

Creating a Bimodal Drop-Size Distribution in the NASA Glenn Icing Research Tunnel

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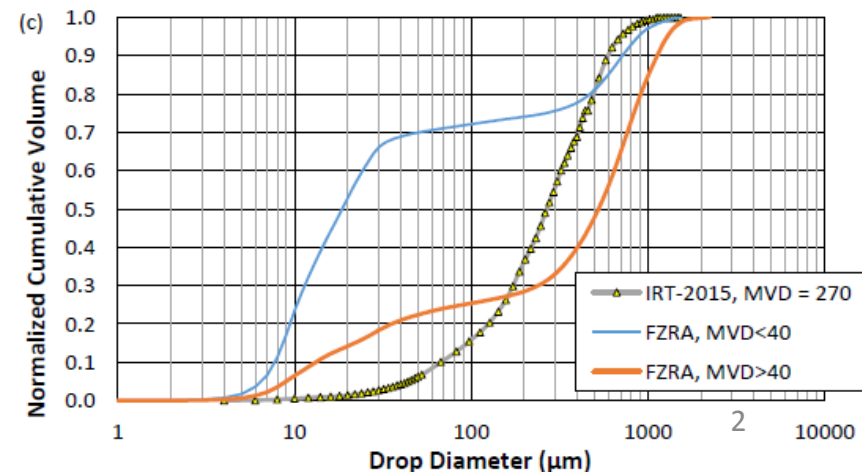
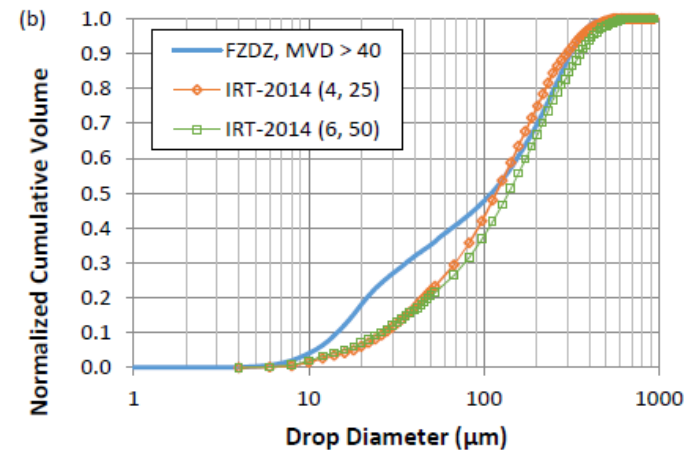
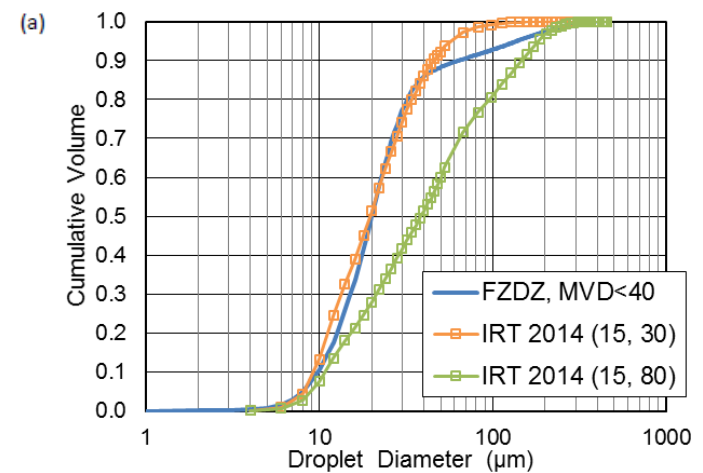
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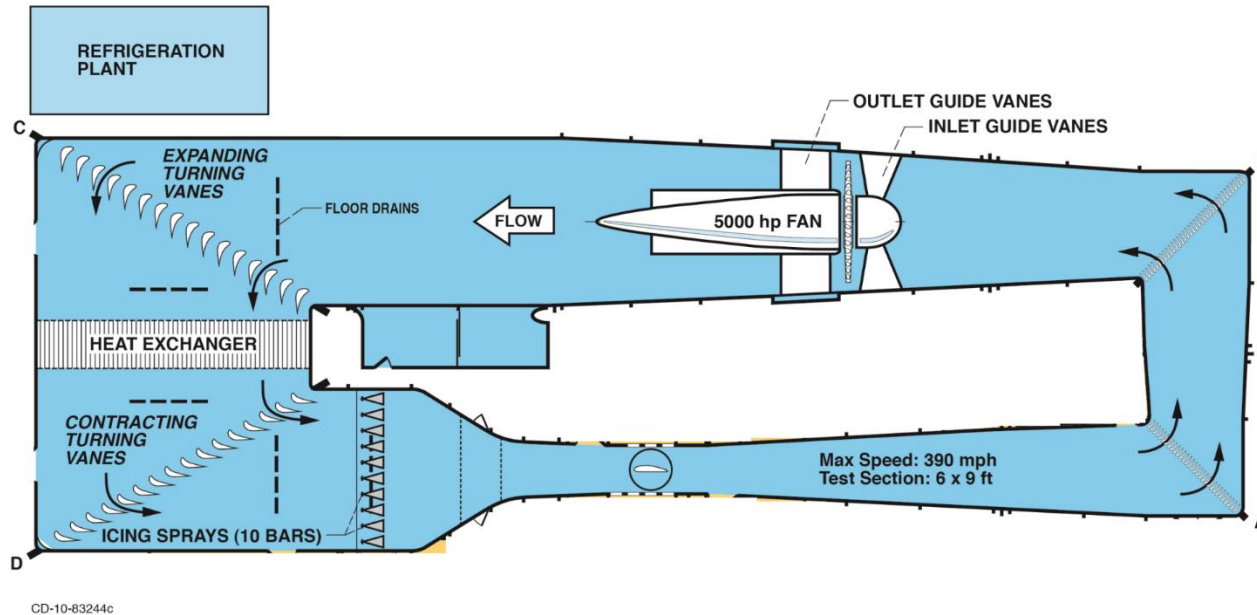
The Problem:

