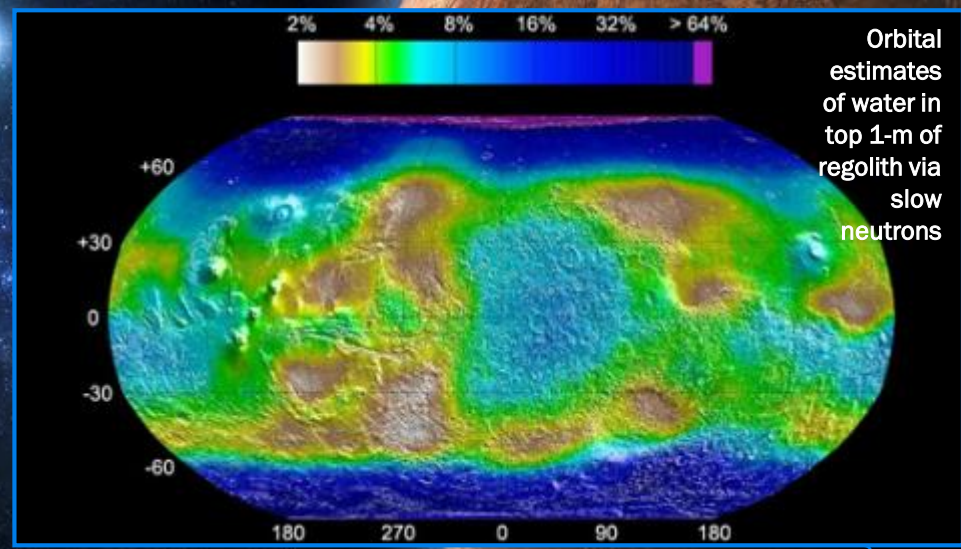
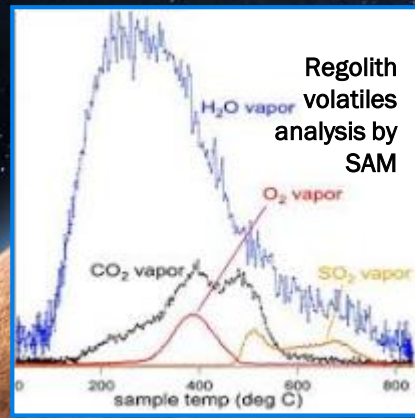
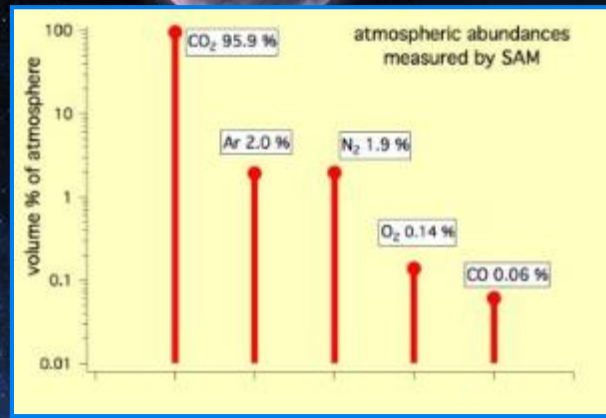
# Outline

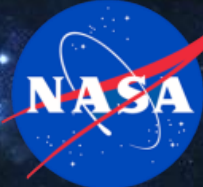
- Martian resources
- Introduction
- Why Mars ISRU?
- Dust removal
- Adsorption/desorption
- CO<sub>2</sub> Freezing/Liquefaction
- Direct compression
- Membranes
- Ionic Liquid adsorption/electrolysis
- Buffer gas capture and separation
- Microchannel technologies
- MARCO POLO/Mars ISRU Pathfinder Project
- Videos
- Challenges
- Future directions



# Martian Resources

- Atmosphere of Mars
  - 95.9% CO<sub>2</sub>
  - 2% Ar, 1.9% N<sub>2</sub>
  - <1% pressure of Earth's atmosphere (~7 mbar)
- Significant Amounts of Water in the Top 1-Meter of Regolith
  - Water ice caps at the poles
  - ~2% at least everywhere else
  - ~10% even at equatorial regions
  - **Curiosity rover ground truth:**
  - **1.5-3% water in surface regolith (SAM)**
  - **Average 2.9% water (DAN), up to 7% in top 60 cm of regolith in some locations-seasonal variation**
  - **Transient liquid water at night in the top 5 cm of regolith**





# Introduction

- In 1976, Robert Ash at Old Dominion U. initiated idea of Mars ISRU using CO<sub>2</sub> from the atmosphere & water from regolith
- Concept: make methane and oxygen via the Sabatier reaction and water electrolysis:
  - $\text{CO}_2 + 4 \text{H}_2 \rightarrow \text{CH}_4 + 2 \text{H}_2\text{O}$
  - $2 \text{H}_2\text{O} \rightarrow 2 \text{H}_2 + \text{O}_2$
  - Freezing using liquid methane for CO<sub>2</sub> collection
- First demonstrated by Zubrin, Clark *et al.* at Lockheed Martin Astronautics in early '90s, but w/H<sub>2</sub> from Earth
  - Used zeolite sorption/desorption for CO<sub>2</sub> collection
  - Leverage: 12:1, but 10.3:1 after discarding excess CH<sub>4</sub>
  - Supplement w/RWGS or CO<sub>2</sub> electrolysis → O<sub>2</sub>
  - Raises leverage to 18:1
- Main issue w/imported H<sub>2</sub>: size of H<sub>2</sub> tanks
  - Low density/high boil-off
  - Too large for practical shrouds & heat shields



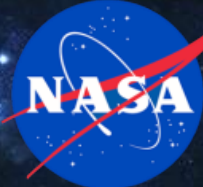
• R. Ash, W. Dowler, and G. Varsi, "Feasibility of Rocket Propellant Production on Mars," *Acta Astronautica*, Vol 5, pp. 705-724, 1978

• R. Zubrin, S. Price, L. Mason, and L. Clark, "Mars Sample Return with In-Situ Resource Utilization: An End to End Demonstration of a Full Scale Mars In-Situ Propellant Production Unit," NASA Contract No. NAS 9-19145. Presented to NASA JSC Jan. 13, 1995.



# Why Mars ISRU?

- “Gear ratio” = mass in LEO/landed mass on Mars surface =  $\sim 10$
- 10 kg IMLEO/1 kg on Mars surface
- Example: MAV (Mars Ascent Vehicle) =  $\sim 6$  tons dry mass
- Propellant
  - 7 tons  $\text{CH}_4$  + 23 tons  $\text{O}_2$
  - 5 tons life support  $\text{O}_2$
  - Total = 35 tons
- **IMLEO  $\sim 300$  tons or  $\sim$ several HLLVs (saves \$billions)**
- Mars atmosphere/water ISRU system  $\sim 1.7$  tons (regolith)
  - $\sim 2.2$  tons w/life support water product
- **Reduces landing mass by  $\sim 30$  tons or  $\sim 60\%$ !**
- Power  $\sim 40$  kW, but also needed for crewed phase
  - Not counted against ISRU system mass



# Dust Removal

- Martian atmosphere contains significant amounts of dust, especially during dust storms
- Can interfere with valves, catalysts, pumps, etc.
- NASA developing three approaches
  - Cyclone separator and HEPA filters (Juan Agui at GRC)
  - Electrostatic dust removal (Carlos Calle at KSC)



Cyclone separator prototype. 10" tall, 2.4" inner diameter. Smaller prototypes were built.

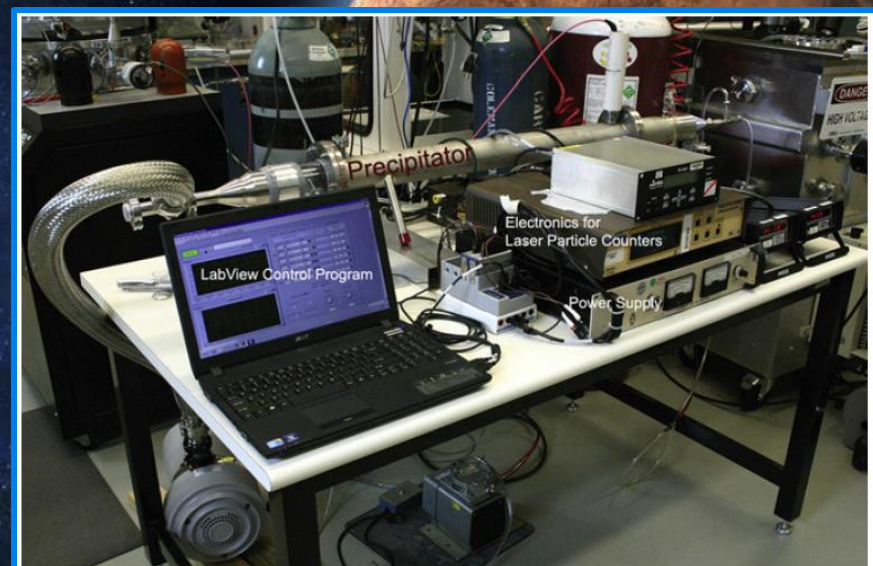


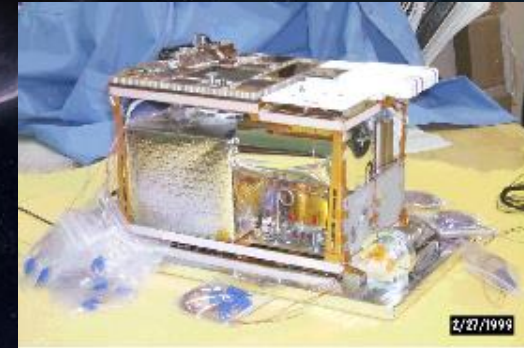
Fig. 2. Electrostatic precipitator in a flow through configuration.

# Adsorption/Desorption - MIP



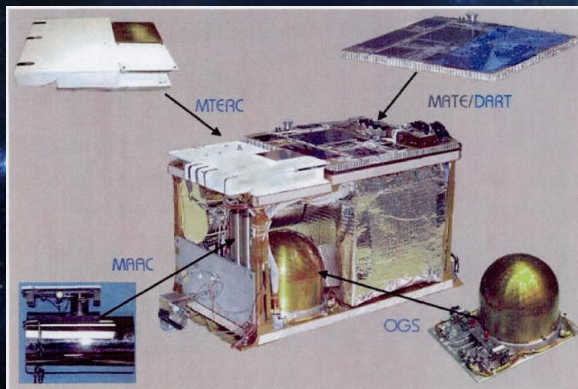
- MIP: Mars In-situ Propellant Production Precursor planned for the canceled Mars Surveyor 2001 Lander
- Led by David Kaplan at JSC
- Mass = 8.5 kg, Power (avg) = 16.0 W
- 40 cm x 24 cm x 25 cm box
- Oxygen Generator Assembly (OGA) Electrolyzes CO<sub>2</sub> to oxygen (~10 g/h) and carbon monoxide
- Used zeolite sorption/desorption (13X) (MAAC from JPL) with night/day cycle (200 K - 450 K)
  - 4.5 g CO<sub>2</sub>/6 h at 0.58 atm pressure
- Designed to run for 300 Mars days (sols).

TRL 6

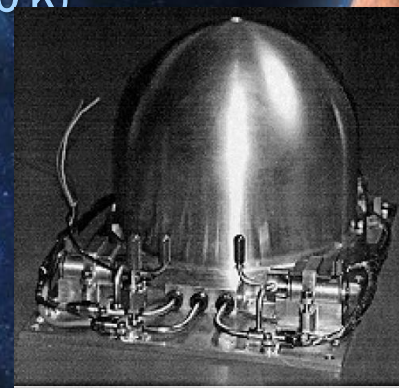


“Mars In-situ Propellant Production Precursor (MIP)”

<http://nssdc.gsfc.nasa.gov/nmc/experimentDisplay.do?id=MS2001L%20%20-06>



Photograph of integrated MIP Development Unit



OGS DU Hardware



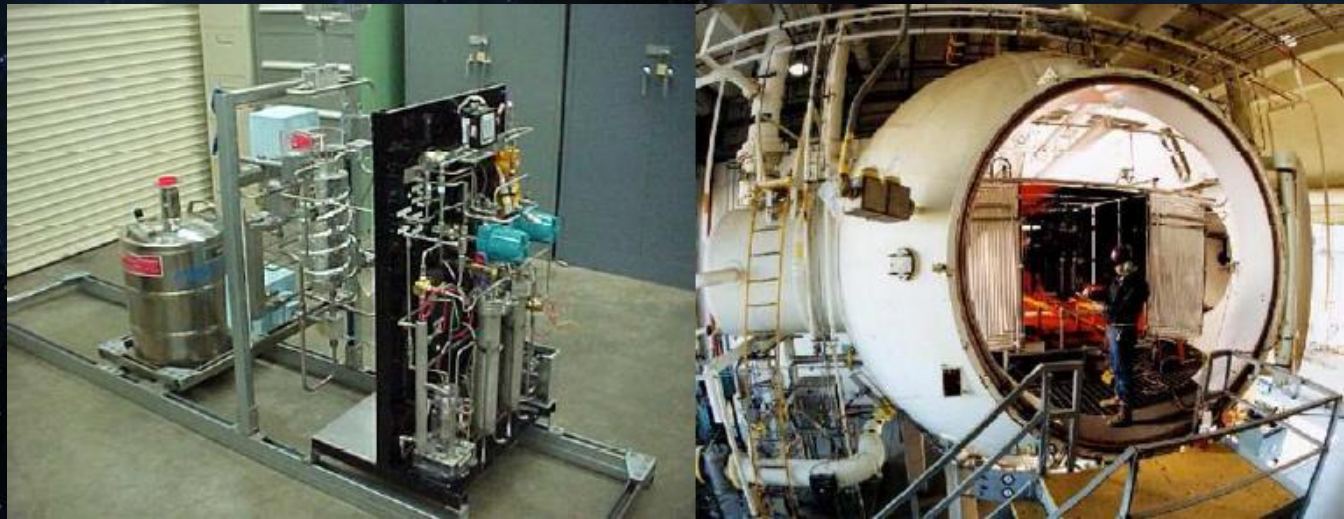
Photograph of OGS Qualification Unit

OGS Flight Design

OGS (Oxygen Generation System) 6



# Adsorption/Desorption



LMA/JSC Mars ISRU System (left); JSC Mars 20 ft. Dia.Environment Chamber (right)

“The end-to-end test started with the adsorption bed removing carbon dioxide from the simulated Mars atmosphere. The bed was then heated to transfer CO<sub>2</sub> to the Sabatier reactor with H<sub>2</sub> gas which was catalytically converted to CH<sub>4</sub> and H<sub>2</sub>O. The H<sub>2</sub>O vapor is condensed and delivered to the H<sub>2</sub>O electrolysis unit where it is electrolyzed into H<sub>2</sub>, which is recycled back to the Sabatier reactor, and O<sub>2</sub>, which is dried and delivered to the liquefaction and storage system. The CH<sub>4</sub> stream from the Sabatier reactor contains residual H<sub>2</sub> since the process is run H<sub>2</sub> rich to maximize the conversion of CO<sub>2</sub>. The CH<sub>4</sub> stream is passed through an electrochemical membrane to recover the H<sub>2</sub> (and a good portion of the water) and recycle it back to the Sabatier reactor. Finally, the CH<sub>4</sub> is passed through a drier and then routed to the liquefaction and storage system. In initial tests, the methane was simply vented overboard, since only one cryocooler was available for the system (used for O<sub>2</sub> liquefaction). The test was run under simulated Mars conditions for 9 days, and test results were favorable, with almost complete conversion of the CO<sub>2</sub>, maximized usage of the H<sub>2</sub>, and smooth operation of the integrated breadboard<sup>13</sup>. Figure 11 depicts the end-to-end Mars ISRU test article and the Mars environment simulation chamber at JSC.”

