# Skew-Symmetric Splitting and Stability of High Order Central Schemes

H.C. Yee, NASA Ames Research Center (Joint work: B. Sjogreen, D. Kotov)

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## **Challenges in Numerical Method Development**

(Multiscale DNS & LES, and Aeroacoustic Turbulence Applications)

- Schemes developed for short time integration might suffer from nonlinear instability for longer time integration
- Stable & Accurate Temporal & Spatial Low Dissipative & Dispersive methods applicable to long time integration are required
- Numerical stability & accuracy requirements are an intricate balancing act
  - > More stable schemes usually contain more numerical dissipation than their higher accuracy schemes counterparts
  - > Turbulence cannot tolerate numerical dissipation
  - > Proper amount of numerical dissipation is required for stability in the vicinity of discontinuities
  - > Flows containing stiff source terms:
    Numerical dissipation & under-resolved grid may lead to incorrect shock speed

### Recent developments:

Yee & Sjogreen, 2007-2009, Sjogreen & Yee, 2016-2017, Wang et al., 2009-2015, Kotov et al., 2011-2014

### **Outline**

- Methods to Improve Nonlinear Stability & Accuracy for Long Time Wave Propagation & Long Time Integration of Complex Compressible Flows
- Skew-Symmetric Splitting of the Inviscid Flux Derivatives
   (This talk concentrates on one of 5 improvements)
- Selected Numerical Results
- Concluding Remarks

#### Remark

Schemes with improve nonlinear stability can benefit short time & long time integrations of nonlinear fluid flows

# Five Methods to Improve Nonlinear Stability & Accuracy (Long Time Wave Propagation & Long Time Integration of Complex Compressible Fluids & Plasma)

### **Under the Yee et al. nonlinear filter approach framework:**

- Standard High Order Linear Filters are to be Replaced by High Order Nonlinear Filters
- Smart Flow Sensors to Provide Locations & Amount of Needed Numerical Dissipation
- Skew-Symmetric Splitting of the Inviscid Flux Derivative Before the Application of Non-Dissipative Centered Schemes
- DRP (Dispersion Preservation-Relation) Schemes as Alternatives to Classical High Order Central Schemes
- Stable High-Order Entropy Conservative Numerical Fluxes with Entropy Satisfying Properties - *Numerical solution satisfies an additional discretized conservation law*

### Remark

Present numerical method development for gas dynamics with Modification can carry over to MHD for short time & long time integration

Yee et al., 2000-2013, Yee & Sjogreen, 2007-2009, Sjogreen & Yee, 2016-2017, Wang et al., 2009-2015, Kotov et al., 2011-2014

## **Skew-Symmetric Splitting of Inviscid Flux Derivatives**

(Improve nonlinear stability for high order central schemes)

Olsson & Oliger 1994, Yee et al. 1999, Ducros et al. 2000, Pirozzoli 2009

- Entropy splitting: Semi-conservative splitting for shock-free turbulence (Olsson & Oliger 1994, Yee et al. 1999-2007, Sandham et al. 2002-present)
- Natural Splitting: Linearized Euler & Non-conservative Systems
- Splitting to Preserve Discrete Momentum and/or Energy Conservation: (Arakawa 1966, Blaisdell et al. 1996, Mansour 1980, etc.)
- Ducros et al. Type Conservative Splitting: Euler & MHD
- Generalized Skew-Symmetric Splitting: 3-parameter family (Pirozzoli 2009)

This talk concentrates only on Ducros et al. type conservative splitting

# **Ducros et al. Splitting**

(Improve nonlinear stability for high order central schemes)

Split the derivative of a product into conservative & non-conservative parts:

$$(ab)_x = \frac{1}{2}(ab)_x + \frac{1}{2}ab_x + \frac{1}{2}a_xb_x$$

Approximation of the split form can be written in conservative form: e.g.,

$$\frac{1}{2}D_0(ab)_j + \frac{1}{2}a_jD_0b_j + \frac{1}{2}b_jD_0a_j = \frac{1}{4}D_+(a_j + a_{j-1})(b_j + b_{j-1})$$

 $D_0$ : 2<sup>nd</sup>-order central,  $D_+u_i = (u_{i+1} - u_i)/\Delta x$ 

The above can be generalized to 2pth-order accurate: Ducros et al. 2000

$$D_{0p}u_j = \sum_{k=1}^p \alpha_k^{(p)} D_0(k) u_j \qquad D_0(k) u_j = (u_{j+k} - u_{j-k})/(2k\Delta x)$$
$$\sum_{k=1}^p \alpha_k^{(p)} = 1 \qquad \sum_{k=1}^p \alpha_k^{(p)} k^{2n} = 0, \quad n = 1, \dots, p-1$$

