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Characterization of DBD Plasma Actuators Performance without External Flow – Part I: Thrust-Voltage Quadratic Relationship in Logarithmic Space for Sinusoidal Excitation

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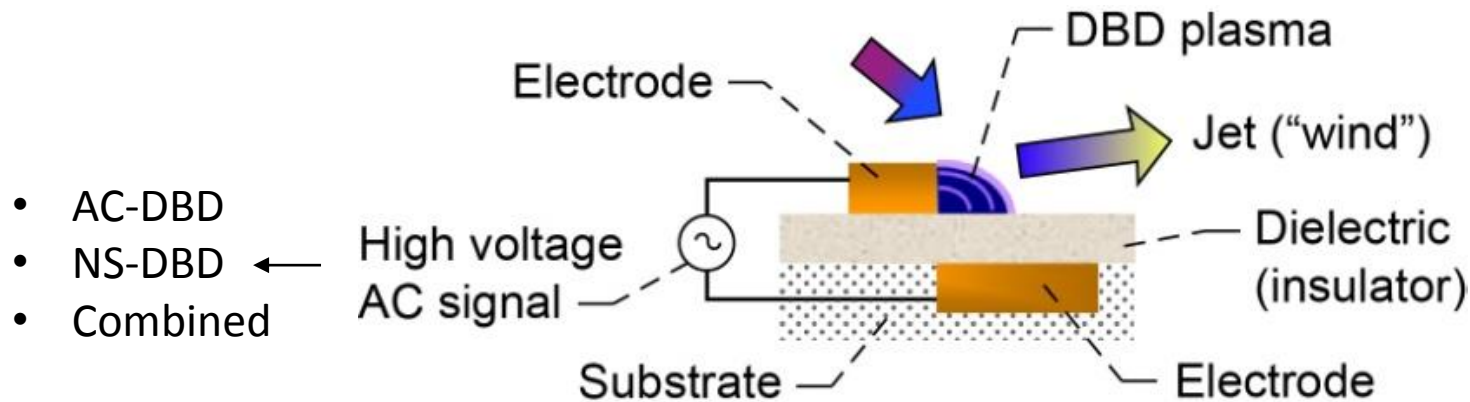
13-17 June , 2016, Washington, DC



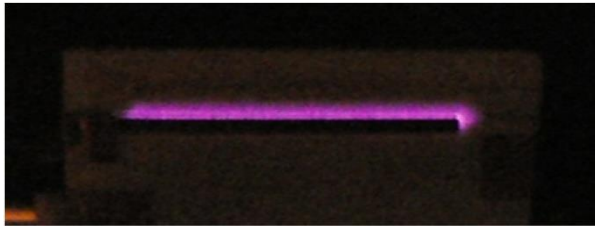
OUTLINE

- Introduction
 - DBD actuator
 - DBD actuator thrust
- Test setup
 - Actuator test article
 - Suspended setup
 - Instrumentation
 - Humidity conditions
- Thrust measurement methodology
 - Burn-in
 - Voltage-frequency sweeps
 - Data correction with anti-thrust
- Results
 - Thrust vs voltage on log-log scale
 - Quadratic curve fit
- Concluding remarks

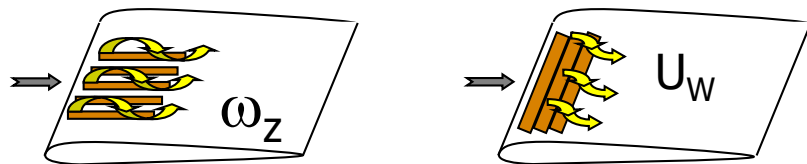
DBD Plasma Actuator



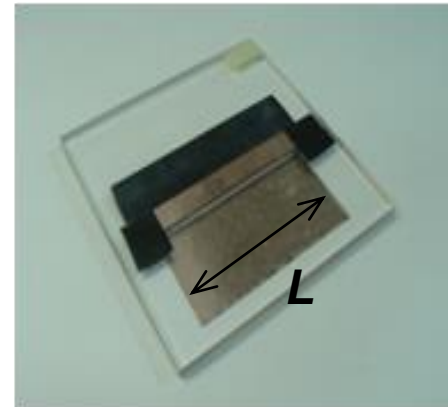
DBD ACTUATOR SCHEMATIC



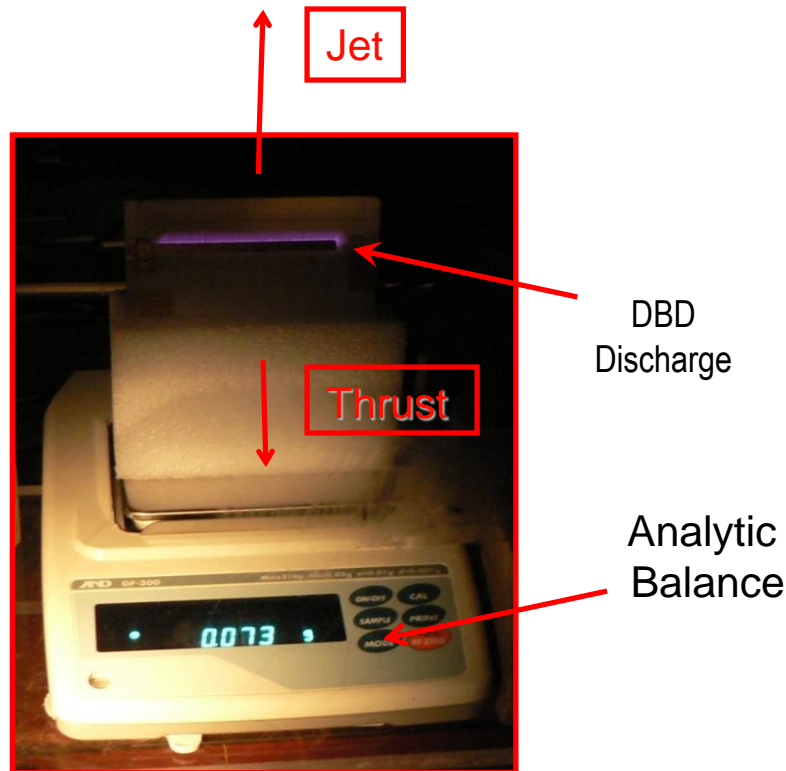
TYPICAL DISCHARGE



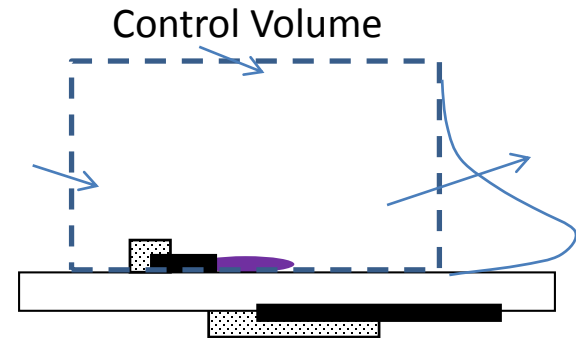
APPLICATIONS



Characterization of Aerodynamic Performance - Thrust Measurements



Thrust read by balance is equal to the momentum generated by the actuator



Surface-parallel direction x:

$$\frac{F_{\text{plasma}}}{L_z} + \frac{F_{\text{shear}}}{L_z} = \underbrace{\rho \int_{\text{right}} v_x^2 dy}_{\text{I}} + \underbrace{\rho \int_{\text{top}} v_x v_y dx}_{\text{II}} - \underbrace{\rho \int_{\text{left}} v_x^2 dy}_{\text{III}} + \underbrace{\int_{\text{right}} p dy}_{\text{IV}} - \underbrace{\int_{\text{left}} p dy}_{\text{V}},$$

Thrust \approx Momentum

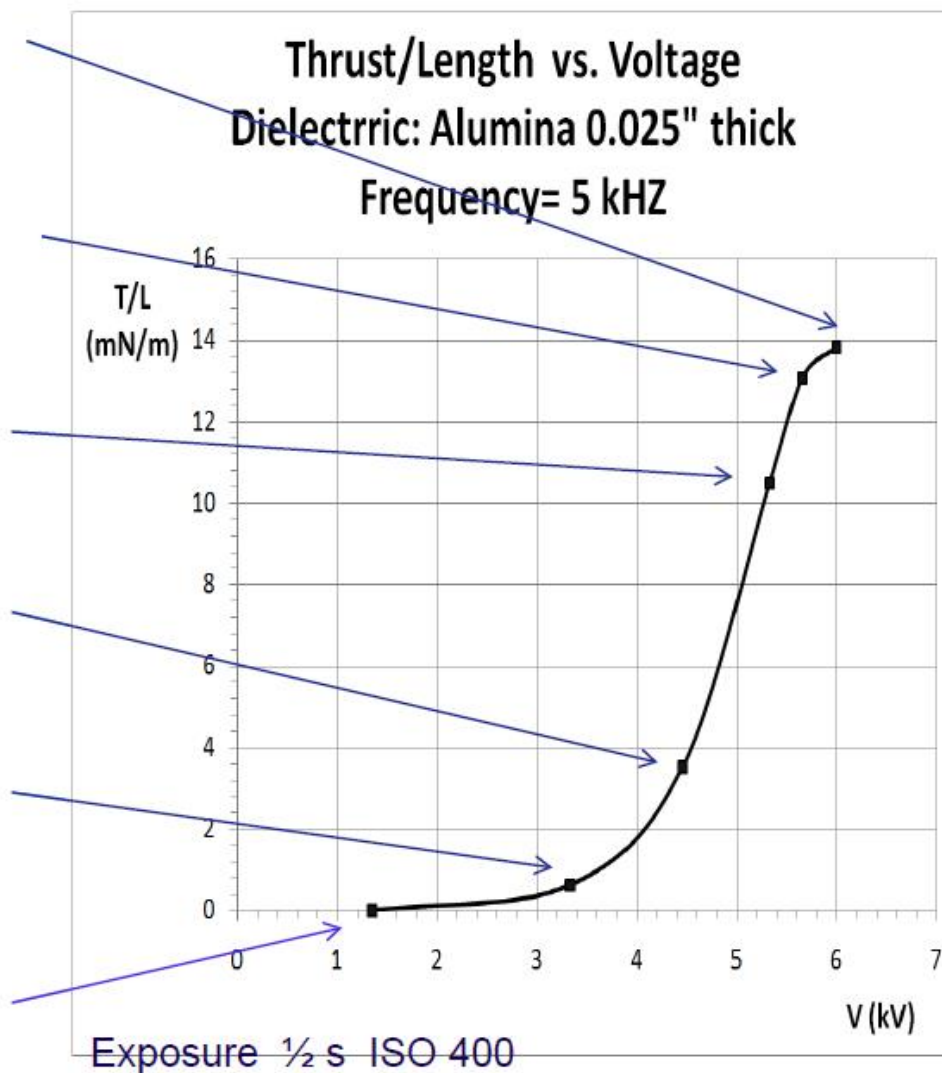
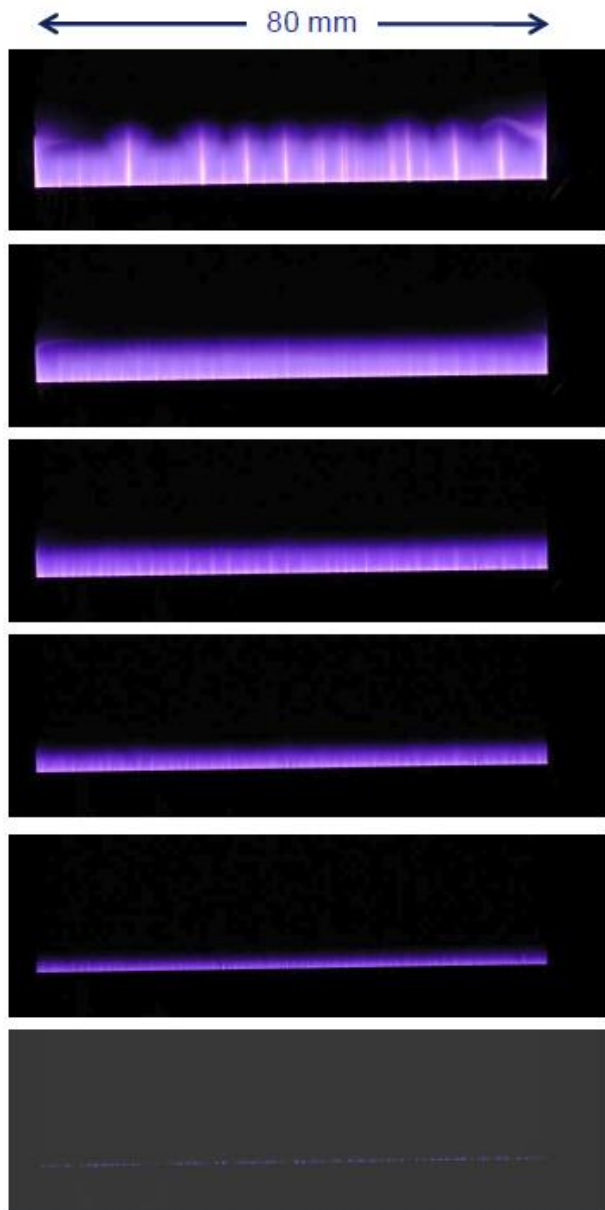
If wall shear is negligible

