Electrical Resistance Heating Technology Overview and NASA KSC Case Study Mississippi Tier II Meeting, July 2017



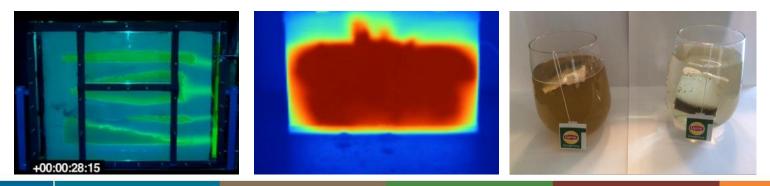
Presentation Content

- ERH Technology Overview
- NASA Kennedy Space Center Case Study
 - Site Background
 - ERH Treatment Performance Monitoring
 - Lessons Learned
 - Path Forward

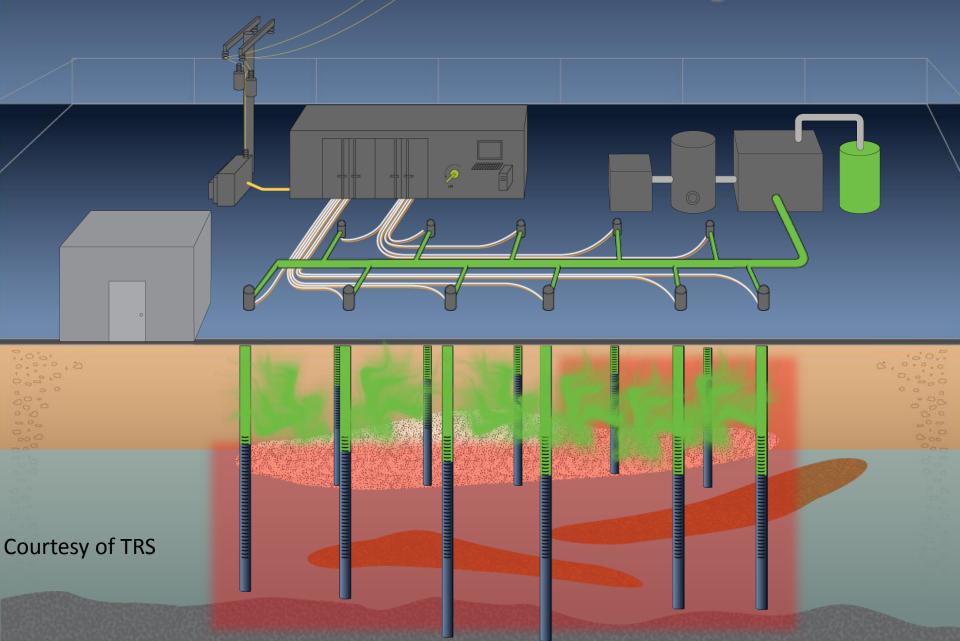


ERH Overview

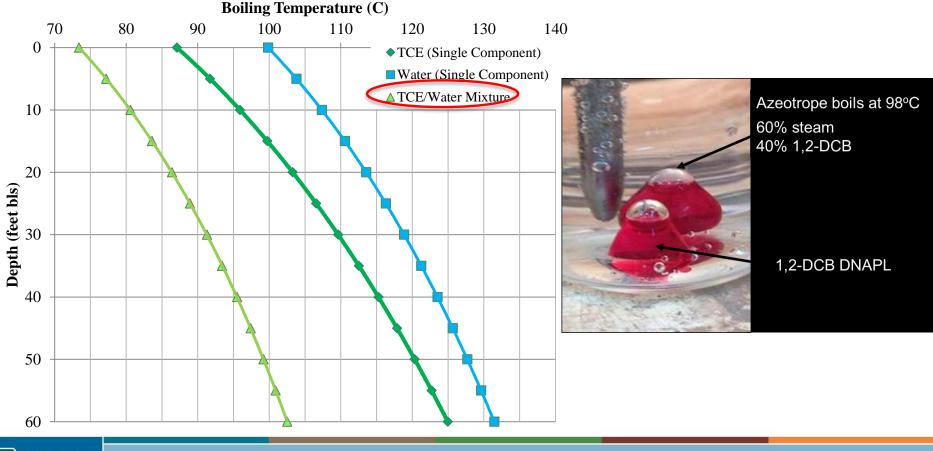
- How does ERH work?
 - Electrical current passes from electrode to electrode
 - Soil resistance heats subsurface to boiling point of water/VOC mixture
 - Boiled water/VOC mixture captured through vapor recovery in vadose zone
 - Vapors and moisture in steam cooled and separated
 - Vapors treated through activated carbon or catalytic oxidation
- Effective in heterogeneous conditions and bedrock
- Addresses source zone matrix diffusion
- Dissolves natural organic material for post-ERH biotic treatment
- Can be applied at a lower intensity to enhance natural attenuation in dilute plumes or induce thermal hydrolysis



Electrical Resistance Heating

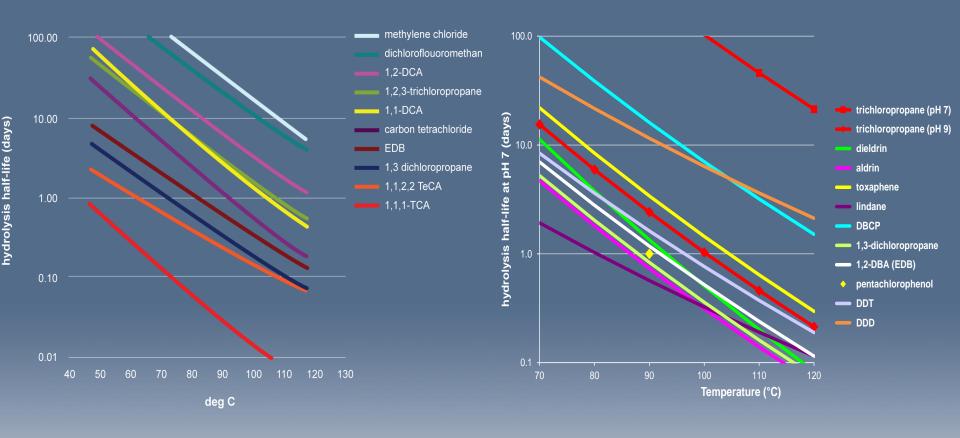


- Many VOCs form a positive heteroazeotropic mixture with water
- What is a positive heteroazeotrope?
 - a mixture where the equilibrium vapor and liquid compositions are equal at a given pressure and temperature
 - the vapor has the same composition as the liquid and the mixture boils at a temperature other than that of the pure components' boiling points (positive azeotrope = lower boiling point)