TRL 6



# Freezing/Sublimation

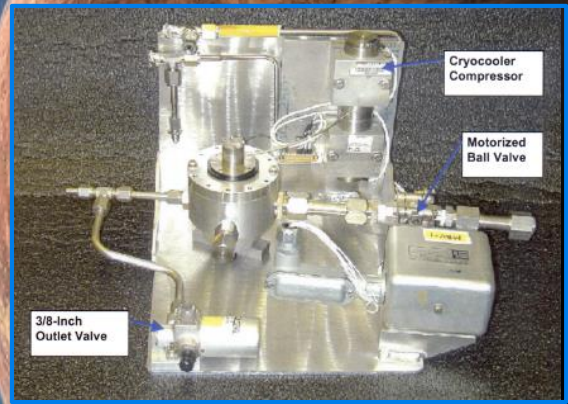
- CO<sub>2</sub> Freezers Look Promising
- CO<sub>2</sub> freezers tested by Pioneer Astronautics, Lockheed-Martin (two scales), and KSC
- Results: ~20, 13, 80, and 100 g/hr using lab-scale systems
  - (equiv. 5-32 g/hr CH<sub>4</sub>)
- Thickness up to 1 cm
- N<sub>2</sub>/Ar was not measured or purified
- CO<sub>2</sub> self-pressurizes via sublimation
- Don Rapp (JPL) estimated a CO<sub>2</sub> freezer for 0.5 kg/hr needs ~1/3 the power and 11% the mass of a compression pump/membrane CO<sub>2</sub> purifier



Pioneer MACDOF  
(LN<sub>2</sub> Chilling)



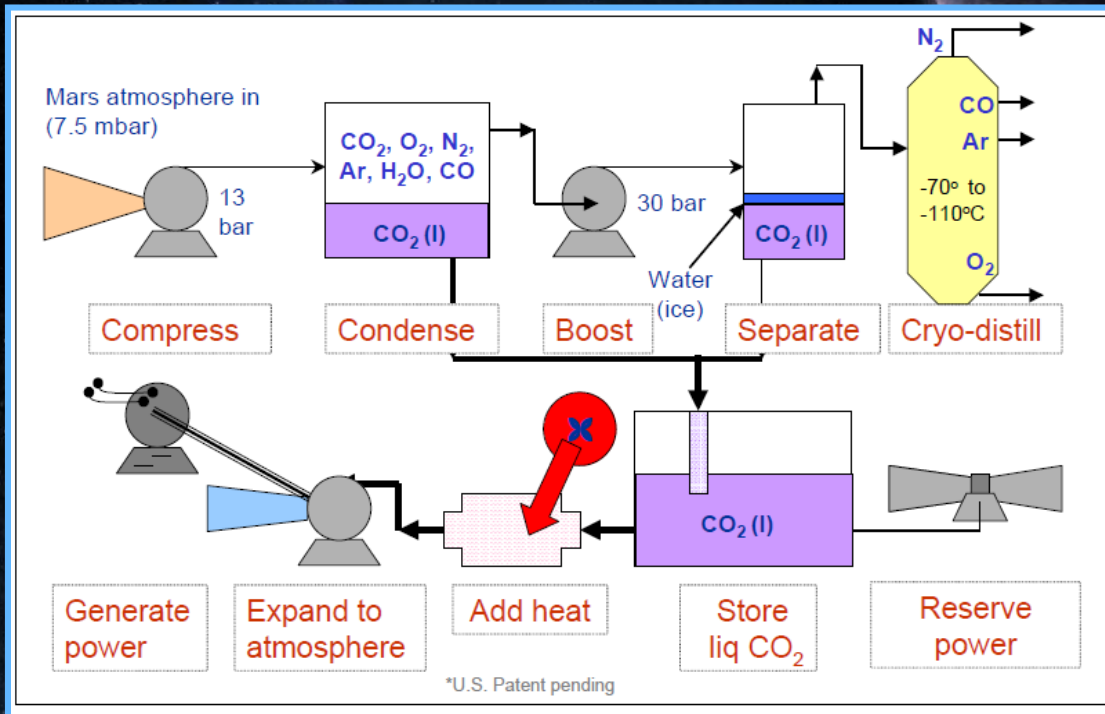
KSC "Ferris Wheel"  
Cold Head Testing



Lockheed Cryocooler Freezer  
0.9 Watt-h/g CO<sub>2</sub>

TRL 3-6

# Direct Compression/Liquefaction



Mars Atmosphere Resource Recovery System (MARRS)  
- NIAC Study

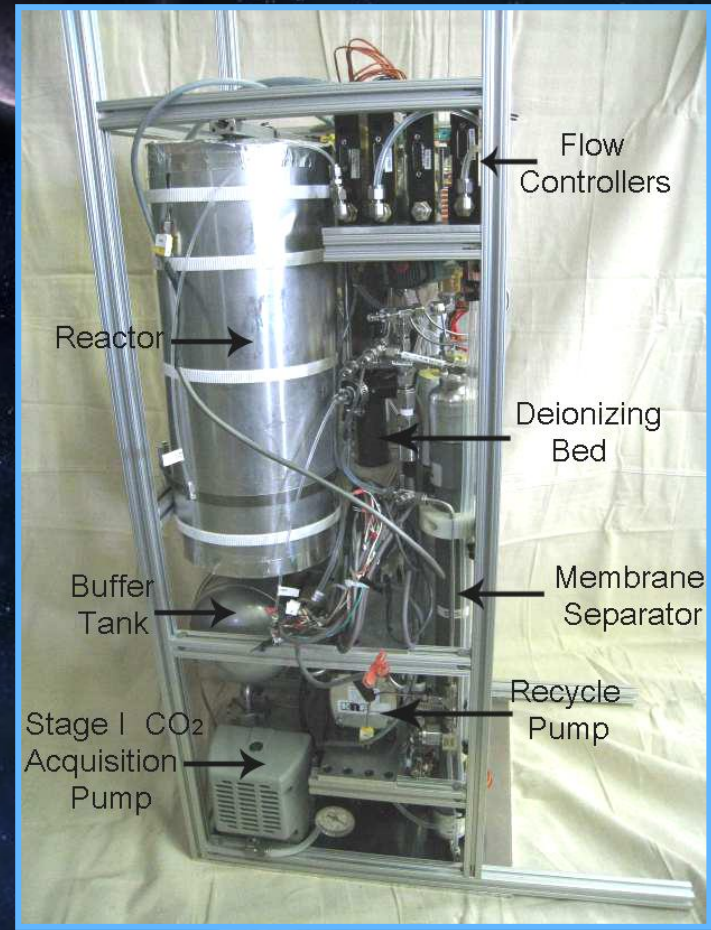
TRL 1-2

- $\text{CO}_2$  Liquefaction and Collection of Other Gases
- Compress very large volumes of the atmosphere to the high pressures required to liquefy  $\text{CO}_2$
- Geared toward larger scale operations: settlements
- Requires very high power source - nuclear reactor
- Not appropriate for Mars Sample Return or early human exploration



# Direct Compression & Processing

- ISRU processes (SOE, RWGS, Sabatier) tolerate lower purity CO<sub>2</sub>
- Pioneer Astronautics tested combined RWGS-Sabatier process with CO<sub>2</sub>/N<sub>2</sub>/Ar for 5-continuous days without degradation of catalyst
  - 1 kg/day of 3.5 O<sub>2</sub> to 1 CH<sub>4</sub>
  - Power = 893 W (678 W optimized)
- N<sub>2</sub> and Ar not separated, but removed during condensation or cryodistillation of products
- Gas separation downstream from CO<sub>2</sub> reduction process may be easier and still provide useful buffer gases
- Two-stage COTS mechanical compression required 242 W (plus chiller), and may require more power than freezing, but was claimed to be less complex
- Mass comparison needs to be done



Pioneer IMISPPS

46 cm x 41 cm x 94 cm; 115 kg (54 kg optimized)

**TRL 4**

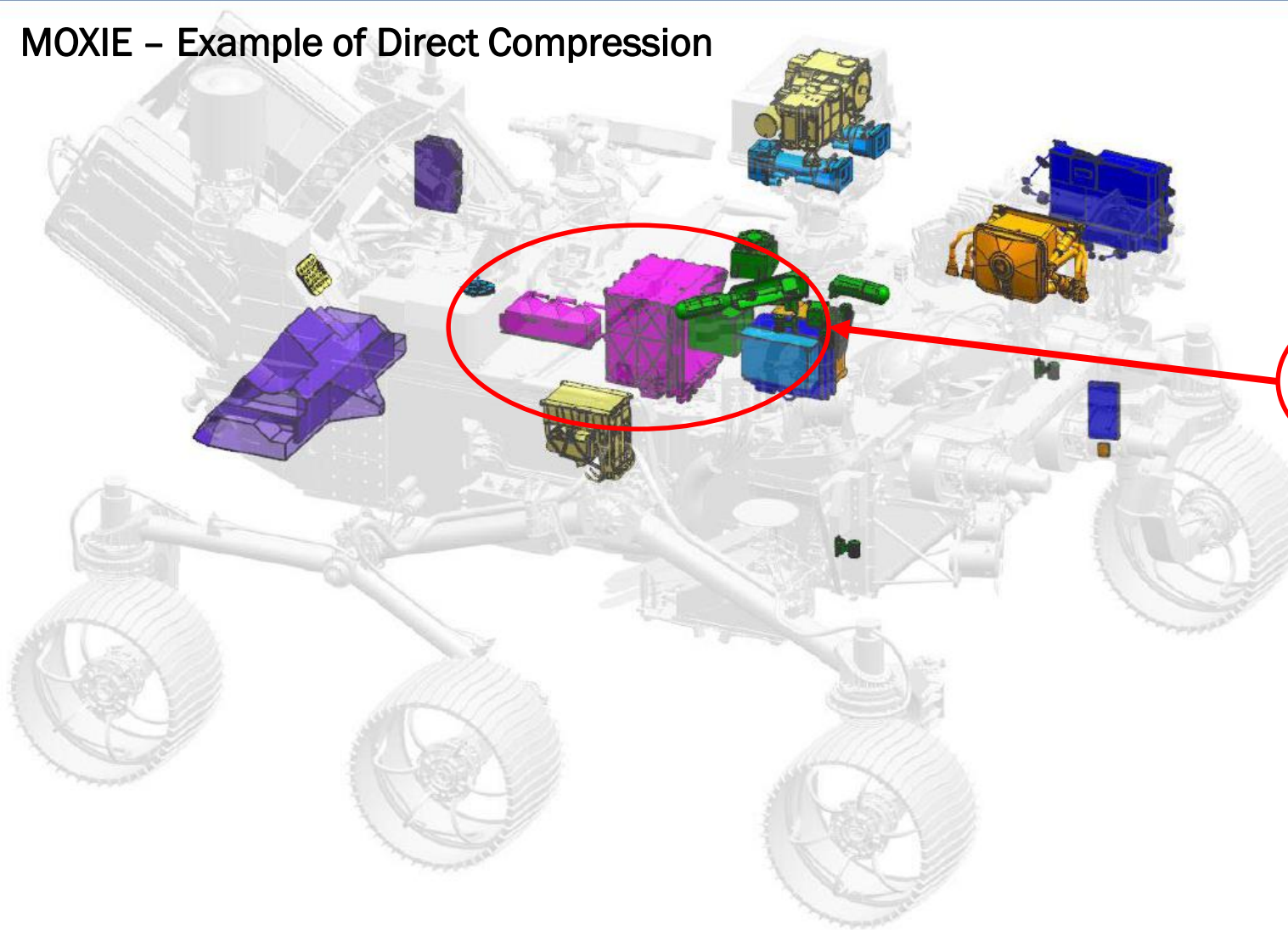
# Mars 2020 Payload Family Picture



Jet Propulsion Laboratory  
California Institute of Technology

Mars 2020 Project

## MOXIE – Example of Direct Compression



Instrument Key
<b>Mastcam-Z</b> Stereo Imager
<b>MEDA</b> Mars Environmental Measurement
<b>MOXIE</b> In-Situ Oxygen Production
<b>PIXL</b> Microfocus X-ray fluorescence spectrometer
<b>RIMFAX</b> Ground Penetrating Radar
<b>SHERLOC</b> Fluorescence and Raman spectrometer and Visible context imaging
<b>SuperCam</b> LIBS and Raman

