# Consideration of Collision "Consequence" in Satellite Conjunction Assessment and Risk Analysis

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on behalf of the Conjunction Assessment Technical Advisory Committee

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## Agenda

- Risk assessment foundational theory
- Aspects of collision consequence
- Collision debris production basics
- Estimating debris production for a particular satellite collision
- Proposed conjunction remediation threshold alterations for lowdebris collisions
- Orbital corridor protection
- Summary of initial proposed construct for considering collision consequence within conjunction assessment (CA)
- Future work

# **Risk Assessment Foundational Theory**

- Risk assessment approaches based on Kaplan construct (1981)
- Risk is combination of event likelihood and event consequence
  - Sometimes treated as product of these two, but this is not always appropriate

### CA has only partially followed this approach

- Large body of work on methods to establish collision likelihood
- Usually static treatment of collision consequence—all satellite collisions uniformly considered catastrophes of highest order
- In early days of CA, with relatively few conjunctions, static concept of collision consequence acceptable

#### In current environment, approach needs re-examination

- Number of conjunctions much larger now
- Deployment of USAF Space Fence radar (September 2018) could increase space catalogue by up to a factor of five
- Consideration of consequence could reduce conjunction remediation need

# **Aspects of Collision Consequence**

#### Protection of primary asset

- Some conjunctions could leave primary asset only crippled but still functional
  - "Glancing blow" or injury/degradation to part of solar array
- However, with current accuracy levels not possible to predict that a particular conjunction would leave only damage of this type
- For any collision, should thus presume complete loss of primary asset

### Protection of orbital corridors and space environment

- Many orbital types significantly enable particular mission types
  - e.g., geosynchronous, sun-synchronous, Molniya
- Debris fields from satellite collisions could permanently ruin these corridors
- Satellite collisions do have very different debris-producing potential
- In contended environment, expected debris production can be discriminator
  - If not all serious conjunctions can be remediated, debris production potential is possible input to choosing which receive remediation
- Can one determine the "debris production potential" of a collision?

– NASA Orbital Debris Program Office (ODPO) provides possible methodology

# **Two Collision Types:** Catastrophic and Non-Catastrophic Collisions

- In catastrophic collisions, both satellites are completely fragmented
- In non-catastrophic collisions, the smaller object is fragmented but the larger one merely cratered
- Former situation obviously produces more debris
- Undoubtedly there are intermediate cases, but this is the ODPO's basic distinction
- ODPO methodology for distinguishing between cases: ratio of relative kinetic energy of smaller object to mass of larger object

- Presumed formula: 0.5 \* m \* Vrel<sup>2</sup> / M

- If ratio exceeds 40,000 Joules / kg, then collision is catastrophic

### **Determining Number of Collision Pieces**

- NASA ODPO EVOLVE 4.0 model contains relationship for number of pieces greater than a certain size generated by a collision
  - $-N(Lc) = 0.1(M)^{0.75}L_c^{-1.71}$
  - Lc is the characteristic length (in meters) above which one is interested in the number of pieces; in a Space Fence era, one might set this to 0.05m
  - M is a momentum component of sorts, and its determination is governed by whether the collision is catastrophic
    - If catastrophic, M is sum of both spacecraft masses (kg)
    - If non-catastrophic, M is mass of smaller object (kg) \* collision velocity (km/s)
- Question: what is dynamic range of results for CA from coupling of catastrophic / non-catastrophic and debris production equations?
  - e.g., will all results be catastrophic and thus high-debris, rendering approach unhelpful for distinguishing among conjunctions?
  - Profiling activity needed to show viability

# **Coupled Equation Input Profiling: Satellite Mass and Conjunction Velocity**

- Conjunction velocities from NASA CA DB (~1.5M conjunctions) shown at right
  - For LEO and HEO, great majority exceed 10,000 m/s
  - GEO much slower: 100 to 2000 m/s

### Masses have large range as well

- Primary payload: up to ~3000km or larger
- Secondary: from 0.01 kg to payload mass
- Profiling should consider dynamic range of both input types
  - For this analysis, primary object mass set to 3000 kg



# **Coupled Equation Input Profiling: Results**

# Catastrophic and non-catastrophic regions distinct

- Catastrophic yellow; non-catastrophic layered; magenta line is boundary
- As mass of lighter satellite approaches that of heavier, more of a continuum in debris production with relative velocity
  - With lighter secondary, discontinuity increases
- Even at high collision velocities, non-catastrophic collisions quite possible for light secondaries
- In short, construct looks promising as possible severity discriminator