## **Ducros et al. Splitting (Cont.)**

(Improve nonlinear stability for high order central schemes)

### **Approximation of the 2pth-order split form in conservation form:**

$$\begin{split} \frac{1}{2}D_p(ab) + \frac{1}{2}D_p(a)b + \frac{1}{2}aD_p(b) &= \\ \frac{1}{\Delta x}\sum_{k=1}^p \frac{1}{2}\alpha_k \left( (a_{j+k}b_{j+k} - a_{j-k}b_{j-k}) + a_j(b_{j+k} - b_{j-k}) + (a_{j+k} - a_{j-k})b_j \right) \\ &= \frac{1}{\Delta x}\sum_{k=1}^p \frac{\alpha_k}{2} \left( \sum_{m=0}^{k-1} (a_{j-m} + a_{j+k-m})(b_{j-m} + b_{j+k-m}) \right. \\ &\left. - \sum_{m=0}^{k-1} (a_{j-1-m} + a_{j-1+k-m})(b_{j-1-m} + b_{j-1+k-m}) \right) = \frac{1}{\Delta x} (h_{j+1/2} - h_{j-1/2}) \end{split}$$

# **2p<sup>th</sup>-order Central Ducros et al. Splitting Numerical Flux for 3D Gas Dynamics**

### 3D Inviscid Flux Derivative in x-Direction:

$$\mathbf{f} = ([\rho u, \rho u^2 + p, \rho uv, \rho uw, (e+p)u]^T$$

### $2p^{th}$ -order Numerical Flux in x-Direction $h_{j+1/2}$ :

$$\begin{array}{l} \mathbf{h}_{j+1/2} = \\ \\ \frac{1}{2} \sum_{k=1}^{p} \alpha_k \sum_{m=1}^{k-1} \begin{pmatrix} (\rho_{j-m} + \rho_{j+k-m})(u_{j-m} + u_{j+k-m}) \\ (\rho_{j-m} u_{j-m} + \rho_{j+k-m} u_{j+k-m})(u_{j-m} + u_{j+k-m}) + p_{j-m} + p_{j+k-m} \\ (\rho_{j-m} v_{j-m} + \rho_{j+k-m} v_{j+k-m})(u_{j-m} + u_{j+k-m}) \\ (\rho_{j-m} w_{j-m} + \rho_{j+k-m} w_{j+k-m})(u_{j-m} + u_{j+k-m}) \\ (e_{j-m} + p_{j-m} + e_{j+k-m} + p_{j+k-m})(u_{j-m} + u_{j+k-m}) \end{pmatrix} \end{array}$$

#### Well-Balanced High Order Nonliner Filter Schemes Non-Reacting & Reacting Flows Yee & Sjögreen, 1999-2010, Wang et al., 2009-2010

#### **Preprocessing step**

Condition (equivalent form) the governing equations by, e.g., *Yee et al. Entropy Splitting, Ducros et al. Splitting, Tadmor Splitting* to improve numerical stability

#### High order low dissipative base scheme step (Full time step)

- High order central, DRP, or entropy conser. num. flux scheme
- SBP numerical boundary closure, matching spatial & temporal order conservative metric evaluation Vinokur & Yee, Sjögreen & Yee, Yee & Vinokur

#### Nonlinear filter step

- Filter the base scheme step solution by a dissipative portion of any
  positive high-order shock capturing scheme, e.g., 7<sup>th</sup>-order positive
  WENO
- Use local flow sensor to control the amount & location of the nonlinear numerical dissipation to be employed

<u>Well-balanced scheme</u>: preserve certain non-trivial physical steady state solutions of reactive eqns exactly **Note**: "Nonlinear Filter Schemes" not to be confused with "LES filter operation"

#### **Nonlinear Filter Step** $(U_t + F_x(U) = 0)$

Denote the solution by the base scheme (e.g. 6<sup>th</sup> order central, 4th order RK)

$$U^* = L^*(U^n)$$

• Solution by a nonlinear filter step

$$U_j^{n+1} = U_j^* - \frac{\Delta t}{\Delta x} \left[ H_{j+1/2} - H_{j-1/2} \right]$$
$$H_{j+1/2} = R_{j+1/2} \overline{H}_{j+1/2}$$

 $\overline{H}_{j+1/2}$  - numerical flux,  $R_{j+1/2}$  - right eigenvector, evaluated at the Roe-type averaged state of  $U_i^*$ 

• Elements of  $\overline{H}_{i+1/2}$ :

$$\overline{h}_{j+1/2} = \frac{\kappa_{j+1/2}^m}{2} \left( s_{j+1/2}^m \right) \left( \phi_{j+1/2}^m \right)$$

 $\phi^m_{j+1/2}$  - Dissipative portion of a shock-capturing scheme  $s^m_{j+1/2}$  - Local flow sensor (indicates location where dissipation needed)  $\mathbf{K}^m_{j+1/2}$  - Controls the amount of  $\phi^m_{j+1/2}$ 

#### **Improved High Order Filter Method**

#### Form of nonlinear filter

$$\overline{h}_{j+1/2} = \frac{\kappa_{j+1/2}^m}{2} \left( s_{j+1/2}^m \right) \left( g_{j+1/2}^m - b_{j+1/2}^m \right)$$

Control amount of dissipation based on (Shock Sensor, ACM local flow condition

Local flow sensor (Harten), Ducros et al, Multiresolution wavelet, etc.)