# Direct Compression/Processing - NASA MOXIE

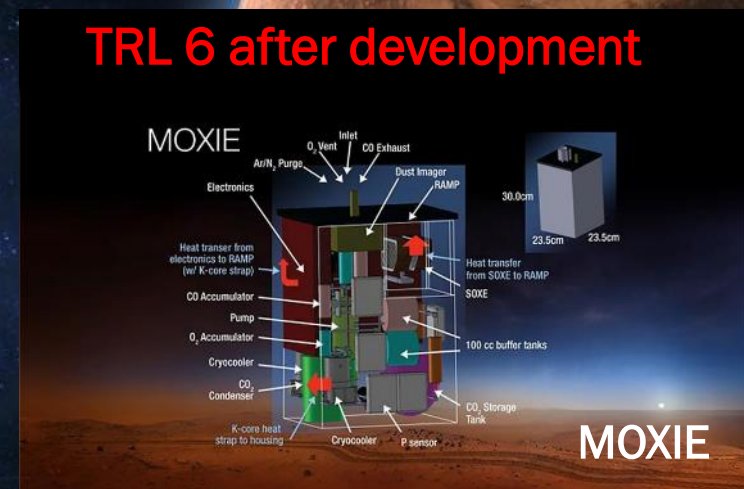
- MOXIE is the Mars OXYgen In situ resource utilization Experiment on the Mars 2020 Rover
- Led by Dr. Michael Hecht, MIT/Haystack Obs.
- Electrolyzes CO<sub>2</sub> to oxygen (~10 g/h) and carbon monoxide
- Initially specified a small cryocooler
- Switched to a small scroll pump from Air Squared (Broomfield, CO)
- N<sub>2</sub> and Ar are not separated from feed, but vented with CO
- Compressor Requirements:
  - A mass flow rate of at least 100 grams per hour
  - An outlet pressure of at least 760 Torr, with 7 Torr inlet pressure
  - A compressor and motor not exceeding 175 mm in length
  - Full compatibility with the working fluid: 95% CO<sub>2</sub>, 3% N<sub>2</sub>, and 2% Ar
  - A total mass of compressor, motor, and controller not exceeding 1.8 kg
  - The ability to function in the Martian environment
  - Further improvements in size, weight, and efficiency throughout development



“MOXIE Single-Stage Scroll Pump Design” for Mars 2020

<https://airsquared.com/news/scroll-compressor-jpl-mars-2020/>

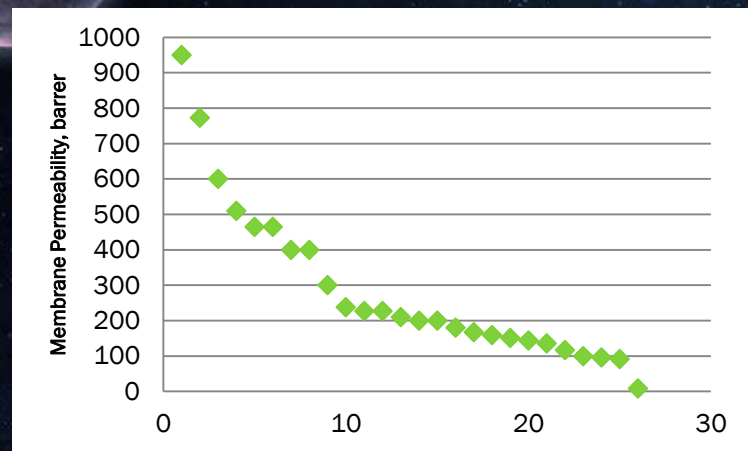
## TRL 6 after development





# CO<sub>2</sub> Capture with Membranes

- Evaluated 28 other membrane materials
  - Top 10 identified
- Mainly polymeric-based: poly-acetate, polyimides, polyamides, poly-sulfone, polycarbonates, and polyethylene, plus zeolite membranes
- Selectivity and permeability are inversely related
- **Pressurization is required (1-10 atm)**
- Polyacetylene and polydimethylsiloxane have the highest permeability
- Trades are needed for selectivity vs permeability and power to compress the CO<sub>2</sub> for separation
- Synthesis required in some cases



Distribution of membrane permeability. Note: For clarity, the top two ranked materials are not included in this graph (1 barrer =  $7.5 \times 10^{-14}$  (cm<sup>3</sup>(STP)-cm)/(cm<sup>2</sup>-s-Pa)).

**TRL 2-3**

# Chemical Processes - Membrane Separations

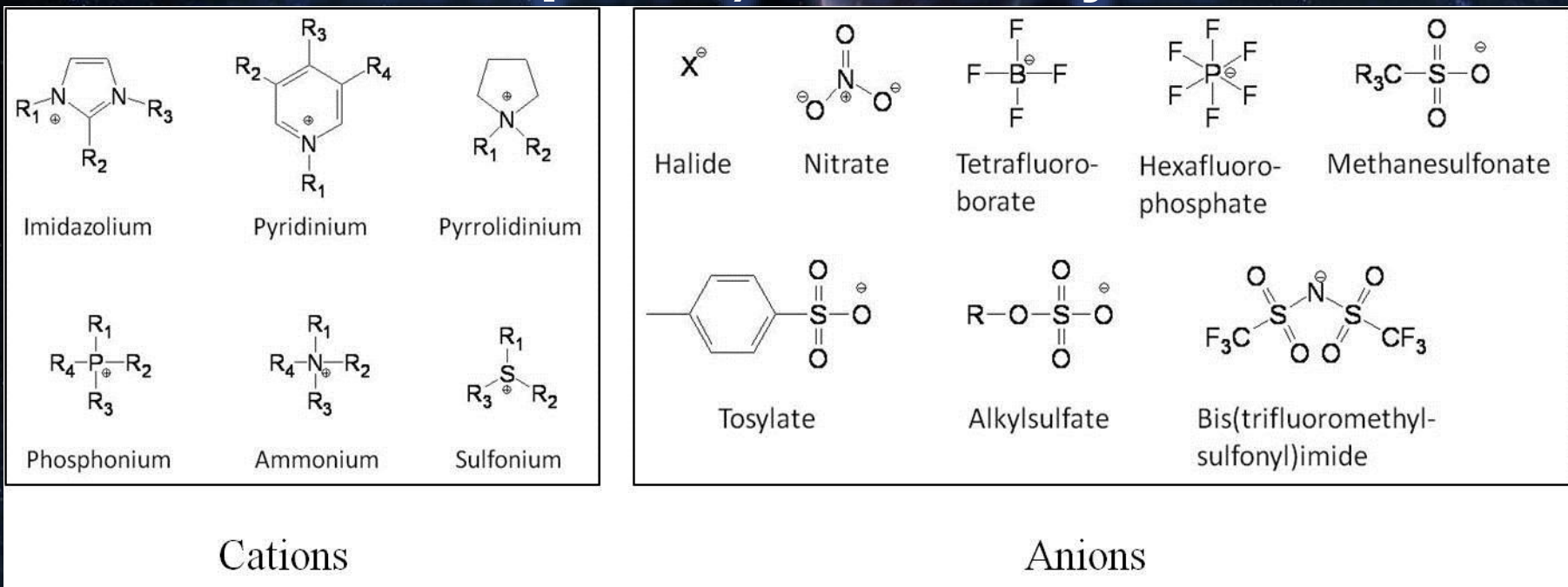
- Air Products Prism modules have been tested by LMA, Pioneer Astronautics and KSC
  - KSC results are good with minor H<sub>2</sub> losses (0.26% average)



		Calculated	Measured	Calculated	Measured	Calculated	Measured
	Stream	H <sub>2</sub> (slpm)	H <sub>2</sub> (slpm)	CO <sub>2</sub> (slpm)	CO <sub>2</sub> (slpm)	CO (slpm)	CO (slpm)
Base Case	Feed	16.825	16.861	7.56	7.522	2.114	2.116
	Permeate	16.812	16.812	7.547	7.547	1.126	1.126
	Reject	0.013	0.013	0.013	0.013	0.988	0.988
Sim-1	Feed	26.265	25.333	7.265	8.126	1.793	1.864
	Permeate	26.058	26.205	7.162	7.189	0.64	0.65
	Reject	0.207	0.059	0.103	0.076	1.153	1.144
Sim-2	Feed	30.748	30.555	7.984	8.07	1.537	1.644
	Permeate	30.011	30.48	7.681	7.801	0.3831	0.541
	Reject	0.737	0.267	0.303	0.184	1.154	0.996
Sim-3	Feed	29.552	29.428	8.605	8.696	2.028	2.047
	Permeate	29.324	29.463	8.486	8.523	0.723	0.834
	Reject	0.228	0.09	0.119	0.082	1.305	1.194
Sim-4	Feed	25.603	25.099	7.035	7.332	1.779	1.986
	Permeate	25.515	25.563	6.987	6.96	0.753	0.747
	Reject	0.088	0.04	0.048	0.076	1.026	1.032
Sim-5	Feed	16.507	17.248	8.921	8.323	2.47	2.327
	Permeate	16.43	16.5	8.843	8.909	1.032	1.384
	Reject	0.077	0.007	0.078	0.012	1.438	1.086
Sim-6	Feed	20.591	20.864	7.036	6.786	1.983	1.96
	Permeate	20.552	20.564	7.008	7.007	0.952	1.024
	Reject	0.039	0.026	0.028	0.029	1.031	0.959

**TRL 4** KSC RWGS Membrane Results

# Ionic Liquids for CO<sub>2</sub> Adsorption/Electrolysis



## Typical cations and anions for ILs

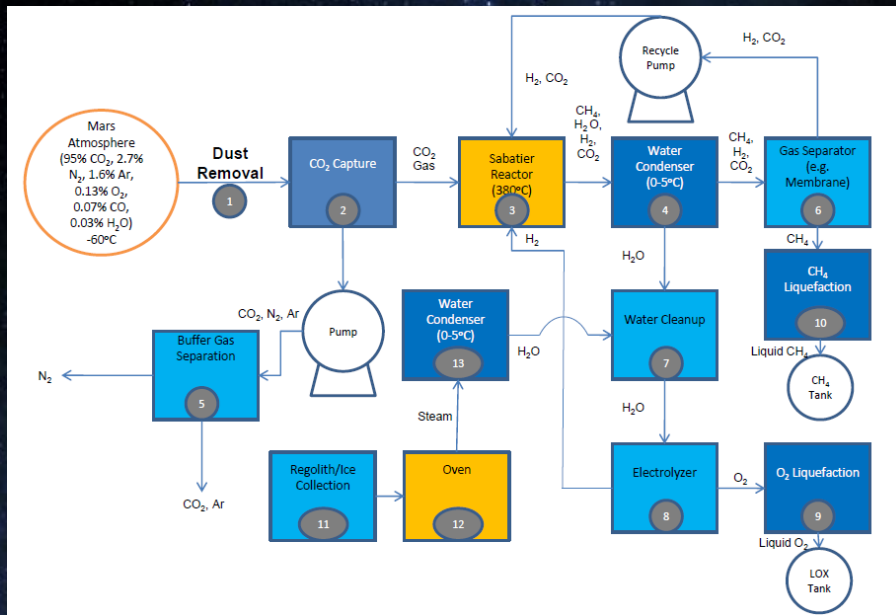
Ionic Liquids are organic, ionic compounds that are liquid at or near room temperatures