Boiling Point/Temperature Behavior

Hydrolysis of Halogenated Alkanes and Pesticides





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Common ERH Misnomers

• Expensive

- In certain settings, competitive to less costly than other source removal technologies
- Selection of technology based on site specific evaluation
- Cost is generally a function of volume and geometry
- Temporal benefit of 6-9 month treatment durations
- Temperature is the goal
 - Steam production is the goal
 - Reducing mass concentrations is the goal
- Electrical conductivity of matrix matters
 - ERH equipment has large dynamic range across many conductivities
- Water is problematic
 - Water (or moisture) conducts electricity
- Vadose zone is challenging
 - Originally developed for the vadose zone
- Only for VOCs
 - Can treat compounds such as chlorinated compounds, pesticides, and energetic compounds

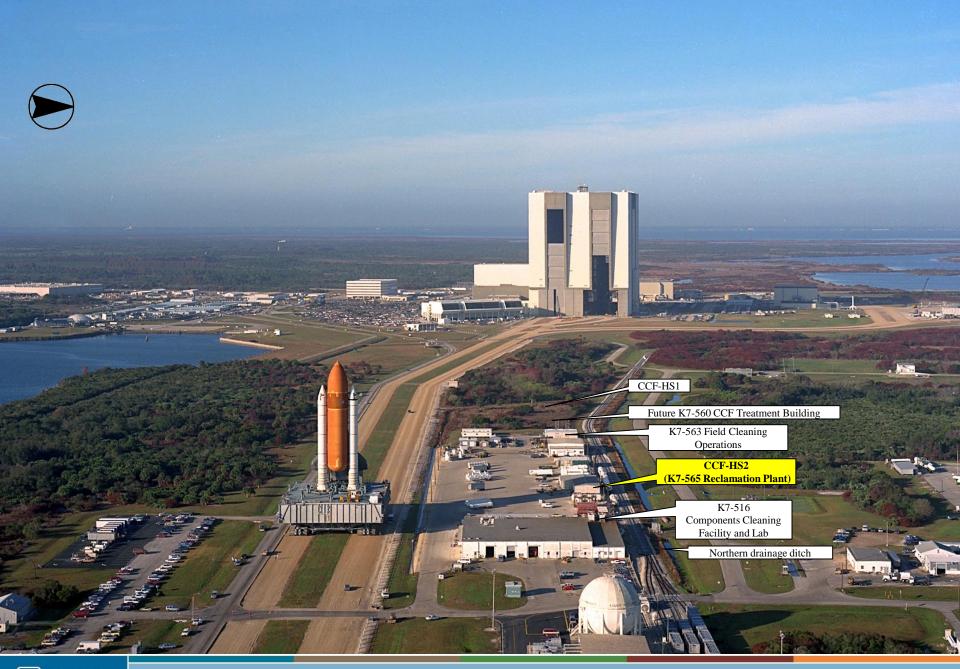


Site Background

- Site: NASA Kennedy Space Center, Components Cleaning Facility
- Area developed in 1962 for cleaning and refurbishment of hardware and an associated analytical laboratory
- Designated Solid Waste Management Unit 030
- Currently site is vacant (buildings demolished ~2006)
- Groundwater plume co-mingled with Area South of K7-0526, SMWU 100
- Located northeast of intersection of Crawler Parkway and Fluid Servicing
 Road





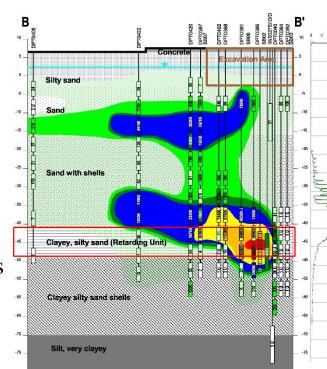


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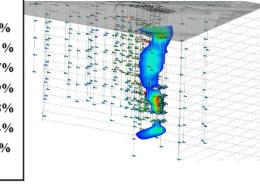
Components Cleaning Facility (1990)

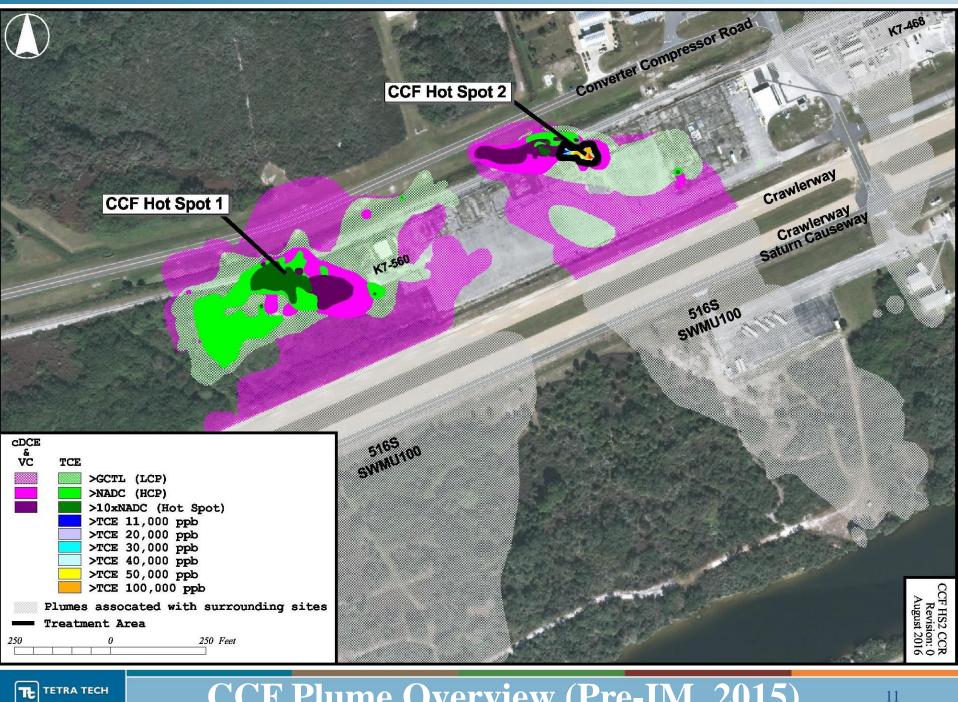
HS2 Site Characterization

- Source zone site characterization:
 - Source zone definition of ~1% TCE solubility (11 mg/L)
 - Investigated by DPT sampling with on-site mobile lab
 - General 10' source zone DPT spacing
 - 5' vertical spacing
 - Selective 1' intervals in semi-confining unit
 - Membrane interface probe borings
- Semi-confining, fine-grained unit from 49 to 61 feet bls
 - 76% of TCE HS mass within fine-grained unit
 - Conceptual model "Storage" or back-diffusion layer
 - 23% of TCE HS mass 10' above fine-grained unit
 - Conceptual model advective layer