# **Collision Debris Production Determination: Estimating Needed Parameters**

- Conjunction velocity easily obtained from orbital states
- Primary object mass known
- Secondary object mass must be determined
  - For intact payloads and rocket bodies, might be able to obtain actual mass value
  - In general (and for debris), mass values will have to be estimated

### Proposal: estimate mass from ballistic coefficient solution

- Ballistic coefficient given by (could also use solar radiation pressure coefficient):

$$B = C_D \frac{A}{M}$$

- If ballistic coefficient, drag coefficient, and frontal area estimated, then satellite mass (M) can be further estimated from above relation
- Given imprecisions for many of these parameters, best to define a PDF for each and thus generate an estimated mass PDF
  - Can be further used to generate a debris piece count PDF

# **Collision Debris Production:** Estimating Ballistic Coefficient (B)

![](_page_9_Figure_1.jpeg)

- Conjunction Data Message (CDM) for particular event gives information about B for primary and secondary objects
  - Estimate of mean value  $(B_{\mu})$
  - Estimation variance  $(B_{\sigma})$  from covariance matrix
- Set of random B values easily generated by N(  $B_{\mu}, B_{\sigma})$

# **Collision Debris Production:** Estimating Drag Coefficient (C<sub>D</sub>)

![](_page_10_Picture_1.jpeg)

- Because ballistic coefficient usually solved for as a single value, relatively less research work directed to C<sub>D</sub>
  - Sustained interest is from atmospheric community, due to attempts to back out atmospheric density values from satellite drag solutions
- Early work in 1960s, with follow-up in 1990s, established basic principles and rules of thumb
  - Snub satellites have typical  $C_D$  value of 2.2
  - Distended satellites with long dimension along velocity vector have larger  $C_D$ , often in range of 3-4
- Recent interest in topic and better models, but are satellite-specific
- For current approach, C<sub>D</sub> values generated by U(2.1, 3.0)
  - Non-stabilized debris unlikely to generate truly large  $C_D$  values
  - Supported by Hubble Space Telescope value of 2.8

![](_page_11_Picture_1.jpeg)

- Possible to estimate satellite areas from sensor signature data
  - Focus on radar cross-section (RCS) as opposed to satellite visual magnitude, since emphasis here is LEO debris
- RCS has units of area, but only under special circumstances can value be roughly equated to satellite physical area
- RCS for sphere illustrates issues with establishing RCS-size relationship (next slide)
- ODPO developed Size Estimation Model (SEM) to facilitate mapping
  - Exploded satellite in vacuum chamber, determined characteristic dimension of each piece, took RCS measurements on each piece, and effected theoryenabled fit of data
  - Intended only for debris smaller than 20cm and to convert entire distributions of RCS to distributions of size, and vice versa
    - Any other use is "off-label"
  - Can be used as starting point for single conversion, with much imprecision

# **RCS/Size Properties:** Conducting Sphere and NASA SEM

### Sphere: three regions of response

- Rayleigh—RCS proportional to r<sup>4</sup>
- Mie—transitional region with oscillating behavior (creeping waves)
- Optical-RCS converges to area
  - Unfortunately, at S-Band occurs only for objects greater than 0.86 – 1.7 m; much larger than most debris

### • NASA SEM

- Within envelope of sphere response
- Imposes unique mapping
- Not precise for single-object use, but how close is it actually?
  - Difficult to evaluate performance against debris (no ground truth)
  - RORSAT spheres offer one opportunity

![](_page_12_Figure_12.jpeg)

# Frontal Area and Mass Estimation: RORSAT Coolant Spheres

### RORSAT satellite coolant

- Nuclear-powered sats with NaK coolant
- Leaked out of dead sats; formed spheres
- Independent study determined sats spherical and 5-6cm in diameter
- Only debris set with established dimensions

### 24 had sufficient data for study

- B and RCS terms
- Calculated projected areas from RCS (using SEM) and compared to actual areas
- Performed mass estimation and compared to "actual" masses (calculated from established sizes and known density)

### Results at right

 Moderate positive bias (typical when working with RCS values), but overall error range quite small

![](_page_13_Figure_12.jpeg)