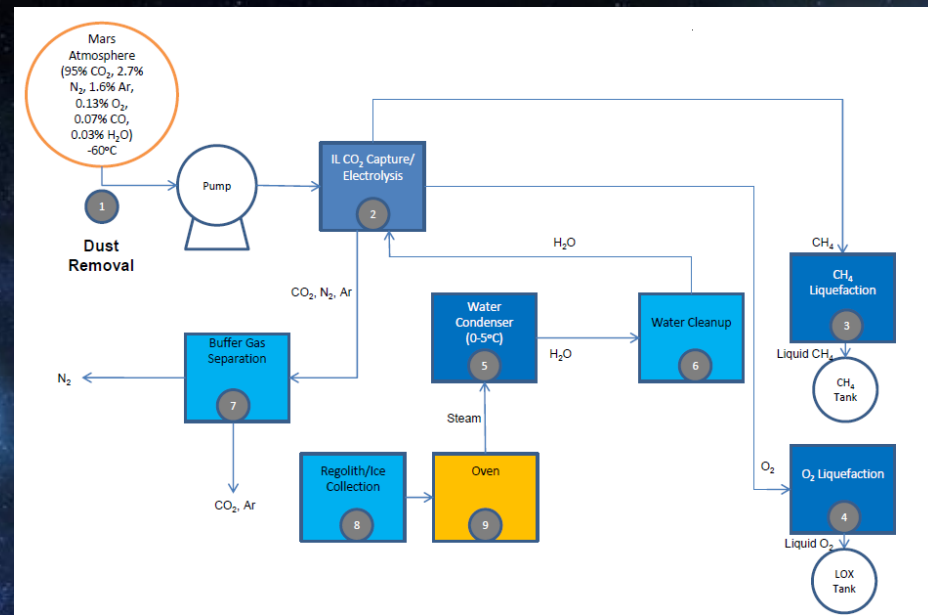


# Potential Benefits for ISRU

### Current Mars Bipropellant Production Process Diagram

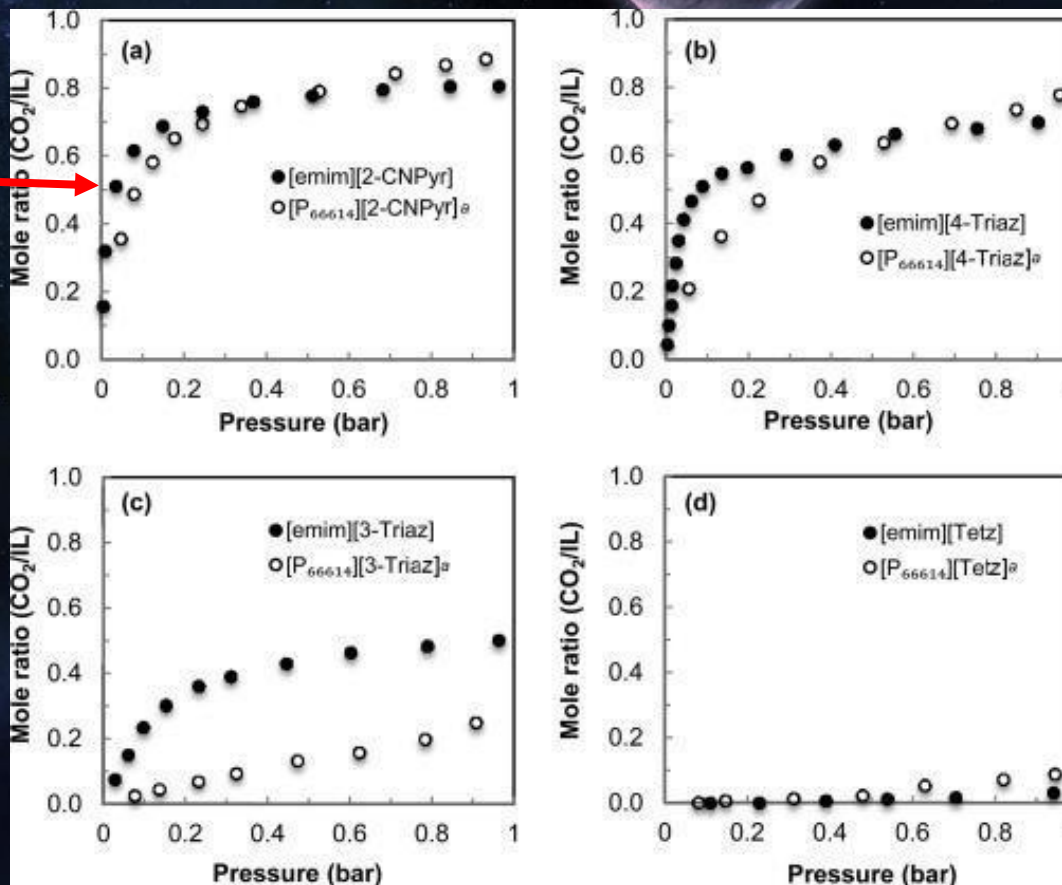


### Mars Bipropellant Production Process Diagram with IL Electrolysis



- Advantages of IL capture/electrolysis:
  - No high temperature processing of CO<sub>2</sub>
  - One less pump and no cryocoolers
  - Four fewer major process steps
  - Estimated ~50% less mass and ~25% less power

# CO<sub>2</sub> Uptake at Low Partial Vacuum ~50% Mole Fraction at ~10 mbar



“CO<sub>2</sub> absorption capacity in (a) [emim][2-CNPy], (b) [emim][4-Triaz], (c) [emim][3-Triaz], and (d) [emim][Tetz] at 22 °C. The CO<sub>2</sub> solubility in [P<sub>66614</sub>]+ counterparts from ref 10 are also shown for comparison.” (Brennecke, 2014)



# Summary of KSC Results (Underlined ILs = Candidates)

Ionic Liquid	CO <sub>2</sub> Capacity, wt.% (R.T., 1 atm, dry)	Electro-chemical Window, V	Conduc-tivity with CO <sub>2</sub> (mS/cm, 40°C)	Compatible with Cu	Other Issues	Tested Solubility of Water, v/v%	Methane Production Rate
[BMIM][TFSI]	0.46	2.1		No			
<u>[BMIM][PF<sub>6</sub>]</u>	0.50	2.4		Yes	Precipitate, Cu darkened		0
<u>[BMIM][BF<sub>4</sub>]</u>	0.55	1.8		Yes			<b>Small</b>
[HMIM][B(CN) <sub>4</sub> ]	0.70	0.6		No			
[EMIM][BF <sub>4</sub> ]	2.6	1.6		No			
AZ-1	9.0	4.4	0.67	No		5	
<u>AZ-2</u>	9.6	2.4		Yes	IL darkened		0
<u>AZ-3</u>	15.6		1.2	Slow color change	Precipitate	5	<b>Possible CH<sub>4</sub> and CO (TiO<sub>2</sub> only)</b>



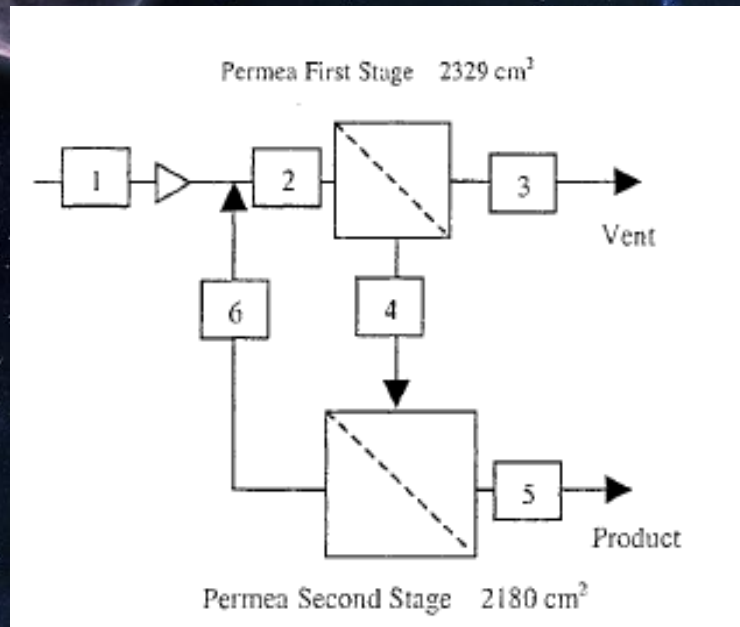
# Ionic Liquids for CO<sub>2</sub> - Summary

TRL 2

- In general, the benefits of ILs are:
  - Low volatility
  - Wide range of regeneration temperatures
  - Less energy to regenerate
  - Potentially lower corrosion
  - High temperature stability
  - Ability to tune performance
- Some major challenges for ILs that still need to be addressed:
  - Limited commercial availability
  - Limited understanding of the reaction mechanisms and kinetics
- Some major challenges for IL membranes that still need to be addressed:
  - Improvements in membrane fabrication (in general)
  - Improvements in large scale membrane fabrication
  - Improvements in producing defect free coating for the membranes

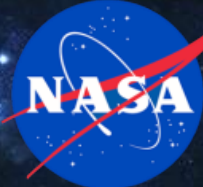
# Buffer Gas Separation

- COTS Membrane Modules Are Adequate
- Parrish (KSC, 2002) studied several commercial membranes:
  - Permea Prism® Alpha Separators PPA-20.
  - Neomecs GT #020101 .
  - Enerfex SS.
  - Enerfex SSP-M100C Membrane sheet.
- Temperatures = -45°C to +30°C.
- Variety of pressures.
- Designed a system that would operate at -44°C and 780 mm Hg (1.03 atm)
- Feed = 30% CO<sub>2</sub>, 26% Ar, and 40% N<sub>2</sub>.
- Predicted product = 6 lpm, 600 ppm CO<sub>2</sub>, 38% Ar and 62% N<sub>2</sub>.
- 47% recovery of the feed.
- Work is needed on Ar/N<sub>2</sub> separation.
  - Ar leads to potential bends issue.



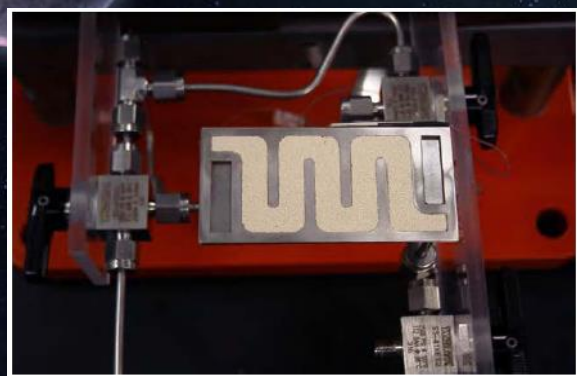
Membrane purification of feed from the capture of CO<sub>2</sub> (Parrish, 2002)

TRL 3-4

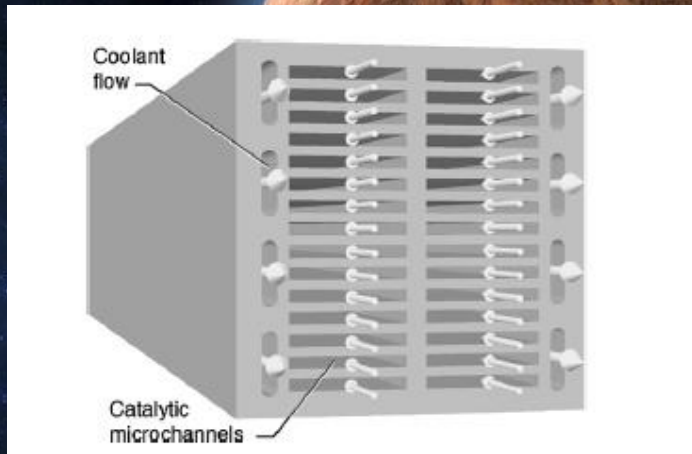


# Microchannel Technologies

- Microchannel reactors offer:
  - Better temperature control of the catalyst bed
  - Reduce temperature gradients and localized “hot spots”
  - Prevent sintering of a packed bed catalyst
  - Large mass savings over the traditional packed bed reactor design,
  - Penalty of increased pressure drop and increased probability of complete catalyst deactivation.
- Potentially improved CO<sub>2</sub> absorption for concentration
  - Lower mass, volume, and power
- Further development is justified

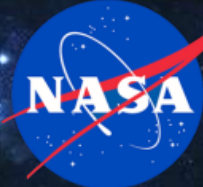


PNNL Microchannel Zeolite CO<sub>2</sub> Absorber



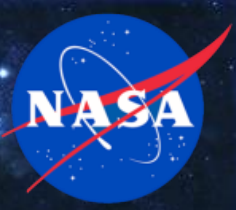
PNNL illustration of a section of microchannel reactor.

TRL 3



# MARCO POLO/ Mars ISRU Pathfinder

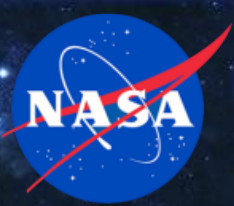
- ISPP: In Situ Propellant Production
  - Demonstrate production of Mars Sample Return propellant
  - Reduce risk for human Mars missions
- MARCO POLO - Mars Atmosphere and Regolith COLlector/PrOcessor for Lander Operations
- The Mars Atmospheric Processing Module (APM)
  - Mars CO<sub>2</sub> Freezer Subsystem
  - Sabatier (Methanation) Subsystem
- Collect, purify, and pressurize CO<sub>2</sub>
- Convert CO<sub>2</sub> into methane (CH<sub>4</sub>) and water with H<sub>2</sub>
- Other modules mine regolith, extract water from regolith, purify the water, electrolyze it to H<sub>2</sub> and O<sub>2</sub>, send the H<sub>2</sub> to the Sabatier Subsystem, and liquefy/store the CH<sub>4</sub> and O<sub>2</sub>
- Test in a Mars analog (field demo)



# What is MARCO POLO?

- First generation integrated Mars soil and atmospheric processing system with mission relevant direct current power
  - 10 KW Fuel Cell for 14 hrs of daytime operations
  - 1KW Fuel Cell for 10 hrs of night time operations
- Demonstrates closed loop power production via the combination of a fuel cell and electrolyzer.
  - The water we make and electrolyze during the day provides the consumables for the 1KW Fuel Cell that night
- Planned for remote and autonomous operations





# Lander Design Concept

## Atmo Processing Module:

- CO2 capture from Mixed Mars atmosphere (KSC)
- Sabatier converts H2 and CO2 into Methane and water (KSC/JSC)

## Liquefaction Module: (TBD)

- Common bulkhead tank for Methane and Oxygen liquid storage

## Water Processing Module: (JSC)

- Currently can process 520g/hr of water (max 694 g/hr)

## C&DH/PDU Module: (JSC)

- Central executive S/W
- Power distribution

## Soil Processing Module: (JSC)

- Soil Hopper handles 30kg (KSC)
- Soil dryer uses CO2 sweep gas and 500 deg C to extract water

## Water Cleanup Module: (KSC)

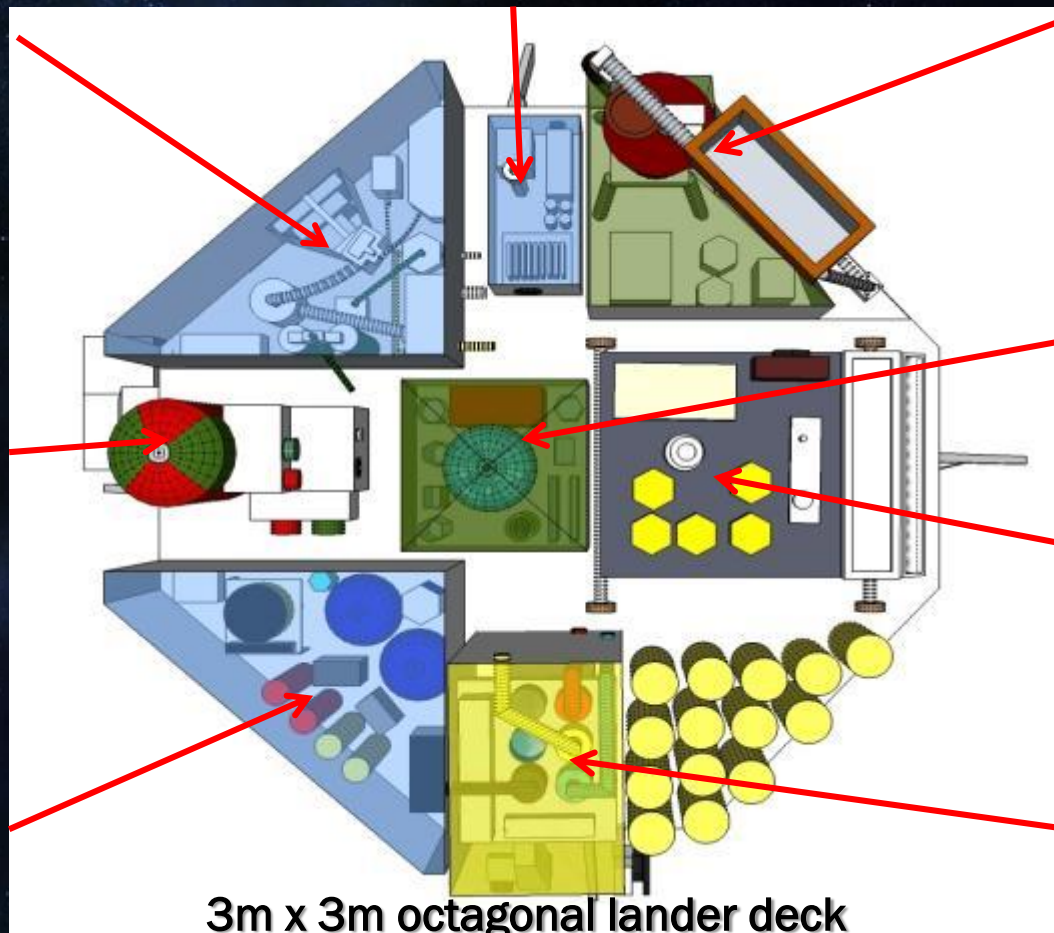
- Cleans water prior to electrolysis
- Provides clean water storage