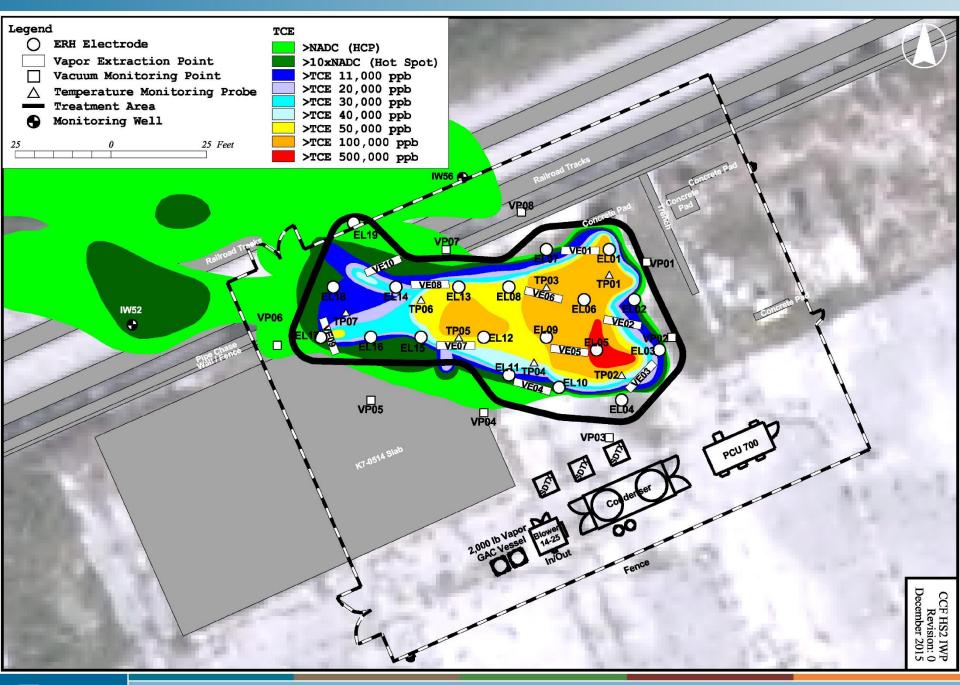
| | | TC | E | | | cDC | E | | | VC | 2 | |
|----------|-----------|--------|--------|-----|-----------|--------|-------|-----|-----------|--------|-------|-----|
| Interval | Dissolved | Sorbed | Total | | Dissolved | Sorbed | Total | | Dissolved | Sorbed | Total | |
| (ft bls) | (lb) | (lb) | (lb) | | (lb) | (lb) | (lb) | | (lb) | (lb) | (lb) | |
| 0 - 10 | 0.6 | 1.1 | 1.8 | 0% | 1.0 | 0.8 | 1.8 | 3% | 0.2 | 0.1 | 0.3 | 2% |
| 10 - 20 | 2.3 | 4.2 | 6.5 | 0% | 4.4 | 3.4 | 7.7 | 12% | 1.8 | 0.5 | 2.3 | 11% |
| 20 - 30 | 0.6 | 1.1 | 1.7 | 0% | 3.7 | 2.8 | 6.5 | 10% | 2.7 | 0.8 | 3.5 | 17% |
| 30 - 40 | 1.7 | 3.1 | 4.7 | 0% | 5.7 | 4.4 | 10.1 | 16% | 2.9 | 0.9 | 3.8 | 19% |
| 40 - 50 | 97.7 | 282.8 | 380.5 | 23% | 9.8 | 11.9 | 21.7 | 35% | 3.9 | 1.8 | 5.7 | 28% |
| 50 - 60 | 129.0 | 1106.3 | 1235.2 | 76% | 3.2 | 11.4 | 14.5 | 23% | 2.1 | 2.8 | 4.9 | 24% |
| >60 | 0.0 | 0.1 | 0.2 | 0% | 0.0 | 0.0 | 0.1 | 0% | 0.0 | 0.0 | 0.0 | 0% |
| Totals: | 232 | 1399 | 1631 | | 28 | 35 | 62 | | 14 | 7 | 20 | |





CCF Plume Overview (Pre-IM, 2015)

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ERH Layout

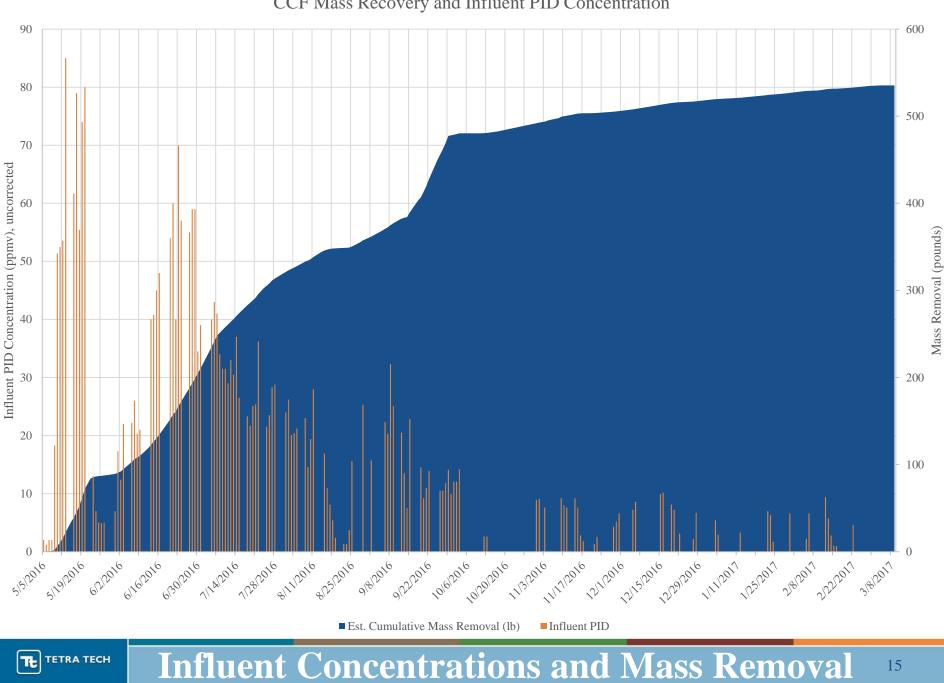
IM Components

| Quantity | Component |
|----------|---|
| 19 | Vertically-bored electrodes (3 elements per electrode) |
| 10 | Horizontal vapor extraction (VE) points |
| 7 | Temperature monitoring points (TMPs) |
| 8 | Vapor monitoring probes (VMPs) |
| 1 | 700-kW power control unit (PCU) |
| 1 | Condenser and cooling tower skid |
| 1 | Vapor recovery blower skid |
| 3 | 2,000 lb. Vapor-phase granular activated carbon (VPGAC) units |
| 2 | 400 lb. Liquid-phase granular activated carbon (LPGAC) units |
| | Electrode field vapor cover |
| | Motion sensing and security camera system |
| | Vinyl coated perimeter fencing |
| | Electrical and potable water utilities |