Any High Order High order central Shock capturing numerical flux (e.g. WENO5)

numerical flux (e.g. 6th order central)

 $2007 - \kappa = \text{global constant}$  $2009 - \kappa_{j+1/2} = \text{local}$ , evaluated at each grid point Simple modification of κ (Yee & Sjögreen, 2009)

$$f(M) = \min \left( \frac{M^2}{2} \frac{\sqrt{4 + (1 - M^2)^2}}{1 + M^2}, 1 \right)$$

For other forms of  $\kappa_{i+1/2}$ ,  $s_{i+1/2}$ , see (Yee & Sjögreen, 2009)

## **Performance of High Order Nonlinear Filter Scheme**

(Skew-Symmetric Splitting of Inviscid Flux Derivative)

### Rapidly Developing Flows: (subsonic, transonic, supersonic & hypersonic)

- > Smooth flows, Yee et al., 1999
- > Flows with discontinuities, Yee et al., Sjogreen & Yee, Sandham et al., 2000-2004
- > Supersonic Mixing & Richtmyer-Meshkov Instability, Yee & Sjogreen, 2004, 2012
- > Extreme Flows positivity-preserving nonlinear filter scheme, Kotov et al., 2014
- > Flows with stiff source terms Wrong shock speed
  High order well-balanced subcell resolution schemes
  Wang et al., Yee et al., Kotov et al., 2009-2015

### **Long Time Integrations, DNS & LES:**

- → > Shock Free Compressible Turbulence (Kotov et al., 2016)
- > Low Speed Turbulence with Shocklets (Kotov et al., 2016)
  - > LES of Temporally Evolving Mixing Layers (Yee et al., 2012)
  - > DNS & LES of Turbulence Interacting with a Stationary Supersonic Shock -- One-sided SGS model & subcell resolution to locate the shock within one grid cell (Kotov et al., 2016)
  - > 3D Forced Turbulence (Time Varying Forcing) (Sjorgreen et al., 2016)
  - > Dual & Direct Cascade Study of 2D Turbulence with Random Forcing (Astrophysical Applications, Kritsuk et al., 2016)

#### **3D Taylor-Green vortex**

(Inviscid & Viscous Shock-Free Turbulence)

Computational Domain:  $2\pi$  square cube,  $64^3$  grid.

(Reference solution on 256<sup>3</sup> grid)

#### **Initial condition**

Final time: t=10

$$\rho = 1, 
p = 100 + ([\cos(2z) + 2][\cos(2x) + \cos(2y)] - 2)/16, 
u_x = \sin x \cos y \cos z 
u_y = -\cos x \sin y \cos z 
u_z = 0.$$
Initial turbulent Mach number:  $M_{t,0} = 0.042$ 

#### Viscous case

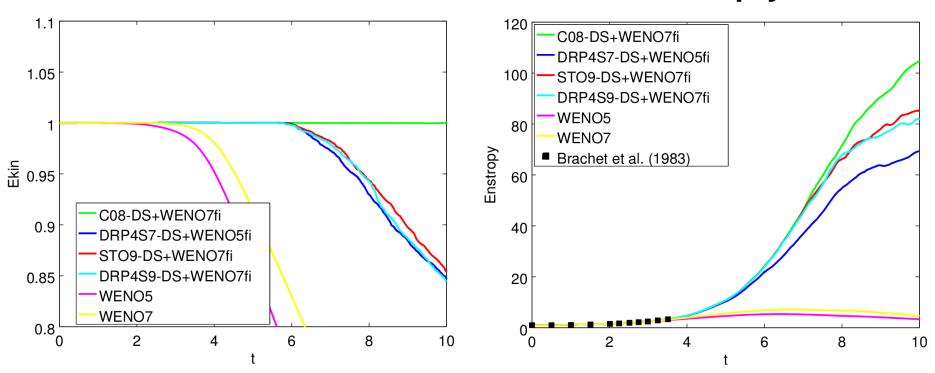
$$\mu/\mu_{ref} = (T/T_{ref})^{3/4}$$
  
 $\mu_{ref} = 0.005, T_{ref} = 1, Re_0 = 2040$ 

# 3D Taylor-Green Vortex (Compressible & Inviscid)

(Comparison of 6 Methods, 64<sup>3</sup> grids)