- Supported by calculation based on Glauert self-similar wall jet - Opaitis et al 2010¹ data
- Contradiction with Durscher & Roy 2012²

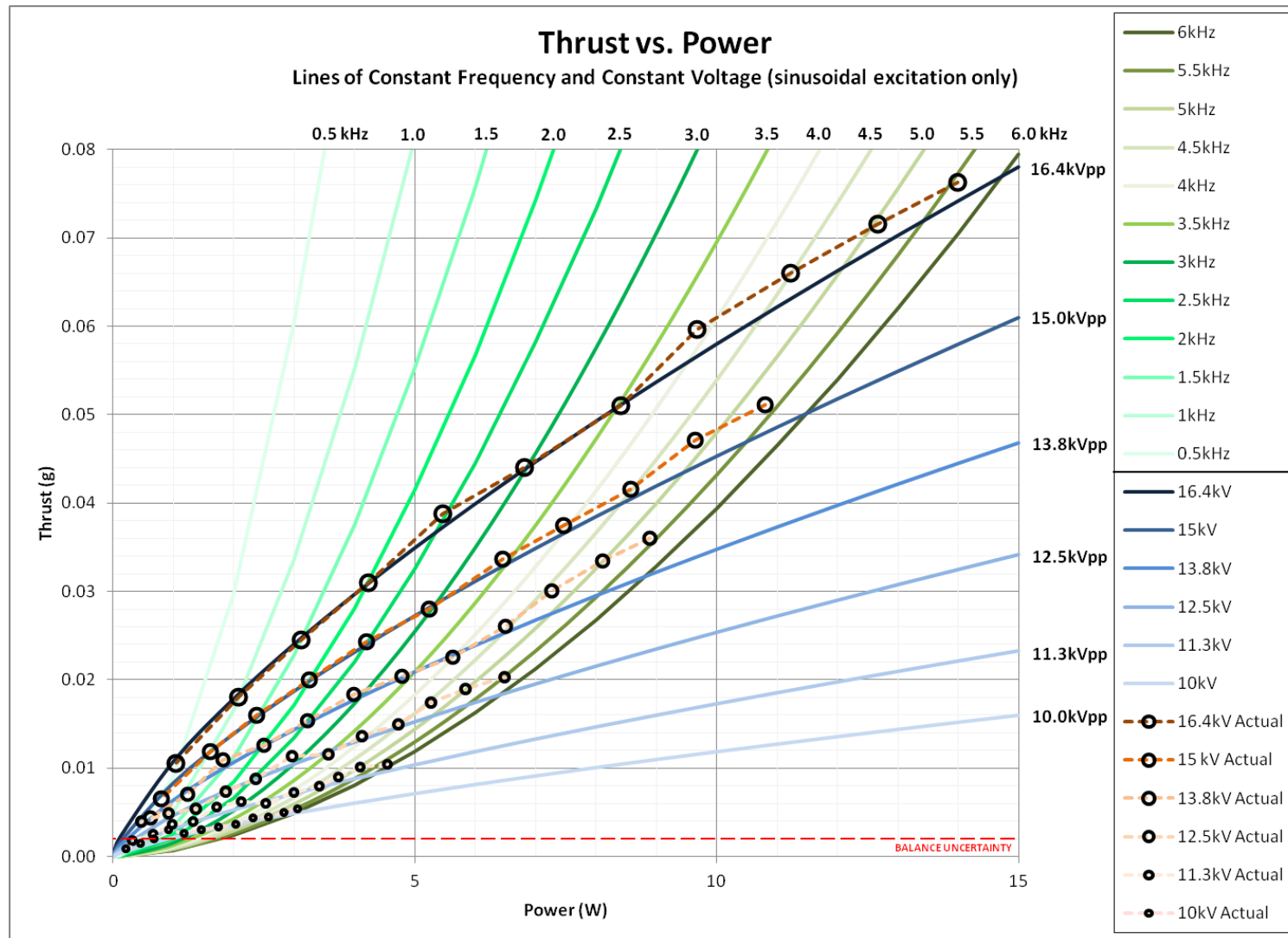
¹ Opaitis, D. F., et al, "Surface Plasma Induced Wall jets," AIAA-2010-469

² Durscher, R., and Roy, S., "Evaluation of Thrust Measurement Techniques for DBD Actuators," Exp. Fluids 53, 2012, pp. 1165–1176

SAMPLE MEASUREMENT



Sample Performance Map

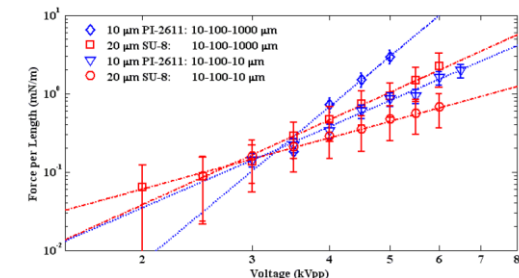
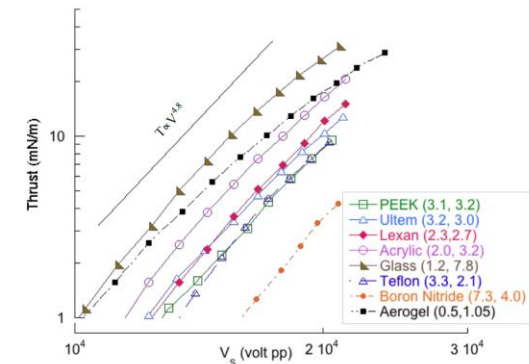
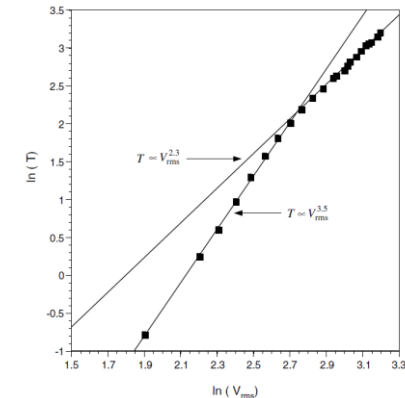


Thrust- Voltage relationships

Power law $T \propto V^m$ at const. frequency.

Proposed m values :

- *Thomas et al, 2009, AIAA Journal*
 $m = 3.5$ low voltage
 $m = 2.3$ high voltage
- Wilkinson et al AIAA-2014-2810
 $m = 4.8$
- Zito et al AIAA 2012-3091 micro-actuators
 $m = 2.2, 3.4, 3.6, 6.6$



We found a different relationship



Objectives

- Generate a quality data set for pure sine waves excitation
- Find thrust-voltage- frequency relations
- Provide bench mark data for numerical simulation
- Provide predictive capability



Thrust Measurement Approach

- Actuator construction
 - Test setup
 - Pure sine waves excitation
 - Low humidity
 - Burn-in procedure
 - Anti thrust data correction
-
- Builds upon Ashpis & Laun AIAA Paper 2014-0486
(also NASA/TM—2014-218115)

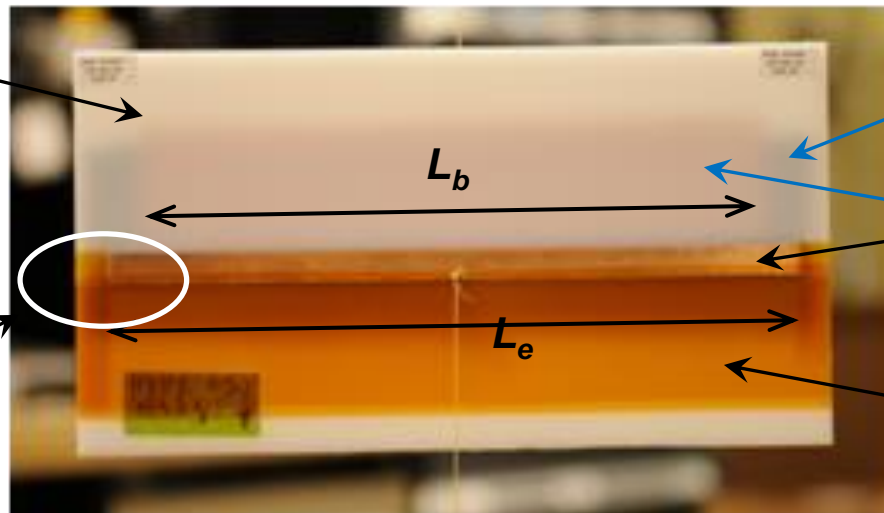
Actuator Test Articles

Nominal Thicknesses: 1/16", 1/8", 1/4"

Covered Electrode length $\approx 10"$

HDPE
(High Density
Poly Ethylene)
 $\epsilon = 2.3$

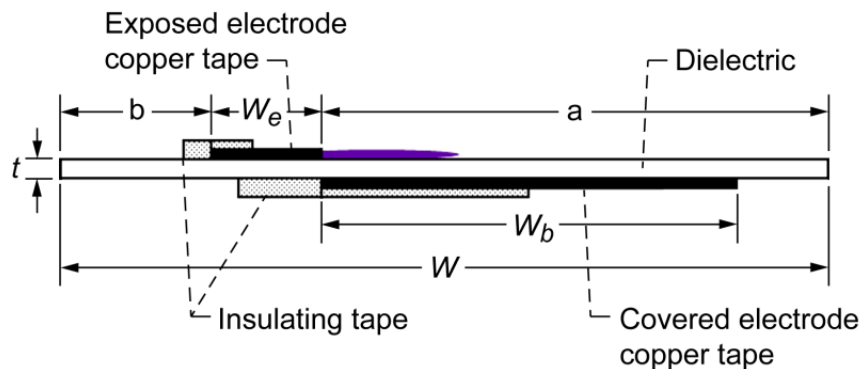
Super Corona
Dope[®]



3M Scotch-Seal
#229

Copper tape
3M #1181

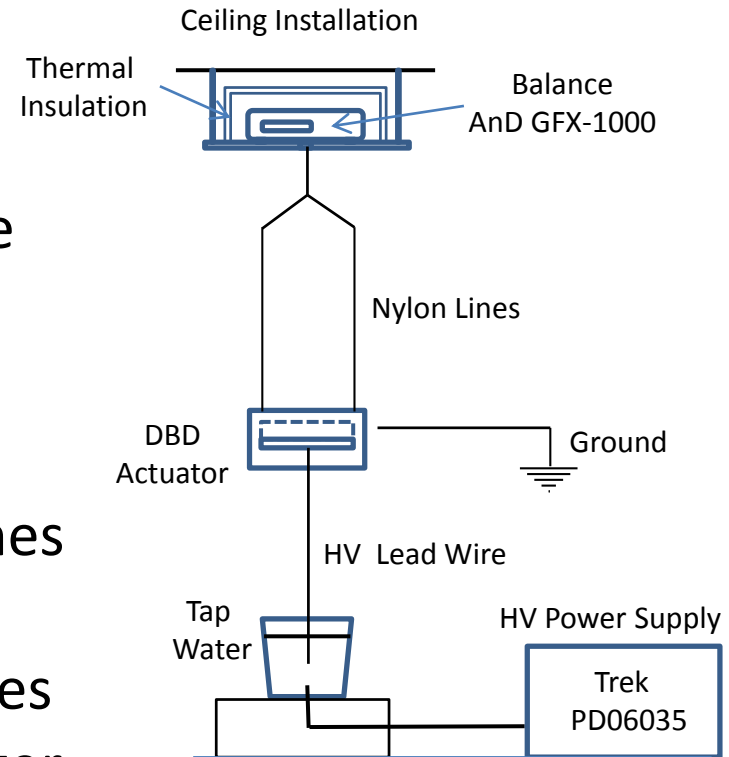
Kapton[®]
3M #5413



Exact dimensions and
details – see paper

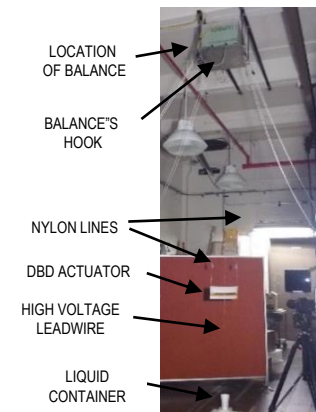
TEST SETUP:

