

An ISRU Propellant Production System to Fully Fuel a Mars Ascent Vehicle

Julie Kleinhenz, NASA Glenn Research Center Aaron Paz, NASA Johnson Space Center

Motivation



- ISRU of Mars resources was baselined in 2009 Design Reference Architecture (DRA) 5.0, but only for Oxygen production using atmospheric CO₂
 - The Methane (LCH₄) needed for ascent propulsion of the Mars Ascent Vehicle (MAV) would need to be brought from Earth
- HOWEVER: Extracting water from the Martian Regolith enables the production of both Oxygen and Methane from Mars resources
 - Water resources could also be used for other applications including: Life support, radiation shielding, plant growth, etc
 - Water extraction was not baselined in DRA5.0 due to perceived difficulties and complexity in processing regolith
- The NASA Evolvable Mars Campaign (EMC) requested studies to look at the quantitative benefits and trades of using Mars water ISRU
 - Phase 1: Examined architecture scenarios for regolith water retrieval.
 Completed October 2015
 - Phase 2: Deep dive of one architecture concept to look at end-to-end system size, mass, power of a LCH₄/LO₂ ISRU production system

Approach



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- Evolvable Mars Campaign
 - Pre-deployed Mars ascent vehicle (MAV)
 - 4 crew members
 - Propellants: Oxygen & Methane
- Generate a system model to roll up mass & power of a full ISRU system and enable parametric trade studies.
 - Leverage models from previous studies and technology development programs
 - Anchor with mass/power/performance from existing hardware
 - Whenever possible used reference-able (published) numbers for traceability.
 - Modular approach to allow subsystem trades and parametric studies





- Propellant mass needs taken from most recently published MAV study:
 - Polsgrove, T. et al. (2015), AIAA2015-4416
- MAV engines operate at mixture ratios (oxygen:methane) between 3:1 and 3.5:1, whereas the Sabatier reactor produces at a 4:1 ratio. Therefore:
 - Methane production is the driving requirement
 - Excess Oxygen will be produced
- Production rate based on a mission timeline of 480 days (16 months)
 - ISRU system arrives one launch opportunity ahead of humans
 - MAV must be fully fueled before human departure from earth
- 26 month launch opportunity
- 9 month transit time
- 1 month margin

16 months

| | | Total mass needed | Rate at 480days continuous operation |
|---------------------|------------------|--|--|
| Requirement: | CH ₄ | 6978 kg | 0.61 kg/hr |
| | | | |
| Reactants needed to | H ₂ O | 15701 kg (785,050 kg 2% soil) | 1.36 kg/hr (68.2 kg/hr soil@2%) |
| meet requirement. | CO2 | 19190 kg | 1.67 kg/hr |
| | | | |
| Results in: | 02 | 27912 kg total (22728 kg propellant, <mark>5184 kg leftover</mark>) | 2.43 kg/hr |
| | | | |

Assumptions



- <u>Production Rate driver:</u> 6978 kg of Methane needed + 0.5% margin
 - Methane is the driver since excess oxygen will be produced using Sabatier process
- <u>Time of ISRU production</u>: 480 day operation, 24hr/day
- <u>Soil Water resource (baseline)</u>: Water from surface regolith = hydrates
 - Ubiquitous (location independent)
 - Available in surface material (subsurface excavation not required)
 - Lower resource yield is more of a worse case for water extraction system
- <u>Processing</u>: <u>Regolith is transported</u> and delivered to a centralized processing plant that is co-located with the Lander/MAV
- Liquefaction: Takes place in the MAV tanks. ISRU system only includes mass/power for crycoolers needed to liquefy. MAV responsible for tanks and zero boil-off systems
- <u>Power Source:</u> Not part of ISRU system. Assumes a fission reactor will be needed for human presence, ISRU will use reactor when humans are not present. (TBD- as power needs are identified)
- Radiators: Not part of ISRU system. ISRU will be packed on lander.



Subsystem Selection for this study



| | Subsystem | Components | Heritage | Use existing |
|--------------------------|-----------------------------|--|--|--|
| Excavation Excavation | | RASSOR 2.0 excavator – Bucket drum rover | KSC prototype hardware, laboratory tests in regolith simulants | hardware with highest flight readiness |
| cessing | Regolith Processing | Auger Conveyor Dryer – heated auger with gas loop for continuous regolith processing | JSC design concept – numerical sizing model, conceptual CAD | Mass, power, performance |
| lith Pro | | Vapor cleanup – Membrane separator | COTS | NASA development |
| Rego | | Water collection – Cold trap | JSC design concept- numerical sizing model | efforts; in- house and |
| | CO ₂ Acquisition | Cryofreezer | COTS –flight heritage KSC cold head conceptual design numerical sizing | solicited • Relevant COTS |
| ц | Sabatier | Microchannel Sabatier | Solicited: Battelle PNNL | hardware |
| uctio | | Regenerative Gas dryer, desiccant | JSC development hardware | |
| nt Prod | | CH_4/H_2 separator | Solicited: Hamilton Sunstrand | These are just a |
| ella | Electrolysis | PEM electrolysis stack, Cathode feed | Giner Inc. | baseline to |
| Prop | | Deionizer | COTS | anchor model, |
| | | Inlet pump, mircorpump | COTS | technology |
| | | Regenerative Gas dryer, desiccant | JSC development hardware | trades TBD |
| | Liquefaction | Cryocooler | COTS | 0 |