### **Kinetic Energy**

### **Enstrophy**



**C08-DS+WEN07fi:** 8th-order central + Ducros split +WEN07fi

DRP4S7-DS+WEN05fi: Tam & Webb 4th-order DRP, 7pt grid stencil + Ducros split +WEN05fi

ST09-DS+WEN07fi: Bogey & Bailly 4th-order DRP, 9pt grid stencil + Ducros split +WEN07fi

DRP4S9-DS+WEN07fi: Tam & Webb 4th-order DRP, 9pt grid stencil + Ducros split +WEN07fi

#### **Compressible Isotropic Turbulence**

(Low Speed Turbulence with Shocklets)

Computational Domain:  $2\pi$  square cube,  $64^3$  grid. (Reference solution on  $256^3$  grid)

#### **Problem Parameters**

**Root-mean-square velocity:**  $u_{rms} = \sqrt{\frac{\langle u_i u_i \rangle}{3}}$ 

**Turbulent Mach number:**  $M_t = \frac{\sqrt{\langle u_i u_i \rangle}}{\langle c \rangle}$ 

Taylor-microscale:  $\lambda = \sqrt{\frac{\langle u_x^2 \rangle}{\langle (\partial_x u_x)^2 \rangle}}$ 

Taylor-microscale Reynolds number:  $Re_{\lambda} = \frac{\langle \rho \rangle u_{rms} \lambda}{\langle \mu \rangle}$ 

Eddy turnover time:  $\tau = \lambda_0/u_{rms.0}$ 

#### **Initial Condition:** Random solenoidal velocity field with the given spectra

$$E(k) \sim k^4 \exp(-2(k/k_0)^2)$$

$$\frac{3}{2}u_{rms,0}^{2} = \frac{\langle u_{i,0}u_{i,0}\rangle}{2} = \int_{0}^{\infty} E(k)dk$$

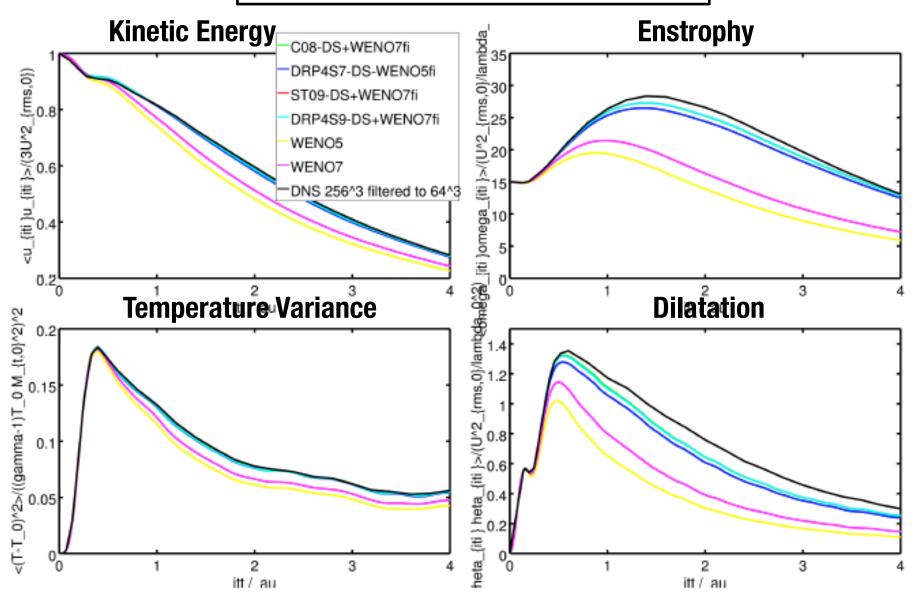
$$u_{rms,0} = 1$$
,  $k_0 = 4$ ,  $\tau = 0.5$ ,  $M_{t,0} = 0.6$ ,  $Re_{\lambda,0} = 100$   
Final time:  $t = 2$  or  $t/\tau = 4$ 

# 3D Isotropic Turbulence with Shocklets Compressible & Inviscid

**Comparison of 6 Methods, 64**<sup>3</sup> grids **Energy Spectra** 1e-2 C08-DS+WENO7fi DRP4S7-DS+WENO5fi ST09-DS+WENO7fi 1e-4 E(大) DRP4S9-DS+WENO7fi WENO5 1e-6 WENO7 DNS 256<sup>3</sup>  $E = k^{-5/3}$ 1e+1 1e + 0k

# **3D Isotropic Turbulence with Shocklets**

**Comparison of 6 Methods, 64<sup>3</sup> grids** 



## **High Order Numerical Method Development in MHD**

(Added Issues Beyond Compressible Gas Dynamics Developments)