## Excavator: (KSC)

- RASSOR 2.0 Rover
- Provides feed to Soil Dryer

## 1KW Fuel Cell and consumable storage (JSC & GRC)

- Uses metal hydride for H2 storage due to availability
- 1KW No Flow Through FC (GRC)
- 10KW FC not shown (JSC)



3m x 3m octagonal lander deck



# Existing Hardware



KSC: Mockup Lander w/Hopper, Mock Oven, and APM Simulator in Regolith Bin



KSC: RASSOR 2.0 Excavator Rover



KSC: Common Bulkhead Cryotank



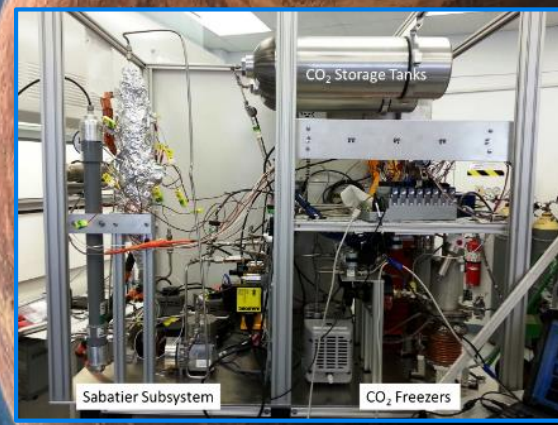
JSC: Soil Processing Module



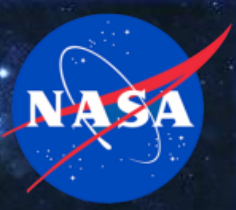
KSC/JSC: Water Cleanup Module



JSC: Water Processing Module (Electrolyzer)

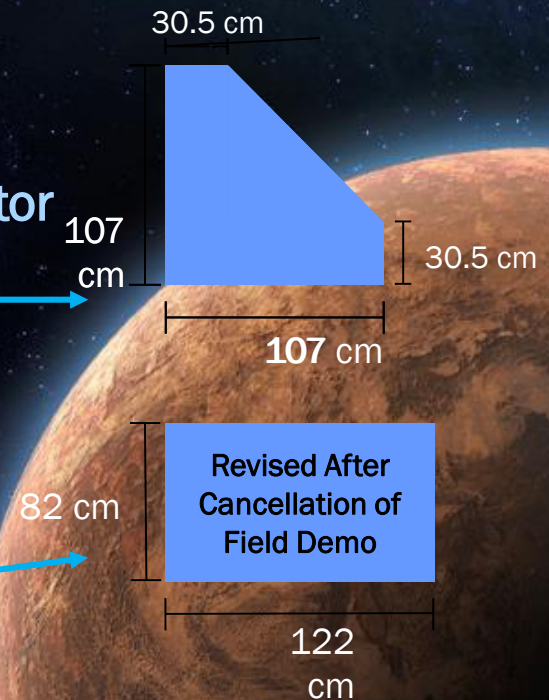


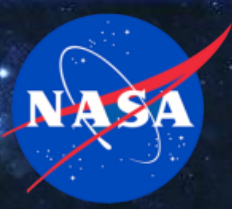
KSC: Atmospheric Processing Module



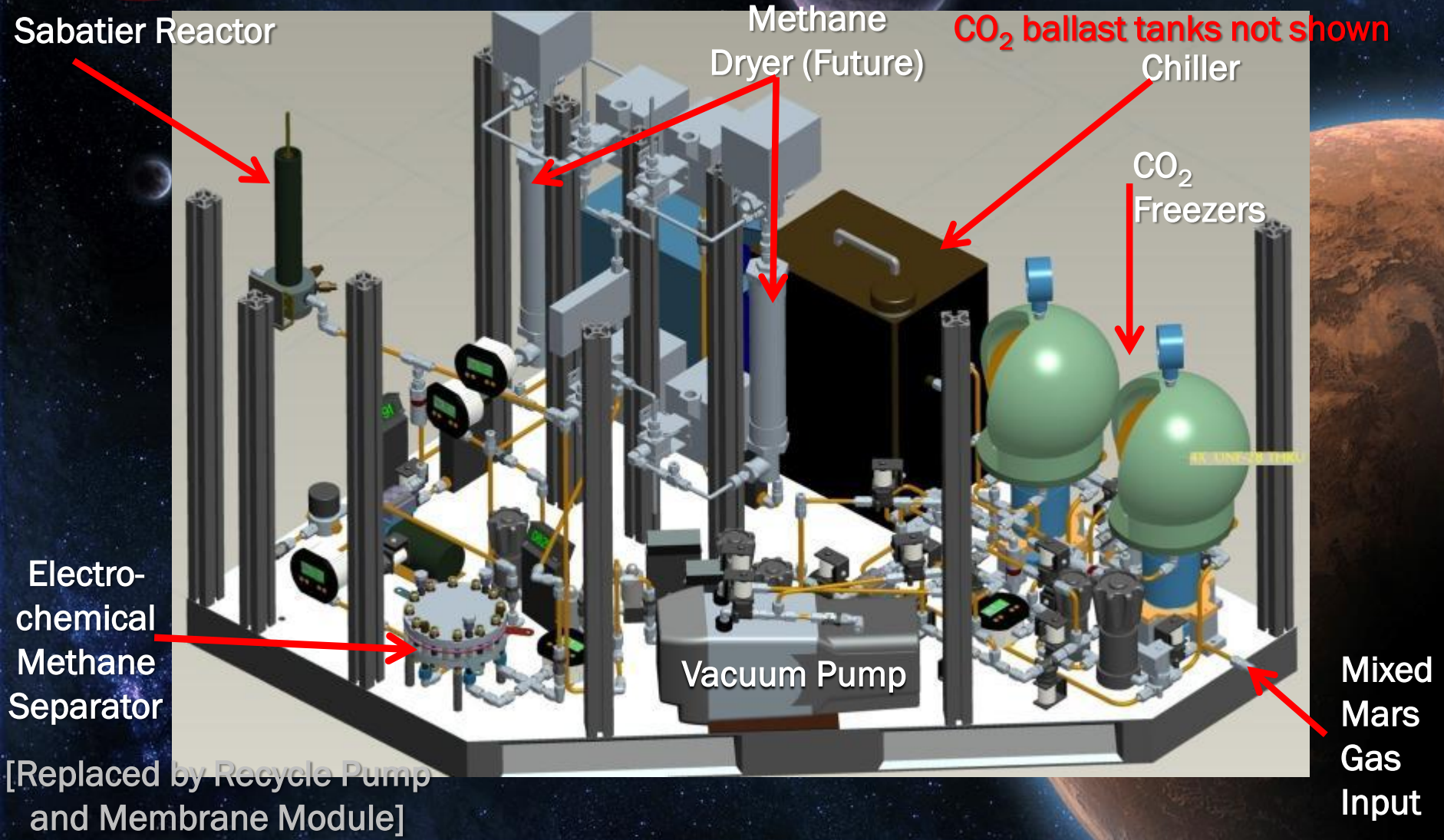
# APM Goals/Requirements

- Collect and purify 88 g CO<sub>2</sub>/h (>99%)
  - From simulated Martian atmosphere
  - 10 mbar; 95.4% CO<sub>2</sub>, 3% N<sub>2</sub>, 1.6% Ar
- Supply 88 g CO<sub>2</sub>/h at 50 psia to the Sabatier reactor
- Convert CO<sub>2</sub> to 32 g CH<sub>4</sub>/h and 72 g H<sub>2</sub>O/h
- Operate autonomously for up to 14 h/day
- Minimize mass and power
- Fit within specified area and volume
  - 9,000 cm<sup>2</sup> pentagon
  - 10,000 cm<sup>2</sup> rectangle for easier lab operations
  - 44 inches tall (112 cm, same as Water Processing Module)
- Support MARCO POLO production goals of 0.032 kg CH<sub>4</sub>/h and 0.128 kg O<sub>2</sub>/day (50% of O<sub>2</sub>) for a total of 2.22 kg propellant/14 h day
- Sufficient for a Mars Sample Return Mission
- ~13% of full-scale O<sub>2</sub> production goal for human Mars Missions (1 kg O<sub>2</sub>/h/module x 3 modules = 3 kg O<sub>2</sub>/h), i.e. 1/8<sup>th</sup> scale