- The FAA's new Appendix O criteria for super-cooled large drops was put into effect in 2015. One of the biggest problems is no facility has shown the ability to create these conditions.
- Appendix O criteria are difficult to create in ground test facilities because of all the parameters that are difficult to match:
 - Large max drop diameter
 - Low liquid water content
 - Bimodality of drop size distribution
 - Trajectories of large drops
 - Temperature of large drops
 - Velocity of large drops
 - Possibility of drop shear
- No experimental facilities also means no validation of icing codes



Test Facility

Icing Research Wind Tunnel



- **Test section size: 6 ft. x 9 ft. (1.8 m x 2.7 m)**
 - All drop-sizing measurements are made in the center of the test section
- **Calibrated test section airspeed range: 50 – 325 kts**
- **Air temperature: -40 degC static to +10 degC total**
- **Calibrated MVD range: 14 – 270 μm**
- **Calibrated LWC range: 0.15 – 4.0 g/m³ (function of airspeed)**
- **Two types of spray nozzles:**
 - Standards = higher water flow rate
 - Mod1 = lower water flow rate

Drop-Sizing Instruments

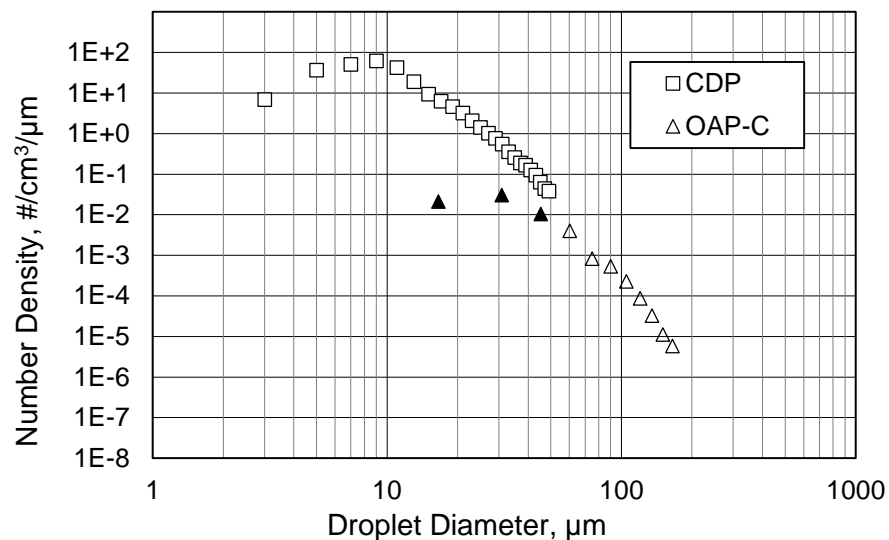
Cloud Droplet Probe (CDP)
(2 – 50 μm)
(Forward Scattering)