### **MHD Equations**:

- > Conservative Form non-strictly hyperbolic system w/ degenerate identical eigenvalues
- > Godunov/Powell Form (1972, 1994) symmetrizable hyperbolic non-conservative system
- > Janhunen Form (2000)
- > Brackbill & Barnes (1980)

# Skew-symmetric Splitting of Inviscid Flux Derivatives: Improve Stability & Minimize Num. Dissipation

- > Yee et al. Entropy Splitting (2000) Only for the gas dynamics portion
- > Ducros et al. Splitting (2000) & Pirozzoli Generalization (2010) Not unique
- > High Order Extension of Tadmor Entropy Conservative Numerical Fluxes (Sjogreen & Yee, 2009) can be viewed as a splitting

### Discrete Conservation Methods: FV vs. FD & DG, etc; Low Order vs. High Order

- > Entropy stable conservative numerical fluxes
  - Low Order: Janhunen (2000), Winters & Gassner (2016), Chandrasekar-Klingenberg (2015)
  - High Order: Sjogreen & Yee (2009) Central, Fjordholm, Mishra & Tadmor (2012) ENO, etc.
- > Momentum conservation, Kinetic energy preservation, etc.

### **Approximate Riemann Solver:** Extension of Roe's Average States

- > Gallice average states (1997)
- > Ismail & Roe (2009) Logarithmic mean for entropy (not square root mean)

**Eigenvector Scaling:** (Roe & Balsara, 1996)

## Non-uniqueness of Ducros et al. Splitting for MHD

(Minimize the use of numerical dissipation for high order central schemes)

- MHD inviscid (ideal) flux derivatives consist of triple products of conservative variables & their derivatives
- No unique guidelines in splitting triple products of derivatives (more choices than their gas dynamics counterparts)

(See Sjogreen & Yee, ICOSAHOM-2016 & Journal version for the chosen forms)

- 3-Forms: Split all 8 flux derivatives, partial or just the gas dynamic portion (all recover to split form of gas dynamics when MHD not present) (Results compare with no splitting)
- Four forms of the MHD Equations to be solved:
  - > Conservative form
  - > Godunov/Powell symmetrizable form (non-conservative)
  - > Janhunen form: (Div B) terms not included in the gas dynamics part of the equations)
  - > Brackbill & Barnes form

The above consists of 16 combinations for the current study

# **Concluding Remarks**

(Compressible Gas Dynamics of a Wide Spectrum of Flow Types)

### **Stability Improvement by Skew-Symmetric Splitting**

Smooth Flows: Stable without added high order linear numerical dissipation

- > Semi-Conservative Entropy Splitting with summation-by-part (SBP) boundary closure energy norm bound (Yee et al. 1999-2007, Sandham et al. 2002-present)
  - Most accurate & stable among the considered three splittings
- > Ducros et al. splitting
  - Improved stability
  - Smaller improvement than Entropy Splitting

Flows with shocks: Under the Yee et al. nonlinear filter framework

**Ducros et al. Splitting Employs Two Types of Central Scheme:** 

- > Classical high order central (6th-order & 8th-order)
- > Three DRP (4th-order, 7-point & 9-point grid stencils)

**Among studied test cases** 

Classical central schemes provide slightly more improvement than DRP

# **Concluding Remarks**

(Compressible Gas Dynamics of a Wide Spectrum of Flow Types)

### **Stability Improvement by Skew-Symmetric Splitting**

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Flows with shocks: Under the Yee et al. nonlinear filter framework

**Ducros et al. Splitting Employs Two Types of Central Scheme:** 

- > Classical high order central (6th-order & 8th-order)
- > Three 4<sup>th</sup>-order 7-point & 9-point grid stencils

Classical central schemes provide slightly more improvement than DRP

# Integrated Approach for Stability, Accuracy & Reliable Simulations (Construction of High Order Low Dissipative Numerical Methods)

Yee et al. (1999-2003), Yee & Sjogreen (2004-2009), Kotov et al. (2013-2016)

### Stability & Accuracy:

- > Interior Scheme & Num. Boundary Scheme (non-periodic BC)
  Summation-by-parts (SBP) boundary closures (Strand 1994, Olsson 1996)
- > Short Time Integration vs. Long Time Integration (DNS & LES)
- > High Order GCL (Geometric Conservation Law) metric evaluation (Sjogreen et al. 2014)

### **Skew-symmetric Splitting of Inviscid Flux Derivatives:**

Further improvement of Stability & Minimize Num. Dissipation

- > Yee et al. Entropy Splitting (2000)
- > Ducros et al. Splitting (2000) & generalization
- > High Order Extension of Tadmor Entropy Conservative Numerical Fluxes (Sjogreen & Yee 2009)

#### Discrete Conservation Methods: FV vs. FD & DG, etc.

- > Entropy stable conservative high order numerical fluxes (Sjogreen & Yee 2009)
- > Momentum conservation, Kinetic energy preservation, etc.