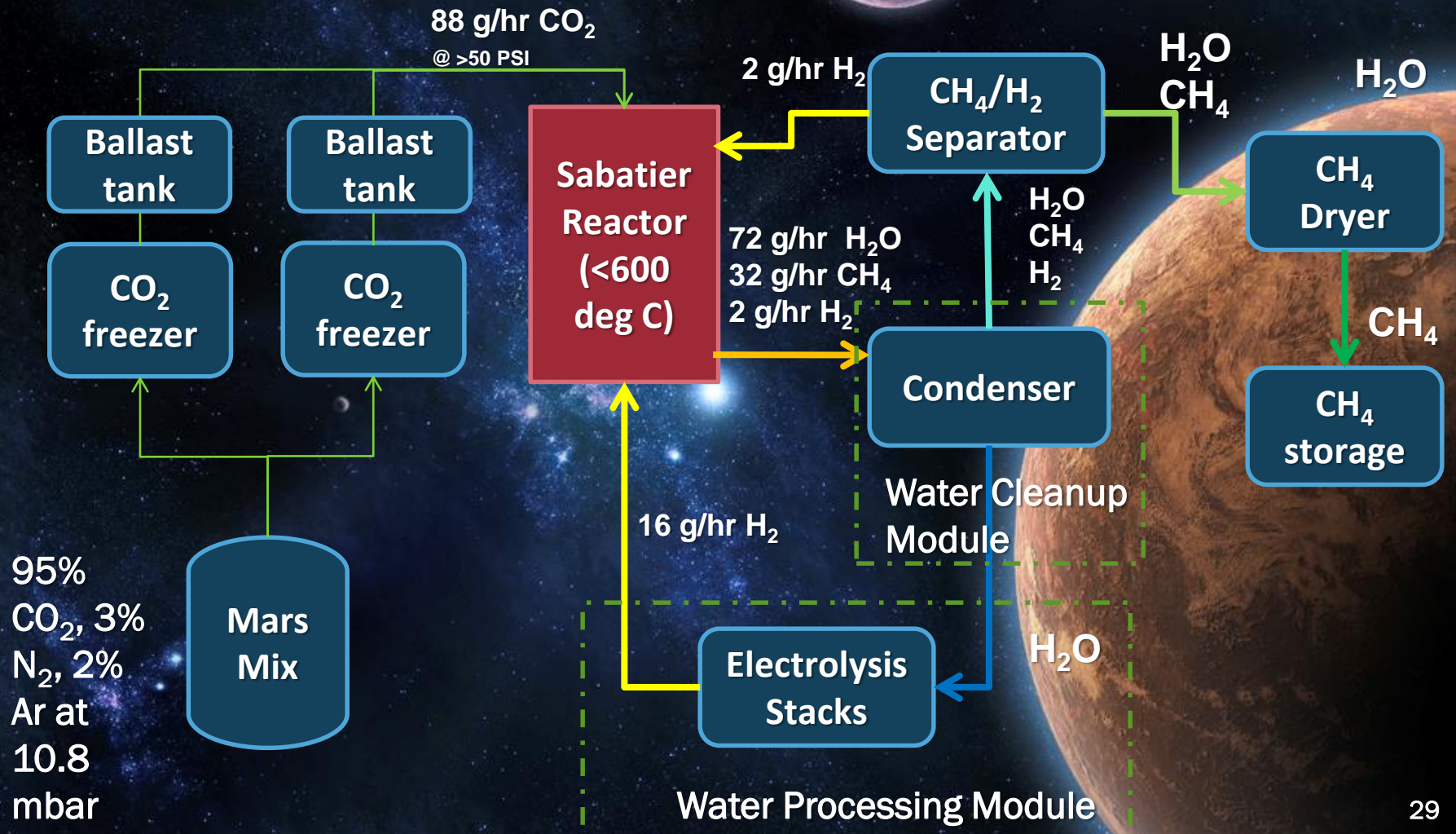


# Atmospheric Processing Module Design



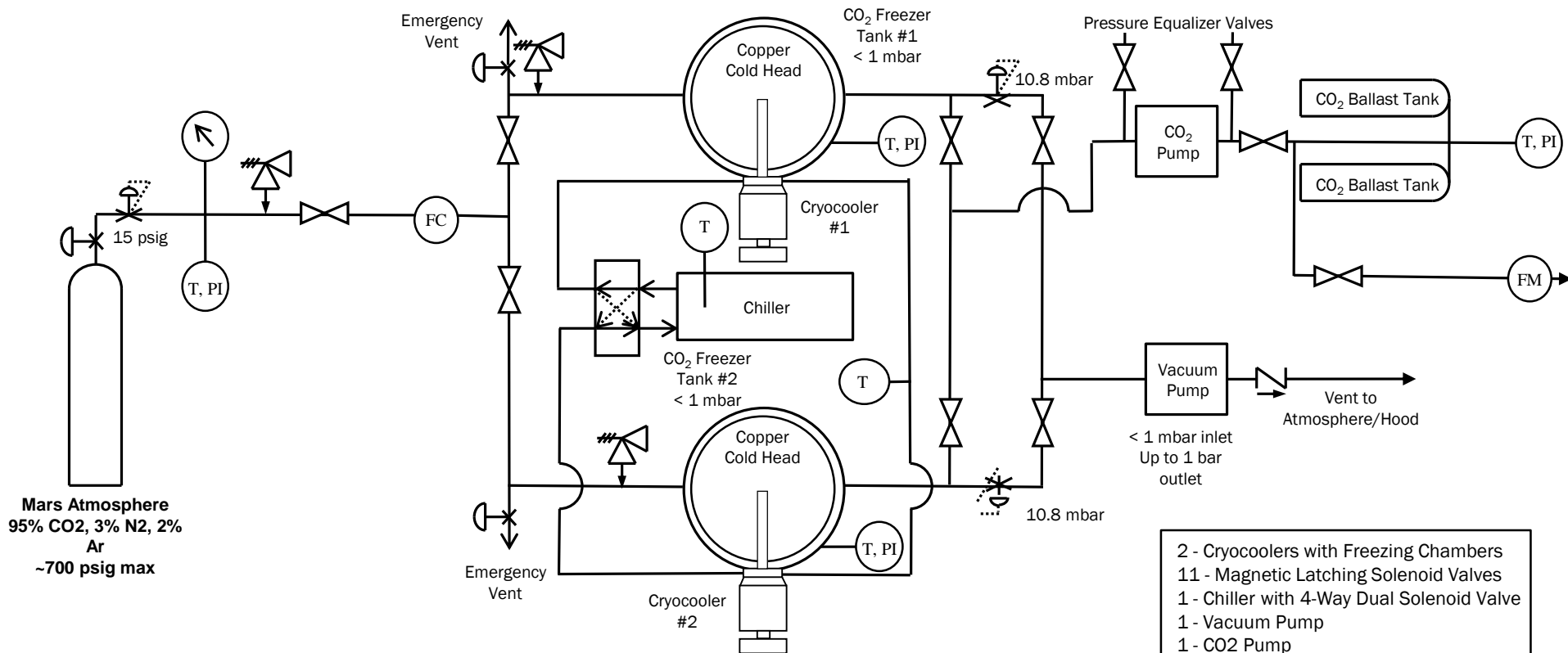


# Atmospheric Processing Operations





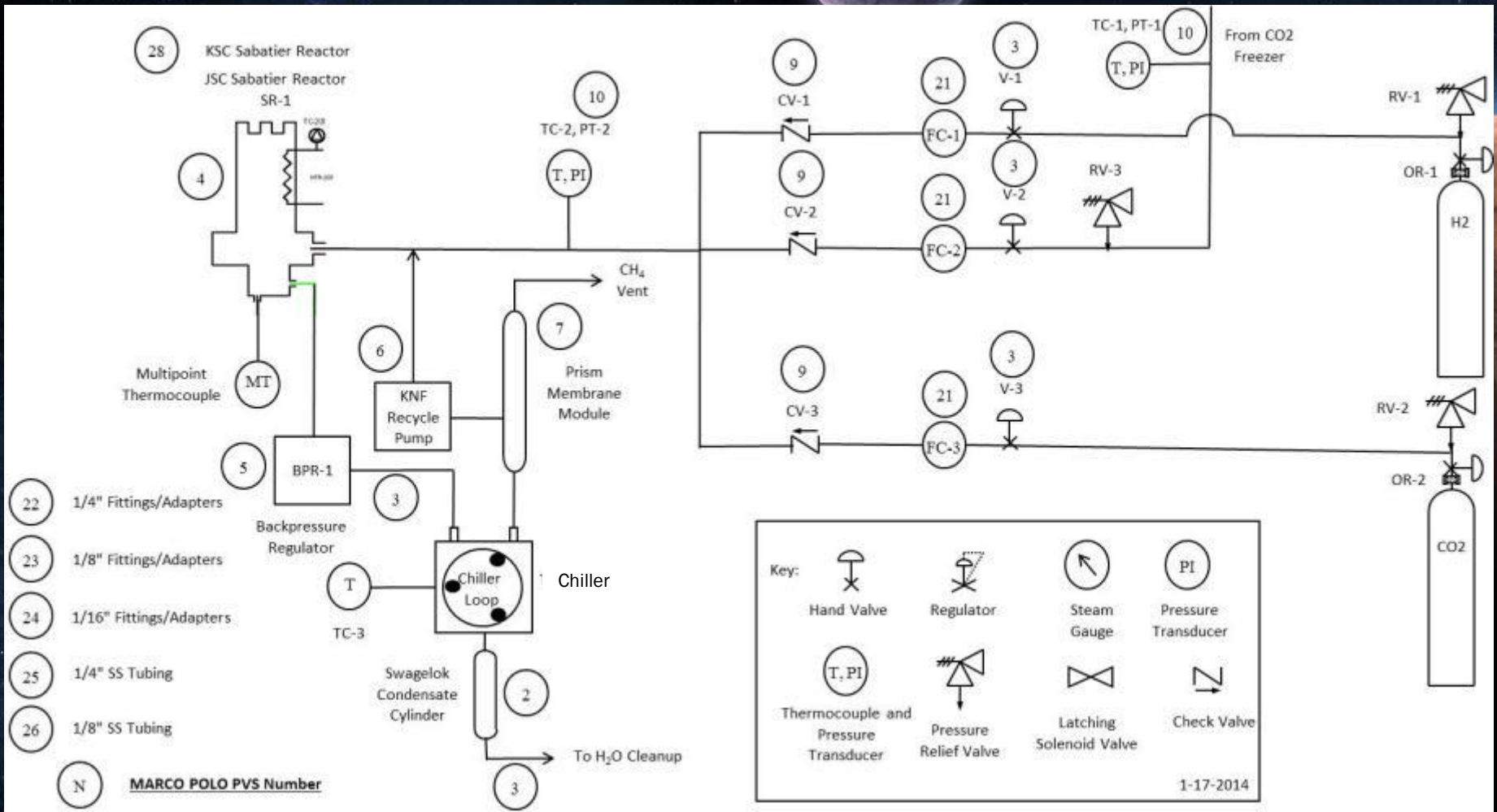
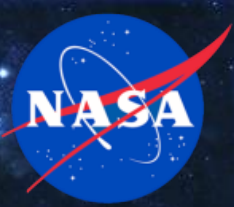
# CO<sub>2</sub> Freezer – Final Design



- 2 - Cryocoolers with Freezing Chambers
- 11 - Magnetic Latching Solenoid Valves
- 1 - Chiller with 4-Way Dual Solenoid Valve
- 1 - Vacuum Pump
- 1 - CO<sub>2</sub> Pump
- 2 - CO<sub>2</sub> Ballast Tanks
- 2 - Vacuum Back Pressure Regulators
- 3 - Pressure Relief Valves
- 1 - Flow Controller
- 1 - Flow Meter
- 3 - Thermocouples and 2 RTDs
- 3 - Pressure Transducers, etc.

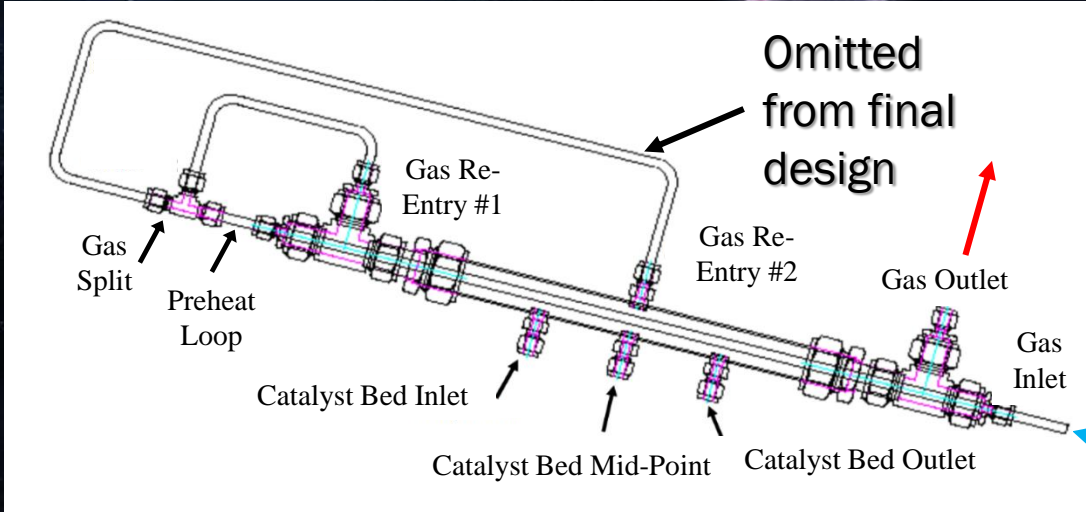


# Sabatier Subsystem Design

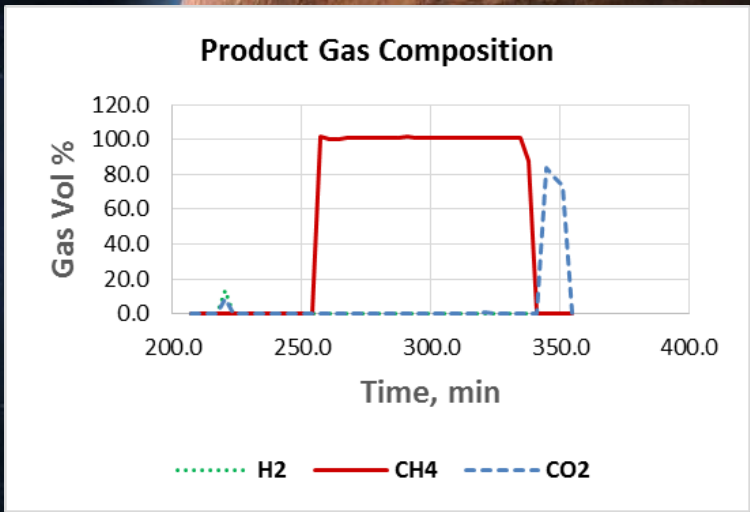




# Design of KSC Sabatier Reactor

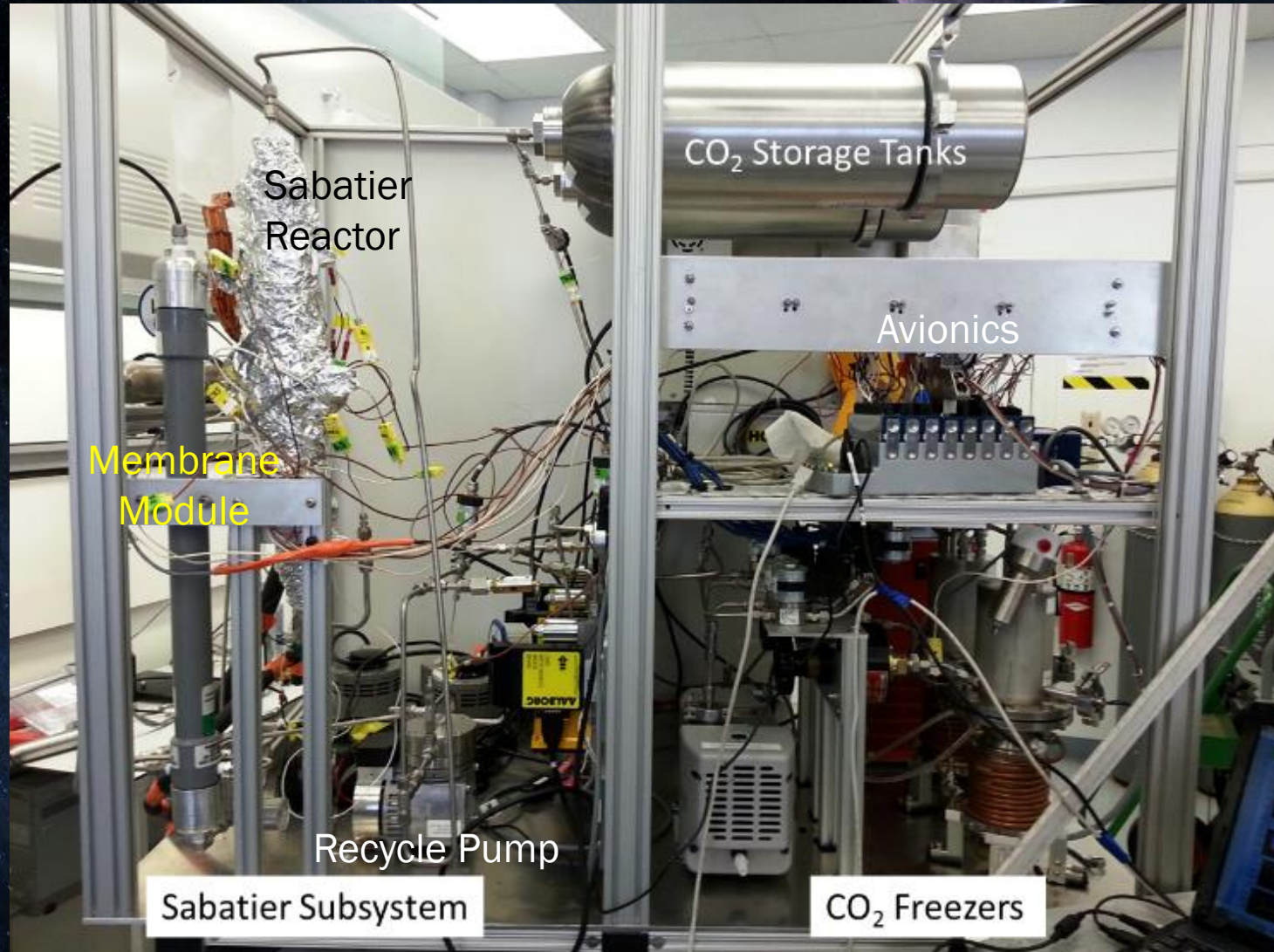


- 30 cm long stainless steel tube w/2.54 cm OD and 0.21 cm wall thickness
- Single-pass conversion = 90% @ 88 g CO<sub>2</sub>/h + 3.5:1 H<sub>2</sub>/CO<sub>2</sub>
- Based on Pioneer Astronautics design for steam oxidation of trash to methane
- 1.5 h integrated test with CO<sub>2</sub> Freezers and recycling system showed 100% conversion to pure CH<sub>4</sub>