IM Timeline

- November 2015: Pre-mobilization Activities
- December 2015: Mobilization Activities
- January to April 2016: IM Installation
- May 2016: Commissioning and Startup
- May 2016 to February 2017: OM&M
- March to April 2017: Demobilization





CCF Mass Recovery and Influent PID Concentration



KSC77

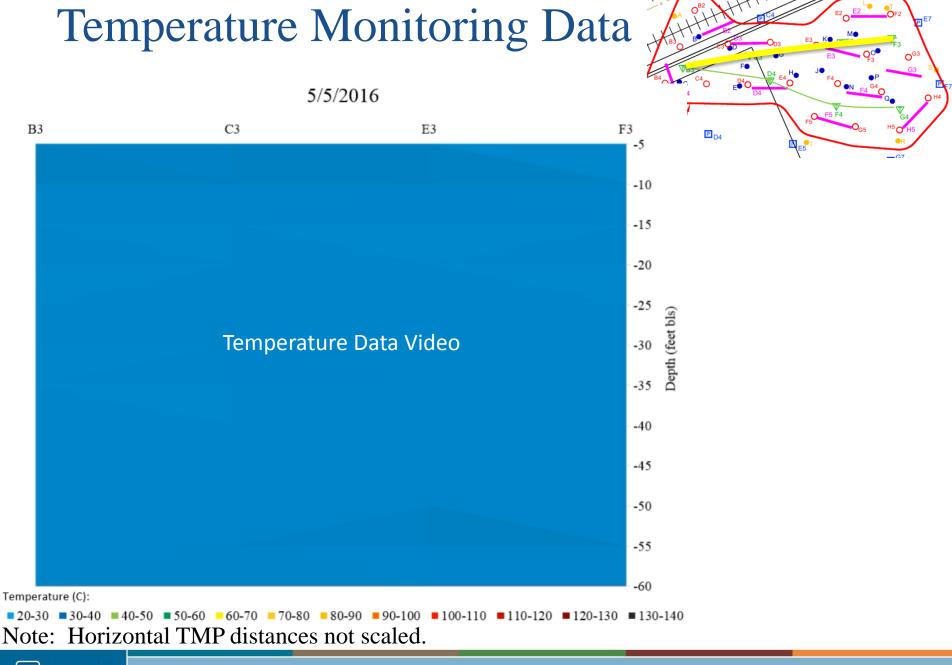


Field Temperatures

| 7 | B3 | | C3 | | D4 | | E3 | | F3 | | F4 | | G4 |
|-------|----------|-------|----------|-------|----------|-------|----------|-------|----------|-------|----------|-------|----------|
| 5 ft | 99.1 °C | 5 ft | 102.7 °C | 5 ft | 99.0 °C | 5 ft | 98.5 °C | 5 ft | 99.7 °C | 5 ft | 98.2 °C | 5 ft | 99.9 °C |
| 10 ft | 102.9 °C | 10 ft | 106.6 °C | 10 ft | 105.8 °C | 10 ft | 103.1 °C | 10 ft | 106.5 °C | 10 ft | 102.7 °C | 10 ft | 104.0 °C |
| 15 ft | 107.8 °C | 15 ft | 109.2 °C | 15 ft | 110.5 °C | 15 ft | 108.9 °C | 15 ft | 109.2 °C | 15 ft | 104.5 °C | 15 ft | 106.6 °C |
| 20 ft | 110.0 °C | 20 ft | 110.2 °C | 20 ft | 110.7 °C | 20 ft | 112.9 °C | 20 ft | 112.2 °C | 20 ft | 114.0 °C | 20 ft | 111.1 °C |
| 25 ft | 112.3 °C | 25 ft | 111.6 °C | 25 ft | 114.3 °C | 25 ft | 115.1 °C | 25 ft | 116.4 °C | 25 ft | 114.5 °C | 25 ft | 113.7 °C |
| 30 ft | 115.5 °C | 30 ft | 115.5 °C | 30 ft | 114.9 °C | 30 ft | 117.7 °C | 30 ft | 118.4 °C | 30 ft | 118.3 °C | 30 ft | 107.2 °C |
| 35 ft | 112.0 °C | 35 ft | 119.0 °C | 35 ft | 115.5 °C | 35 ft | 119.4 °C | 35 ft | 118.8 °C | 35 ft | 117.2 °C | 35 ft | 117.6 °C |
| 40 ft | 118.9 °C | 40 ft | 121.0 °C | 40 ft | 101.3 °C | 40 ft | 122.3 °C | 40 ft | 122.8 °C | 40 ft | 122.1 °C | 40 ft | 111.6 °C |
| 45 ft | 122.7 °C | 45 ft | 124.0 °C | 45 ft | 119.8 °C | 45 ft | 123.0 °C | 45 ft | 125.6 °C | 45 ft | 122.7 °C | 45 ft | 120.7 °C |
| 50 ft | 125.7 °C | 50 ft | 126.6 °C | 50 ft | 126.8 °C | 50 ft | 125.1 °C | 50 ft | 127.5 °C | 50 ft | 126.8 °C | 50 ft | 126.7 °C |
| 55 ft | 128.2 °C | 55 ft | 128.5 °C | 55 ft | 122.0 °C | 55 ft | 128.7 °C | 55 ft | 129.7 °C | 55 ft | 126.8 °C | 55 ft | 124.5 °C |
| 60 ft | 130.5 °C | 60 ft | 129.3 °C | 60 ft | 125.4 °C | 60 ft | 119.1 °C | 60 ft | 122.7 °C | 60 ft | 128.2 °C | 60 ft | 128.9 °C |

| PCU | Field Data: | Blower OUT Data: | |
|--|---|--|--|
| Main Contactor (Green = Open) (Red = Closed) Total Uptime: 1445 Hours Electrode Voltage: 127 VAC Electrode Total Power: 780 kW | Field Vacuum: -2.00 PSIa Manifold Temp "Condenser IN": 80.6°C Manifold Temp "Condenser OUT": 36.6°C | Manifold Temp: Manifold Pressure: Humidity: Air Flow: | 64.6°C 2.756 "WC 34.6 %R.H. 336. SCFM |