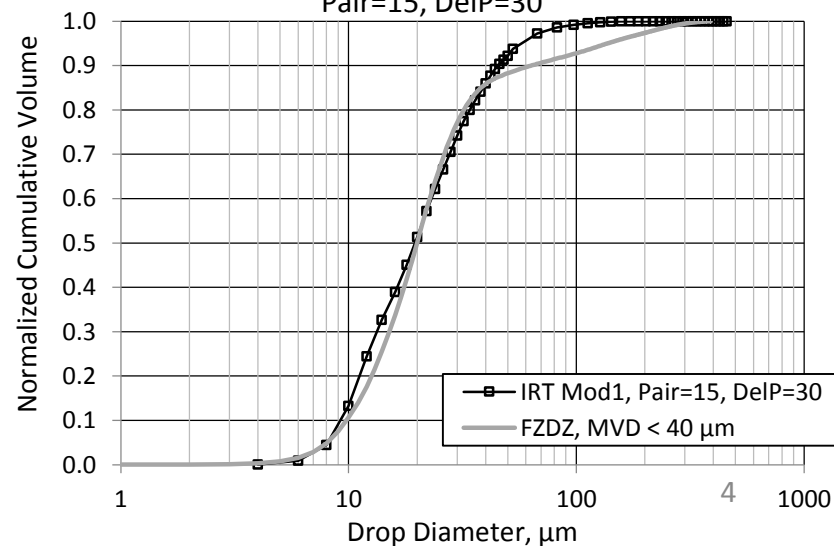
Optical Array Probe (OAP)
(15 – 450 μm)
(Diode Shadowing)