- Out in the room without enclosure
- Balance installed near ceiling
- Balance thermally insulated to eliminate temperature drift
- Test article suspended on nylon lines
- High voltage applied via a liquid interface eliminates lead wire forces
 - Lead wire immersed in tap water
 - Power supply charges tap water



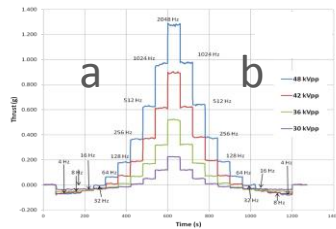
Excitation Voltage

- Waveform- Sine Wave
 - Distortion monitoring



Humidity effects

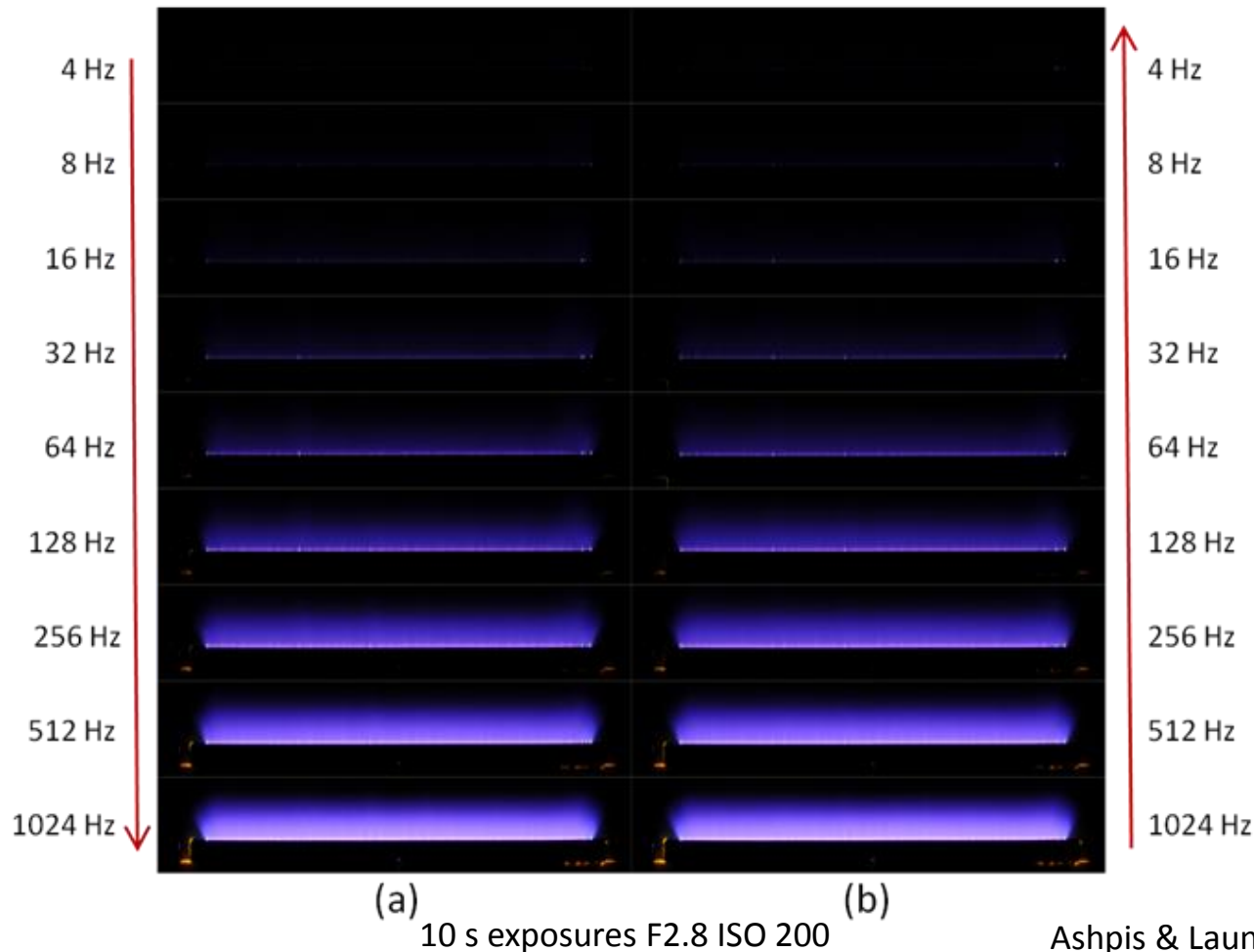
- Benard et al 2009 AIAA-2009-488
 - Peak wall-jet velocity decreases with humidity
- Ashpis & Laun AIAA-2014-0486
 - Thrust decreases with humidity (44%)
- Wilkinson et al AIAA-2014-2810
 - Material dependence – water retention



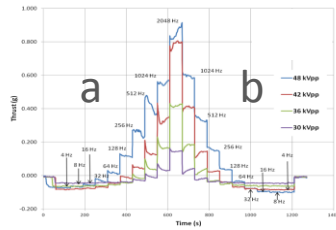
Humidity Effects

48 kVpp Frequency Sweep

“Dry” RH 18%, Dew Point 33 °F



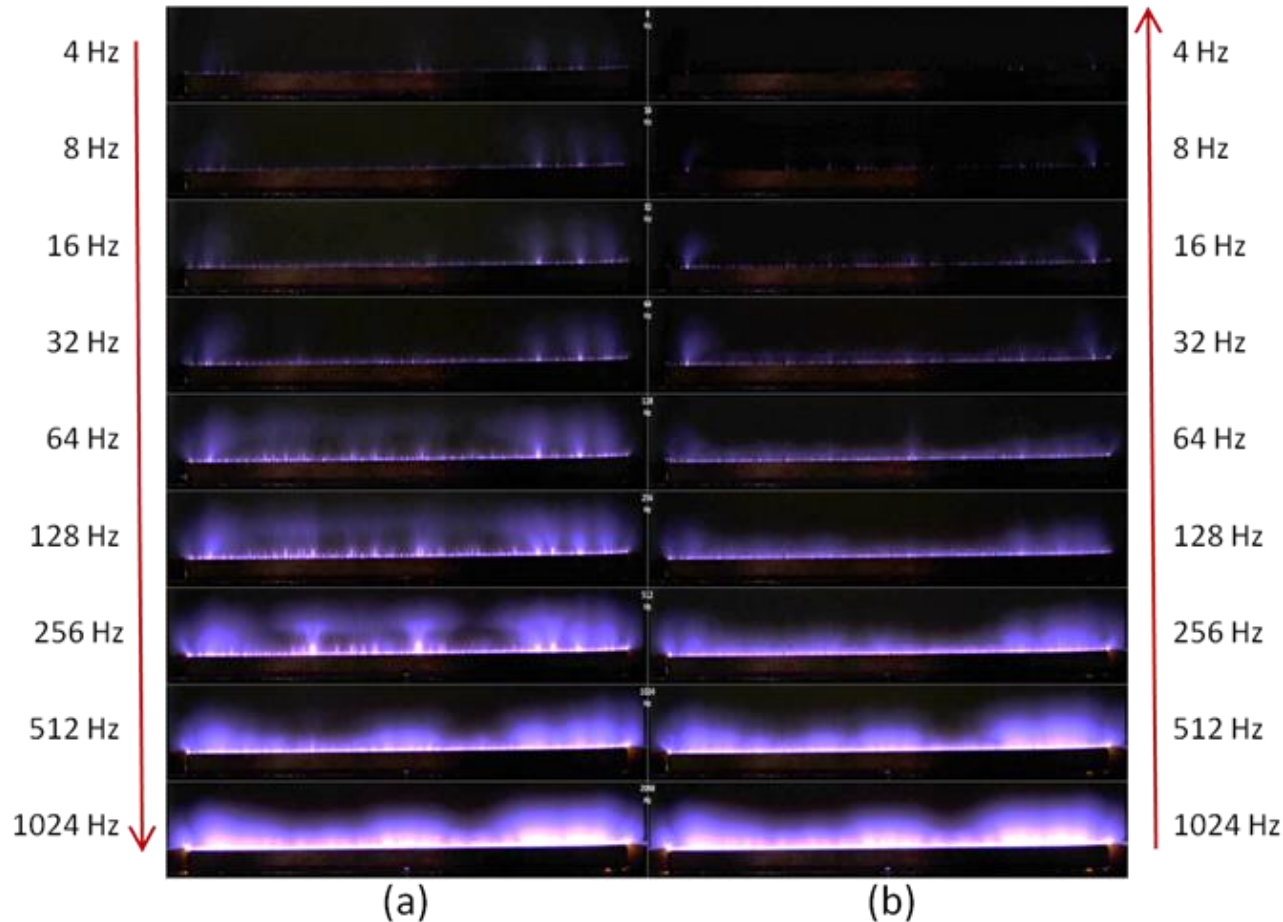
Ashpis & Laun AIAA-2014-0486



Humidity Effects – Cont.

48 kVpp Frequency Sweep

“Humid” RH 50%, Dew Point 57 °F



10 s exposures F2.8 ISO 200

Ashpis & Laun AIAA-2014-0486

Ambient Humidity Conditions

All tests in dry conditions

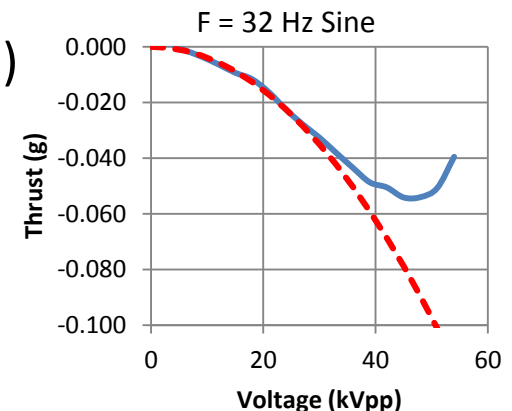
Actuator Nominal thickness	Dew Point (DP)	Relative Humidity (RH)	Temp
inch	° F	%	° F
1/16	39	22	81
1/8	37	26	74
1/4	37	26	74

Anti-thrust Data Correction

Anti-thrust Hypothesis (Ashpis & Laun AIAA-2014-0486):