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Performance Monitoring

- Hot sampling techniques utilized
 - Stainless steel cooling coil in ice bath for sample cooling
 - Artesian conditions due to the difference in formation pressure/temperature at depth; traditional DPT methods were not used
 - Waterloo profiler with adaptive sample approach (focused sampling in 1' increments)
- 3-man drill crew allowed resting and engineering controls to manage heat stress
- Sampling intervals and optimized based on data from round to round



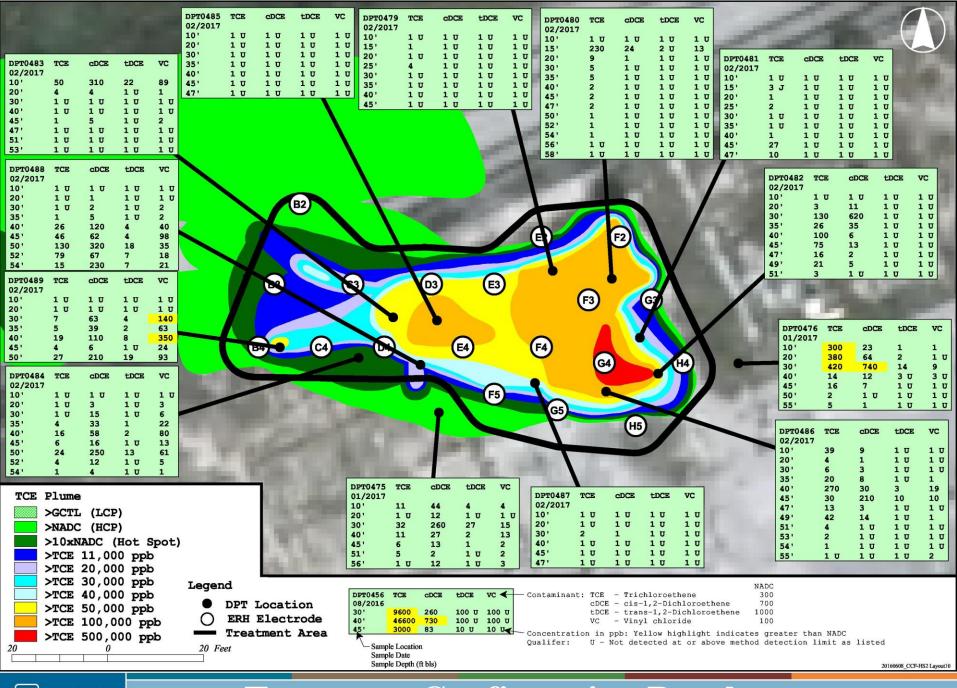




| Legend DP0441 TCE NOR V DP0443 TCE NOR V DP0443 TCE NOR V DP0444 TCE NOR V DP0445 TCE DD0 DD0 DD0 < | | | | | | | | | | | | | | | | | | | | | | | | 255 |
|--|--|-------|--------|---|--------|------|------|--|--|--------------------|---------------------------|------|---|------|-------|------|-------|--------------|-------|-----|---------|--|----------|--|
| 301 240 240 240 100 201 3 1 1 100 201 0 2 0 | | | | | | TCE | CDCE | | | | CDCE | vc | | TCE | CDCE | VC | | | CDCE | VC | | TCE | CDCE | VC |
| 30: 28' 30: 50: 21' 15: 10' 30' 3'' 10' 5'' 0.2' </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>240</td> <td>2400</td> <td></td> <td></td> <td></td> <td>40</td> <td>٤</td> <td></td> <td></td> <td>27</td> <td>1</td> <td></td> <td></td> <td>3 U</td> <td>41</td> <td></td> <td>0.22 0</td> <td>I 0.20 U</td> <td>0.13 U</td> | | | | | | 240 | 2400 | | | | 40 | ٤ | | | 27 | 1 | | | 3 U | 41 | | 0.22 0 | I 0.20 U | 0.13 U |
| DP70422 TCB cbCB VC 45 2200 350 2200 300 2200 300 2200 2200 300 2200 200 2000 2200 200 2000 2200 2000 2000 2200 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 2000 | | | | | | | | | Name and Address of the Owner o | | | | Constant and a second se | | | | 60' | 3 ប | 3 U | 1 U | 55' | | | |
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| 20' 950 3300 1100 5' 260 1300 740 5' 260 1300 740 5' 260 1300 740 5' 260 25' 2000 120 100 100 100 100 100 100 100 10 | | TCE | CDCE | vc | | | | | | | | | | | | | | | | / | | TOE | CDCB | VC |
| 30° 9° 9° 450 10° | | 950 | 3500 | 1100 | | | | | | | | | | | | | | | | | | | | |
| a g - 1100 200 100 200 11/2015 55 - 50 120 320 300 5100 530 520 11/2015 200 100 100 11/2015 200 100 100 100 | | | | 170 | | | | | | CR (| | | | | | 1000 | | | | | 60' | 610 | 5900 | 1500 |
| 50' 4300 1900 930 100' 20' 79 4400 790 10' 10' 20' 10' 10' 20' 10' 10' 10' 20' 10' <t< td=""><td></td><td></td><td></td><td></td><td></td><td>- N</td><td></td><td></td><td></td><td></td><td></td><td>Ŭ</td><td></td><td></td><td>1</td><td>1000</td><td></td><td></td><td></td><td>/</td><td></td><td>TCE</td><td>CDCE</td><td>VC</td></t<> | | | | | | - N | | | | | | Ŭ | | | 1 | 1000 | | | | / | | TCE | CDCE | VC |
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| Legend CDCE | | | | | | | | | | | | | | | | | | | | | | | | 110 |
| Legend CDCE & DPT Location Treatment Area VC TCE >GCTL (LCP) >SGCTL (LCP) >NADC (HCP) >TCE 11,000 ppb >TCE 11,000 ppb >TCE 20,000 ppb >TCE 30,000 ppb >TCE 30,000 ppb | | 120 U | 6000 | 790 | | | | | | | | | | | | | | | | | | | | State 2003 |
| CDCE DPT Location Treatment Area VC TCE >CDC1 (LCP) >NADC (HCP) >10xNADC (Hot Spot) >TCE 11,000 ppb >TCE 20,000 ppb >TCE 30,000 ppb >TCE 30,000 ppb | Legend | 1 | | | | | | | | | | | | | | | | | | | 40' | 14 | 28 | 1 |