Number Density for Mod1, Pair=15, DelP=30

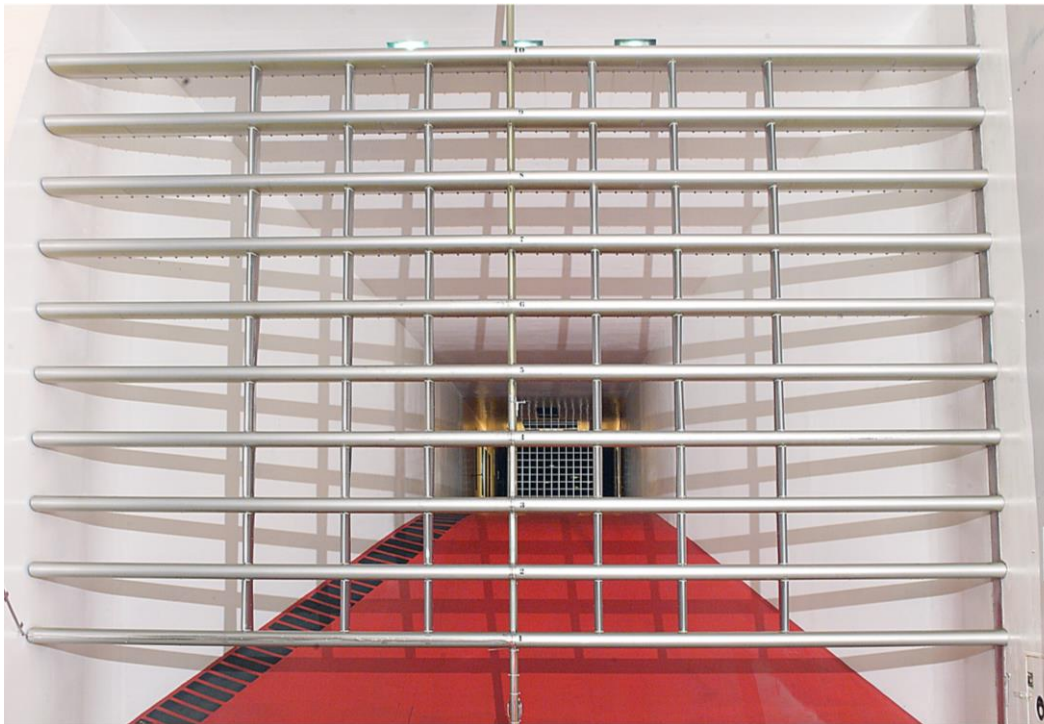


Normalized Cumulative Volume for Mod1,
Pair=15, DelP=30



IRT Drop-Size Measurement Procedures

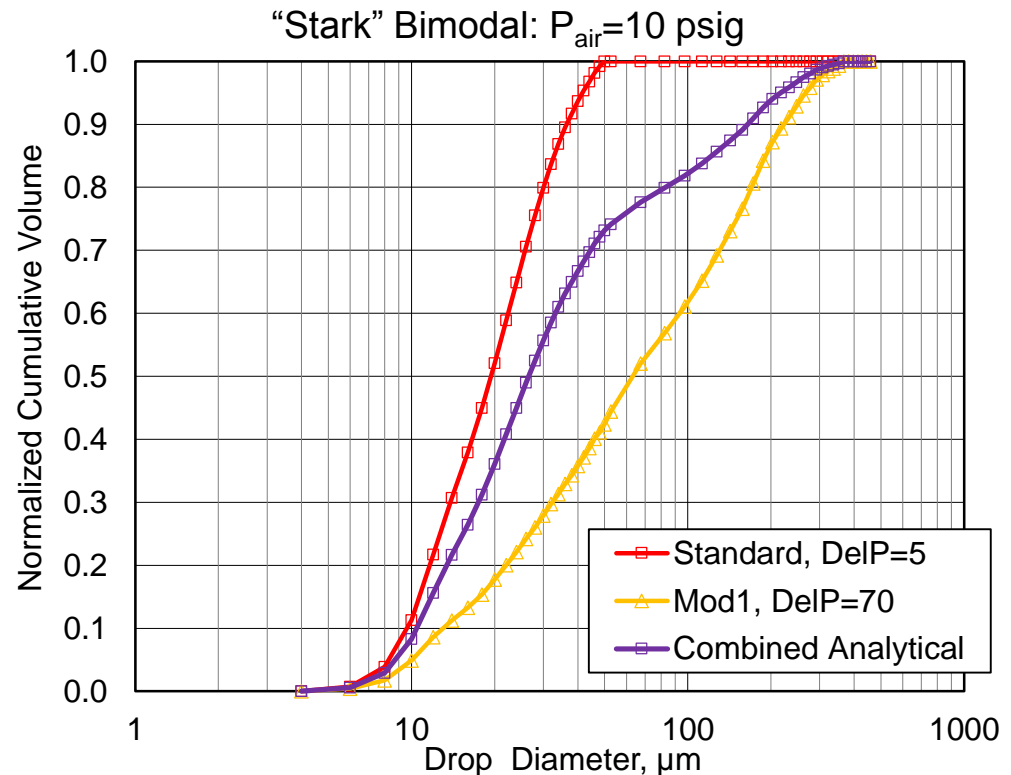
IRT Spraybars (viewed from upstream)



- Drop-size measurements are typically made with only the even- or odd-numbered spraybars
- This reduces number density, which in turn reduces the chances of coincidence error from the probes.
- It is also helpful in testing because spraying less water means the probe is more likely to remain free of ice.
- This is done ONLY for characterizing particle size distribution measurements. A study is done at each full calibration to determine which set of bars are best.

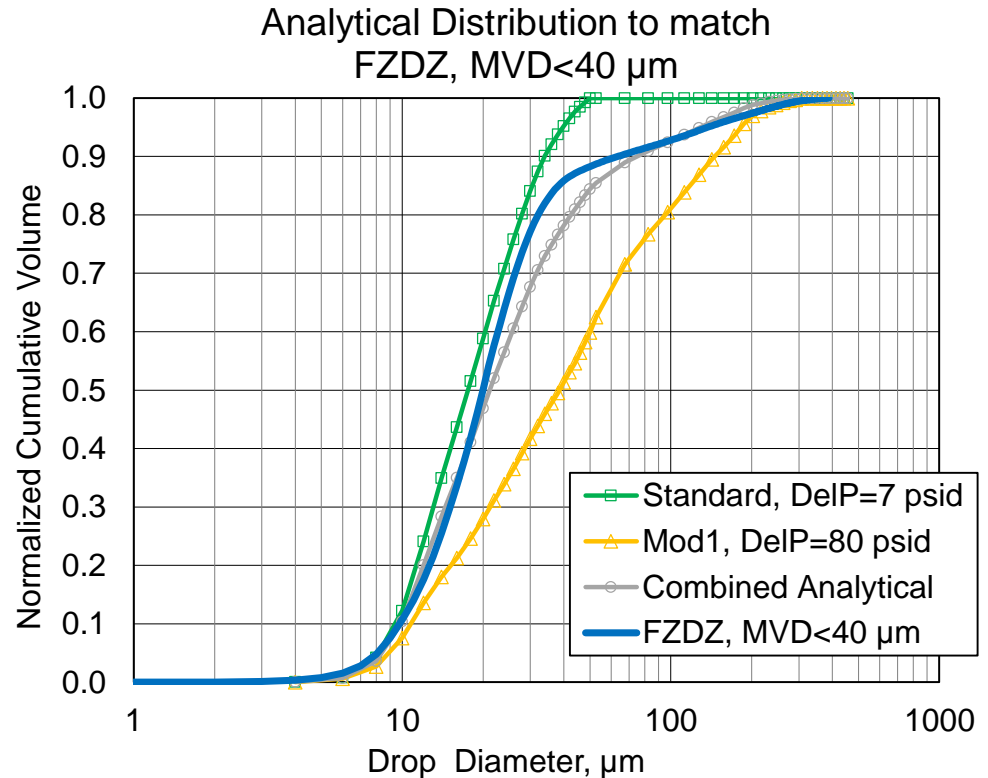
Creating Bimodal Distributions, Analytically

- Superimpose two drop-size distributions (one from Mod1 nozzles, one from Standard nozzles):
 - add the two liquid water contents values for each bin size
 - IRT spraybars have only one air manifold, so both conditions must have the same air pressure.
- Calculate the new total volume
- Normalize LWC in each bin by the new total water content
- Calculate the Normalized Cumulative Volume. Plot against drop size.
- *The “stark” bimodal (right) is the most distinctly bimodal distribution that can currently be created.*