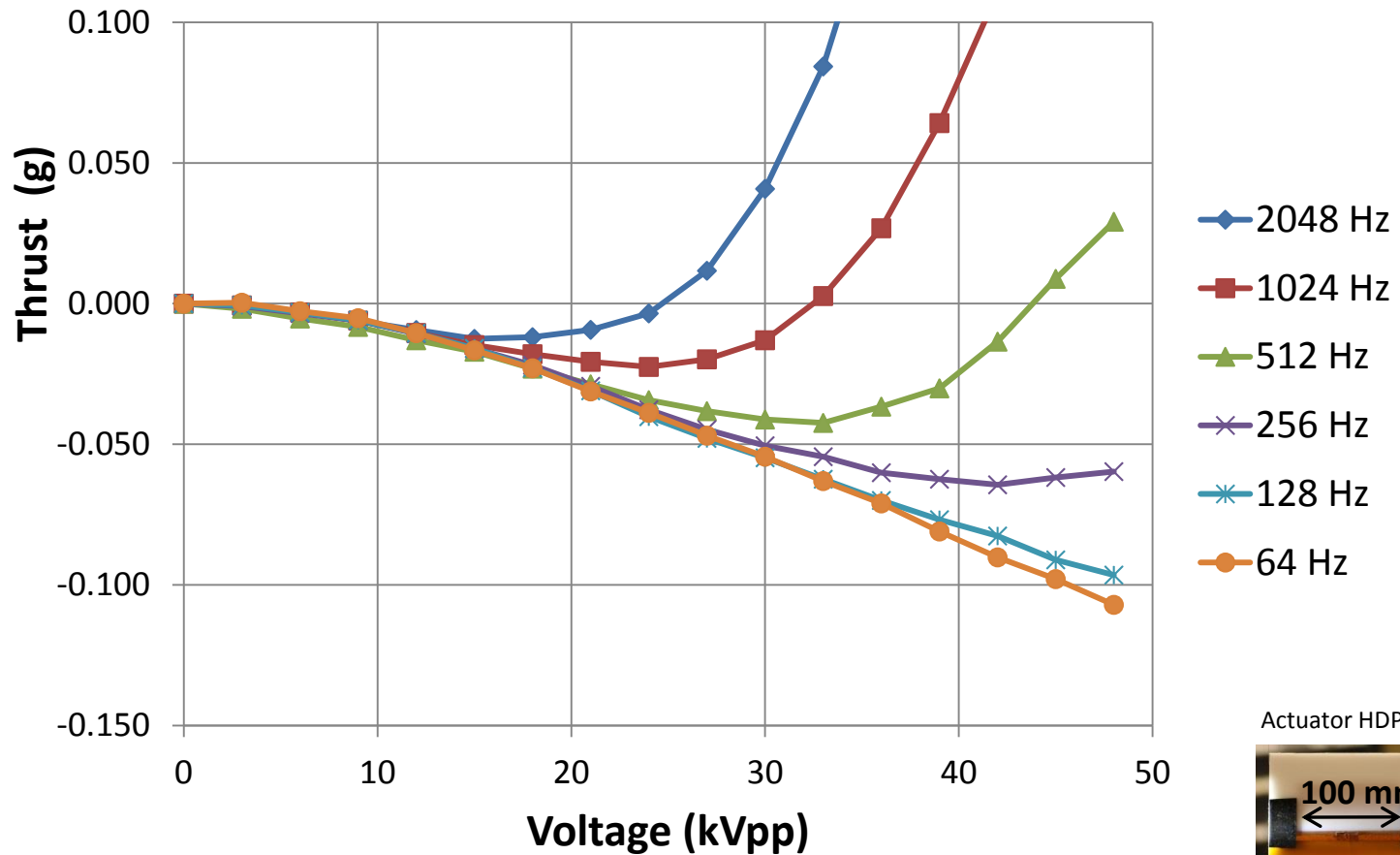
Total Thrust = Plasma Thrust + Anti-thrust

- **Plasma Thrust** is the quantity of interest for actuator performance
- It needs to be separated from the total thrust
- Anti-thrust $\sim -V^2$ (parabolic fit)
- Frequency independent
 - Observed from 4 to 64 Hz (at moderate voltages)
- Assumptions
 - Frequency independent at all frequencies
 - Extrapolated for higher voltages
- Depends on:
 - Actuator geometry & dielectric properties
 - Installation - proximity to surrounding objects and their grounding
 - Ambient conditions – Pressure, Humidity, etc. (?)
 - Actuator insulation (?)

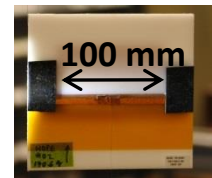


Anti-thrust:

Thrust vs. Voltage



Actuator HDPE #2



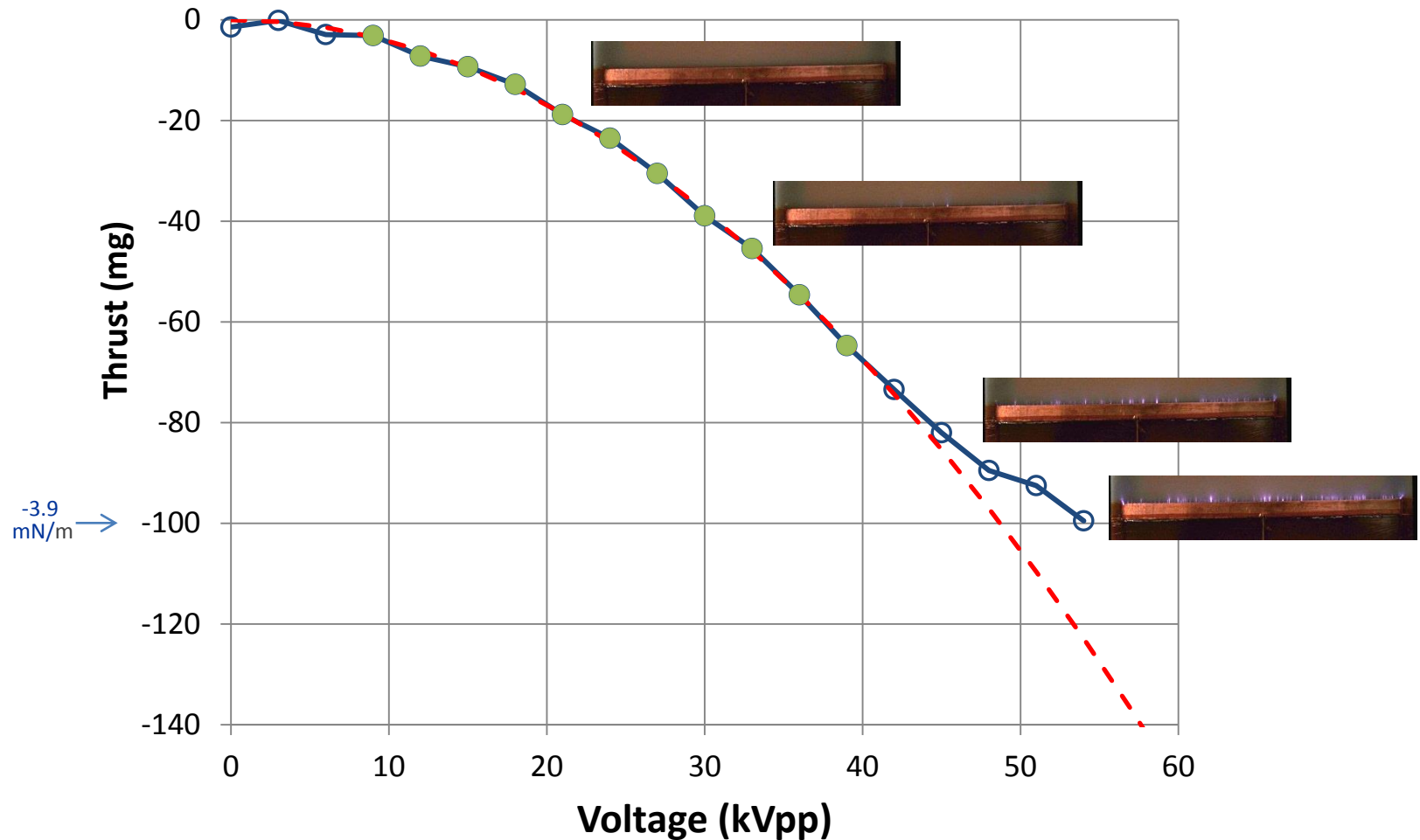
Ashpis & Laun AIAA-2014-0486

Anti-thrust:

Actuator HDPE #3



Thrust vs. Voltage @ 4Hz



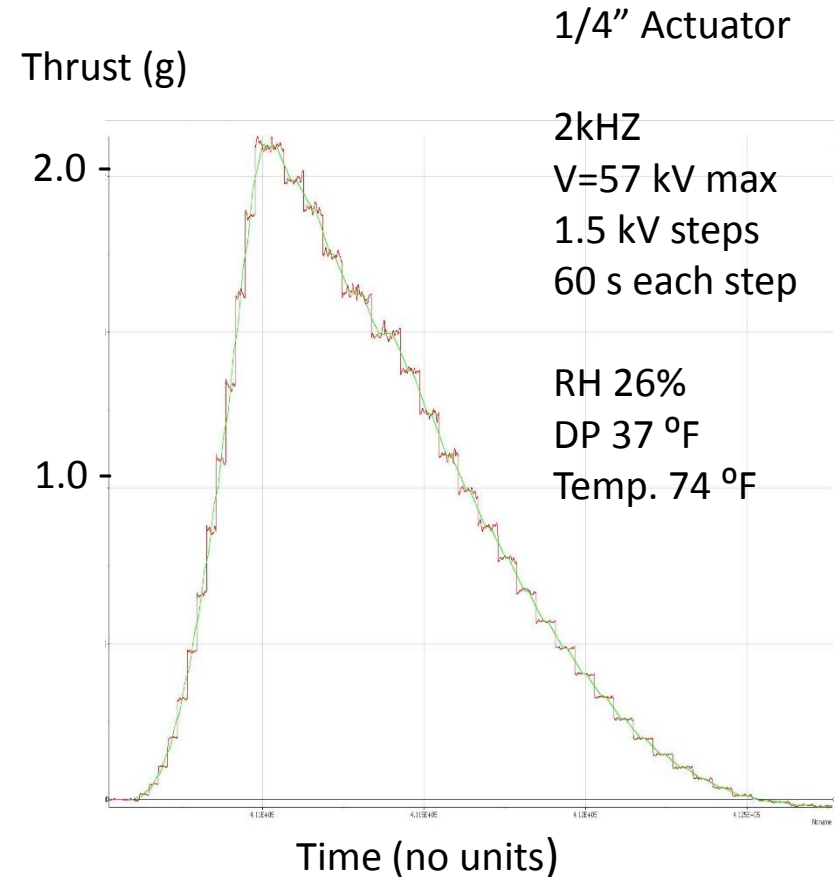
Ashpis & Laun AIAA-2014-0486

Burn-in and testing

- Set max frequency & voltage
- Step up gradually to max values
- Dwell \approx 10-20 min
- Return gradually to zero

Perform a series of tests:

- Set frequency
- Step to max voltage,
- Step down in voltage, 60 sec at each voltage.