| CDCE Treatment Area VC TCE >GCTL (LCP) >NADC (HCP) >10xNADC (Hot Spot) >TCE 11,000 ppb >TCE 20,000 ppb >TCE 30,000 ppb | | | | | | | | | | | | | | | | | | | | | | and the second | | |
| C Treatment Area VC TCE >SCTL (LCP) >NADC (HCP) >10xNADC (Hot Spot) >TCE 11,000 ppb >TCE 20,000 ppb >TCE 30,000 ppb >TCE 30,000 ppb | CDCE | | | | | | | 1 | | | | | | | | | | | X | | | | | 1773 - Contra - Contr |
| VC ICE SGCTL (LCP) 11/2015 NADC (HCP) 30' 9 34 13 SIGURATION (Hot Spot) 30' 9 34 13 STCE 11,000 ppb 50' 4100 1400 410 STCE 20,000 ppb 50' 4100 1400 410 STCE 30,000 ppb DPT0440 TCE CDCE VC DPT0440 TCE CDCE VC DPT0430 TCE CDCE VC | 8 | | reati | ient. | Area | | DPTO | 443 T | CE cD | CE V | c I | | | | _ \ | | | | | | DDT0430 | TOP | | |
| 30' 9 34 13 40' 510 xNADC (HcP) 30' 9 34 13 40' 510 xNADC (Hct Spot) 510 29 2 U >TCE 11,000 ppb 50' 400 140 >TCE 20,000 ppb 50' 1500 8100 1200 >TCE 30,000 ppb PDF0440 TCE CDCE VC DPT0438 TCE CDCE VC | VC | | | | | | | | | | | | T | | | | | | | | | ICE | CUCE | vc |
| 40' 510 29 2 U 45' 8600 7800 51 50' 4100 1400 410 50' 20500 4300 40 U 55' 1500 8100 1200 DPT0440 TCE CDCE VC DPT0438 TCE CDCE VC | | | | | | | | | | | | | 1 | | | | | | | | | | | |
| >10xNADC (Hot Spot) 45' 8600 7800 51 >TCE 11,000 ppb 50' 4100 1400 410 >TCE 20,000 ppb 55' 1500 8100 1200 >TCE 30,000 ppb DPT0440 TCE CDCE VC DPT0438 TCE CDCE VC DPT0438 TCE CDCE VC | | | | | | | | | | | | | | | | 1 | | | | | | | | |
| >TCE 20,000 ppb 55' 1500 8100 1200 55' 443000 37600 5000 U >TCE 30,000 ppb DPT0440 TCE CDCE VC DPT0438 TCE CDCE VC D | | | | | | ot) | 45' | 8 | 600 78 | 300 5 | 1 | | | | | 1 | | | | | 45' | | | |
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| >TCE 30,000 ppb DPT0440 TCE cDCE VC DPT0430 TCE cDCE VC DPT0438 TCE cDCE VC DPT0429 TCE cDCE <td></td> <td>1</td> <td></td> <td></td> <td></td> <td>5000 0</td> | | | | | | | | | | | | | | | | | | | | 1 | | | | 5000 0 |
| >TCE 50,000 ppb 20' 89 590 1100 20' 3 U 120 22 20' 60 U 5500 1800 20' 3 U 120 22 20' 60 U 5500 1800 >TCE 100,000 ppb 30' 22 120 41 30' 4 7 8 30' 20 340 310 30' 6 6 2 20' 3 U 27 1 U >TCE 500,000 ppb 40' 290 22 3 U 40' 9 18 1 U 40' 19 40 2 U 40' 3 U 27 1 U 50' 1800 30' 20 340 310 30' 50' 180 30' 20' 3 U 27 1 U 50' 20' 18 33 U 27 1 U 50' 100' 10 U 45' 3 U 21 1 U 50' 140 110 99 50' 86800 13600 100 U 50' 18 33 23 50' 0' 0' 0' 0' 0' 0' 0' 0' 0' 0' 0' 0' 0 | | | | | | | | | CE cD | DCE V | | | TCE | CDCE | | | TCE | CDCE | VC | | | CDCE | VC | |
| >TCE 100,000 ppb 30' 22 120 41 30' 4 7 8 30' 20 340 310 30' 6 6 2 40' 40' 9 18 1 U 40' 19 40 2 U 40' 3 U 27 1 U // > > TCE 500,000 ppb 45' 14000 4600 40 U 45' 41 22 5 45' 2200 2100 10 U 45' 3 U 27 1 U 45' 3 U 27 1 U 45' 3 U 21 1 U 40' 50' 186800 13600 100 U 50' 18 33 23 55' 26 44 20 40' | | | | | | | | | 9 59 | 0 1 | | | 3 U | 120 | | | 60 U | 5500 | 1800 | | | 3 U | 1 | še TČH |
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| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | >TCE 5 | 500,0 | dag 00 | | | | | Manager and States | | | | | | | | | | | | | | S2 er |
| <u>55' 770 3200 12500 55' 3 3 び 15 55' 76000 55300 7900 55' 26 44 20</u> いっつ | 15 | | | | | Feet | 50' | 3 | 3300 59 | 00 1 | 00 5 | 0' | 140 | 110 | 99 50 |) ' | 86800 | 13600 | 100 U | | | | 23 | 101 201 |
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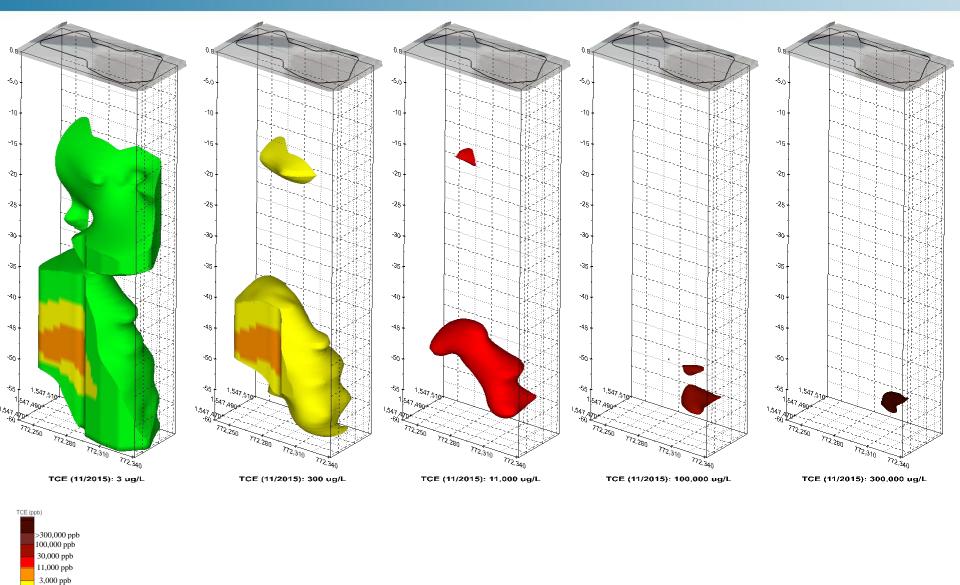
Baseline DPT Sampling Results