#### Numerical Dissipation Control: Yee et al., Yee & Sjogreen, and Kotov et al. (1999-2016)

- > Turbulence cannot tolerate num. dissipation Proper amount is needed in the vicinity of high shear, shocks & contacts
- > Different requirements in the minimization of num. dissipation for different flow types
- > Adaptive flow sensor to control the amount of num. dissipation

#### Reacting Flow/Combustion: Yee et al., Wang et al., Yee & Sweby, LeVeque & Yee (1990 – 2015)

- > Stiff source terms with shock May lead to incorrect shock speed
- > Preserve certain physical steady states exactly Well-balanced scheme

### **Gas Dynamics vs. MHD scheme constructions**

Some Gas Dynamics development can carry over to MHD (Items with an arrow)

## **Astrophysical Applications: 2D Turbulence**

(Joint work with Alexei G. Kritsuk, U.C. San Diego)

### **Application**: *Energetics of the ISM in Galactic Disks*

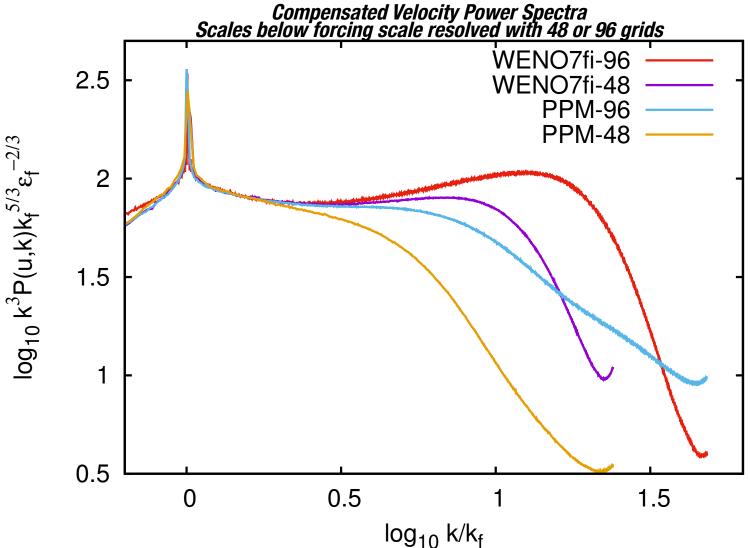
- > Dual energy cascade study
- > Does the inverse energy cascade work in the compressible case?
- > What are the corresponding scaling relations?

### Grid size:

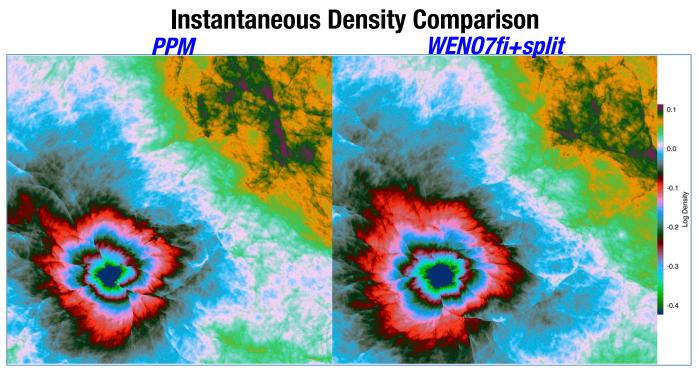
- > Physics Study: 512<sup>2</sup>, 2,048<sup>2</sup>, 8,192<sup>2</sup>, 16,384<sup>2</sup>
- > Computation Grid Resolutions: 2,048<sup>2</sup>, 8,192<sup>2</sup>, 16,384<sup>2</sup>

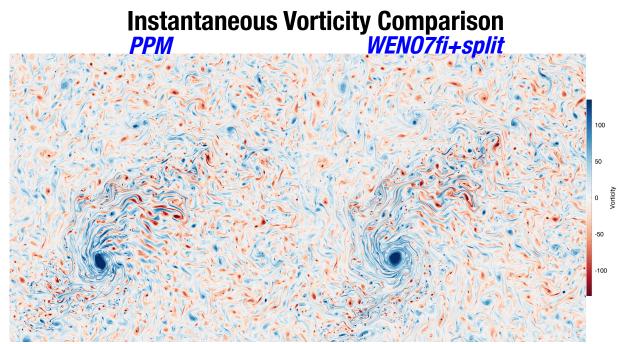
### **Scheme Comparison: PPM vs WEN07fi+split**