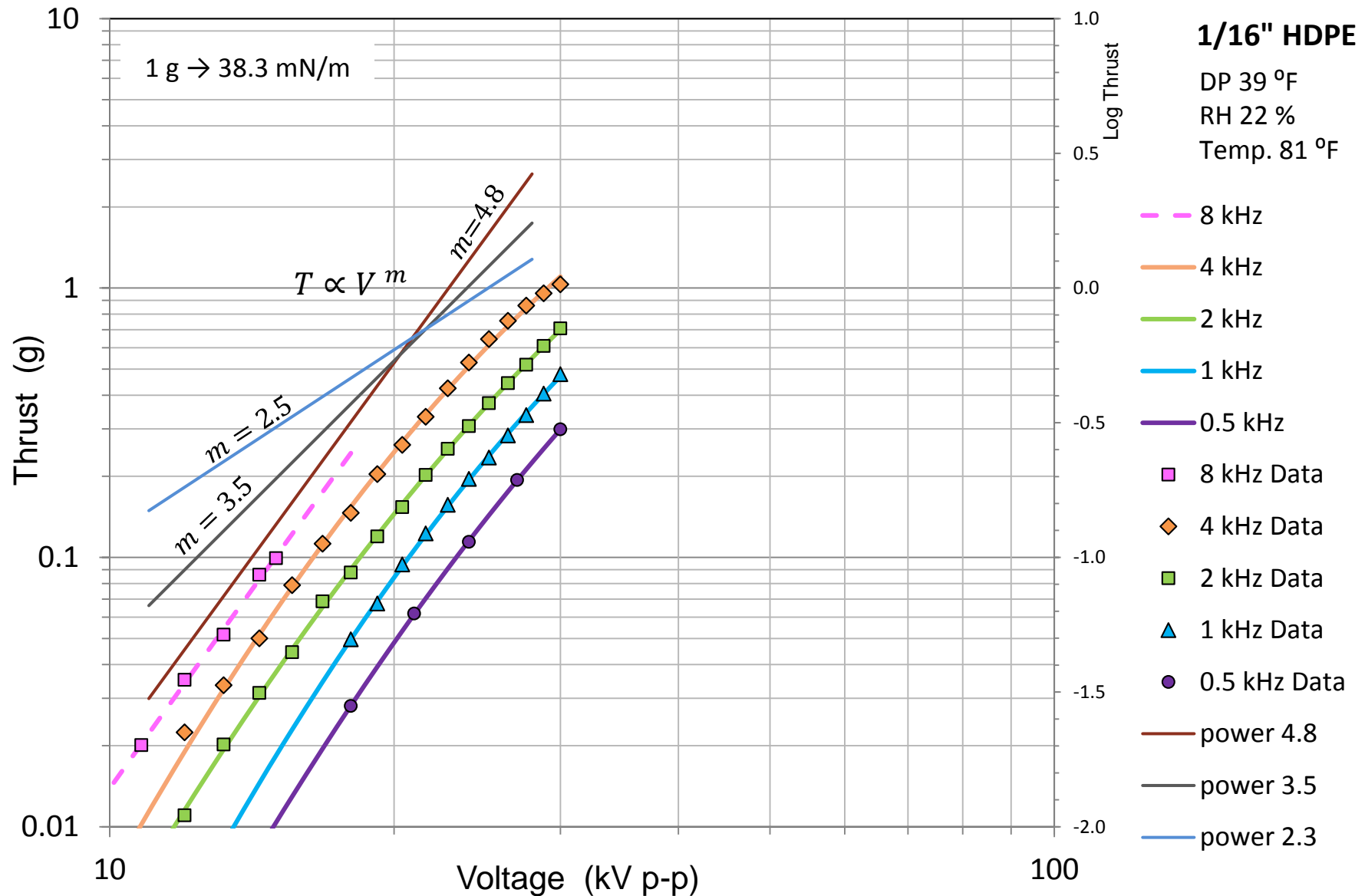


Typical test profile

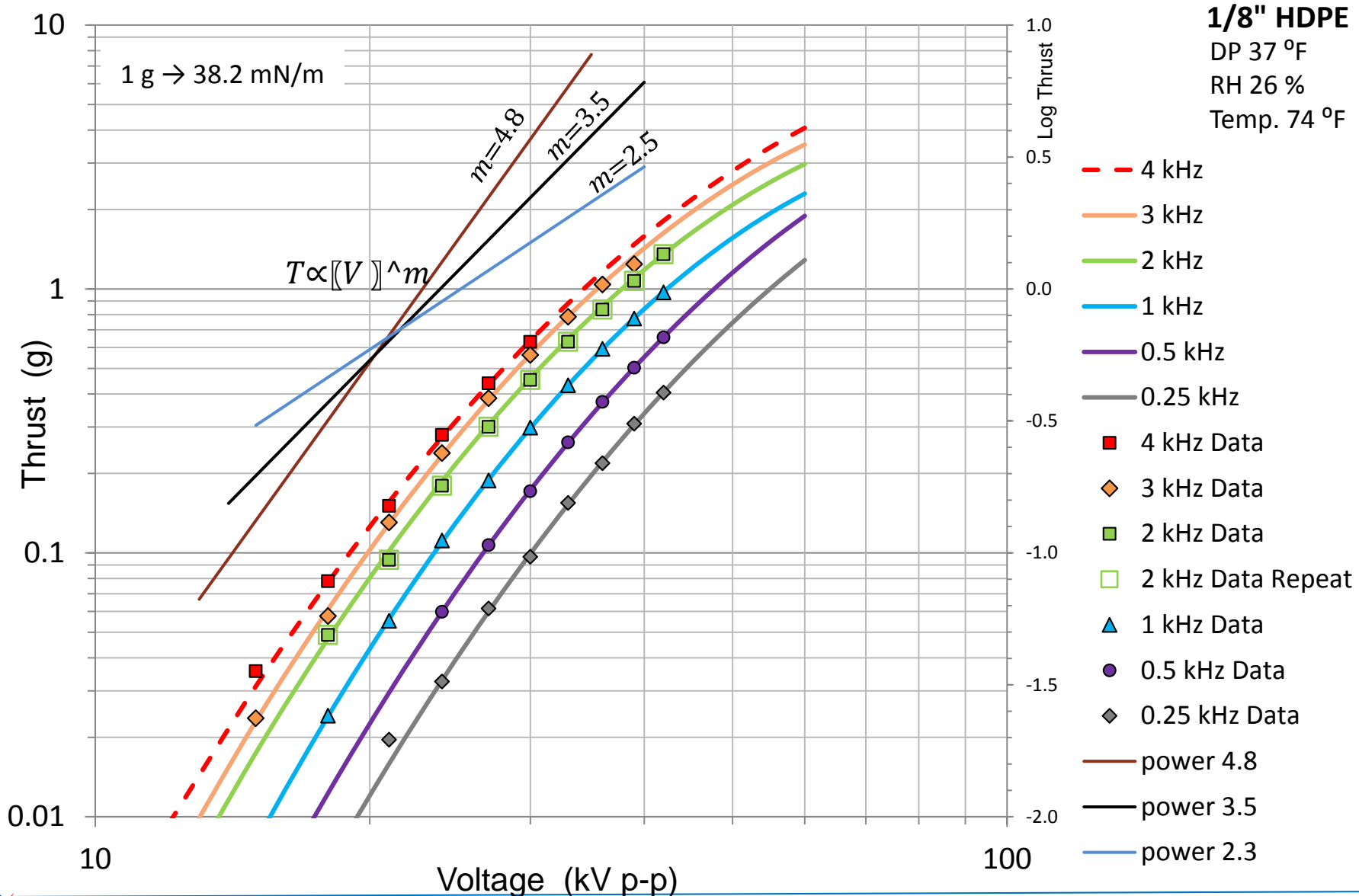


RESULTS

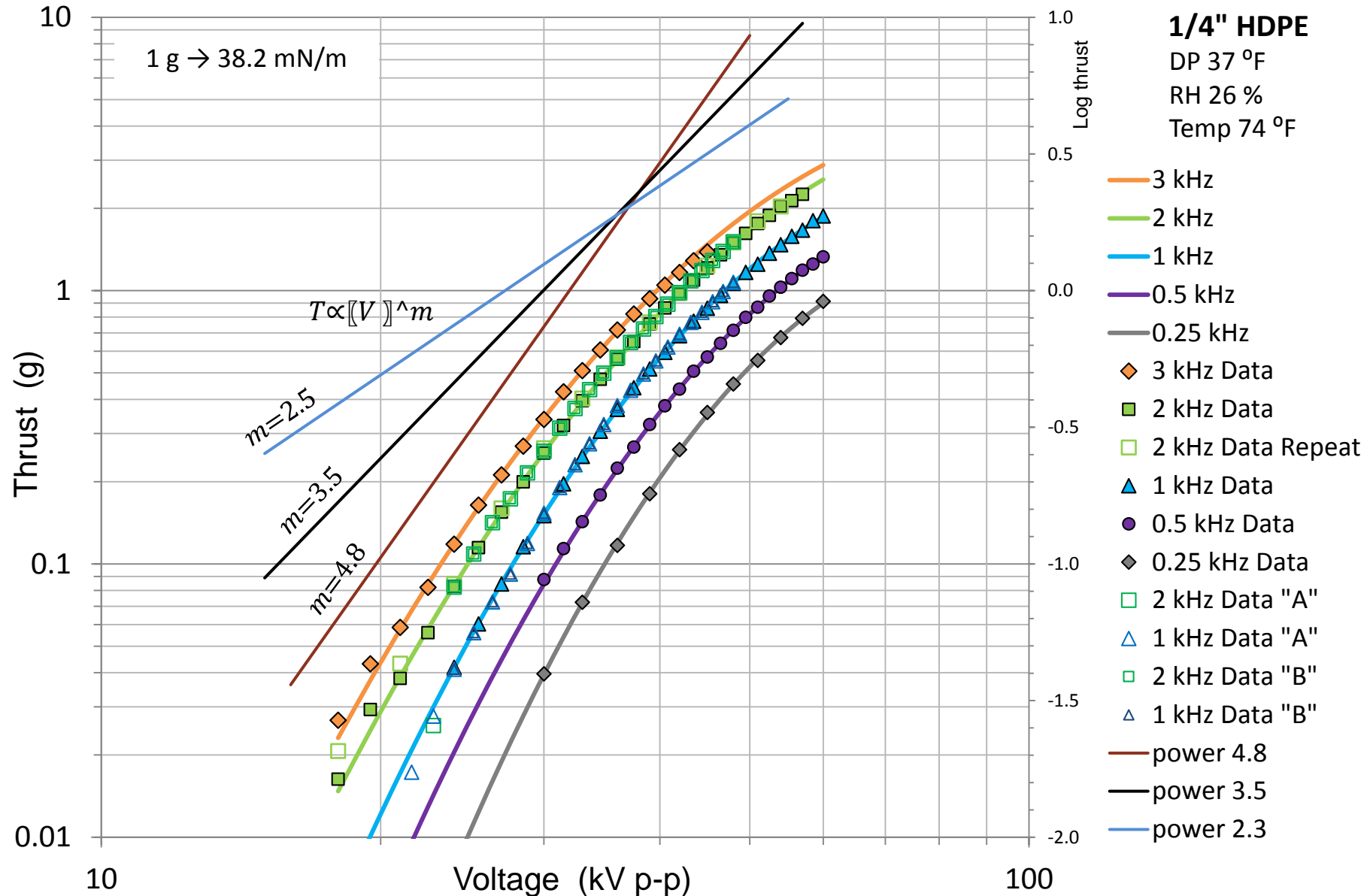
Results - 1/16" actuator



Results - 1/8" actuator



Results - 1/4" actuator



Quadratic curve fit coefficients

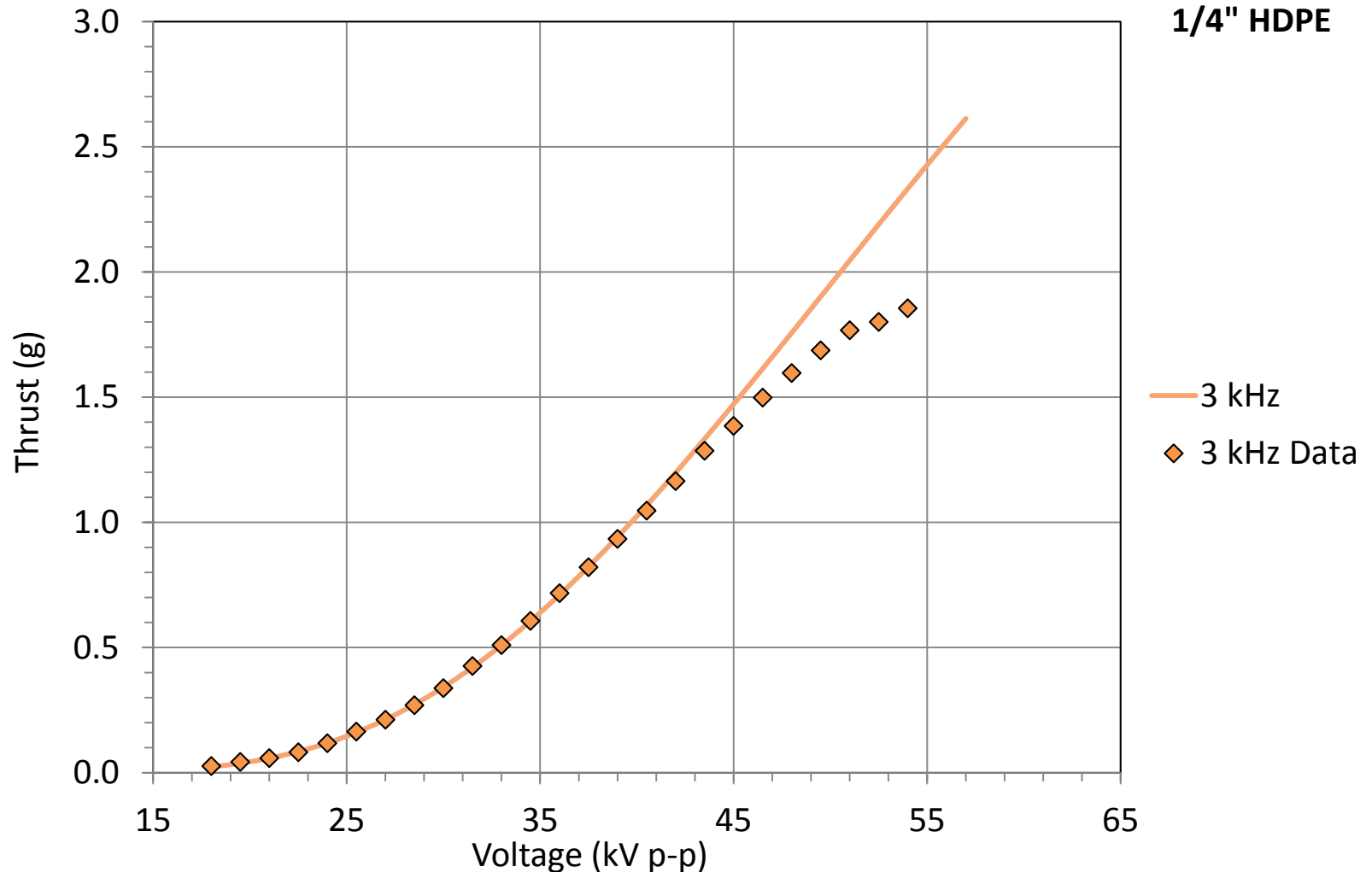
$$\log(T) = a [\log(V)]^2 + b[\log(V)] + c$$