TETRA TECH



Treatment Confirmation Results

20

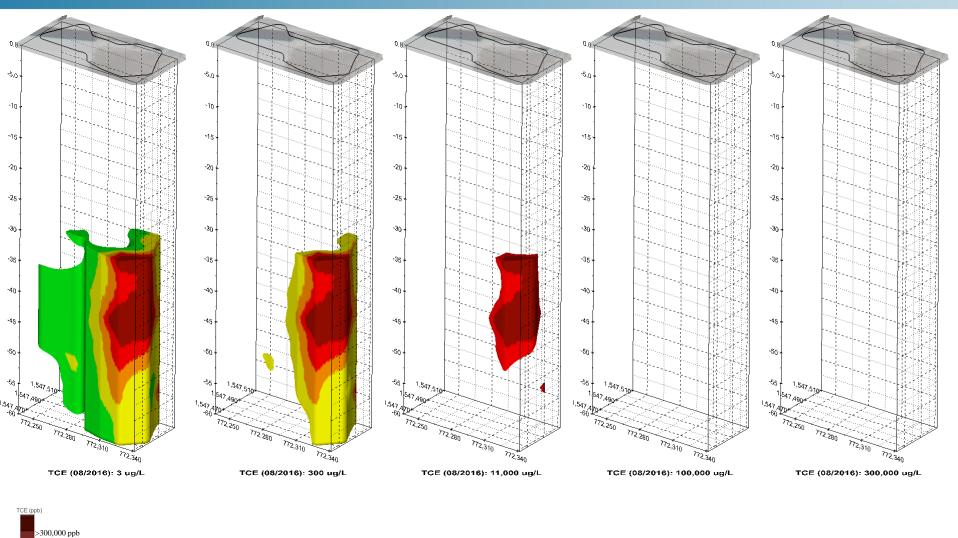




300 ppb

3 ppb

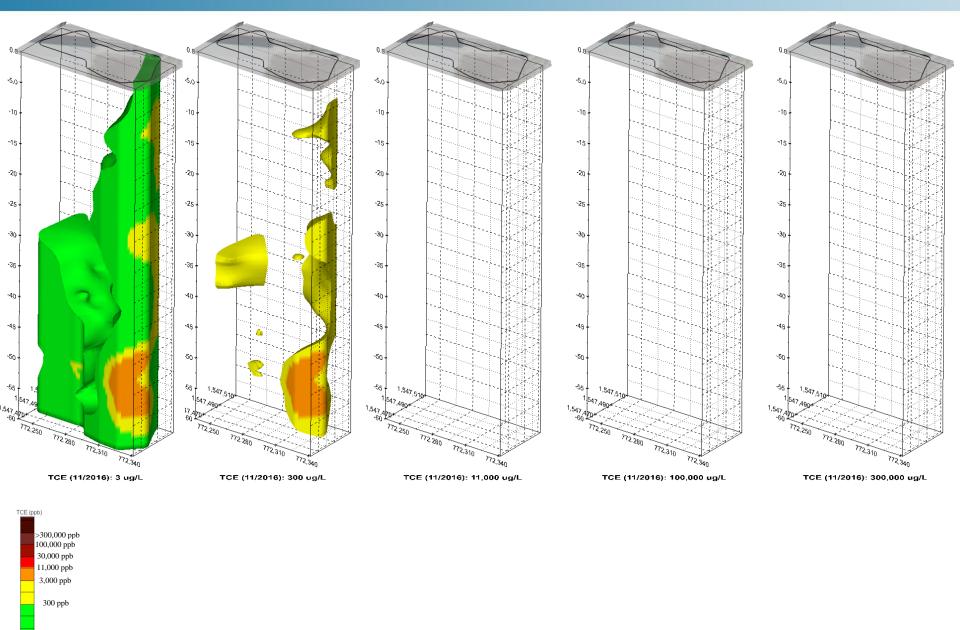
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TCE EVS Plumes, August 2016

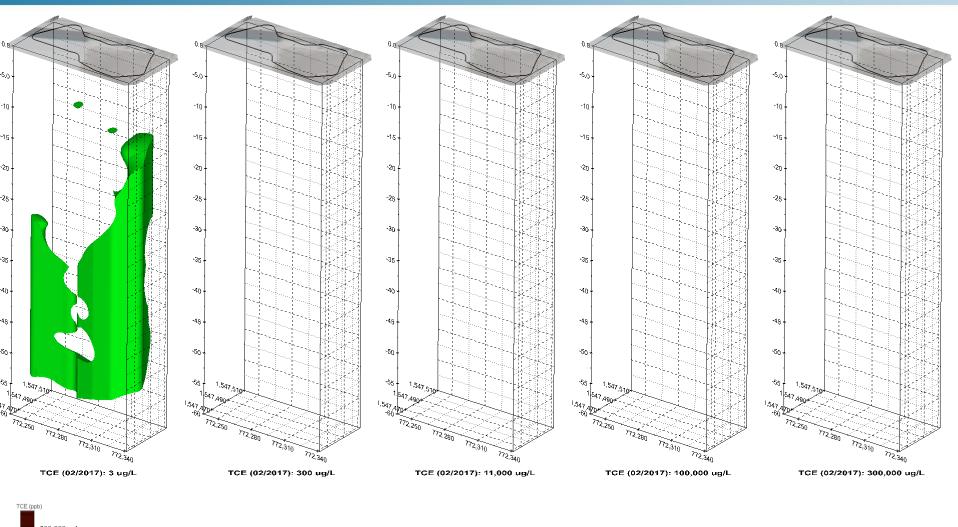


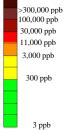
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TCE EVS Plumes, November 2016