# Mass Estimation Procedure: Summary

- Obtain needed orbital and signature information from latest CDM
  - $-B_{\mu}$ ,  $B_{\sigma}$ , median RCS value
- Create X samples of each input to ballistic coefficient equation
  - B from normal distribution defined by  $B_{\mu}$  and  $B_{\sigma}$
  - $-C_{D}$  from uniform distribution between 2.1 and 3.0
  - A from RCS value fed into SEM, turned into circular area, and used as anchor for uniform distribution +/- one order of magnitude (OoM) from anchor
    - e.g., if anchor is 0.02 m2, samples for A are [U(0.002, 0.02, X/2); U(0.02, 0.2, X/2)]
    - Extremely generous error bounds—presumes SEM only good to +/- 1 OoM
- Yields X values for secondary object mass
- V<sub>rel</sub> and primary object mass presumed known without error
- By using debris production equations, can generate X estimates of amount of debris that collision will produce
- Can break down X estimates by percentile points
  - For most situations, issue reduces to whether or not collision is catastrophic

# **Debris Production Estimation: Historical Conjunction Profiling**

#### Procedure run against portion of NASA conjunction database

- LEO conjunctions from January to June 2016
- 14,000 unique events for which secondary a debris object with established RCS
  - CDM with largest Pc taken as event representative
- 100,000 Monte Carlo samples of estimated # of debris pieces, per event

### Summarized by percentile point

– CDF curves for 50<sup>th</sup>, 75<sup>th</sup>, 90<sup>th</sup>, and 95<sup>th</sup> percentile of each event's 100,000 results

### Graph morphology

- Flattened and then suddenly vertical behavior indicates transition to catastrophic collision
- 50% of events do this at the 95<sup>th</sup> percentile; about 30% do at the 90<sup>th</sup> percentile
- If  $C_D$  span increased to 2.1 4.0, percentages drop from ~8-10%

# **Debris Production Estimation: Historical Conjunction Profiling Results**

![](_page_16_Figure_1.jpeg)

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# Low-Debris-Production Cases: Pc Threshold Alterations

- 95% threshold seems reasonable starting point for separation
  - Conservative—if one-in-twenty chance of large debris production, then treated as a large debris case
  - About half of profiled events are given this designation, so a good separator of events into two types
    - Although far from all ever became serious events
- Current Pc remediation thresholds (1-4 E-04) were generated with the large-debris situation in mind

- So small-debris situations should show a leniency from this level

 For primaries that have difficulty remediating conjunctions, offset is from 0.5 to 1 OoM increased leniency in Pc remediation threshold

- Electric propulsion is good example

### Probably a good initial proposal for low-debris situations

 – 0.5 to 1 OoM, with exact value determined by experience and owner/operator risk tolerance

# **Orbital Corridor Population**

- Would seem that satellites in "high-value" corridors deserve additional protection
  - Geosynchronous, sun-synchronous, Molniya-greatly facilitate certain missions
  - Debris population in these orbits would seem more injurious and therefore should engender more risk-adverse posture

### Not as straightforward in practice

- Sun-synchronous can be conceived in a variety of ways
- Debris at higher orbits pollute lower ones (both immediately and eventually through decay), so this would have to be considered as well
  - Although ~100km lower than Fengyun 1C and Iridium-COSMOS, half of A-Train conjunction events against debris from these two collisions
  - "Protected Zones" about orbits would thus need to become excessively large

### Geosynchronous orbit the exception

- Debris in GEO will remain for a very long time and pass a number of payloads as it moves toward and librates about one of the two libration points
- Due to persistent threat, should not abate Pc threshold for small-debris cases

	LEO/HEO Orbits	GEO Orbits
Catastrophic Collision	Х	Х
Non-Catastrophic Collision	X + (0.5 – 1) OoM	Х

- X is the current Pc remediation threshold (usually ~1E-04)
- X abated by 0.5 to 1 OoM for low-debris collisions in LEO and HEO
  - Perhaps 5E-04 to 1E-03
- No corresponding abatement in GEO, due to debris persistence and ease of orbital corridor pollution

### **Future Work**

#### Construct is merely CATAC initial proposal

- Will be refined over the next 12 months with additional studies

#### Planned future work

- More comprehensive error analysis on satellite frontal area estimation
  - Perhaps using cubesats as an additional dataset, since many have known dimensions
- More comprehensive error analysis on satellite drag coefficient estimation
  - Better understanding of debris shape and area-to-mass distributions for small debris
- Further refinement of actual construct to be used for operational CA