Actuator	f (kHz)	a	b	c
1/16"	0.5	-2.820	12.328	-12.583
	1	-3.483	13.919	-13.287
	2	-2.688	11.352	-11.059
	4	-3.300	12.869	-11.767
	8	-0.236	5.410	-7.031
1/8"	0.25	-3.158	13.977	-14.759
	0.5	-3.307	14.217	-14.546
	1	-3.766	15.211	-14.780
	2	-3.349	13.636	-13.182
	3	-3.358	13.628	-13.141
	4	-3.281	13.324	-12.769
1/4"	1	-8.785	32.672	-30.248
	2	-6.282	23.973	-22.520
	3	-6.054	23.035	-21.509
	4	-4.626	18.321	-17.553
	8	-7.313	26.571	-23.800

Observed
relationships:
 $(b-c)/a \approx \text{const.}$
 $b \approx -c$

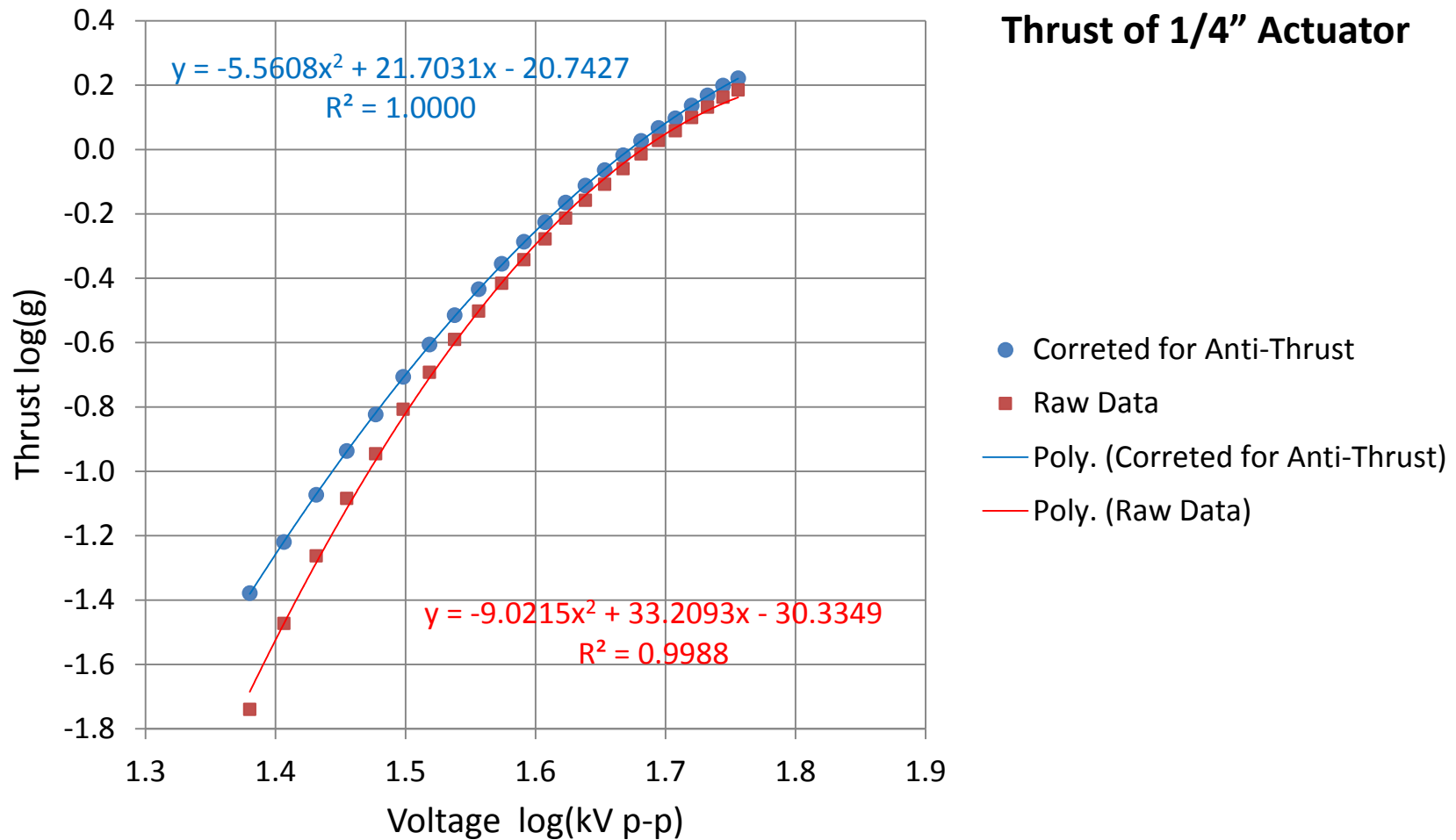
Effect of Including waveform distortions