Notional Packaging: Subsystems



Notional Packaging: Full ISRU System



Approach: Production requirement met by 3 independent ISRU systems including:





| Methane & Oxygen ISRU (soil water + atmosphere processing) | VS | Oxygen Only ISRU (atmospheric processing) |
|---|----|---|
| Ascent Propellant Production | VS | Ascent Propellants + Life support Consumables |
| Low Yield Regolith (Ubiquitous) | VS | High Yield Surface Regolith (Localized) |

• Oxygen Only ISRU:

- As called out in DRA 5.0
- Using Solid Oxide Electrolysis
- Full system model

Life Support Consumables

- Defined in study below
- Most conservative case, assumes highly 'water rich' scenario
 - Open loop ECLSS
 - Mars water use for everything from drinking water to Laundry.

| Stephen J. Hoffman, Alida Andrews, B. Kent Joosten, Kevin Watts, "A Water-Rich Mars Surface Mission Scenario", to be published IEE | EE-2422, IEEE Aerospace Conference, |
|--|-------------------------------------|
| Big Sky, MO, March 4-11, 2017 | , , , , |

| ISRU | ISRU O ₂ | | ISRU H ₂ O | |
|------------|---------------------|------------|----------------------------------|----------|
| Ascent | Life | Ascent | Processed into | Life |
| Propellant | Support | Propellant | O ₂ & CH ₄ | Support |
| → 22728 kg | 1906 kg | 6978 kg | 18891 kg | 24179 kg |
| | | | | Ī |

M-WIP - Definition of Reference Reserve Cases



| | Deposit Type | | | |
|---|----------------------------|------------------------------|------------------------------|--------------------------------------|
| | | B. Poly-hydrated | | D. Typical |
| Essential Attribute | A. Ice | Sulfate | C. Clay | Regolith (Gale) |
| Depth to top of deposit (stripping ratio) | 3 m | 0 m | 0 m | 0 m |
| geometry, size | bulk | bulk | bulk | bulk |
| Mechanical character of overburdern | sand | NA | NA | NA |
| Concentration and state of water-bearing phase within the minable volume | | | | |
| -Phase 1 | 90% ice | 40% gypsum ¹ | 40% smectite ² | 23.5% basaltic glass ³ |
| –Phase 2 | | 3.0% allophane ⁴ | 3.0% allophane ⁴ | 3.0% allophane ⁴ |
| –Phase 3 | | 3.0% akaganeite ⁵ | 3.0% akaganeite ⁵ | 3.0% akaganeite ⁵ |
| –Phase 4 | | 3.0% smectite ² | 3.0% akaganeite ⁵ | 3.0% bassanite ⁶ |
| –Phase 5 | | | | 3.0% smectite ² |
| Geotechnical properties | | | | |
| –large-scale properties ("minability"), e.g. competence, hardness | competenthard | sandeasy | sandeasy | sandeasy |
| –fine-scale properties ("processability"), e.g. competence, mineralogy | no crushing needed | no crushing needed | no crushing needed | no crushing needed |
| The nature and scale of heterogeneity | variation in impurities | ±30% in concentration | ±30% in concentration | ±30% in concentration |
| Distance to power source | 1 km | 1 km | 1 km | 100 m |
| Distance to processing plant | 1 km | 1 km | 1 km | 100 m |
| Amenability of the terrain for transportation | flat terrain | flat terrain | flat terrain | flat terrain |
| Presence/absence of deleterious impurities | dissolved salts | none | none | perchlorate? |
| First order power requirements | TBD | TBD | TBD | TBD |

1. ~20 wt% water, 100-150°C

- 2. ~4 wt% water, 300°C
- 3. ~1 wt% water, >500°C
- 4. ~20 wt% water, 90°C
- 5. ~12 wt% water, 250°C
- 6. ~6 wt% water, 150°C

The M-WIP (Mars Water ISRU Planning) study was lead by SMD/Mars Program office and involved academy and industry members to identify impacts of Mars resources and their location, and the data still needed to best define them.