Matching to FZDZ, MVD<40 μm

- We chose from the available IRT measured drop size distributions taken during the cloud calibration
- Requirements: air pressures must match, nozzle types must be different
- Optimized to a condition that was within 10% and matched better to the top 10% of the normalized cumulative LWC

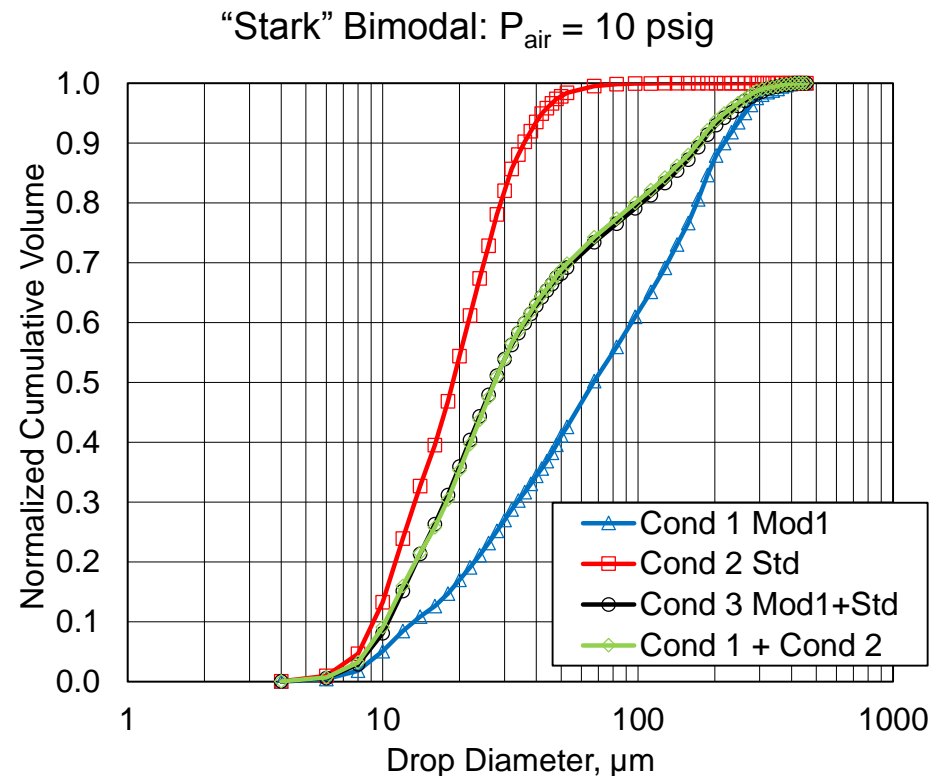


Test Goals

- Measured 4 spray conditions for the FZDZ, $MVD < 40 \mu m$ “match” distribution, and 3 for the “stark” bimodal:
 1. Mod1 nozzles only (mono-modal, even spraybars)
 2. Standard nozzles only (mono-modal, even spraybars)
 3. Mod1 & Standard nozzles together (bimodal), even-numbered spraybars
 4. Mod1 & Standard nozzles together (bimodal), all spraybars
- Compare the simultaneous-spray bimodal to the FZDZ, $MVD < 40 \mu m$ distribution
- Combine the measurements of the two individual sprays and compare the analytical superposition to the measured Mod1 & Standard simultaneous spray
- Compare the even-numbered spraybars to all-spraybars