# Atmospheric Processing Module



Sabatier Reactor

CO<sub>2</sub> Storage Tanks

Avionics

Membrane Module

Recycle Pump

Sabatier Subsystem

CO<sub>2</sub> Freezers

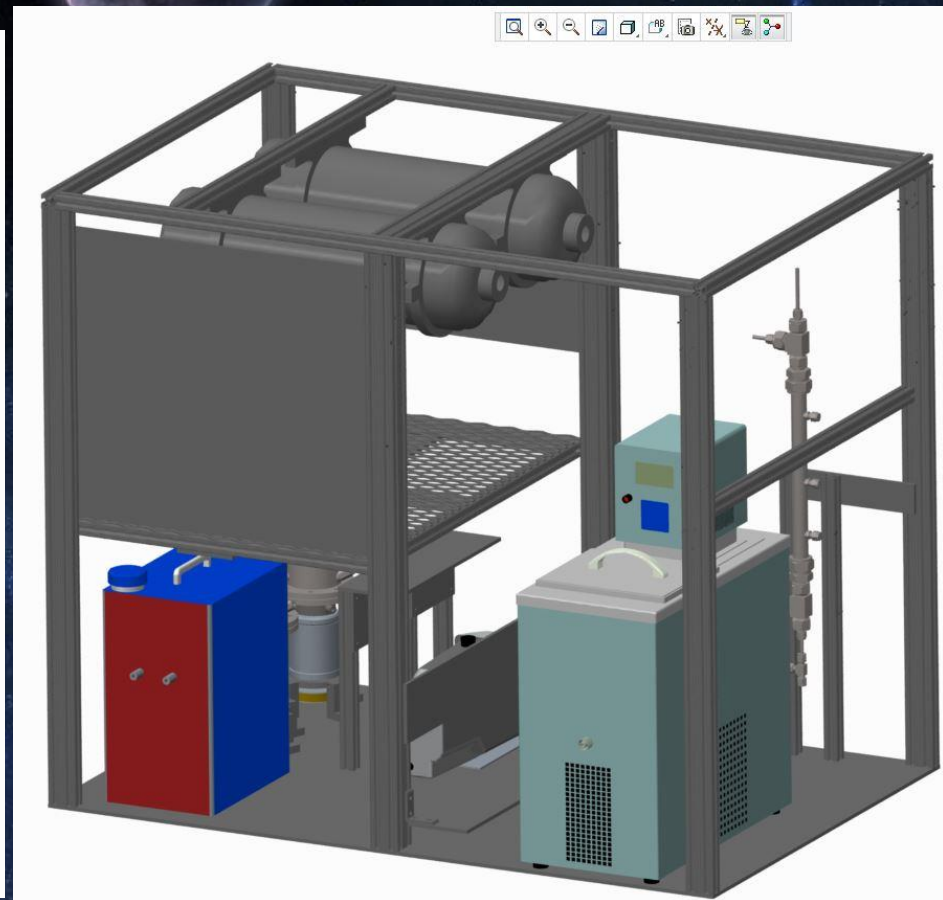
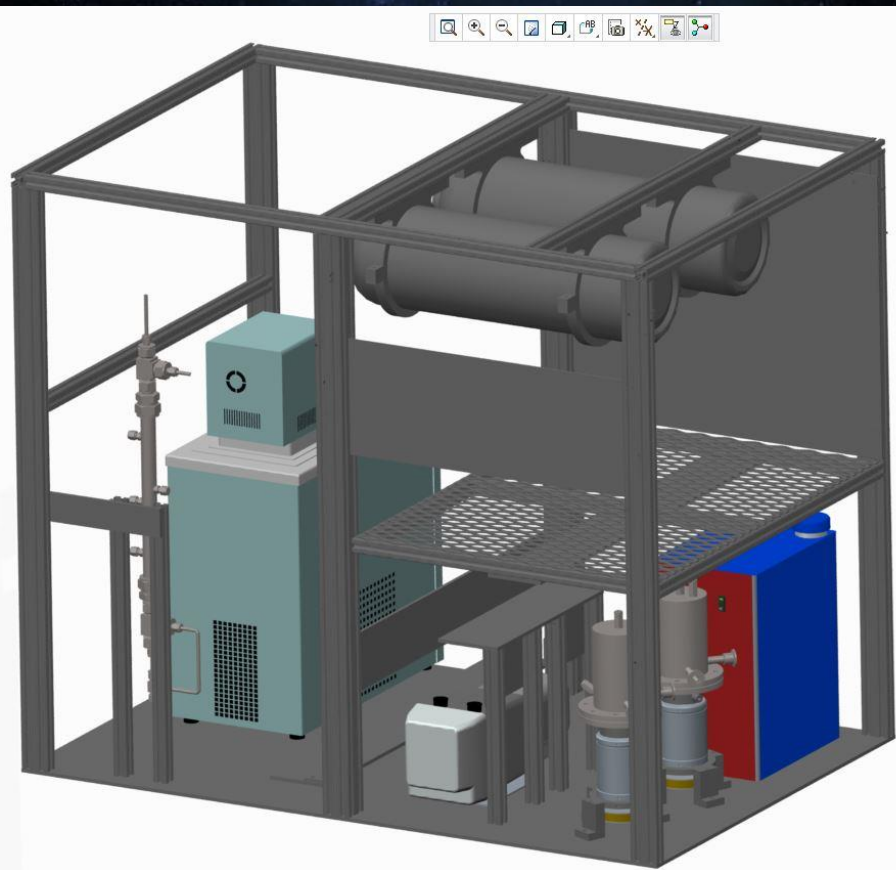


Copper Heat Exchanger

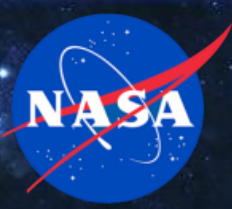


CO<sub>2</sub> Freezers and Chiller

# 3D Model of the APM Major Components

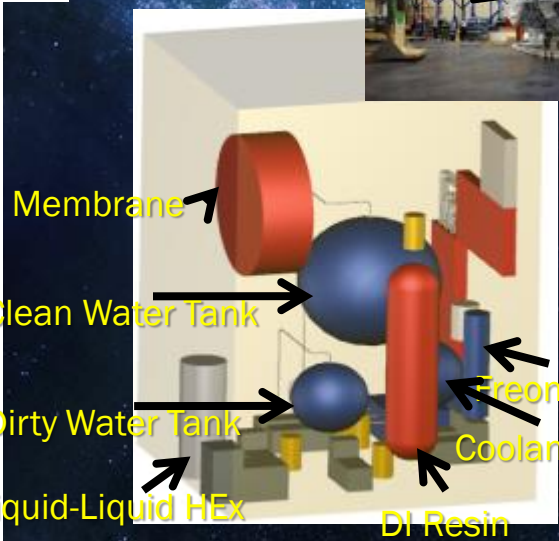
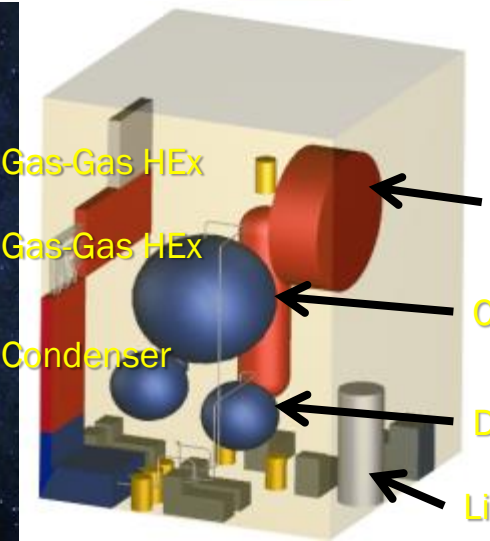
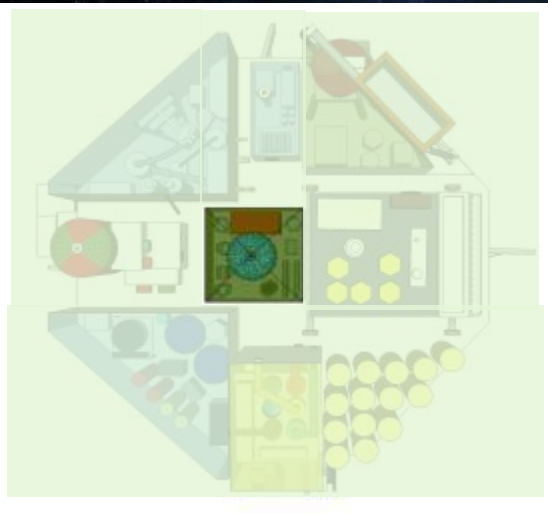


Major component mass = 154 kg

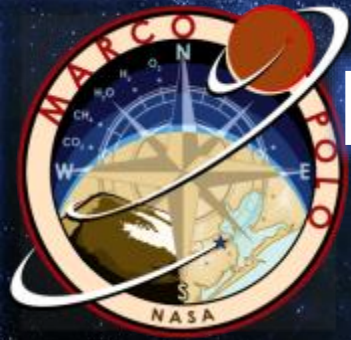


# Water Cleanup Module (KSC)

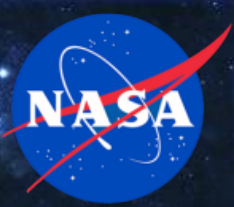
- Tested with Water Processing Module at JSC
- Used to recycle fuel cell water from the MMSEV to H<sub>2</sub> and O<sub>2</sub>
- MMSEV = Multi Mission Space Exploration Vehicle



Ion exchange resin instead of membrane separator included in the final version



# Lander and Soil Processing Module (KSC)



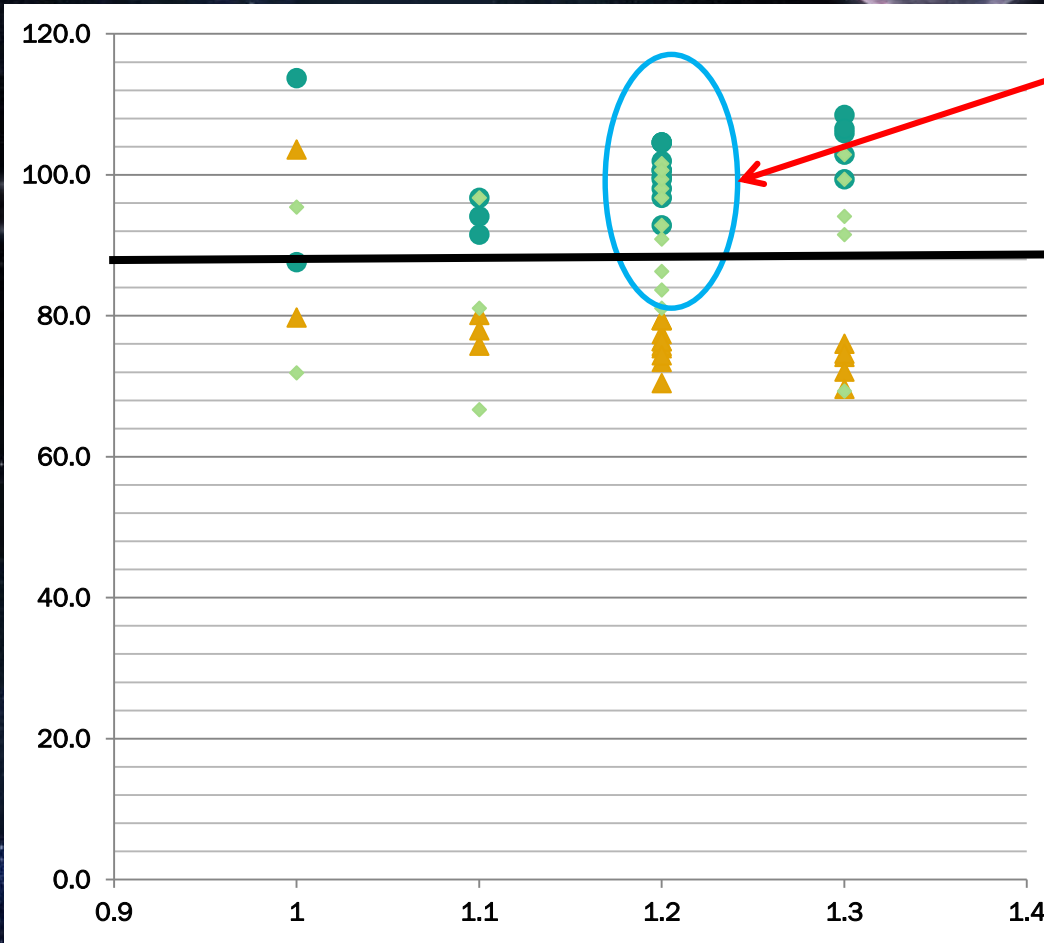
Van Townsend (KSC/ESC) with MARCO POLO lander and Soil Processing Module (under construction)



RASSOR (Regolith Advanced Surface Systems Operations Robot) will feed the hopper (2 x 40 kg drums, 25 cm/s, 60% on duty time)



# CO<sub>2</sub> Freezer Testing

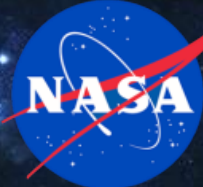


- Avg. Capture Rate =  $99 \pm 3$  g/hr at 1.2 SLPM (1.4 hr test)
- Avg. Sublimation Rate =  $95 \pm 8$  g/hr (1.4 hr test)
- Avg. Capture Fraction =  $79 \pm 3\%$
- Exceeds 88 g/hr requirement
- Better performance than test stand!