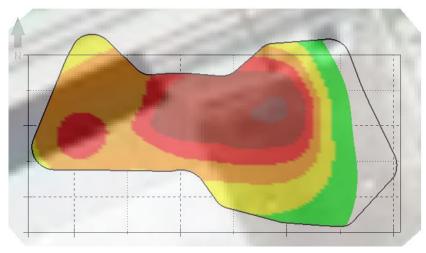




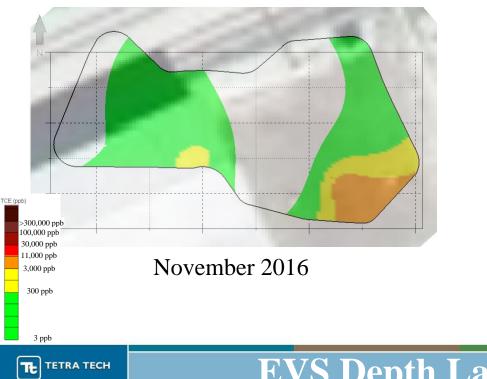
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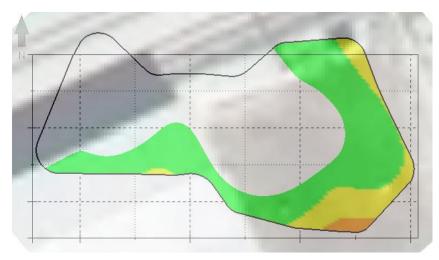
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TCE EVS Plumes, February 2017

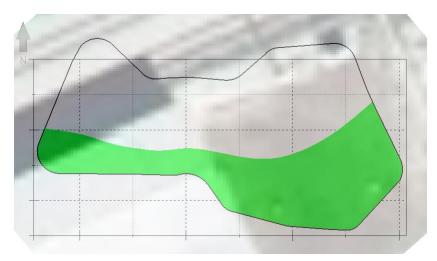


Baseline, November 2015

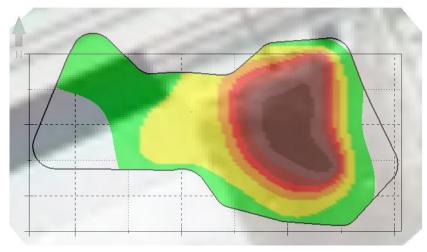




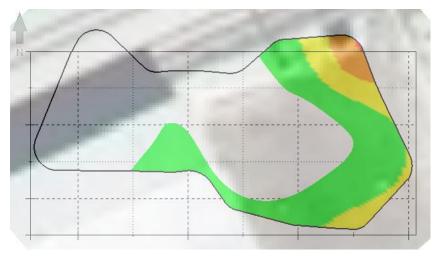
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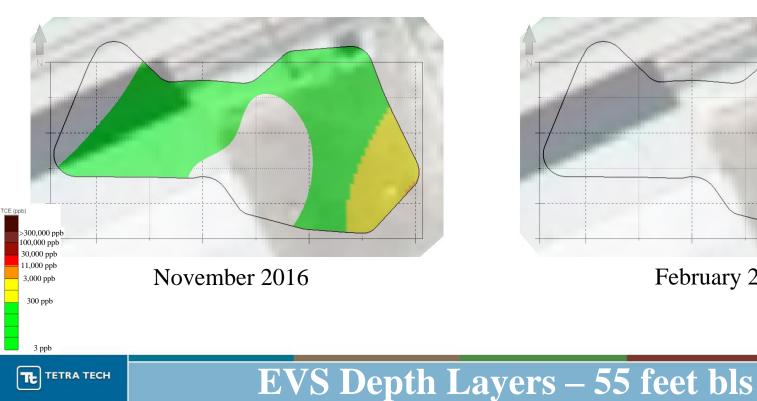
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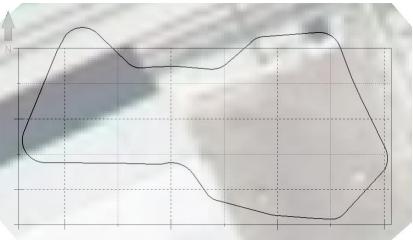


Baseline, November 2015



August 2016





February 2017

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| PM DPT # (DPT-0) | Max TCE PM Result (µg/L) | Baseline DPT # (DPT-0) | Baseline TCE Result (µg/L) | % TCE Concentration Reduction | Orders of Magnitude Reduction |
|---------------------|-----------------------------|---------------------------|-------------------------------|-------------------------------------|-------------------------------------|
| 479 | 4 | 433 | 203,000 | 99.998% | 4.7 |
| 480 | 230 | 434 | 459,000 | 99.950% | 3.3 |
| 481 | 27 | 435 | 383,000 | 99.993% | 4.2 |
| 482 | 130 | 436 | 1,430,000 | 99.991% | 4.0 |
| 486 | 270 | 439 | 443,000 | 99.939% | 3.2 |
| 487 | 2 | 393 | 241,000 | 99.999% | 5.1 |
| 485 | 1 | 441 | 116,000 | 99.999% | 5.1 |
| 483 | 50 | 442 | 68,800 | 99.927% | 3.1 |
| 488 | 130 | 396 | 37,200 | 99.651% | 2.5 |
| 484 | 24 | 443 | 8,600 | 99.721% | 2.6 |
| 489 | 27 | 431 | 40,000 | 99.933% | 3.2 |

| Average % Reduction (of >100 ppm baseline locatio |
|---|
|---|

Average % Reduction (of <100 ppm baseline locations):</th>99.808%

Average % Reduction (overall): 99.918%



Lessons Learned

- Site conditions can change from investigation to design
 - Ensure the installation is appropriate for site conditions
 - DPT baseline sampling resulted in revision of treatment area and +2 electrodes
- Advocate f_{oc} soil data in source area
 - orders of magnitude sensitivity in mass estimates
- Sonic electrode installation significantly reduced waste
 - Minimal drilling spoils; soil displaced outward in boring
 - Liquid IDW treated and discharged onsite with mobile air stripper
- Effective communication with facility and project stakeholders is paramount
- Continuous data review and subcontractor interaction an important aspect of efficiently optimizing ERH performance
- High resolution site monitoring provided effective optimization tools
- Performance based contract an effective risk management resource to secure key subcontractors to objectives
 - Without performance guarantee to ERH subcontractor, typical ERH contracts are based on subsurface energy delivery or temperature targets. In those cases, site objectives to <NADC levels (e.g., <300 ppb TCE) may not be accomplished.

Conclusions and Path Forward

- IM successfully removed TCE source zone and contaminant mass in fine grained and overlying units
- Operations terminated based on confirmation DPT sampling results and secondary lines of evidence such as temperature, mass removal trends, etc.
- Source zone transitioning to MNA
- Air sparging treatment planned for surrounding dilute plume

Thank you! Questions?

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