Results: “Stark” Bimodal

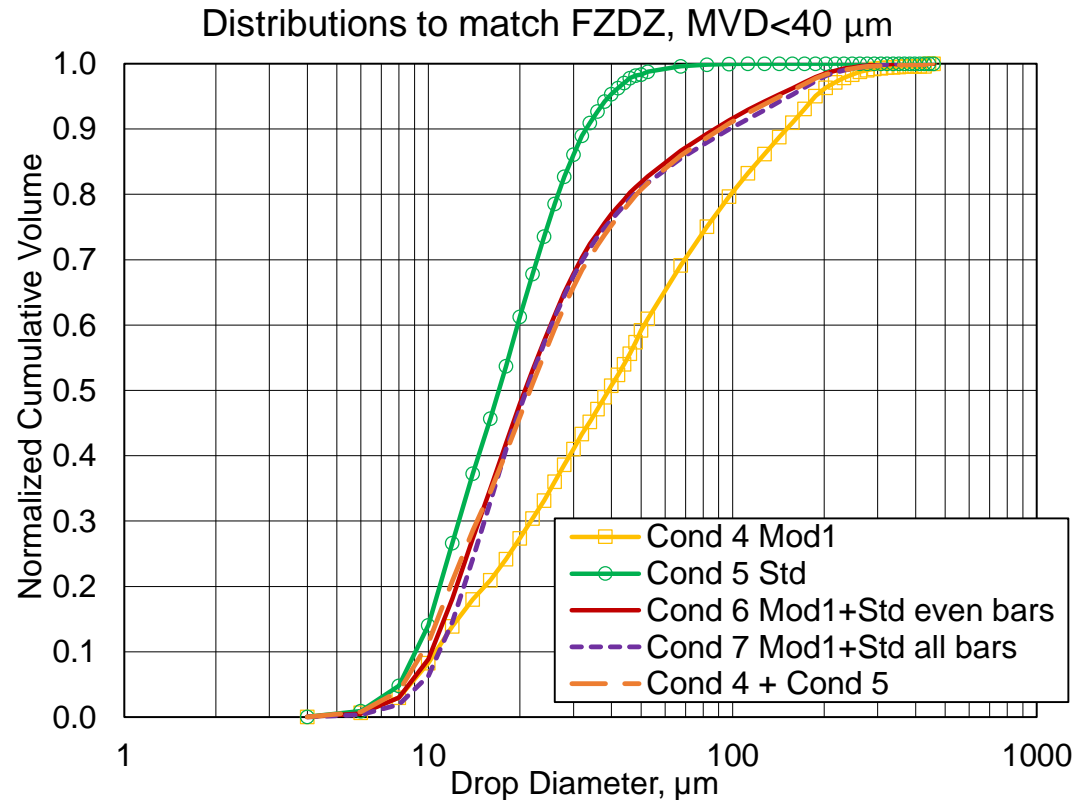
- Compared the analytical sum of the two individual sprays to the distribution measured when everything was sprayed at once



| Compared Distributions | | | Mean Diff. | Max Diff. | Diam. at Max Diff. |
|------------------------------|----|-----------------------------------|------------|-----------|--------------------|
| Pair=10, sum of Mod1 and Std | vs | Pair=10, Mod1+Std expt, even bars | 0.3% | 1.0% | 10 μm |

Results: FZDZ, MVD<40 μm case

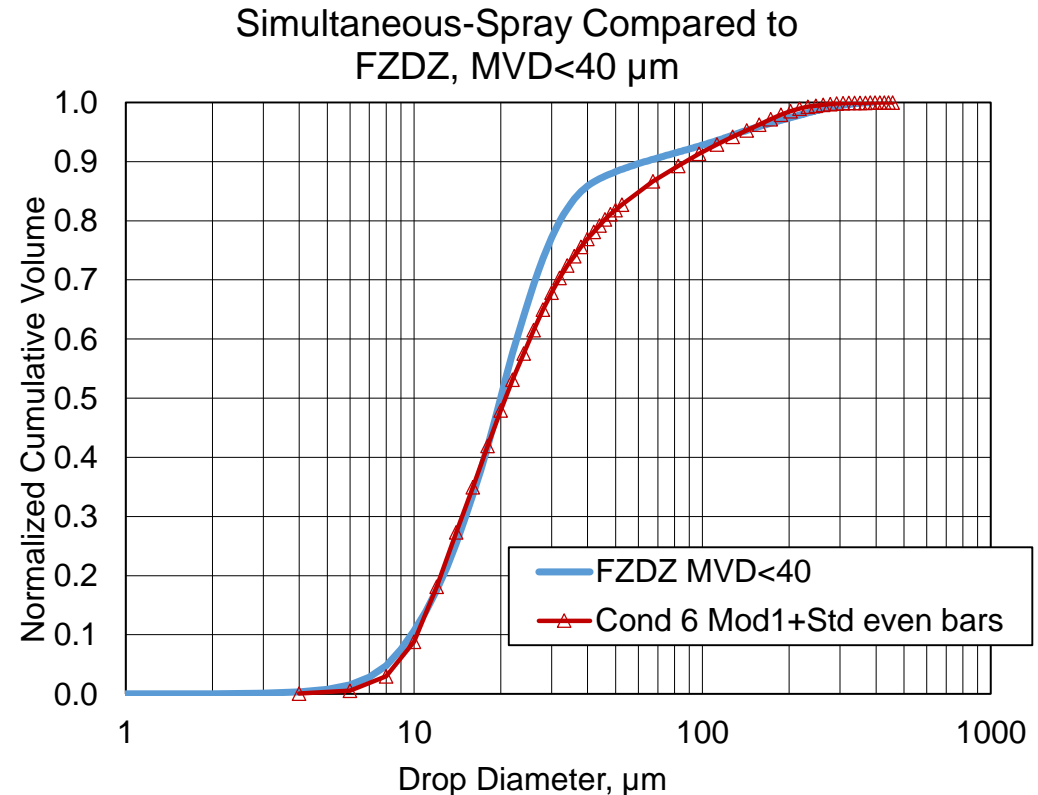
- Compared the analytical sum of the two individual sprays to the distribution measured when everything was sprayed at once
- Also compared spraying even-numbered bars with spraying all bars
- Comparisons were good in both cases



| Compared Distributions | | | Mean Diff. | Max Diff. | Diam. at Max Diff. |
|------------------------------------|----|-----------------------------------|------------|-----------|--------------------|
| Pair=15, sum of Mod1 and Std | vs | Pair=15, Mod1+Std expt, even bars | 0.6% | 2.2% | 26 μm |
| Pair=15, Mod1+Std, expt., all bars | vs | Pair=15, Mod1+Std expt, even bars | 0.7% | 3.5% | 12 μm |