88 g/hr Requirement

- ▲ % CO2 Capture
- CO2 Collection Rate, g/hr
- ◆ CO2 Sublimation Rate in 1.4 hr, g/hr

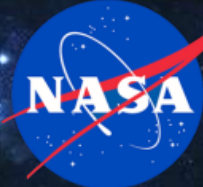
Mars Atmosphere Simulant Flow Rate, SLPM



# Long-Duration Tests Were Successful

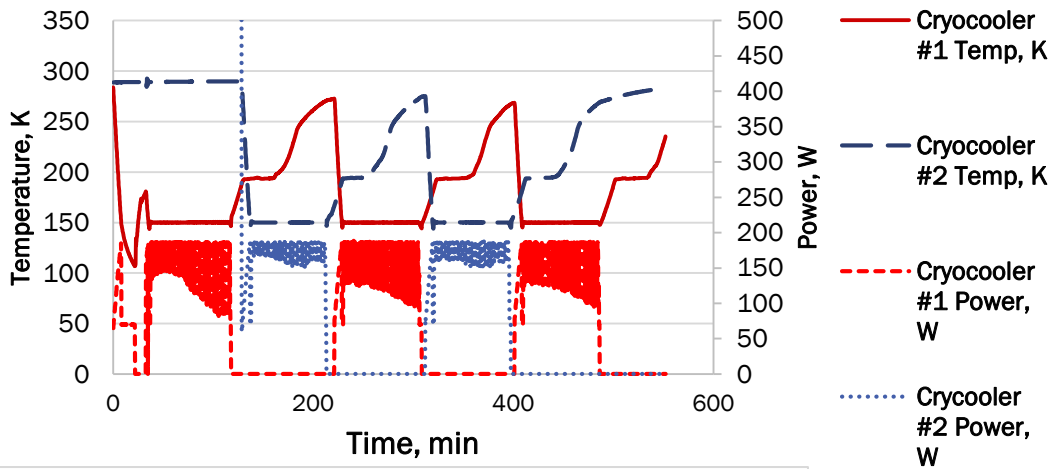
<b>Run No.</b>	<b>1</b>	<b>2</b>	<b>3</b>	<b>4</b>
Sabatier Run Duration	7.0 h	7.0 h	7.0 h	7.0 h
Gas Composition	CO <sub>2</sub>	CO <sub>2</sub>	Mars Gas	Mars Gas
<b>Average CO<sub>2</sub> Freezing Rate (Goal = 88 g/h)</b>	<b>102 g/h</b>	<b>100 g/h</b>	<b>102 g/h</b>	<b>99 g/h</b>
<b>Average Fraction of CO<sub>2</sub> Frozen</b>	<b>80%</b>	<b>70%</b>	<b>70%</b>	<b>73%</b>
Average Cryocooler Power	139 W	150 W	158 W	138 W
<b>Average “Lift” Needed to Freeze CO<sub>2</sub></b>	<b>0.19 W/g/h</b>	<b>0.21 W/g/h</b>	<b>0.22 W/g/h</b>	<b>0.20 W/g/h</b>
Average CO <sub>2</sub> Supply Rate to Freezers	128 g/h	142 g/h	146 g/h	135 g/h
<b>Average CH<sub>4</sub> Production Rate</b>	<b>32 g/h</b>	<b>32 g/h</b>	<b>32 g/h</b>	<b>32 g/h</b>
<b>Average CH<sub>4</sub> Purity</b>	<b>99.9%</b>	<b>99.9%</b>	<b>96.0%*</b>	<b>99.9%</b>
<b>Average H<sub>2</sub>O Produced</b>	<b>67 g/h</b>	<b>69 g/h</b>	<b>64 g/h</b>	<b>70 g/h</b>
Missing H <sub>2</sub> O (vs. 72 g/h)	6.9%	4.2%	11.1%	2.8%

\*Due to pressure losses during manual draining of Sabatier water condenser



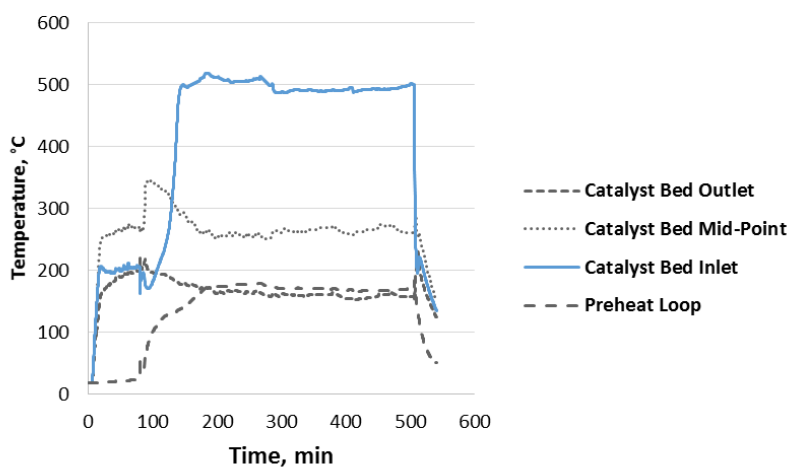
# Selected Results from Long-Duration Tests

### Cryocooler Temperature and Power



CO<sub>2</sub> Freezer Cold Head Temperatures and Cryocooler Power Consumption during the Third Run of the 7-h Integrated Test Series

### Sabatier Reactor Temperatures



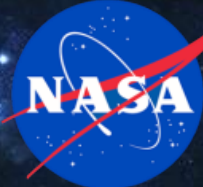
Sabatier Reactor Temperatures during the Second Run of the 7-Hour Integrated Test Series



# Conclusions from the Long-Duration Tests

- **CO<sub>2</sub> Freezer Subsystem operates well**
  - Exceeds 88 g/h freezing and supply rate
  - Freezes ~70% of incoming CO<sub>2</sub>
  - Provides valuable data for power to freeze CO<sub>2</sub> at Mars pressure
    - Averages 0.22 W/g CO<sub>2</sub> frozen = only 108% of theoretical
  - Contributes to Human Mars Mission ISRU system designs, e.g. 680 W lift for 3.1 kg CO<sub>2</sub>/h
- **Sabatier Subsystem also operates well**
  - New reactor is efficient
  - Recycling system (membrane module + recycle pump) works well (but recycle pump failed recently)
  - Pure CH<sub>4</sub> obtained at expected rate
  - ~6% of water is missing (<1% of loss is in CH<sub>4</sub>)



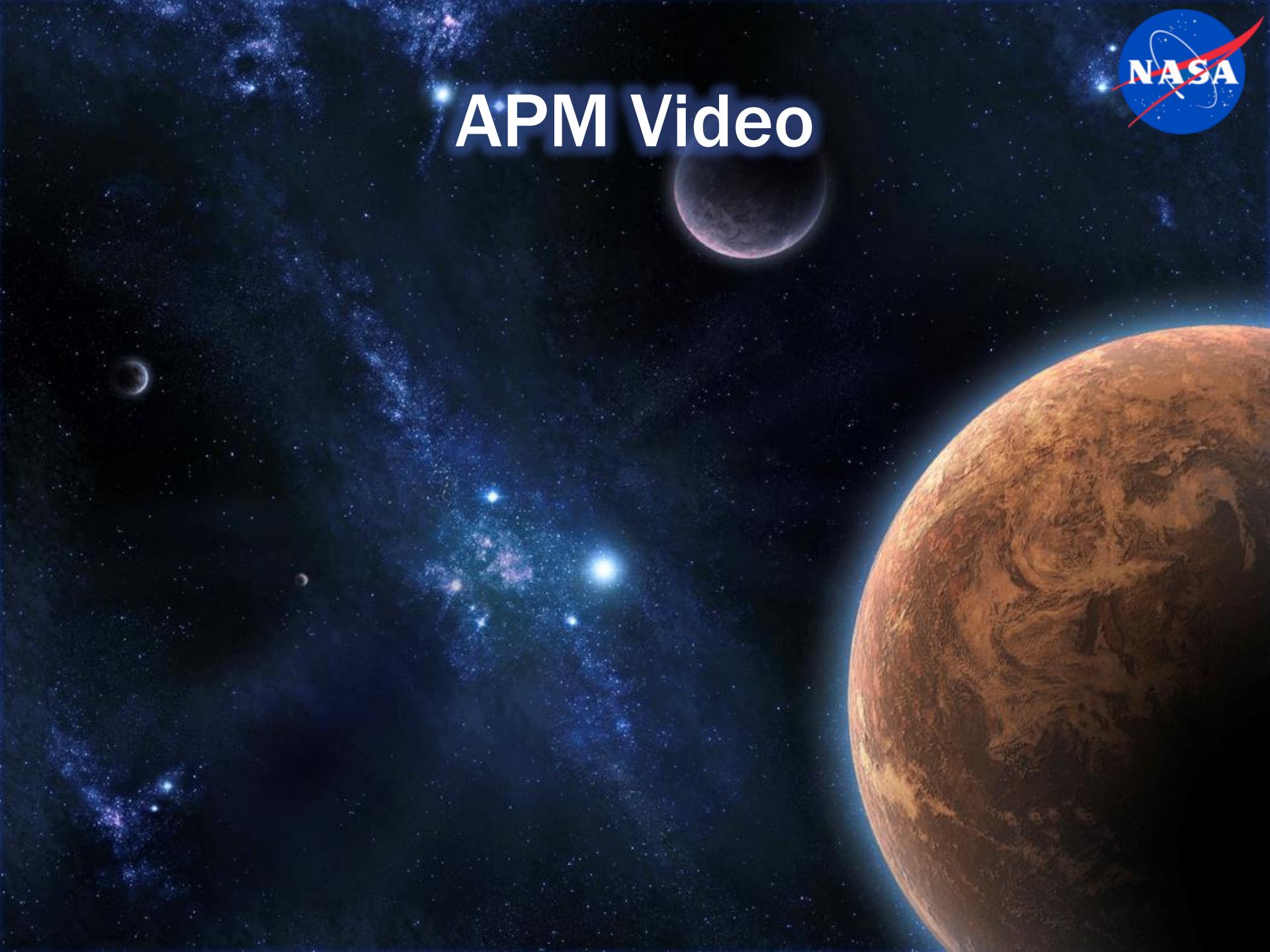


# Recent Work and Current Status

- Additional integrated tests performed
- Faster and slower production rates tested
  - 1.0-1.6 SLPM feed to CO<sub>2</sub> Freezers (87-71% frozen; 4800-5400 J/g)
  - Sabatier works at 0.3 to 1.2 SLPM CO<sub>2</sub> (0.75 SLPM nominal, 550° C max T)
  - Some CO observed in CH<sub>4</sub> after higher flow rates (catalyst damaged)
- Better LabVIEW automation implemented (sequences)
- Performed “virtual” integrated MARCO POLO tests with other systems at KSC in May and September – Hardware integration planned in FY17
- Ran Sabatier Subsystem w/Mars Gas Simulant – Good results. But Ar & N<sub>2</sub> in CH<sub>4</sub>
- Now modeling CO<sub>2</sub> Freezers and Sabatier for scaling up to full-scale versions
- Long Term Goal is to continue to refine ISRU technologies for potential robotic Mars missions using Mars Pathfinder (2026/28)

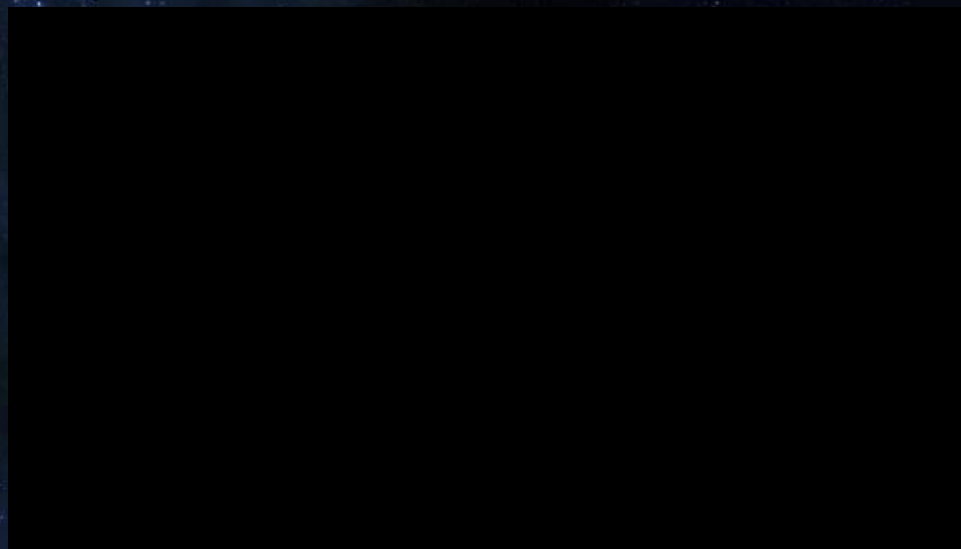


# APM Video

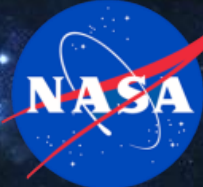




# Video of Virtual Integrated Test



<https://www.youtube.com/watch?v=cRLnAeL3wdU>



# Challenges

- Trade Studies based on small-scale tests and modeling followed by testing of full-scale components and subsystems up to TRL 6
- Funding (as usual)



## Future Direction

### [Tony's Wish List – Same As 2 Weeks Ago]

- NASA has restarted its ISRU Project
- NASA should fully embrace ISRU
- Integrated human exploration of the inner solar system
- Moon, asteroids, Mars moons, Mars
- Commercial development of key technologies in partnership w/NASA to reduce costs
  - i.e. shared funding
  - Habitats, ISRU, spacecraft, launch vehicles, etc.
  - Asteroid mining
- Pick an architecture and stick with it for >>8 years