• The MWIP team report is posted: <u>http://mepag.nasa.gov/reports/Mars_Water_ISRU_Study.pptx</u>

Human Mission Mars Soil Excavation for Water





Surface area required per mobile excavator with the following assumptions:

- 3 mobile excavators used
- Each excavator provides 40% of required water
 - Excavation depth = ~5cm (2.0 in)

Trade: higher yield regolith

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- The real benefit of targeting higher yield regolith is the power saving
 - Less regolith to heat
 - Heating at a lower temperature



Case Study Definitions



| Case | Title | Description |
|------|---|--|
| 0 | No ISRU | Represented by the total propellant mass needed for ascent propulsion, this is meant to be a comparison of the landed mass needed for Mars |
| | | Ascent. With no ISRU the total methane and oxygen for propulsion must be landed. |
| 1 | Oxygen-Only ISRU, propulsion | Oxygen for ascent propulsion is produced using atmospheric CO ₂ . All methane is transported from earth. |
| 2 | Methane ISRU, propulsion, Case D regolith | Methane and oxygen for ascent propulsion are both produced using both water from regolith and atmospheric CO ₂ . The regolith is assumed to be Case D, "Typical" regolith a represented by Gale Crater with ~1.3% water content. |
| 3 | Methane ISRU, w/life support, Case D regolith | Same as Case 2 but with additional water and oxygen requirements for life support |
| 4 | Methane ISRU, propulsion, Case B regolith | Same as Case 2 except using Case B regolith with ~8% water content |
| 5 | Methane ISRU, w/life support, Case B regolith | Same as Case 3 using Case B regolith with ~8% water content |

| Deposit Type | | | | |
|--------------|--------------------------|--------------|----------------------------|--|
| A. Ice | B. Poly-hydrated Sulfate | C. Clay | D. Typical Regolith (Gale) | |
| | 8.6% @ 150°C | 2.7% @ 300°C | 1.3% @ 300°C | |

Results: Consumable production





Mass Results



ISRU system Landed Mass Comparison

(ISRU Hardware + Propellant from Earth)

The ISRU system leverages the power and radiator systems that are pre-positioned by the lander for human systems. So these are not explicitly part of the ISRU system.

| | ISRU Hardware Mass, mT | Total Mass, mT | Production Ratio: Propellant produced per kg of total mass |
|---|------------------------------|--|---|
| Case 3 ISRU propellants, & life support | 2.2 | 2.2 | 13.5 |
| Case 2 ISRU propellants, baseline regolith | 1.7 | 1.7 | 17.7 |
| Case 1 ISRU O ₂ propellant | 0.93 | 8.0 (1mt hardware + 7mt Methane) | 2.9 |
| Case 0 No ISRU | 0 | 29.7 (23mt Oxygen + 7mt Methane) | na |

- The addition of methane production increases mass 1 mT over the oxygen-only case suing the lowest yield regolith
- Total mass considers ascent propellant mass transported from earth. However producing that propellant in-situ will save additional mass:
 - Propellant required to deliver hardware and ascent propellants from LEO
 - EDL systems to land the ascent propellant
 - Storage and conditioning systems for propellant during transit and surface operations
- Propellant production Ratio = Mass Propellant Produced / Hardware mass
 - Full ISRU offers a 6x improvement over oxygen-only ISRU using the lowest yield regolith

Overall Mass comparison



- Mass reductions are compared to total ascent propellants only
- Mass savings in LEO is about 10kg per ever 1 kg of propellant produced
 - LEO Mass savings on the order of 300 mT with full ISRU system
 - Reduces cost and eliminates several heavy lift launch vehicles























Power results



- The EMC architecture estimated 40kW would be needed for crew habitation (surface activities). ISRU would use power source during unscrewed periods.
 - All but Case 3 fall in this ball park. Case 3 approach was a 'water rich' scenario, so using the lowest yield regolith for this case is overly conservative



 Using heat recuperation for the regolith thermal heat significantly reduces electrical power requirements.

Heat could be recuperated from fission reactor

Conclusions



- Model for end-to-end Mars ISRU systems have been developed to look at power/mass/volume trades
 - Oxygen only and Methane/Oxygen systems
 - Modular to permit other technologies and architectures
 - A "deep dive" study was preformed on one system to examine benefits from an EMC mission standpoint
- A system to produce all 30 mT of Mars ascent propellant is estimated to weigh 1.7 mT using the lowest yield regolith.
 - An oxygen-only system weighs 0.93 mT + 7 mT of methane = 8 mT
- Using higher yield regolith has only marginal impact on mass, but reduces power requirements 52kW to 35kW, where an oxygen only system is 35kW.
 - This power reduction is primarily thermal energy to heat the regolith, which could be recuperated from other sources.
- The inclusion of life support consumables (worst case) from ISRU would only have a marginal impact provided that a higher yield regolith is used.
 - This would require targeting a resource rich specific landing site

Oxygen only: Reduces Propellant mass 73%, could save 230 mT in LEO Methane/Oxygen: Reduces Propellant mass 94%, could save 300 mT in LEO