Results: Created condition compared to App O FZDZ, MVD<40 μm

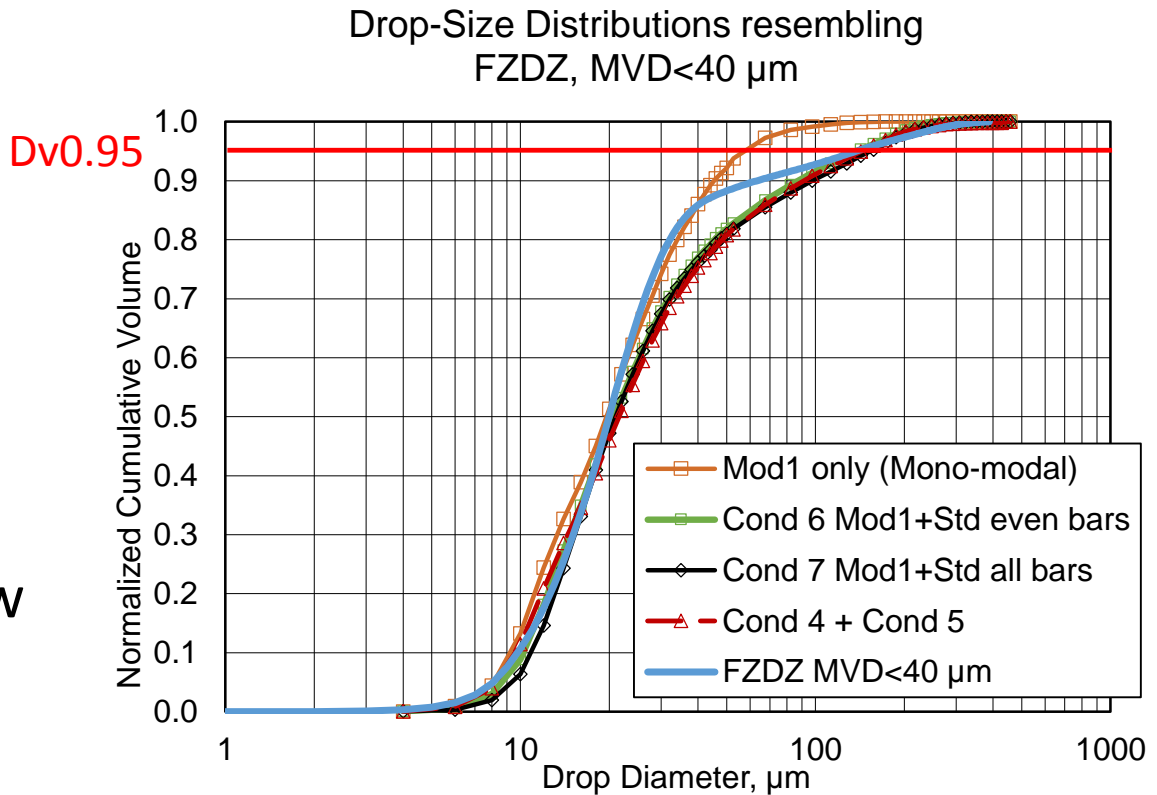
- Compared the distribution measured when everything was sprayed at once to the App O FZDZ MVD<40 μm
- Distributions matched within 10%



| Compared Distributions | | | Mean Diff. | Max Diff. | Diam. at Max Diff. |
|-------------------------------------|----|-----------------------------------|------------|-----------|--------------------|
| App. O., FZDZ, MVD<40 μm | vs | Pair=15, Mod1+Std expt, even bars | 2.7% | 9.6% | 36 μm |