Thrust plot linear scales - with waveform distortion



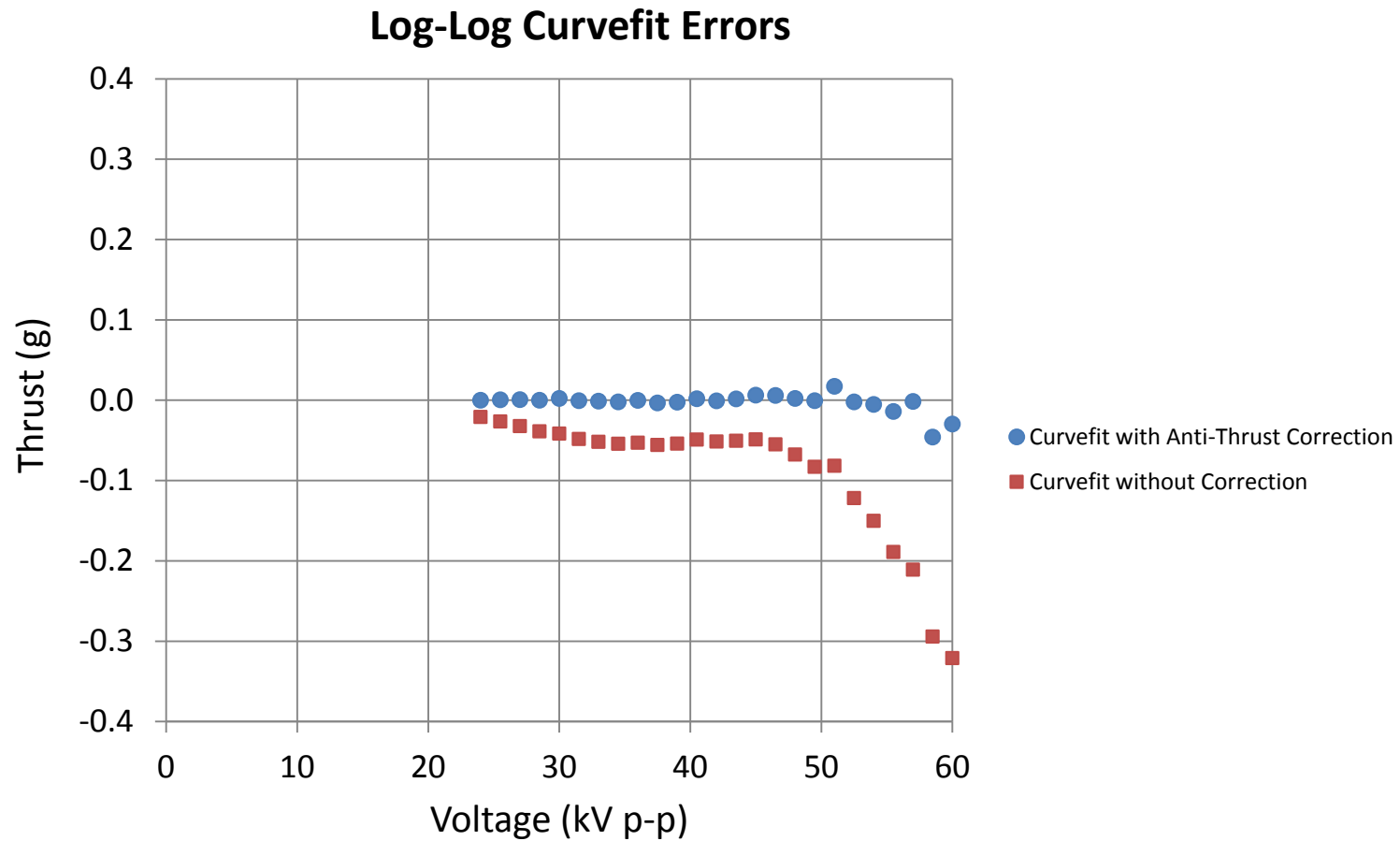
Effect of anti-thrust correction

Log-Log scale

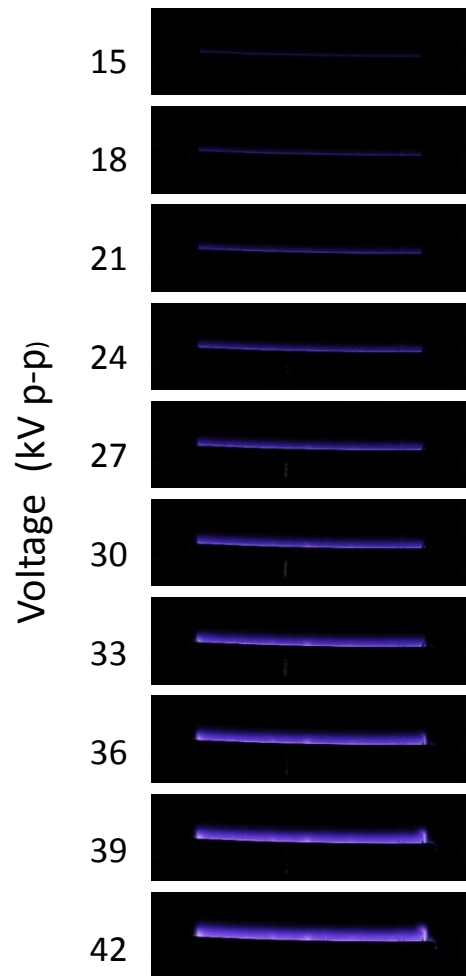


Effect of anti-thrust correction

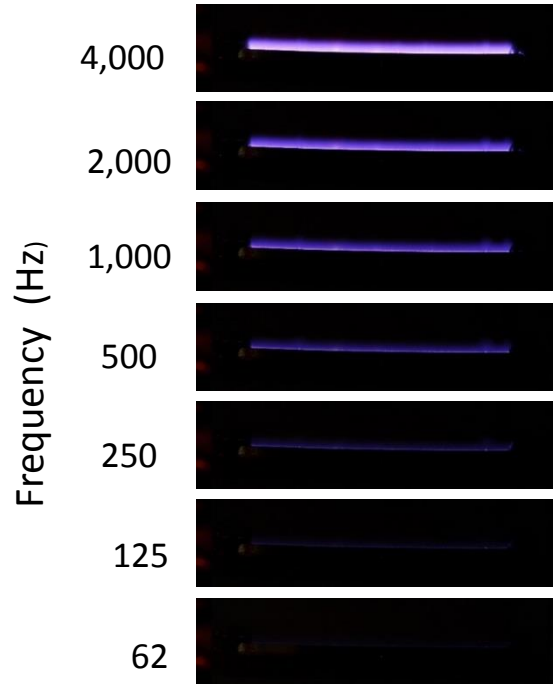
Curvefit errors



Discharge Images - 1/8" Actuator



(a) Constant Frequency 2 kHz
5 s exposure

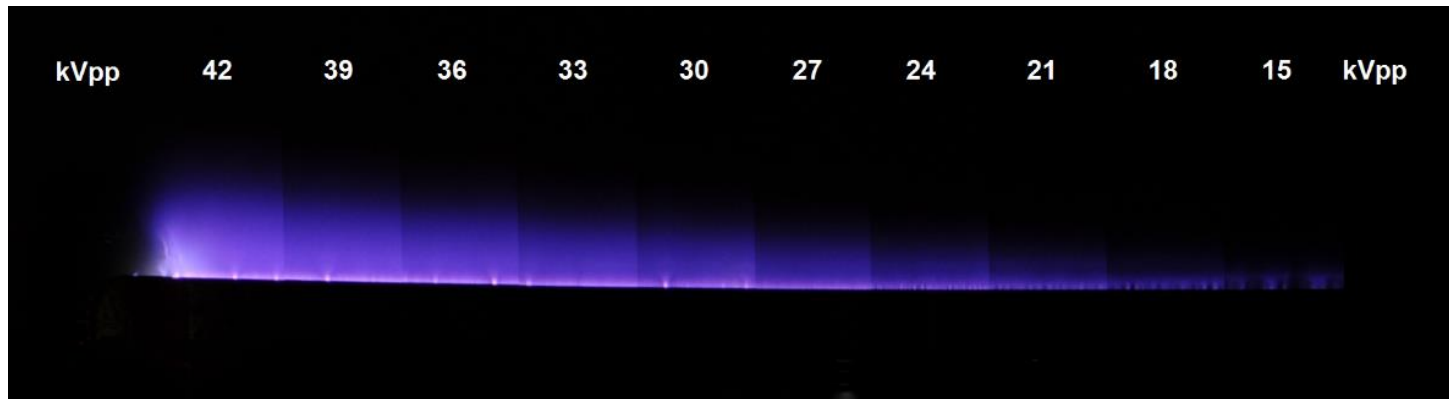


(b) Constant Voltage 27 kV p-p
30 s exposure

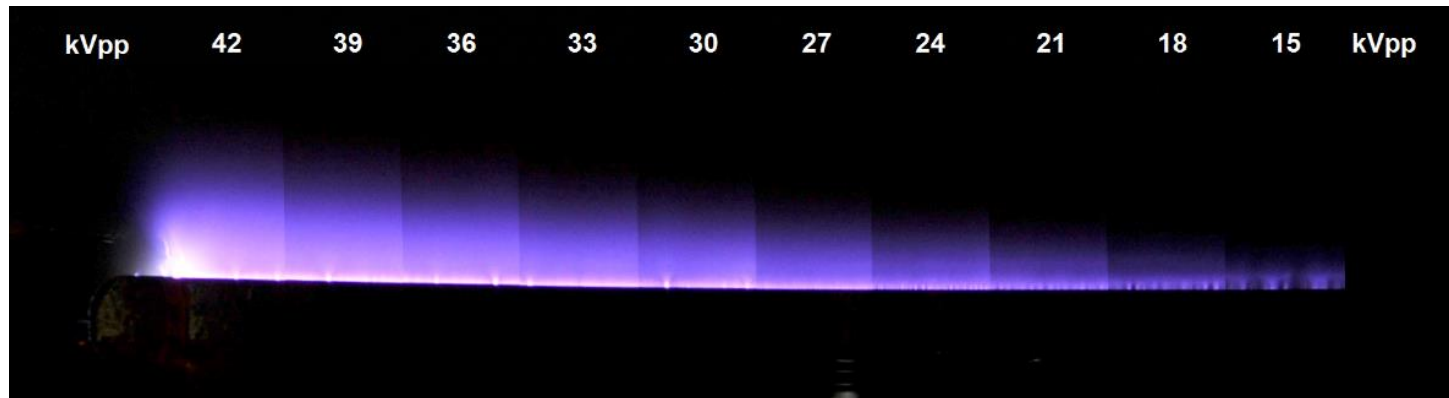
No saturation filaments observed

Discharge Images Composites- 1/8" Actuator

Constant frequency 2 kHz

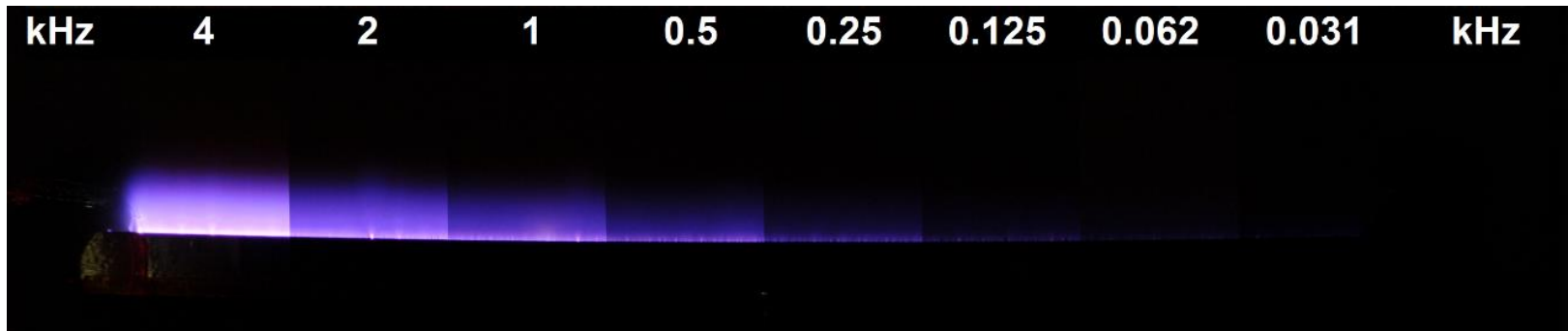


(a) Fixed exposure. $f = 2$ kHz

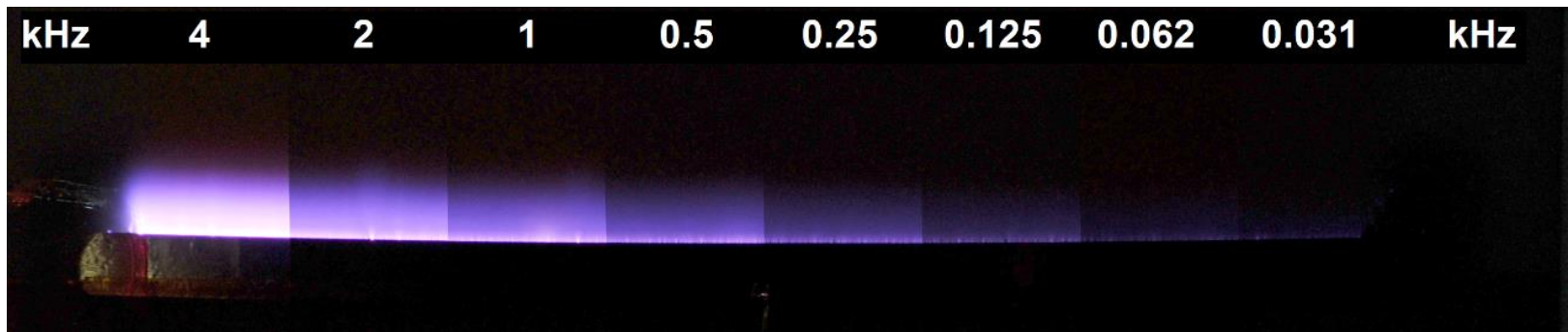


(b) Gamma enhanced. $f = 2$ kHz

Discharge Images Composites- 1/8" Actuator Constant Voltage 27 kVp-p

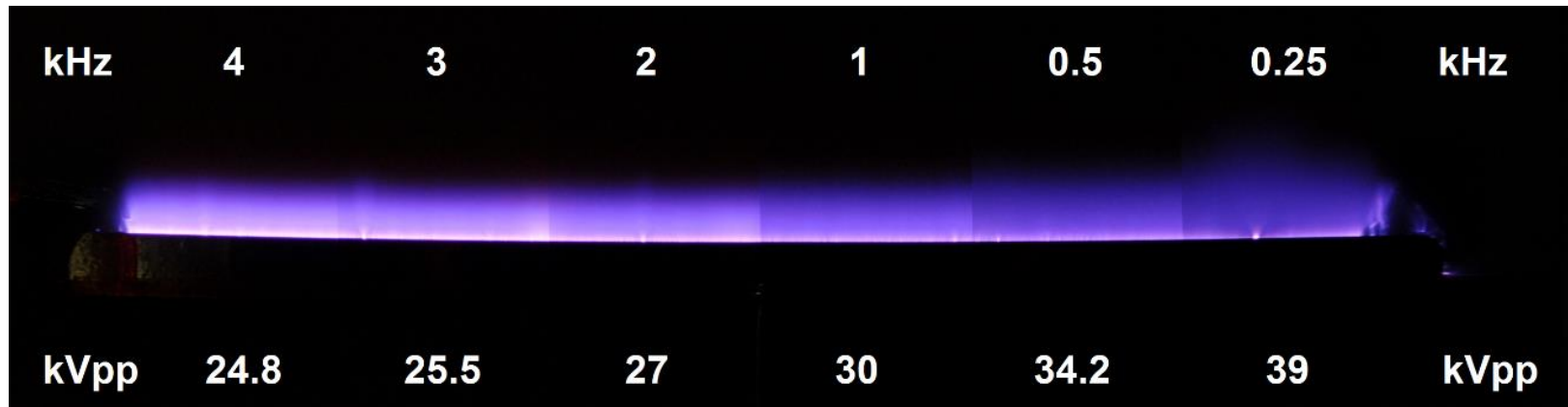


(a) Fixed exposure. $V = 27$ kV p-p

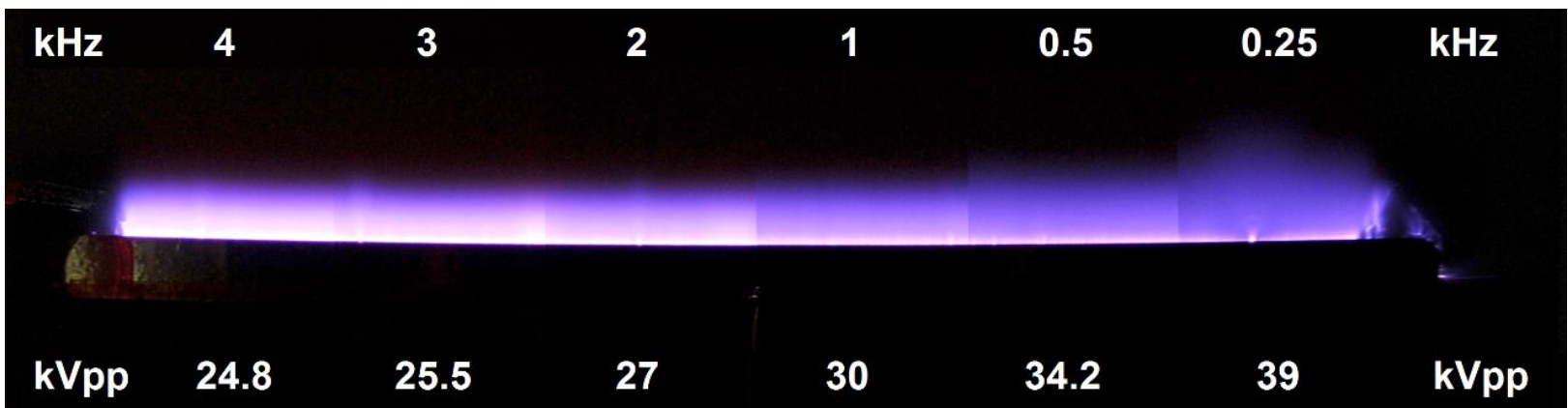


(b) Gamma enhanced. $V = 27$ kV p-p

Discharge Images Composites- 1/8" Actuator Constant Thrust 300 mg



(a) Fixed exposure. $T = 300$ mg



(b) Gamma enhanced. $T = 300$ mg

Summary and Discussion

For pure sinusoidal excitation waveform:

- Thrust vs voltage at fixed frequencies can be correlated via quadratics on log-log scales
- The fit is very good, $R^2 = 0.9993$ to 0.9999
- Smooth, orderly curves, nested, no overlap.
- Power law $T \propto V^m$ is not a good representation over the full voltage ranges.
 - $m = 3.5, 2.3, 4.8$, were proposed, $m = 2.2, 3.4, 3.6, 6.6$ for micro-actuators
- Logarithmic terms plausible - appear in electric field solutions
- Deviations from quadratics in log space can be due to
 - Non-sinusoidal wave forms, harmonics, edge, humidity
 - No compensation for anti thrust
 - No separation of plasma of interest from parasitic plasma



Discussion – Cont.

- Curve fits will not be quadratic or have large deviations if distorted waveform thrust data is included, or if anti-thrust correction not performed.
- Humid conditions increases the randomness in the data.
- Thrust-Frequency at constant voltage relations seems also to follow quadratic
- Quadratic thrust-voltage relationship in log space for sine waveforms and dry environment can be considered as measure of quality of the test.