2D Compressible Turbulence: Isothermal  $\gamma$ =1.001, periodic BCs Flow determined by grid N, energy injection rate & energy injection scale



Spectral Bandwidth: WEN07fi+split 2.2 X > PPM;  $\sim$ 4 times less CPU in 2D for same resolution (assume 25%) Note: If P(k) is a spectrum and P(k) $\sim$ k<sup>n</sup>, then the compensated spectrum is k<sup>-n</sup>P(k)

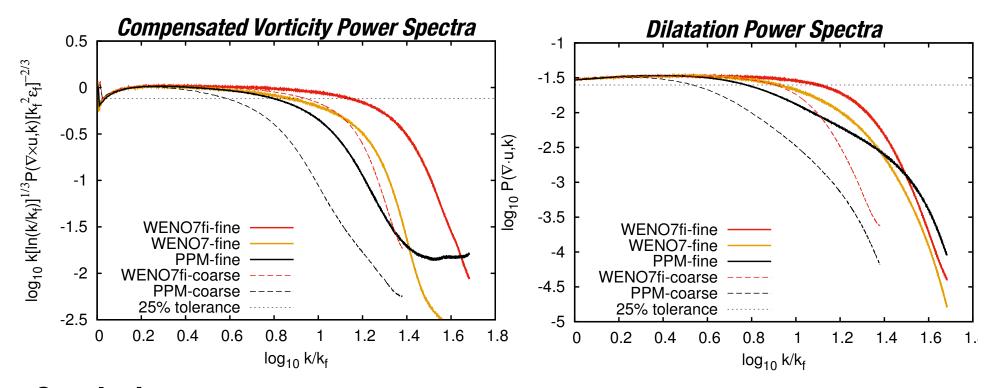




### **Scheme Comparison: PPM, WEN07, WEN07fi+split**

2D Compressible Turbulence: Isothermal  $\gamma$ =1.001, periodic BCs Flow determined by grid N, energy injection rate & energy injection scale

### **Direct Cascade study: Coarse vs. fine grids**



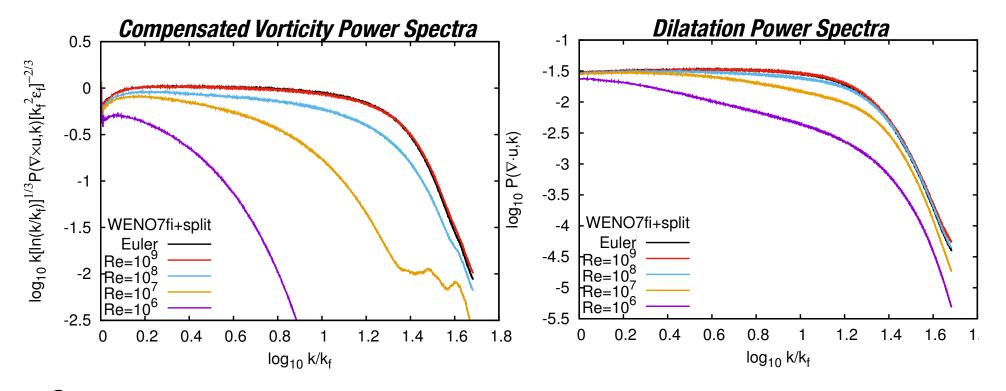
### **Conclusion:**

- Vorticity bandwidth: WEN07/PPM=1.2; WEN07fi/WEN07=1.8; WEN07fi/PPM=2.2
- <u>Dilatation bandwidth</u>: <u>WEN07/PPM=1.5</u>; <u>WEN07fi/WEN07=1.5</u>; <u>WEN07fi/PPM=2.2</u>
- Absolute WEN07fi bandwidth: for vorticity 68%; for dilatation 66%

### **Euler vs. NS Comparison: WEN07Fi+split**

2D Compressible Turbulence: Isothermal  $\gamma$ =1.001, periodic BCs Flow determined by grid N, energy injection rate & energy injection scale

Isothermal Fluids:  $T=T_0$  Constant Dynamic Viscosity,  $Re=10^6$ ,  $10^7$ ,  $10^8$ ,  $10^9$ 



### **Summary:**

WEN07fi+split correctly captures theoretically predicted spectra for both incompressible & compressible diagnostics in the limit of vanishing controlled numerical dissipation

# 3-D Compressible MHD (Ideal)

$$\begin{bmatrix} \begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho w \\ e \\ B_x \\ B_y \\ B_z \end{pmatrix}_t + \operatorname{div} \begin{pmatrix} \rho \mathbf{u} \mathbf{u}^T + (p + \frac{1}{2}B^2)I - \mathbf{B}\mathbf{B}^T \\ \mathbf{u}(e + p + \frac{1}{2}B^2) - \mathbf{B}(\mathbf{u}^T\mathbf{B}) \\ \mathbf{u}\mathbf{B}^T - \mathbf{B}\mathbf{u}^T \end{bmatrix} = 0$$