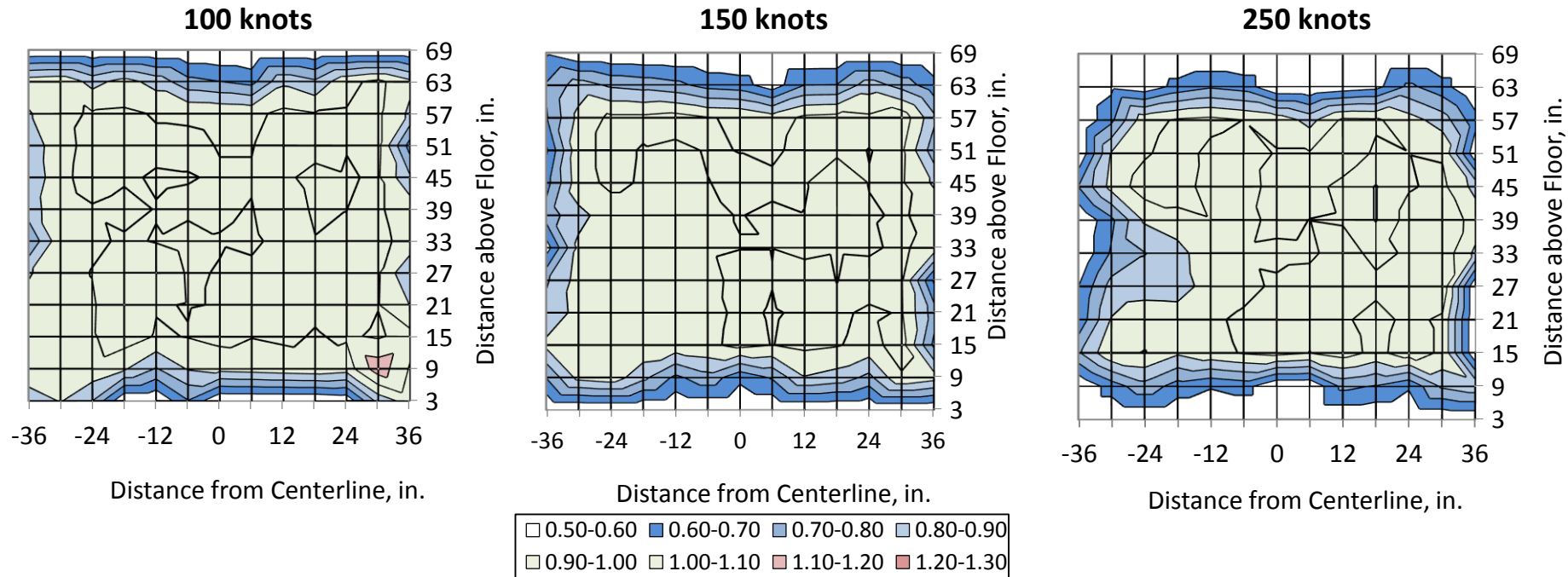
Further comparison

- Now Comparing MVD, Number Density, and Dv0.95
- Slope of curve is shallow in the upper region, so comparing Dv0.95 is tricky
- Number Density is reflective of number & type of nozzles spraying



| Distribution Name | MVD (μm) | Dv0.95 (μm) | Number Density ($\#/\text{cm}^3$) |
|--|-----------------------|--------------------------|-------------------------------------|
| $P_{\text{air}} = 15$, Mod1 nozzles only (mono-modal) | 19.3 | 58.0 | 492 |
| $P_{\text{air}} = 15$, Mod1+Std expt, even bars | 20.8 | 138.4 | 1692 |
| $P_{\text{air}} = 15$, Mod1+Std expt, all bars | 21.0 | 153.8 | 2671 |
| $P_{\text{air}} = 15$, sum of Mod1 and Std | 21.6 | 143.2 | 1670 |
| App. O., FZDZ, MVD<40 μm | 20.0 | 137.1 | -- |

Further Results: Cloud Uniformity



- Used the IRT's 6 ft x 6 ft icing grid to measure cloud uniformity of the FZDZ, MVD<40 μm match at three airspeeds
- Plots show the local LWC ratioed to the average of the center 12 elements
- Cloud uniformity is excellent for all three cases: $\pm 10\%$
- Likely because over half the volume is contributed by the Standard nozzles, which typically have excellent cloud uniformity

Conclusions

- The IRT can create a drop-size distribution that matches Appendix O FZDZ, MVD<40 μm within 10%
- Combining conditions analytically has been proven to compare well with spraying them simultaneously. This suggests that we are not getting drop coalescence, and we can perform similar analyses to predict other bimodal distributions in the IRT.
- Spraying only the even-numbered bars gives a distribution much like spraying all bars.
- Cloud uniformity (at least LWC) for this condition is excellent.

Further Considerations:

- Liquid Water Content for this condition is much too high: at an airspeed of 250 knots it is 1.45 g/m^3 , instead of the desired $0.29 - 0.44 \text{ g/m}^3$.
 - This means that model testing with this drop-size distribution will need to use scaling methods to match the freezing fraction.
- The primary interest is in the effect this drop-size distribution has on an ice shape or ice protection system.
 - This work has been started and progress thus far will be described in the next talk
- There are still many parameters of SLD conditions that remain to be met. This presentation addresses the IRT's current attempts to understand the effect of bimodality.

Questions?