Conclusion

- Proper approach is needed to obtain benchmark data for DBD actuators
 - Actuator construction
 - The test setup and measurement system
 - Proper isolation of plasma thrust generated by the spanwise edge
 - Low ambient humidity
- The benchmark results can be used for numerical validation and development of models
- Accurate extrapolation of data for power supply and components design.

Thank You



Questions ?

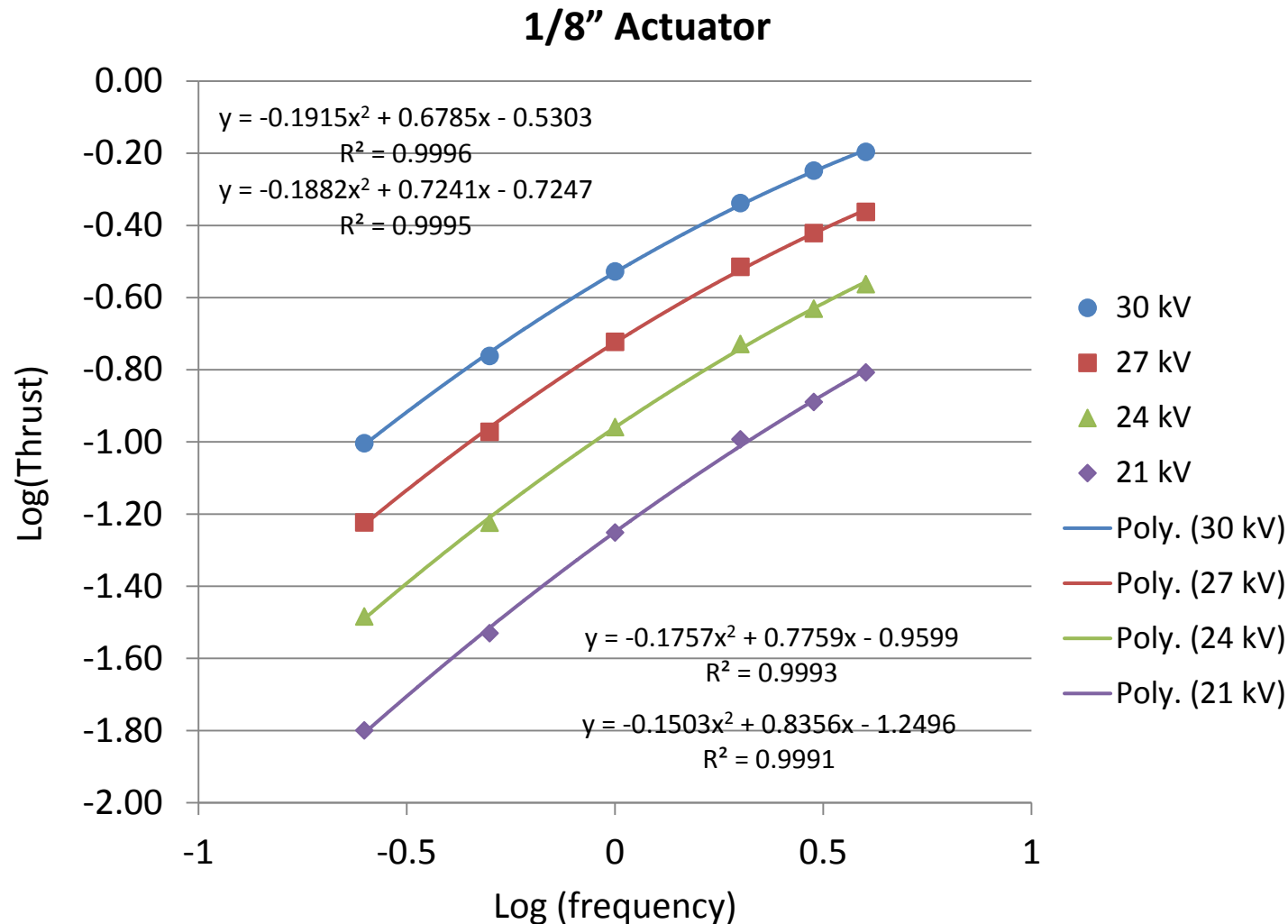


BACKUP CHARTS A

- **Thrust-Frequency at const. Voltage**
- **Actuator detailed dimensions**
- **Normalization lengths**
- **Unit conversions**

Thrust – frequency at const. voltage

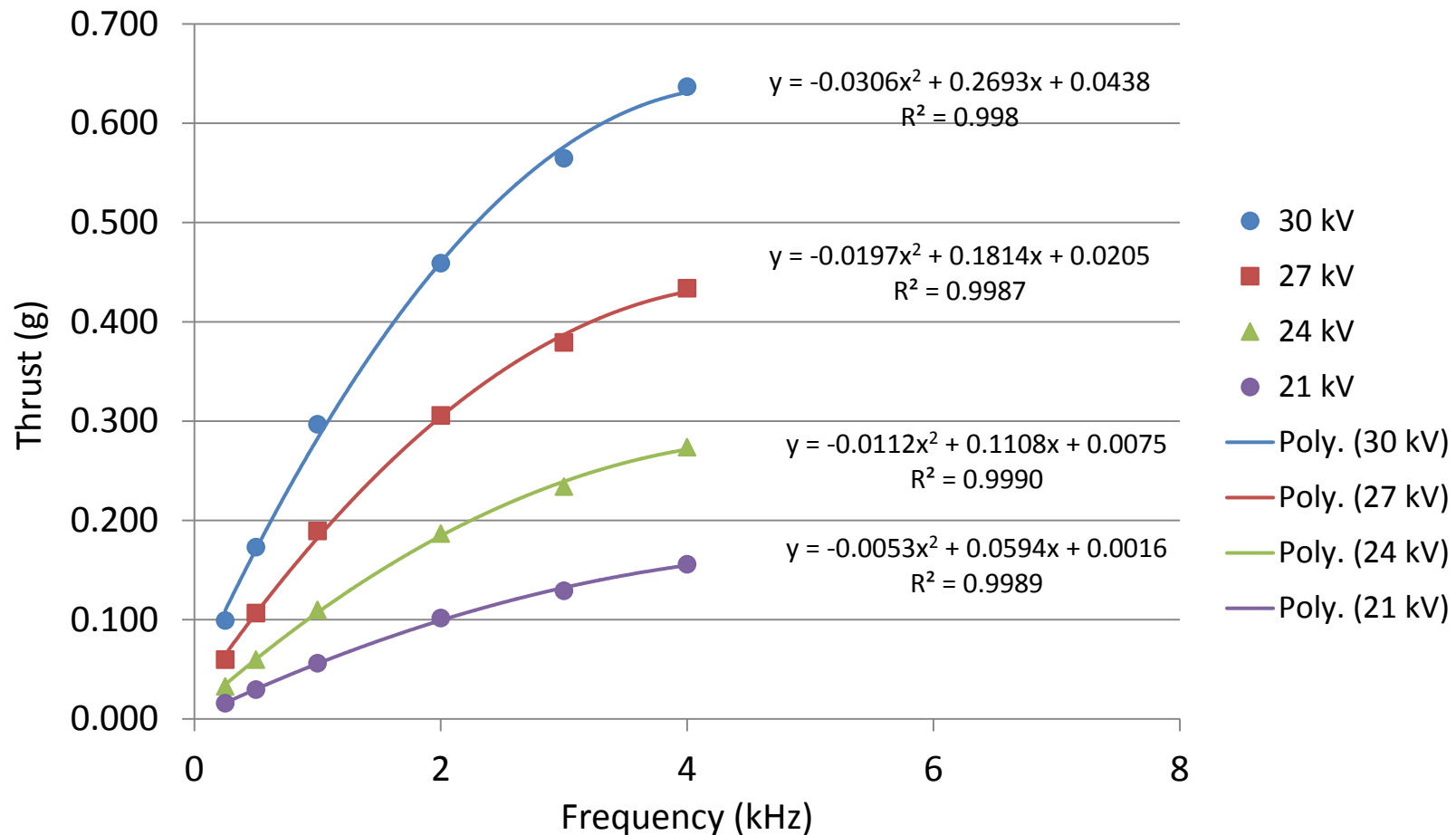
Log-Log scale



Thrust – frequency at const. voltage

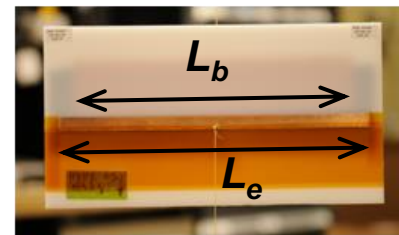
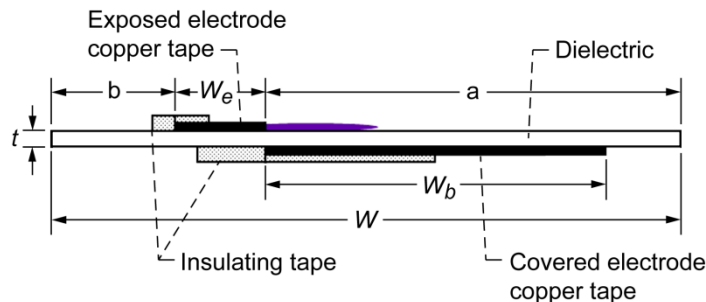
Linear scale

1/8" Actuator



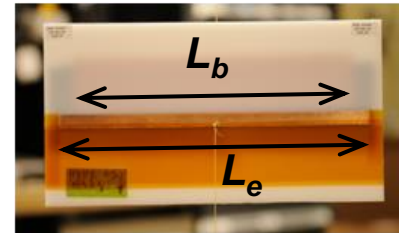
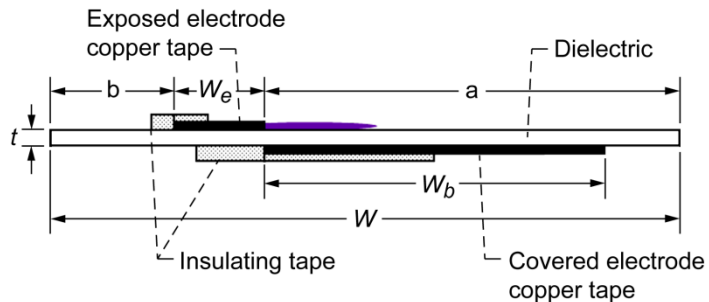
Actuator Test Articles

- HDPE - High Density Poly Ethylene
 - Dielectric Constant: 2.3 at 1 kHz
 - Dielectric Strength: 22 MV/m
 - Dissipation Factor: 0.0005 at 1 kHz
- 3M #1181 Copper tape w/ conductive adhesive
 - Copper thickness: 0.04 mm (1.4 mil)
 - Adhesive thickness: 0.03 mm (1.2 mil)
- Super Corona Dope[®]: MG Chemicals Inc. Cat. No. 4226-1L
 - Used for edge Insulation buildup
- Kapton[®] 3M #5413, 0.08 mm (3 mil) thick
 - Used for upstream edge insulation
- 3M Scotch-Seal No. 229 pads
 - Used for covered electrode insulation



Designation	t (Nominal)	t	W_e	W_b	L_e	W	a	b
	inch	mm	mm	mm	mm	mm	mm	mm
HDPE #5	1/16	1.53	12.7	51	282	154	86.5	54.0
HDPE #7	1/8	3.16	12.0	48	283	164	81.0	59.0
HDPE #3	1/4	6.09	12.0	48	254	154	76.5	64.5

Thrust Normalization Length



Designation	t (Nominal)	L_e (exposed electrode)	L_b (covered electrode)	L_{e-} <i>uninsulated</i> (exposed electrode)	Thrust T to T/L_e conversion factor	Thrust T to T/L_b conversion factor	Thrust T to $T/L_{e-uninsulated}$ conversion factor
	inch	mm	mm	mm	g to mN/m	g to mN/m	g to mN/m
HDPE #5	1/16	282	256	218	34.78	38.31	44.98
HDPE #7	1/8	283	257	249	34.65	38.16	39.38
HDPE #3	1/4	254	256.5	259	38.61	38.23	37.86



conversions

- $1 \text{ g} = 9.80665 \text{ mN}$
- $1 \text{ mg} = 0.00980665 \text{ mN}$
- $1 \text{ mN} = 0.101971621298 \text{ g}$
- $1 \text{ mN} = 101.971621298 \text{ mg}$