Conservative

$$\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho w \\ e \\ B_x \\ B_y \\ B_z \end{pmatrix}_{t} + \operatorname{div} \begin{pmatrix} \rho \mathbf{u} \\ \rho \mathbf{u} \mathbf{u}^T + (p + \frac{1}{2}B^2)I - \mathbf{B}\mathbf{B}^T \\ \mathbf{u}(e + p + \frac{1}{2}B^2) - \mathbf{B}(\mathbf{u}^T\mathbf{B}) \\ \mathbf{u}\mathbf{B}^T - \mathbf{B}\mathbf{u}^T \end{pmatrix} = -(\nabla \cdot \mathbf{B}) \begin{pmatrix} 0 \\ B_x \\ B_y \\ B_z \\ \mathbf{u}^T\mathbf{B} \\ u \\ v \\ w \end{pmatrix}$$

Non-conservative (Symmetrizable - Godunov, Powell)

$$\mathbf{u} = (u, v, w)^{T}$$

$$\mathbf{B} = (B_{x}, B_{y}, B_{z})^{T}$$

$$B^{2} = B_{x}^{2} + B_{y}^{2} + B_{z}^{2}$$

$$p = (\gamma - 1)(e - \frac{1}{2}\rho(u^{2} + v^{2} + w^{2}) - \frac{1}{2}(B_{x}^{2} + B_{y}^{2} + B_{z}^{2}))$$

## Compressible Orszag-Tang Vortex ( $\gamma = 5/3$ )

Density at T=3.14

WAV66+AD8

801 x 801

No Filter on B

X

6

I.C.

$$\begin{pmatrix} \rho \\ u \\ v \\ w \\ p \\ B_x \\ B_y \\ B_z \end{pmatrix} = \begin{pmatrix} 25/9 \\ -\sin y \\ \sin x \\ 0 \\ 5/3 \\ -\sin y \\ \sin 2x \\ 0 \end{pmatrix}$$

**BC: Periodic** 

Domain:  $0 < x < 2\pi$ 

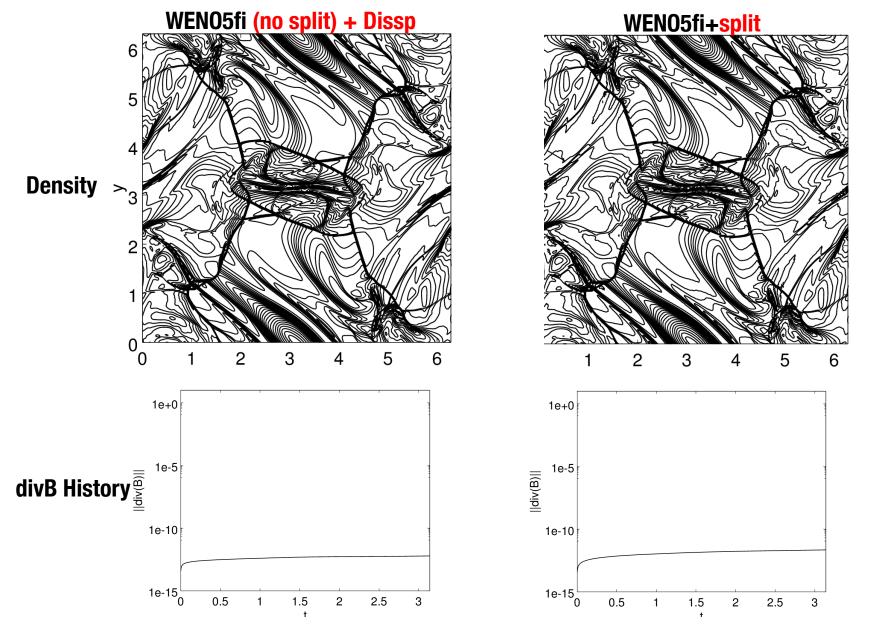
 $0 < y < 2\pi$ 6 0

X

Filter All

5

# Ducros et al. Splitting - Orszag-Tang Vortex Test case (Only on the Gas Dynamic Variables)



# High Order Discrete Conservation Methods (High Order Numerical Fluxes for compressible MHD)

Entropy stable conservative numerical fluxes

Low Order: Janhunen (2000), Winters-Gassner (2016), Chandrasekar-Klingenberg (2015) High Order: Sjogreen-Yee (2009) - Central, Fjordholm, Mishra, & Tadmor (2012) - ENO, etc.

Momentum conservation, Kinetic energy preservation, etc.

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